



### **DEVELOPMENT REVIEW APPLICATION**

Effective 4/17/19

Please check the appropriate box and refer to supplemental forms for submittal requirements. All fees must be paid at the time of application.								
Administrative Decisions	De	ecisions	Requiring a Pul	blic Meeting or Hearing	Policy	Decisions		
☐ Archaeological Certificate (Form P3)		Site Plar orm P1)	n – EPC includin	g any Variances – EPC		☐ Adoption or Amendment of Comprehensive Plan or Facility Plan (Form Z)		
☐ Historic Certificate of Appropriatenes (Form L)	s – Minor	Master E	Development Pla	n (Form P1)		ption or Amendment of ation (Form L)	Historic	
☐ Alternative Signage Plan (Form P3)		Historic orm L)	Certificate of App	oropriateness – Major	☐ Ame	endment of IDO Text (F	form Z)	
Minor Amendment to Site Plan (Form	n P3) 🗆	Demoliti	on Outside of HF	PO (Form L)	☐ Ann	exation of Land (Form 2	Z)	
☐ WTF Approval (Form W1)		Historic	Design Standard	ds and Guidelines (Form L)	□ Ame	endment to Zoning Map	– EPC (Form Z)	
		Wireless orm W2)	Telecommunica	ations Facility Waiver	☐ Ame	endment to Zoning Map	– Council (Form Z)	
					Appea	ls		
					□ Dec	ision by EPC, LC, ZHE	, or City Staff (Form	
APPLICATION INFORMATION								
Applicant: Pam Kearney, As Age	nt				Ph	one: 302-318-123	0	
Address: Scout Services, 490 Qu	ıail Ridge D	rive					outservices.com	
City: Westmont				State: IL	Zip	: 60559		
Professional/Agent (if any):					Ph	Phone:		
Address:					Em	Email:		
City:				State:	Zip	:		
Proprietary Interest in Site:				List all owners:				
BRIEF DESCRIPTION OF REQUEST								
Installation of canopy for emplo	yee shade i	n drive-	thru. No chai	nge to parking. Store v	vill not	close.		
SITE INFORMATION (Accuracy of the	e existing lega	l descrip	tion is crucial!	Attach a separate sheet if	necessa	ıry.)		
Lot or Tract No.: TR D-1-B PLAT (	DF TRS D-1	-A & D-	1-B	Block:	Un	it:		
Subdivision/Addition: Montgomery	Plaza			MRGCD Map No.:	UPC Code: 101706148301640115			
Zone Atlas Page(s): F-17-Z		Existing	Zoning: MX-N	Л	Proposed Zoning: same			
# of Existing Lots:		# of Pro	posed Lots:		To	Total Area of Site (acres): 1.0171		
LOCATION OF PROPERTY BY STREET	ETS				•			
Site Address/Street: 5009 Montgon	nery Blvd NE	Betwee	n: Chick-fil	-A	and:			
CASE HISTORY (List any current or p	-			may be relevant to your re	equest.)			
Was originally approved in 201	1 Main pr	oject #	1000736. His	tory A-1681 & Z-74-81	-1			
Signature:	•	-		<u> </u>		te: 8/4/2020		
Printed Name: Pam Kearney, As Agent □ Applicant or □ Agent								
FOR OFFICIAL USE ONLY								
Case Numbers	Action	n Fees Case Numbers			Action	Fees		
Meeting/Hearing Date:		1		1	Fe	e Total:		
Staff Signature: Date: Project #					oject #			

FORM P3: ADMINISTRATIVE DECISIONS AND MINOR AMENDMENTS A single PDF file of the complete application including all plans and documents being submitted must be emailed to PLNDRS@cabq.gov prior to making a submittal. Zipped files or those over 9 MB cannot be delivered via email, in which case the PDF must be provided on a CD. INFORMATION REQUIRED FOR ALL ADMINISTRATIVE DECISIONS OR AMENDMENTS Letter of authorization from the property owner if application is submitted by an agent Zone Atlas map with the entire site clearly outlined and labeled **ARCHEOLOGICAL CERTIFICATE** Archaeological Compliance Documentation Form with property information section completed Only the information above is required unless the City Archaeologist determines that the application does not qualify for a Certificate of No Effect, in which case a treatment plan prepared by a qualified archaeologist that adequately mitigates any archeological impacts of the proposed development must be submitted and reviewed for a Certificate of Approval per the criteria in IDO Section 14-16-6-5(A)(3)(b) MINOR AMENDMENT TO SITE PLAN - ADMIN, EPC, or DRB Justification letter describing, explaining, and justifying the request per the criteria in IDO Section 14-16-6-4(X)(2) Three (3) copies of all applicable sheets of the approved Site Plan being amended, folded Copy of the Official Notice of Decision associated with the prior approval Three (3) copies of the proposed Site Plan, with changes circled and noted Refer to the Site Plan Checklist for information needed on the proposed Site Plan. Minor Amendments must be within the thresholds established in IDO TABLE 6-4-5. Any amendment beyond these thresholds is considered a Major Amendment and must be processed through the original decision-making body for the request. MINOR AMENDMENT TO SITE DEVELOPMENT PLAN APPROVED PRIOR TO THE EFFECTIVE DATE OF THE IDO Justification letter describing, explaining, and justifying the request per the criteria in IDO Section 14-16-6-4(Y)(1)(a) Three (3) copies of all applicable sheets of the approved Site Development Plan being amended, folded Copy of the Official Notice of Decision associated with the prior approval Three (3) copies of the proposed Site Development Plan, with changes circled and noted Refer to the Site Plan Checklist for information needed on the proposed Site Plan. Minor Amendments must be within the thresholds established in IDO TABLE 6-4-5. Any amendment beyond these thresholds is considered a Major Amendment and must be processed through the original decision-making body for the request. **ALTERNATIVE SIGNAGE PLAN** Proposed Alternative Signage Plan compliant with IDO Section 14-16-5-12(F)(5) Justification letter describing, explaining, and justifying the request per the criteria in IDO Section 14-16-6-5(F)(4)(c) Required notices with content per IDO Section 14-16-6-4(K)(6) Office of Neighborhood Coordination notice inquiry response and proof of emailed notice to affected Neighborhood Association representatives Sign Posting Agreement

I, the applicant or agent, acknowledge that if a scheduled for a public meeting or hearing, if requ		nis application, the application will not be
Signature:		Date: 8/4/2020
Printed Name: Pam Kearney, As Agent		☐ Applicant or ☐ Agent
FOR OFFICIAL USE ONLY		
Project Number:	Case Numbers	THE PARTY OF THE P
	-	
	-	
	<del>-</del>	1706
Staff Signature:		MEXICA
Date:		

### Bernalillo County Assessor Parcels:

UPC 101706148301640115

Tax Year 2020

MONTGOMERY PLAZA Owner

PARTNERS LLC

Legal TR D-1-B PLAT OF TRS D-1-A &

Description D-1-B MONTGOMERY PLAZA

(BEINGA REPL OF TR D-1 MONTGOMERY PLAZA) CONT

1.0171 AC

Owner

Complete 100 SUN AVE NE SUITE 100

ALBUQUERQUE NM 87109

Address

Complete 5009 MONTGOMERY BLVD NE

Site

ALBUQUERQUE NM 87109

Address



### IDO Zone Info

IDO Zone District MX-M

IDO District Moderate Intensity

Definition

IDO Category Mixed-Use

IDO Use Table URL More info

Last Update Date 7/28/2017

Old Zoning SU-1

Designation

Old Zoning C-2 WITH

Description WAREHOUSING

### Platted Parcels (AGIS)

Full Address 5001 MONTGOMERY BLVD NE

Lot D1A Block 0000

Subdivision MONTGOMERY PLAZA

PIN ABQ61202

### Platted Parcels (AGIS)

Full Address 5009 MONTGOMERY BLVD NE

Lot D1B

Block 0000

Subdivision MONTGOMERY PLAZA

PIN ABQ213744



September 27, 2019 Letter of Authorization

Chick-Fil-A Inc. 5200 Buffington Rd. Atlanta, GA 30349

To Whom It May Concern,

Chick-fil-A, Inc. authorizes Scout Services and their representatives, specifically Pam Kearney, to represent the company in matters associated with the permitting of Drive Thru Canopies at its various locations around the country

Sincerely,

Sr. Principal Project Lead, Existing Restaurants

State of Georgia County of Dekalb

Signed and sworn to (or affirmed) before me on About 7, 2019 (name(s) of individual(s) making statement), who proved to M. Troy Tripp me on the basis of satisfactory evidence to be the person(s) who appeared before me.

Personally Known Produced Identification

My commission expires:

Type of ID

Seal/Stamp

Sydnik H Guest

(Notary name, typed, stamped or

printed)

Notary Public, State of Georgia

 From:
 Rodenbeck, Jay B.

 To:
 Pam Kearney

 Cc:
 Trujillo, Concetta M.

Subject: RE: Help Needed with Administrative Amendment BP-2020-25270

**Date:** Wednesday, July 22, 2020 6:47:50 PM

Attachments: <u>image003.png</u>

image004.png image005.png

DRB EPC application.pdf

FormP3.pdf

### Pam,

For an Administrative Amendment application, you need to submit the following to our office **via email** at this time due to the Coronavirus:

- 1. Filled out and signed/dated application sheets (attached to this message).
- 2. Letter of authorization from the property owner if application is submitted by an agent.
- 3. Zone Atlas map with the entire site clearly outlined and labeled (go to the following web-site to obtain the required map: <a href="https://cabq.maps.arcgis.com/home/webmap/viewer.html?">https://cabq.maps.arcgis.com/home/webmap/viewer.html?</a> webmap=f12cf8ebe9514a2d8d09e2c7a095d2f4).
- 4. Justification letter describing, explaining, and justifying the request per the criteria in IDO Section 14-16-6-4(X)(2).
- 5. A copy of all applicable sheets of the approved Site Plan being amended (that Concetta sent you).
- 6. Copy of the Official Notice of Decision associated with the prior approval.
- 7. A copy of the proposed Site Plan, with changes circled and noted.
- 8. A PDF file of the complete application, including all plans and documents, emailed to <a href="mailto:PLNDRS@cabq.gov">PLNDRS@cabq.gov</a>, mgould@cabq.gov, and <a href="mailto:jrodenbeck@cabq.gov">jrodenbeck@cabq.gov</a>. If the file size is over 9 megabytes in size, please send us the submission via WeTransfer at <a href="https://wetransfer.com/">https://wetransfer.com/</a>.

The application fee is \$50. You can pay the fee online (the preferable option at this time) or pay via check, with the check mailed to:

City of Albuquerque Planning Department C/O Maggie Gould or Jay Rodenbeck 600 2<sup>nd</sup> Street NW Ground Floor Albuquerque, NM 87102

You can pay online once you have submitted your Administrative Amendment application and our office has confirmed reception. Our clerks will direct you to this option at that time if desired.

### WeTransfer Instructions:

You will initially be directed to a page which gives you the option of going to the free version of the site (send up to 2 GB at a time), or the subscription-based version of the site (send up to 20 GB at a time). Click on the link to the free version of the site, and you will be directed to the free version of

the site (a screenshot of the WeTransfer webpage is attached). You just add the email address(es) to send files to, add your files and a message of what you're sending, then click the "Transfer" icon.

When you receive files from a sender on WeTransfer, you will receive an email from the sender. Within the email message is an icon labeled "Get your files" that you click on to download the files from the sender (a screenshot of an email from a sender is attached). Once you click on that icon, a webpage appears with a "Download" icon. Just click on the "Download" icon, and the files sent to you will then download onto your computer. Once you download the files, you can place them where you want. If the sender sends more than one file to you, you will be send a Zip file which you will have extract the individual files from.



### **Jay Rodenbeck**

Planner

o 505.924.3994

e irodenbeck@cabq.gov

cabq.gov/planning

From: Pam Kearney <pkearney@scoutservices.com>

**Sent:** Wednesday, July 22, 2020 3:34 PM

**To:** Rodenbeck, Jay B. <jrodenbeck@cabq.gov> **Cc:** Trujillo, Concetta M. <cmtrujillo@cabq.gov>

**Subject:** Help Needed with Administrative Amendment BP-2020-25270

Jay,

Can you help me with this Information today?

Thank you,

Pam

Pam Kearney 302-318-1230

866-504-3888 x106

**Scout Services** 

490 Quail Ridge Dr. Westmont. IL 60559



### FIND US ONLINE

Visit us at www.scoutservices.com



From: Trujillo, Concetta M. <<u>cmtrujillo@cabq.gov</u>>

Sent: Wednesday, July 22, 2020 12:41 PM

**To:** Pam Kearney < <u>pkearney@scoutservices.com</u>> **Cc:** Rodenbeck, Jay B. < <u>jrodenbeck@cabq.gov</u>>

**Subject:** RE: Resubmit Task Submission Complete for BP-2020-25270

Good Morning Pam,

You need to apply for an Administrative Amendment to the site plan on file. I am added Jay Rodenbeck to the email. He will be able to assist you with this process.

Jay- Can you assist Pam with an AA to add a Canopy to the Drive-Thru. She currently has this project in for permitting.

Thanks, Concetta



### **CONCETTA TRUJILLO**

zoning plan examiner

o 505.924.3833

e cmtrujillo@cabq.gov

cabq.gov/planning

From: Pam Kearney [mailto:pkearney@scoutservices.com]

Sent: Wednesday, July 22, 2020 11:05 AM

To: Trujillo, Concetta M.

Subject: FW: Resubmit Task Submission Complete for BP-2020-25270

Importance: High

Hi, Concetta.

I need your help with this please.

It was rejected on ProjectDox with our resubmittal.

This is the Site Plan that was originally approved in 2011.

What is needed in order to clear your comments? I have not received a reply to any of the emails that I've sent.

Your help would really be appreciated, Pam

Pam Kearney 302-318-1230

866-504-3888 x106

Scout Services

490 Quail Ridge Dr. Westmont. IL 60559



### FIND US ONLINE

Visit us at <u>www.scoutservices.com</u>



From: Pam Kearney

**Sent:** Monday, July 20, 2020 4:07 PM

To: jrodenbeck@cabq.gov

Cc: Gomez, Ernest P. <epgomez@cabq.gov>; rbrito@cabq.gov; Tena, Victoria C. <vtena@cabq.gov>

**Subject:** Resubmit Task Submission Complete for BP-2020-25270

**Importance:** High

Good Afternoon, Jay.

I was told that you might be able to help us.

We have an application in for a canopy in the drive-thru of a Chick-fil-A.

When we did the due diligence for this project, we were told that there were not any Planning or

Zoning reviews needed.

I just resubmitted our project to ProjectDox.

One of the comments referred to an Administrative Amendment.

Concetta advised us that we needed to locate the site plan that was approved originally in 2011. Chick-fil-A was able to locate the attached that was submitted then and provide it.

I am attaching that here, but also included it in the resubmittal.

Is this enough to take care of these comments referring to the Administrative Amendment?

Your help in solving would be greatly appreciated, Pam

Pam Kearney 302-318-1230

866-504-3888 x106

Scout Services

490 Quail Ridge Dr. Westmont. IL 60559



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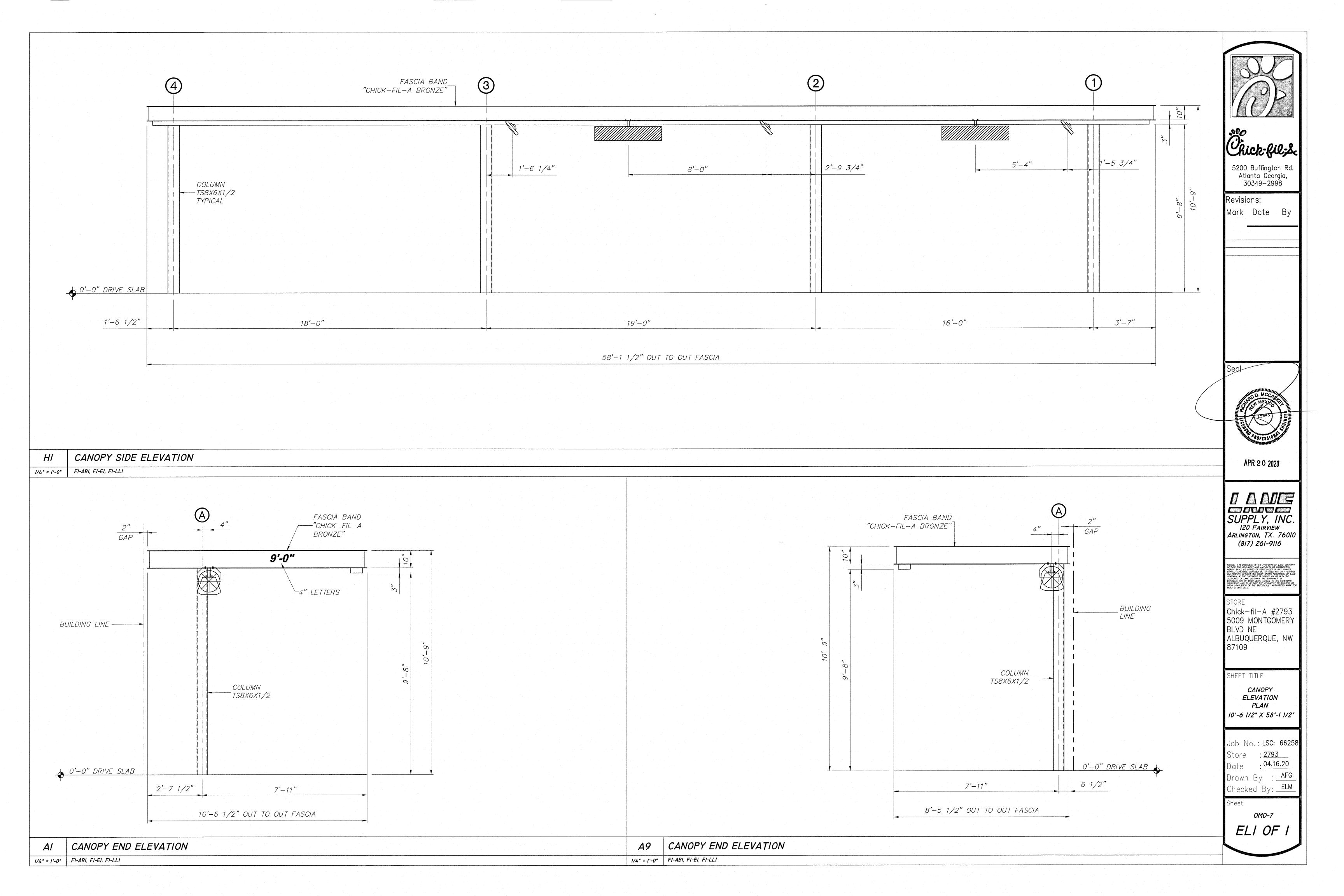


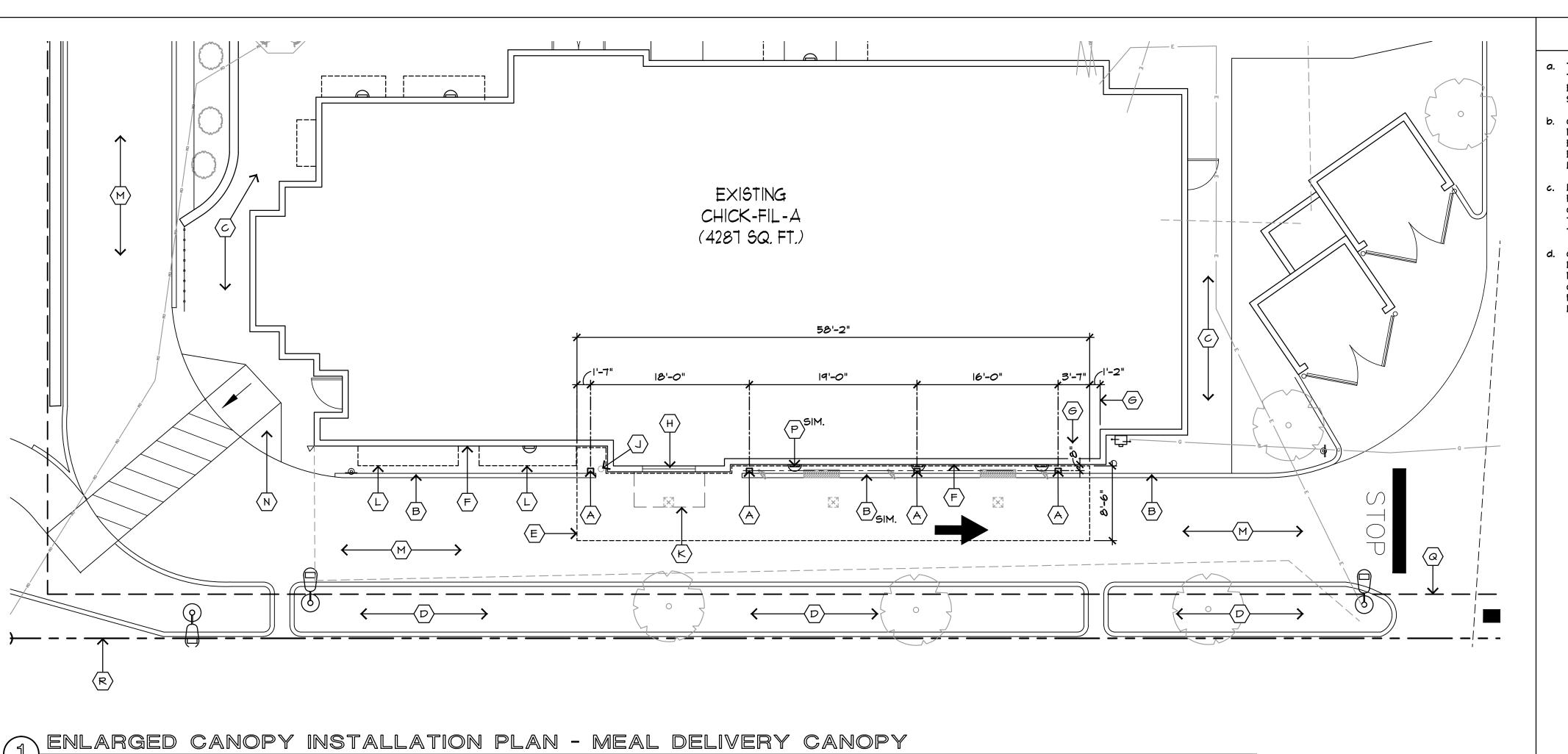
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This message has been analyzed by Deep Discovery Email Inspector.

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This message has been analyzed by Deep Discovery Email Inspector.





SEE STRUCT. DRAWINGS

## GENERAL NOTES

- a. THE DIMENSIONS SHOWN ON THESE DRAWINGS ARE TO CENTER OF COLUMN LINE ONLY AND HAVE BEEN ESTABLISHED IN ACCORDANCE WITH CHICK-FIL-A STANDARD DESIGN GUIDELINES.
- b. COLUMNS SHALL BE INSTALLED IN A MANNER AS NOT TO DISTURB THE EXISTING EXTERIOR BUILDING FOUNDATIONS NOR UNDERMINE THE EXISTING EXTERIOR BUILDING STEM WALLS/FOOTINGS.
- WHERE AN OFFSET CAISSON FOOTING OR SPREAD FOOTING IS REQUIRED, THE G.C SHALL COORDINATE THE EXISTING FIELD CONDITIONS TO THE CANOPY FABRICATOR FOR APPROVAL PRIOR TO INSTALLATION OF THE FOOTINGS.
- d. COLUMNS NEEDING TO BE RELOCATED INTO THE DRIVE LANE OR TEAM WALK WAY, THE G.C. SHALL NOTIFY THE FIELD CONSTRUCTION MANAGER TO GAIN PROPER APPROVAL FROM CHICK-FIL-A PRIOR TO COMMENCEMENT OF SAID CONSTRUCTION WORK

# ⟨-⟩CONSTRUCTION NOTES - MEAL DELIVERY

- A. NEW SHADE CANOPY STEEL SUPPORT COLUMN WITH CONCRETE FOOTING BELOW.
  SEE STRUCTURAL DRAWINGS FOR FURTHER DETAILS. EXISTING CONCRETE /
  LANDSCAPING TO BE REPAIRED OR REPLACED AS REQUIRED PROVIDE FLUSH
  TRANSITION BETWEEN NEW AND EXIST. CONC. SURFACES.
  - B. EXISTING CONCRETE CURB TO REMAIN. SAW CUT AND REMOVE PORTION OF CURB AS REQUIRED FOR INSTALLATION OF NEW FOOTING. UPON FOOTING INSTALLATION G.C. SHALL PATCH AND REPAIR EXIST. CURB AS REQUIRED. PROVIDE SMOOTH TRANSITION BETWEEN NEW AND EXIST. CONC. CURB. G.C. SHALL REPLACE ANY KNOWN CRACKED OR DAMAGED ON SITE CONC. CURBING
  - C. EXISTING CONCRETE WALKWAY TO REMAIN
  - D. EXISTING LANDSCAPING AREA TO REMAIN.
  - E. DASHED LINE INDICATING OUTLINE OF OVERHEAD CANOPY. REFER TO CANOPY SHOP DRAWINGS WITH-IN THIS SET.
  - F. FACE OF EXISTING EXTERIOR BUILDING WALL. DO NOT DISTURB.
  - G. X/Y DIMENSION SHOWN FOR ILLUSTRATIVE PURPOSES ONLY. GC TO FIELD VERIFY EXACT LOCATION AND NOTIFY CHICK-FIL-A PROJECT TEAM IF CANOPY LOCATION CHANGES AND IMPACTS OTHER CONSTRUCTION RELATED CONDITIONS.
  - H. EXISTING MEAL DELIVERY PICK UP WINDOW. DO NOT DISTURB.
- J. EXISTING BOLLARD TO BE REMOVED.
- K. DASHED LINE INDICATING EXISTING AWNING TO BE REMOVED. GC TO REPAIR EXIST. EXTERIOR WALL AS REQUIRED APPLY TOUCH-UP PAINT FIELD MATCH EXIST. COLOR AND WALL FINISH. PROVIDE FLUSH TRANSITION FOR ALL PATCH WARD
- L. EXISTING AWNING TO REMAIN, NO CHANGE.
- M. EXISTING DRIVE THRU LANE TO REMAIN.
- N. EXIST. A.D.A. COMPLIANT CONC. CURB RAMP TO REMAIN. DO NOT DISTURB.
- P. EXISTING SECURITY LIGHTS TO REMAIN.
- Q. EXISTING BUILDING SETBACK LINE SHOWN FOR REFERENCE.
- R. EXISTING PROPERTY LINE SHOWN FOR REFERENCE.

# REFERENCE:

SCALE: 1/8" = 1'-



# **GENERAL NOTES**

- a. THE DIMENSIONS SHOWN ON THESE DRAWINGS ARE TO CENTER OF COLUMN LINE ONLY AND HAVE BEEN ESTABLISHED IN ACCORDANCE WITH CHICK-FIL-A STANDARD DESIGN GUIDELINES.
- NOT TO DISTURB THE EXISTING EXTERIOR
  BUILDING FOUNDATIONS NOR UNDERMINE THE
  EXISTING EXTERIOR BUILDING STEM
  WALLS/FOOTINGS.
- c. WHERE AN OFFSET CAISSON FOOTING OR SPREAD FOOTING IS REQUIRED, THE G.C SHALL COORDINATE THE EXISTING FIELD CONDITIONS TO THE CANOPY FABRICATOR FOR APPROVAL PRIOR TO INSTALLATION OF THE FOOTINGS.
- d. COLUMNS NEEDING TO BE RELOCATED INTO THE DRIVE LANE OR TEAM WALK WAY, THE G.C. SHALL NOTIFY THE FIELD CONSTRUCTION MANAGER TO GAIN PROPER APPROVAL FROM CHICK-FIL-A PRIOR TO COMMENCEMENT OF SAID CONSTRUCTION

# **\*** CONSTRUCTION NOTES - FACE TO FACE

- NEW SHADE CANOPY STEEL SUPPORT COLUMN WITH CONCRETE FOOTING BELOW. SEE STRUCTURAL DRAWINGS FOR FURTHER DETAILS. EXISTING CONCRETE / LANDSCAPING TO BE REPAIRED OR REPLACED AS REQUIRED PROVIDE FLUSH TRANSITION BETWEEN NEW AND EXIST. CONC. SURFACES.
- 2. EXISTING CONCRETE CURB TO REMAIN. SAW CUT AND REMOVE PORTION OF CURB AS REQUIRED FOR INSTALLATION OF NEW FOOTING. UPON FOOTING INSTALLATION G.C. SHALL PATCH AND REPAIR EXIST. CURB AS REQUIRED. PROVIDE SMOOTH TRANSITION BETWEEN NEW AND EXIST. CONC. CURB. G.C. SHALL REPLACE ANY KNOWN CRACKED OR DAMAGED ON SITE CONC. CURBING (TYP.).
- 3. EXISTING CONCRETE WALKWAY TO REMAIN.
- 4. EXISTING LANDSCAPING AREA TO REMAIN.
- 5. NEW 24" WIDE TEAM MEMBER DEMARCATION STRIPING. USE TRAFFIC RATED PAINT. MIN. (2) COATS.
- 6. FACE OF EXISTING EXTERIOR BUILDING. WALL DO NOT DISTURB.
- 7. X/Y DIMENSION SHOWN FOR ILLUSTRATIVE PURPOSES ONLY. GC TO FIELD VERIFY EXACT LOCATION OF COLUMN STARTING POINT. NOTIFY CHICK-FIL-A PROJECT TEAM OF ANY DISCREPANCIES IMPACTING OTHER CONSTRUCTION PHASES OR RELATED CONDITIONS.
- 8. EXISTING DRIVE THRU ORDER POINT MENU BOARD. DO NO DISTURB.
- 9. EXISTING CLEARANCE BARS TO REMAIN. DO NOT DISTURB.
- IO. DASHED LINE INDICATING OUTLINE OF OVERHEAD CANOPY. REFER TO CANOPY DRAWINGS WITHIN-IN THIS SET.
- II. EXISTING BUILDING SETBACK LINE SHOWN FOR REFERENCE.
- 12. EXISTING PROPERTY LINE SHOWN FOR REFERENCE.

# REFERENCE:

SCALE: 1/8" = 1'-0".







ATLANTA, GEORGIA 30349

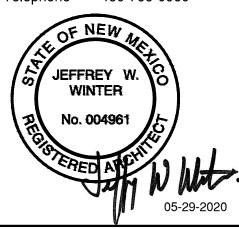
(404) 765-8000

THESE PLANS AND SPECIFICATIONS, AS WELL AS CHICK-FIL-A, INC. NAME AND LOGO, TRADEMARKS AND DESIGNS ARE THE EXCLUSIVE PROPERTY OF CHICK-FIL-A CORPORATION. ANY REPRODUCTION, MODIFICATION, DISCLOSURE AND/OR USE OF THESE MATERIALS (OR ANY PORTION OF THEM) WITHOUT CHICK-FIL-A'S PRIOR WRITTEN CONSENT



IS STRICTLY PROHIBITED.

1743 E. McNair Drive, Suite 200 Tempe, Arizona 85283 Telephone 480-755-0959



Revision Schedule

Rev Date By Description

# CANOPY PROGRAM ICK-FIL-A ORE #2793 AONTGOMERY BLVD. NI QUERQUE, NM 87109

Issue Date: 05-29-2020

Drawn By: GA

Job Number: 19060

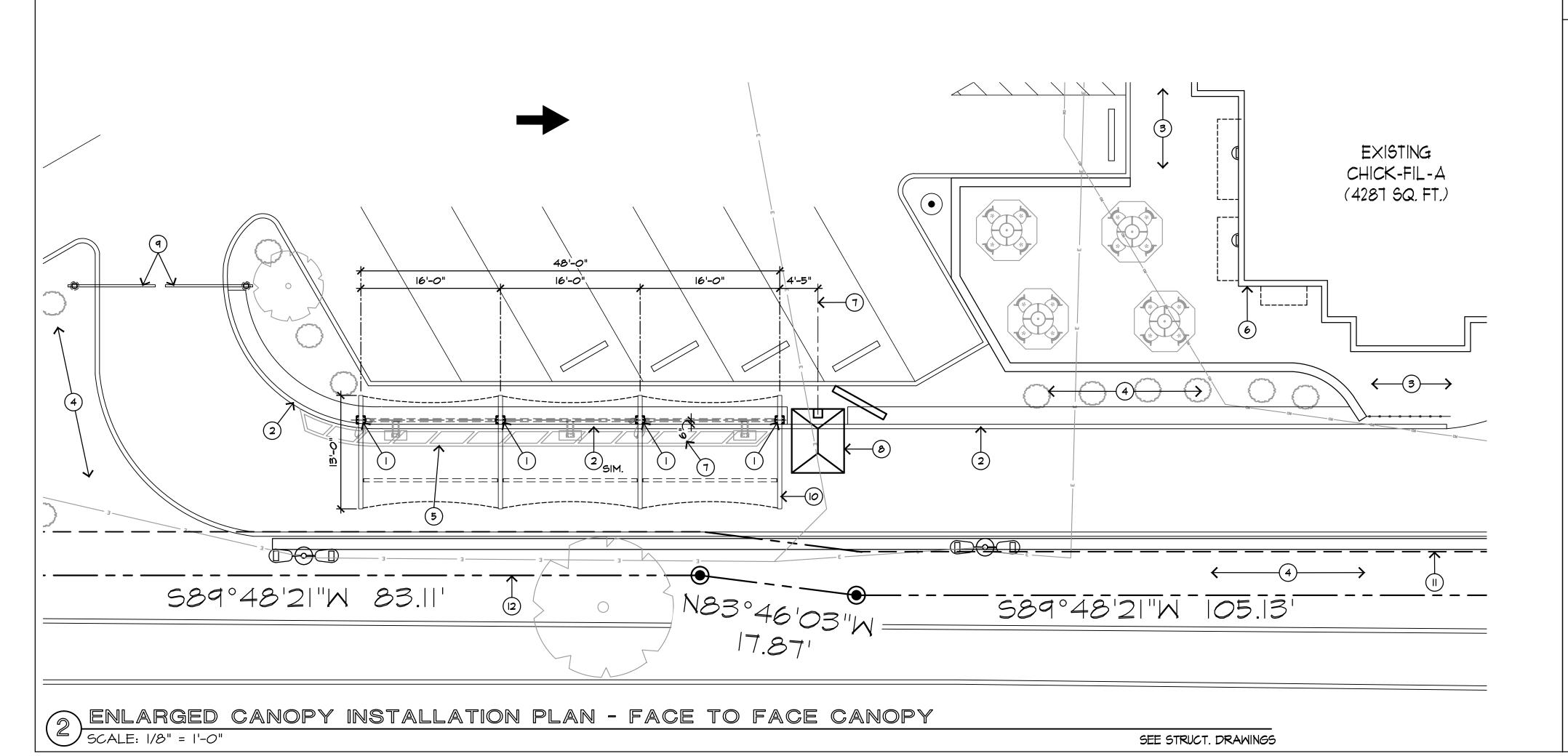
Sheet Title:

Enlarged Canopy Plan

Sheet Number:

**A-2** 

As indicated



SCALE: 1/8" = 1'-0"





120 Fairview Arlington, TX 76010 817-261-9116

### **DESIGN CALCULATIONS FOR:**

Chick-fil-A #2793 Outside Meal Delivery Canopy 5009 Montgomery Blvd NE Albuquerque, NM

Four-Column Canopy:

10'-2" X 57'-9" Canopy

Lane Reference Number:

LSC-66258

Date:

20-Apr-20

### **TABLE OF CONTENTS:**

Canopy Calculations:

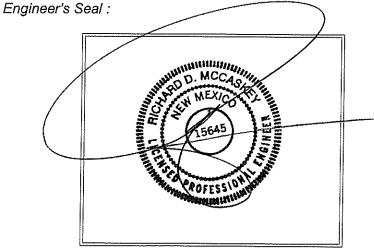
Design Loads: 1-2 Deck Design: 3-5 Purlin Design: 6-9 Header Design: 10-13

Column & Foundation Design:

14-16

### Attachments:

Lane SL-316 Deck Panel Properties Lane Standard Cap Plate Design Lane Standard Base Plate Design Design Sketch



APR 20 2020

Calculations By: Lane Supply, Inc. LSC -66258 Customer: Chick-fil-A #2793 Outside Meal Delivery Canopy By: JMCP 10'-2" X 57'-9" Canopy Project: Check: Code: 2015 International Building Code Roof Loads: Dead Load = 3.00 psf (SL-316 Deck) Live/Snow Load = 20.00 psf TOTAL = 23.00 psf Fascia Load: Height = 10.00 in. Dead Load = 5.83 plf Wind Loads: Risk Category = П V, ULT Speed = 116 m.p.h. Exp С V, ASD Speed = 90 m.p.h. Exp C Height = 15 ft Kd =0.85 Kh = 0.85 G = 0.85 qz =14.93 psf Lateral Load =  $1.0 (H) \cdot qz =$ 16.00 psf Deck Uplift =  $-1.7 (V) \cdot G \cdot qz =$ -21.58 psf Frame Uplift =  $-1.1 (V) \cdot G \cdot qz =$ -13.96 psf Base Shear: V =  $CS \cdot W =$ 0.340 • W Site Class = D Ss(0.2) =0.44 S1(1.0) =0.13 Fa = 1.45 Fv = 2.27 SM1 = Fv•S1 = 0.30 SMS = Fa•Ss = 0.64 SD1 =  $2/3 \cdot SM1 =$ 0.20 SDS = 2/3•SMS = 0.43 R= 1.25 Risk Category = Н CS = (SDS/R) =0.340 (12.8-2)Seismic Design Category Based on SDS: С Seismic Design Category Based on SD1: D

Design Category: D

### Section 7.1--Symbols & Notation

Ce = 1.2 Exposure Factor as determined from Table 7-2 Ct = 1.2 Thermal factor as determined from Table 7-3

D = Snow Density in pcf as determined from Eq. 7-4

hb = Height of balanced snow load determined by dividing Pf by D, in feet.

hd = Height of snow drift, in feet

hc = Clear height from top of balanced snow to top of parapet, ft

hr = 0.83 = Fascia height, ft

Is = 1.0 = Importance factor (see Table 7-4).

Pf = Snow load on flat roofs, psf.

Pg = 20 =ground snow, psf.

Pd = Maximum intensity of drift surcharge load, psf.

lu = 10.541667 = Length of roof upwind of the drift, feet

w = Width of snow drift, in feet

### Section 7.3--Flat-Roof Snow Loads, Pf

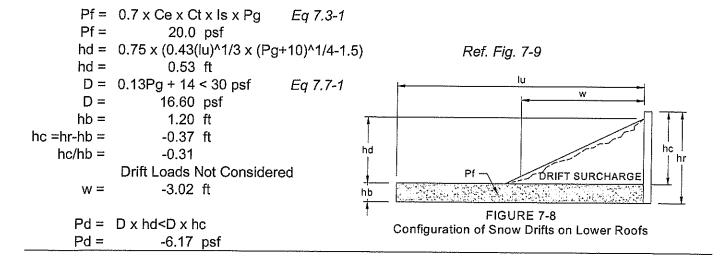
The snow load, Pf, on a roof with a slope equal to or less than 15° shall be calculated in psf using equation 7.3-1, but not less than the following minimum values for low slope roofs: where Pg is 20 psf or less Pf = I(Pg), where Pg exceeds 20 psf, Pf = I(Pg).

### Section 7.7 & Section 7.8

The geometrey of the surcharge load due to snow drifting shall be approximated by a triangle as shown in figure 7-8. Drift loads shall be superimposed on the balanced snow load. If hc/hb is less than 0.2, drift loads are not required to be applied. The height of such drifts shall be taken as 0.75 x hd as determined from Fig 7-9, with lu equal to the length of the roof upwind of the projection or parapet wall. If the side of a roof projection is less than 15 ft long, a drift load is not required to be applied to that side. If the height, hd, is equal to or less than hc, the drift width shall equal 4hd and the drift height shall equal hd. If this height exceeds hc, the drift width, w, shall equal 4 hd²/hc and the drift height shall equal hc. However, the drift width w shall not exceed 8hc. The maximum intensity of the drift surcharge load, pd, equals hd x D where the snow density, D, is defined by Eq 7.7-

### Section 7.10--Rain-On-Snow Surcharge Load

For locations where Pg is 20 psf or less but not zero, all roofs with a slope less than W/50, shall have a 5 psf rain-on-snow surcharge load applied to establish the design snow loads. This rain-on-snow augmented design load applies only to the balanced load case and need not be used in combination with drift, sliding, unbalanced, or partial loads.



V         23.00 psf         o         v                     AA         BA         CA                               CA	P1						P2	
	<u>V</u>		psf				\	<u>/</u>
Wd=         3.00 psf         X1=         1.00 ft           Wl=         20.00 psf         L1=         2.71 ft           Deck: Ww=         -21.58 psf         L2=         4.42 ft           Frame: Ww=         -13.96 psf         X2=         2.00 ft           P1=         5.83 plf         X2=         2.00 ft           P2=         5.83 plf         X2=         2.00 ft           MAd=         7.33 ft-lbs/ft         RA=         50.78 p           MAl=         10.00 ft-lbs/ft         Frame: RAw=         -35.45 p           Deck: MAw=         -10.79 ft-lbs/ft         Deck: RA(d+I)=         66.38 p           MA(d+I)=         17.33 ft-lbs/ft         RA(d+I)=         66.38 p           Deck: MA(d+w)=         -3.46 ft-lbs/ft         Frame: RA(d+w)=         -19.84 pl           Deck: MA(d+w)=         -3.46 ft-lbs/ft         RBd=         3.98 pl           MAB(d+I)=         17.58 ft-lbs/ft         RBd=         3.98 pl           Peck: MAB(d+w)=         -15.35 ft-lbs/ft         RBd=         3.98 pl           MBC(d+I)=         47.60 ft-lbs/ft         RBd=         3.98 pl           MBC(d+I)=         47.60 ft-lbs/ft         Frame: RB(d+I)=         -63.12 pl           Deck: MBC(d+w)= <td></td> <td></td> <td></td> <td>_</td> <td></td> <td>=</td> <td></td> <td>-</td>				_		=		-
W = 20.00 psf	< X1>	<	L1	>   <	L2	>	< X2>	
W = 20.00 psf			_					
Deck : Ww			•					
Frame: Ww= -13.96 psf			•					
P1= 5.83 plf P2= 5.83 plf  RAd= 15.60 p  MAd= 7.33 ft-lbs/ft RAl= 50.78 p  MAl= 10.00 ft-lbs/ft Frame: RAw= -35.45 p  Deck: MAw= -10.79 ft-lbs/ft Deck: RAw= -54.78 pl  MA(d+I)= 17.33 ft-lbs/ft RA(d+I)= 66.38 pl  Deck: MA(d+w)= -3.46 ft-lbs/ft Frame: RA(d+w)= -19.84 pl  Deck: MA(d+w)= 17.58 ft-lbs/ft RBl= 71.25 pl  MAB(d+I)= 17.58 ft-lbs/ft RBl= 71.25 pl  Frame: RBw= -40.84 pl  Deck: MBC(d+W)= -33.45 ft-lbs/ft RB(d+I)= 75.23 pl  MBC(d+I)= 47.60 ft-lbs/ft Frame: RB(d+w)= -36.86 pl  Deck: MBC(d+w)= -33.45 ft-lbs/ft RCl= 93.22 pl  MCd= 17.67 ft-lbs/ft RCl= 93.22 pl  MCd= 40.00 ft-lbs/ft RCl= 93.22 pl  MCd= 40.00 ft-lbs/ft RCl= 93.22 pl  Deck: MCw= -43.16 ft-lbs/ft Frame: RCw= -65.08 pl  Deck: MCw= -43.16 ft-lbs/ft Deck: RCw= -100.58 pl  Deck: MC(d+w)= -25.49 ft-lbs/ft RC(d+w)= -42.62 pl						4.42	ft	
RAd=			•		X2=	2.00	ft	
MAd= 7.33 ft-lbs/ft RAl= 50.78 p  MAl= 10.00 ft-lbs/ft Frame: RAw= -35.45 p  Deck: MAw= -10.79 ft-lbs/ft Deck: RAw= -54.78 p  MA(d+l)= 17.33 ft-lbs/ft Prame: RA(d+l)= 66.38 p  MA(d+l)= 17.33 ft-lbs/ft RA(d+w)= -19.84 p  Deck: MA(d+w)= -3.46 ft-lbs/ft Frame: RA(d+w)= -39.18 p  MAB(d+l)= 17.58 ft-lbs/ft RBd= 3.98 p  Deck: RA(d+w)= -15.35 ft-lbs/ft RBl= 71.25 p  Frame: RBw= -40.84 p  Deck: RBw= -63.12 p  MBC(d+l)= 47.60 ft-lbs/ft RB(d+l)= 75.23 p  Deck: MBC(d+w)= -33.45 ft-lbs/ft Frame: RB(d+w)= -36.86 p  Deck: RB(d+w)= -59.14 p  MCd= 17.67 ft-lbs/ft RCd= 22.46 p  MCd= 40.00 ft-lbs/ft RCd= 93.22 p  Deck: MCd= -43.16 ft-lbs/ft Frame: RCw= -65.08 p  MC(d+l)= 57.67 ft-lbs/ft Deck: RCw= -100.58 p  Frame: RC(d+w)= -25.49 ft-lbs/ft RCd+ll= 115.68 p  Frame: RC(d+w)= -42.62 p  Frame: RC(d+w)= -42.62 p			•					
MAd=       7.33 ft-lbs/ft       RAI=       50.78 p         MAI=       10.00 ft-lbs/ft       Frame: RAw=       -35.45 p         Deck: MAw=       -10.79 ft-lbs/ft       Deck: RAw=       -54.78 p         MA(d+I)=       17.33 ft-lbs/ft       RA(d+I)=       66.38 p         Deck: MA(d+w)=       -3.46 ft-lbs/ft       Frame: RA(d+w)=       -19.84 pl         Deck: RA(d+w)=       -39.18 pl         MAB(d+I)=       17.58 ft-lbs/ft       RBd=       3.98 pl         Deck: MAB(d+w)=       -15.35 ft-lbs/ft       RBi=       71.25 pl         Frame: RBw=       -40.84 pl       Deck: RBw=       -63.12 pl         MBC(d+I)=       47.60 ft-lbs/ft       RB(d+I)=       75.23 pl         Deck: MBC(d+w)=       -33.45 ft-lbs/ft       Frame: RB(d+w)=       -36.86 pl         Deck: MBC(d+w)=       -35.45 ft-lbs/ft       RCd=       22.46 pl         MCl=       40.00 ft-lbs/ft       RCd=       22.46 pl         MCl=       40.00 ft-lbs/ft       RCd=       93.22 pl         Deck: MCw=       -43.16 ft-lbs/ft       Deck: RCw=       -65.08 pl         Deck: MC(d+I)=       57.67 ft-lbs/ft       Deck: RCw=       -100.58 pl         Frame: RC(d+w)=       -42.62 pl	P2=	5.83	plf					
MAd=       7.33 ft-lbs/ft       RAI=       50.78 p         MAI=       10.00 ft-lbs/ft       Frame: RAw=       -35.45 p         Deck: MAw=       -10.79 ft-lbs/ft       Deck: RAw=       -54.78 p         MA(d+I)=       17.33 ft-lbs/ft       RA(d+I)=       66.38 p         Deck: MA(d+w)=       -3.46 ft-lbs/ft       Frame: RA(d+w)=       -19.84 pl         Deck: RA(d+w)=       -39.18 pl         MAB(d+I)=       17.58 ft-lbs/ft       RBd=       3.98 pl         Deck: MAB(d+w)=       -15.35 ft-lbs/ft       RBi=       71.25 pl         Frame: RBw=       -40.84 pl       Deck: RBw=       -63.12 pl         MBC(d+I)=       47.60 ft-lbs/ft       RB(d+I)=       75.23 pl         Deck: MBC(d+w)=       -33.45 ft-lbs/ft       Frame: RB(d+w)=       -36.86 pl         Deck: MBC(d+w)=       -35.45 ft-lbs/ft       RCd=       22.46 pl         MCl=       40.00 ft-lbs/ft       RCd=       22.46 pl         MCl=       40.00 ft-lbs/ft       RCd=       93.22 pl         Deck: MCw=       -43.16 ft-lbs/ft       Deck: RCw=       -65.08 pl         Deck: MC(d+I)=       57.67 ft-lbs/ft       Deck: RCw=       -100.58 pl         Frame: RC(d+w)=       -42.62 pl								
MAI=         10.00 ft-lbs/ft         Frame: RAw=         -35.45 pt           Deck: MAw=         -10.79 ft-lbs/ft         Deck: RAw=         -54.78 pt           MA(d+I)=         17.33 ft-lbs/ft         RA(d+I)=         66.38 pt           Deck: MA(d+w)=         -3.46 ft-lbs/ft         Frame: RA(d+w)=         -19.84 pt           Deck: RA(d+w)=         -39.18 pt           MAB(d+I)=         17.58 ft-lbs/ft         RBd=         3.98 pt           Deck: RA(d+w)=         -39.18 pt           MAB(d+I)=         17.53 ft-lbs/ft         RBI=         71.25 pt           Frame: RBw=         -40.84 pt         Peck: RBw=         -63.12 pt           MBC(d+I)=         47.60 ft-lbs/ft         RB(d+I)=         75.23 pt           Deck: MBC(d+w)=         -33.45 ft-lbs/ft         Frame: RB(d+w)=         -36.86 pt           Deck: MBC(d+w)=         -33.45 ft-lbs/ft         RCd=         22.46 pt           MCl=         40.00 ft-lbs/ft         RCl=         93.22 pt           Deck: MCw=         -43.16 ft-lbs/ft         Frame: RCw=         -65.08 pt           Deck: MC(d+I)=         57.67 ft-lbs/ft         Deck: RCw=         -100.58 pt           Deck: MC(d+w)=         -25.49 ft-lbs/ft         RC(d+I)=         115.68 pt								
Deck : MAw=         -10.79 ft-lbs/ft         Deck : RAw=         -54.78 pt           MA(d+I)=         17.33 ft-lbs/ft         RA(d+I)=         66.38 pt           Deck : MA(d+w)=         -3.46 ft-lbs/ft         Frame : RA(d+w)=         -19.84 pt           Deck : RA(d+w)=         -39.18 pt           MAB(d+I)=         17.58 ft-lbs/ft         RBd=         3.98 pt           Deck : RAB(d+w)=         -15.35 ft-lbs/ft         RBI=         71.25 pt           Frame : RBw=         -40.84 pt         -40.84 pt           Deck : RBw=         -63.12 pt         RB(d+I)=         75.23 pt           Deck : MBC(d+I)=         47.60 ft-lbs/ft         Frame : RB(d+w)=         -36.86 pt           Deck : MBC(d+w)=         -33.45 ft-lbs/ft         Frame : RB(d+w)=         -59.14 pt           MCd=         17.67 ft-lbs/ft         RCd=         22.46 pt           MCl=         40.00 ft-lbs/ft         RCl=         93.22 pt           Deck : MCw=         -43.16 ft-lbs/ft         Frame : RCw=         -65.08 pt           Deck : MC(d+I)=         57.67 ft-lbs/ft         Deck : RCw=         -100.58 pt           Frame : RC(d+w)=         -25.49 ft-lbs/ft         RC(d+I)=         115.68 pt								•
MA(d+l)=       17.33 ft-lbs/ft       RA(d+l)=       66.38 pt         Deck: MA(d+w)=       -3.46 ft-lbs/ft       Frame: RA(d+w)=       -19.84 pt         Deck: RA(d+w)=       -39.18 pt         MAB(d+l)=       17.58 ft-lbs/ft       RBd=       3.98 pt         Deck: MAB(d+w)=       -15.35 ft-lbs/ft       RBl=       71.25 pt         Frame: RBw=       -40.84 pt         Deck: RBw=       -63.12 pt         MBC(d+l)=       47.60 ft-lbs/ft       RB(d+l)=       75.23 pt         Deck: MBC(d+w)=       -33.45 ft-lbs/ft       Frame: RB(d+w)=       -36.86 pt         Deck: MBC(d+w)=       -43.45 ft-lbs/ft       RCd=       22.46 pt         MCl=       40.00 ft-lbs/ft       RCl=       93.22 pt         Deck: MCw=       -43.16 ft-lbs/ft       Frame: RCw=       -65.08 pt         Deck: MC(d+l)=       57.67 ft-lbs/ft       Deck: RCw=       -100.58 pt         Deck: MC(d+w)=       -25.49 ft-lbs/ft       RC(d+l)=       115.68 pt         Frame: RC(d+w)=       -42.62 pt					Frame	: RAw=	-35.45	plf
Deck : MA(d+w)=         -3.46 ft-lbs/ft         Frame : RA(d+w)=         -19.84 pl           Deck : RA(d+w)=         -39.18 pl           MAB(d+l)=         17.58 ft-lbs/ft         RBd=         3.98 pl           Deck : MAB(d+w)=         -15.35 ft-lbs/ft         RBi=         71.25 pl           Frame : RBw=         -40.84 pl         -40.84 pl           Deck : RBw=         -63.12 pl         -63.12 pl           MBC(d+l)=         47.60 ft-lbs/ft         Frame : RB(d+w)=         -36.86 pl           Deck : MBC(d+w)=         -33.45 ft-lbs/ft         Frame : RB(d+w)=         -59.14 pl           MCd=         17.67 ft-lbs/ft         RCd=         22.46 pl           MCl=         40.00 ft-lbs/ft         RCl=         93.22 pl           Deck : MCw=         -43.16 ft-lbs/ft         Frame : RCw=         -65.08 pl           MC(d+l)=         57.67 ft-lbs/ft         Deck : RCw=         -100.58 pl           Deck : MC(d+w)=         -25.49 ft-lbs/ft         RC(d+l)=         115.68 pl           Frame : RC(d+w)=         -42.62 pl	+						54.78	plf
Deck : RA(d+w)= -39.18 pl   MAB(d+l)= 17.58 ft-lbs/ft RBd= 3.98 pl   Deck : MAB(d+w)= -15.35 ft-lbs/ft RBl= 71.25 pl   Frame : RBw= -40.84 pl   Deck : RBw= -63.12 pl   MBC(d+l)= 47.60 ft-lbs/ft RB(d+l)= 75.23 pl   Deck : MBC(d+w)= -33.45 ft-lbs/ft Frame : RB(d+w)= -36.86 pl   Deck : RB(d+w)= -59.14 pl   MCd= 17.67 ft-lbs/ft RCd= 22.46 pl   MCl= 40.00 ft-lbs/ft RCl= 93.22 pl   Deck : MCw= -43.16 ft-lbs/ft Frame : RCw= -65.08 pl   MC(d+l)= 57.67 ft-lbs/ft Deck : RCw= -100.58 pl   Deck : MC(d+w)= -25.49 ft-lbs/ft RC(d+w)= -42.62 pl	` .					RA(d+I)=	66.38	plf
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Deck : MA(d+w)=	-3.46	ft-lbs/ft		Frame: R	(A(d+w)=	-19.84	plf
Deck : MAB(d+w)= -15.35 ft-lbs/ft RBI= 71.25 pl Frame : RBw= -40.84 pl Deck : RBw= -63.12 pl MBC(d+l)= 47.60 ft-lbs/ft RB(d+l)= 75.23 pl Deck : MBC(d+w)= -33.45 ft-lbs/ft Frame : RB(d+w)= -36.86 pl Deck : RB(d+w)= -59.14 pl  MCd= 17.67 ft-lbs/ft RCd= 22.46 pl MCl= 40.00 ft-lbs/ft RCl= 93.22 pl Deck : MCw= -43.16 ft-lbs/ft Frame : RCw= -65.08 pl MC(d+l)= 57.67 ft-lbs/ft Deck : RCw= -100.58 pl Deck : MC(d+w)= -25.49 ft-lbs/ft RC(d+w)= -42.62 pl					Deck: R	:A(d+w)=	-39.18	plf
Deck : MAB(d+w)= -15.35 ft-lbs/ft RBI= 71.25 pl Frame : RBw= -40.84 pl Deck : RBw= -63.12 pl MBC(d+l)= 47.60 ft-lbs/ft RB(d+l)= 75.23 pl Deck : MBC(d+w)= -33.45 ft-lbs/ft Frame : RB(d+w)= -36.86 pl Deck : RB(d+w)= -59.14 pl  MCd= 17.67 ft-lbs/ft RCd= 22.46 pl MCl= 40.00 ft-lbs/ft RCl= 93.22 pl Deck : MCw= -43.16 ft-lbs/ft Frame : RCw= -65.08 pl MC(d+l)= 57.67 ft-lbs/ft Deck : RCw= -100.58 pl Deck : MC(d+w)= -25.49 ft-lbs/ft RC(d+w)= -42.62 pl								
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	` ,							
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Deck : MAB(d+w)=	-15.35	ft-lbs/ft			RBI=	71.25	plf
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					Frame	: RBw=	-40.84	plf
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					Deck	: RBw=	-63.12	plf
Deck : RB(d+w)=       -59.14 pl         MCd=       17.67 ft-lbs/ft       RCd=       22.46 pl         MCl=       40.00 ft-lbs/ft       RCl=       93.22 pl         Deck : MCw=       -43.16 ft-lbs/ft       Frame : RCw=       -65.08 pl         MC(d+l)=       57.67 ft-lbs/ft       Deck : RCw=       -100.58 pl         Deck : MC(d+w)=       -25.49 ft-lbs/ft       RC(d+l)=       115.68 pl         Frame : RC(d+w)=       -42.62 pl	, ,					₹B(d+l)=	75.23	plf
MCd=       17.67 ft-lbs/ft       RCd=       22.46 pl         MCl=       40.00 ft-lbs/ft       RCl=       93.22 pl         Deck: MCw=       -43.16 ft-lbs/ft       Frame: RCw=       -65.08 pl         MC(d+l)=       57.67 ft-lbs/ft       Deck: RCw=       -100.58 pl         Deck: MC(d+w)=       -25.49 ft-lbs/ft       RC(d+l)=       115.68 pl         Frame: RC(d+w)=       -42.62 pl	Deck : MBC(d+w)=	-33.45	ft-lbs/ft		Frame: R	B(d+w)=	-36.86	plf
MCI=       40.00 ft-lbs/ft       RCI=       93.22 pl         Deck: MCw=       -43.16 ft-lbs/ft       Frame: RCw=       -65.08 pl         MC(d+I)=       57.67 ft-lbs/ft       Deck: RCw=       -100.58 pl         Deck: MC(d+w)=       -25.49 ft-lbs/ft       RC(d+I)=       115.68 pl         Frame: RC(d+w)=       -42.62 pl					Deck: R	B(d+w)=	-59.14	plf
MCI=       40.00 ft-lbs/ft       RCI=       93.22 pl         Deck: MCw=       -43.16 ft-lbs/ft       Frame: RCw=       -65.08 pl         MC(d+I)=       57.67 ft-lbs/ft       Deck: RCw=       -100.58 pl         Deck: MC(d+w)=       -25.49 ft-lbs/ft       RC(d+I)=       115.68 pl         Frame: RC(d+w)=       -42.62 pl								
Deck : MCw=         -43.16 ft-lbs/ft         Frame : RCw=         -65.08 pl           MC(d+l)=         57.67 ft-lbs/ft         Deck : RCw=         -100.58 pl           Deck : MC(d+w)=         -25.49 ft-lbs/ft         RC(d+l)=         115.68 pl           Frame : RC(d+w)=         -42.62 pl						RCd=	22.46	plf
	MCI=	40.00	ft-lbs/ft			RCI=		•
MC(d+I)= 57.67 ft-lbs/ft Deck: $RCw=$ -100.58 pt Deck: $MC(d+w)=$ -25.49 ft-lbs/ft $RC(d+I)=$ 115.68 pt Frame: $RC(d+w)=$ -42.62 pt	Deck: MCw=	-43.16	ft-lbs/ft		Frame	: RCw=		•
Deck : MC(d+w)= -25.49 ft-lbs/ft	MC(d+l)=	57.67	ft-lbs/ft	<del></del>	Deck	: RCw=		•
Frame : RC(d+w)= -42.62 pl	Deck: MC(d+w)=	-25.49	ft-lbs/ft			***************************************	***************************************	•
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								-

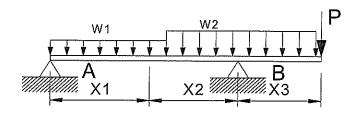
USE 20 GAUGE GRADE C DECK +S=.3961 in^3 -S=.3036 in^3 FY=40 ksl

DECK DESIGN:	Deck 2			
Wd=	3.00	psf	P1	P2
WI=	20.00		v 23.00 psf	v - 1
Deck: Ww=	-21.58	psf	^A	^B
Frame: Ww=	-13.96	psf	< X1>  <	> < X2 ->
P1=	5.83	plf		• ,
P2=	5.83	plf		
L=	4.42	ft		
X1=	0.79	ft		
X2=	2.00	ft		
		e		.09 plf
MA(d)=		ft-lbs/ft	· · · · · · · · · · · · · · · · · · ·	.42 plf
MA(I)=		ft-lbs/ft		.55 plf
Deck: MA(w)=		ft-lbs/ft	······································	.49 plf
MA(d+I)=		ft-lbs/ft	RA(d+l)= 73	.51 plf
Deck: MA(d+w)=	-1.20	ft-lbs/ft	Frame: RA(d+w)= -24.	.46 plf
			Deck: RA(d+w)= -44.	40 plf
				20 plf
MB(d)=		ft-lbs/ft	· · · · · · · · · · · · · · · · · · ·	22 plf
MB(I)=		ft-lbs/ft		09 plf
Deck: MB(w)=	-43.16		Deck: RBw= -99.	05 plf
MB(d+l)=		ft-lbs/ft	RB(d+l)= 114.	42 plf
Deck: MB(d+w)=	-25.49	ft-lbs/ft	· · · · · · · · · · · · · · · · · · ·	89 plf
			Deck: RB(d+w)= -77.	85 plf
MAB(d+l)=	44.63	ft-lhs/ft		
Deck : MAB(d+w)=	-32.77			
		100/10		

USE 20 GAUGE GRADE C DECK +S=.3961 in^3 -S=.3036 in^3 FY=40 ksl

DECK DESIGN:	Deck 3				
Wd=	3.00	psf	P1		P2
=!W	20.00	psf	v 23.00	psf	v
Deck: Ww=	-21.58	psf	^A		^B
Frame : Ww=	-13.96	psf	< X1>  <	L>	< X2 ->
P1=	5.83	plf			•
P2=	5.83	plf			
L=	4.42	ft			
X1=	1.63	ft			
X2=	2.00	ft			
			RAd=	16.38	plf
MA(d)=	13.44	ft-lbs/ft	RAI(MAX)=	82.65	•
MA(I)=	26.41	ft-lbs/ft	Frame: RAw=	-51.37	•
Deck: MA(w)=	-28.49	ft-lbs/ft	Deck: RAw=	-79.40	•
$\overline{MA(d+l)}=$	39.85	ft-lbs/ft	RA(d+l)=	99.02	
Deck: MA(d+w)=	-15.05	ft-lbs/ft	Frame: RA(d+w)=	-35.00	•
			Deck: RA(d+w)=	-63.02	plf
			RBd=	19.42	plf
MB(d)=	17.67	ft-lbs/ft	RBI(MAX)=	93.22	· <del>-</del>
MB(I)=	40.00	ft-lbs/ft	Frame: RBw=	-60.91	plf
Deck: MB(w)=	-43.16	ft-lbs/ft	Deck: RBw=	-94.13	plf
MB(d+l)=	57.67	ft-lbs/ft	RB(d+l)=	112.64	plf
Deck : MB(d+w)=	-25.49	ft-lbs/ft	Frame: RB(d+w)=	-41.49	plf
			Deck: RB(d+w)=	-74.71	plf
MAR/dull-	40 EE	ft lba <i>lft</i>			
MAB(d+l)=		ft-lbs/ft			
Deck : MAB(d+w)=	-25.18	IL-IDS/IT			

Wd1 =	24.09 plf
WI1 =	61.42 plf
Ww1 =	-36.55 plf
Wd2 =	15.98 plf
Wi2 =	71.25 plf
Ww2 =	-40.84 plf
Pd=	31.87 lbs
Pi=	0.00 lbs
Pw=	0.00 lbs
X1 =	16.46 ft
X2 =	1.54 ft
X3 =	1.33 ft



	RAd=	213	lbs	
	RAI=	550	lbs	
	RAw=	-327	lbs	
•	RA(d+l)=	763	lbs	
	RA(d+w)=	-114	lhe	

	RBd=	261	lbs	
	RBI=	666	lbs	
	RBw=	-392	lbs	
_	RB(d+l)=	927	lbs	
	RR(d+w)=	-131	lhe	

MB(d+l) =	-120 ft-lbs I	 OK
MB(d+w) =	-20 ft-lbs I	OK
MAB(d+l)=	3384 ft-lbs li	 OK
MAB(d+w)=	-519 ft-lbs li	OK

Deflections: (inches)	Overhang	Midspan
DL=	-0.019	0.083
DL+LL=	-0.071	0.302

USE: W6X12	Fy =	50 H	ksi

Wd=   32.46 pff   P   V   125.68 pff   Wi=   93.22 pff   V   125.68 pff   Pd=   27.19 lbs     (	BEAM DESIG	BN:	P-b								
Wwe	Wd=	32.46	plf			IP					····
Wwe Pd= 27.19 lbs       27.19 lbs       A       BA         Pd= 27.19 lbs         √−√√√√√√√√√√√√√√√√√√√√√√√√√√√√√√√√√√√	WI=	93.22	! plf			V		125.68	B plf		
Pi	Ww=	-65.08	plf							<del>7</del>	
Pw	Pd=	27.19	lbs			<x< td=""><td>&gt;</td><td>&lt;</td><td>L</td><td>&gt;</td><td></td></x<>	>	<	L	>	
L= 18.00 ft DL= -0.019 0.083 X= 1.33 ft DL+LL= -0.076 0.327  MA(d) = 65 ft-lbs	PI=	0.00	Ibs			•		•			
L= 18.00 ft DL=	Pw=	0.00	lbs	Defle	ctions:	(inches)		Overhang	Midspan		
MA(d) = 65 ft-lbs	L=	18.00	ft		DL=	· · · · · ·			· · · · · · · · · · · · · · · · · · ·	_	
MA(d) = 65 ft-lbs	X=	1.33	ft	[	DL+LL=			-0.076			
MA(d) = 65 ft-lbs				(+dov	vnward,	-upward)					
MA(I) = 83 ft-lbs	MA(d) =	65	ft-lbs	•		, ,		RAd=	: 36	6 lbs	
MA(d+l) =	MA(I) =	83	ft-lbs								
MA(d+l) =		-58	ft-lbs								
MA(d+w) = 7 ft-lbs lu= 1.33 ft RA(d+w)= -310 lbs    RBd= 289 lbs RBI(Max)= 839 lbs RBI(Max)= -583 lbs RBW= -583 lbs RBW= -583 lbs RBW= -583 lbs RBW= -583 lbs RBMAB(d+w)= -1325 ft-lbs lu= 1.33 ft RB(d+w)= -294 lbs     USE: W8X10				_	1.33	ft		***********			<del> </del>
RBd= 289   lbs   RBI(Max)= 839   lbs   RBW= -583   lbs   RBW= -583   lbs   RBW= -583   lbs   RBW= -583   lbs   RBMAB(d+w)=   -1325   ft-lbs   lu=   1.33   ft   RB(d+w)=   -294   lbs   RB(d+w)=   -294   lbs   RBMAB(d+w)=   -298   lbs   -298   lbs   RBMAB(d+w)=   -298   lbs   RBMAB(d+w)=   -298   lbs   -298   lbs   RBMAB(d+w)=   -298   lbs   -298   lbs   RBMAB(d+w)=   -											
MAB(d+I)= 5058 ft-lbs lu= 9.00 ft RB(d+V)= 1128 lbs MAB(d+W)= -1325 ft-lbs lu= 1.33 ft RB(d+V)= 1128 lbs MAB(d+W)= -1325 ft-lbs lu= 1.33 ft RB(d+W)= -294 lbs    USE: W8X10	( ,								3.		
MAB(d+I)= 5058 ft-lbs lu= 9.00 ft RB(d+V)= 1128 lbs MAB(d+W)= -1325 ft-lbs lu= 1.33 ft RB(d+V)= 1128 lbs MAB(d+W)= -1325 ft-lbs lu= 1.33 ft RB(d+W)= -294 lbs    USE: W8X10								RBd=	28	9 lbs	
MAB(d+l)= 5058 ft-lbs lu= 9.00 ft RB(d+l)= 1128 lbs RB(d+w)= -1325 ft-lbs lu= 1.33 ft RB(d+w)= -294 lbs      USE: W8X10											
MAB(d+l)= 5058 ft-lbs lu= 9.00 ft RB(d+l)= 1128 lbs RB(d+w)= -1325 ft-lbs lu= 1.33 ft RB(d+w)= -294 lbs    USE: W8X10											
MAB(d+w)= -1325 ft-lbs lu= 1.33 ft RB(d+w)= -294 lbs    USE: W8X10	MAB(d+I)=	5058	ft-lbs lu=		9.00	ft			******		
USE: W8X10 Fy = 50 ksi  BEAM DESIGN: P-c  Wd= 31.38 plf Wl= 82.65 plf Ww= -51.37 plf L= 19.00 ft   114.02 plf	• •							• •			
BEAM DESIGN: P-c	(,		77.100		.,,,,			112(G-11)	20	1 100	
BEAM DESIGN: P-c		USE:	W8X10		Fv =		50	ksi			
Wd=       31.38 plf         Wl=       82.65 plf         Ww=       -51.37 plf         L=       19.00 ft	***		***************************************						<del></del>		
Wd=       31.38 plf         Wl=       82.65 plf         Ww=       -51.37 plf         L=       19.00 ft	BEAM DESIG	N:	P-c	***************************************		··········					
WI				plf	***************************************				· · · · · · · · · · · · · · · · · · ·		
Ww= -51.37 plf L= 19.00 ft		WI=		-							
L= 19.00 ft											
114.02 plf		L=		•							
C											
C		•	114.02	plf							
RI= 785   lbs     785   lbs			۸		^						
R = 785 lbs     Md= 1415.9 ft-lbs   Rw= -488 lbs     Mi= 3729.4 ft-lbs   R(d+l)= 1083 lbs     Mw= -2318.2 ft-lbs   R(d+w)= -190 lbs     M(d+l)= 5145.2 ft-lbs   Lu= 9.50 ft   OK     M(d+w)= -902.4 ft-lbs   Lu= 1.33 ft   OK     USE: W6X15   Fy = 50 ksi     Deflections: (inches)   Midspan     DL= 0.109     DL+LL= 0.396			<	L	>	R	d=	298	lbs		
Md=       1415.9 ft-lbs       Rw=       -488 lbs         Ml=       3729.4 ft-lbs       R(d+l)=       1083 lbs         Mw=       -2318.2 ft-lbs       R(d+w)=       -190 lbs         M(d+l)=       5145.2 ft-lbs       Lu=       9.50 ft       OK         M(d+w)=       -902.4 ft-lbs       Lu=       1.33 ft       OK            USE:       W6X15       Fy =       50 ksi         Deflections:       (inches)       Midspan         DL=       0.109         DL+LL=       0.396			•		•						
MI= 3729.4 ft-lbs R(d+l)= 1083 lbs  Mw= -2318.2 ft-lbs R(d+w)= -190 lbs  M(d+l)= 5145.2 ft-lbs Lu= 9.50 ft OK  M(d+w)= -902.4 ft-lbs Lu= 1.33 ft OK  USE: W6X15 Fy = 50 ksi  Deflections: (inches) Midspan  DL= 0.109  DL+LL= 0.396		Md=	1415.9	ft-lbs							
Mw= -2318.2 ft-lbs R(d+w)= -190 lbs  M(d+l)= 5145.2 ft-lbs Lu= 9.50 ft OK M(d+w)= -902.4 ft-lbs Lu= 1.33 ft OK  USE: W6X15 Fy = 50 ksi  Deflections: (inches) Midspan DL= 0.109 DL+LL= 0.396					-					_	
M(d+l)= 5145.2 ft-lbs											
M(d+w)= -902.4 ft-lbs						,	,				
M(d+w)= -902.4 ft-lbs		M(d+l)=	5145.2	ft-lbs		L	u=	9.50	ft	OK	
USE:         W6X15         Fy =         50 ksi           Deflections:         (inches)         Midspan           DL=         0.109           DL+LL=         0.396			-902.4	ft-lbs							
Deflections: (inches) Midspan  DL= 0.109  DL+LL= 0.396		• •									
Deflections: (inches) Midspan  DL= 0.109  DL+LL= 0.396											
DL= 0.109 DL+LL= 0.396		USE:	W6X15		Fy =		50	ksi			
DL= 0.109 DL+LL= 0.396	_								•		
DL+LL= 0.396		_		inches	)	~	1				
(+downward, -upward)						0.396					
			(+downward,	-upwa	rd)	WII.					

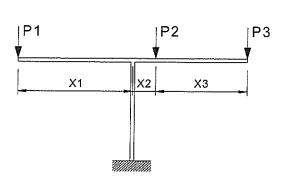
BEAM DESIGN	N:	P-d					
	Wd=	29.42	2 plf				
	WI=		•				
	Ww=		•				
	L=	19.00	) ft				
		122.64	1 plf	=			
		^	^				
		<	L>				
		4007		_RI=			
	Md=		ft-lbs	Rw=			
	MI=			R(d+l)=			
	Mw=	-2748.4	+ ft-lbs	R(d+w)=	-299	lbs	
	M(d+l)=	5534.1	ft-lbs	Lu=	9.50	ft	ОК
	M(d+w)=			Lu=			ok
	, ,						
	USE:	W8X10	Fy =	50	ksi		
***************************************	OOL.	7707(10		30	KSI	;	
		Deflections:		Midspan	_		
		DL=		0.097			
		DL+LL=		0.403			
DEAM DEGICAL	1.	(+downward	, -upward)				
BEAM DESIGN Wd=	31.38	P-e		D			
₩I=	82.65	•		P	444.00	i.e	
Ww=	-51.37	•		V	114.02 ^A	pii B^	=
Pd=	21.46	•		<>	• •	D	
PI=	0.00						
Pw=	0.00		Deflections: (	(inchee)	Overhang	Midspan	
L=	16.00		DL=	(inches)	-0.026	0.047	-
X=	3.38		DL+LL=		-0.020	0.047	
Λ	0.00	TC .	(+downward,	-unward)	-0.104	0.176	
MA(d) =	251	ft-lbs	( · 50 minarai u,	apwaraj	RAd=	394	lhs
MA(I) =		ft-lbs			RAI=	970	
MA(w) =	-293				RAW=	-603	
MA(d+1) =		ft-lbs lu=	1.33	ff	RA(d+I)=	1364	
MA(d+w) =		ft-lbs lu=	3.38		RA(d+w)=	-209	
` '						<b></b>	
					RBd=	235	lbs
					RBI(Max)=	661	
					`RBẃ=	-393	
MAB(d+l)=		ft-lbs lu=	8.00	ft	RB(d+l)=	896	
MAB(d+w)=	-619	ft-lbs lu=	1.33	ft	RB(d+w)=	-157	
	USE:	W6X15	Fy =	50	ksi		

BEAM DESIG	N:	P-f						
Wd=	29.42	plf		P	***************************************			
W!=	93.22	plf		v	122.64	plf		
Ww=	-60.91	plf			^A	B^	=	
Pd=	25.45	lbs		] <x< td=""><td>-&gt;  &lt;</td><td>L&gt; </td><td></td><td></td></x<>	->  <	L>		
PI=	0.00	lbs		•	•	•		
Pw=	0.00	lbs	Deflections:	(inches)	Overhang	Midspan		
L=	16.00	ft	DL=	*****	-0.022	0.041	•	
X=	3.38	ft	DL+LL=		-0.105	0.178		
			(+downward,	-upward)				
MA(d) =	253	ft-lbs		, ,	RAd=	376	lbs	
MA(I) =	531	ft-lbs			RAI=	1094	lbs	
MA(w) =	-347	ft-lbs			RAw=	-714	lbs	
MA(d+l) =	784	ft-lbs lu=	1.33	ft	RA(d+l)=	1469	lbs	
MA(d+w) =	-93	ft-lbs lu=	3.38	ft	RA(d+w)=	-339	lbs	
					RBd=	219	lbs	
					RBI(Max)=	746	lbs	
					RBw=	-466	lbs	
MAB(d+I)=	3799	ft-lbs lu=	8.00	ft	RB(d+l)=	965	lbs	-
MAB(d+w)=	-962	ft-lbs lu=	1.33	ft	RB(d+w)=	-246	lbs	
<u></u>	USE:	W8X10	<u> </u>		50 ksi			

P1d =	45 lbs	
P1I =	146 lbs	
Plw =	-102 lbs	
P2d =	261 lbs	
P2l =	666 lbs	
P2w =	-392 lbs	
P3d =	366 lbs	
P3I =	968 lbs	
P3w =	-676 lbs	
Beam Wt =	20 plf	
	·	
X1 =	1.42 ft	
X2 =	1.29 ft	

4.42 ft

X3 =



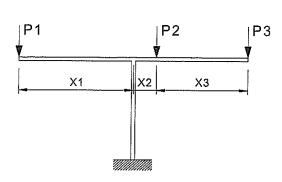
BEAM:				
Left Hand Side	· //// //	****		
Md =	-84	ft-lbs		
MI =	-207	ft-lbs		
Mw =	144	ft-lbs		
Md+MI =	-290	ft-lbs	lu =	1.42 ft
Md+Mw =	61	ft-lbs	iu =	1.42 ft
Md+0.75•I+0.75•Mw =	347	ft-lbs	lu =	1.42 ft
Right Hand Side				
Md =	-2754	ft-lbs		
MI =	-6385	ft-lbs		
Mw =	4363	ft-lbs		:
Md+MI =	-9139	ft-lbs	lu =	4.42 ft
Md+Mw =	1610	ft-lbs	lu =	4.42 ft
Md+0.75•l+0.75•Mw =	10815	ft-lbs	lu =	4.42 ft

USE:	W6X20	Fy =	50 ksi			
			***************************************			
COLUMN:			Pd =	815	lbs	
Md =	= 2670	ft-lbs	P! =	1780	lbs	
M(ULL) =	= 6648	ft-lbs	Pw =	-1169	lbs	
M(D+L) =	9318	ft-lbs	Pd + Pl =	2594	lbs	-
			Pd + Pw =	-355	lbs	

P1d =	0	lbs
P1I =	0	lbs
Plw =	0	lbs
P2d =	511	lbs
P2I =	1335	lbs
P2w =	-815	lbs
P3d =	568	lbs
P31 =	1725	lbs
P3w =	-1161	lbs
Beam Wt =	21	plf
X1 =	0.00	ft
X2 =	1.29	ft

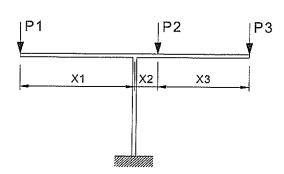
4.42 ft

X3 =



BEAM:	<del></del>			·	· · · · · · · · · · · · · · · · · · ·
Left Hand Side		····			
Md =	-0	ft-lbs			
MI =	-0	ft-lbs			
Mw =	-0	ft-lbs			
Md+MI =	-0	ft-lbs	lu =	0.00	ft
Md+Mw =	-0	ft-lbs	lu =	0.00	ft
Md+0.75•I+0.75•Mw =	0	ft-lbs	lu =	0.00	ft
Right Hand Side					
Md =	-4245	ft-lhe			
Mi =	-11569				
Mw =	7681				
Md+MI =	-15814		  u =	4.42	ft
Md+Mw =		ft-lbs		4.42	
Md+0.75•l+0.75•Mw =	18682			4.42	

USE:	W8X21	<u>Fy = </u>	50 ksi	
COLUMN:			Pd =	1199 lbs
Md =	4245	ft-lbs	PI =	3060 lbs
M(ULL) =	11595	ft-lbs	Pw =	-1976 lbs
M(D+L) =	15839	ft-lbs	Pd + Pl =	4259 lbs
			Pd + Pw =	-777 lbs



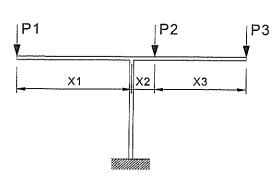
Beam Wt = 21 plfX1 = 0.00 ft

X1 = 0.00 ft X2 = 1.29 ftX3 = 4.42 ft

BEAM:	***************************************	<del></del>	<del></del>	
Left Hand Side		-1		
Md =	-0	ft-lbs		
MI =	-0	ft-lbs		
Mw =	-0	ft-lbs		
Md+Ml =	-0	ft-lbs lu =	0.00	ft
Md+Mw =	-0	ft-lbs lu =	0.00	ft
Md+0.75•l+0.75•Mw =	0	ft-lbs lu =	0.00	ft
Right Hand Side				
Md =	-3879	ft-lbs		
MI =	-11181	ft-lbs		
Mw =	7098	ft-lbs		
Md+MI =	-15060	ft-lbs lu =	4.42	ft
Md+Mw =	3219	ft-lbs lu =	4.42	ft
Md+0.75•I+0.75•Mw =	17588	ft-lbs lu =	4.42	ft

USE:	W8X21	Fy =	50 ksi	
COLUMN:			Pd =	1152 lbs
Md		ft-lbs	PI =	3078 lbs
M(ULL)	V1111111111111111111111111111111111111	ft-lbs	Pw =	-1925 lbs
M(D+L) :	= 14847	ft-lbs	Pd + Pl =	4230 lbs
			Pd + Pw =	-773 lbs

P1d = P1I = P1w = P2d = P2l = P2w = P3d = P3l = P3w =	Ō	lbs lbs lbs lbs
Beam Wt =	20	



X1 = 0.00 ft X2 = 1.29 ftX3 = 4.42 ft

BEAM:		
Left Hand Side		100000
Md =	-0 ft-lbs	
MI =	-0 ft-lbs	
Mw =	-0 ft-lbs	
Md+MI =	-0 ft-lbs lu =	0.00 ft
Md+Mw =	-0 ft-lbs lu =	0.00 ft
Md+0.75•l+0.75•Mw =	0 ft-lbs lu =	0.00 ft
Right Hand Side		
Md =	-2981 ft-lbs	
MI =	-7495 .ft-lbs	
Mw =	4857 ft-lbs	
Md+MI =	-10475 ft-lbs lu =	4.42 ft
Md+Mw =	1876 ft-lbs lu =	4.42 ft
Md+0.75•I+0.75•Mw =	12244 ft-lbs lu =	4.42 ft

USE:	W6X20	Fy =	50 ksi	
COLUMN:	•		Pd =	00 <i>4</i> lba
Md =	2004	ff lbo		884 lbs
		ft-lbs	PI =	2063 lbs
M(ULL) =		ft-lbs	Pw =	-1317 lbs
M(D+L) =	10492	ft-lbs	Pd + P! =	2947 lbs
			Pd + Pw =	-433 lbs

Column Design		AISC	14th ed, Use i	First Order An	alysis Criteria
P DL = 1.2	0 kips		Clr. Ht.=		
PLL = 3.0	6 kips		Fascia Ht.=	1.00	ft
P WL = -1.9	8 kips		Col. Trib=	18.43	ft
Base Shear = 0.4	1 kips		Wind Load=	16.00	psf
	8⊸kips		# of COL.=	1.00	•
M WL = w(Fascia Ht•2.5•Col Trib./# of	col•L)+ w(Wrap•1	/2 Clr. Ht^2)	Max All. Defl =	1.20	in
M Seis = Base Shear x L		ſ	Vlax Defl Ratio =	L/	100
M Unbal = Live Load x Col. Trib.x (Canor	y Width/2)^2/2		Max Defl. =	0.26	in, OK
L = Clr. Ht. + Fascia Ht/2					
Pr = 4.26 kips 1.6Pr	<0.5Py First-Or	der Analysis A	Allowed (A-7-1	I)	
Py = 533.60 kips					
$N = 0.01 \cdot Yi (A-7-2)$		Use:	TS8X6X1/2		
B2 = 1.02  OK,  A-8-6		Fy =	46.00	ksi	
MWL = 8.10  kip-ft		K =	1.00		:
M Seis = 4.08 kip-ft		L, Col =	10.00	ft	
MDL(Nod) = 0.09  kip-ft		A =	11.60	in^2	
M LL(Nod) = 0.22  kip-ft		[=	62.50	in^4	
M Unbal DL= 4.24 kip-ft		Cm =	1.00		
M Unbal LL= 11.59 kip-ft		Pe1 =	395.43	kips	
M Unbal WL= 7.68 kip-ft		B1 =	1.02	(A-8-3)	
		P,AII =	266.89	kips	
		M, All =	57.30	kip-ft	
Load Combination	Pr, Kips	Mr, Kip-ft	Equation	Result	
D+L	4.26	16.43	0.29	OK	
D+W	1.20	20.46	0.36	OK	
D+0.7E	1.20	7.31	0.13	OK	
D+0.75W+0.75L	3.49	25.44	0.45	OK	
D+0.75(0.7E)+0.75L	3.49	15.58	0.28	OK	

Top Connection: Welded Moment	Base Plate: MODLBP8 - 30

Spread Footing Design

From Column			****		Unbalanced	Load to Colur	nn	
P dl =	1.20	kips		_	M dl =		kip-ft	<del></del>
P II =	3.06	kips			M II =		kip-ft	
P wl =	-1.98	kips			M wl =		kip-ft	
					From Latera		·	
Soil Density =	110	pcf			M wl =	8.10	kip-ft	
Width =	6.50	ft			M el =	6.63	kip-ft	
Length =	6.50	ft						LENGTH
Depth =	3.00	ft						LENGTH/2 LENGTH/2
e =	2.58	ft					<del></del>	
a =	0.00	ft						
b =	0.00	ft					WIDTH	r l
c =	0.00	ft						- b
ķ	(ern = L/6 =		1.08	ft				PM
Footing	Weight =		19.01					<del> </del>
Soil	Weight =		0.00	•			<del>,                                    </del>	
	Ū			•			DEPTH	
Total Loads to S	pread Foo	ting					ال	
PDL =	20.21	kips		MDL =	7.34	kip-ft		
PLL =	3.06			MLL =	19.50	kip-ft		
PWL =	-1.98	kips		MWL =	10.67	kip-ft		
				MEL =	6.63	kip-ft		

				Soil Pressure
Load Combination	Pr, Kips	Mr, Kip-ft	ecc, ft	psf
D+L	23.27	26.84	1.15	808.41
D+W	18.24	18.01	0.99	495.15
0.6D+W	10.15	15.08	1.49	259.94
0.6D+0.7E	12.13	9.05	0.75	154.70
D+0.7E	20.21	11.98	0.59	410.22
D+0.75W+0.75L	21.02	29.97	1.43	851.85
D+0.75(0.7E)+0.75L	22.51	25.45	1.13	759.20

q(ALLOW)= 1500.00 psf OK

### REINFORCING:

M = 20911.77 ft-lbs/ft

Assume: f'c=3000 psi, Fy=40000 psi

d =

32.63 in

As(REQ'D)=

0.44 in^2

As(PROV.)=

0.59 in^2

OK

USE #6's AT 9"O.C. T&B, EACH WAY

Foundation: (Restrained at Grade)

 $d^2=(4.25*M)/(S3*b)$ 

M(MAX)=	32897 ft-lbs	Pmax=	4.26 kips
S3=	100 PCFXd	Footing Area=	7.07 ft^2
b=	3.000 ft	Bearing=	602.48 psf
d=	7.753 ft	-	·
Footing=	Round		
USE:	3.00 FT.RND. X	8.00 ft deep footing	

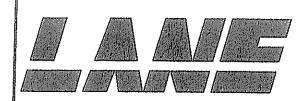
As=12\*M/(jd\*24000)=

0.4406 in^2

USE:

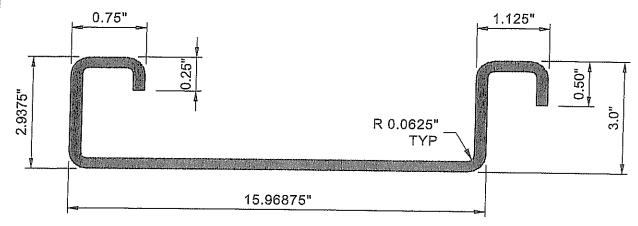
10 #8's (RND. Cage) w/ #4 Ties @ 4" O.C. w/135 degree hooks In The Top 3'-0" of The Footing, #4 Ties @ 12" o.c w/ 135 Degree Hooks In The Balance of Footing

Footing design to allow offset column placement of 1'-9" from centerline of footing.



LANE SUPPLY, INC.

120 Fairview Arlington, Texas 76010 817-261-9116



# SL-316 DECK PANEL

	Section Properties											
Gage.	Wt, psf	Thickness, in	ASTM 653	+!, in <sup>4</sup>	-l, in⁴	+S, in <sup>3</sup>	-S, in <sup>3</sup>	+M, ft-lbs/ft	-M, ft-lbs/ft			
20	2.20	0.0359	Grade 40	0.9346	0.4680	0.3961	0.3036	592.70	454,44			
	2.20		Grade 50	0.9208	0.4522	0.3879	0.2880	725.86	538.92			
18	2.93	0.0478	Grade 40	1.2486	0.6827	0.5329	0.4377	797.77	655.28			
	· mesti e militare a a que sa e e a a a a a a a a a a a a a a a a	and the same of th	Grade 50	1.2129	0.6518	0.5141	0.4296	962.09	803.92			

### Notes:

- 1 Designed per AISI Cold Formed Steel Manual, 2007 ed.
- 2 Complete calculations are available upon request.
- 3 ± M is allowable bending moment.

Issued 12-5-14

O Di-4- M		.11		1.E.e. 1			
	oment Capac				Beam Over		
Desig	gn Moment =	18.70	Kip-Ft	Assumes on	lly Moment Lo	ading	
		_					
	BOLT			PLATE			
	Material:	A325		Fy =	36.00	ksi	
	Diameter:	0.88	in.	t =	2.25	in.	
Tensi	ile Capacity:	26.50	kips	a =	1.50	in.	
				b =	1.50	in.	
	COLUMN:	TS8X6X1/2		BEAM:	W6X20		
	Fy ≃	46.00	ksi	Fy =	36.00	ksi	
	w =	6.00	in.	bf =	6.02	in.	
	tw =	0.29	in.	tf =	0.37	in.	
				tw =	0.26	in.	
				gage =	3.50		
				33			
Bending w/Pr	ying on the F	lange of the W	/F				······
-			******				
B =		kips/Bolt					
T =		kips/Bolt					
b =	1.62	in.					
a =	1.26	in.					
b' =	, 1.18	in.		Use 3/8" Stif	ffeners In Hea	ader	
a' =	1.70	in.		W/ 5/16" Fille	et Welds		
p =	3.00	in.					
ġ' =	0.94						
delta =	0.69						
rho =	0.70						
Beta =	1.11	****				•	
alpha' =	1.00						
t'reqd =	0.88	in	OTICENIED	פ מבטים ואו מ	r= Λ h δ	•	
rrega –	0.00	UI.	SHEENER	S REQ'D IN B	EAM		
Bending w/Pr	ying on the C	ap Plate					
B =		kips/Bolt			· · · · · · · · · · · · · · · · · · ·		
T =		kips/Bolt					
b =	1.50						
a =	1.50						
b' =	1.35						
a' =	1.94						
p =	1.75						
d' =	0.94						
delta =	0.46						
rho =	0.70						
no = Beta =		114.					
	1.10						
alpha' =	1.00	in					
t'reqd =	1.33	III.					

Can Dlata M		_: <u>.</u> .		1 A (* 1 - P**)	5 0	
Cap Plate Me			IZ: E1		Beam Over	
Desi	gn Moment =	18.70	Kip-Ft	Assumes on	nly Moment Lo	ading
	POL 1	r		D! A T.		
	BOL1			PLATE		
	Material:	A325		Fy =	36.00	
	Diameter:	0.88		t =	<del>-</del>	
lensi	ile Capacity:	26.50	kips	a =	1.50	
				b =	1.50	in.
	COLLINANI.	TOOYOYAYO		Pro. pro. A & A	14121404	
	COLUMN:	TS8X6X1/2		BEAM:	W8X21	
	Fy =	46.00		Fy =	36.00	
	w =	6.00		bf =	5.27	
	tw =	0.29	in.	tf =	0.40	
				tw =	0.25	in.
				gage =	2.75	in.
Bending w/Pr	rying on the F	lange of the V	<u>/F</u>			
B =	26.50	king/Polt				
T =		kips/Bolt				
b =		kips/Bolt				
_	1.25					
a =	1.26					
b' =	0.81				ffeners In Hea	ader
a' =	1.70			W/ 5/16" Fill	et Welds	
p =	3.00					
d' =	0.94					
delta =	0.69					
rho =	0.48	ın.				
Beta =	1.61					
alpha' =	1.00		_			
t'reqd =	0.73	in.	STIFFENER	S REQ'D IN B	EAM	
Ponding w/Dn	uina on the C	'an Diata				
Bending w/Pry		kips/Bolt				
T =		kips/Bolt				
b =	1.50					
a = b' =	1.50 1.35				1	
a' =	1.94					
p =	1.38					
d' =	0.94					
delta =	0.32					
rho =	0.70	ın.				
Beta =	1.10					
alpha' =	1.00					
t'reqd =	1.58	ın.				

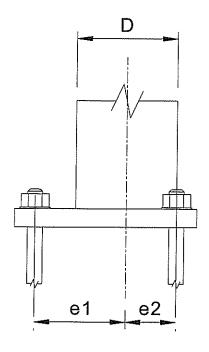
Moment = 30.00 kip-ft Column = TS8X6X1/26 in. D =e1 = 9 in. e2 = 3 in. Anchor Bolts = 1 1/2 in t plate = 2.00 in A36 Steel Plate Fy = 36 ksi E70 Electrode Fw= 0.928 kips / in / 16th A307 Anchor Bolts Ft = 20 ksi

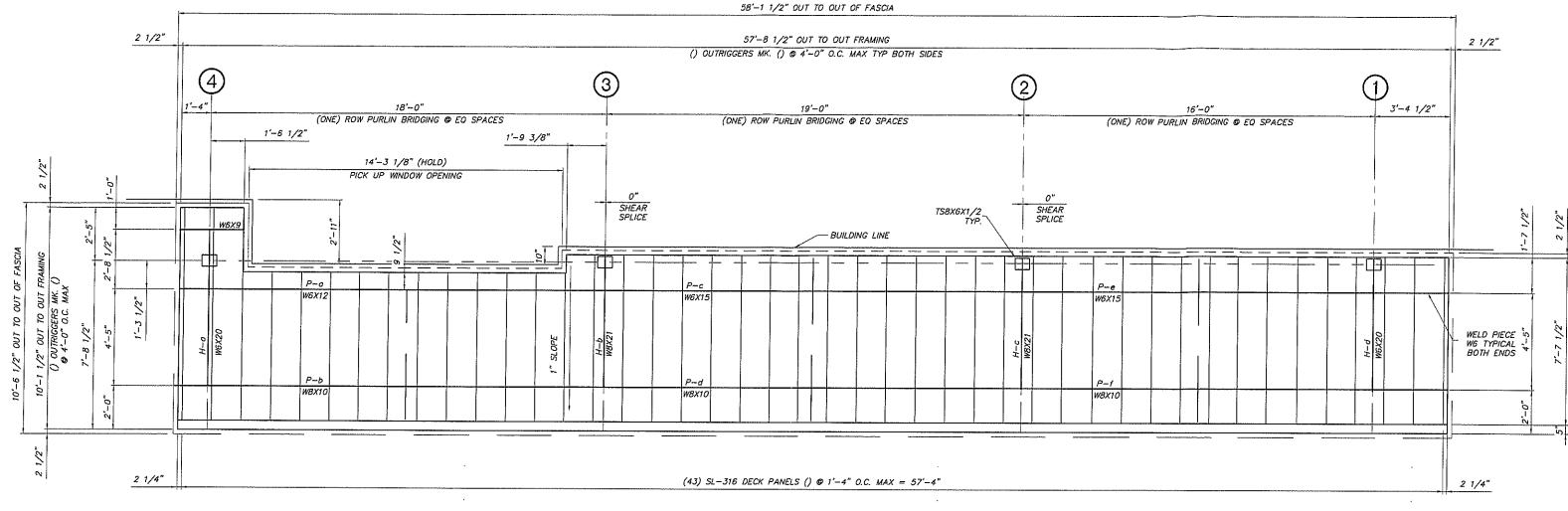
### Clockwise Moment

Pbolt = 12.86 kips < 35.3, OK t(req'd) = 1.69 in t(actual) = 2.00 in Weld(req'd) = 4.62 /16th's Weld(actual) = F.P. /16th's

### Counter-Clokwise Moment

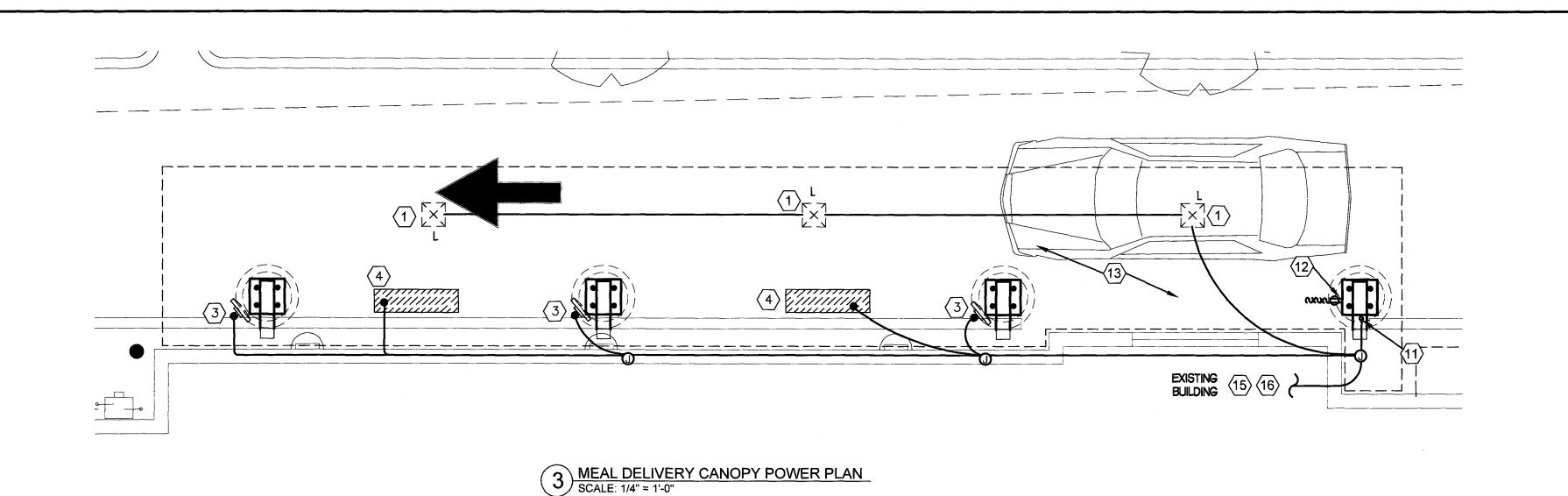
Pbolt = 22.50 kips < 35.3, OK

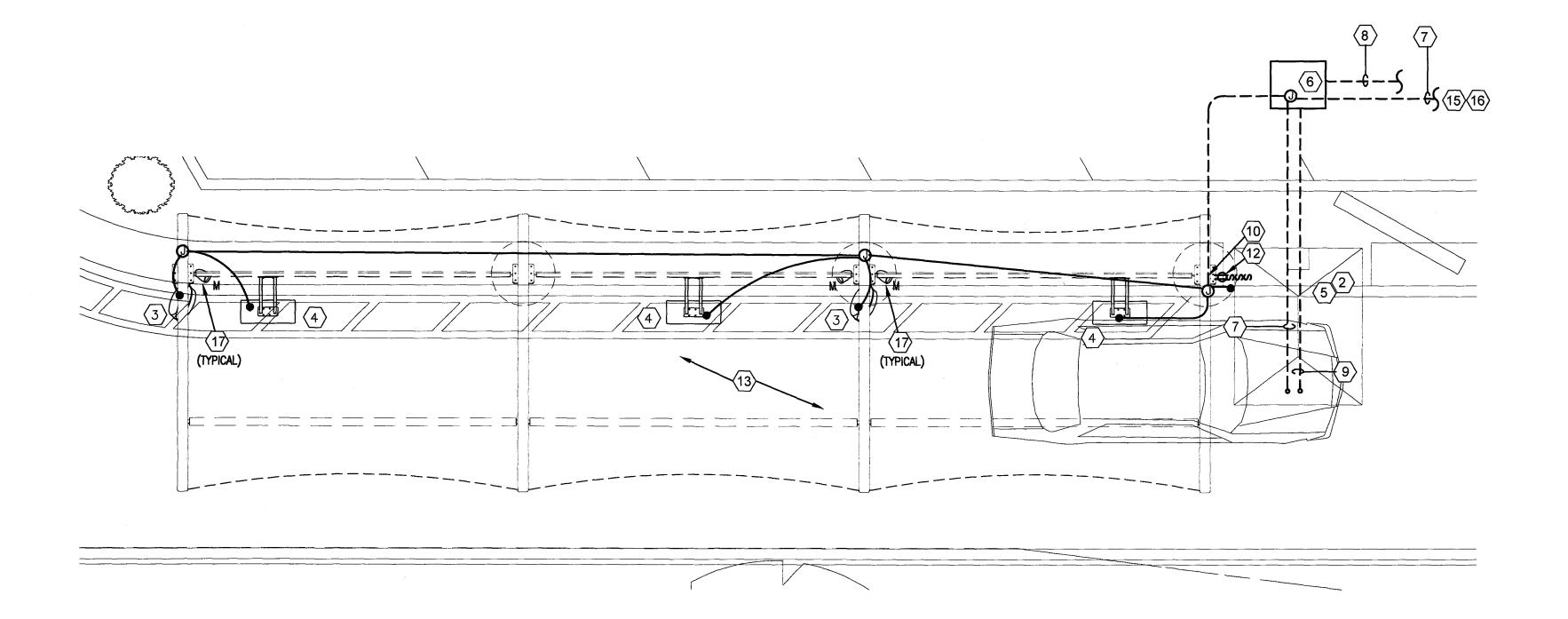




# DESIGN LOADS:

```
DEAD LOAD = 3 p.s.f.(DECK + LIGHTS) + WEIGHT OF STRUCTURAL COMPONENTS
                                   LIVE LOAD = 20 \text{ p.s.f.}
                                   SNOW LOAD = 20^{\circ} p.s.f.
                                V, ULT = 116 m.p.h. EXP. C
                                V, ASD = 90 m.p.h. EXP. C
                       BLDG CODE = 2015 INTERNATIONAL BUILDING CODE
                           EQUIVALENT LATERAL FORCE PROCEDURE
LATERAL FORCE RESISTING SYSTEM = CANTILEVERED COLUMN SYSTEM-ORDINARY STEEL MOMENT FRAME
                                       Pf = 20 p.s.f.
                                        Ce = 1.2
                                         Ct = 1.2
                                         ls = 1.0
                             W = DRIFT LOADS NOT CONSIDERED
                             Pd = DRIFT LOADS NOT CONSIDERED
                                     SITE CLASS = D
                                     Ss(0.2) = 0.44
                                      S1(1.0) = 0.13
                                        SDS = 0.43
                                        SD1 = 0.20
                                        Fa = 1.45
                                        Fv = 2.27
                                        R = 1.25
                             SEISMIC IMPORTANCE FACTOR = 1.0
                                    RISK CATEGORY = II
                               SEISMIC DESIGN CATEGORY = D
                                       CS = 0.340
                                 CONSTRUCTION TYPE = IIB
                                OCCUPANCY CATEGORY = M
                   TOTAL SEISMIC BASE SHEAR BOTH DIRECTIONS = 1.38 KIPS
```





LEGEND ---- UNDERGROUND ABOVE GROUND

ORDER CANOPY POWER PLAN

# KEYED NOTES (-)

- $\langle 1 \rangle$  CEILING LIGHT PROVIDED BY CANOPY SUPPLIER AND INSTALLED BY E.C.
- $\langle 2 
  angle$  existing open/closed lights on order canopy.
- $\langle 3 
  angle$  AIR CIRCULATING FAN (WITH INTEGRAL ON-OFF SWITCH) PROVIDED BY OTHERS. FANS TO BE HARDWIRED IN APPROPRIATE CONDUIT ABOVE CANOPY
- 4 INFRARED GAS HEATER WITH INTEGRAL ON-OFF SWITCH PROVIDED BY OTHERS.
- (5) EXISTING MENUBOARD WITH CANOPY.
- $\langle 6 
  angle$  EXISTING IN-GROUND QUAZITE PULLBOX FOR SLOP DATA CABLES WITH POWER NEMA 3R JUNCTION BOX MOUNTED INSIDE THE PULLBOX.
- $\langle 7 \rangle$  EXISTING 2" UNDERGROUND SCH40 PVC CONDUIT WITH POWER CONDUCTORS, SEE WIRING SCHEMATIC.
- (8) EXISTING 2" UNDERGROUND SCH40 PVC CONDUIT FOR AUDIO SYSTEM/DETECTOR LOOP CABLES.
- (9) EXISTING 1" EMPTY UNDERGROUND SCH40 PVC CONDUIT FOR AUDIO SYSTEM/DETECTOR LOOP CABLES.
- 10 INSTALL UNDERGROUND 3" SCH40 PVC CONDUIT UP INTO THE CANOPY COLUMN WITH TYPE MC CABLE (GALVANIZED STEEL WITH PVC JACKET) RUN WITHIN FOR THE 120V POWER FOR LIGHTS, 120 VOLT POWER FOR FANS, AND 24 VOLT POWER FOR THE INFRARED GAS HEATERS.
- (11) AT EXISTING BUILDINGS STUB A 3" CHASE THRU THE EXTERIOR WALL FROM THE CEILING SPACE ABOVE THE KITCHEN TO ABOVE THE CANOPY'S COLUMN FOR THE MC CABLE POWER CIRCUITS TO GO THRU THE COLUMN MOUNTED SWITCHES AND OUTLET.
- (12) PROVIDE ONE DUPLEX GFCI (WITH IN-USE WP COVER PLATE) AND THREE 120V SINGLE-POLE SWITCHES (EACH WITH HUBBELL #RW51550 WP COVER PLATE) MOUNTED ON THE COLUMN IN FLUSH MOUNTED METAL SINGLE GANG BOXES FOR LOCAL ON-OFF CONTROL OF THE FAN, HEATERS, AND CANOPY LIGHTS. SEE WIRING SCHEMATIC AND CANOPY COLUMN DETAILS FOR FURTHER INFORMATION. ALL SURFACE MOUNTED ITEMS AND COVER PLATES TO BE FIELD PAINTED MATTE BLACK. INSTALL BLANK COVERPLATE WHEN HEATERS ARE NOT INSTALLED AND THE THIRD SWITCH IS NOT REQUIRED.
- (13) ALL CONDUIT AND BOXES SHALL BE CONCEALED FROM NORMAL VIEW; UNDERGROUND, IN COLUMNS, OR ABOVE THE CANOPY (ON THE ROOF). MC CABLE (GALVANIZED STEEL WITH PVC JACKET) TO BE USED INSIDE THE COLUMNS, BUT MUST CONVERT BACK TO IMC ABOVE THE ROOF. ALL EXPOSED ELECTRICAL BOXES TO BE NEMA 3R CAST-METAL.

- 14 NOT USED
- $\langle 15 \rangle$  PROVIDE ONE (1) 20A/1P CIRCUIT FOR LIGHTS AND ONE (1) 20A/1P CIRCUIT FOR FANS. CONNECT TO NEXT AVAILABLE SPARE/SPACE IN LIGHTING PANEL FOR EACH. CONTRACTOR SHALL PROVIDE APPROPRIATE BREAKER SIZE AND LOAD. LIGHTING LOAD ON CIRCUIT NOT TO EXCEED 1.8 KW. FIELD VERIFY NUMBER OF SPARES/SPACES PRIOR TO BID. REPORT ANY DISCREPANCIES TO ENGINEER PRIOR TO CONSTRUCTION.
- $\langle 16 \rangle$  PROVIDE ONE (1) #8 CU EQUIPMENT GROUND TO BE BONDED TO CANOPY STRUCTURE AND GAS PIPING PER MANUFACTURER'S RECOMMENDATIONS.
- (17) COLUMN MOUNTED SINGLE LIGHT PROVIDED BY OTHERS/GC AND INSTALL BY E.C.

NOTES: FOR ALL CONDUITS: REFER TO PLANS FOR OTHER CONDUITS, REFER TO VENDOR DRAWINGS FOR CONDUIT AND WIRING REQUIREMENTS FOR LOW VOLTAGE SYSTEMS AND CONTROL WIRING.

MULTIPLE 1PH CIRCUITS MAY OCCUPY THE SAME CONDUIT IN ACCORDANCE WITH THE NEC, MAXIMUM OF THREE AND OF DIFFERENT PHASES.

LOW VOLTAGE AND CONTROL WIRING SHALL BE IN SEPARATE CONDUIT FROM BUILDING TO CANOPY.

# LIGHTING FIXTURE (LUMINAIRE) SCHEDULE - CHICK-FIL-A

<u> </u>								
MARK	MANUFACTURER	CATALOG NUMBER	NO. LAMPS/TYPE	SYL LAMP NO.	WATTS	VOLTS	MOUNTING	REMARKS
М	ACCUSERV	HBLED26YB4.0/R14-3B	LED	_	26	120	MOUNTED ON COLUMN	REFER TO NOTE #2 IN THIS SCHEDULE
L	LSI INDUSTRIES	LSI CRUS_SM-SC-LED-LW-30-CW-UE-WHT	LED	_	74	120	MOUNTED ON CANOPY	

LUMINAIRES UTILIZING DOUBLE-ENDED LAMPS AND CONTAIN BALLASTS THAT CAN BE SERVICED IN PLACE SHALL HAVE A DISCONNECTING MEANS EITHER INTERNAL OF EXTERNAL TO EACH LUMINAIRE PER THE LIGHTING FIXTURE PACKAGE IS AVAILABLE THROUGH A NATIONAL ACCOUNT PROGRAM.

NOTE! AS NOTED IN THE SPECIFICATIONS, ALL WIRING LAYOUTS, LAYOUTS ARE SCHEMATIC. EXACT LOCATIONS SHALL BE DETERMINED BY THE CONSTRUCTION AND STRUCTURE OF THE BUILDING AND SHALL BE VERIFIED AND COORDINATED IN THE FIELD. EACH TRADE CONTRACTOR SHALL VERIFY WITH THE GENERAL CONTRACTOR THAT

FIELD VERIFY ALL CONDITIONS

HE HAS THOROUGHLY REVIEWED AND COORDINATED ALL LOCATIONS AND ROUTINGS WITH ALL OTHER TRADES PRIOR TO FABRICATION OF CONDUITS, DUCTS, OR PIPING, AND START OF INSTALLATION OF SAME (INCLUDING SPRINKLER PIPING WHEN PRESENT ON JOB). ANY INSTALLATION OR CONSTRUCTION CONFLICTS WHICH OCCUR IN THE FIELD SHALL BE RESOLVED BY THE TRADE CONTRACTOR TO THE SATISFACTION OF THE OWNER AND ARCHITECT AND AT NO EXPENSE TO THE OWNER, ARCHITECT AND/OR GENERAL CONTRACTOR.

THE CONTRACTOR SHALL CONTACT THE ARCHITECT, ENGINEER OR OWNER PRIOR TO BIDDING FOR INTERPRETATIONS AND CLARIFICATIONS OF THE DESIGN AND INCLUDE IN HIS BID ALL COSTS TO MEET THE DESIGN INTENT. CLARIFICATIONS MADE BY THE ARCHITECT, ENGINEER OR OWNER AFTER BIDDING WILL BE FINAL AND SHALL BE IMPLEMENTED AT CONTRACTORS COST.

BIDDING CONTRACTORS SHALL HAVE A WORKING KNOWLEDGE OF LOCAL CODES AND ORDINANCES AND SHALL INCLUDE IN THEIR BIDS THE COSTS FOR ALL WORK INSTALLED IN STRICT ACCORDANCE WITH GOVERNING CODES, THE PLANS AND SPECIFICATIONS NOT WITHSTANDING, THE CONTRACTOR SHALL ALERT ARCHITECT, ENGINEER OR OWNER OF ANY APPARENT DISCREPANCIES BETWEEN GOVERNING CODES AND DESIGN INTENT.

COMPARIS	SON LOAD	SUM	MARY		
EXISTING LOAD BASED ON DATA RECEIV	VED .				
				899.77	AMP
	QTY.		WATTS	AMPS	S
-DRIVE THRU CANOPY LIGHTS	3	Χ	26	0.2	AMP
-MEAL DELIVERY CANOPY LIGHTS	3	Χ	74	0.6	AMP:
-DRIVE THRU CANOPY FANS	2	Χ	264	1.5	AMP:
-MEAL DELIVERY CANOPY FANS	3	Χ	264	2.2	AMP:
TOTAL ADDED AMPS				4.5	AMP:
NEW CONNECTED AMPS				904.3	AMP
EXISTING SERVICE SIZE IS 1000 AMPS	BASED ON EXIS	STING DA	TA RECEIVED		

ALBUQUERQUE, NM 87109 CANOPY POWER AND LGT PLAN

CANOPY ROLL OUT

PROGRAM FSU 2793

5009 MONTGOMERY

BLVD NE,

**INTERPLAN** 

ENGINEERING INTERIOR DESIGN PROJECT MANAGEMENT

604 COURTLAND STREET

ORLANDO, FLORIDA 32804 PH 407.645.5008 FX 407.629.9124

5200 Buffington Atlanta Georgia, 30349-2998

Revisions:

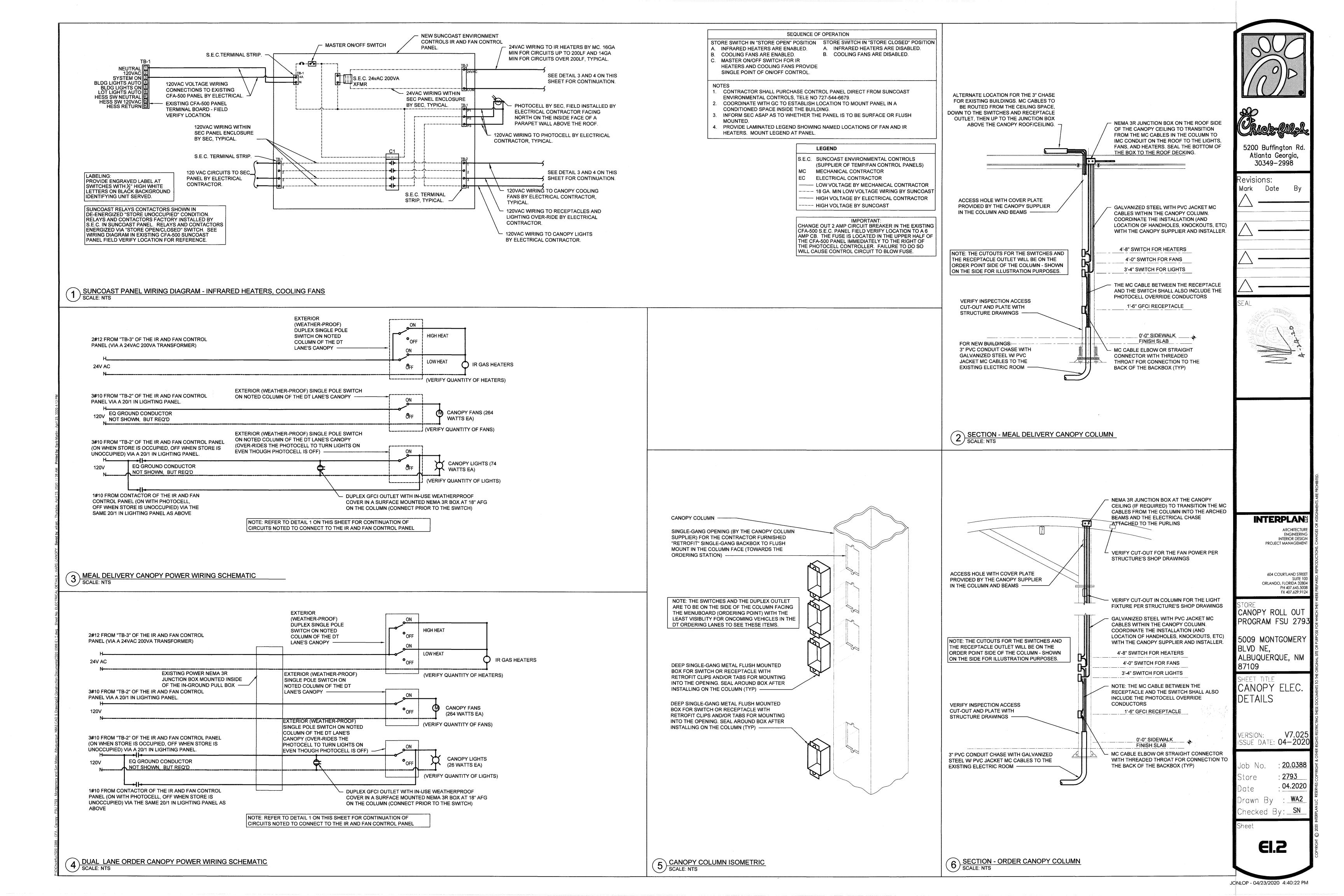
Mark Date

SUE DATE: 04-202

: <u>2793</u> . 04.2020 Checked By: <u>SN</u>

EI.I

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### GUST EFFECT FACTOR: 0.85 SEISMIC DESIGN: SEISMIC LOAD DOES NOT CONTROL THE DESIGN BASED ON THE ASSUMPTION THAT THE FABRIC HAS NEGLIGIBLE MASS

FABRIC: 0.20 PSF

GROUND SNOW LOAD: 10 PSF

SNOW EXPOSURE FACTOR: 1.0

ULTIMATE WIND SPEED: 115 MPH NOMINAL WIND SPEED: 90 MPH WIND IMPORTANCE FACTOR: 1.0 WIND EXPOSURE CATEGORY: C

THERMAL FACTOR: 1.2

ROOF LIVE LOAD: 5 PSF

ROOF SNOW LOAD: 0 PSF (SEE OWNER NOTES)

SNOW LOAD IMPORTANCE FACTOR: 1.0

SNOW LOAD:

IVE LOAD:

WIND LOAD:

OWNER NOTES FABRIC MEMBRANE(S) MUST BE REMOVED IF LIVE LOAD/ROOF SNOW LOAD IS EXPECTED TO EXCEED 15 PSF AND/OR THE WIND SPEED IS EXPECTED TO EXCEED A NOMINAL DESIGN WIND SPEED OF 86 MPH OR 76 MPH SUSTAINED WIND LOAD TO PREVENT DAMAGE. THE OWNER ACCEPTS FULL RESPONSIBILITY OF REMOVING THE FABRIC FROM THE STEEL FRAME

WHEN ANY OR ALL OF THESE CONDITIONS MAY OCCUR. the Steel Structure with the fabric removed, was designed to withstand dead LOADS, ROOF LIVE LOADS, SNOW LOADS AND WIND SPEEDS AS SPECIFIED ABOVE PER THE LOCAL CODE REQUIREMENTS. IF THE ABOVE LOADS ARE EXCEEDED OR ADDITIONAL LOADS ARE INDUCED STRUCTURAL FAILURE MAY OCCUR. THE OWNER IS RESPONSIBLE FOR AND ACCEPTS FULL LIABILITY FOR ANY ISSUES CAUSED BY EXCEEDING THE DESIGN CRITERIA LOADS.

### **GENERAL NOTES** . FABRIC MEETS NFPA 701-04. 2. ALL EXPOSED STEEL TO BE POWDERCOATED.

FOUNDATION DESIGN

CONCRETE COMPRESSIVE STRENGTH AFTER 28 DAYS: 3,000 PSI STEEL REINFORCEMENT: ASTM-A615, GRADE 60

ASSUMED VERTICAL FOUNDATION PRESSURE: 1,500 PSF

ASSUMED LATERAL BEARING PRESSURE: 100 PSF/F THE VERTICAL AND LATERAL BEARING PRESSURE VALUES WERE CONSIDERED PER CONDITIONS OF CURRENT BUILDING CODE.

THE FOUNDATION DESIGN IS BASED ON TABLE 1806.2 OF THE INTERNATIONAL BUILDING CODE, CLASS 5 SOIL MATERIAL. IF THE FOOTING DEPTH DOES NOT MEET LOCAL FROST REQUIREMENTS, FOOTINGS SHALL BE RE-ESIGNED UNDER THE DIRECTION OF AN ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY

# TO VERIFY THE LOCAL FROST DEPTH.

MATERIALS

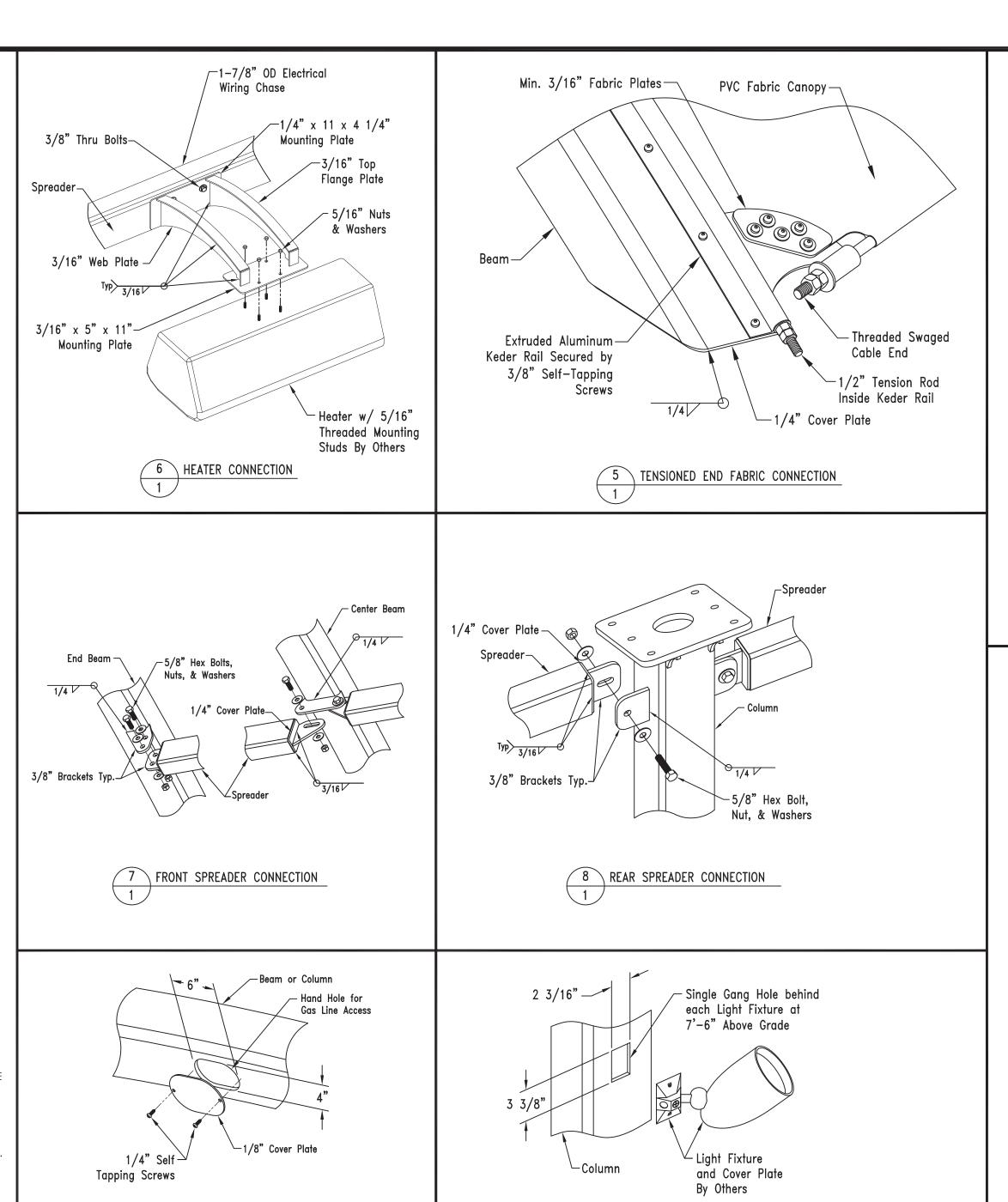
1. ALL MATERIALS LISTED BELOW MAY NOT BE SPECIFIC TO THIS PROJECT.

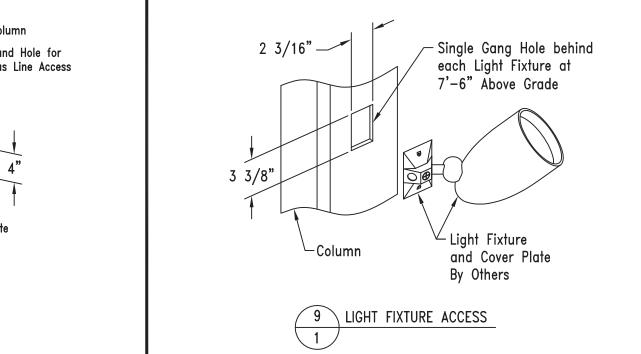
1. ALL MATERIALS LISTED BELOW MAT NOT BE STECTIVE TO THIS TROSLET.								
MEMBER TYPE	ASTM	MIN. YIELD STRENGT						
W SHAPES	A992	50 KSI						
RECTANGULAR HSS TUBES	A500(GRADE B)	46 KSI						
SQUARE HSS TUBES	A500(GRADE B)	46 KSI						
round hss tubes	A500(GRADE B)	42 KSI						
SCHEDULE PIPE	A500(GRADE B&C)	50 KSI						
ROUND MECHANICAL TUBING	A519	45 KSI						
MISCELLANEOUS PLATES/SHAPES	A36	36 KSI						
CONNECTION BOLTS	A325	92 KSI						
headed anchor bolts	F1554	36 KSI						
hooked anchor bolts	A307	36 KSI						

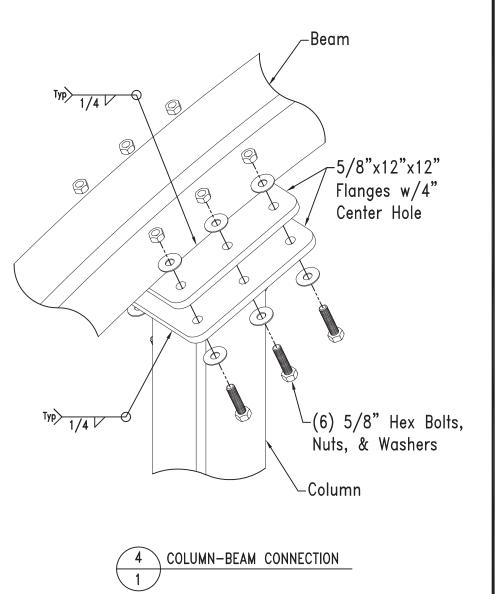
1/4" STAINLESS AIRCRAFT CABLE SHALL HAVE A NOMINAL STRENGTH OF 6,400 LBS.

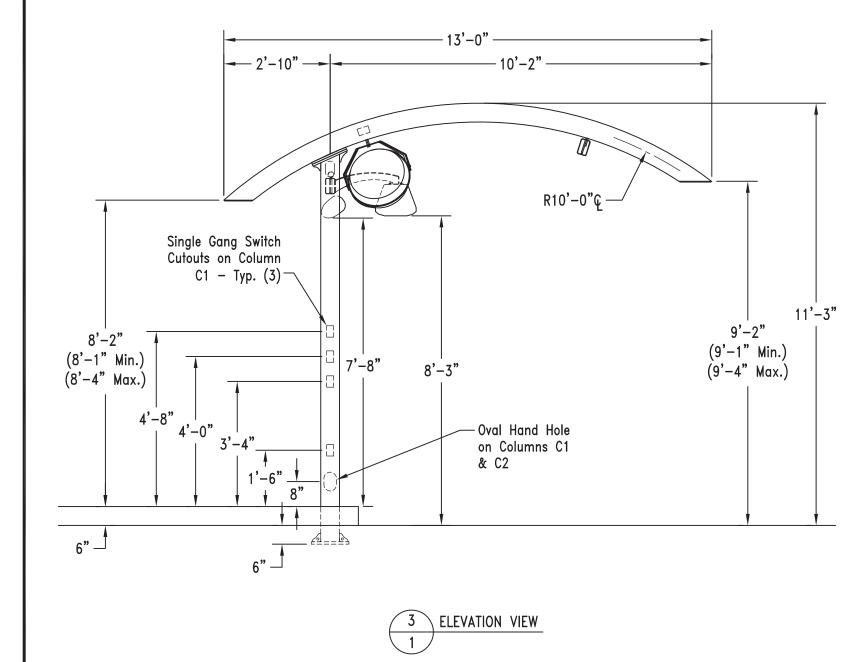
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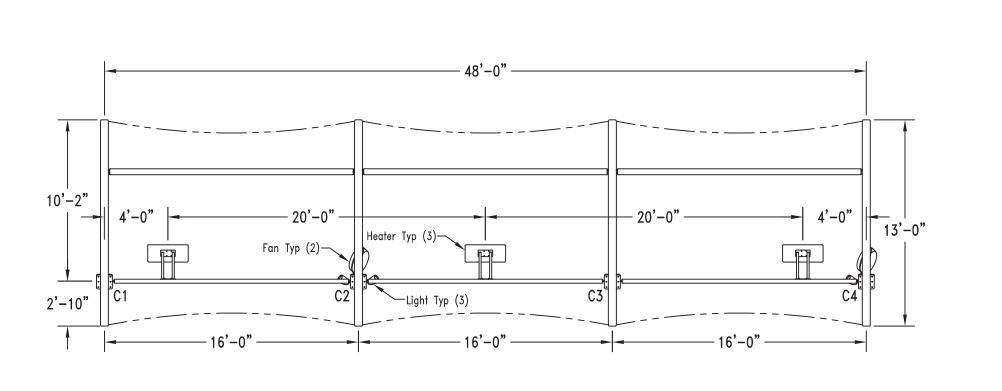
l.	TABLE								
	STRUCTURE	EAVE HEIGHT	COLUMN SIZE	BEAM SIZE	SPREADER SIZE	FOOTING SIZ & REINF.			
	CFA 48'x13' Single Lane	9'–2" Above Grade	6" × 6" 1/4" Wall	6" × 6" 3/8" Wall	5" x 3" 3/16" Wall	As Per Sheet 2			

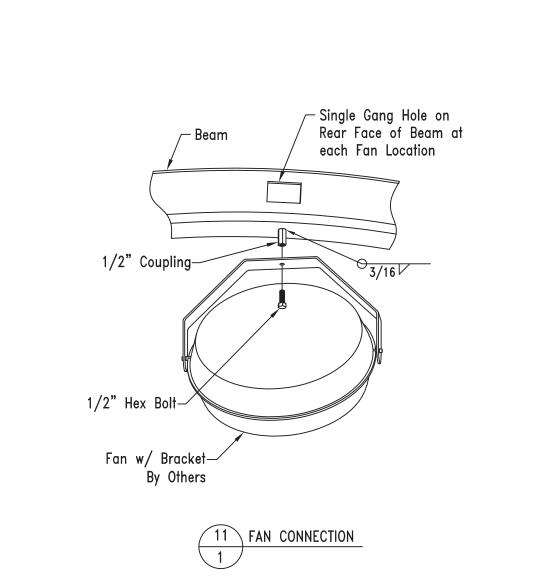




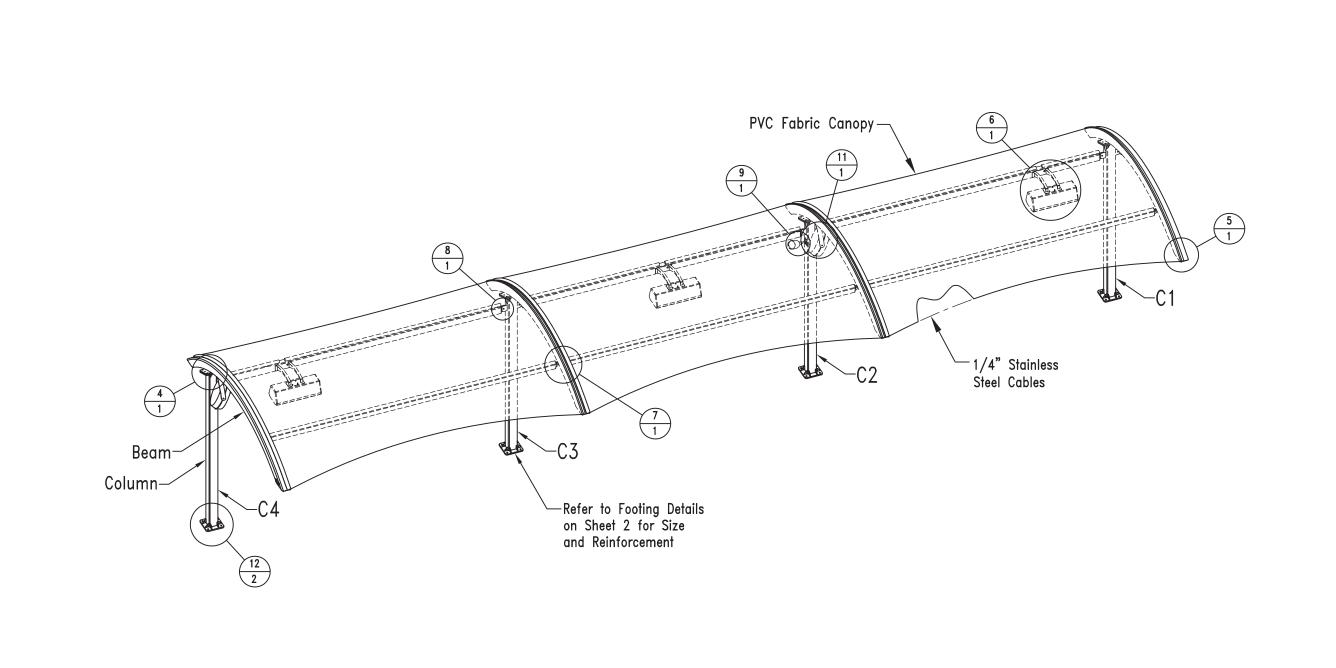




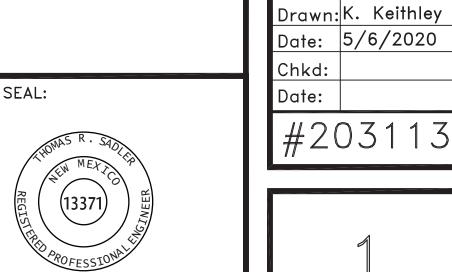




10 ACCESS COVER CONNECTION



1 CUSTOM SHADE STRUCTURE



Sheet No.

Revisions:

Date: By:

B

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Superio Adamson Carrollton,

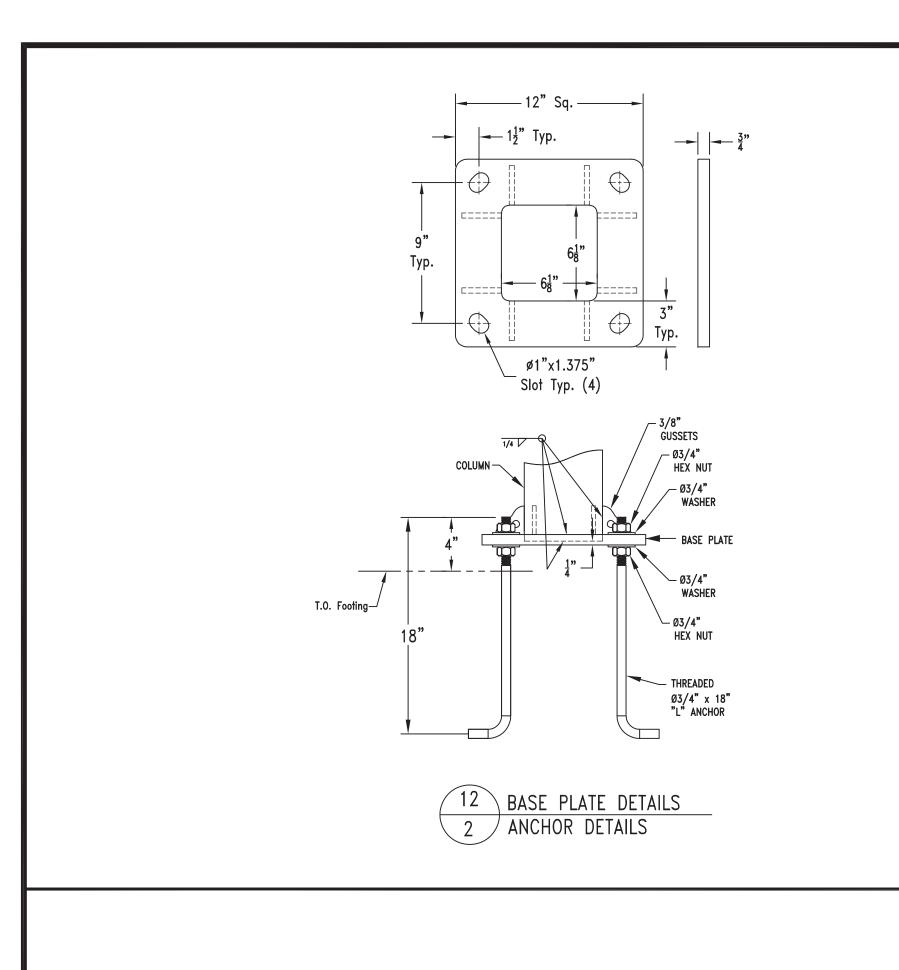
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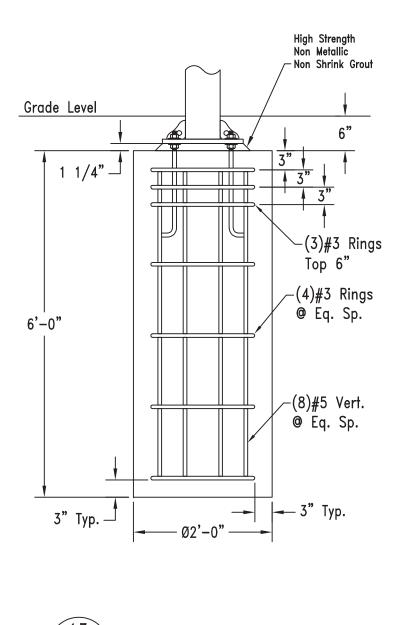
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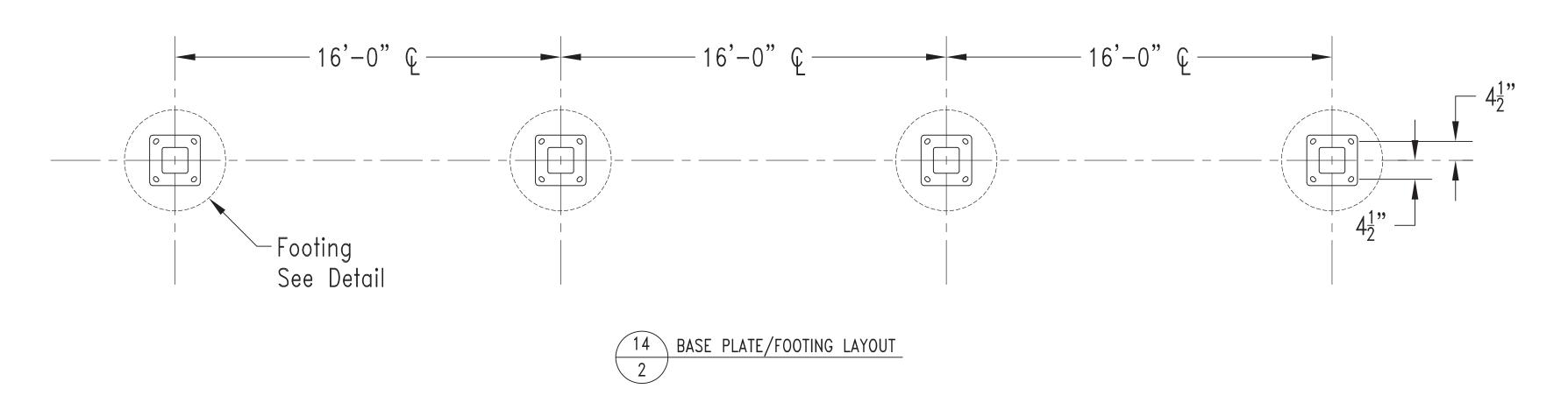
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Ы Z





13 AUGER FOOTING DETAIL



STATE OF NEW

MEXICO

IS THE EXCLUSIVE ANUFACTURER ED OR REPRODUCED Store#

Shade

SUPERIORAL PRODUCTS

Superior Shade ) Adamson Industrial Blvd. Carrollton, GA 30117

150

IS PLAN/DRAWING IS THE EXCLUS OPERTY OF THE MANUFACTURER D MAY NOT BE USED OR REPRODIOLE OR IN PART WITHOUT THE WRMISSION FROM THE MANUFACTURI

Revisions:

Date: By:

Drawn: K. Keithley
Date: 5/6/2020
Chkd:

Date: #203113

Sheet No.

SEAL:

REGISTIONAS R. SADITOR NEXT CONTRACTOR NEXT CONTRACTOR

