



DEVELOPMENT REVIEW BOARD APPLICATION

Please check the appropriate box(es) an of application.	d refer to	supplemental fo	orms for submittal requ	irement	ts. All fees must be	paid at the time		
SUBDIVISIONS	☐ Fina	l Sign off of EPC Sit	e Plan(s) (Form P2)					
☐ Major – Preliminary Plat (Form P1)	☐ Ame	endment to Site Plan	(Form P2)	□ Vac	cation of Public Right-of-	-way (Form V)		
☐ Minor – Preliminary/Final Plat (Form S2)	MISCE	LLANEOUS APPLI	CATIONS	☐ Vacation of Public Easement(s) DRB (Form V)				
☐ Major - Final Plat (Form S1)	□ Exte	ension of Infrastructu	re List or IIA (Form S1)	☐ Vacation of Private Easement(s) (Form V)				
☐ Amendment to Preliminary Plat (Form S2)	☐ Mino	or Amendment to Inf	rastructure List (Form S2)	PRE-A	APPLICATIONS			
☐ Extension of Preliminary Plat (FormS1)	□ Tem	nporary Deferral of S	W (Form V2)	□ Ske	etch Plat Review and Co	mment (Form S2)		
	☐ Side	ewalk Waiver (Form	V2)					
SITE PLANS	☐ Wai	ver to IDO (Form V2	2)	APPE	AL			
□ DRB Site Plan (Form P2)	☐ Wai	ver to DPM (Form V	2)	□ Dec	cision of DRB (Form A)			
BRIEF DESCRIPTION OF REQUEST								
				_				
APPLICATION INFORMATION								
Applicant:					one:			
Address:			T		nail:			
City:			State:	Zip:				
Professional/Agent (if any):			one:					
Address:					nail:			
City:			State:	Zip):			
Proprietary Interest in Site:	logal dos	enintien is enveigl	List all owners:					
Lot or Tract No.:	iegai des	scription is crucial!	Block:					
Subdivision/Addition:			MRGCD Map No.:	Unit: UPC Code:				
Zone Atlas Page(s):	Fyi	sting Zoning:	WINGOD Wap No		Proposed Zoning			
# of Existing Lots:		f Proposed Lots:			Total Area of Site (Acres):			
LOCATION OF PROPERTY BY STREETS		T Topocod Lote.		1.0	tar, 110a 01 0 100 (7 to100).			
Site Address/Street:	Bet	ween:		and:				
CASE HISTORY (List any current or prior pro	ect and ca	ase number(s) that	may be relevant to your re	equest.)				
Signature: Killy M. K.				Da	ite:			
Printed Na					Applicant or ☐ Agent			
FOR OFFICIAL USE ONLY								
Case Numbers Act	ion	Fees	Case Numbers		Action	Fees		
				<u> </u>				
Meeting Date:			Ι		e Total:			
Staff Signature:			Date:	Pr	oject #			



Courtyard I 7500 Jefferson St. NE Albuquerque, NM 87109-4335

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May 22, 2020

Ms. Jolene Wolfey, DRB Chair City of Albuquerque Planning Department 600 2nd Street NW Albuquerque, NM 87103

Re: Montage Unit 4 Subdivision – Preliminary Plat

Dear Ms. Wolfey:

Enclosed for Development Review Board (DRB) preliminary plat review and comment are digital copies of the following information:

- Agent Authorization Letter
- Application for Development Review
- Zone Atlas Maps
- Proof of Neighborhood Meeting coordination
- Landfill disclosure Statement
- Preliminary Plat
- Drainage Report and Grading Plan
- Proof of Water and Sewer Availability Request Letter
- Infrastructure List
- Overall Paving Plan showing the proposed street cross sections and site plan
- Sidewalk Deferral and Waiver
- TIS form
- Submittal Fees (to be paid online)

This preliminary plat is being presented to the Development Review Board for the purpose of obtaining City review and approval. It represents the 4th Unit to Mesa del Sol, Montage Subdivision – a private residential development. Inspiration encompasses 34 acres subdivided into 189 lots of varying sizes and 6 private open space tracts. Roadway right-of-way and pavement widths are indicated on the preliminary plat and cross section exhibit.

We request that this item be scheduled for the next appropriate DRB hearing. Please feel free to contact me at 505-318-7815 with questions or comments.

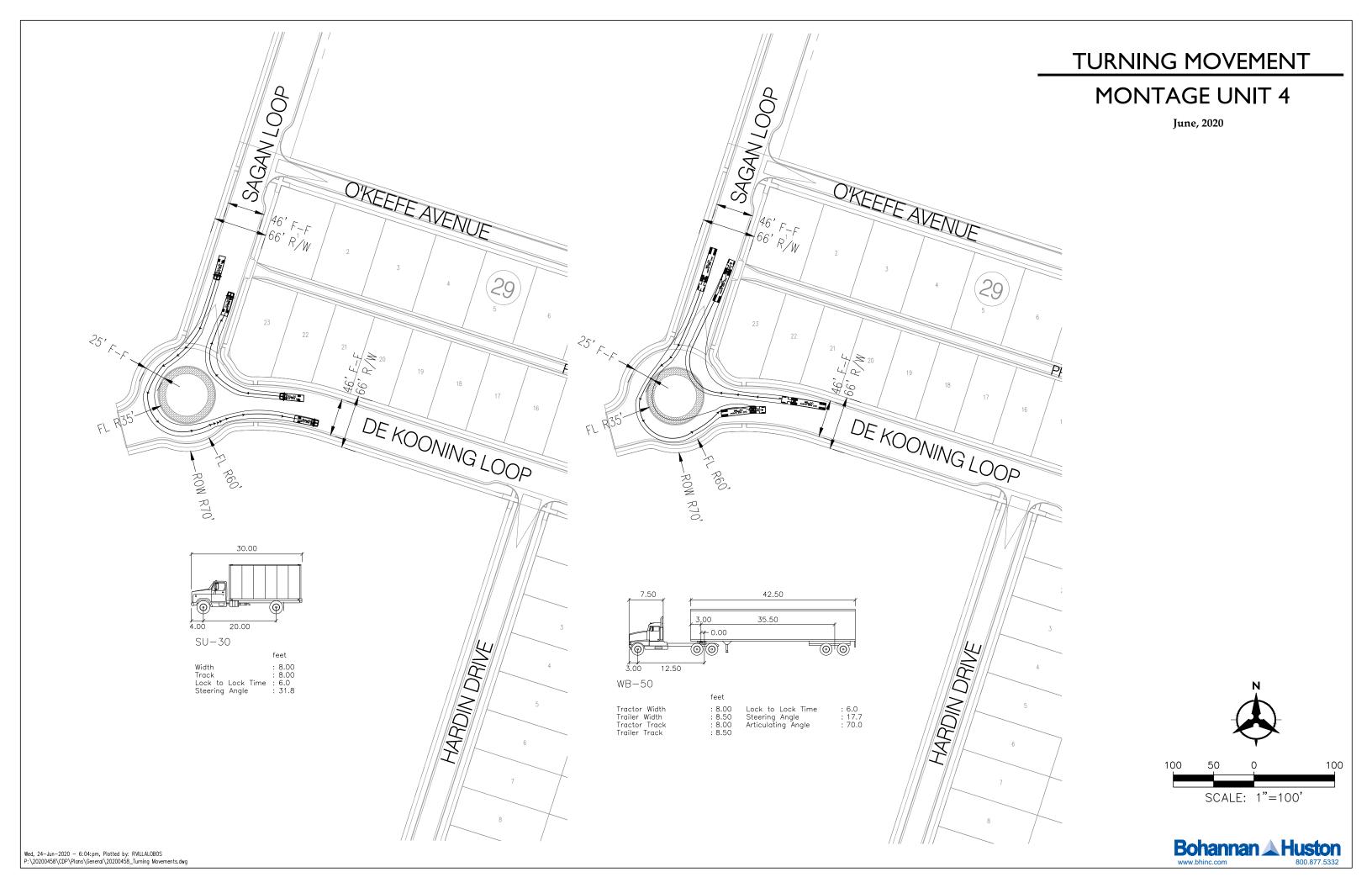
Sincerely,

Kelly M. K.

Kelly M. Klein P.E.
Project Manager
Community Development and Planning

Engineering A

Spatial Data A



DRAINAGE REPORT
FOR
MESA DEL SOL
RESIDENTIAL
MONTAGE UNIT 3 AND 4

AMENDMENT (REVISED FOR UNIT 4)

MAY 2020

Prepared for:

Corazon del Mesa 3B, LLC 9600 Tennyson St. NE

Bohannan A Huston

Engineering
Spatial Data
Advanced Technologies



UNIT 4 AMENDMENT TO:

DRAINAGE REPORT
FOR
MESA DEL SOL
RESIDENTIAL
MONTAGE UNIT 3 AND 4

(ORIGINAL: JANUARY 2019) AMENDED MAY 2020

Prepared for:

MESA DEL SOL, LLC 5700 UNIVERSITY BLVD WEST SE - SUITE 310 ALBUQUERQUE, NM 87106

Prepared by:

BOHANNAN HUSTON, INC. COURTYARD I 7500 JEFFERSON STREET NE ALBUQUERQUE, NM 87109

Prepared By:

1 05/22/202

Kelly Klein, P.E Design Engineer Date

TABLE OF CONTENTS

I.	PURPOSE	1
II.	CONCEPTS AND METHODOLOGIES	1
III.	SITE LOCATION AND CHARACTERISTICS	1
IV.	EXISTING HYDRAULIC AND HYDROLOGIC CONDITIONS	2
٧.	DEVELOPED HYDRAULIC AND HYDROLOGIC CONDITIONS	2
	A. PERMANENT STORM WATER DETENTION PONDS	
	B. ONSITE DEVELOPED BASINS	4
	1. OUTFALL 'A'	4
	2. OUTFALL 'B'	4
	3. Outfall 'C'.	
VI.	CONCLUSION	5
	APPENDICES	
ΑP	PENDIX A - STREET HYDRAULICS, STORM DRAIN INLET ANALYSIS, ANI HYDRAULICS	O ALLEY
AP	PENDIX B - INFILTRATION CALCULATIONS	
ΑP	PENDIX C - POND VOLUME CALCULATIONS	

EXHIBITS

EXHIBIT 1 -	UNIT 4 PRELIMINARY PLAT
EXHIBIT 2 -	Amended DEVELOPED CONDITIONS BASIN MAPS
EXHIBIT 3 -	Amended INLET AND STORM DRAIN ANALYSIS
EXHIBIT 4 -	GRADING PLAN

APPENDIX D - BASIN SUMMARY SHEET

I. PURPOSE

This purpose of this drainage amendment is to amend the approved drainage report, Drainage *Report for Mesa Del Sol Residential Montage Unit 3 and 4*, *January 2019*, due to the revised layout for Unit 4 from the previous drainage report. Unit 4 consists of 189 single family detached and attached residential lots on approximately 37 acres which will be developed as one unit. The new layout introduces new basin configurations and revises the storm drain network from the previous approved report within the Unit 4 boundary. Unit 3 is currently constructed in accordance with the above approved drainage report and will not be altered by Unit 4. This amendment is submitted in support of grading approval and preliminary plat approval for Montage Unit 4 by the DRB.

II. CONCEPTS AND METHODOLOGIES

The same concepts and methodologies are implemented for this amendment as in the original Drainage Report and are listed in summary below.

- Drainage conditions were analyzed utilizing the 100-year, 6-hour storm event in accordance with the COA *DPM*. The results are included in Appendices A through C. Street capacity and storm drain inlet calculations supporting this new layout for Unit 4 are located in Appendix A.
- 2. Onsite runoff will be captured by retention ponds, which are designed to retain and infiltrate approximately the 2-year storm volume, as well as the 100-year 10-day storm volume. Pond 2A will be upsized to accommodate the flows from Unit 4.
- 3. This amendment conforms to the Level B Master Plan for Mesa del Sol.
- 4. This amendment conforms to the prior approved drainage reports.
 - Drainage Report for Mesa del Sol Residential Montage Unit 1 and 2, prepared by Bohannan Huston, Inc., dated January 2011. COA Record # R16D0034
 - Drainage Report for Mesa del Sol Residential Montage Unit 3 and 3, prepared by Bohannan Huston, Inc., dated January 2019. COA Record # R16D006.

III. SITE LOCATION AND CHARACTERISTICS

As mentioned in the previous report, Mesa del Sol Residential Montage Unit 3 and 4 will be developed in two units, Unit 3 and 4. Unit 3 has been constructed. Unit 4 is the subject of this amendment.

The site has been previously graded with relatively flat slopes and generally slopes from west to east at an average grade of about 0.5%.

IV. EXISTING HYDRAULIC AND HYDROLOGIC CONDITIONS

The land comprising Mesa del Sol Residential Montage Unit 4 is currently undeveloped, but was graded several years ago. Ponds 2A, 2B, 3 and 4 are currently graded and accept developed runoff from existing Units 1 and 2, as well as undeveloped runoff to the west of these ponds. Pond 3 and 4 have been graded and certified as part of the Financial Guaranty Release for COA Record # R16D006. Ponds 2A and 2B have also been graded to contain approximately 11.5 ac-ft at a MWSEL of 5300'. Runoff generated by Unit 4 in its present state drains toward the existing ponding areas 2A and 2B.

V. DEVELOPED HYDRAULIC AND HYDROLOGIC CONDITIONS

A. PERMANENT STORM WATER DETENTION PONDS

Ponds 1, 2A, 2B, 3, and 4 function as retention ponds for this project and in the future, which is consistent with the drainage concept throughout the Mesa del Sol area, both commercial and residential. Per the Master Plans and the approved Drainage Reports, Ponds 1, 2A, 2B, and 3 will act in series as a single "linear pond" with flows capable of moving from one pond into another thus equalizing the volume in each pond to a maximum surface elevation of 5300". The capacities of the ponds required for the development of Unit 4 are presented Pond Summary Table below.

Pond 4 was designed and built to accept developed flows from a developed Unit 4 as laid out in the original drainage report. Since the new Unit 4 layout does not change the runoff volume going to Pond 4, Pond 4 will not require any additional volume and will remain in its current configuration

Existing ponds 2B and 3 were designed and built per the original drainage report to accept developed flows from developed Units 1, 3 and 4. These ponds will remain in their current configuration. The new Unit 4 will divert some of the intended flow from Pond 3 into Pond 2A. Pond 3 will therefore continue to have adequate capacity for the developed flows discharging directly into it and will have additional available volume for equalizing overflow from the other ponds in series with it.

Pond 2A was originally designed to assist in accommodating flows from Montage Units 1 and 2 as well as the offsite flows from the west - with the intent to upgrade and increase the capacity of the ponds, as needed, when further development of the Mesa Del Sol area is completed. With the build-out of Unit 4, Pond 2A will be increased to accommodate the flows from Unit 4. The offsite flows from the west are directed towards Pond 2A. Since Ponds 2A, 2B and 3 act as a single pond, the additional volume of runoff generated from the offsite flows will be captured in the additional cumulative capacity of the linear ponds without requiring the construction of Future Pond 1 at this time.

In addition, in conformance with the previous drainage reports. Pond 2A will also be designed to infiltrate the more frequent 2-yr (90th percentile) storms within 96 hours, but construction at this time will exclude the forebay design and installation. This improvement will be provided at a later date with a separate grading submittal. Infiltration calculations follow the same methodology as the previous reports and are found in Appendix B.

POND SUMMARY - REQUIRED VOLUMES FOR CURRENT BUILDOUT OF UNITS 1,2, 3 AND 4											
POND	MAX WSEL	REQ'D STORAGE VOLUME (AC-FT)	MAX DEPTH (FT)	Existing AVAILABLE VOLUME (AC-FT)	Proposed AVAILABLE VOLUME (AC-FT)						
1 (Future)	N/A	0.0	N/A	N/A	N/A						
2A	5300.0	9.2	7.0	4.5	7.7						
2B	5300.0	7.6	11.0	7.0	7.0						
3	5300.0	8.5	11.0	11.2	11.2						
TOTAL*		25.4		22.7	25.9						
4	5291.0	8.62	8.0	10.2	10.2						

NOTES:

- * PONDS 1, 2A, 2B AND 3 ARE INTENDED TO ACT AS ONE POND PER APPROVED DRAINAGE PLANS
- 1. EXISTING POND 2A IS INTENDED TO CAPTURE OFFSITE FLOWS UNTIL FUTURE POND 1 IS CONSTRUCTED
- 2. EXISTING POND 4 HAS BEEN CONSTRUCTED
- 3. POND 2A WILL BE UPSIZED BY THIS PROJECT TO ACCOMMODATE FLOWS FROM UNITS 4, AS WELL AS UNITS 1, 2, 3

B. ONSITE DEVELOPED BASINS

The new layout for Unit 4 differs slightly from the original drainage report, and the basin boundaries for Unit 4 have been modified to accommodate the grading and drainage of the new layout while being in conformance with the previous master plans. One notable basin change is the addition of a portion of the original "Future Basin 1" to "Future Basin 4". These newly defined Basins are identified as Future Basin 1a, and Future Basin 4a and Future Basin 4b on the Amended Developed Conditions Basin Map for Unit 4 found in Exhibit 2-1. Exhibit 2-2 overlays the new basin boundaries over the original basin boundaries and shows the differences in runoff areas.

1. OUTFALL 'A'

Outfall 'A' discharges into Pond 3 and consists of Basins A-1, A-2, A-3, A-4, A-5 and A-6, as well as a portion of Future Basin 1, as shown on the Developed Conditions Basin Map from the original Drainage Report. Unit 4 modifies some of the basin boundaries, but, under the new configuration, flow that was intended to enter this Outfall "A" system was actually directed to the new "Outfall C" system. See Exhibit 2-2. The flow within Outfall "A" system was reduced from 122 cfs to 106 cfs. The new flows are identified on the Amended Inlet and Storm Drain Analysis Map found in Exhibit 3. See Appendix A for the revised street hydraulics and storm drain inlet analysis.

2. OUTFALL 'B'

Outfall 'B' discharges into Pond 4 and consists of Basins B-1, B-2, B-3, B-4, B-5, B-6, B-7, Future Basin 2 and Future Basin 3, as well Future Basin 1a as shown on the Developed Conditions Basin Map from the original Drainage Report. Although Unit 4 makes some changes to the original Basin boundaries and inlet locations due to final grading, these flows remain the same as the original Outfall "B" system. See Exhibit 2. Appendix A shows the street hydraulics and storm drain inlet analysis for the new Unit 4 storm drain extension in Scorsese Avenue that is part of Outfall "B".

3. OUTFALL 'C'.

This outfall consists of Basin C-1, C-2, C-3, C-4, Future Basins 4a and 4b. These flows will enter proposed storm drain inlets within these basins and ultimately discharge into Pond 2A. Flows in this Outfall "C" system are greater than anticipated in the prior approved drainage reports. See Exhibit 2-1 for the Basin Map contributing to Outfall "C". Appendix A

shows the street hydraulics and storm drain inlet analysis for the new Unit 4 storm drain in DeKooning and Sagan Loop that is part of Outfall "B".

VI. CONCLUSION

Onsite developed runoff generated by the site will be conveyed to retention ponds utilizing surface street flows in conjunction with underground public storm drain pipe networks. The linear ponds 2A, 2B and 3 are connected in series to act as one pond with a maximum surface elevation of 5300. The cumulative volume of these ponds is capable of retaining the 100 yr -10 day storm for the onsite and offsite flows. The drainage concept outlined by this Amendment consists of retention ponding of developed Unit 4 runoff consistent with existing development throughout Mesa del Sol, and in conformance with previously approved Level A and Level B Master Plan drainage concepts and prior approved drainage reports.

APPENDICES

APPENDIX A: STREET HYDRAULICS, STORM

DRAIN INLET ANALYSIS AND

ALLEY HYDRAULICS

APPENDIX B: INFILTRATION CALCULATIONS

APPENDIX C: POND VOLUME CALCULATIONS

APPENDIX D: BASIN SUMMARY SHEET

APPENDIX A

STREET HYDRAULICS, STORM DRAIN INLET ANALYSIS, AND ALLEY HYDRAULICS

Street Section Capacities

66ft row 0.4%

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
1.0	0.0	0.9	4.0	12.0	0.1	7.0	56.0	0.0
2.0	9.4	0.7	5.0	33.0	0.6	8.0	56.6	0.7
3.0	10.0	0.0	6.0	54.0	0.1	9.0	66.0	0.9

WSEL	DEPTH INC	FLOW AREA	FLOW RATE	WETTED PER	FLOW VEL	TOPWID PLUS	TOTAL ENERGY
FT.		SQ.FT.	(CFS)	(FT)	(FPS)	OBSTRUCTIONS	(FT)
0.100	0.100	0.169	0.125	3.481	0.737	3.388	0.108
0.200	0.200	0.866	0.831	11.970	0.960	11.788	0.214
0.300	0.300	2.548	3.334	22.129	1.308	21.858	0.327
0.400	0.400	5.237	8.611	32.288	1.644	31.929	0.442
0.500	0.500	8.934	17.475	42.447	1.956	41.999	0.560
0.600	0.600	13.514	32.242	47.664	2.386	47.128	0.689
0.700	0.700	18.279	51.113	50.815	2.796	50.219	0.822
0.800	0.800	23.794	70.473	60.680	2.962	60.082	0.936

52ft row 0.4%

POINT DIST 1.0 0.0 2.0 11.4 3.0 12.0	ELEV 0.9 0.7 0.0	PC	OINT 4.0 5.0 6.0	DIST 14.0 26.0 38.0	ELEV 0.1 0.4 0.1	PC	7.0 40 8.0 40	SST ELEV 0.0 0.0 0.6 0.7 2.0 0.9
WSEL FT.	DEPTH INC	FLOW AREA SQ.FT.	FLO RAT (CF	E	WETTED PER (FT)	FLOW VEL (FPS)	TOPWID PLUS OBSTRUCT	ENERGY
0.100 0.200 0.300 0.400 0.500 0.600 0.700 0.800 0.900	0.100 0.200 0.300 0.400 0.500 0.600 0.700 0.800 0.900	0.169 0.863 2.535 5.160 8.045 10.949 13.914 17.631 22.337	0.1 0.8 3.3 9.0 18.7 31.1 43.4 54.0	30 20 03 53 47 13	3.481 11.905 21.978 29.111 29.385 29.660 32.819 42.708 52.597	0.737 0.961 1.310 1.745 2.331 2.845 3.120 3.065 3.124	3.388 11.723 21.707 28.752 28.940 29.128 32.226 42.113 52.000	0.214 0.327 0.447 0.585 0.726 0.851 0.946

Stryker_half section-slope-0.51%

POINT 1.0 2.0	DIST 0.0 9.4	ELEV 0.9 0.7	PC	INT 3.0 4.0	DIST 10.0 12.0	ELEV 0.0 0.1	PC		DIST 33.0	ELEV 0.6
WS FT		DEPTH INC	FLOW AREA SQ.FT.	FLO RAT (CF	E	WETTED PER (FT)	FLOW VEL (FPS)	TOPW PLU OBSTRU		TOTAL ENERGY (FT)
0.0 0.0 0.0 0.1 0.1 0.1 0.1 0.2 0.2 0.2	40 60 80 00 20 40 60 80 00 22 40 60 80	0.020 0.040 0.060 0.080 0.100 0.120 0.140 0.160 0.200 0.220 0.240 0.260 0.280 0.300	0.003 0.014 0.030 0.054 0.085 0.122 0.170 0.237 0.325 0.433 0.561 0.709 0.877 1.065 1.274	0.0 0.0 0.0 0.0 0.1 0.1 0.2 0.3 0.4 0.6 0.8 1.1	06 18 39 70 15 58 27 29 69 50 78 57	0.348 0.696 1.044 1.392 1.740 2.088 2.937 3.953 4.969 5.985 7.001 8.017 9.033 10.049 11.065	0.285 0.452 0.592 0.717 0.832 0.940 0.933 0.957 1.013 1.083 1.160 1.239 1.319 1.398 1.477	0.3 0.6 1.0 1.3 1.6 2.0 2.8 3.8 4.8 5.8 6.9 7.9 9.9	78 16 55 94 33 73 80 87 94 01 08 15 22	0.021 0.043 0.065 0.088 0.111 0.134 0.154 0.174 0.196 0.218 0.241 0.264 0.287 0.310 0.334
0.3 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.5 0.5	20 40 60 80 00 20 40 60 80 00 20	0.300 0.320 0.340 0.360 0.400 0.420 0.440 0.460 0.480 0.500 0.520 0.540	1.274 1.503 1.751 2.020 2.309 2.619 2.948 3.297 3.667 4.057 4.467 4.897 5.347	2.3 2.8 3.4 4.1 4.8 5.6 6.5 7.5 8.6 9.8 11.1 12.5	37 59 51 18 62 87 97 94 83 66 46	11.065 12.080 13.096 14.112 15.128 16.144 17.160 18.176 19.192 20.208 21.223 22.239 23.255	1.477 1.555 1.632 1.708 1.783 1.857 1.929 2.001 2.071 2.140 2.209 2.276 2.343	10.9 11.9 12.9 13.9 14.9 16.9 17.9 18.9 21.0 22.0 23.0	36 43 50 57 64 71 78 85 93 00	0.334 0.358 0.381 0.405 0.429 0.454 0.478 0.502 0.527 0.551 0.576 0.601 0.625

36ft row_one way (per X section) 0.4%

POINT	DIST	ELEV	P	TNIO	DIST	ELEV	P	OINT	DIST	ELEV
1.0	0.0	0.7		4.0	6.0	0.0		7.0	24.0	-0.3
2.0	4.3	0.5		5.0	14.5	-0.2		8.0	24.7	0.3
3.0	5.0	0.0		6.0	23.0	-0.3		9.0	36.0	0.6
WSE:	L	DEPTH	FLOW	FI	LOW	WETTED	FLOW	TO)PWID	TOTAL
		INC	AREA	R.F	ATE	PER	VEL	E	PLUS	ENERGY
FT.			SQ.FT.	((CFS)	(FT)	(FPS)	OBST	RUCTIONS	(FT)
-0.24	0	0.100	0.355	0.	. 293	6.142	0.826	7	7.100	0.111
-0.14	0	0.200	1.220	1.	.531	11.285	1.255	12	2.200	0.224
-0.04	0	0.300	2.595	4.	192	16.427	1.616	17	7.300	0.341
0.06	0	0.400	4.452	9.	142	19.669	2.053	19	0.480	0.466
0.16	0	0.500	6.412	16.	618	19.978	2.592	19	714	0.604
0.26	0	0.600	8.395	25.	.774	20.287	3.070	19	9.948	0.747
0.36	0	0.700	10.424	34.	.989	22.031	3.357	21	.630	0.875
0.46	0	0.800	12.840	43.	.112	27.125	3.358	26	5.690	0.975
0.56	0	0.900	15.793	53.	.151	33.250	3.365	32	2.800	1.076

20ft row (alley) 0.4%

POINT	DIST	ELEV	P	OINT	DIST	ELEV	PO	INT DIST	Γ ELEV
1.0	0.0	0.4		4.0	5.5	0.1		7.0 16.0	0.0
2.0	3.4	0.3		5.0	10.0	0.2		8.0 16.6	5 0.3
3.0	4.0	0.0		6.0	14.5	0.1		9.0 20.0	0.4
	_								
WSE	L	DEPTH	FLOW	FLO	W	WETTED	FLOW	TOPWID	TOTAL
		INC	AREA	RAT	E	PER	VEL	PLUS	ENERGY
FT.			SQ.FT.	(CF	S)	(FT)	(FPS)	OBSTRUCTIO	ONS (FT)
0.10	Ο	0.100	0.205	0.1	4 1	4.638	0.690	4.584	0.107
0.20	0	0.200	1.036	1.1	10	12.156	1.071	12.049	0.218
0.30	0	0.300	2.327	4.0	27	13.293	1.730	13.136	0.347
0.40	0	0.400	3.887	7.1	69	20.173	1.844	20.000	0.453

Rothko-sta	14+00. txt
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						Rothk	0-sta 1	1.0044J	ХC			
			MANNTH	16'5 N *	0.017 SLO	PE = 0.60	6					
1.0 2.0 3.0 4.0	0.0 11.4 11.8 12.0	0.9 0.7 0.7 0.7	PC	5.0 1 6.0 2 7.0 3	1ST ELEV 4.0 0.1 6.0 0.4 8.0 0.1 0.0 0.0		9.0 10.0 11.6	015Y 40.2 40.6 52.0	0.7 0.7 0.7 0.9	INLEIS # 1 & #2		
6.10 0.10 0.10 0.10 0.20 0.30 0.30 0.40	50 50 50 50	0.050 0.100 0.150 0.200 0.250 0.300 0.350 0.350 0.400	PLOW AREA SQ.FT. 0.039 0.156 0.366 0.795 1.476 2.408 3.591 4.981	FLOW RATE (CFS) 0.022 0.371 0.911 1.996 3.773 6.377 10.458	3.290 6,318 11,423 16,527 21,631 26,735 28,839	PLOW VEC. (FPS) 0.560 0.889 1.033 1.146 1.353 1.776 2.100	2. 4. 6. 12. 22. 22. 27.	WID JUS RUCTION 484 048 996 021 047 072 098 123 148	YOTAL EMERGY 5 (FT) 0.055 0.112 0.166 0.220 0.278 0.398 0.399 0.469 0.545	LOCATED @ INTERSECTION OF ROTHER & NAUMAN		
 0.50 0.69 0.69 0.70 0.75 0.80	10 10 10 10 10 10	0,450 0,500 0,550 0,550 0,650 0,700 0,750 0,750 0,800 0,850	6.391 7.803 9.217 10.631 12.047 13.536 15.271 17.253 19.482	15.811 21.999 28.965 36.660 45.046 50.311 56.085 63.381 72.298	29.045 29.148 29.251 29.354 33.282 38.227 43.171 48.116	2.474 2.619 3.143 3.448 3.739 3.717 3.673 3.674 3.705	29. 29. 29. 32. 37. 42.	148 174 159 224 250 270 176 113 057	0.545 0.624 6.704 0.785 6.867 0.913 6.960 1.010			
(BASI	~ A	- 1	-	13.2 c	FS		/				
4	3 6	50102	E 04	د. ما	1 - 2.7	2000						
STREET CAPACITY Value CAPACITY Value CAPACITY Value CAPACITY												
,	X =	0.87	10	90'	1	0 L		2	,			
IN	LET	Cf	PACI	74	_/							
		0.65			/							
(0 5.	0.2	40 -	8.2	c Fs							
2-	0.2	— x.	2-0.	6 =>	1.3	- = _!	.4	M	8.12=	25.2-1.8x		
	. /	JAL.	/U-x		ζ.9	/4	-X		×	- 2 9.5 CFS (PEZ DUBLE 'A)		
7	45.	4 CF	5 -2	(9.	S CFS) = ;	26.4	1 0	18			

		0 0 1 5			0.5
MANNING'S	N =	0 017	SLOPE	= (), ()	115

POINT 1.0 2.0	DIST 0.0 11.4	ELEV 0.9 0.7	- 1	POINT DI: 4.0 14 5.0 26	.0 0.1 .0 0.4	PC	DINT DIST 7.0 40.0 40.6	ELEV 0.0 0.7	INLETS 1 + 2
3.0	12.0	0.0		6.0 38	.0 0.1		9.0 52.0	0.9	
									Located @
WSE	CL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	TOTAL	Intersection of ROTHKO + NAUMAN
		INC	AREA	RATE	PER	VEL	PLUS	ENERGY	.^
FT.			SQ.FT.	(CFS)	(FT)	(FPS)	OBSTRUCTIONS	(FT)	KOTHKO + NAVMAN
0.02	20	0.020	0.007	0.002	0.696	0.282	0.678	0.021	
0.04		0.040	0.027	0.012	1.392	0.447	1.355	0.043	
0.06		0.060	0.061	0.036	2.088	0.586	2.033	0.065	
0.08		0.080	0.108	0.077	2.785	0.710	2.710	0.088	
0.10		0.100	0.169	0.140	3.481	0.824	3.388	0.111	
0.12		0.120	0.244	0.227	4.177	0.930	4.066	0.133	
0.14		0.140	0.339	0.314	5.862	0.925	5.733	0.153	
0.16		0.160	0.474	0.450	7.876	0.949	7.729	0.174	
0.18		0.180	0.649	0.652	9.891	1.005	9.726	0.196	
0.20		0.200	0.863	0.928	11.905	1.075	11.723	0.218	
0.22		0.220	1.118	1.286	13.920	1.150	13.720	0.241	
0.24		0.240	1.412	1.735	15.934	1.228	15.717	0.263	
0.26		0.260	1.746	2.283	17.949	1.307	17.713	0.287	
0.28		0.280	2.120	2.940	19.963	1.386	19.710	0.310	
0.30		0.300	2.535	3.712	21.978	1.464	21.707	0.333	
0.32		0.320	2.989	4.608	23.992	1.542	23.704	0.357	
0.34		0.340	3.483	5.635	26.007	1.618	25.701	0.381	
0.36		0.360	4.017	6.800	28.021	1.693	27.697	0.405	
0.38		0.380	4.586	8.278	29.056	1.805	28.715	0.431	
0.40		0.400	5.160	10.065	29.111	1.950	28.752	0.459	
0.42		0.420	5.736	11.990	29.166	2.090	28.790	0.488	
0.44	0	0.440	6.312	14.046	29.221	2.225	28.827	0.517	
0.46		0.460	6.889	16.230	29.276	2.356	28.865	0.546	STREET CAPACITY
0.48		0.480	7.467	18.537	29.331	2.483	28.903	0.576	The same of the sa
0.50	0	0.500	8.045	20.966	29.385	2.606	28.940	0.606	Q= 22.66 CFS
0.52	0	0.520	8.624	23.512	29.440	2.726	28.978	0.636	
0.54	0	0.540	9.204	26.174	29.495	2.844	29.016	0.666	d=0.52 ' K 0.67V
0.56	0	0.560	9.785	28.947	29.550	2.958	29.053	0.696	
0.58	0	0.580	10.366	31.831	29.605	3.071	29.091	0.727	E= 0.63' L 0.90V
0.60	0	0.600	10.949	34.823	29.660	3.181	29.128	0.757	
0.62	0	0.620	11.531	37.921	29.715	3.288	29.166	0.788	
0.64	0 .	0.640	12.115	41.123	29.770	3.394	29.204	0.819	
0.66	0	0.660	12.700	44.428	29.825	3.498	29.241	0.850	
0.68	0	0.680	13.290	46.862	30.841	3.526	30.249	0.873	
0.70	0	0.700	13.914	48.538	32.819	3.488	32.226	0.889	
0.72	0	0.720	14.579	50.454	34.797	3.461	34.203	0.906	· ·
0.74	0	0.740	15.283	52.604	36.774	3.442	36.181	0.924	
0.76		0.760	16.026	54.983	38.752	3.431	38.158	0.943	
0.78		0.780	16.809	57.589	40.730	3.426	40.136	0.963	
0.80		0.800	17.631	60.422	42.708	3.427	42.113	0.983	
0.82		0.820	18.493	63.480	44.686	3.433	44.090	1.003	
0.84		0.840	19.395	66.766	46.663	3.442	46.068	1.024	
0.86		0.860	20.336	70.280	48.641	3.456	48.045	1.046	
0.88	80	0.880	21.317	74.026	50.619	3.473	50.023	1.068	

· Basin A-1 = 22.66CFS

INLET CAPACITY (From Nomograph)

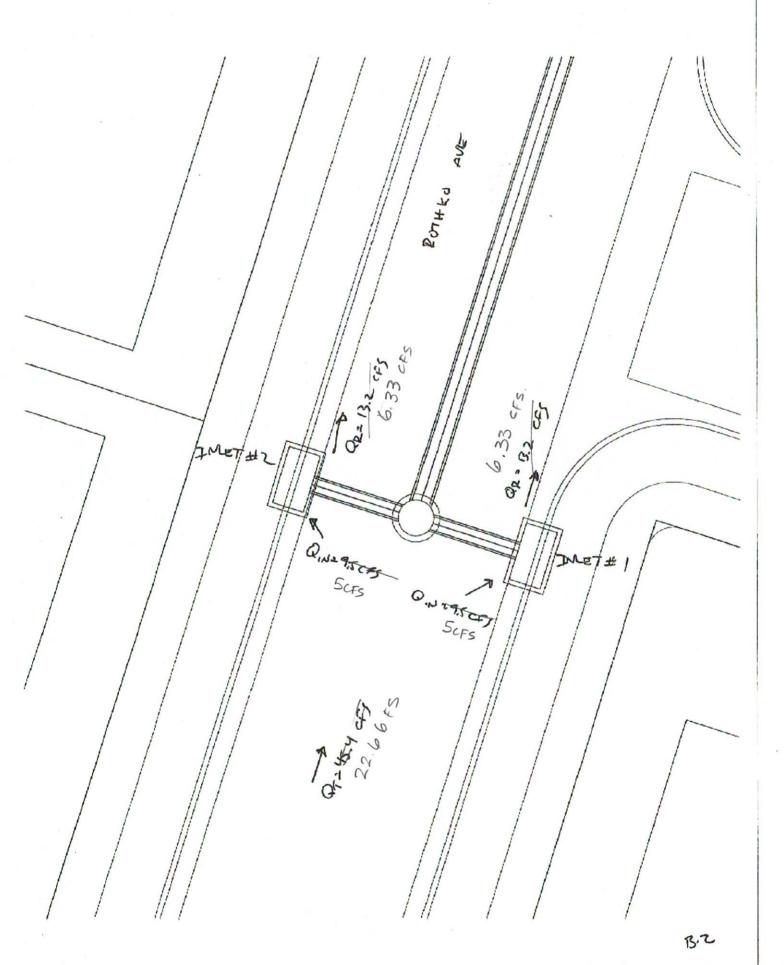
C 5=0.52%

d=0.51

Qinlet = 5.0 cfs.

Per single "A"

RESIDUAL = 22.87 CFS - 2(5.0CFS) = 12,66CFS



B-2 (Rev)

Rothko-sta 16+50.txt

		MANNING'S	N = 0.017 SUC	PE - 0.006	314 144.5.1.		
POINT 1.0 2.0 3.0 4.0	0.0 0.5 21.4 0.7 21.8 0.7	7 FOINT 5.0 6.6 7.0	DIST ELEV 14.0 0.1 26.0 0.4 38.0 0.1	9 10 11	NT DIST 0.0 40.2 0.0 40.6 0.0 52.0	6.7 6.7 6.7 6.9	
	12.0 0.0	, B.G	40.0 0.0	PLOW	TOPWID	TOTAL	INCERS # 3 8 #4
FT.	INC	SQ.FT.	(CFS) (FT)	(FPS)	PLUS OBSTRUCTIONS	EMERGY (FT)	LOCATED @ INTERSECTION
0.05 0.10 0.15	0 100	0.039 0.156 0.366 0.795	0.022 1.645 0.139 3.290 0.371 6.318 0.911 11.423 1.996 16.527	0.560 0.889 1.013 1.146	2.484 4.048 6.996 12.021	0.055 0.112 0.166 0.220 0.278	OF ROTHER & STRAND
0, 15 0, 20 0, 25 0, 30 0, 35	0.300	4108	1.774 73.001	1.353 1.567 1.776	17.647 22.072 27.098	0.278 0.336 0.399 0.469	85 Fe1469 d 2 1544
0.40 0.45 0.50	0 0.400 0 0.450 0 0.500	2 KO3 2	28.839	2.474 2.819	29.123	0.469 0.545 0.624 0.704	
0.55 0.60 0.65 0.70	0 0.600 0 0.650	13.536 50	.999 29.045 .965 29.148 .660 29.251 .048 29.354	3.143 3.448 3.739 3.717	29.174 29.199 29.224 29.250 32.226	0.285 0.867 0.915	
0.75 0.80 0.85	0.750	15.271 54 17.253 65 19.482 72	.085 38.227 .381 43.171 .196 48.116	3.673 3.674 3.706	37.170 42.113 47.057	0.960 1.010 1.064	
	BASIN) A-2	17.0	cfs			A SU
			- 26.4	CFS		6	1/04
	JNLETS	+1H42	43.4	CFT		19/	
		_	13. 1	٠.,	Q	1/2	<i>[</i>
		PACITY					
45	5.048-3	6.66	45,048-	43.4 -	8.3	98	2348 => 0.192536 = 7.2724 -8.388>
			0.867-		0.0	92	2 2348 = 0.192536 = 7.2724 -8.388 x × 2 0.54 -x X 2 0.90' Vak
<i></i>							
TVICE	TCAPA	CITY	_				
45.0	48-36.6	ا ب _ بره	7.048- 43	<u>1</u> >	9.250	3 =_	2.348 => 0.1174 = 5.4522 - 8.758
	5 -0.60	100 mary 100 mg	.65-1	_ 7	0.05	d	2.348 => 0.1174 = 5.4522 - 8.758x
			/				
	@ S = (0.695, d	= 0.64				
		0.24	- 9 CFS				
		240 -	- 3 CFS 13.5 OF,	5			
_	2-0.2	- = 5-	0.6	> 1.0	- > 1.	4	> 7.7: 24.3 - 1.8x y: 9.2 cfs (PEZ DWBLE'A)
13	7.5-5	13.3	-×	5.5	13.5	~×	x = 9.2 CFS (DUBLE'A)
							7
1	REIN	4					
/-	43.	4 CPS -	2(9.2	cfs) =	25.0	CF	3
				,			
					Page 1		

Rothko - Slope 0.52%

			MANNIN	NG'SN = 0	.017 SLOPE	= 0.005	5		
									INLETS 3+4
POINT	DIST	ELEV	PC		ST ELEV	PO	DINT DIST	ELEV	Management (Management American Commission of the Commission of th
1.0	0.0	0.9			0.1		7.0 40.0	0.0	
2.0	11.4	0.7			0.4		8.0 40.6	0.7	1 - + 1 0
3.0	12.0	0.0		6.0 38	0.1		9.0 52.0	0.9	Located @
									Intersection of
WS	SEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	TOTAL	
		INC	AREA	RATE	PER	VEL	PLUS	ENERGY	ROTH KO LSTRAND
FI	۲.		SQ.FT.	(CFS)	(FT)	(FPS)	OBSTRUCTIONS	(FT)	
0.0	200	0.020	0 007	0.002	0.696	0.282	0.678	0.021	
0.0		0.040	0.007	0.012	1.392	0.447	1.355	0.043	
0.0		0.060	0.027	0.012	2.088	0.586	2.033	0.045	
0.0		0.080	0.108	0.030	2.785	0.710	2.710	0.088	
0.1		0.100	0.169	0.140	3.481	0.824	3.388	0.111	
0.1		0.120	0.244	0.227	4.177	0.930	4.066	0.133	
0.1		0.140	0.339	0.314	5.862	0.925	5.733	0.153	
0.1		0.140	0.474	0.450	7.876	0.949	7.729	0.174	
0.1		0.180	0.649	0.652	9.891	1.005	9.726	0.196	
0.2		0.200	0.863	0.928	11.905	1.075	11.723	0.218	
0.2		0.220	1.118	1.286	13.920	1.150	13.720	0.241	
0.2		0.240	1.412	1.735	15.934	1.228	15.717	0.263	
0.2		0.260	1.746	2.283	17.949	1.307	17.713	0.287	
0.2		0.280	2.120	2.940	19.963	1.386	19.710	0.310	
0.3		0.300	2.535	3.712	21.978	1.464	21.707	0.333	
0.3		0.320	2.989	4.608	23.992	1.542	23.704	0.357	
0.3		0.340	3.483	5.635	26.007	1.618	25.701	0.381	
0.3		0.360	4.017	6.800	28.021	1.693	27.697	0.405	
0.3		0.380	4.586	8.278	29.056	1.805	28.715	0.431	
0.4		0.400	5.160	10.065	29.111	1.950	28.752	0.459	
0.4		0.420	5.736	11.990	29.166	2.090	28.790	0.488	
0.4		0.440	6.312	14.046	29.221	2.225	28.827	0.517	
0.4		0.460	6.889	16.230	29.276	2.356	28.865	0.546	
0.4		0.480	7.467	18.537	29.331	2.483	28.903	0.576	
0.5		0.500	8.045	20.966	29.385	2.606	28.940	0.606	
0.5		0.520	8.624	23.512	29.440	2.726	28.978	0.636	STREET CAPACITY
0.5	40	0.540	9.204	26.174	29.495	2.844	29.016	0.666	STREET CHINETT
0.5	60	0.560	9.785	28.947	29.550	2.958	29.053	0.696	
0.5	080	0.580	10.366	31.831	29.605	3.071	29.091	0.727	Q=31.62 CFS
0.6	00	0.600	10.949	34.823	29.660	3.181	29.128	0.757	d= 0.58% 2 0.67 V E= 0.725 2 0.9 V
0.6	520	0.620	11.531	37.921	29.715	3.288	29.166	0.788	d= 0.305 =
0.6	40	0.640	12.115	41.123	29.770	3.394	29.204	0.819	E-0.775 L 0.9 V
0.6	60	0.660	12.700	44.428	29.825	3.498	29.241	0.850	E - 0.123
0.6	088	0.680	13.290	46.862	30.841	3.526	30.249	0.873	
0.7	00	0.700	13.914	48.538	32.819	3.488	32.226	0.889	
0.7	20	0.720	14.579	50.454	34.797	3.461	34.203	0.906	
0.7		0.740	15.283	52.604	36.774	3.442	36.181	0.924	
0.7		0.760	16.026	54.983	38.752	3.431	38.158	0.943	
0.7		0.780	16.809	57.589	40.730	3.426	40.136	0.963	
0.8		0.800	17.631	60.422	42.708	3.427	42.113	0.983	
0.8		0.820	18.493	63.480	44.686	3.433	44.090	1.003	
0.8		0.840	19.395	66.766	46.663	3.442	46.068	1.024	
0.8		0.860	20.336	70.280	48.641	3.456	48.045	1.046	
0.8	80	0.880	21.317	74.026	50.619	3.473	50.023	1.068	

RESIDUAL FLOW = 12.66 CFS

BASIN A-2 = 18.96 CFS

31.62 CFS

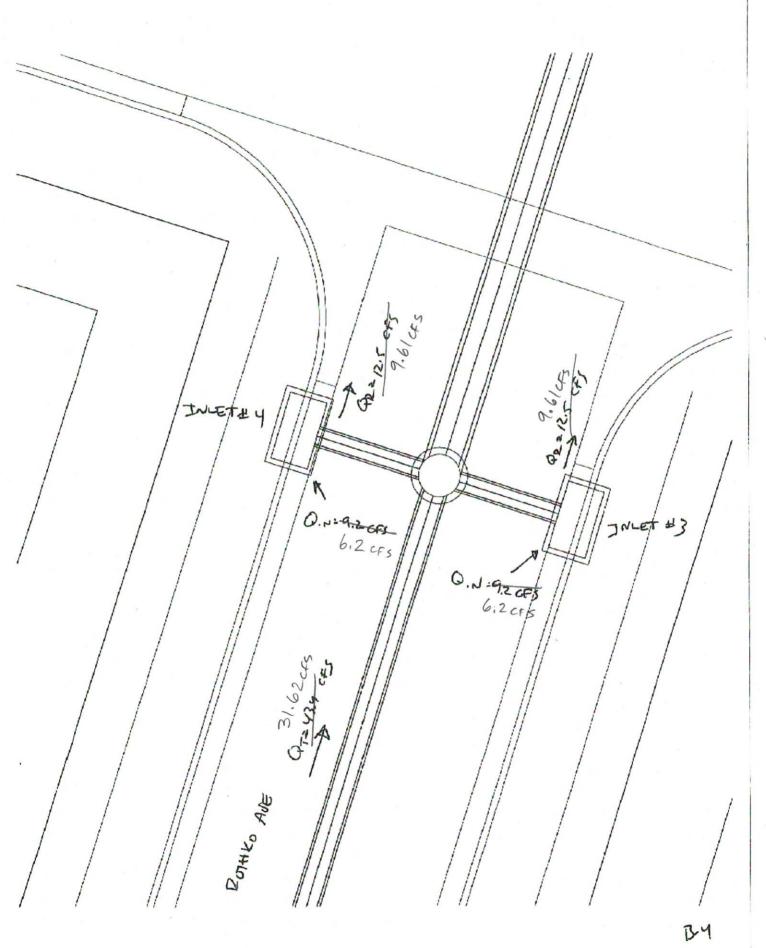
INLET CAPACITY (From Nomograph) $C = 0.52^{\circ}/.$ $d = 0.58^{\circ}$ Quilet = 6.2 cts

Per single 'A"

B-3 (Rev)

RESIDUAL = 31.62 FS - 2 (6.2cFs) = 19.22

This is under the Allowable Residual flow of 25cfs



B-4(Rev)

Scorsese	-579	7 345B	TYT

MANNING'S N = 0.017 SLOPE = 0.055	
POINT DIST ELEV POINT DIST CLEV POINT DIST ELEV 1.0 0.0 0.9 5.0 14.0 0.1 9.0 40.2 0.7 为以后了 进行 生性 2.0 11.4 0.7 6.0 26.0 0.4 10.0 40.6 0.7	
2.0 11.4 0.7 6.0 25.0 9.4 19.0 40.5 0.7 3.0 11.8 0.7 7.0 88.0 9.1 11.0 52.0 0.9	_
WSEL DEPTH FLOW FLOW WETTED FLOW TOPHIO TOTAL LOCATES Q INTERSECTION O	-
WSEL DEPTH FLOW FLOW WE'TED FLOW TOPWHO TOTAL 1NC AREA PER VOL PLUS EVERGY FT. SQ.FT. (CFS) (FT) (FPS) DESTRUCTIONS (FT) SCORGE & NAUMAN 3.050 0.050 0.050 0.039 0.020 1.645 0.511 2.464 0.054	
0.100 0.100 0.156 0.127 3.290 0.811 4.048 0.110 0.150 0.356 0.356 0.338 6.318 0.525 6.990 0.163	
0.200 0.200 0.795 0.832 11.423 1.046 12.021 0.217 0.250 0.250 1.476 1.823 16.527 1.235 17.047 0.274 0.300 0.300 2.408 3.444 21.631 1.430 22.072 0.332	
0.550	
C.500	
C.850	
6.750 0.750 15.271 51.199 38.227 1.353 37.170 0.925 6.800 0.800 17.253 57.359 43.171 3.354 42.313 0.975 6.850 0.859 19.482 95.307 48.115 3.383 47.057 1.028	
Enver Day 1 2 256 CEC	
6.506 6.500 7.803 20.062 25.045 2.57 25.174 0.603 6.550 6.550 9.217 25.441 29.148 2.869 29.199 6.678 6.500 6.600 10.631 33.466 29.251 3.148 29.224 0.754 6.600 6.600 12.047 41.123 29.334 3.413 29.250 6.831 6.700 0.700 11.535 45.927 33.282 3.393 32.226 6.879 6.700 0.700 11.535 45.927 33.282 3.393 32.226 6.879 6.800 0.800 17.253 37.859 43.171 3.354 42.139 6.975 6.800 0.800 17.253 37.359 48.115 3.383 47.057 1.028 FULURE BAS.A Z - 25.6 CFS 19 46 FUTURE RAS.A 3 - 76 CFS 19 46 FUTURE RAS.A 3 - 76 CFS	
RASIN B-2 8.0 CF5	
19% FUTURE BASIN 3-76 CFS	
44.2 CFS / SF 65	
STREET CAPACITY	
11/11/11/11/11/11	
45.93-41.12 = 45.93-44.2 > 4.01 1.73 > 0.08 0,879-× 0.86 √ dl	
0.879-0.631	
INET CAPACITY	
45.93-41.12 45.93-44.72 = 1.73 = 0.0365 = 3.367-4.81× 0.72-665 0.70-× = 0.70-× = 0.0365 = 3.367-4.81× X= 0.67 / 12	
45.93-41.12 45.93-44.2 = 4.57 = 1.05 0.7-x = 0.67 /2 = 0	
@ 5: a.5%, d: 0.67'	
0.24 - 9 CFS 2.04 - 15. CFS	
2.0% - 13. (4)	
1 15-x 0= 27-x(10) 7 x =10 cts	
$\frac{159}{2-0.2} \xrightarrow{2/5-x} \Rightarrow \frac{6}{1.9} = \frac{15-x}{.5} = 9 = 27 - x(1.2) \Rightarrow x = 10 \text{ efs}$ (PZZ DURLE	(A.)
2-4.2 /2-4.5	
DESINAL NOW THE	
DEJ. WAL 44.2 CFS -2(10 CPS) = 242 CFS	
Page 1	

MANNING'	S	N	=	0.017	SLOPE =	0.005

POINT	DIST	ELEV		POINT D	IST ELEV	7 P	OINT DIST	ELEV	INLETS 15+16
1.0	0.0	0.9		4.0 1	4.0 0.1		7.0 40.0	0.0	AND THE PROPERTY OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE
2.0	11.4	0.7		5.0 2	6.0 0.4	l	8.0 40.6	0.7	
3.0	12.0	0.0		6.0 3	8.0 0.1		9.0 52.0	0.9	Located e intersection
									of Scorsesc & Nauman
WSE	L	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	TOTAL	110,000
0,0000		INC	AREA	RATE	PER	VEL	PLUS	ENERGY	Nauman
FT.			SQ.FT.	(CFS)	(FT)	(FPS)	OBSTRUCTION	S (FT)	
0.02	0	0.020	0.007	0.002	0.696	0.282	0.678	0.021	
0.04		0.040	0.027			0.447	1.355	0.043	
0.06		0.060	0.061			0.586	2.033	0.065	
0.08		0.080	0.108			0.710	2.710	0.088	
0.100		0.100	0.169		3.481	0.824	3.388	0.111	
0.120		0.120	0.244		4.177	0.930	4.066		
0.140		0.140	0.339		5.862	0.925	5.733	0.133	
0.160		0.160	0.474		7.876	0.949		0.153	
0.180		0.180	0.649		9.891		7.729	0.174	
0.200		0.200	0.863			1.005	9.726	0.196	
0.220		0.220			11.905	1.075	11.723	0.218	
0.240			1.118		13.920	1.150	13.720	0.241	
0.240		0.240	1.412		15.934	1.228	15.717	0.263	
			1.746		17.949	1.307	17.713	0.287	
0.280		0.280	2.120		19.963	1.386	19.710	0.310	
0.300		0.300	2.535		21.978	1.464	21.707	0.333	
0.320		0.320	2.989		23.992	1.542	23.704	0.357	
0.340		0.340	3.483		26.007	1.618	25.701	0.381	
0.360		0.360	4.017	6.800	28.021	1.693	27.697	0.405	
0.380		0.380	4.586		29.056	1.805	28.715	0.431	
0.400		0.400	5.160	10.065	29.111	1.950	28.752	0.459	
0.420		0.420	5.736	11.990	29.166	2.090	28.790	0.488	
0.440		0.440	6.312	14.046	29.221	2.225	28.827	0.517	
0.460		0.460	6.889	16.230	29.276	2.356	28.865	0.546	
0.480		0.480	7.467	18.537	29.331	2.483	28.903	0.576	
0.500		0.500	8.045	20.966	29.385	2.606	28.940	0.606	
0.520		0.520	8.624	23.512	29.440	2.726	28.978	0.636	
0.540		0.540	9.204	26.174	29.495	2.844	29.016	0.666	
0.560) (0.560	9.785	28.947	29.550	2.958	29.053	0.696	
0.580) (0.580	10.366	31.831	29.605	3.071	29.091	0.727	
0.600) (0.600	10.949	34.823	29.660	3.181	29.128	0.757	
0.620) (0.620	11.531	37.921	29.715	3.288	29.166	0.788	STREET CA PACITY
0.640) (0.640	12.115	41.123	29.770	3.394	29.204	0.819	DIRECT CHINCITY
0.660) (0.660	12.700	44.428	29.825	3.498	29.241	0.850	^
0.680	(0.680	13.290	46.862	30.841	3.526	30.249	0.873	Q= 42.09 CFS
0.700	(0.700	13.914	48.538	32.819	3.488	32.226	0.889	1-1
0.720	(0.720	14.579	50.454	34.797	3.461	34.203	0.906	d= 0.65' L 0.67 V
0.740		0.740	15.283	52.604	36.774	3.442	36.181	0.924	d= 0.65' \(0.67' \) E = 0.83' \(\text{ 0.90'} \)
0.760		0.760	16.026	54.983	38.752	3.431	38.158	0.943	K= 1 83' / 200' V
0.780		0.780	16.809	57.589	40.730	3.426	40.136	0.963	E - U, UJ 2 0.70
0.800		0.800	17.631	60.422	42.708	3.427	42.113	0.983	
0.820		0.820	18.493	63.480	44.686	3.433	44.090	1.003	
0.840		0.840	19.395	66.766	46.663	3.442	46.068	1.003	
0.860		0.860	20.336	70.280	48.641	3.442	48.045		
0.880		0.880	21.317	74.026				1.046	
0.000			41.31/	74.026	50.619	3.473	50.023	1.068	

Future Basin 2 = 28.64 cfs (Master Plan Flow).

Basin B-2 = 8.31 cfs

Future Basin 3 (partial) = 5.14 cfs

42.09 cfs

From Nomograph

INLET CAPACITY

Q Q = 42.09 CFS
S = 0.5 1/2,
d = 0.65'
Q inlet = 7.7 CFS
LPET Single A)

RES: DUAL

42.09 CFS = 2 (7.7 CFS) = 26.69 CFS

13.35cfs HAUMAY 村 Az.09145 Scorese AVE

B-12A (REV)

Scorsese-sta 13+50.txt

MAYNING'S N = D.017 SLOPE = 0.005	16
POINT DIST ELSY POINT DIST ELEV POINT DEST ELEV 1.0 0.0 0.9 3.0 14.0 0.1 19.0 40.2 0.7 2.0 11.4 3.7 6.0 26.0 0.4 10.0 40.6 0.7 3.0 11.8 0.7 7.9 38.0 0.1 11.0 52.0 6.9 4.0 12.0 0.6 8.0 40.0 0.0	INCEL 3 年1 年 日 日 日
WSEL DEPTH FLOW FLOW WETTED FLOW TOPATD TOTAL INC AREA RATE PER VEL PLUS ENERGY	LOCATED @ INTERFECT.IN UF
FT. SQ.FT. (CFS) (FT) (FPS) GESTRUCTIONS (FT)	SCORSESE & NAUMAN
9.150 0.150 0.366 0.338 6.318 0.925 6.925 0.163 9.200 0.200 0.795 0.832 11.423 1.046 12.021 0.217	
0.300	
0.450 0.450 6.39\ 1.4.433 28.942 2.258 29.148 0.529 / 0.500 0.500 7.803 20.082 29.048 2.574 29.174 0.603 / 0.550 0.550 0.717 25.441 29.748 2.869 29.100 0.678	
0.650 0.650 12.047 41.123 29.354 3.413 29.250 0.831 0.700 0.700 13.536 45.927 33.282 3.393 32.226 0.879 0.750 0.750 15.271 31.199 38.227 3.353 37.170 0.925	
0.800 0.800 17.253 57.859 43.171 3.354 42.113 0.975 0.850 0.850 19.482 65.907 48.136 3.383 47.057 1.028	
RBIDUAL - 24.2 CFS	
INCES #12 416	
STREET CAPACITY	x= 0.65' de
2644-20.08 = 26.44 -24.2 => 6.36 - 2.27 3 4.3	165' / ole
0.65-0.60 0.68-× 0.08 0.65-×	X 3 0 1 2 3
V.03 - V.05	
INVET CAPACITY	112 = 3.498 - 6.36)=
2644-54.5	X= 0.53;
26.44-21.08 = C. 0.05 0.55-x 0.05 - 0.50 0.55-x 0.05 0.55-x 0.05 0.55-x 0.05 0.55-x 0.05 0.55-x 0.05 0.55-x	X - 0.33°
0.55 Kele	
@ 5: 0.540, d. 0.53' @ 246 - 10.5 CFS @ 25 25 25 25 25 25 25 25 25 25 25 25 25	
024 10.5 CFS / SU &	
30.2% - 5.5 CFS	
0.215	1 2 190 190
$\frac{106.5.5}{2-0.2} = \frac{105-1}{2-0.5} \Rightarrow \frac{5}{1.9} = \frac{10.5-1}{1.5}$	= 3 4.3 = 1042 1.000
2-0.2 2/-0.5	X = 6.5 C+3
	(PEZ DURLE 'A')
PESIDUAL -112-01 = 116 CFS	
24.2 CFS-2(6.3 CF) = 11.6 CFS	
Page 1	

			Scorsese	- Slope 0	.50%			1
		MANNI	ING'S N = 0.	017 SLOP	E = 0.005	5		NLETS 17218
	DIST ELEV		POINT DIS	T ELEV	P	DINT DIST	ELEV	
1.0	0.0 0.9		4.0 14.	0 0.1		7.0 40.0	0.0	LOCATED C
	11.4 0.7		5.0 26.			8.0 40.6	0.7	. 1 1 (
3.0	12.0 0.0		6.0 38.	0 0.1		9.0 52.0	0.9	intersection of Scorsese & Strand
								a committee of
WSEL	DEDMI	DI ON	DI OU					Scorsese & Strana
WSEL	DEPTH INC	FLOW AREA	FLOW RATE	WETTED	FLOW	TOPWID	TOTAL	
FT.	INC	SQ.FT.	(CFS)	PER (FT)	VEL	PLUS	ENERGY	Carl In
		50.11.	(CF3)	(FI)	(FPS)	OBSTRUCTIONS	(FT)	
0.020	0.020	0.007	0.002	0.696	0.282	0.678	0.021	
0.040	0.040	0.027	0.012	1.392	0.447	1.355	0.043	
0.060	0.060	0.061	0.036	2.088	0.586	2.033	0.065	
0.080	0.080	0.108	0.077	2.785	0.710	2.710	0.088	
0.100	0.100	0.169	0.140	3.481	0.824	3.388	0.111	
0.120	0.120	0.244	0.227	4.177	0.930	4.066	0.133	
0.140	0.140	0.339	0.314	5.862	0.925	5.733	0.153	
0.160	0.160	0.474	0.450	7.876	0.949	7.729	0.174	
0.180	0.180	0.649	0.652	9.891	1.005	9.726	0.196	
0.200	0.200	0.863	0.928	11.905	1.075	11.723	0.218	
0.220	0.220	1.118	1.286	13.920	1.150	13.720	0.241	
0.240	0.240	1.412	1.735	15.934	1.228	15.717	0.263	
0.260	0.260	1.746	2.283	17.949	1.307	17.713	0.287	
0.280	0.280	2.120	2.940	19.963	1.386	19.710	0.310	
0.300	0.300	2.535	3.712	21.978	1.464	21.707	0.333	
0.320	0.320	2.989	4.608	23.992	1.542	23.704	0.357	
0.340	0.340	3.483	5.635	26.007	1.618	25.701	0.381	
0.360	0.360	4.017	6.800	28.021	1.693	27.697	0.405	
0.380	0.380	4.586	8.278	29.056	1.805	28.715	0.431	
0.400	0.400	5.160	10.065	29.111	1.950	28.752	0.459	
0.420	0.420	5.736	11.990	29.166	2.090	28.790	0.488	
0.460	0.440	6.312	14.046	29.221	2.225	28.827	0.517	
0.480	0.480	6.889 7.467	16.230	29.276	2.356	28.865	0.546	
0.500	0.500	8.045	18.537 20.966	29.331	2.483	28.903	0.576	7
0.520	0.520	8.624	23.512	29.385 29.440	2.606	28.940	0.606	
0.540	0.540	9.204	26.174	29.440	2.726 2.844	28.978	0.636	
0.560	0.560	9.785	28.947	29.550	2.958	29.016 29.053	0.666	
0.580	0.580	10.366	31.831	29.605	3.071	29.091	0.696 0.727	
0.600	0.600	10.949	34.823	29.660	3.181	29.128	0.757	
0.620	0.620	11.531	37.921	29.715	3.288	29.166	0.788	STREET CAPACITY
0.640	0.640	12.115	41.123	29.770	3.394	29.204	0.819	SIKEE! CAPACITY
0.660	0.660	12.700	44.428	29.825	3.498	29.241	0.850	
0.680	0.680	13.290	46.862	30.841	3.526	30.249	0.873	Q=43,22 crs
0.700	0.700	13.914	48.538	32.819	3.488	32.226	0.889	
0.720	0.720	14.579	50.454	34.797	3.461		0.906	d= 0.651
0.740	0.740	15.283	52.604	36.774	3.442	36.181	0.924	E=0.84' L 0.90' V
0.760	0.760	16.026	54.983	38.752	3.431	38.158	0.943	
0.780	0.780	16.809	57.589	40.730	3.426	40.136	0.963	
0.800	0.800	17.631	60.422	42.708	3.427	42.113	0.983	
0.820	0.820	18.493	63.480	44.686	3.433		1.003	
0.840	0.840	19.395	66.766	46.663	3.442		1.024	
0.860	0.860	20.336	70.280	48.641	3.456		1.046	
0.000	0.880	21.317	74.026	50.619	3.473	50.023	1.068	

RESIDUAL FLOW = 26.69 CFS
BASIN 30 = 9.26 CFS
FUTURE BASIN 3(partial) = 7.27 CFS
43.22 CFS

INLET CAPACITY (From Nomograph)

C S = 0.5%

d = 0.65'

Qinlet = 7.7 CFS

RESIDUAL

43,22cfs - 2(7.7cfs) = 27.82cfs.

B-13(rev)

STRAND OR 5459 0=7,745 0-1745 1 Ed - So. 1888 Ideal 10 million THET # Q = 43,22 SCORSESE AVE 13-14 (Rev)

			MANN	ING'S N = 0	0.017 s	LOPE = 0.00	5			EXISTING
POINT	DIST	DT D11								INLETS 19 + 20
1.0	0.0	ELEV	1					IST	ELEV	1100013 19 4 00
2.0	11.4	0.9				.1		0.0	0.0	1
3.0	12.0	0.7				. 4		0.6	0.7	Located @ intersecti
3.0	12.0	0.0		6.0 38	0 0	.1	9.0 5:	2.0	0.9	
										OF SCOESESE & MOTHER
WSE	т.	DEPTH	FLOW	ELOM	tan mmn	D 77.011				SCUESESE & MOTHER
WOL		INC	AREA	FLOW RATE	WETTE		TOPWII	D	TOTAL	
FT.		1110	SQ.FT.	(CFS)	PER	VEL	PLUS		ENERGY	
			50.11.	(CFS)	(FT)	(FPS)	OBSTRUCT	LIONS	(FT)	
0.020) (0.020	0.007	0.002	0.69	6 0.276	0.678	0	0 001	
0.040) (0.040	0.027	0.012	1.39		1.355		0.021	
0.060		0.060	0.061	0.035	2.08		2.033		0.043	
0.080		0.080	0.108	0.075	2.78		2.710		0.065	
0.100		0.100	0.169	0.137	3.48		3.388		0.088	
0.120		0.120	0.244	0.222	4.17		4.066			
0.140		0.140	0.339	0.308	5.862		5.733		0.133	
0.160		0.160	0.474	0.441	7.87		7.729		0.133	
0.180) (180	0.649	0.639	9.89		9.726		0.175	
0.200		.200	0.863	0.909	11.905		11.723		0.195	
0.220) (.220	1.118	1.260	13.920		13.720		0.217	
0.240	0	.240	1.412	1.699	15.934		15.720		0.240	
0.260		.260	1.746	2.237	17.949		17.713		0.286	
0.280	0	.280	2.120	2.880	19.963		19.710		0.309	
0.300	0	.300	2.535	3.637	21.978		21.707		0.332	
0.320	0	.320	2.989	4.515	23.992		23.704		0.355	
0.340	0	.340	3.483	5.521	26.007		25.701		0.333	
0.360	0	.360	4.017	6.663	28.021		27.697		0.403	
0.380	0	.380	4.586	8.111	29.056		28.715		0.429	
0.400	0	.400	5.160	9.862	29.111		28.752		0.457	
0.420		.420	5.736	11.747	29.166		28.790		0.485	
0.440	0	.440	6.312	13.762	29.221		28.827		0.514	
0.460	0	.460	6.889	15.902	29.276		28.865		0.543	
0.480	0	.480	7.467	18.163	29.331		28.903		0.572	
0.500	0	.500	8.045	20.542	29.385		28.940		0.601	
0.520	0	.520	8.624	23.037	29.440		28.978		0.631	
0.540	0	.540	9.204	25.645	29.495		29.016		0.661	
0.560	0	.560	9.785	28.362	29.550		29.053		0.691	STREET CAPACITY
0.580	0	.580	10.366	31.188	29.605	3.009	29.091		0.721	And the second s
0.600		.600	10.949	34.119	29.660		29.128		0.751	Q=33.77CFS
0.620		.620	11.531	37.155	29.715	3.222	29.166		0.781	
0.640		.640	12.115	40.292	29.770	3.326	29.204		0.812	d=0.6' L0.67 V
0.660		.660	12.700	43.530	29.825	3.428	29.241		0.843	E= 0.75' < 0,9 V
0.680		.680	13.290	45.916	30.841	3.455	30.249		0.866	E= 0.15 2 0,9 V
0.700		.700	13.914	47.557	32.819	3.418	32.226		0.882	
0.720		.720	14.579	49.434	34.797	3.391	34.203		0.899	
0.740		.740	15.283	51.541	36.774	3.373	36.181		0.917	
0.760			16.026	53.872	38.752	3.362	38.158		0.936	
0.780			16.809	56.426	40.730	3.357	40.136		0.955	
0.800			17.631	59.201	42.708	3.358	42.113		.975	
0.820			18.493	62.197	44.686	3.363	44.090		.996	
0.840			19.395	65.417	46.663	3.373	46.068		.017	
0.860		.860	20.336	68.860	48.641	3.386	48.045		.038	
0.880	0.	.880	21.317	72.530	50.619	3.402	50.023		.060	

RESIDUAL FLOW = 27.82 CFS Monitage 3B Basin 2 (partial) = 5.95 cfs

DLANNED

33.77 cfs Z 39.8 cfs

- PLANNED FLOW FROM UNIT 3:

SEE NEXT PAGE

Scorsese-sta 19+50.txt

		MANHI	ING S N = J.	OTI STOP	* 0.003			
3.0 11	.0 0.9		5.0 14. 6.0 26. 7.0 38. 8.0 40.	0.1 0 0.4 0 6.1	PC 1	9.0 40.2 10.0 40.6 11.0 52.0	0.7 0.7 0.7 0.9	TWENS # 14 4 # # 120
WSEL FT.	DEPTH	FLOW AREA SQ.FT.	FLOW RATE (CFS)	WETTED PER (FT)	FLOW VEL (FPS)	TOPWID PLUS DESTRUCTIONS	TOTAL ENERGY (FT)	COCATED C IMPRECION OF
0,050 0,150 0,150 0,260 0,250 0,360 0,450 0,450 0,500 0,500 0,650 0,650 0,750 0,750 0,850	0.050 0.100 0.150 0.250 0.250 0.350 0.350 0.450 0.450 0.550 0.650 0.750 0.750 0.850 0.850	0.039 0.156 0.795 1.476 2.408 3.591 4.981 6.391 7.803 9.217 10.536 12.047 12.536 12.253 13.482	0.020 0.127 0.338 0.832 1.823 3.444 5.822 9.547 14.423 20.082 26.441 33.456 41.123 45.927 51.199 65.907	1.645 3.290 6.318 11.423 16.527 21.651 26.735 28.942 29.045 29.148 29.251 29.354 31.282 38.227 42.171 48.116	0.511 0.811 0.925 1.046 1.235 1.430 1.621 1.917 2.258 2.574 2.869 3.448 3.433 3.354 3.354 3.393	2. 484 4. 048 5. 996 12. 021 17. 047 22. 072 23. 123 29. 148 29. 174 29. 199 22. 250 37. 170 47. 175 47. 057	0.094 0.110 0.163 0.217 0.274 0.332 0.457 0.529 0.603 0.678 0.678 0.831 0.879 0.975 1.028	SCORSEDE & MOTHER WELL

DIST

0.0

ELEA

0.9

POINT

1.0

0.380

0.400

0.420

0.440

0.460

0.480

0.500

0.520

0.540

0.560

0.600

0.620

0.640

0.660

0.680

0.720

0.740

0.760

0.780

0.800

0.820

0.840

0.380

0.400

0.420

0.440

0.460

0.480

0.500

0.520

0.540

0.560

0.580

0.600

0.620

0.640

0.660

0.680

0.700

0.720

0.740

0.760

0.780

0.800

0.820

0.840

4.521

5.135

5.791

6.487

7.224

8.002

8.820

9.679

10.579

11.515

12.456

13.399

14.341

15.285

16.230

17.180

18.164

19.188

20.252

21.355

22.497

23.679

24.901

26.162

7.497

8.872

10.399

12.086

13.937

15.960

18,161

20.545

23.119

26.231

29.879

33.714

37.732

41.927

46.298

50.196

53.646

57.308

61.184

65.279

69.598

74.146

78.928

83.947

30.057

32.112

34.167

36.223

38.278

40.333

42.388

44.444

46.499

47.554

47.609

47.664

47.719

47.774

47.829

48.843

50.816

52.789

54.762

56.735

58.708

60.681

62.654

64.627

MANNING'S	ът	_	0.017	CIODE -	0 00 5
MANNING'S	IN	=	0.01/	SLOPE =	0.005

ELEA

0.1

POINT

7.0

DIST

56.0

ELEV

0.0

29.715

31.752

33.790

35.827

37.865

39.903

41.940

43.978

46.016

47.053

47.091

47.128

47.166

47.204

47.241

48.246

50.219

52.192

54.164

56.137

58.109

60.082

62.055

64.027

0.423

0.446

0.470

0.494

0.518

0.542

0.566

0.590

0.614

0.641

0.669

0.698

0.728

0.757

0.787

0.813

0.836

0.859

0.882

0.905

0.929

0.953

0.976

1.000

0.750

0.757

0.765

0.772

0.779

0.785

0.792

0.798

0.804

0.812

0.822

0.832

0.841

0.850

0.858

0.863

0.866

0.868

0.871

0.874

0.877

0.879

0.882

0.885

DIST

12.0

POINT

4.0

2.0	9.4	0.7		5.0	33.0	0.6		8.0	56.6	0.7		
3.0	10.0	0.0		6.0	54.0	0.1		9.0	66.0	0.9		
WS	EL	DEPTH	FLOW	FL	OW	WETTED	FLOW	TO	PWID	TOPWID	TOTAL	FROUDE
		INC	AREA	RA	TE	PER	VEL	P	LUS	WATER	ENERGY	NO.
FT			SQ.FT.	(C	FS)	(FT)	(FPS)	OBST	RUCTIONS		(FT)	
0.0	20	0.020	0.007	0.	002	0.672	0.267	0	.653	0.653	0.021	0.471
0.0	40	0.040	0.026	0.	011	1.343	0.424	1	.306	1.306	0.043	0.529
0.0	60	0.060	0.059	0.	033	2.015	0.556	1	.959	1.959	0.065	0.566
0.0	80	0.080	0.104	0.	070	2.686	0.673	2	.612	2.612	0.087	0.593
0.1	00	0.100	0.163	0.	128	3.358	0.781	3	.265	3.265	0.109	0.616
0.1	20	0.120	0.235	0.	207	4.030	0.882	3	.918	3.918	0.132	0.635
0.1	40	0.140	0.323	0.	291	5.393	0.898	5	.263	5.263	0.153	0.639
0.1	60	0.160	0.449	0.	405	7.448	0.902	7	.301	7.301	0.173	0.641
0.1	80	0.180	0.615	0.	582	9.504	0.946	9	.339	9.339	0.194	0.649
0.2	00	0.200	0.823	0.	828	11.559	1.007	11	.376	11.376	0.216	0.660
0.2	20	0.220	1.071	1.	152	13.614	1.076	13	.414	13.414	0.238	0.672
0.2	40	0.240	1.359	1.	562	15.670	1.149	15	.451	15.451	0.261	0.683
0.2	60	0.260	1.689	2.	065	17.725	1.223	17	.489	17.489	0.283	0.694
0.2	80	0.280	2.059	2.	671	19.780	1.297	19	.527	19.527	0.306	0.704
0.3	0 0	0.300	2.470	3.	387	21.835	1.371	21	.564	21.564	0.329	0.714
0.3	20	0.320	2.921	4.	220	23.891	1.445	23	.602	23.602	0.352	0.724
0.3	40	0.340	3.414	5.	178	25.946	1.517	25	.639	25.639	0.376	0.733
0.3	60	0.360	3.947	6.	268	28.001	1.588	27	.677	27.677	0.399	0.741

1.658

1.728

1.796

1.863

1.929

1.995

2.059

2.123

2.185

2.278

2.399

2.516

2.631

2.743

2.853

2.922

2.953

2.987

3.021

3.057

3.094

3.131

3.170

3.209

29.715

31.752

33.790

35.827

37.865

39.903

41.940

43.978

46.016

47.053

47.091

47.128

47.166

47.204

47.241

48.246

50.219

52.192

54.164

56.137

58.109

60.082

62.055

64.027

Basin C4 = 16.49 cfs Partial Basin C2 = 3.15 cfs Future Basin 4A = 12.55 cfs TOTAL = 32.19 cfs Street Capacity Q = 32.19 cfs d = .59 < .67' E = .69' < .90'

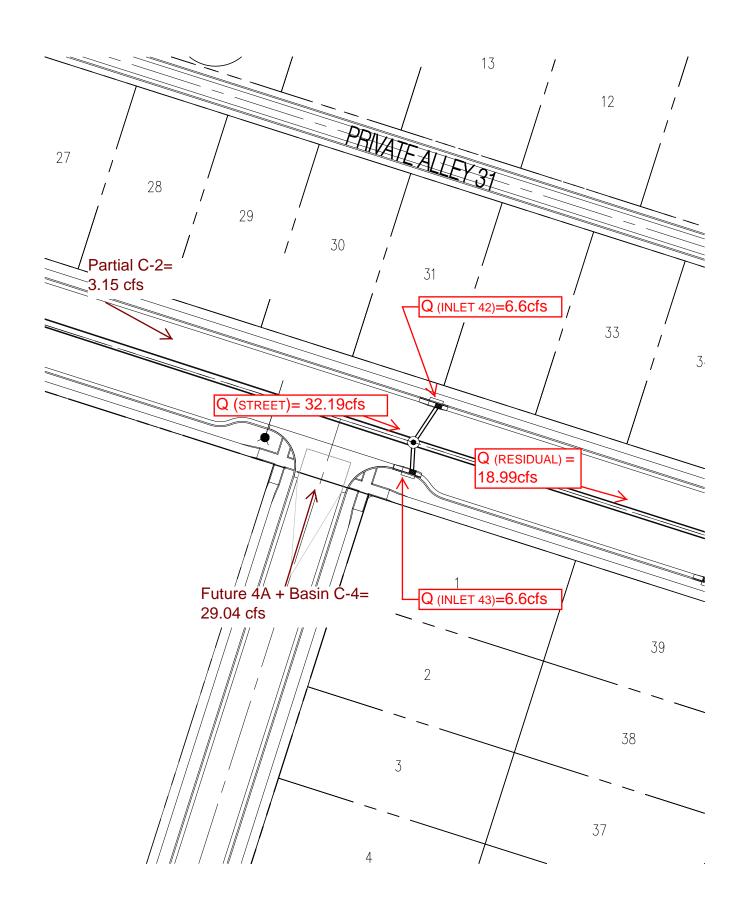
Inlet Capacity

@ S = .45%

d = .59

Q inlet = 6.6 cfs

per SINGLE GRATE



POINT

4.0

MANNING'S N = 0.017 SLOPE = 0.004

ELEV

0.1

POINT

7.0

DIST

56.0

ELEV

0.0

DIST

12.0

1.0	0.0			1.0 12.0			7.0 50.0	0.0		
	9.4	0.7		5.0 33.0			8.0 56.6	0.7		
3.0	10.0	0.0		6.0 54.0	0.1		9.0 66.0	0.9		
WS	ET.	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID PLUS OBSTRUCTIONS	TOPWID	TOTAL	FROUDE
		INC	AREA	RATE	PER	VEL	DITIC	WATER	ENERGY	NO.
FT		INC			(FT)	(EDG)	OBSTRUCTIONS	WAIEK		NO.
FI	•		SQ.FT.	(CFS)	(FI)	(FPS)	OBSTRUCTIONS		(FT)	
							0.650			
0.0			0.007	0.002	0.672 1.343	0.252		0.653	0.021	0.444
0.0		0.040	0.026			0.400	1.306	1.306	0.042	0.498
0.0		0.060	0.059	0.031 0.066	2.015	0.524		1.959	0.064 0.086	0.533
0.0	80	0.080	0.104	0.066	2.686	0.635	2.612	2.612	0.086	0.559
0.1		0.100	0.163	0.120	3.358	0.736	3.265	3.265	0.108 0.131	0.581
0.1	20	0.120	0.235	0.195	4.030	0.832	3.918	3.918	0.131	0.599
0.1		0.140	0.323			0.847		5.263	0.151 0.171	0.602
0.1		0.160	0.449	0.274 0.382	7.448	0.850		7.301	0.171	0.604
0.1		0.180	0.615	0.549	9 504		9.339	9.339	0.192	0.612
0.2		0.200	0.823	0.781	11.559	0.892 0.949	11.376	11.376	0.192 0.214	0.622
0.2		0.200	1.071	1.086	13.614	1.015	13.414	13.414	0.214	0.633
0.2		0.240	1.359	1.472	15.670	1.083		15.451	0.258	0.644
0.2		0.260	1.689	1.947	17.725	1.153		17.489	0.281	0.654
0.2		0.280	1.689 2.059 2.470	2.518	19.780	1.223		19.527	0.303	0.664
0.3		0.500	2.1.0	3.193	21.835	1.293		21.564	0.326	0.674
0.3	20	0.320	2.921	3.979	23.891	1.362	23.602	23.602	0.349	0.682
0.3	40	0.340	3.414	4.882	25.946	1.430		25.639	0.372	0.691
0.3	60	0.360	3.947	5.910	28.001	1.497	27.677	27.677	0.395	0.699
0.3	80		4.521	7.069	30.057	1.564	29.715	29.715	0.418	0.707
0.4		0.400	5.135	8.365	32.112	1.629	31.752	31.752	0.441	0.714
0.4		0.420		9.805					0.465	0.721
0.4				11.394		1.756				
0.4		0.460	7.224	13.140		1.819		37.865	0.511	0.720
0.4		0.480	8.002	15.047		1.881		39.903	0.535	0.740
0.4		0.500	8.820	17.122	42.388	1.941		41.940	0.559	0.746
0.5			9.679	19.370	44.444 46.499	2.001	43.978	43.978	0.582	0.752
0.5				21.797	46.499	2.060	46.016	46.016	0.606	0.758
0.5		0.560		24.731	47.554	2.148	47.053	47.053	0.632	0.765
0.5		0.580	12.456	28.170				47.091	0.660	0.775
0.6		0.600	13.399	31.786 35.574	47.664	2.372 2.480	47.128	47.128	0.688	0.784
0.6	20	0.620	14.341	35.574	47.719	2.480	47.166	47.166	0.716	0.793
0.6	40	0.640	15.285	39.530	47.774	2.586 2.690	47.204	47.204	0.744	0.801
0.6	60	0.660	16.230	43.650	47.829	2.690	47.241	47.241	0.773	0.809
0.6	80	0.680	17.180	47.325	48.843	2.755	48.246	48.246	0.798	0.814
0.7			18.164	50.578	50.816	2.755 2.784	50.219	50.219	0.798 0.821	0.816
0.7			19.188	54.030	52.789	2.816	52.192	52.192	0.843	0.819
0.7		0.740	20.252	57.685	54.762	2.816 2.848	54.164	54.164	0.866	0.821
0.7		0.760		61.546	56.735	2.882	56.137	56.137	0.889	0.821
0.7		0.780		65.618	58.708	2.882	58.109	58.109	0.912	0.826
0.7		0.800		69.906	60.681	2.952	60 000			
		0.820			60.001	2.952 2.988	60.082 62.055 64.027	60.002	0.330	0.832
0.8					62.654	2.988	04.055	04.055	0.959	0.834
0.8	4 U	0.840	26.162	79.146	64.627	3.025	64.027	64.027	0.982	0.834

Inlets 44&45 and 46&47

POINT

1.0

DIST

0.0

ELEV

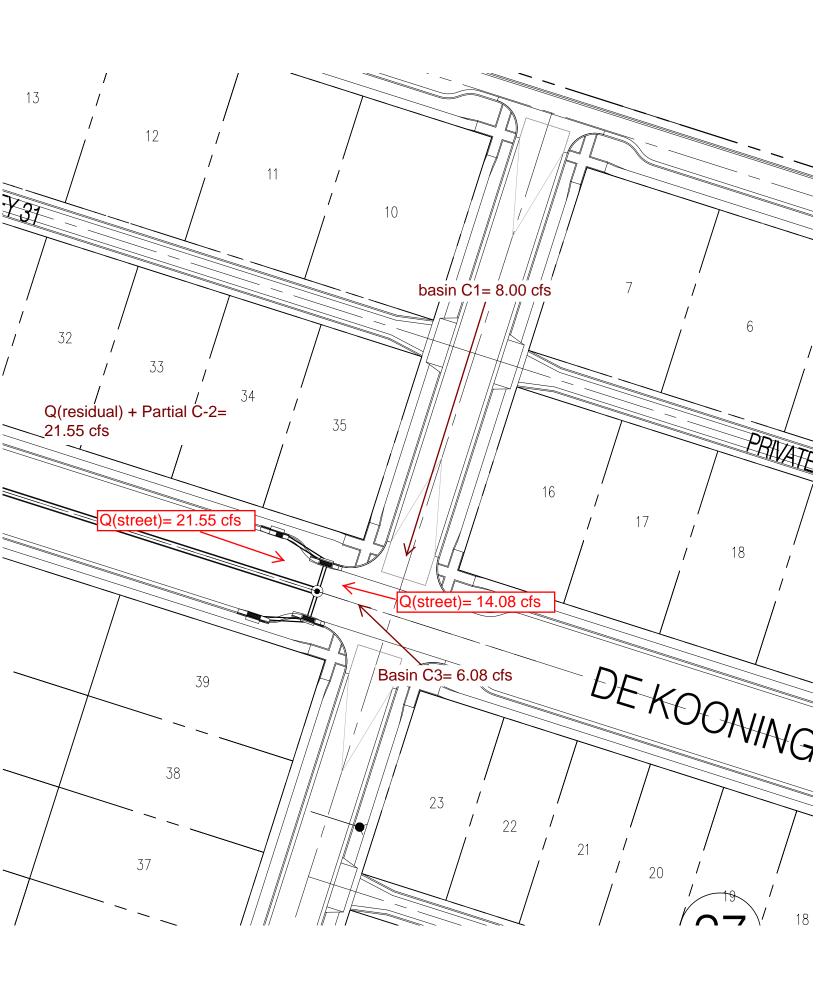
0.9

Residual Flow = 18.99 cfs
Partial Basin C2 = 2.96 cfs
Basin C1 = 8.00 cfs
Basin C3 = 6.08 cfs
TOTAL = 36.03 cfs

Inlet Capacity (Sump condition)

Q(inlet) = 36.03 cfs / 4 inlets

Q inlet= 9.0 cfs (See Sump Calcs)



ANALYSIS OF AN INLET IN A SUMP CONDITION

DeKooning and Dasburg

Q=1.2*(64.4*H)^0.5 Wing opening* A=2.0 sf C = 0.6 $Q=C*A*(2*G*H)^{0.5}$ Q=0.6*3.72*(64.4*H)^0.5 A(single grate)=3.72 sf Grate opening INLET TYPE: Single Grate Type "A" with curb opening wings on both sides on inlet. ORIFICE: C = 0.6L(single grate)=[(2.67')+2(1.8')]=6.27 ft $Q = 3.0(4.0) \text{H}^{1.5} = 12.0 \text{H}^{**} \text{1Q} = 3.0(6.27) \text{H}^{1.5} = 18.81 \text{H}^{1.5}$ C=3.0Q=C*L*H^1.5 Wing opening L=4.0 ftC = 3.0

*not included in the orifice calcs

			Q (CFS)	Q (CFS)	Q (CFS)	TOTAL	
			WEIK	WEIK	OKIFICE	>	
	WS	HEIGHT	WING	SINGLE	SINGLE	(CFS)	
	ELEVATION	ELEVATIONABOVE INLE	OPENING	GRATE	GRATE		COMMENTS:
~FL @ INLET	0.00	0.00	0.00	0.00	0.00	0.00	Flow at single "A" inlet w/ two wing openings
	0.10	0.10	0.38	0.59	5.66	1.35	Weir controls on grate analysis
	0.20	0.20	1.07	1.68	8.01	3.83	
	0.30	0.30	1.97	3.09	9.81	7.03	Q(100 yr) = 9.0 cfs is provided at this depth
	0.40	0.40	3.04	4.76	11.33	10.83	
	0.50	0.50	4.24	6.65	12.67	15.14	
	0.60	09.0	5.58	8.74	13.87	19.90	Q(2X100 yr) = 18.0 cfs is provided at this deptl
TOP OF CURB	0.70	0.70	7.03	11.02	14.99	25.07	
	0.80	0.80	8.59	13.46	16.02	30.63	
ROW LIMIT	0.90	0.90	10.25	16.06	16.99	36.55	
	1.00	1.00	12.00	18.81	17.91	41.91	

The total runoff intercepted by the inlet at the low point in the road is:

NOTE:

Q(100) = 2*[(runoff of the wing opening) + (the lesser of the weir or orifice amount taken by the double grate)].

SAGAN INLETS

Traffic Circle 1/2 Section

MANNING'S N = 0.017 SLOPE = 0.005

POINT	DIST	ELEV	PC	OINT D	IST	ELEV	PO	INT	DIST	ELEV
1.0	0.0	1.3		4.0 3	0.0	0.3		7.0	60.7	0.7
2.0	28.5	0.8		5.0 5	8.0	0.1		8.0	70.0	0.9
3.0	29.1	0.3		6.0 6	0.0	0.0				
WSE	L	DEPTH	FLOW	FLOW		WETTED	FLOW		PWID	TOTAL
		INC	AREA	RATE		PER	VEL	F	LUS	ENERGY
FT.			SQ.FT.	(CFS)		(FT)	(FPS)	OBSI	RUCTIONS	(FT)
0.02	0	0.020	0.003	0.001		0.349	0.282	1	215	0.021
0.04		0.040	0.014	0.006		0.698	0.448		555	0.043
0.01		0.060	0.011	0.018		1.047	0.587		895	0.015
0.08		0.080	0.054	0.039		1.396	0.711		2.235	0.088
0.10		0.100	0.085	0.070		1.745	0.825		2.575	0.111
0.12		0.120	0.122	0.114		2.093	0.931		2.915	0.133
0.14		0.140	0.187	0.127		5.160	0.677		5.973	0.147
0.16		0.160	0.329	0.221		9.132	0.674		.936	0.167
0.18		0.180	0.549	0.410		13.104	0.746		3.900	0.189
0.20	0	0.200	0.850	0.710		17.076	0.836		.864	0.211
0.22		0.220	1.229	1.143		21.048	0.930	21	.827	0.233
0.24	0	0.240	1.688	1.729		25.020	1.024		.791	0.256
0.26		0.260	2.226	2.485		28.992	1.116	29	.755	0.279
0.28		0.280	2.826	3.583		30.421	1.268		.171	0.305
0.30		0.300	3.462	4.924		31.356	1.422		.216	0.331
0.32		0.320	4.086	6.484		31.417	1.587		.261	0.359
0.34		0.340	4.712	8.211		31.477	1.743		.306	0.387
0.36		0.360	5.339	10.098		31.537	1.891		351	0.416
0.38		0.380	5.966	12.137		31.598	2.034		396	0.410
0.40		0.400	6.594	14.323		31.658	2.172		.441	0.473
0.42		0.420	7.224	16.651		31.718	2.305		486	0.503
0.44		0.440	7.854	19.118		31.778	2.434		531	0.532
0.46		0.460	8.485	21.719		31.839	2.560		.576	0.562
0.48		0.480	9.117	24.450		31.899	2.682		.621	0.592
0.50		0.500	9.750	27.310		31.959	2.801		.666	0.622
0.52		0.520	10.384	30.294		32.020	2.917		.711	0.652
0.54	0	0.540	11.018	33.401		32.080	3.031	31	.756	0.683
0.56	0	0.560	11.654	36.627		32.140	3.143	31	.801	0.714
0.58	0	0.580	12.290	39.972		32.201	3.252	31	.846	0.745
0.60	0	0.600	12.928	43.432		32.261	3.360	31	.891	0.776
0.62		0.620	13.566	47.005		32.321	3.465		.936	0.807
0.64		0.640	14.205	50.691		32.381	3.569		.981	0.838
0.66		0.660	14.845	54.487		32.442	3.670		2.026	0.870
0.68		0.680	15.489	57.843		32.979	3.735		2.552	0.897
0.00		0.700	16.150	60.776		33.993	3.763		3.552	0.897
0.70		0.700	16.130	63.845		35.008	3.763		1.567	0.944
0.74		0.740	17.532	67.052		36.022	3.824		5.574	0.968
0.76		0.760	18.254	70.398		37.036	3.857		5.581	0.991
0.78		0.780	19.000	73.100		38.688	3.847		3.230	1.010
0.80		0.800	19.784	75.622		40.683	3.822		.224	1.027
0.82		0.820	20.609	78.404		42.678	3.804		2.219	1.045
0.84	0	0.840	21.473	81.442		44.673	3.793	44	1.213	1.064

Future Basin 4b = 32.52 cfs

Basin C6 = 2.78 cfs TOTAL = 35.3 cfs

Street has capacity

Sagan and Alley 32 Intersection slope .45%

MANNING'S N = 0.017SLOPE = 0.005and 39 @ Sump POINT DIST ELEV POINT DIST ELEV POINT DIST ELEV condition 1.0 0.0 0.9 4.0 12.0 0.1 7.0 56.0 0.0 2.0 9.4 0.7 5.0 33.0 0.6 8.0 56.6 0.7 10.0 3.0 0.0 6.0 54.0 0.1 9.0 66.0 0.9 WSEL DEPTH FLOW FLOW WETTED FLOW TOPWID TOPWID TOTAL FROUDE PER ENERGY INC AREA RATE VEL PLUS WATER NO. FT. SQ.FT. (CFS) (FT) (FPS) OBSTRUCTIONS (FT) 0.020 0.020 0.007 0.002 0.672 0.267 0.653 0.653 0.021 0.471 0.040 0.040 0.026 0.011 1.343 0.424 1.306 1.306 0.043 0.529 0.060 0.060 0.059 0.033 2.015 0.556 1.959 1.959 0.065 0.566 0.080 0.080 0.104 0.070 2.686 0.673 2.612 2.612 0.087 0.593 0.100 0.100 0.163 0.128 3.358 0.781 3.265 3.265 0.109 0.616 0.235 0.207 3.918 0.120 0.120 4.030 0.882 3.918 0.132 0.140 0.140 0.323 0.291 5.393 0.898 5.263 5.263 0.153 0.639 0.160 0.160 0.449 0.405 7.448 0.902 7.301 7.301 0.173 0.641 0.615 0.180 0.180 0.582 9.504 0.946 9.339 9.339 0.194 0.649 0.200 0.200 0.823 0.828 11.559 1.007 11.376 11.376 0.216 0.660 0.220 0.220 1.071 1.152 13.614 1.076 13.414 13.414 0.238 0.672 0.240 0.240 1.359 15.670 15.451 0.261 1.562 1.149 15.451 0.683 0.260 0.260 1.689 2.065 17.725 1.223 17.489 17.489 0.283 0.694 0.280 0.280 2.059 2.671 19.780 1.297 19.527 19.527 0.306 0.704 0.300 0.300 2.470 3.387 21.835 1.371 21.564 21.564 0.329 0.714 0.320 2.921 4.220 1.445 23.602 0.352 0.320 23.891 23.602 0.724 0.340 0.340 3.414 5.178 25.946 1.517 25.639 25.639 0.376 0.733 0.360 28.001 27.677 27.677 0.399 0.360 3.947 6.268 1.588 0.741 0.380 0.380 4.521 7.497 30.057 1.658 29.715 29.715 0.423 8.872 1.728 31.752 0.400 0.400 5.135 31.752 0.757 32.112 0.446 0.420 0.420 5.791 10.399 34.167 1.796 33.790 33.790 0.470 0.765 0.440 0.440 6.487 12.086 36.223 1.863 35.827 35.827 0.494 0.772 0.460 0.460 7.224 13.937 38.278 1.929 37.865 37.865 0.518 0.779 0.480 0.480 8.002 15.960 40.333 1.995 39.903 39.903 0.542 0.785 0.500 0.500 8.820 18.161 42.388 2.059 41.940 41.940 0.566 0.792 0.520 0.520 9.679 20.545 44.444 2.123 43.978 43.978 0.590 0.798 0.540 0.540 10.579 23.119 46.499 2.185 46.016 46.016 0.614 0.804 0.560 0.560 11.515 26.231 47.554 2.278 47.053 0.641 47.053 0.812 0.580 0.580 12.456 29.879 47.609 2.399 47.091 47.091 0.669 0.822 13.399 2.516 0.600 0.600 33.714 47.664 47.128 47.128 0.698 0.832 0.620 0.620 14.341 37.732 47.719 2.631 47.166 47.166 0.728 0.841 0.640 0.640 15.285 41.927 47.774 2.743 47.204 47.204 0.757 0.850 0.660 0.660 16.230 46.298 47.829 2.853 47.241 47.241 0.787 0.858 0.680 17.180 50.196 48.843 2.922 48.246 48.246 0.813 0.863 0.680 0.700 0.700 18.164 53.646 50.816 2.953 50.219 50.219 0.836 0.866 0.720 0.720 19.188 57.308 52.789 2.987 52.192 52.192 0.859 0.868 0.740 0.740 20.252 61.184 54.762 3.021 54.164 54.164 0.882 0.871 0.760 56.735 0.760 21.355 65.279 3.057 56.137 56.137 0.905 0.874 0.780 0.780 22.497 69.598 58.708 3.094 58.109 58.109 0.929 0.877 23.679 0.800 60.082 0.953 0.879 0.800 74.146 60.681 3.131 60.082 0.820 0.820 24.901 78.928 3.170 62.055 0.976 0.882 62.654 62.055 0.840 0.840 26.162 83.947 64.627 3.209 64.027 64.027 1.000 0.885 Inlets 40, 41

Future Basin 4b = 32.52 cfs Basin C6 = 2.78 cfs Partial Basin C5 = 1.59 cfs TOTAL = 36.89 cfs Street Capacity Q = 36.89 cfs d = .62 < .67' E = .72' < .90' Inlet Capacity @ S = .45% d = .62 Q inlet = 7.4 cfs Inlets 40, 41

Residual Flow = 36.89 - 2*(7.4) = 22.1cfs

Inlet 39
Sump condition:
Residual flow = 22.1 cfs
Partial Basin C5 = 6.26 cfs
TOTAL = 28.36 cfs

SAGAN LOOP ANALYSIS OF AN INLET IN A SUMP CONDITION -

 $Q=C*A*(2*G*H)^{0.5}$ INLET TYPE: Double Grate Type "A" with curb opening wings on both sides on inlet. ORIFICE: Q=C*L*H^1.5

Wing opening* C=0.6Grate opening C=0.6Grate opening C=3.0Wing opening C = 3.0

 $Q=0.6(7.14)((64.4*H))^{0.5}$ $Q=1.2*(64.4*H)^{0.5}$ L(double grate)=[2(2.67')+2(1.8')]=8.94 ft A(double grate)=7.14 sf $Q=3.0(4.0)H^{1.5}=12.0H^{1}$. $Q=3.0(8.94)H^{1.5}=26.82*H^{1.5}$ L = 4.0 ft

*not included in the orifice calcs

A=2.0 sf

			Q (CFS)	Q (CFS)	Q (CFS)	TOTAL	
			WEIR	WEIR	ORIFICE	Ö	
	WS	HEIGHT	"A"	DOUBLE	DOUBLE	(CFS)	
	ELEVATION	ELEVATIONABOVE INLET	OPENING	GRATE	GRATE		COMMENTS:
~FL @ INLET	0.00	0.00	0.00	0.00	0.00	0.00	Flow at double "A" inlet w/ two wing openings
	0.10	0.10	0.38	0.85	10.87	1.61	Weir controls on grate analysis
	0.20	0.20	1.07	2.40	15.37	4.55	
	0.30	0.30	1.97	4.41	18.83	8.35	
	0.40	0.40	3.04	6.78	21.74	12.86	
	0.50	0.50	4.24	9.48	24.31	17.97	
	0.60	09.0	5.58	12.46	26.63	23.62	
TOP OF CURB	0.70	0.70	7.03	15.71	28.76	29.76	Q(100 yr) = 28.36 cfs is provided at this depth
	0.80	0.80	8.59	19.19	30.75	36.36	
ROW LIMIT	0.90	0.90	10.25	22.90	32.61	43.39	$Q(2 \times 100 \text{ yr}) = 56.72 \text{ cfs OVERFLOWS**}$ at this depth
	1.00	1.00	12.00	26.82	34.38	50.82	

The total runoff intercepted by the inlet at the low point in the road is: NOTE:

Qr(100) = 2*[(runoff of the wing opening) + (the lesser of the weir or orifice amount taken by the double grate)].

** This inlet has an emergency overflow into POND 2A

APPENDIX B INFILTRATION CALCULATIONS

POND INFILTRATION CALCULATIONS:

Per the Original Drainage report:

Infiltration calculations were based on an average of percolation test results performed by Geo-Test, Inc. on a permanent pond immediately north of Albuquerque Studios Mesa del Sol, New Mexico dated May 17, 2007, File No. 1-61211 (see summary tables below). A percolation rate of 0.3 in/hr. was recorded for 24" above ground surface, which was neglected for our average in our infiltration calculations. This was based on the assumption that the ponds would be cleaned and maintained before the point of virtually no infiltration was reached. The average infiltration used was 1.74 in/hr. A factor of safety of 1.1 was then used for the infiltration basin and a factor of safety of 2.0 was used for the remaining area of the pond to determine the time to infiltrate the required storm water volume, which is approximately the 2-year storm water volume in Equation 1.

Equation 1.

T_{Drain}=Vol req / ((i pond (Ainf basin)) + (i infiltration basin (Aeff)))

Where:

Vol req = Storm Volume (cf)

i pond = Pond Infiltration rate = i/2.0 (in/hr)

i infiltration basin = Infiltration basin rate= i/1.1 (in/hr)

 $A_{inf basin} = Area Infiltration Basin (sf)$

Aeff = Avg Pond Area Minus Infiltration basin (sf)

POND INFILTRATION SUMMARY

POND	100-YR 10- DAY RETENTION VOLUME (AC- FT)	2-YR RETENTION VOLUME (AC- FT)	AREA OF INFILTRATION BASIN (SF)	AVG AREA OF POND (SF)	TIME TO INFILTRATE 100-YR 10- DAY VOLUME (HR)	TIME TO INFILTRATE 2-YR VOLUME (HR)
1 (Future)	N/A	N/A	N/A	N/A	N/A	N/A
2A	8.29	3.6	1500	100000	49	21
2B	7.66	3.32	1500	50000	92	39
3	8.54	3.71	1500	70000	72	31
4*	19.04	8.26	5000	130000	85	37

^{*}denotes possible future configuration

APPENDIX C POND VOLUME CALCULATIONS

Pond 2A: AS BUILT

Project:
Basin Description: Montage Unit 4

Contour Elevation	Contour Area (sq. ft)	Depth (ft)	Incremental Volume Avg. End (cu. ft)	Cumulative Volume Avg. End (cu. ft)	Incremental Volume Conic (cu. ft)	Cumulative Volume Conic (cu. ft)
5,294.00	759.0007	N/A	N/A	0	N/A	0
5,295.00	6,496.4904	1.00	3628	3628	3159	3159
5,296.00	15,521.0366	1.00	11009	14637	10686	13845
5,297.00	25,072.6797	1.00	20297	34933	20107	33952
5,298.00	42,363.5936	1.00	33718	68652	33342	67294
5,299.00	59,924.2855	1.00	51144	119795	50891	118185
5,300.00	84,854.3372	1.00	72389	192185	72029	190214

Pond 2B: AS-BUILT

Project:
Basin Description: Montage Unit 4

Contour Elevation	Contour Area (sq. ft)	Depth (ft)	Incremental Volume Avg. End (cu. ft)	Cumulative Volume Avg. End (cu. ft)	Incremental Volume Conic (cu. ft)	Cumulative Volume Conic (cu. ft)
5,289.00	12,478.9924	N/A	N/A	0	N/A	0
5,290.00	16,122.6783	1.00	14301	14301	14262	14262
5,291.00	18,786.6043	1.00	17455	31755	17438	31700
5,292.00	21,202.8257	1.00	19995	51750	19983	51682
5,293.00	23,590.7187	1.00	22397	74147	22386	74068
5,294.00	26,062.4611	1.00	24827	98974	24816	98885
5,295.00	28,575.2261	1.00	27319	126292	27309	126194
5,296.00	31,184.1365	1.00	29880	156172	29870	156064
5,297.00	33,867.6816	1.00	32526	188698	32517	188581
5,298.00	36,671.9663	1.00	35270	223968	35261	223841
5,299.00	39,685.1846	1.00	38179	262146	38169	262010
5,300.00	43,671.2971	1.00	41678	303825	41662	303672

Proposed Pond 2A Project: Basin Description: Montage Unit 4

Contour Elevation	Contour Area (sq. ft)	Depth (ft)	Incremental Volume Avg. End (cu. ft)	Cumulative Volume Avg. End (cu. ft)	Incremental Volume Conic (cu. ft)	Cumulative Volume Conic (cu. ft)
5,294.000	20,854.86	N/A	N/A	0.00	N/A	0.00
5,295.000	32,595.13	1.000	26724.99	26724.99	26507.44	26507.44
5,296.000	41,640.14	1.000	37117.64	63842.63	37025.46	63532.90
5,297.000	53,401.03	1.000	47520.59	111363.22	47398.84	110931.74
5,298.000	64,637.35	1.000	59019.19	170382.42	58929.86	169861.60
5,299.000	81,800.83	1.000	73219.09	243601.51	73050.87	242912.47
5,300.000	97,355.21	1.000	89578.02	333179.53	89465.27	332377.74

APPENDIX D BASIN SUMMARY SHEET

BASIN SUMMARY

** Basins from Original Unit 3 and 4 Basin Map Volume for Future Basin 5 from Unit 1 and 2 Existing and Developed Conditions Map

(AC)	(AC)	UNITS	UNITS	А	В	С	AMENDED UNIT 4 REV-D	PREV-D	AMENDED UNIT 4 10 YR	AMENDED UNIT 4 100YR	PREV UNIT 4 100YR*	TOTAL for AMENDED Unit 3 & 4	100 YR 6HR	AMENDED UNIT 4 100 YR 10-DAY	PREV UNIT 4 100Y-10D*	TOTAL for AMENDED Unit 3 & 4
									-							
6.0	5.8	34	32	0.0%	22.7%	22.7%	54.6%	53.0%	13.85	22.66	21.83	22.66	0.79	1.23	1.17	1.23
5.1	4.7	27	21	0.0%	24.1%	24.1%	51.9%	46.0%	11.51	18.96	17.01	18.96	0.66	1.01	0.87	1.01
1.9	4.4	16	17	0.0%	13.4%	13.4%	73.2%	41.0%	5.14	8.07	15.49	8.07	0.29	0.48	0.77	0.48
	1.9			0.0%	26.5%	26.5%	47.0%		4.11		6.87	20.24	0.24		0.35	1.09
0.7		0		0.0%	24.9%	24.9%	50.3%	47.0%	1.66	2.74			0.10	0.14		
1.3		11		0.0%	12.6%	12.6%	74.8%	47.0%	3.48	5.44			0.20	0.33		
0.0	4.4	16	16	0.0%	30.4%	30.4%	39.2%	39.2%	8.97			23.60	0.52			0.75
	1.6			0.0%	33.5%	33.5%	33.0%		6.16		5.45	12.74	0.18		0.25	0.83
1.6	3.2	5	9	0.0%		24.9%	50.3%	33.0%	3.53	5.84			0.41	0.52	0.50	
				0.0%	24.5%	24.5%	51.0%		13.28	0.00	21.93	21.93	0.76	0.00	1.16	0.00
																5.39
										55	00.00			•	0.0.	6.19
																3
									1		I					
	22			0.0%	23.1%	23.1%	53.9%		5 18		8 48	34.75	0.30		0.46	1.86
1.0		4								3.46	0.10	0 0		0.17	0.10	0.17
		8														0.25
	22		10					46.0%			7 96	7 96			0.41	0.44
				_				10.070	_	0.01				0.11		0.94
2.4	2.0	13								8 96	11.00			0.48	0.00	0.0 .
	4.6		23	_						2.71		16.97		0.13		0.89
																1.19
																0.57
																0.50
0.0	2.0		- ' '								10.80			0.00	0.57	0.00
2.1		n/a								7.81	10.00				0.51	0.41
	7.7		n/a								28.64				1.52	1.35
0.0	7.1	II/a	TI/A	0.070	24.570	24.570	31.070		13.57				0.00			8.58
			-						-	61.04	66.93			3.24	3.56	8.57
									1			102.73				6.57
									1							
0.0	0.8	3	3	0.0%	30.0%	30.0%	40.0%	40.0%	1.64	2.80	2.80	2.80	0.09	0.14	0.14	0.14
	0.0		Ü					10.070			2.00	2.00			0.14	0.14
									_							
0.7		4		0.078	23.070	23.070	JZ.4 /0		1.09				0.10			
										47.31				2.48		
0.4		,	,	0.00/	0.4.50	0.4.50/	54.00/		7.00	10.55			0.11	0.07		
8.7		n/a	n/a	0.0%	24.5%	24.5%	51.0%		19.69				1.13			
										45.07				2.39		
	5.1 1.9 0.7 1.3	5.1 4.7 1.9 4.4 1.9 0.7 1.3 0.0 4.4 1.6 1.6 1.6 3.2 1.0 1.2 2.2 2.9 2.4 0.7 0.0 4.6 0.0 6.6 0.0 3.7 0.0 2.9 2.1 6.8 7.7	5.1 4.7 27 1.9 4.4 16 1.9 0.7 0 1.3 11 0.0 4.4 16 1.6 3.2 5 1.0 4.5 22 2.2 12 2.9 2.9 2.1 13 0.7 7 0.0 4.6 23 0.0 6.6 28 0.0 3.7 10 0.0 2.9 11 2.1 n/a 6.8 7.7 n/a 0.0 0.8 3 2.3 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9 1.6 9	5.1	5.1 4.7 27 21 0.0% 1.9 4.4 16 17 0.0% 0.0 1.9 0.0% 0.0% 1.3 11 0.0% 0.0% 0.0 4.4 16 16 0.0% 1.6 3.2 5 9 0.0% 1.0 4 0.0% 0.0% 1.0 4 0.0% 0.0% 2.2 12 10 0.0% 2.9 0.0% 0.0% 0.0% 2.9 0.0% 0.0% 0.0% 0.0 4.6 23 23 0.0% 0.0 3.7 10 10 0.0% 0.0 3.7 10 10 0.0% 0.0 2.9 11 11 0.0% 2.1 n/a n/a 0.0% 2.1 n/a n/a 0.0% 0.0 0.8 3 3 0.0%	5.1 4.7 27 21 0.0% 24.1% 1.9 4.4 16 17 0.0% 13.4% 0.7 0 0.0% 24.9% 1.3 11 0.0% 12.6% 0.0 4.4 16 16 0.0% 30.4% 1.6 3.2 5 9 0.0% 24.9% 1.6 3.2 5 9 0.0% 24.5% 1.0 4 0.0% 23.1% 1.2 8 0.0% 23.1% 2.9 0.0% 23.6% 0.7 7 0.0% 23.6% 0.0 4.6 23 23 0.0% 25.3% 0.0 4.6 23 23 0.0% 28.1% 0.0 3.7 10 10 0.0% 24.5% 0.0 3.7 10 10 0.0% 24.5% 2.1 n/a n/a 0.0% 24.5%	5.1 4.7 27 21 0.0% 24.1% 24.1% 1.9 4.4 16 17 0.0% 13.4% 13.4% 0.7 0 0.0% 24.9% 24.9% 1.3 11 0.0% 24.9% 24.9% 0.0 4.4 16 16 0.0% 30.4% 30.4% 1.6 3.2 5 9 0.0% 24.9% 24.9% 1.6 3.2 5 9 0.0% 24.5% 24.5% 1.0 4 0.0% 23.1% 23.1% 23.1% 1.2 8 0.0% 23.1% 23.1% 2.9 0.0% 23.6% 28.6% 2.4 13 0.0% 23.6% 23.6% 0.7 7 0.0% 23.6% 23.6% 0.0 4.6 23 23 0.0% 25.3% 25.3% 0.0 4.6 23 23 0.0% 28.1%	5.1 4.7 27 21 0.0% 24.1% 24.1% 51.9% 1.9 4.4 16 17 0.0% 13.4% 13.4% 73.2% 0.0 1.9 0.0% 24.9% 24.9% 50.3% 1.3 11 0.0% 12.6% 12.6% 74.8% 0.0 4.4 16 16 0.0% 30.4% 30.4% 39.2% 1.6 3.2 5 9 0.0% 24.9% 24.9% 50.3% 1.6 3.2 5 9 0.0% 24.5% 24.5% 51.0% 1.0 4 0.0% 23.1% 23.1% 53.9% 53.9% 1.0 4 0.0% 23.1% 23.1% 53.9% 2.2 12 10 0.0% 23.7% 23.6% 23.6% 2.4 13 0.0% 23.6% 23.6% 52.8% 0.7 7 0.0% 23.6% 23.6% 52.8%	5.1 4.7 27 21 0.0% 24.1% 24.1% 51.9% 46.0% 1.9 4.4 16 17 0.0% 13.4% 13.4% 73.2% 41.0% 0.7 0 0.0% 26.5% 26.5% 26.5% 47.0% 1.3 11 0.0% 12.6% 12.6% 74.8% 47.0% 1.3 11 0.0% 12.6% 12.6% 74.8% 47.0% 0.0 4.4 16 16 0.0% 30.4% 33.5% 33.0% 1.6 3.2 5 9 0.0% 24.9% 24.9% 50.3% 33.0% 1.6 3.2 5 9 0.0% 24.9% 24.9% 50.3% 33.0% 1.6 3.2 1 0.0% 23.1% 23.1% 53.9% 42.8% 1.0 4 0.0% 23.1% 23.1% 53.9% 42.8% 1.2 8 0.0% 23.1% 23	5.1 4.7 27 21 0.0% 24.1% 24.1% 51.9% 46.0% 11.51 1.9 4.4 16 17 0.0% 13.4% 13.4% 73.2% 41.0% 5.14 0.7 0 0.0% 26.5% 26.5% 47.0% 4.0% 4.11 0.7 0 0.0% 24.9% 24.9% 50.3% 47.0% 1.66 1.3 11 0.0% 24.9% 24.9% 74.8% 47.0% 3.48 0.0 4.4 16 16 0.0% 33.5% 33.5% 33.0% 6.16 1.6 3.2 5 9 0.0% 24.9% 24.9% 50.3% 33.0% 35.3 1.0 4 0.0% 23.1% 23.1% 53.9% 5.18 1.2 8 0.0% 23.1% 23.7% 53.9% 5.26% 46.0% 5.05 1.2 8 0.0% 23.6% 23.6% 55.2%	5.1 4.7 27 21 0.0% 24.1% 51.9% 46.0% 11.51 18.96 1.9 4.4 16 17 0.0% 13.4% 13.4% 73.2% 41.0% 5.14 8.07 0.7 0 0.0% 26.5% 26.5% 26.5% 47.0% 41.11 0.0% 24.9% 24.9% 50.3% 47.0% 1.66 2.74 1.3 11 0.0% 12.6% 12.6% 74.8% 47.0% 3.48 5.44 1.0 4.4 16 16 0.0% 30.4% 39.2% 8.97 3.48 5.44 1.6 3.2 5 9 0.0% 24.9% 24.9% 39.2% 8.97 3.53 5.84 2.6% 2.6% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 33.5% 3	5.1 4.7 27 21 0.0% 24.1% 51.9% 46.0% 11.51 18.96 17.01 1.9 4.4 16 17 0.0% 22.5% 26.5% 47.0% 5.14 8.07 15.49 0.7 0 0.0% 22.9% 24.9% 50.3% 47.0% 3.48 5.44 0.0 4.4 16 16 16 0.0% 33.0% 12.6% 74.8% 47.0% 3.48 5.44 1.6 32 5 9 0.0% 33.5% 33.2% 39.2% 8.97 1.6 32 5 9 0.0% 23.4% 50.3% 33.0% 3.53 5.84 1.6 3.2 5 9 0.0% 24.5% 24.5% 51.0% 13.28 0.00 21.93 1.0 4 0.0% 23.1% 23.1% 53.9% 5.18 8.48 1.0 4 0.0% 22.1% 22.1% 52.	5.1 4.7 2.7 2.1 0.0% 24.1% 51.9% 48.0% 11.51 18.96 17.01 18.96 1.9 4.4 16 1.7 0.0% 13.4% 13.4% 73.2% 41.0% 5.14 8.07 18.49 8.07 0.7 0 0.0% 22.49% 28.5% 47.0% 4.11 6.67 20.24 0.7 0 0.0% 22.49% 50.3% 47.0% 1.66 2.74 1.3 11 0.0% 12.6% 74.8% 47.0% 3.66 2.74 1.6 16 16 0.0% 30.4% 30.2% 30.2% 8.97 2.25.0 1.6 3.2 5 9 0.0% 32.49% 50.3% 33.0% 5.66 5.45 12.74 1.6 3.2 2 9 0.0% 23.1% 53.9% 5.18 8.48 34.75 1.6 3.2 1 0.0% 23.1% 23.1% <td> 5.1</td> <td>5.1 4.7 2.7 2.1 0.0% 24.1% 51.9% 46.0% 11.51 18.98 17.01 18.98 0.06 1.01 1.9 4.1 10 0.0% 26.9% 26.9% 47.0% 41.0% 0.87 20.24 0.24 0.00 0.00 26.9% 24.0% 25.0% 36.0% 36.2% 36.0% 36.</td> <td>5.1 4.7 27 21 1 0.0% 24.1% 24.1% 51.9% 60.0% 11.51 18.96 12.01 18.96 0.68 1.01 0.07 1.0 0.07 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0</td>	5.1	5.1 4.7 2.7 2.1 0.0% 24.1% 51.9% 46.0% 11.51 18.98 17.01 18.98 0.06 1.01 1.9 4.1 10 0.0% 26.9% 26.9% 47.0% 41.0% 0.87 20.24 0.24 0.00 0.00 26.9% 24.0% 25.0% 36.0% 36.2% 36.0% 36.	5.1 4.7 27 21 1 0.0% 24.1% 24.1% 51.9% 60.0% 11.51 18.96 12.01 18.96 0.68 1.01 0.07 1.0 0.07 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

^{*} Based on Area of basins in Unit 4 (excluding Unit 3B)

EXHIBITS

EXHIBIT 1: UNIT 4 PRELIMINARY PLATS

EXHIBIT 2: Amended DEVELOPED CONDITIONS

BASIN MAPS

EXHIBIT 3: Amended INLET AND STORM DRAIN

ANALYSIS

EXHIBIT 4: GRADING PLAN

EXHIBIT 1 UNIT 4 PRELIMINARY PLATS

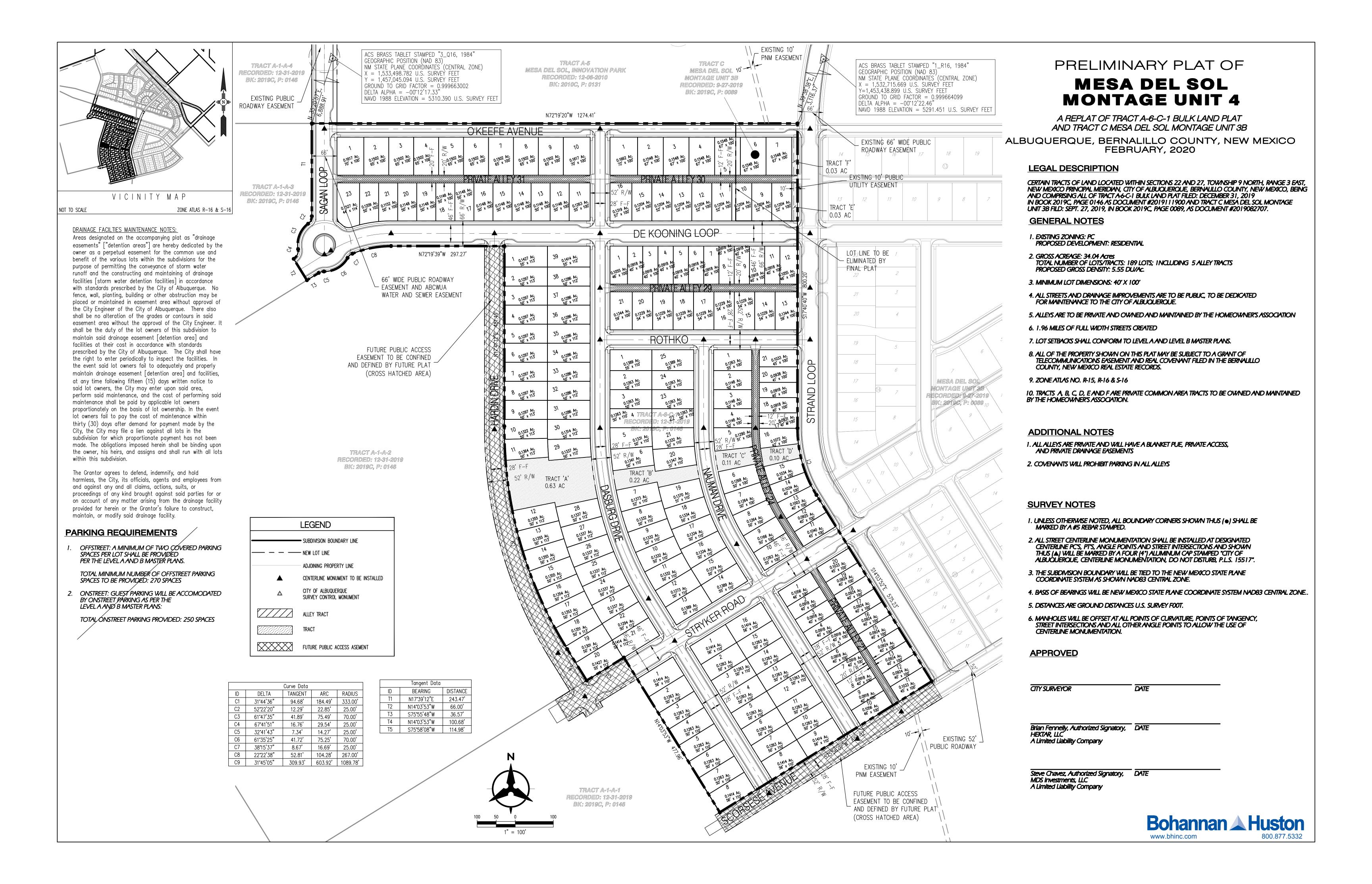
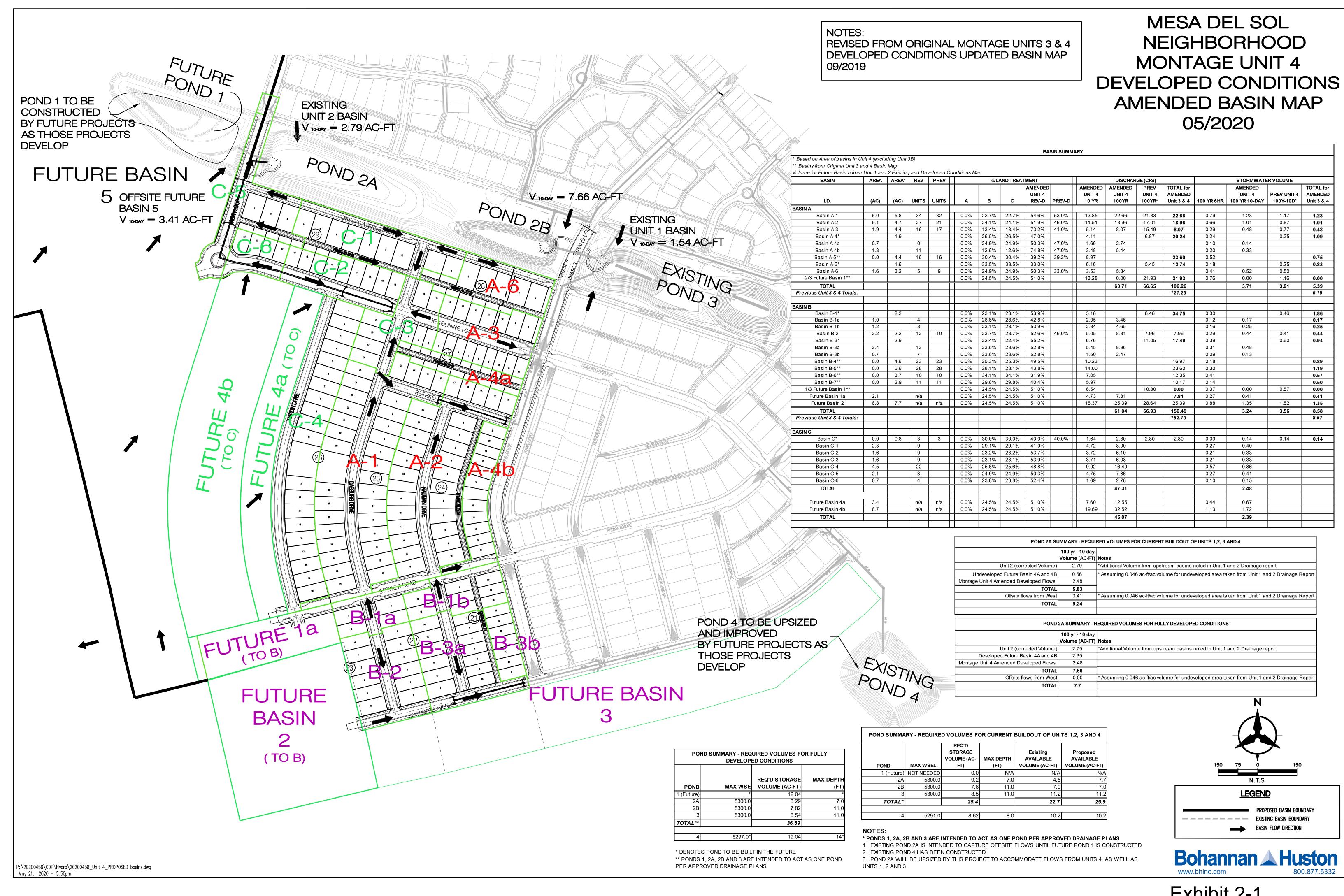


EXHIBIT 2

Amended DEVELOPED CONDITIONS BASIN MAPS



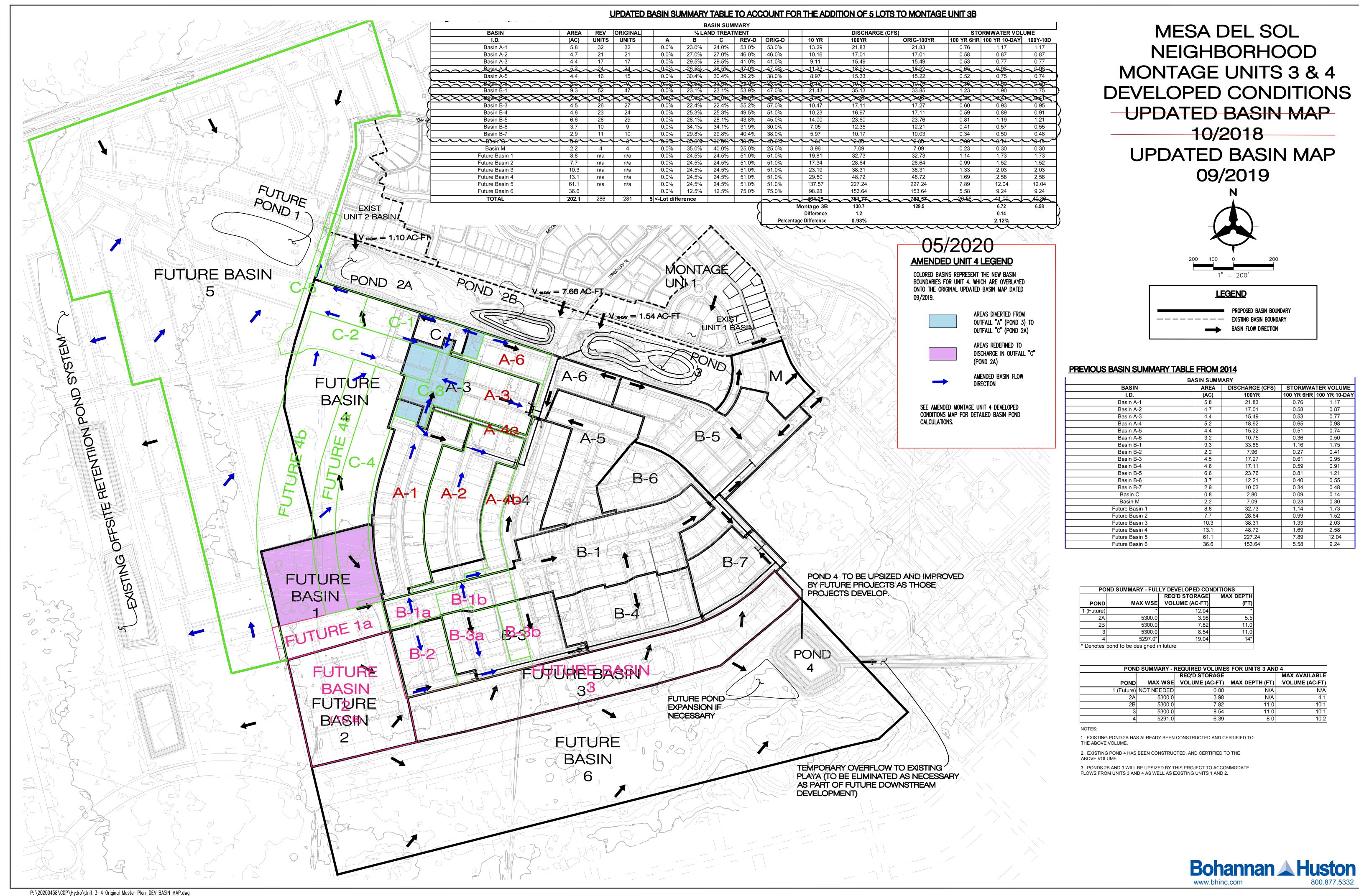


EXHIBIT 3

Amended INLET AND STORM DRAIN ANALYSIS



			SUMI	MARY OF INLET FLOW	VS			
ID	STREET SLOPE	STREET FLOW DEPTH (ft)	STREET FLOW UPSTREAM OF INLET (cfs)	REVISED STREET FLOW UPSTREAM OF INLET (cfs)	FLOW CAPTURED BY INLET (cfs)	REVISED FLOW CAPTURED BY INLET (cfs)	STREET FLOW BYPASSING INLET (cfs)	REVISED STREET FLOW BYPASSING INLET (cfs)
IN1	0.60%	0.52	22.7	11.4	9.5	5.0	13.2	6.4
IN2	0.60%	0.52	22.7	11.4	9.5	5.0	13.2	6.4
IN3	0.60%	0.58	21.7	16.2	9.2	6.2	12.50	10.0
IN4	0.60%	0.58	21.7	16.2	9.2	6.2	12.50	10.0
IN5	SUMP	0.60	13.3	10.6	13.3	10.6	N/A	N/A
IN6	SUMP	0.60	13.3	10.6	13.3	10.6	N/A	N/A
IN7	0.75%	0.60	22.0	20.2	9.2	9.2	12.8	11.0
IN8	0.75%	0.60	22.0	20.2	9.2	9.2	12.8	11.0
IN9	0.75%	0.51	12.8	11.0	7.0	7.0	5.8	4.0
IN10	0.75%	0.51	12.8	11.0	7.0	7.0	5.8	4.0
IN11	SUMP	0.60	13.3	10.6	13.3	10.6	N/A	N/A
IN12	SUMP	0.60	13.3	10.6	13.3	10.6	N/A	N/A
IN13	0.60%	0.63	22.1		9.3		12.80	,
IN14	0.60%	0.63	22.1		9.3		12.80	
IN15	0.50%	0.65	22.1	21.0	10.0	7.7	12.1	13.3
IN16	0.50%	0.65	22.1	21.0	10.0	7.7	12.1	13.3
IN17	0.50%	0.65	12.1	21.6	6.3	7.7	5.8	13.9
IN18	0.50%	0.65	12.1	21.6	6.3	7.7	5.8	13.9
IN19	0.50%	0.64	19.9	19.4	8.9	8.9	11.0	10.5
IN20	0.50%	0.64	19.9	19.4	8.9	8.9	11.0	10.5
IN21	0.50%	0.52	11.0		6.0		5.00	
IN22	0.50%	0.52	11.0		6.0		5.00	
IN23	0.50%	0.63	19.1		8.9		10.20	
IN24	0.50%	0.63	19.1		8.9		10.20	
IN25A	0.75%	0.59	18.9		7.6		11.30	
IN25	0.75%	0.59	11.3		8.8		2.50	
IN26A	0.75%	0.59	18.9		7.6		11.30	
IN26	0.75%	0.59	11.3		8.8		2.50	
IN27				DELETED				
IN28	SUMP	0.40	8.9		8.9		N/A	
IN29	SUMP	0.51	17.7		17.7		N/A	
IN30	SUMP	0.40	8.9		8.9		N/A	
IN31	SUMP	0.55	11.9		11.9		N/A	
IN32	SUMP	0.55	11.9		11.9		N/A	

ID	SIZE INCHES	SLOPE (%)	Q (cfs) ALLOWABLE	Q (cfs) ACTUAL	Revised Q
0001		. ,			07.0
SDP1	48	1.00%	143.8	122.8	97.2
SDP2	48	1.00%	143.8	122.8	97.2
SDP3	42	1.00%	100.6	69.8	54.8
SDP4	36	1.00%	66.7	37.4	22.4
SDP5	36	1.00%	66.7	37.4	22.4
SDP6	24	1.80%	30.7	19.0	10.0
SDP7	36	1.00%	66.7	53.0	42.4
SDP8	18	1.40%	12.5	13.3	
SDP9	24	39.30%	141.7	26.5	
SDP10	18	1.40%	12.5	13.3	5.0
SDP11	24	40.50%	143.9	26.5	5.0
SDP12	18	1.20%	11.7	9.2	9.2
SDP13	24	46.30%	153.9	16.2	16.2
SDP14	18	1.20%	11.7	9.2	9.2
SDP15	24	47.70%	156.3	16.2	16.2
SDP16	18	43.70%	69.5	9.2	6.2
SDP17	18	42.30%	68.3	9.2	6.2
SDP18	18	10.40%	33.9	9.5	5.0
SDP19	18	10.40%	33.9	9.5	5.0
SDP20	60	0.85%	239.9	191.0	
SDP21	60	0.85%	239.9	191.0	
SDP22	48	0.85%	132.4	110.8	
SDP23	42	0.85%	92.8	60.0	
SDP24	42	0.85%	92.8	42.4	
SDP25	36	1.10%	70.8	23.8	
SDP26	18	7.80%	29.4	11.9	
SDP27	18	4.20%	21.6	11.9	
SDP28	24	18.40%	96.9	18.6	
SDP29	18	9.30%	32.0	9.3	
SDP30	18	8.80%	31.1	9.3	
SDP31	18	42.20%	68.2	8.8	
SDP32	18	41.40%	67.6	8.8	
SDP33	18	1.30%	11.8	12.7	
SDP34	24	45.10%	151.9	25.4	
SDP35	18	1.30%	11.8	12.7	
SDP36	24	44.20%	150.5	25.4	
SDP37	48	1.00%	143.6	80.2	
SDP38	48	1.00%	143.6	80.2	
SDP39	36	1.00%	66.7	62.4	
SDP40	36	1.00%	66.7	62.4	
SDP41	36	1.00%	66.7	32.6	30.8
SDP42	36	1.10%	69.2	32.6	15.4
SDP43	24	9.40%	69.4	16.3	7.7
SDP44	18	1.50%	12.8	10	7.7
SDP45	18	1.50%	12.8	10	7.7
SDP46	24	9.10%	68.2	16.3	7.7
SDP47	18	1.10%	11	8.9	
SDP48	24	47.50%	155.9	14.9	
SDP49	18	1.10%	11	8.9	
SDP50	24	45.90%	153	14.9	
SDP51	18	82.80%	95.6	8.9	

ID	SIZE	SLOPE (%)	Q (cfs) ALLOWABLE	Q (cfs) ACTUAL
SDP53	42	1.74%	132.7	95.5
SDP54	42	0.96%	98.6	64.0
SD55	42	0.50%	71.1	64.0
SD56	18	11.03%	34.9	7.4
SD57	18	10.49%	34.0	7.4
SD58	42	0.50%	71.1	49.2
SD59	42	0.50%	71.1	49.2
SD60	42	0.50%	71.1	49.2
SD61	42	0.50%	71.1	49.2
SD62	18	12.53%	37.2	6.6
SD63	18	15.17%	40.9	6.6
SD64	36	0.50%	47.2	36.0
SD65	18	1.19%	11.5	9.0
SD66	18	8.54%	30.7	9.0
SD67	18	3.51%	19.7	9.0
SD68	18	11.87%	36.2	9.0

	SUN	MARY OF	INLET FLOWS Ne	ew SD	
	STREET	STREET	STREET FLOW	FLOW	STREET
ID	SLOPE	FLOW	UPSTREAM OF	CAPTURE	FLOW
	JLOI L	DEPTH	INLET (cfs)	D BY	BYPASSIN
IN39	0.62%	Sump	31.52	31.52	0
IN40	0.40%	0.62	18.6	7.4	11.2
IN41	0.40%	0.62	18.6	7.4	11.2
IN42	0.45%	0.60	16.4	6.9	9.5
IN43	0.45%	0.60	16.4	6.9	9.5
IN44	0.62%	Sump	9.0	9.0	0.0
IN45	0.62%	Sump	9.0	9.0	0.0
IN46	0.62%	Sump	9.0	9.0	0.0
IN47	0.62%	Sump	9.0	9.0	0.0

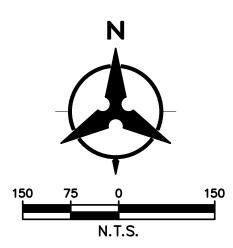
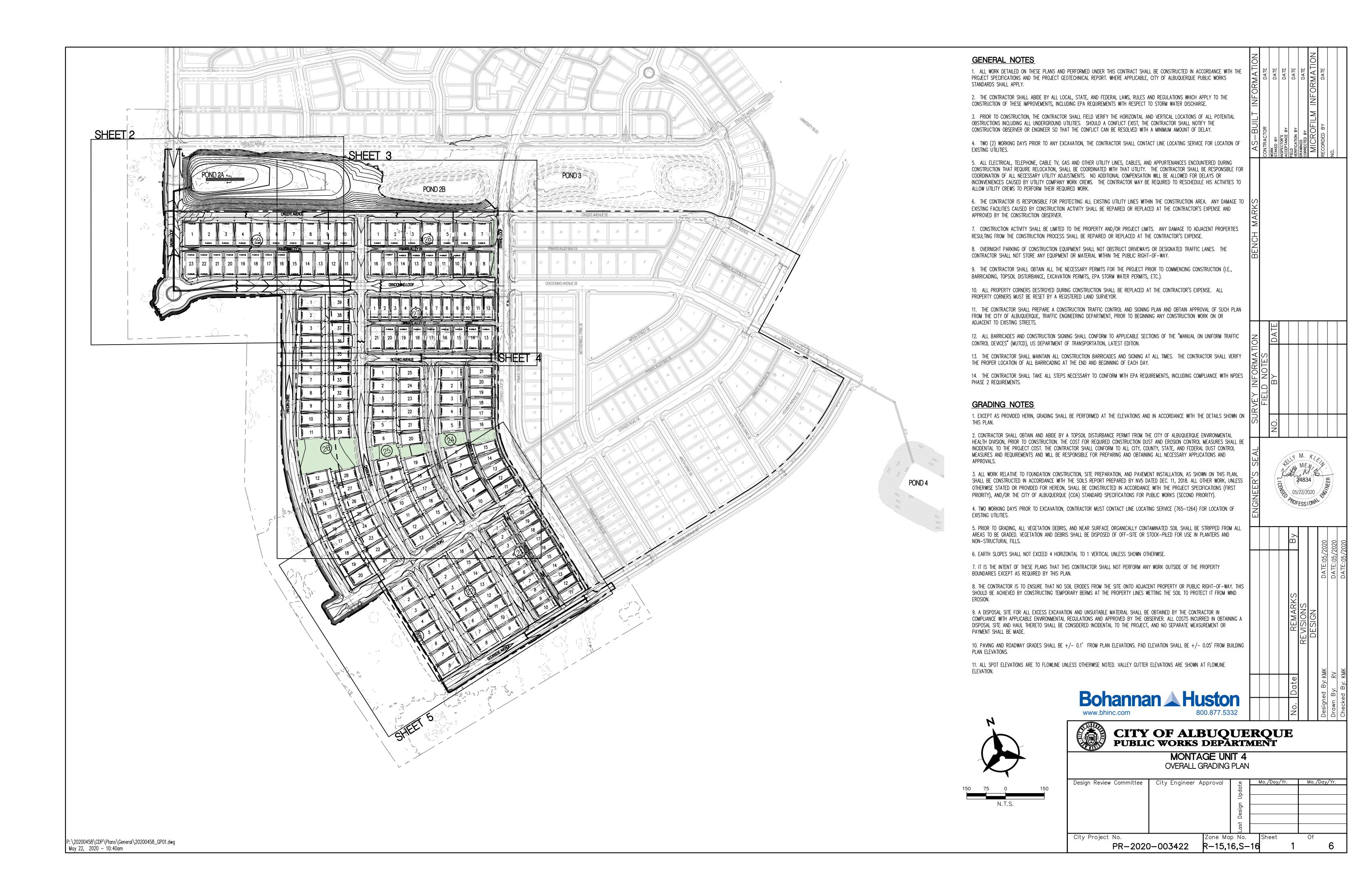
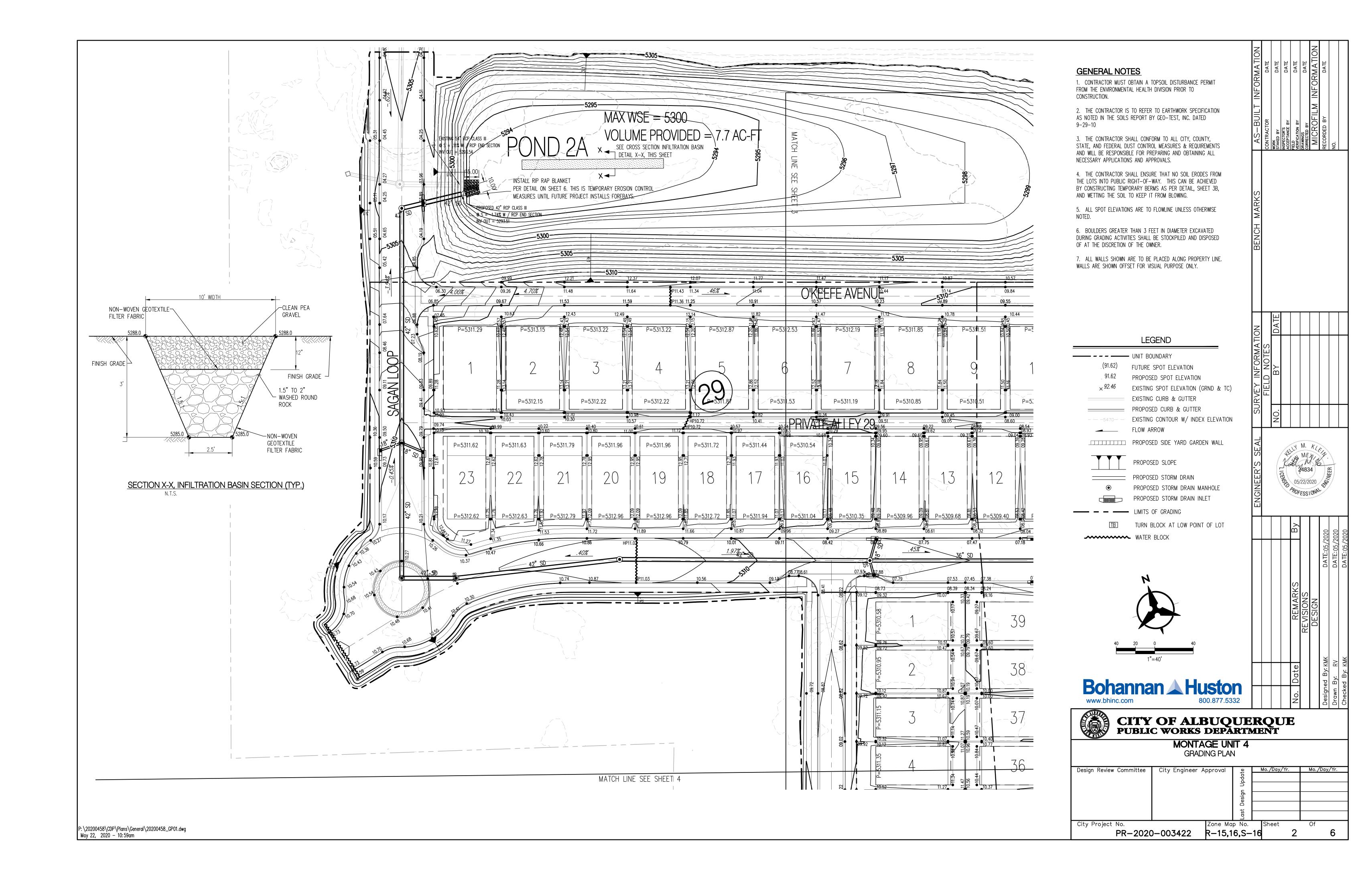
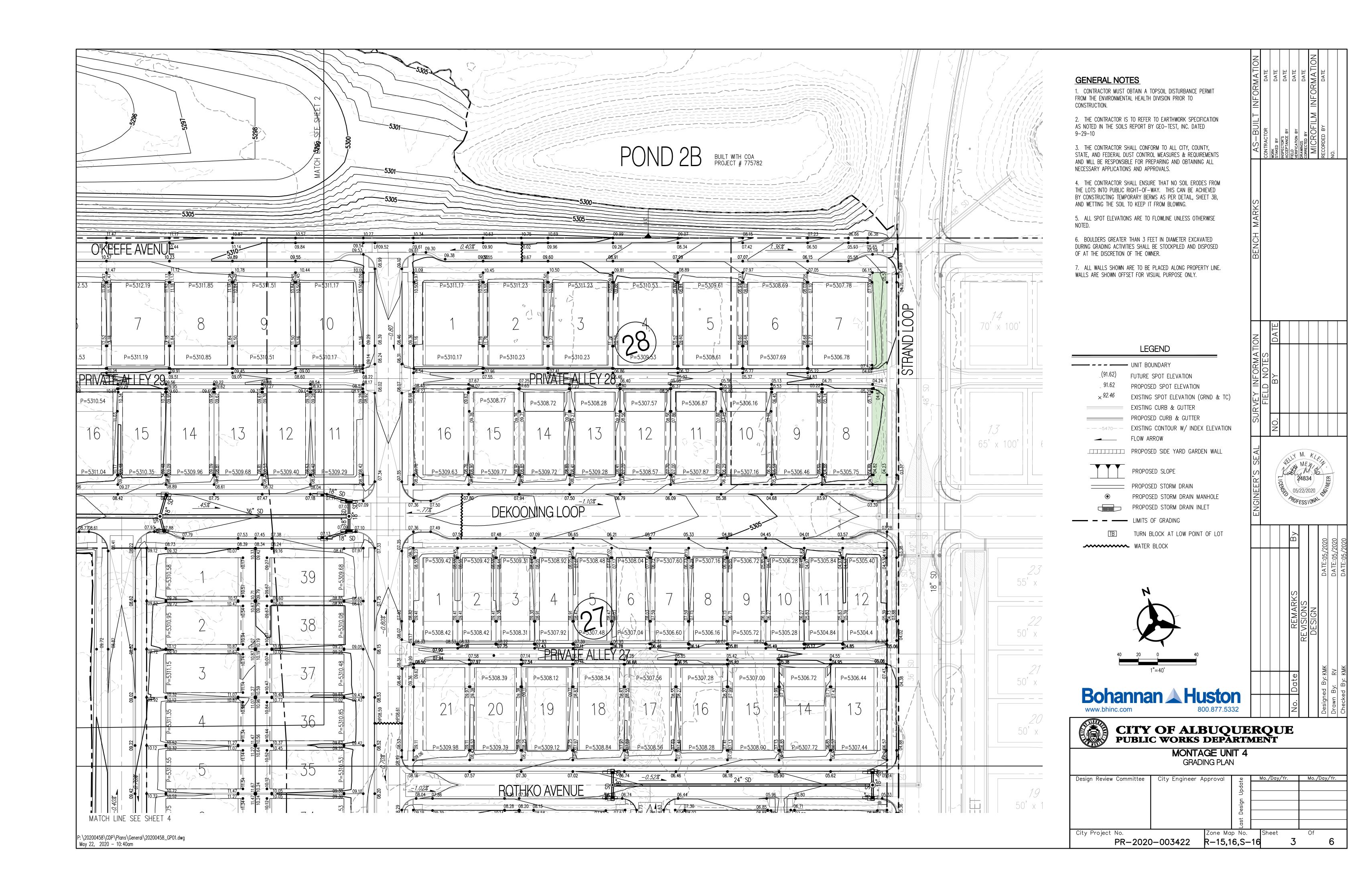


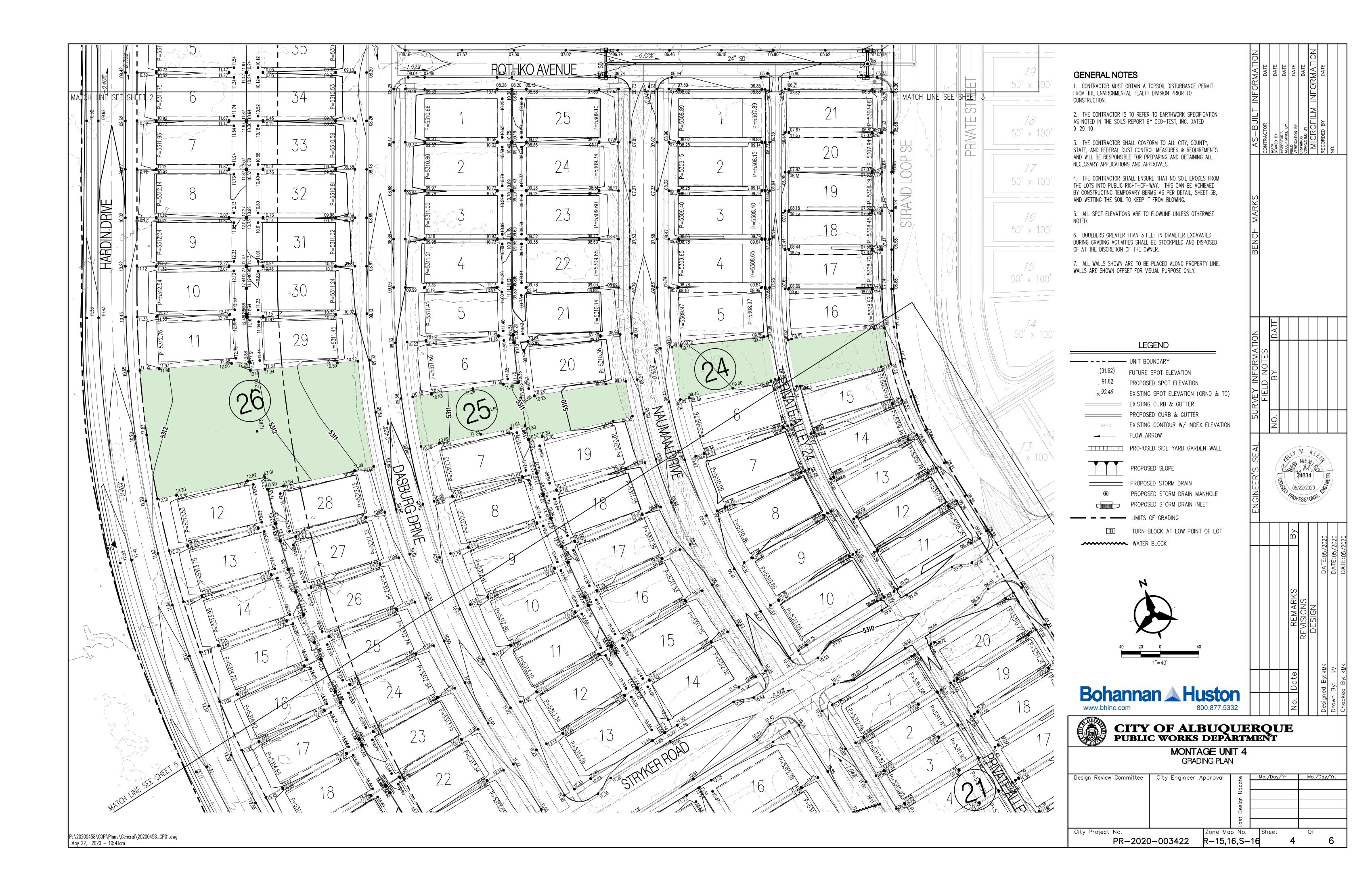


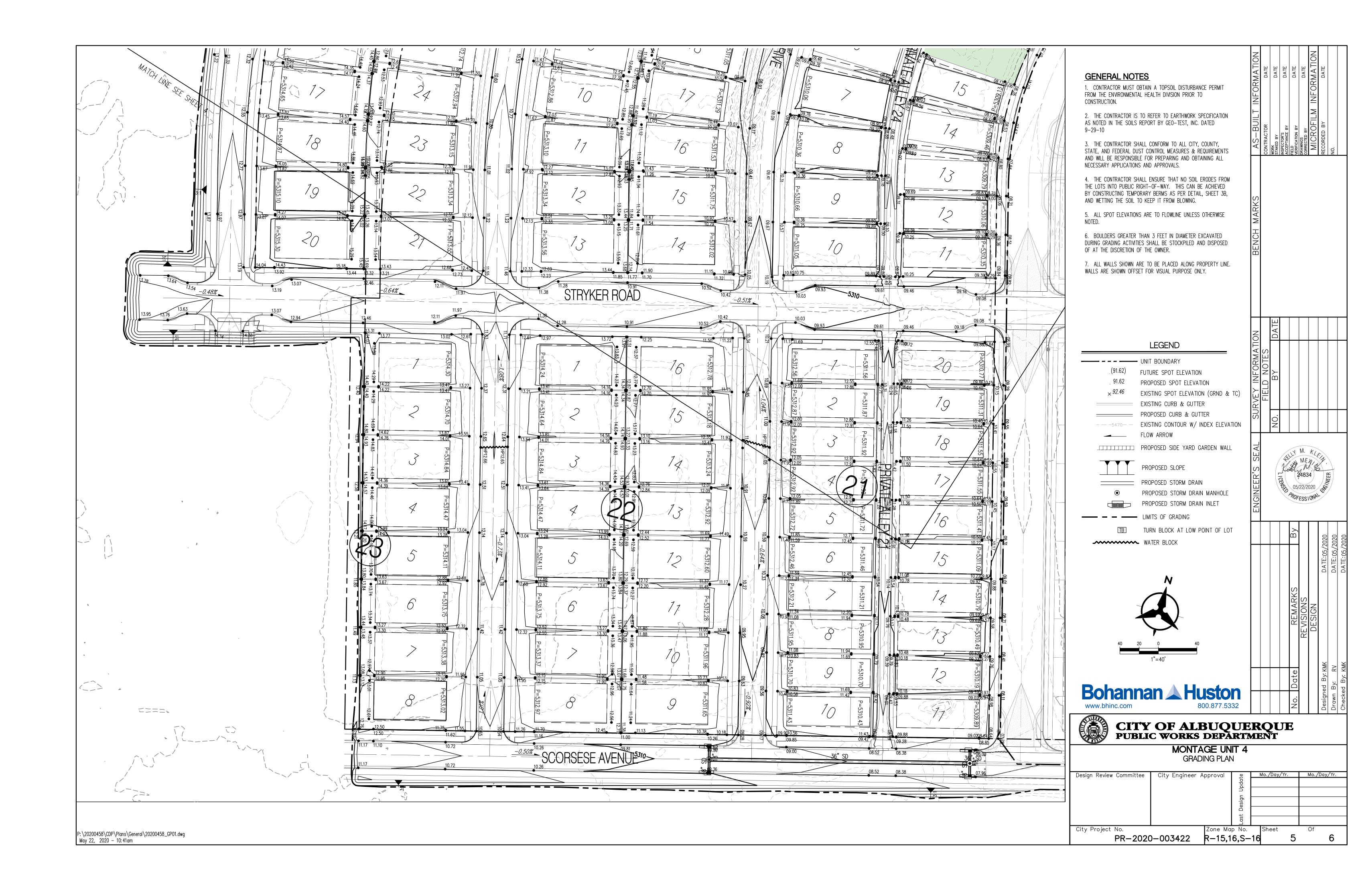
EXHIBIT 4 UNIT 4 GRADING PLAN

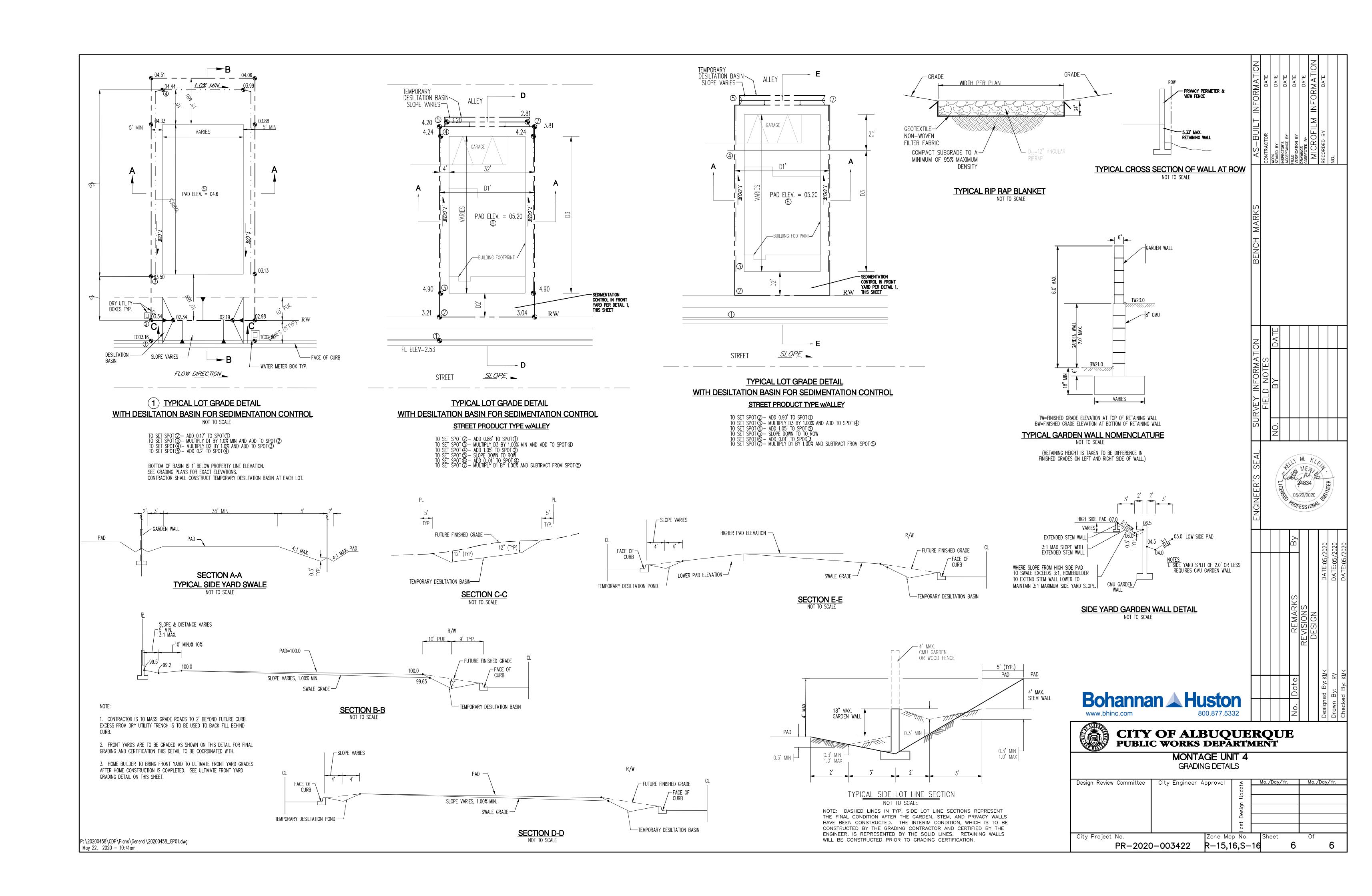












RE: Agent Authorization Letter - Subdivision Submittal Tract A-6-C-1 and Tract C Montage 4

DRB Chair - Jolene Wofley

City of Albuquerque 600 2nd St NW Albuquerque, NM 87102

Dear Ms. Wofley,

Please find this letter as Authorization for the DRB action of the Sketch Plat through Final Plat of a Major Subdivision Submittal for Mesa del Sol Tract A-6-C-1 Montage Unit 4 requesting DRB consideration for creating 196 lots from the existing 33.0880 Acre parcel to be represented by the following firm(s) and individuals:

Ravens Wing Consulting, LLC

CSI-Cartesian Surveys, Inc. Manny Barrera, PE

Will Plotner, Jr., PS

Others as designated Bohannan Huston, Inc. Michael Balaskovits, PE Consensus Planning, Inc

Yolanda Padilla Moyer, PE Jim Strozier, FAICP Kelly Klein, PE Chris Green, PLA, ASLA

Others as designated. Michael Voss, AICP

Feel free to contact me if you have any questions or concerns.

Respectfully,

Corazon del Mesa 4, LLC

9600 Tennyson St NE

Albuquerque, NM 871/22

Kelly Klein

From: Manny Barrera <mannybarrera@ravenswingconsulting.com>

Sent: Tuesday, February 25, 2020 1:43 PM

To: 4district6@gmail.com; paulsanchez7771@gmail.com **Subject:** DRB Pre Application Notice Neighborhood Meeting Notice

Attachments: Zone Atlas Pages .pdf

District 6 Coalition of Neighborhood Associations c/o – Paul Sanchez 400 Cardenas Dr NE Albuquerque, NM 87108

RE: Neighborhood Pre Application Notification for DRB Action Preliminary Plat – Mesa del Sol Montage Unit 4

Dear Neighbors:

This letter is notification that Ravens Wing Consulting and Bohanan Huston Inc. are preparing an application for a Major Subdivision of Land to be submitted to the Development Review Board (DRB) on behalf of Corazon Del Mesa 4, LLC.

The subject site is legally described as Tract A-6-C-1, Mesa Del Sol Innovation Park (approx. 33 acres). The site is generally located south of Stieglitz Avenue and west of Strand Loop. It is zoned PC and within the Mesa Del Sol Framework Plan. The applicant is proposing to subdivide the property into single family residential housing, creating approximately 194 lots (+/-).

A Vacation action of an unused PNM utility easement will be requested as part of the DRB actions.

As part of the IDO regulations, we are providing you an opportunity to discuss the application prior to submittal. Should you desire to request a meeting regarding this request, please do not hesitate to email me at mannybarrera@ravenswingconsulting.com or contact me by phone at 505-314-3346. Per the IDO, you have 15 days or until March 11, 2020 to request a meeting. If you do not want to schedule a meeting, please let me know so we can proceed with our applications.

Affected Neighborhood Associations and Homeowner Associations may request a Facilitated Meeting regarding this project by contacting the Office of Neighborhood Coordination (ONG) by email at ONC@cabq.gov or by phone at (505) 924-3914.

This notice is under the IDO procedures and a meeting is required before DRB submittal.

Respectfully,

MIL

Manny Barrera, PE



Kelly Klein

From: Carmona, Dalaina L. <dlcarmona@cabq.gov>

Sent: Friday, February 21, 2020 9:29 AM

To: mannybarrera@ravenswingconsulting.com
Subject: 2500 O'Keeffe Avenue SE Public Notice Inquiry

Attachments: Montage 4 Zone Atlas - and Plat .pdf

Dear Applicant,

See list of associations below regarding your Public Notice Inquiry. In addition, we have included web links below that will provide you with additional details about the new Integrated Development Ordinance (IDO) requirements. The web links also include notification templates that you may utilize when contacting each association. Thank you.

Association	First	Last	Email	Address	City	State	Zip	Mobile	I
Name	Name	Name		Line 1	Ĵ		1	Phone	
District 6	Dominic	Peralta	4district6@gmail.com	3800	Albuquerque	NM	87108		Ī
Coalition of				Lead					
Neighborhood				Avenue					
Associations				SE					
District 6	Paul	Sanchez	paulsanchez7771@gmail.com	400	Albuquerque	NM	87108	5059779598	Ī
Coalition of				Cardenas					
Neighborhood				Drive					
Associations				NE					

IDO – Public Notice Requirements & Template: https://www.cabq.gov/planning/urban-design-development/public-notice

IDO – Neighborhood Meeting Requirements & Template: https://www.cabq.gov/planning/urban-design-development/neighborhood-meeting-requirement-in-the-integrated-development-ordinance

IDO - Administration & Enforcement section: http://documents.cabq.gov/planning/IDO/IDO-Effective-2018-05-17-Part6.pdf

Thanks,



Dalaina L. Carmona

Senior Administrative Assistant
Office of Neighborhood Coordination
Council Services Department
1 Civic Plaza NW, Suite 9087, 9th Floor
Albuquerque, NM 87102

505-768-3334

dlcarmona@cabq.gov or ONC@cabq.gov Website: www.cabq.gov/neighborhoods



Confidentiality Notice: This e-mail, including all attachments is for the sole use of the intended recipient(s) and may contain confidential and privileged information. Any unauthorized review, use, disclosure or distribution is prohibited unless specifically provided under the New Mexico Inspection of Public Records Act. If you are not the intended recipient, please contact the sender and destroy all copies of this message.

From: webmaster=cabq.gov@mailgun.org [mailto:webmaster=cabq.gov@mailgun.org] On Behalf Of ISD WebMaster

Sent: Thursday, February 20, 2020 11:22 AM

To: Office of Neighborhood Coordination <mannybarrera@ravenswingconsulting.com>

Cc: Office of Neighborhood Coordination <onc@cabq.gov> **Subject:** Neighborhood Meeting Inquiry Sheet Submission

Neighborhood Meeting Inquiry For:

Development Review Board

If you selected "Other" in the question above, please describe what you are seeking a Neighborhood Meeting Inquiry for below:

Contact Name

Manny Barrera

Telephone Number

505-314-3346

Email Address

mannybarrera@ravenswingconsulting.com

Company Name

Ravens Wing Consulting, LLC

Company Address

3102 10th St NW

City

Albuquerque

State

NM

ZIP

87107

Legal description of the subject site for this project:

Bulk Land Plat Tract A-6-C-1

Physical address of subject site:

2500 O'Keeffe Avenue Albuquerque, NM 87106

Subject site cross streets:

Strand and DeKooning

Other subject site identifiers:

Mesa del Sol Montage Unit 3B

This site is located on the following zone atlas page:

S-16, R-15 & R-16

This message has been analyzed by Deep Discovery Email Inspector.



City of Albuquerque P.O. Box 1293 Albuquerque, New Mexico 87103

Planning Department

Martin J. Chave	z, Mayor	Richard Dineen, Director		
Interoffice Memo	orandum			
April 14, 2008				
Subject: Albue	querque Archaeological Ordi	nance—Compliance Documentation		
Project Number(s): Case Number(s):				
Agent: Applicant: Legal Description:		and NE ¼ and SW ¼ and SE ¼ of n 27, Township 9 North, Range 3 East		
Acreage: Zone Atlas Page:	416 acres Q-16/R-16/S-16			
CERTIFICATE OF	F APPROVAL: YesX_ F NO EFFECT: Yes N			
Proposed Innovatio	III Cultural Resource Surven n Park and First Neighborho alillo County, NM by Quirolo	y of 168.4 Hectares (416 Acres) for the od Developments on Mesa del Sol, b, Brown, and Brown (Kenneth Brown		
CERTIFICATE OF sites in project area)	NO EFFECT IS ISSUED (re	f O-07-72 Section 4B(1) no significant		
SUBMITTED: Matthew Schmader, I Superintendent, Oper Acting City Archaeol	Space Division			



February 25, 2020

District 6 Coalition of Neighborhood Associations c/o – Paul Sanchez 400 Cardenas Dr NE Albuquerque, NM 87108

RE: Neighborhood Pre Application Notification for DRB Action Preliminary Plat – Mesa del Sol Montage Unit 4

Dear Neighbors:

This letter is notification that Ravens Wing Consulting and Bohanan Huston Inc. are preparing an application for a Major Subdivision of Land to be submitted to the Development Review Board (DRB) on behalf of Corazon Del Mesa 4, LLC.

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This notice is under the new IDO procedures and a meeting is required before DRB submittal.

Respectfully,

Manny Barrera, PE

Ravens Wing Consulting, LLC



February 25, 2020

District 6 Coalition of Neighborhood Associations c/o – Dominic Peralta 3800 Lead Avenue SE Albuquerque, NM 87108

RE: Neighborhood Pre Application Notification for DRB Action Preliminary Plat – Mesa del Sol Montage Unit 4

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Respectfully,

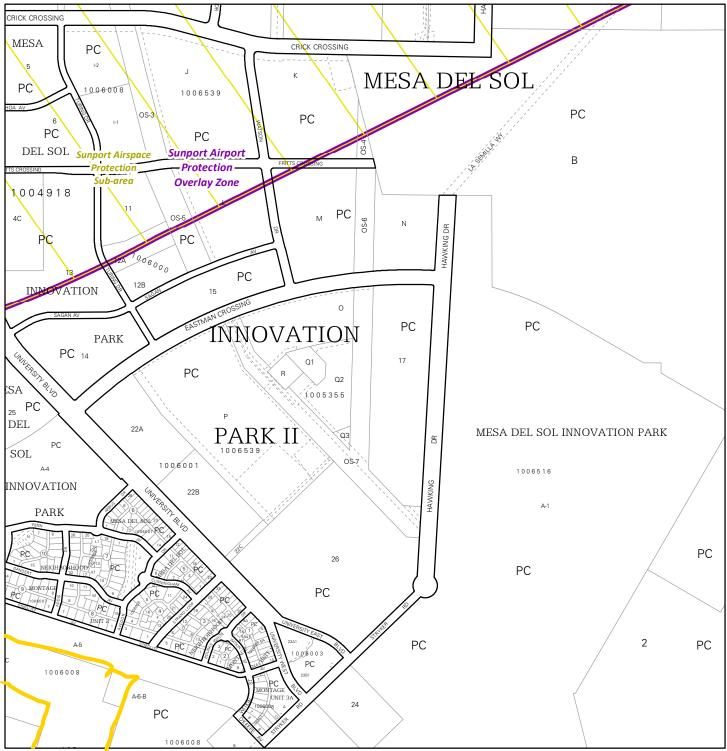
Manny Barrera, PE

Ravens Wing Consulting, LLC

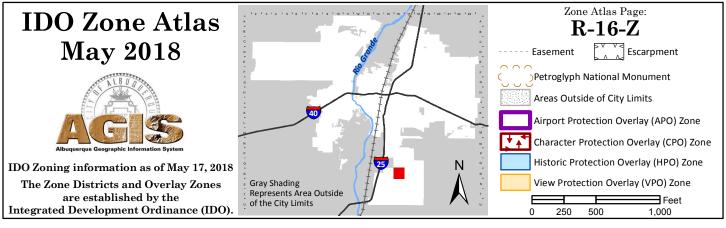
FORM S1: SUBDIVISION OF LAND - MAJOR

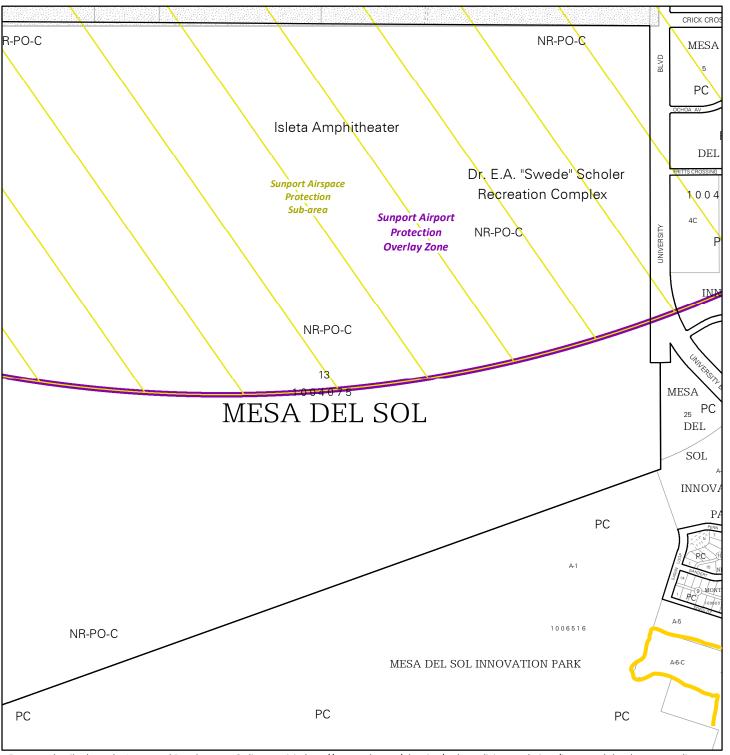
Please refer to the DRB public meeting schedule for meeting dates and deadlines. Your attendance is required.

>> INFORMATION REQUIRED FOR ALL MAJOR SUBDIVISION REQUESTS						
Interpreter Needed for Meeting? if yes, indicate language: X A Single PDF file of the complete application including all documents being submitted reprior to making a submittal. Zipped files or those over 9 MB cannot be delivered via emprovided on a CD. PDF shall be organized with the Development Review Application at the remaining documents in the order provided on this form. X Zone Atlas map with the entire site clearly outlined and labeled Letter of authorization from the property owner if application is submitted by an agent Sign Nosting Agreement	ail, in which case the PDF must be					
MAJOR SUBDIVISION PRELIMINARY PLAT MAJOR AMENDMENT TO PRELIMINARY PLAT Sites 5 acres or greater: Archeological Certificate in accordance with IDO Section 14-16-6-5(A) TIS Traffic Impact Study Form Form DRWS Drainage Report, Grading and Drainage Plan, and Water & Sewer Availability Statement submittal information Letter describing, explaining, and justifying the request per the criteria in IDO Section 14-16-6-6(J) Proof of Sketch Plat per IDO Section 14-16-6-6(J)(2)(b) Attended DRB on 3/04/2020 for Sketch Plat Required notices with content per IDO Section 14-16-6-4(K)(6) X Office of Neighborhood Coordination notice inquiry response X Copy of notification letter and proof of first class mailing X Proof of emailed notice to affected Neighborhood Association representatives X Buffer map and list of property owners within 100 feet (excluding public rights-of-way) provided by Planning Department or created by applicant, copy of notifying letter, and proof of first class mailing Preliminary Plat including the Grading Plan with property owner's and City Surveyor's signatures on the plat (7 copies, 24" x 36" folded) Sidewalk Exhibit and/or cross sections of proposed streets (3 copies, 11" by 17" maximum) Site sketch with measurements showing structures, parking, building setbacks, adjacent rights-of-way and street improvements (to include sidewalk, curb & gutter with distance to property line noted) if there is any existing land use (7 copies, folded) MA Landfill disclosure statement on the plat per IDO Section 14-16-5-2(G) if site is within a designated landfill buffer zone Proposed Infrastructure List						
□ EXTENSION OF PRELIMINARY PLAT □ INFRASTRUCTURE LIST EXTENSION OR AN INFRASTRUCTURE IMPROVEMENTS AN For temporary sidewalk deferral extension, use Form V. □ Letter describing, explaining, and justifying the request per IDO Sections 14-16-6-4(W) □ Copy of the Official DRB Notice of Decision for any prior approvals □ Required notices with content per IDO Section 14-16-6-4(K)(6) □ Office of Neighborhood Coordination notice inquiry response □ Copy of notification letter and proof of first class mailing □ Proof of emailed notice to affected Neighborhood Association representatives □ Buffer map and list of property owners within 100 feet (excluding public rights-of-way created by applicant, copy of notifying letter, and proof of first class mailing □ Preliminary Plat or site plan reduced to 8.5" x 11" □ Copy of DRB approved infrastructure list	and 14-16-6-6(J)					
I, the applicant or agent, acknowledge that if any required information is not submitted with the scheduled for a public meeting, if required, or otherwise processed until it is complete.						
Signature:	Date: 05/22/2020					
Printed Name: Kelly Klein, PE	☐ Applicant or 崔 Agent					
FOR OFFICIAL USE ONLY						
Case Numbers: Project Number: Staff Signature:						

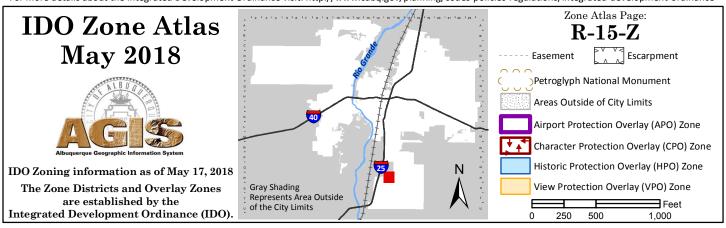


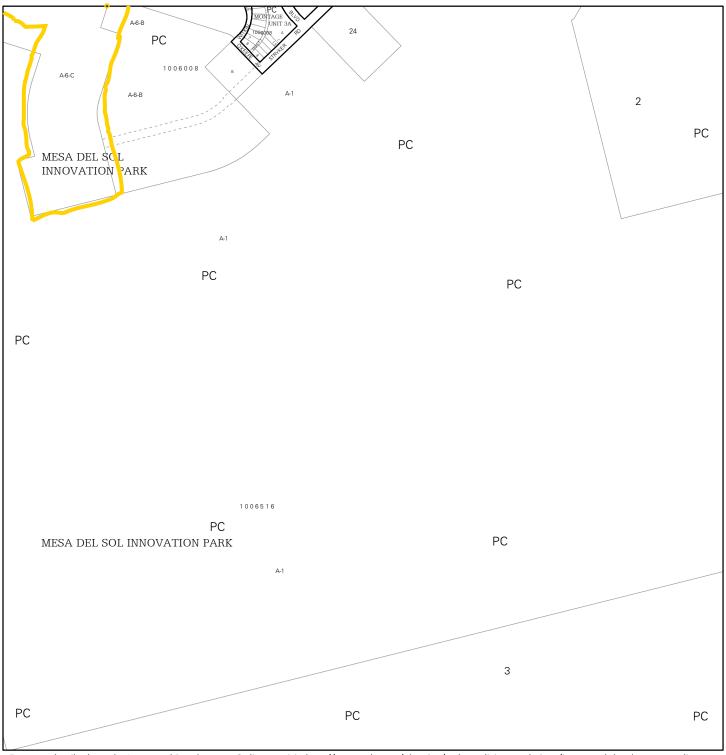
For more details about the Integrated Development Ordinance visit: http://www.cabq.gov/planning/codes-policies-regulations/integrated-development-ordinance



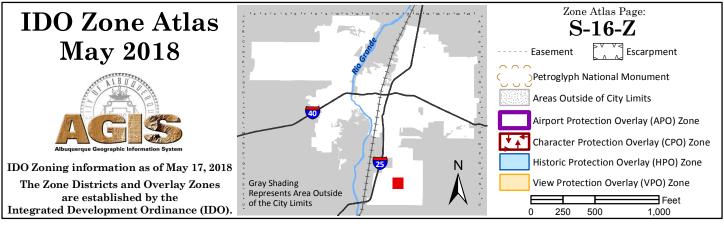


For more details about the Integrated Development Ordinance visit: http://www.cabq.gov/planning/codes-policies-regulations/integrated-development-ordinance





For more details about the Integrated Development Ordinance visit: http://www.cabq.gov/planning/codes-policies-regulations/integrated-development-ordinance



Current DRC	
Project No.	

Figure 12

INFRASTRUCTURE LIST

EXHIBIT 'A'

TO SUBDIVISION IMPROVEMENTS AGREEMENT DEVELOPMENT REVIEW BOARD (D.R.B.) REQUIRED INFRASTRUCTURE LIST

Date Submitted:	May 8, 2020
Date Site Plan for Bldg Permit Approv	
Date Site Plan for Sub. Approved:	
Date Preliminary Plat Approved:	
Date Preliminary Plat Expires:	
, , , , , , , , , , , , , , , , , , ,	
DRB Project No.	

MESA DEL SOL NEIGHBORHOOD, MONTAGE UNIT 4 (REPLAT OF TRACT A-6-B, MESA DEL SOL INNOVATION PARK AND TRACT B, MONTAGE UNIT 4)

Following is a summary of PUBLIC/PRIVATE Infrastructure required to be constructed or financially guaranteed for the above development. This Listing is not necessarily a complete listing. During the SIA process and/or in the review of the construction drawings, if the DRC Chair determines that appurtenant items and/or unforeseen items have not been included in the infrastructure listing, the DRC Chair may include those items in the listing and related financial guarantee. Likewise, if the DRC Chair determines that appurtenant or non-essential items can be deleted from the listing, those items may be deleted as well as the related portions of the financial guarantees. All such revisions require approval by the DRC Chair, the User Department and agent/owner. If such approvals are obtained, these revisions to the listing will be incorporated administratively. In addition, any unforeseen items which arise during construction which which are necessary to complete the project and which normally are the Subdivider's responsibility will be required as a condition of project acceptance and close out by the City.

SIA Sequence #	COA DRC Project #	Size	Type of Improvement	Location	From	То	Private Inspector	City Inspector	City Cnst Engineer
		PUBLIC ROADWA	Y IMPROVEMENTS						
		48' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON BOTH SIDES*	STRYKER RD	FUTURE	STRAND LOOP	/	/	/
		46' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON BOTH SIDES*	DEKOONING AVE	FUTURE	STRAND LOOP	/	/	/
		46' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON WEST SIDE ONLY*	SAGAN LOOP	DEKOONING AVE	STIEGLITZ AVE	/	/	/
		19' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON SOUTH SIDE ONLY*	O'KEEFE AVE	SAGAN LOOP	STRAND LOOP	/		/
		28' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON BOTH SIDES*	HARDIN DRIVE	STRYKER RD	DEKOONING AVE	/	/	/
		28' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON BOTH SIDES*	DASBURG DRIVE	SCORSESE AVE	O'KEEFE AVE	/	/	/
		28' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON BOTH SIDES*	ROTHKO	DASBURG DRIVE	STRAND LOOP	/	/	/
		28' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON BOTH SIDES*	SCORSESE AVE	BLOCK 23	STRAND LOOP	/		/
		28' F-F	RESIDENTIAL PAVING W/ PCC CURB & GUTTER & PCC 5' WIDE SIDEWALK ON BOTH SIDES*	NAUMAN DRIVE	SCORSESE AVE	ROTHKO	/		/
			EETLIGHTS; SIDEWALKS DEFERRED PER I BE CONSTRUCTED.	EXHIBIT; PAVEMENT WID	THS ARE TYPICAL WIDTHS A	AND EXCLUDE AREAS WHERE			

SIA Sequence #	COA DRC Project #	Size	Type of Improvement	Location	From	То	Private Inspector	City Inspector	City Cnst Engineer
		PRIVATE ROADWAY	IMPROVEMENTS			[
		12' PRIVATE ALLEY	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND 3.4' GRAVEL STRIP OUTSIDE CURB BOTH SIDES	BLOCK 30	SAGAN LOOP	DASBURG DRIVE	/	/	/
		12' PRIVATE ALLEY	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND 3.4' GRAVEL STRIP OUTSIDE CURB BOTH SIDES	BLOCK 29	DASBURG DRIVE	STRAND LOOP	/		
		12' PRIVATE ALLEY	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND 3.4' GRAVEL STRIP OUTSIDE CURB BOTH SIDES	BLOCK 27	DASBURG DRIVE	STRAND LOOP	/	/	/
		12' PRIVATE ALLEY	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND 3.4' GRAVEL STRIP OUTSIDE CURB BOTH SIDES	BLOCK 24	STRYKER RD	ROTHKO	/		
		12' PRIVATE ALLEY	RESIDENTIAL PAVING W/ PCC CURB & GUTTER AND 3.4' GRAVEL STRIP OUTSIDE CURB BOTH SIDES	BLOCK 21	SCORSESE AVE	STRYKER RD	/		/
							/		/
							/		

SIA Sequence #	COA DRC Project #	Size	Type of Improvement	Location	From	То	Private Inspector	City Inspector	City Cnst Engineer	
	PUBLIC WATERLINE IMPROVEMENTS									
		12" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	STRYKER RD	FUTURE	STRAND LOOP	/	/	/	
		6" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	DEKOONING AVE	FUTURE	STRAND LOOP	/	/	/	
		6" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	SAGAN LOOP	DEKOONING AVE	STIEGLITZ AVE	/	/		
		6" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	O'KEEFE AVE	SAGAN LOOP	STRAND LOOP	/	/		
		6" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	HARDIN DRIVE	STRYKER RD	DEKOONING AVE	/	/		
		6" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	DASBURG DRIVE	SCORSESE AVE	O'KEEFE AVE	/	/		
		6" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	ROTHKO	DASBURG DRIVE	STRAND LOOP	/	/	/	
		6" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	SCORSESE AVE	BLOCK 23	STRAND LOOP	/	/		
		6" DIA	WATERLINE W/ NEC. VALVES FH'S, MJ'S & RJ'S	NAUMAN DRIVE	SCORSESE AVE	ROTHKO	/			
							/	/		
							/	/		
		_								

SIA Sequence #	COA DRC Project #	Size	Type of Improvement	Location	From	То	Private Inspector	City Inspector	City Cnst Engineer		
	PUBLIC SANITARY SEWER IMPROVEMENTS										
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	STRYKER RD	DASBURG DRIVE	STRAND LOOP	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	DEKOONING AVE	SAGAN LOOP	STRAND LOOP	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	O'KEEFE AVE	LOT 19 (BLOCK 30)	STRAND LOOP	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	HARDIN DRIVE	LOT 20 (BLOCK 26)	DEKOONING AVE	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	DASBURG DRIVE	STRYKER RD	SCORSESE AVE	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	DASBURG DRIVE	LOT 13 (BLOCK 25)	DEKOONING AVE	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	ROTHKO AVENUE	DASBURG DRIVE	STRAND LOOP	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	SCORSESE AVE	BLOCK 23	STRAND LOOP	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	NAUMAN DRIVE	LOT 10 (BLOCK 24)	ROTHKO	/	/	/		
		8" DIA	SANITARY SEWER W/ NEC. MH'S & SERVICES	NAUMAN DRIVE	STRYKER RD	SCORSESE AVE	/	/			
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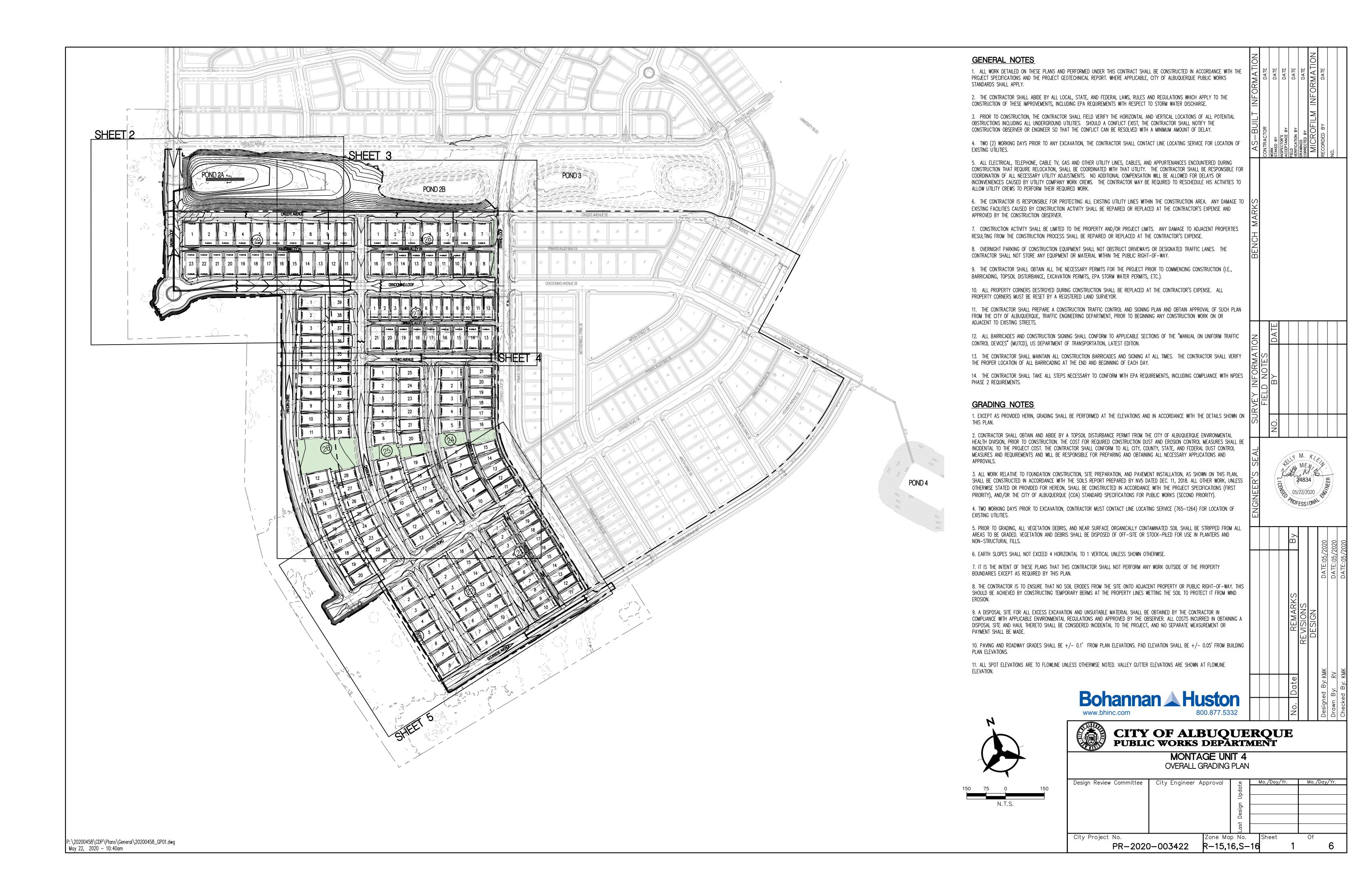
SIA Sequence #	COA DRC Project #	Size	Type of Improvement	Location	From	То	Private Inspector	City Inspector	City Cnst Engineer
		PUBLIC STORM DR	AIN IMPROVEMENTS						
		18"-42" DIA	RCP W/ NEC. MH'S, LATERALS & INLETS	SAGAN LOOP	DEKOONING AVE	160' N OF O'KEEFE AVE	/	/	- /
		18"-42" DIA	RCP W/ NEC. MH'S, LATERALS & INLETS	DEKOONING AVE	SAGAN LOOP	DASBURG DRIVE	/	/	
		18"-24" DIA	RCP W/ NEC. MH'S, LATERALS & INLETS	ROTHKO AVENUE	NAUMAN DRIVE	STRAND LOOP	/	/	
		18"-36" DIA	RCP W/ NEC. MH'S, LATERALS & INLETS	SCORSESE AVE	STRAND LOOP	50' WEST OF STRAND LP	/	/	
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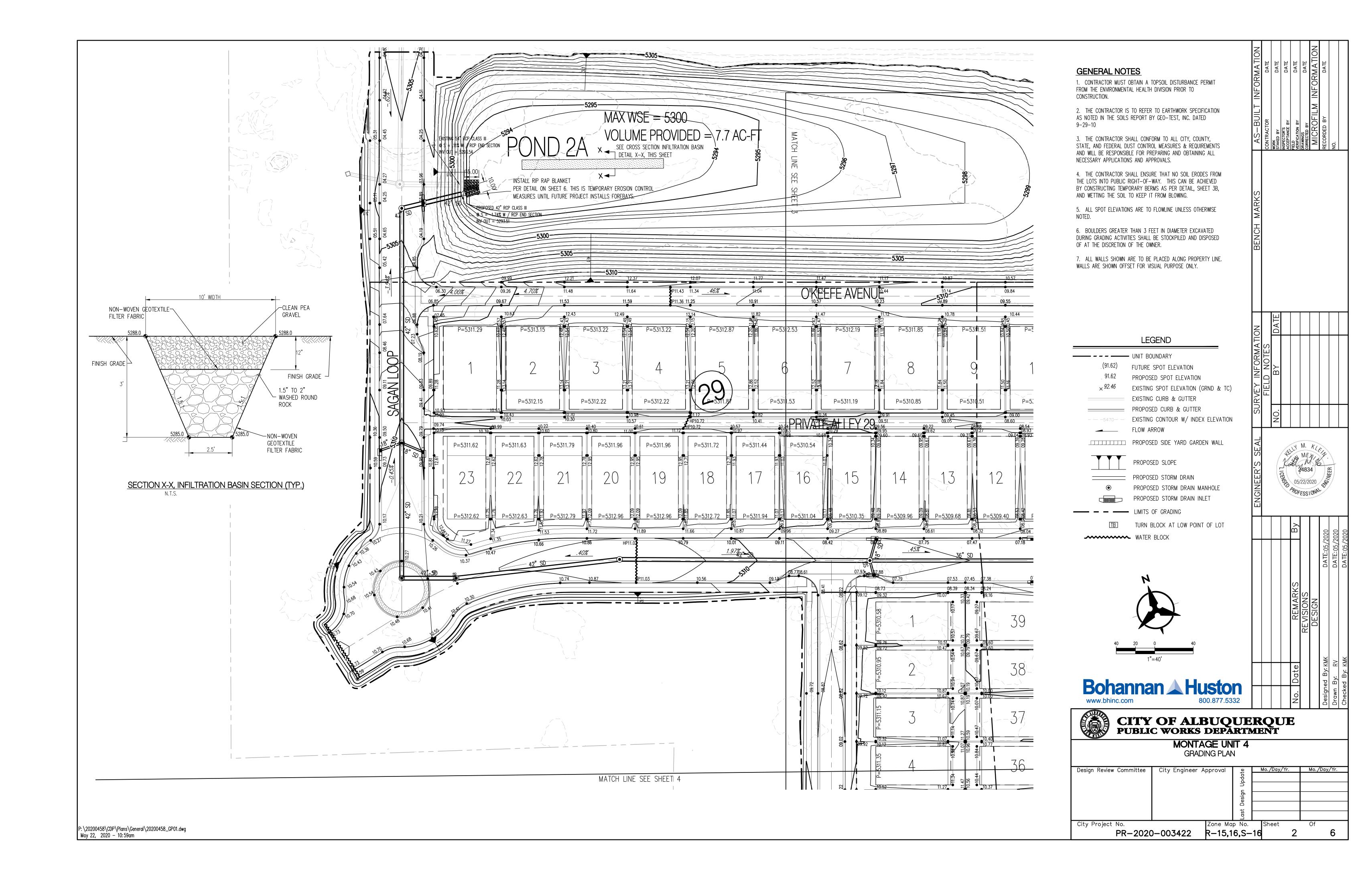
SIA Sequence #	COA DRC Project #	Size	Type of Improvement	Location	From	То	Private Inspector	City Inspector	City Cnst Engineer
	AGENT/OWNER				DEVELOPMENT REVIEW B	BOARD MEMBER APPRO	VALS		
KELLY KLEIN		5/15/2020							
PREPARED BY: P		DATE	DRE	3 CHAIR	DATE		PARKS & RECREATION		DATE
BOHANNAN HUST FIRM:	ON, INC.		TRANSPORTATI	ION DEVELOPMENT	DATE		AMAFCA		DATE
SIGNATURE	SIGNATURE				DATE		CODE ENFORCEMENT		DATE
	LOWED TO CONSTR WITHOUT A DRB EXT								
			CITY E	ENGINEER	DATE				DATE
				DESIGN REVIEW C	OMMITTEE REVISIONS				
REVIS	SION	DATE	DRC	CHAIR		USER DEPARTMENT		AGENT/OWNE	R

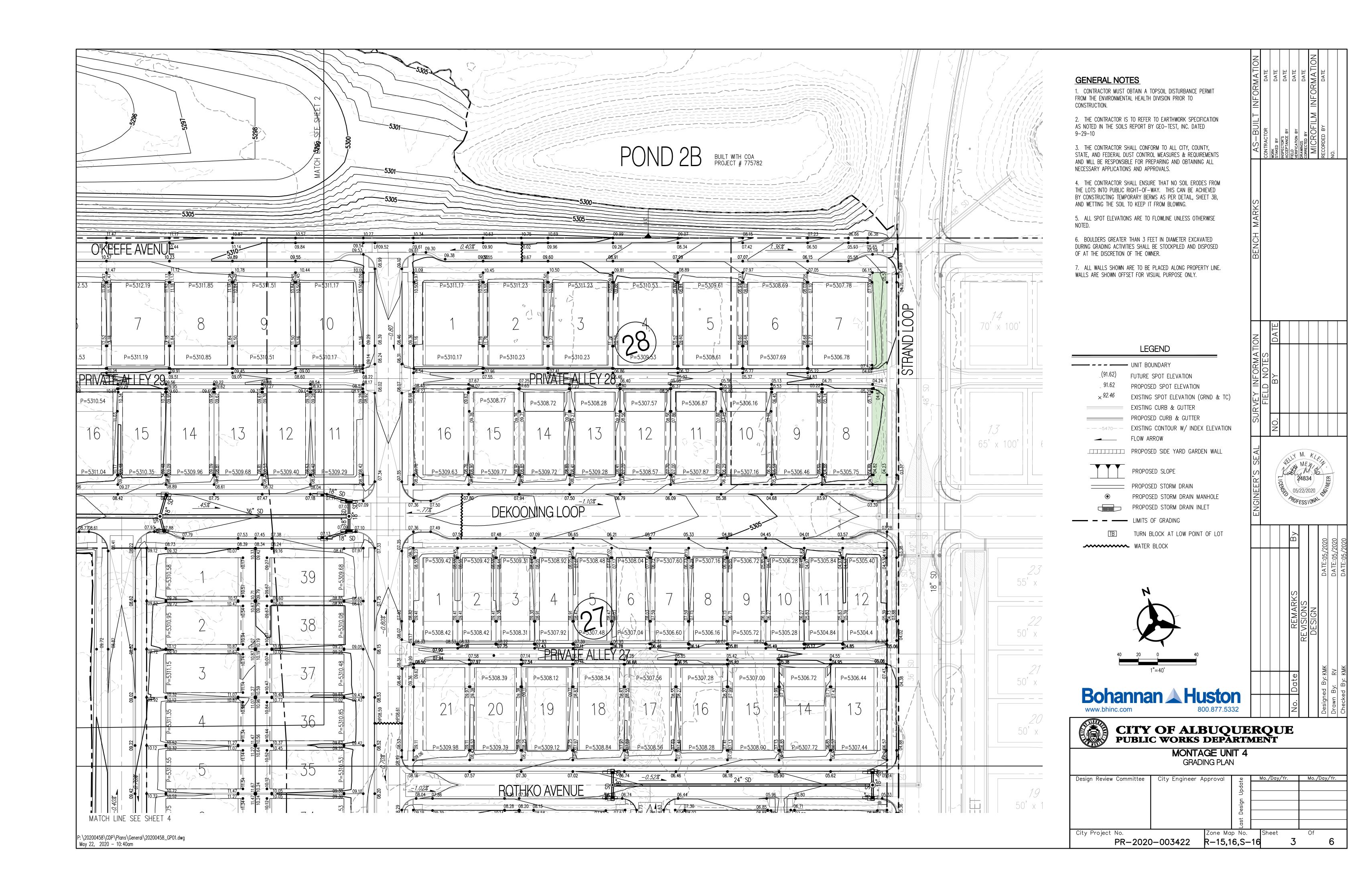


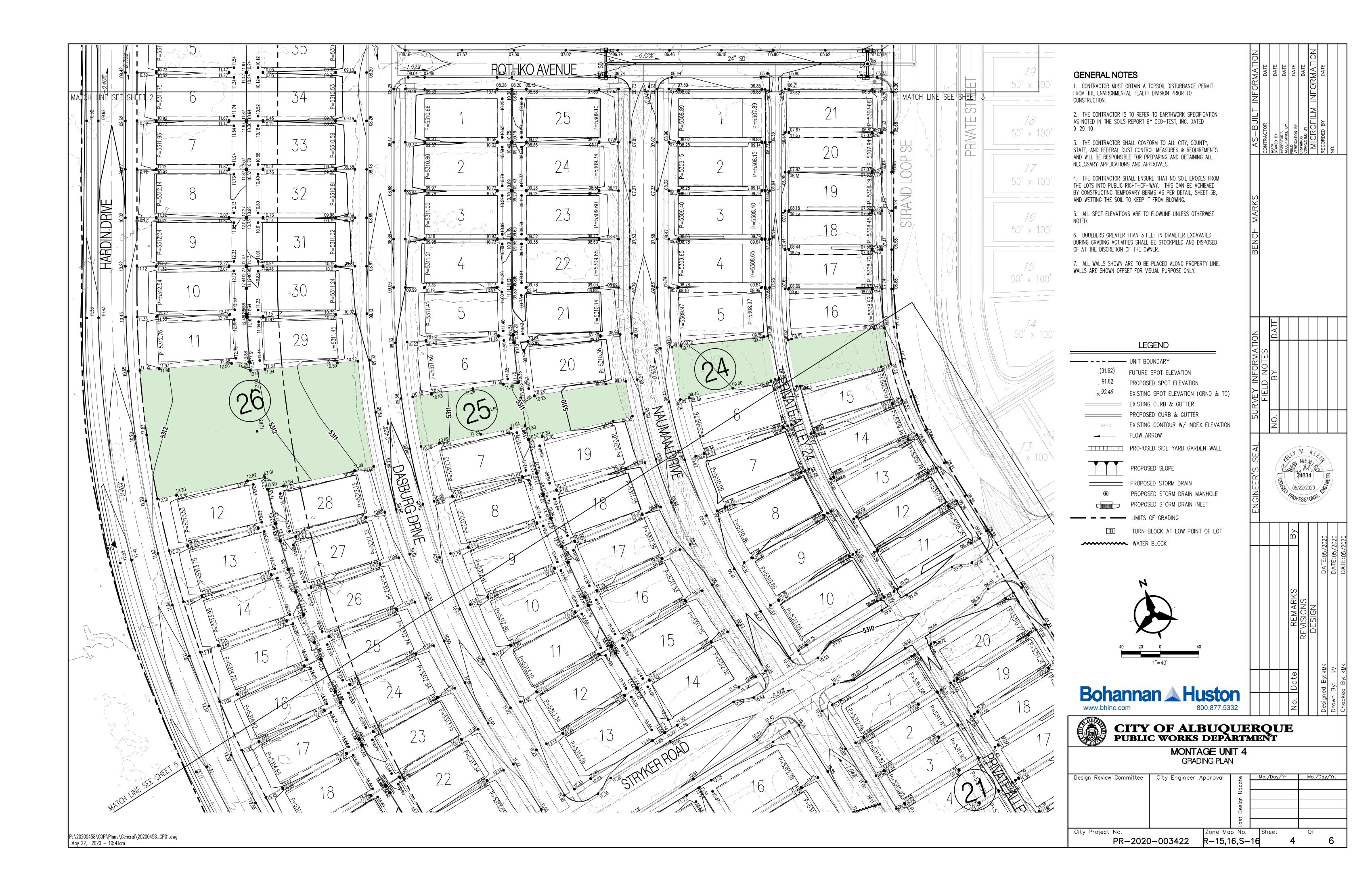
U.S. Postal Service™ CERTIFIED MAIL® RECEIPT **F471** Domestic Mail Only For delivery information, visit our website at www.usps.com®. ALBURUERUE NI 87108 M Certified Mail Fee \$3.55 0110 E, NM 20 17 \$0.00 Extra Services & Fees (check box, add fee as apprend Return Receipt (hardcopy) \$0.00 Postmark ги Return Receipt (electronic) FEB 2 5 Hora 20 \$0.00 Certified Mail Restricted Delivery \$_ Adult Signature Required \$ \$0.00 Adult Signature Restricted Delivery \$ 마 Postage \$0.55 02/25/2020 Total Postage and Fees 0 Sent To Street and Apt. No., or PO Box No. City, State, ZIP+4® PS Form 3800, April 2015 PSN 7530-02-000-9047

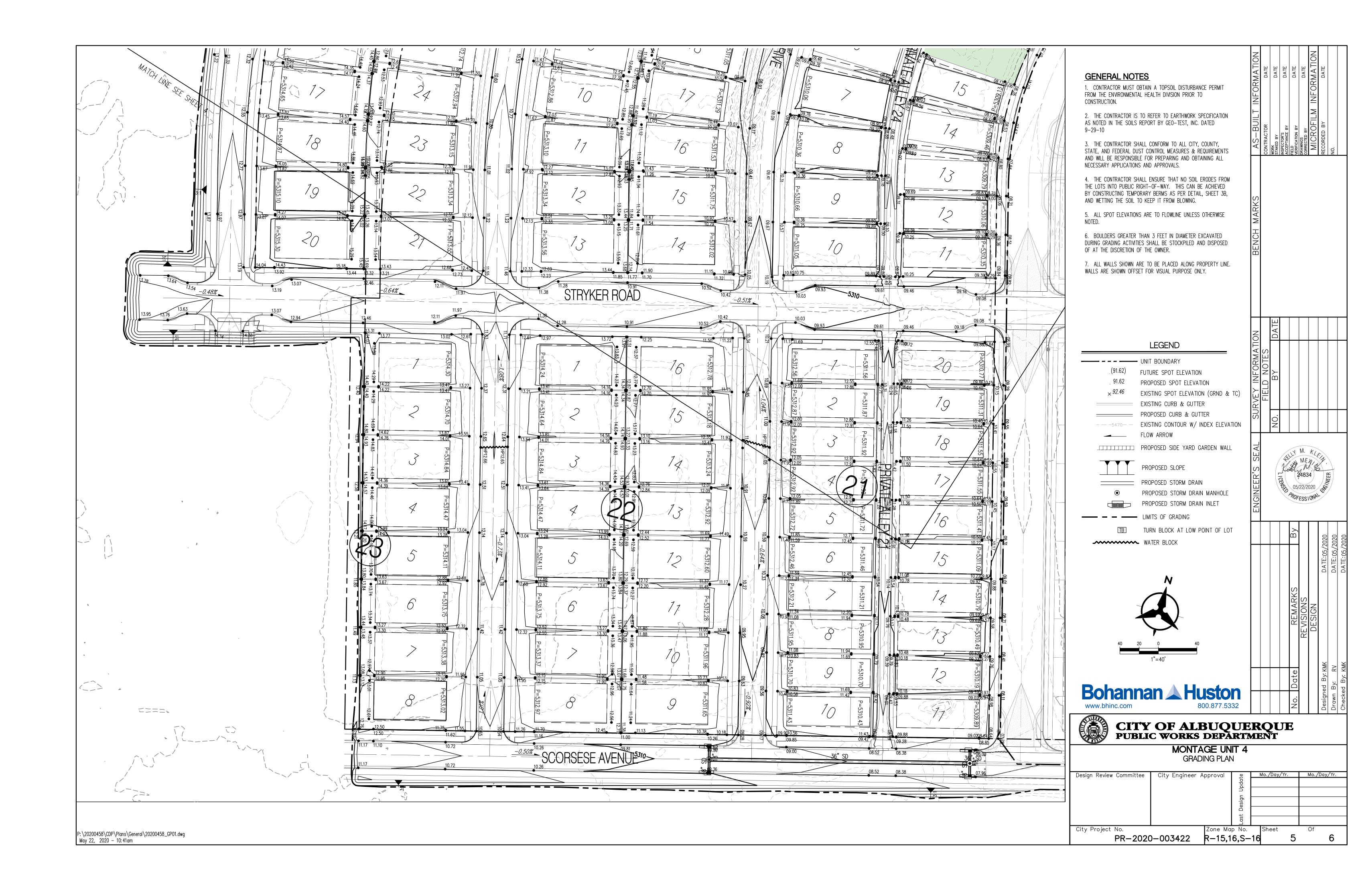
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	UPTOWN DR NE ACELAND DR NE IE, NM 87110-9998 10146-0110 300) 275-8777 572020 03:49 PM	Product Qty Unit	First-Class Mail® 1 \$0.55	Letter (Domestic) (ALBUQUERQUE, NM 87108) (Weight:0 Lb 0.60 0z) (Estimated Delivery Date) (Thursday 02/27/2020)	Certified (USPS Certified Mail #) (USPS Certified Mail #) (USPS 70191640000217316488)	(elec) First-Class Mail® 1 \$0.55	Letter (Domestic) (ALBUQUERQUE, NM 87108) (Weight:0 Lb 0.60 02) (Estimated Delivery Date) (Thursday 02/27/2020)	Certified (USPS Certified Mail #) (USPS Certified Mail #) (70191640000217316471) Return Receipt (alec)	Total:	Debit Card Remit'd (Card Name:MasterCard) (Account #:XXXXXXXXXXXXXX3011) (Approval #)

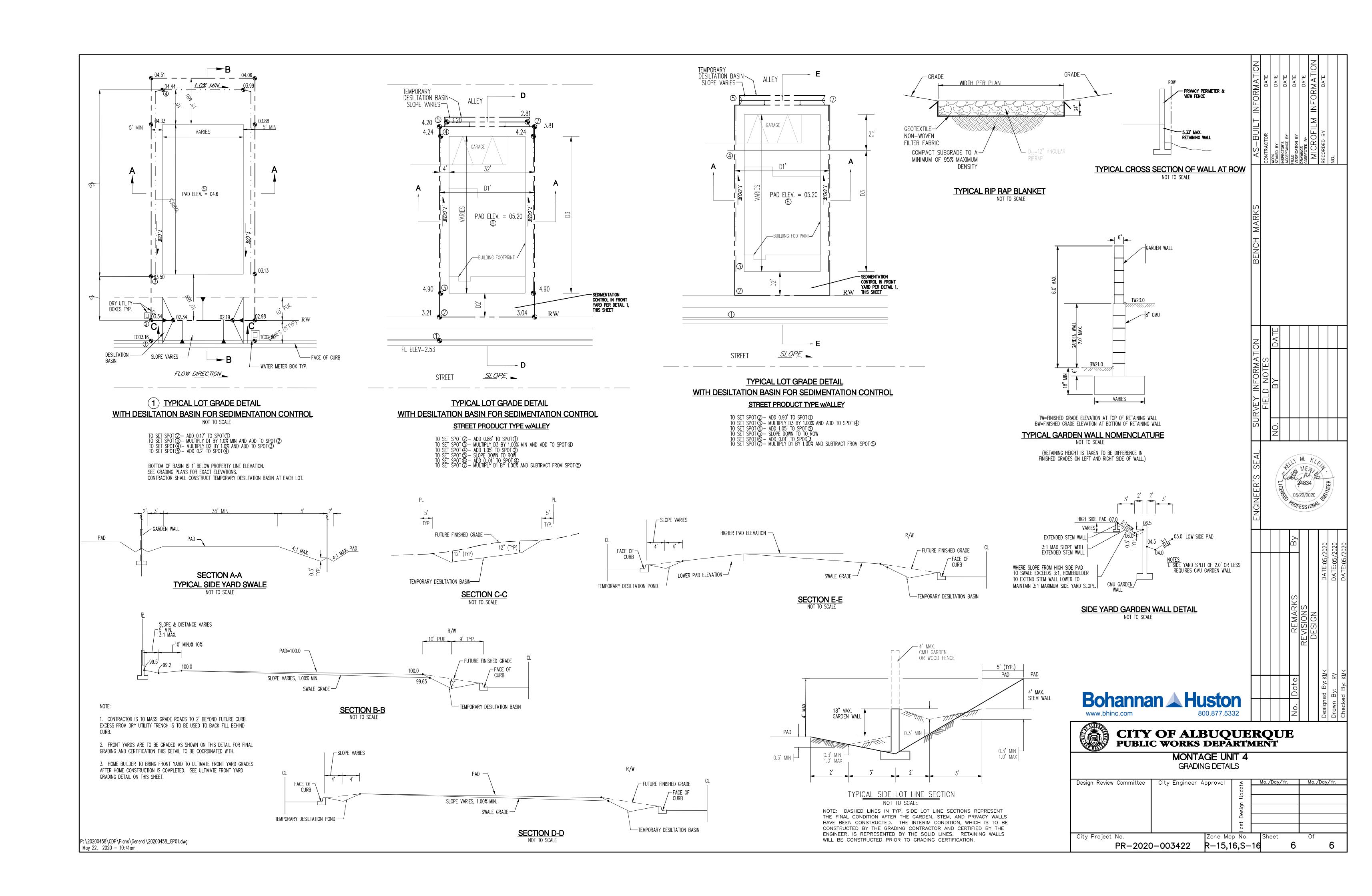


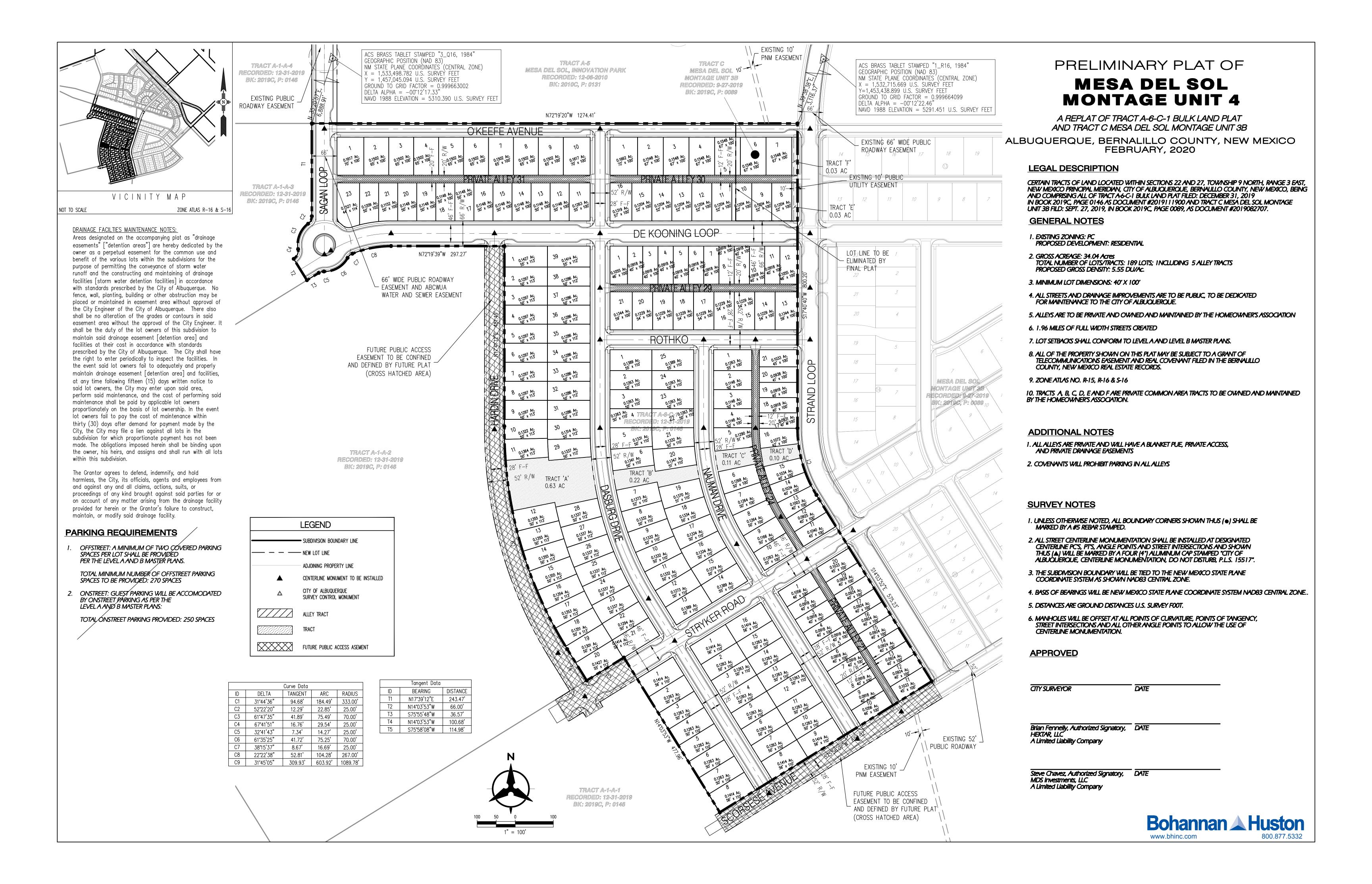


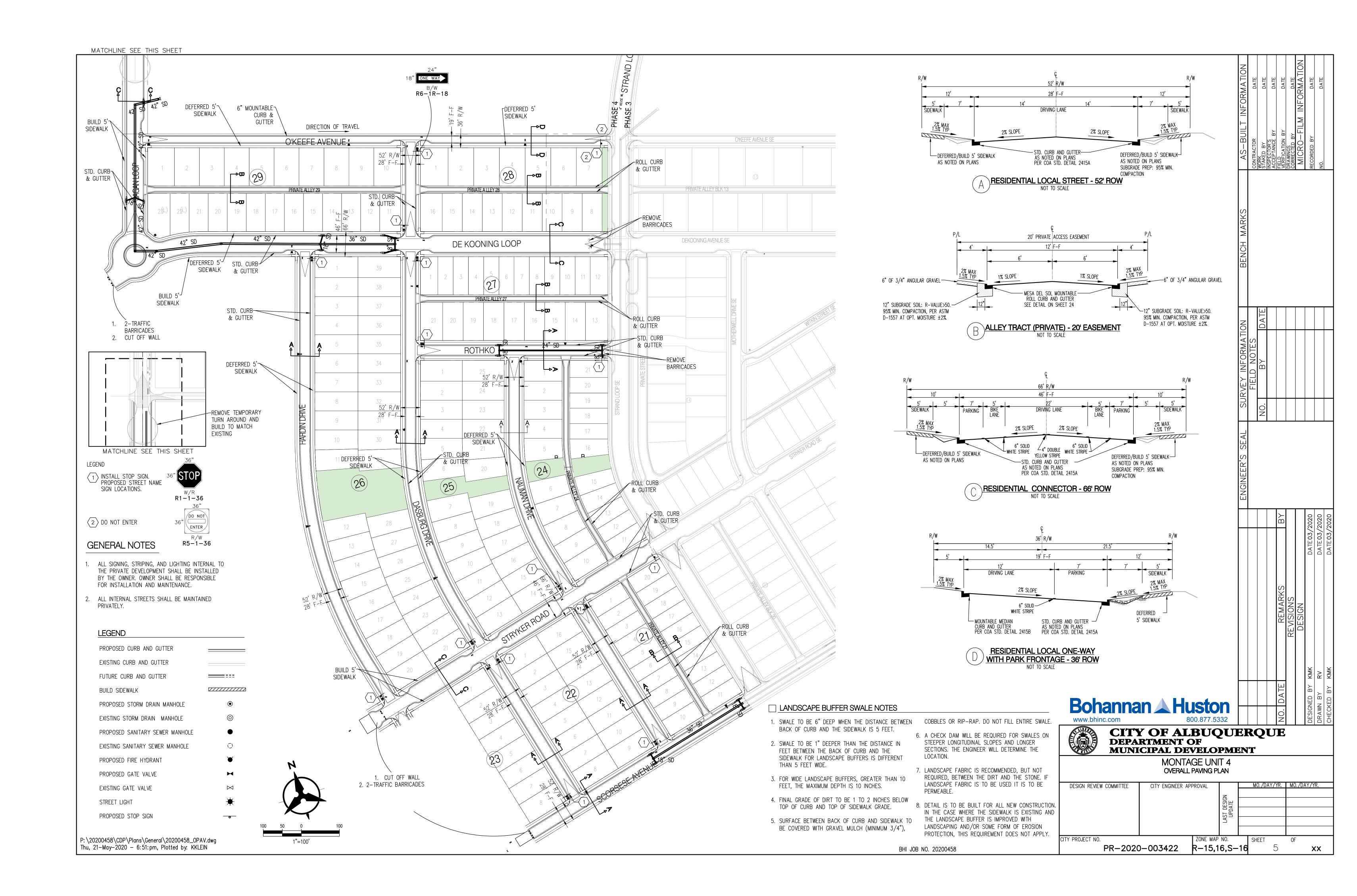


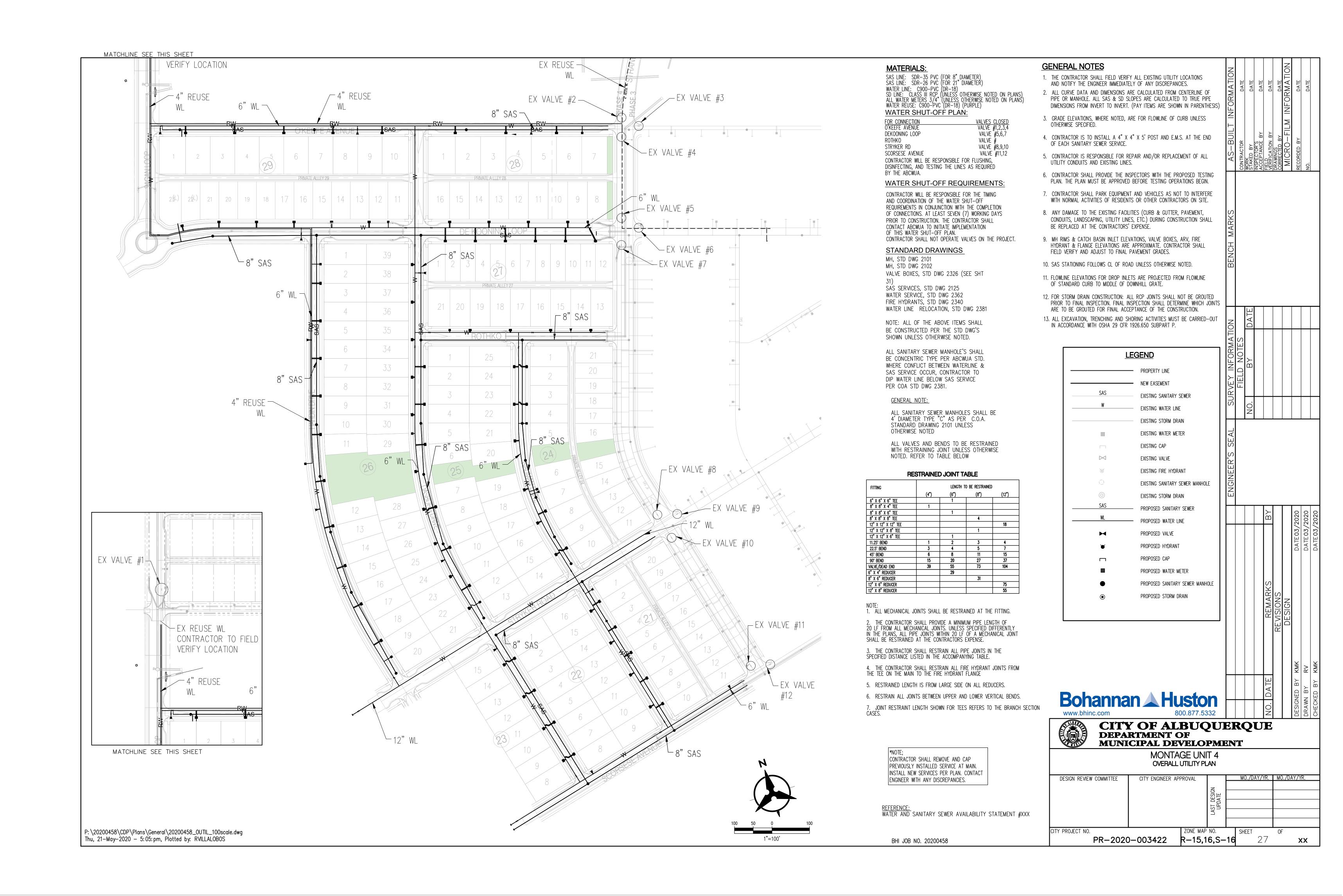






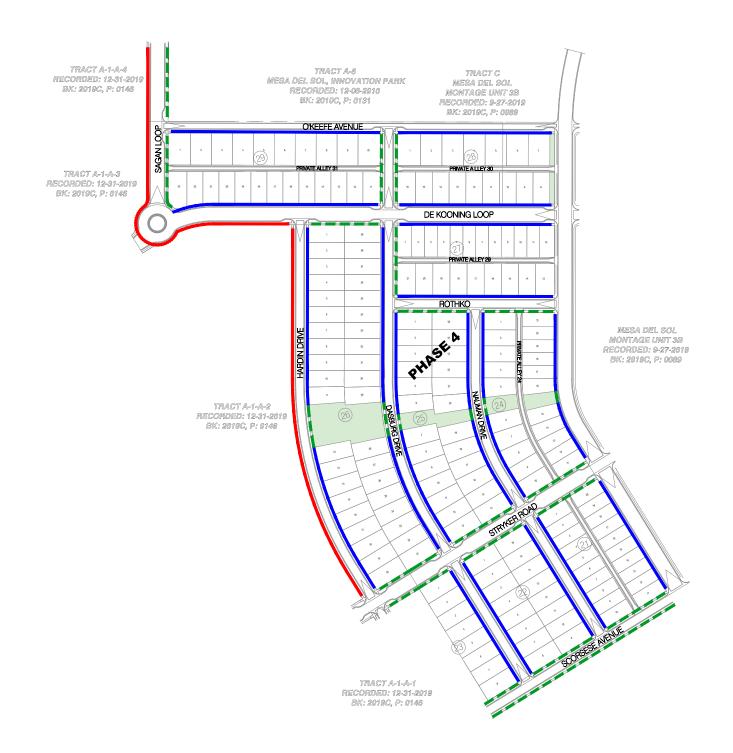






SIDEWALK EXHIBIT MESA DEL SOL MONTAGE UNIT 4

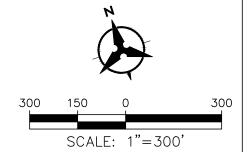
May, 2020



DEFERRED Sidewalks are to be built on a lot—by—lot basis as home construction is completed. The deferral is requested to reduce damage to sidewalks due to building construction activities.

<u>TO BE BUILT — SIDEWALK</u>

 <u>FUTURE SIDEWALK</u> — To be constructed as part of a future development





CITY OF ALBUQUERQUE

TRAFFIC IMPACT STUDY (TIS) FORM

APPLICANT: Corazon del Mesa 4, LLC DA	TE OF REQUEST: 5 / 20 / 2020 ZONE ATLAS PAGE(S): R-15-Z, R-16-Z and S-16-Z
CURRENT:	LEGAL DESCRIPTION:
ZONING PC	LOT OR TRACT #BLOCK #
PARCEL SIZE (AC/SQ. FT.) 34.04 acres	SUBDIVISION NAME MESA DEL SOL MONTAGE UNIT 4
REQUESTED CITY ACTION(S):	
ANNEXATION []	SITE DEVELOPMENT PLAN:
ZONE CHANGE []: FromTo	_ SUBDIVISION* [\sqrt{]} AMENDMENT []
SECTOR, AREA, FAC, COMP PLAN []	BUILDING PERMIT [] ACCESS PERMIT []
AMENDMENT (Map/Text) []	BUILDING PURPOSES [] OTHER [] *includes platting actions
PROPOSED DEVELOPMENT:	GENERAL DESCRIPTION OF ACTION:
NO CONSTRUCTION/DEVELOPMENT []	# OF UNITS: 189
NEW CONSTRUCTION [✓]	BUILDING SIZE: Single Family home(sq. ft.)
EXPANSION OF EXISTING DEVELOPMENT []	
determination. APPLICANT OR REPRESENTATIVE Kelly M. Klein, P.E.	DATE May 22, 2020
(To be signed upon completion of	processing by the Traffic Engineer)
Planning Department, Development & Building Services I $2^{\rm ND}$ Floor West, 600 $2^{\rm nd}$ St. NW, Plaza del Sol Building, City,	Division, Transportation Development Section - 87102, phone 924-3994
TRAFFIC IMPACT STUDY (TIS) REQUIRED: YES [] NO	[] BORDERLINE []
THRESHOLDS MET? YES [] NO [] MITIGATING R Notes:	EASONS FOR NOT REQUIRING TIS: PREVIOUSLY STUDIED: []
	velopment process manual) must be held to define the level of analysis hanges to the development proposal identified above may require an
TRAFFIC ENGINEER	DATE
	EPC and/or the DRB. Arrangements must be made prior to submittal if a m, otherwise the application may not be accepted or deferred if the
TIS -SUBMITTED/_ /FINALIZED/_ / TRAFFIC ENGI	NEER DATE

Kelly Klein

From: Regina Villalobos

Sent: Thursday, March 5, 2020 3:55 PM

To: Kelly Klein

Subject: FW: Availabilty Statement Request Form

Hi Kelly,

This is what I got from the City about the water/sewer availability submittal.

Thank you,

Regina Villalobos

Engineer Intern, Community Development and Planning Bohannan Huston p. 505.823.1000 | d. 505.923.3354 | c. 505.204.4898

----Original Message-----

From: donotreply@abcwua.org <donotreply@abcwua.org>

Sent: Thursday, March 5, 2020 3:52 PM

To: Regina Villalobos < rvillalobos@bhinc.com > Subject: Availabilty Statement Request Form

Thank you. Your Availability Statement Form submission has been sent.

Project Name:

Mesa del Sol Montage Unit 4

Project Description:

This project proposes approximately 198 single-family residential lots within water zone RI-3E. The site is located south of existing Unit 1 and west of existing Unit 3B.

Project Address:

PO BOX 95078 ALBUQUERQUE NM 87199-5078

Development Type:

Residential

Fire Flow Requirement (if Residential enter N/A):

N/A

Legal Description:

TR A-6-C PLAT OF TRS A-6-A, A-6-B & A-6-C MESA DEL SOLINNOVATION PARK (A REPL OF TR A-6 MESA DEL SOL INNOVATIONPARK)

Zone Atlas Page:

R-16-Z & S-6-Z

DRB Project Number (if applicable)

CDRA Project Number (if applicable) Jurisdiction: City Requestor Name: Regina Villalobos Requestor Company: **Bohannan Huston Inc** Requestor Address: 7500 Jefferson St NE, Albuquerque, NM 87109 Requestor Phone Number: 505-923-3354 Requestor Email: rvillalobos@bhinc.com Prior Availability Statement Number: Attachment: 20200458_Water_Sewer_Availability_CombinedFINAL.pdf



March 04, 2020

Courtyard I 7500 Jefferson St. NE Albuquerque, NM 87109-4335

www.bhinc.com

voice: 505.823.1000 facsimile: 505.798.7988 toll free: 800.877.5332

David Gutierrez
ABCWUA
Planning Dept./Utility Development Section
Development and Building Services
600 Second Street NW
Albuquerque, NM 87102

Re: Water and Sanitary Sewer Availability Request for Mesa del Sol Montage Unit 4

Dear Mr. Gutierrez:

This letter is a request for water and sanitary sewer availability for the subject project. This project proposes approximately 198 single-family residential lots within water zone RI-3E. The site is located south of existing Unit 1 and west of existing Unit 3B.

Attached is an exhibit demonstrating proposed utility connections based on existing infrastructure located on the previous units of this development.

In accordance with the level A/B Master Plans, as approved by the Planning Commission, we are using a street/alley access and utility system within the neighborhood. The enclosures listed below are included for your use in preparing the water and sewer availability statement for this project:

- Zone Map #R-16, #S-16
- Exhibit 1 Conceptual Utility Plan for Mesa del Sol Montage Unit 4
- Level B Water/Sewer Master Plans for reference

The subdivision will be serviced by internal 6" water lines that connect to the exiting stubs built in Montage Unit 3B. With this project the water lines will be connected to form a looped system from Sagan Loop to Strand Loop. In addition, a 12" water line will be continued from Unit 3B and constructed in Stryker Road.

The subdivision will be serviced by internal 8" sanitary sewer lines. The sewer system will connect to the systems built previously in Unit 3B. With the exception of the SAS line in O'Keefe that will out fall to the existing SAS line in Stieglitz Avenue, the subdivision will outfall to the existing 21" SAS line in Stryker Road. Since the average grade of the site is 0.5%, sanitary sewer slopes have been a primary driver of grading and utility design in order to avoid premature construction of large lift stations.

Please feel free to call me with any questions.

Sincerely,

Kelly Klein, P.E. Project Manager

Community Development & Planning

Kelly M.K

RV/ kmk Enclosures

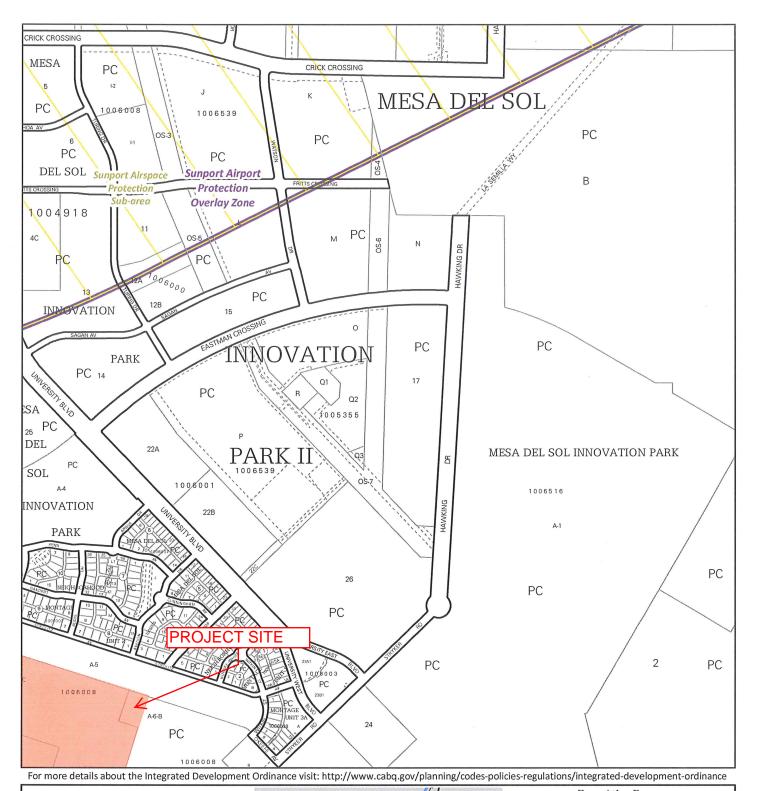
cc: Manny Barrera Mike Fietz

Michael Balaskovits, BHI

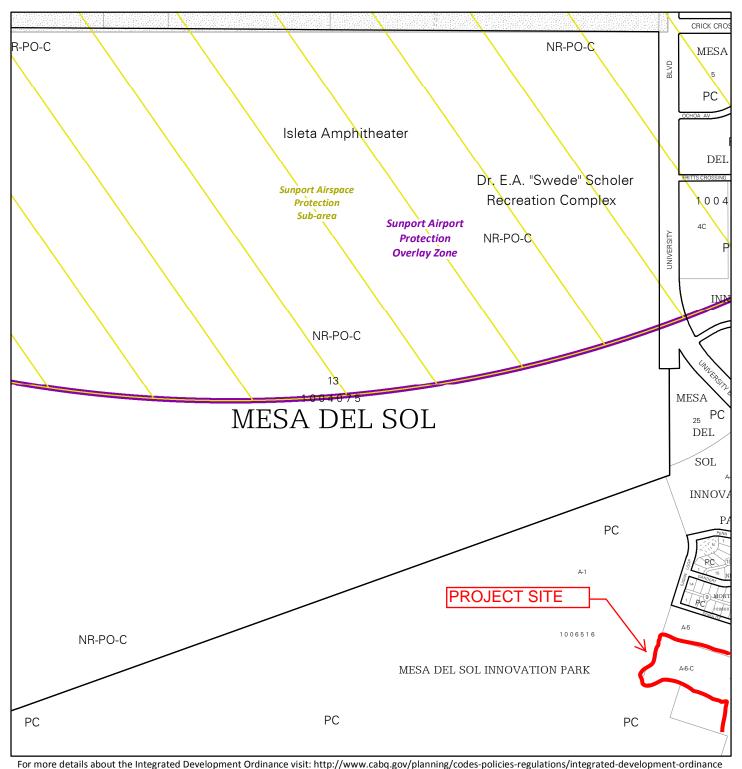
Engineering A

Spatial Data

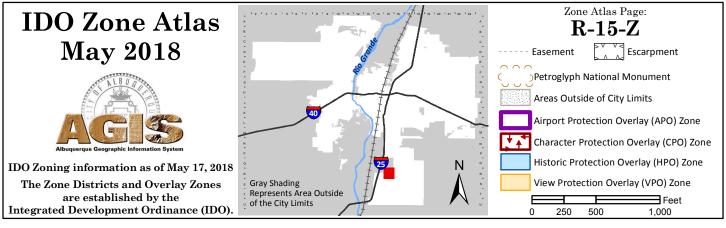
Advanced Technologies A

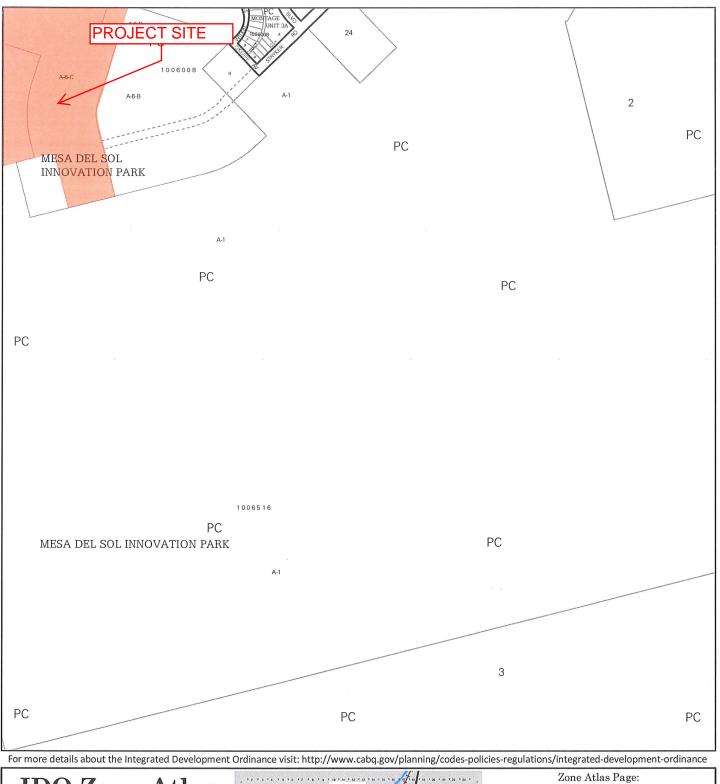


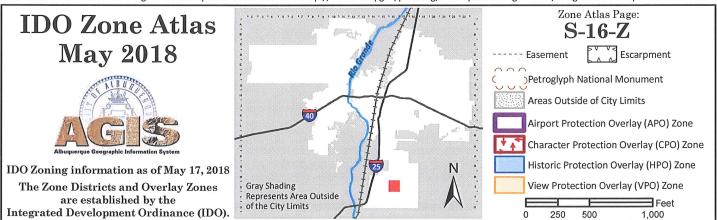
Zone Atlas Page: **IDO Zone Atlas** R-16-Z May 2018] Escarpment - Easement Petroglyph National Monument Areas Outside of City Limits Airport Protection Overlay (APO) Zone Character Protection Overlay (CPO) Zone Historic Protection Overlay (HPO) Zone IDO Zoning information as of May 17, 2018 The Zone Districts and Overlay Zones View Protection Overlay (VPO) Zone **Gray Shading** Represents Area Outside of the City Limits are established by the Feet Integrated Development Ordinance (IDO). 1,000

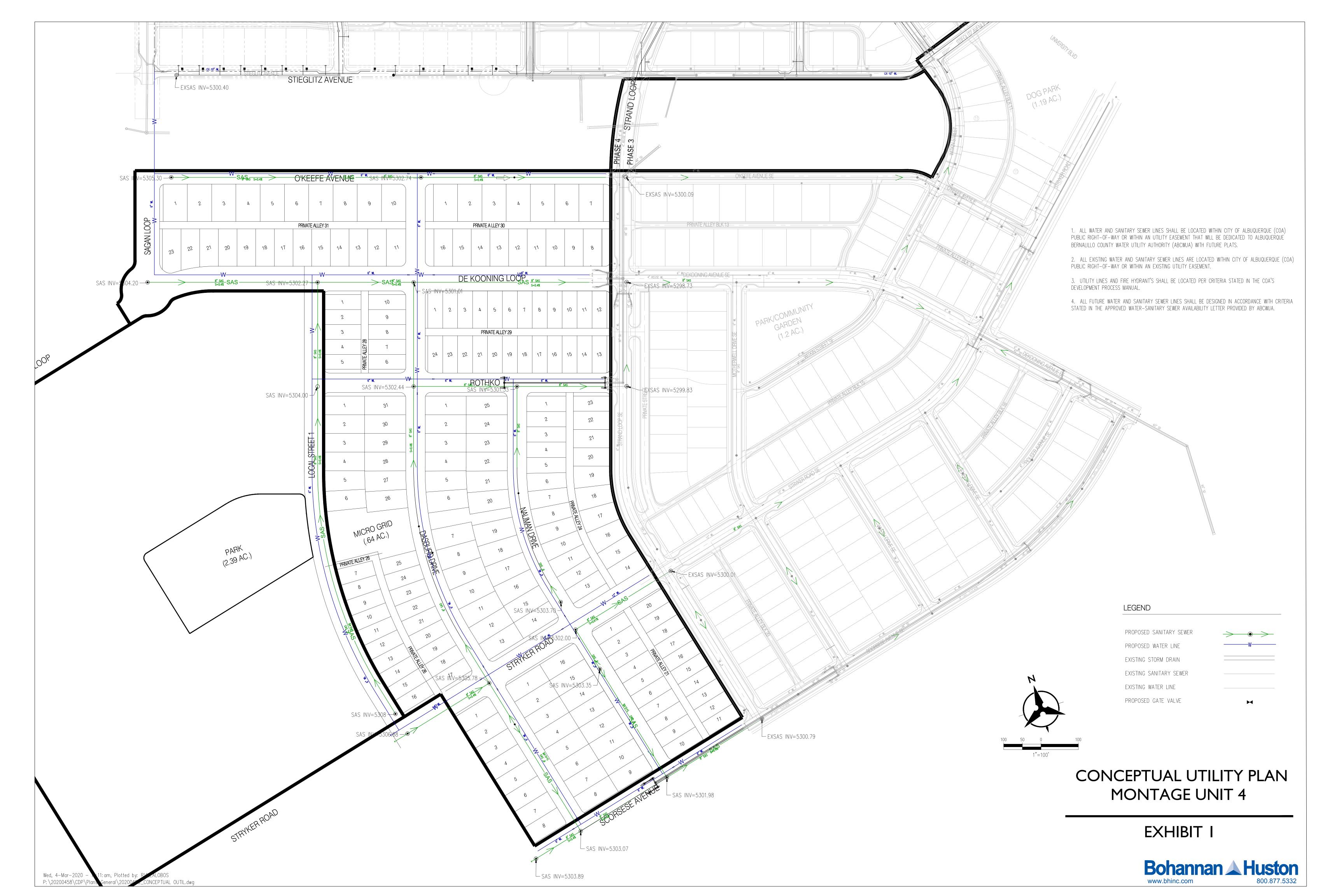


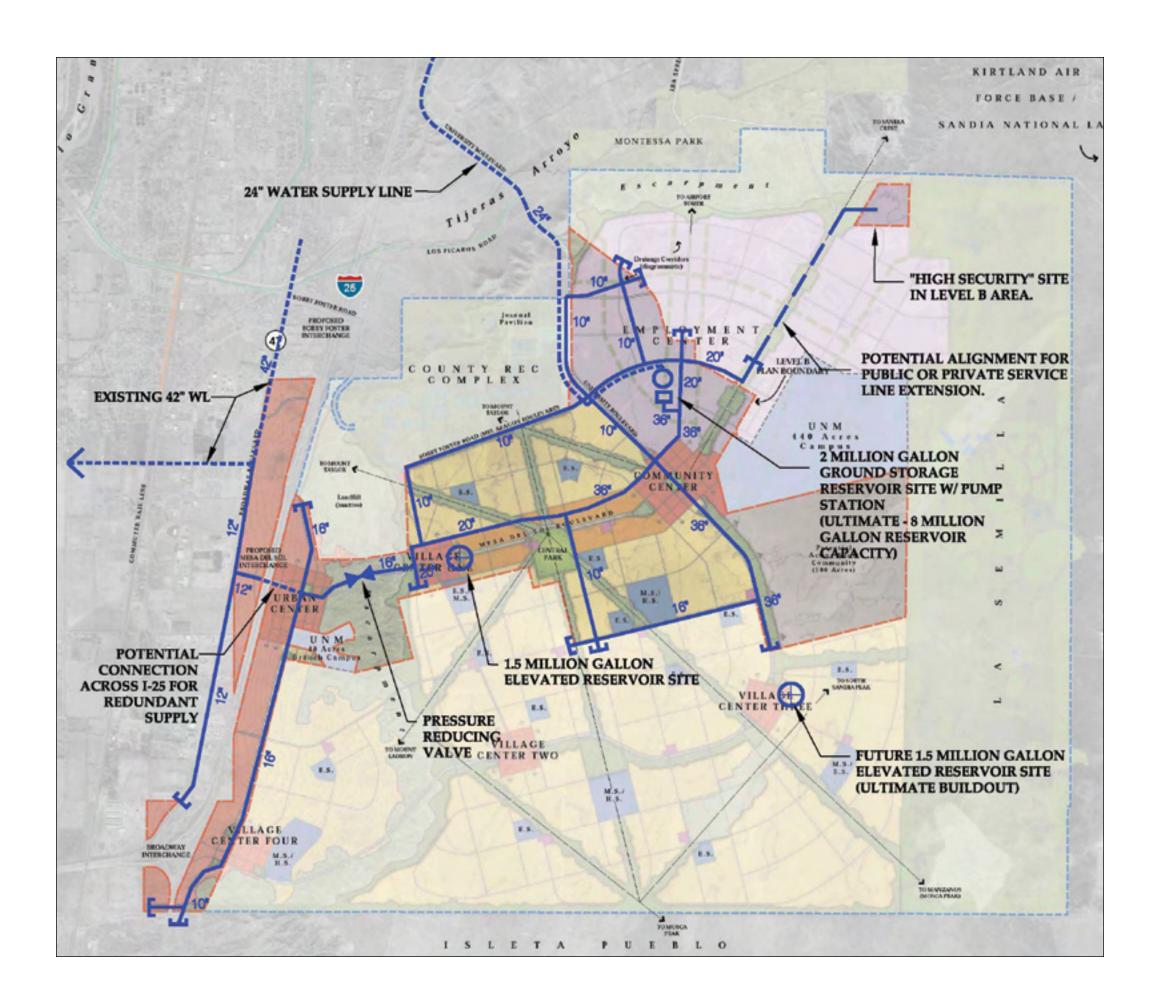
For more details about the integrated Development Ordinance visit: http://www.cabd.gov/planning/codes-policies-regulations/integrated-development-ordinance











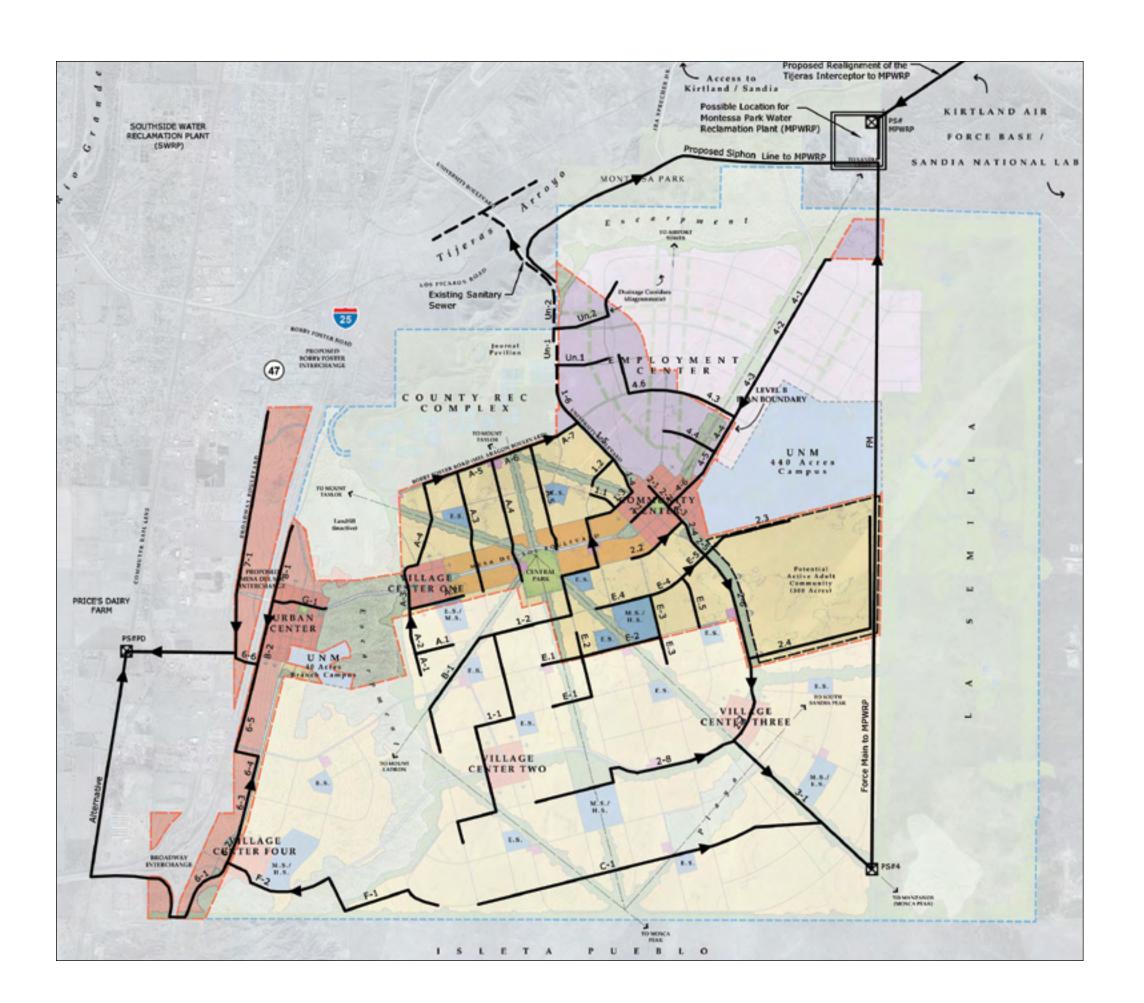
PREFERRED WATER SYSTEM: TRUNK INFRASTRUCTURE PLAN Figure 5-1

Notes

- The water infrastructure and line sizing shown on this plan is illustrative and subject to change with further planning with the water utility authority.
- Water wells and associated well collector system are anticipated prior to full development of Level B area.







SANITARY SEWER MASTER PLAN INCLUDING LEVEL A AREA Figure 5-2

Legend

