DRAINAGE LETTER REPORT <u>FOR</u> <u>ALAMEDA BOULEVARD SAN PEDRO TO WYOMING</u> <u>PROJECT</u> <u>CITY PROJECT NO. 7663.91</u>

1.8

January 2012

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I. INTRODUCTION AND SITE LOCATION

Part of the Alameda Boulevard Widening Project from I-25 to Wyoming includes the installation of a storm drain that will tie into a proposed 72" storm drain in San Pedro Drive on the west and tie into an existing 36" storm drain in Alameda Boulevard just east of Louisiana Boulevard. The storm drain system will also extend south in Louisiana Boulevard to Signal Avenue and then east to an existing 36" storm drain in Signal Avenue. The construction of the proposed storm drain is sized to accept the runoff from the ultimate Alameda street section and the adjacent properties and will eliminate the need for three existing retention ponds in the project area.

The Alameda storm drain discharges to the recently constructed or soon to be constructed storm drain included as part of the San Pedro Storm Drain Project. There is also an existing parallel storm drain system in San Pedro ranging from 48" to 54" diameter. The eventual outfall for both San Pedro Storm Drains are either 5-36" RCP culverts under I-25 north of Eagle Rock or the 8-36" RCP culverts under I-25 north of Alameda Place. The peak runoff for the developed condition is determined by following the basins and hydrology in the North Albuquerque Acres Master Drainage Plan (NAAMDP), by Resource Technology Inc. dated October 1998 and revising the basins based on subsequent drainage reports in the drainage area.

II. METHODOLOGY

A hydrologic analysis was not performed for this report. The hydrology given in the NAADMP was used to determine the peak flows that drain to the San Pedro Storm Drain. The hydrologic analyses in the NAAMDP was based on Section 22 of the City of Albuquerque Development Process Manual (DPM), entitled "Drainage, Flood Control, and Erosion Control," January, 1993.

The hydraulic analyses of the proposed storm drain system was also based on Section 22 of the DPM for determining pressure flow conditions and head losses at manholes. Microsoft Excel spreadsheet software was used to calculate the hydraulic grade line in storm drains under pressure and for determining head losses at manholes. Graphs given in Section 22 of the DPM were used to determine storm inlet capacities.

Pipe sizes, invert and rim elevations, and system geometry were taken from the record drawings provided by the COA as well as survey data taken for the project by the design team.

III. DRAINAGE ANALYSIS

A. HYDROLOGY

The scope of work identified reviewing the drainage basins in the NAADMP and revising those basins based on subsequent drainage reports that affect the basins that drain to Alameda within the project area. The NAADMP and San Pedro Storm Drain Project DAR identified basins 117.32 and 117.4 draining to Alameda Boulevard. For the developed condition, these basins have Land Treatment Type D percentages ranging from 50% to 60%.

Basins 117.32 and 117.4 were further divided based on previous drainage reports in the project area or on the proposed storm inlet locations along Alameda Boulevard. Basin 117.32 was divided into 9 sub-basins and Basin 117.4 was divided into 4 sub-basins (refer to Exhibit I). For each of the revised basins it was assumed that the Land Treatment D percentage would be the same for the similar basins in the NAADMP. Therefore, the revised basin area was multiplied by the unit peak flow (CFS/ACRE) to determine the peak flow from that basin. To be conservative, the peak flows from each basin were added instead of routed. Exhibit I shows the revised drainage basins and peak flows for each basin and at critical analysis points. Table 1 shows the peak flows for the revised drainage basins.

Basins	Area (acres)	Type D Land Treatment (%)	CFS/Acre	100yr Peak Flow (CFS)
117.321	0.54	50	3.82	2.06
117.322	2.44	50	3.82	9.32
117.323	2.68	50	3.82	10.24
117.324	1.37	50	3.82	5.23
117.325	1.25	50	3.82	4.77
117.326	5.96	50	3.82	22.77
117.327	4.80	50	3.82	18.34
117.328	5.34	50	3.82	20.40
117.329	6.74	50	3.82	25.75
117.41	17.75	60	4.02	71.36
117.42	14.29	60	4.02	57.45
117.43	0.85	60	4.02	3.42
117.44	0.43	60	4.02	1.33

Table 1 Revised Drainage Basin Peak Flows

B. STORM DRAIN HYDRAULICS

1. INTRODUCTION

The proposed storm drain system was modeled using record drawings and topographic and planimetric survey data obtained in the field. The design survey was produced in the NAVD 88 vertical datum. Two systems were modeled to determine the hydraulic grade line (HGL) of the proposed systems. The proposed storm drain system data were input to the models and flows were input at various points in the system represented by locations future flow interception points.

2. STORM INLET CAPACITIES

Storm inlet capacities were determined for the proposed storm drain to be constructed in Alameda and Louisiana. Graphs given in Section 22 of the DPM were used to determine storm inlet capacities. First, the depth of flow in the ultimate street section was determined using Plate 22.3 D-4. The proposed street slope and one-half of the street flows are inputs to the graph to obtain the depth of flow. Then the depth of flow and street slope are input to Plate 22.3 D-6 for

double grate inlets to determine the inlet capacity. It is assumed that each double grate will be 50% clogged and therefore the inlet capacity is reduced by half. Table 2 gives the inlet capacities for the proposed storm drain system.

Inlet Station	Contributing Basins	½ Street Flow (CFS)	Street Slope (%)	Flow Depth (FT)	Inlet Capacity (CFS)	Number of Inlets	Bypass Flow (CFS)
29+00	117.325 & 117.321	3.42	2.83	0.29	1.85	2	0.00
24+50	117.326	11.39	3.11	0.41	3.40	3	1.19
20+00	117.327	10.36	2.40	0.40	3.30	3	0.46
15+50	117.328	10.66	2.61	0.40	3.35	3	0.61
11+00	117.329	13.49	3.00	0.44	4.80	3	0.00

Table 2 Storm Inlet Capacities

3. STORM DRAIN HYDRAULICS

The hydraulic grade line analysis for the proposed storm drain was completed using an Excel spreadsheet that was developed using the methodology given in Section 22.3 of the DPM. The analysis showed that the downstream portion of the proposed Alameda Storm Drain System just east of San Pedro Drive is under pressure flow. The pressure flow unseals between the manholes at station 11+00 and station 15+50 and continues in gravity flow conditions.

The remainder of the storm drain system flows in gravity flow conditions. Therefore, between manholes the hydraulic grade line equals the normal depth of the storm drain. Table 3 gives the normal depths for each pipe segment under gravity flow conditions.

Segment Stations	Pipe Dia. (IN)	Pipe Slope (%)	Peak Flow (CFS)	Velocity (FPS)	Normal Depth (FT)
Alameda					
15+50 to 20+00	48	2.89	205.0	21.77	2.81
20+00 to 24+50	48	2.61	185.2	20.51	2.70
24+50 to 27+10	42	2.85	165.1	20.12	2.78
27+10 to 29+00	42	2.83	159.8	20.01	2.71
29+00 to 29+80	42	2.94	153.0	20.25	2.56
29+80 to 31+45	42	2.94	142.8	20.04	2.43
31+45 to 33+50	42	2.18	133.5	17.47	2.59
33+50 to 36+67	42	2.10	133.5	17.18	2.63
36+67 to 38+04	36	6.43	71.4	22.91	1.36
38+04 to 40+77	36	2.54	63.2	15.68	1.67
Louisiana					
11+10 to 12+74	36	0.80	60.9	9.61	2.52
7+54 to 11+10	36	0.65	57.5	8.53	2.72
12+74 to 13+59	24	1.42	1.33	4.45	0.30
Signal	36	1.88	57.5	13.67	1.73

Table 3 Storm Drain Normal Depth

The head losses through the manholes equals the heal loss due to bend losses, junction losses, and manhole losses. Table 4 shows the total head losses at each of the manholes.

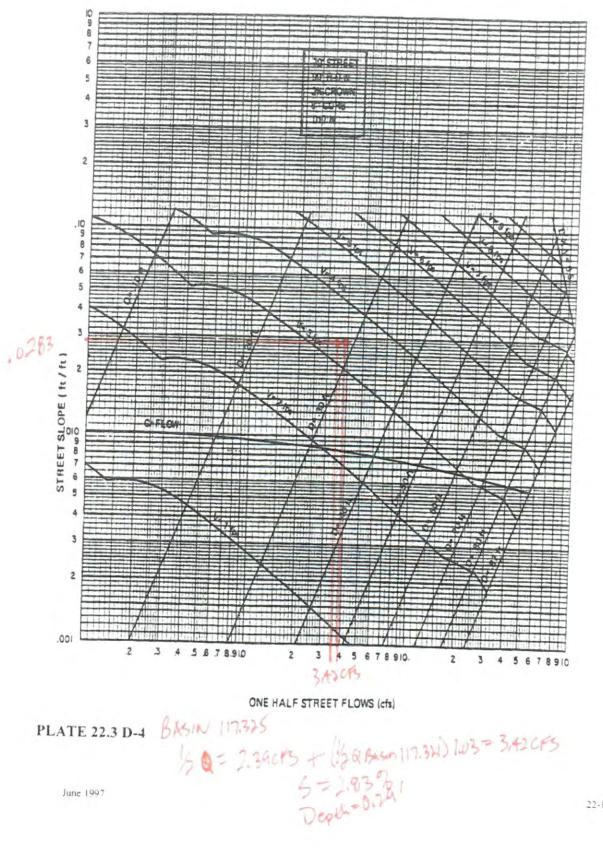
Station **Bend Loss Junction Loss Manhole Loss Total Losses** (FT) (FT) (FT) (FT) Alameda 0.00 1.60 0.33 1.93 20+00 24+50 0.00 1.27 0.31 1.58 27+10 0.00 0.38 0.31 0.69 29+00 0.00 0.32 0.64 0.32 29+80 0.00 0.73 0.31 1.04 31+45 0.00 1.68 0.24 1.92 33+50 0.00 0.00 0.23 0.23 2.51 2.92 36+67 0.00 0.41 38+04 0.00 2.56 0.21 2.77 Louisiana 7+05 0.00 0.00 0.15 0.15 7+55 0.58 0.00 0.15 0.73 11+10 0.00 0.41 0.06 0.47

Table 4 Manhole Head Losses

APPENDIX A HYDRAULIC CALCULATIONS

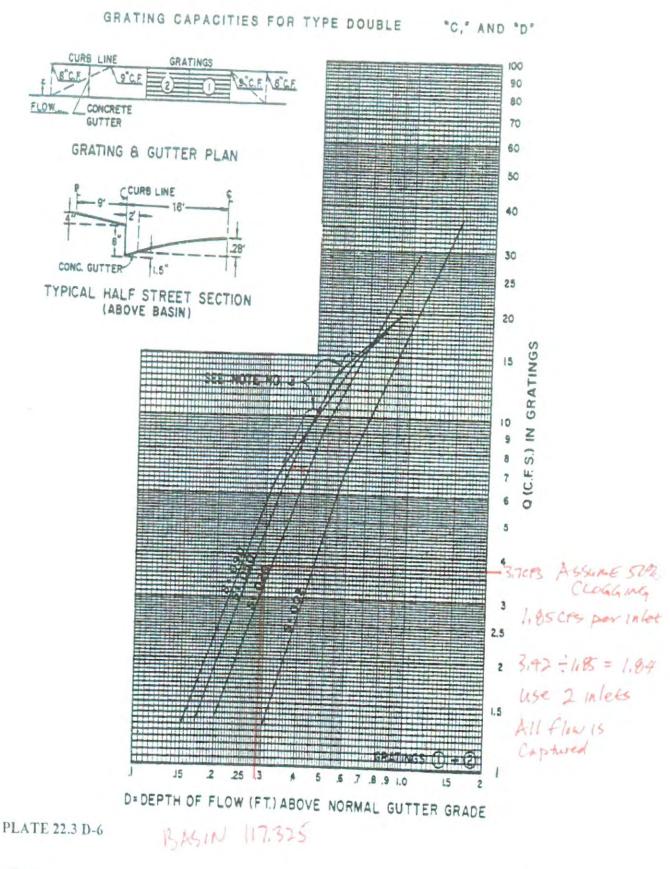
Chapter 22 - Drainage, Flood Control and Erosion Control

STREET CAPACITY



1

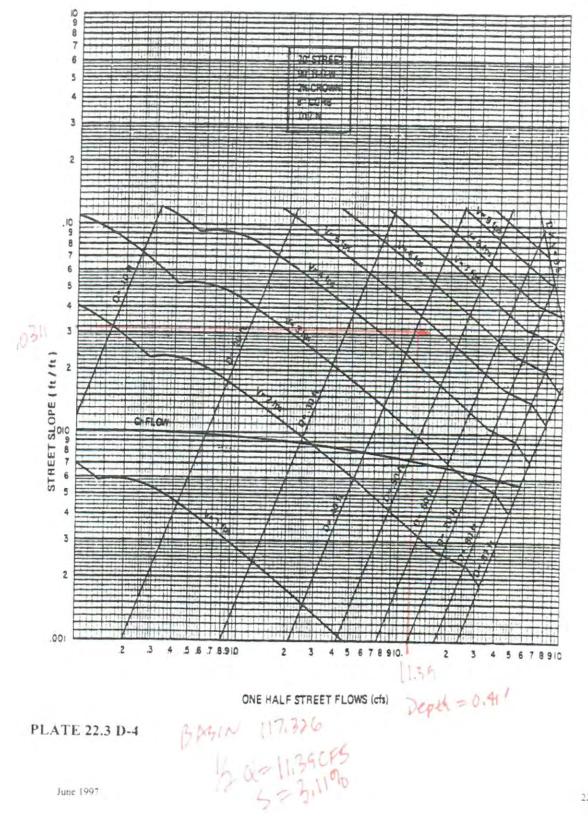
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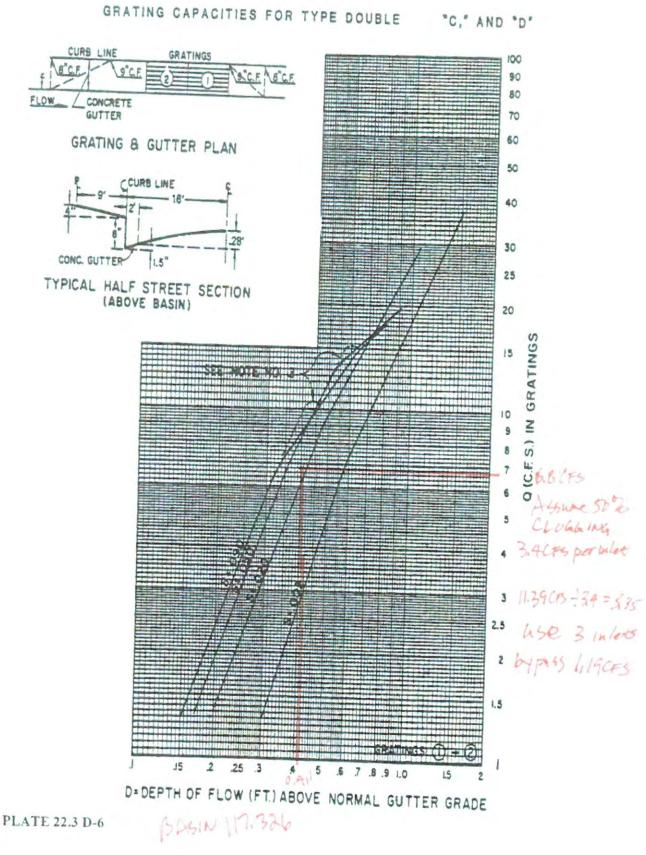
22-145

Chapter 22 - Drainage, Flood Control and Erosion Control

STREET CAPACITY



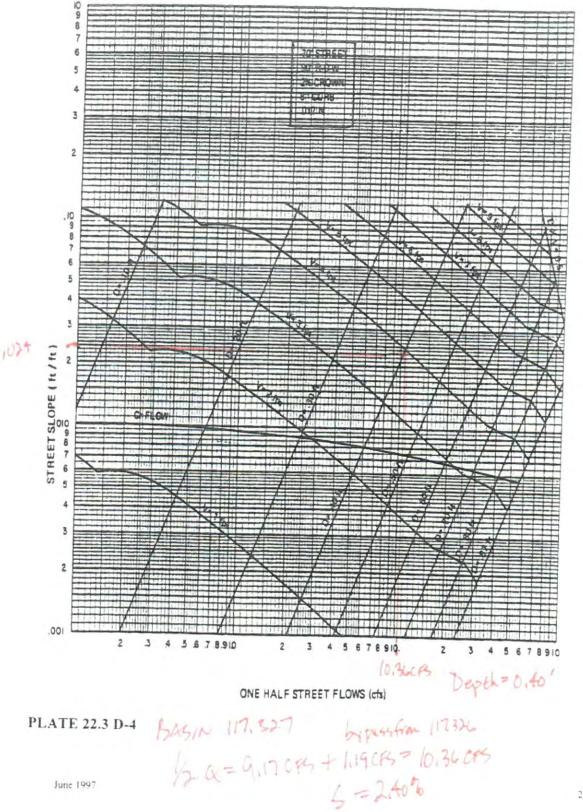
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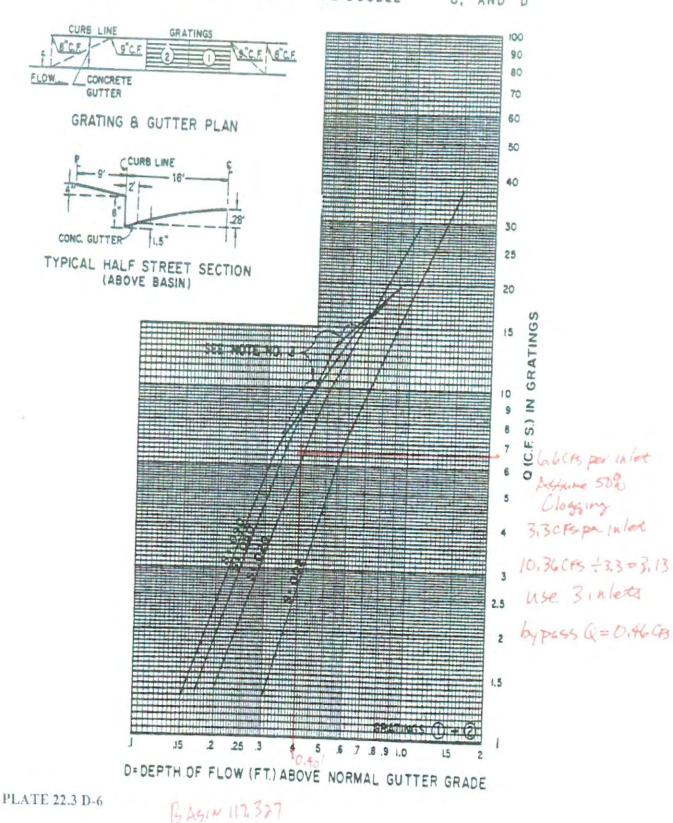
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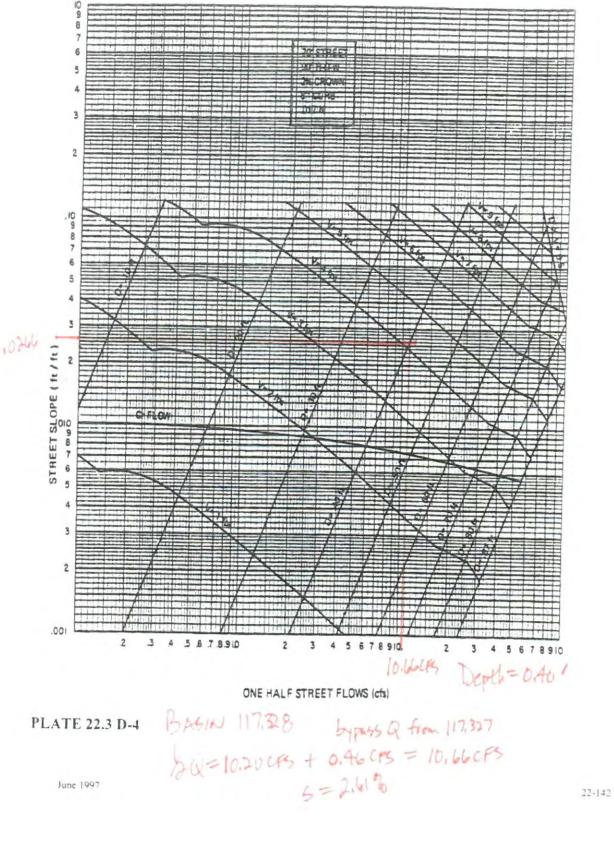


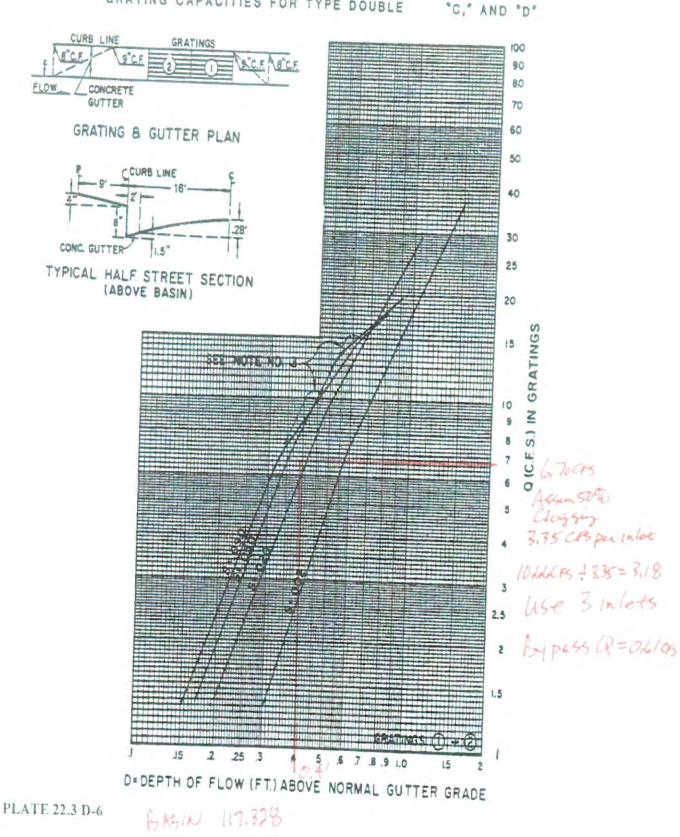
GRATING CAPACITIES FOR TYPE DOUBLE "C." AND "D"

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STREET CAPACITY



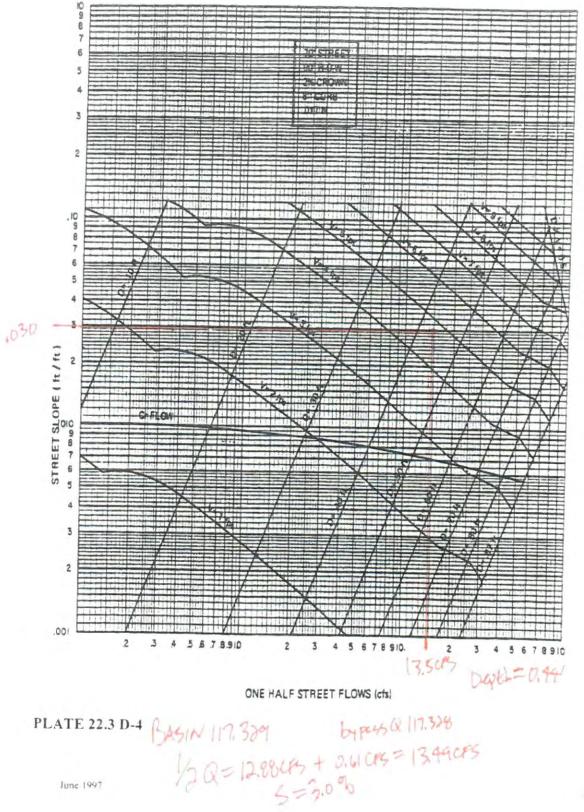


GRATING CAPACITIES FOR TYPE DOUBLE "C." AND "

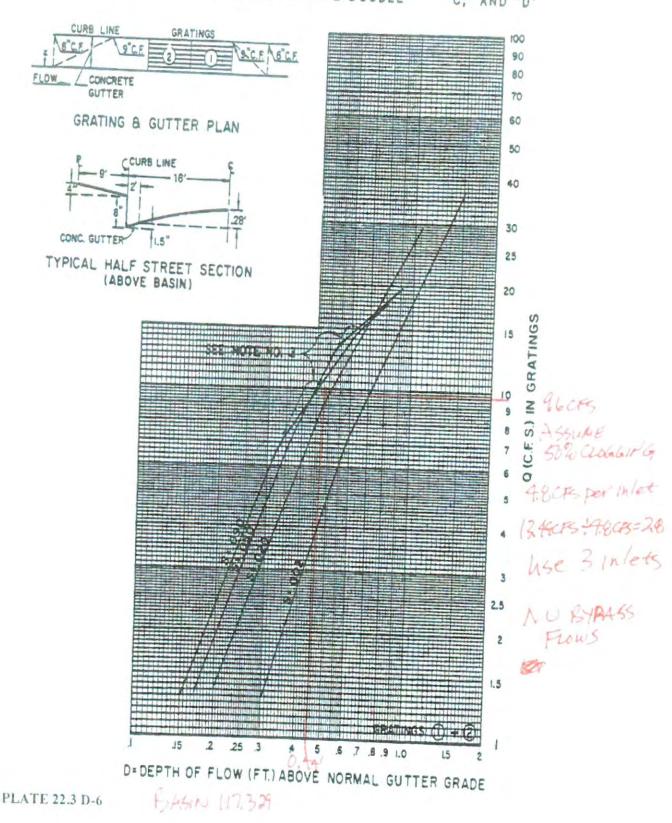
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STREET CAPACITY



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GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"

						SU	MMAF	O YS	F HYDI	RAU	LIC	CALCU	LATIC	ONS								BY:	DBT		
				_				(CLOSE	DCO	ONC	TIUC				100		100				DATE	1/10/12		
								1			1			1				1		1	1 2.4	SHEE	T: 1 of 1	1	
ROJECT:	ALAMEDA	FROM	1 SAN	PEDRO	TOEA	ST OF L	OUISIAN	AAND	LOUISIA	NAFR	OM S	SIGNAL TO	ALAME	DA								1,000		-	
100 year	10 Te - 17			1	L					1.000							1.1		1		N	1000	1.1.1		
1	2	3	4	5	6	7	8	9	10	1	11	12	13	14	1	15	16	17	18	19	20	21	22	23	
							1.1.1.1				JUN	CTION	LOSSE	S											1.
STATION	STRUCT	D	Q	A	V	K	Sf	L	DELTA	Q	D	ANGLE	hf	hb	Aavg	hj	hmh	ht	hmisc	SUM	E.G.	hv	H.G.	GROUND ELEV.	
	1	1			-		-						1	1.2.3	1.1.1				17-1		1		5228,70		E
0+23.88	WYE	1				1.00								0.00					0.00	0.00	5231.26	2.56	5228.70	5230.00	
		60	252	19.64	12.83	2606	0.0094	19					0.18			100		2.0		0.18	5231.44	2.56	5228.88	1	
0+44.56	BEND				-		Low-	1	45			F		0.36	19.64	0,00	0.13	0.00	1	0.49	5231.92	2.56		5230.00	
	11	60	252	19.64	12.83	2606	0.0094	56				1.2	0.52			120.1		-		0.52	5232.45	2.56			in the second
1+00	MH	100.00				1				27	24	80		0.00	17.77	0.02	0.00	0.00	1	0.02	5232.47	3.11	5229.36	5231.50	
10 10 10 10 1	1.00	54	225	15.90	14.15	1967.6	0.0131	450		1			5.88		1.	100.0	1.00			5.88	5238.35	3.11	5235.24	and the second second	
5+50	MH		1.0	-	1.1.1.1.1.1.1					1			1.	0.00	15.90	0.00	0.16	0.00	1.1.1	0.16	5238.51	3.11	5235.40	5244.00	
	1	54	225	15.90	14.15	1967.6	0.0131	0			A		0.00	1.11		1				0.00	5238.51	3.11	5235.40		and the second se
EMARKS:	BETWEEN	STAT	ION 1	1+00 AN	D 15+50	HGL B	ECOMES	NON-	PRESSU	RE	Man	ning's n: 0.	013	10.1			1.1.1								
	AND CONT	INUE	SUNE	DER GRA	AVITY F	LOW CC	NDITION	NS I		-			1											-	

Page 1

cular Pipe Flow			Alameda Bo	ulevard		
Diameter (ftin)	4.00	48	Station 15+5	50 to Station	20+00	
Slope	0.0289	ft/ft		and the second		
Manning's N	0.013	1				
Percent full	70%					
Depth	2.81	ft				
theta	3.97					
Area	9.42	sf				
Wetted Perimeter	7.94	ft				
Surface Width	3.661	ft				
Q	205.02	cfs				
V	21.77	fps				
Depth	theta	A		т	Q	V
0.20	0.90	0.23	1.80	1.74	1.17	4.99
0.40	1.29	0.65	2.57	2.40	5.10	7.80
0.60	1.59	1.18	3.18	2.86	11.87	10.04
0.80	1.85	1.79	3.71	3.20	21.38	11.95
1.00	2.09	2.46	4.19	3.46	33.45	13.62
1.20	2.32	3.17	4.64	3.67	47.82	15.08
1.40	2.53	3.92	5.06	3.82	64.21	16.38
1.60	2.74	4.69	5.48	3.92	82.29	17.53
1.80	2.94	5.48	5.88	3.98	101.71	18.55
2.00	3.14	6.28	6.28	4.00	122.10	19.43
2.20	3.34	7.08	6.68	3.98	143.03	20.20
2.40	3.54	7.87	7.09	3.92	164.06	20.84
2.60	3.75	8.65	7.50	3.82	184.71	21.36
2.80	3.96	9.40	7.93	3.67	204.45	21.76
3.00	4.19	10.11	8.38	3.46	222.67	22.03
3.20	4.43	10.78	8.86	3.20	238.69	22.15
3.40	4.69	11.38	9.38	2.86	251.63	22.10
3.60	5.00	11.91	9.99	2.40	260.26	21.85
3.80	5.38	12.33	10.76	1.74	262.39	21.28
4.00	6.28	12.57	12.57	0.00	244.19	19.43 Full

ircular Pipe Flow			Alameda Bou	ulevard	and the second second		
Diameter (ftin)	4.00	48	Station 20+0	0 to Station	24+50		n
Slope	0.0261	ft/ft					
Manning's N	0.013			L de la serie de			
Percent full	68%	1			1		
Depth	2.70	ft					
theta	3.86						
Area	9.03						1
Wetted Perimeter	7.72						1.0
Surface Width	3.746	ft					
Q	185.21		· · · · · · · · · · · · · · · · · · ·				
V	20.51	fps					
Depth	theta	A		Т	Q	V	
0.20	0.90	0.23	1.80	1.74	1.11	4.74	
0.40	1.29	0.65	2.57	2.40	4.84	7.41	
0.60	1.59	1.18	3.18	2.86	11.28	9.54	
0.80	1.85	1.79	3.71	3.20	20.32	11.36	
1.00	2.09	2.46	4.19	3.46	31.79	12.94	
1.20	2.32	3.17	4.64	3.67	45.45	14.33	
1.40	2.53	3.92	5.06	3.82	61.02	15.57	
1.60	2.74	4.69	5.48	3.92	78.20	16.66	
1.80	2.94	5.48	5.88	3.98	96.66	17.62	
2.00	3.14	6.28	6.28	4.00	116.03	18.47	
2.20	3.34	7.08	6.68	3.98	135.92	19.19	
2.40	3.54	7.87	7.09	3.92	155.91	19.80	
2.60	3.75	8.65	7.50	3.82	175.53	20.30	
2.80	3.96	9.40	7.93	3.67	194.29	20.68	
3.00	4.19	10.11	8.38	3.46	211.61	20.93	
3.20	4.43	10.78	8.86	3.20	226.83	21.05	
3.40	4.69	11.38	9.38	2.86	239.13	21.00	
3.60	5.00	11.91	9.99	2.40	247.33	20.76	
3.80	5.38	12.33	10.76	1.74	249.35	20.22	
4.00	6.28	12.57	12.57	0.00	232.06	18.47	Full

ircular Pipe Flow			Alameda Bo	ulevard		
Diameter (ftin)	3.50	42	Station 24+5	50 to Station	27+10	
Slope	0.0285	ft/ft				
Manning's N	0.013					
Percent full	80%					
Depth	2.78	ft				
theta	4.41					
Area	8.21	sf				
Wetted Perimeter	7.71	ft				
Surface Width	2.823	ft				
Q	165.10	cfs				
V	20.12	fps				
Depth	theta	A		т	Q	V
0.18	0.90	0.18	1.58	1.53	0.82	4.54
0.35	1.29	0.50	2.25	2.10	3.55	7.08
0.53	1.59	0.90	2.78	2.50	8.26	9.12
0.70	1.85	1.37	3.25	2.80	14.87	10.86
0.88	2.09	1.88	3.67	3.03	23.27	12.37
1.05	2.32	2.43	4.06	3.21	33.26	13.70
1.23	2.53	3.00	4.43	3.34	44.66	14.88
1.40	2.74	3.59	4.79	3.43	57.24	15.93
1.58	2.94	4.20	5.15	3.48	70.75	16.85
1.75	3.14	4.81	5.50	3.50	84.92	17.65
1.93	3.34	5.42	5.85	3.48	99.48	18.35
2.10	3.54	6.03	6.20	3.43	114.11	18.93
2.28	3.75	6.62	6.56	3.34	128.48	19.41
2.45	3.96	7.19	6.94	3.21	142.20	19.77
2.63	4.19	7.74	7.33	3.03	154.88	20.01
2.80	4.43	8.25	7.75	2.80	166.02	20.12
2.98	4.69	8.72	8.21	2.50	175.02	20.08
3.15	5.00	9.12	8.74	2.10	181.02	19.85
3.33	5.38	9.44	9.42	1.53	182.51	19.33
3.50	6.28	9.62	11.00	0.00	169.85	17.65 Full

ular Pipe Flow		.)	Alameda Bo			
Diameter (ftin)	3.50		Station 27+1	0 to Station	29+00	
Slope	0.0283	ft/ft				
Manning's N	0.013					
Percent full	77%					
Depth	2.71	ft				
theta	4.30					
Area	7.99					
Wetted Perimeter	7.52	ft				
Surface Width	2.930	ft				
Q	159.80	cfs				
V	20.01	fps				
Depth	theta	A		T	Q	V
0.18	0.90	0.18	1.58	1.53	0.81	4.52
0.35	1.29	0.50	2.25	2.10	3.53	7.06
0.53	1.59	0.90	2.78	2.50	8.23	9.09
0.70	1.85	1.37	3.25	2.80	14.82	10.82
0.88	2.09	1.88	3.67	3.03	23.18	12.33
1.05	2.32	2.43	4.06	3.21	33.14	13.65
1.23	2.53	3.00	4.43	3.34	44.50	14.83
1.40	2.74	3.59	4.79	3.43	57.04	15.87
1.58	2.94	4.20	5.15	3.48	70.50	16.79
1.75	3.14	4.81	5.50	3.50	84.63	17.59
1.93	3.34	5.42	5.85	3.48	99.13	18.28
2.10	3.54	6.03	6.20	3.43	113.71	18.87
2.28	3.75	6.62	6.56	3.34	128.02	19.34
2.45	3.96	7.19	6.94	3.21	141.70	19.70
2.63	4.19	7.74	7.33	3.03	154.34	19.94
2.80	4.43	8.25	7.75	2.80	165.44	20.05
2.98	4.69	8.72	8.21	2.50	174.40	20.01
3.15	5.00	9.12	8.74	2.10	180.39	19.78
3.33	5.38	9.44	9.42	1.53	181.86	19.26
3.50	6.28	9.62	11.00	0.00	169.25	17.59 Full

|A| = 0

rcular Pipe Flow			Alameda Bo	ulevard	1		1.1
Diameter (ftin)	3.50	42	Station 29+0	00 to Station	29+80		
Slope	0.0294	ft/ft			1		
Manning's N	0.013					·	
Percent full	73%		-				
Depth	2.56	ft					
theta	4.11						
Area	7.55						
Wetted Perimeter	7.19						
Surface Width	3.098						
Q	153.00						
V	20.25	fps					
Depth	theta	A		Т	Q	V	
0.18	0.90	0.18	1.58	1.53	0.83	4.61	
0.35	1.29	0.50	2.25	2.10	3.60	7.19	
0.53	1.59	0.90	2.78	2.50	8.39	9.27	1
0.70	1.85	1.37	3.25	2.80	15.11	11.03	
0.88	2.09	1.88	3.67	3.03	23.63	12.56	
1.05	2.32	2.43	4.06	3.21	33.78	13.92	
1.23	2.53	3.00	4.43	3.34	45.36	15.11	
1.40	2.74	3.59	4.79	3.43	58.13	16.18	
1.58	2.94	4.20	5.15	3.48	71.86	17.11	
1.75	3.14	4.81	5.50	3.50	86.25	17.93	
1.93	3.34	5.42	5.85	3.48	101.04	18.64	
2.10	3.54	6.03	6.20	3.43	115.90	19.23	
2.28	3.75	6.62	6.56	3.34	130.49	19.71	
2.45	3.96	7.19	6.94	3.21	144.43	20.08	
2.63	4.19	7.74	7.33	3.03	157.31	20.32	
2.80	4.43	8.25	7.75	2.80	168.62	20.44	
2.98	4.69	8.72	8.21	2.50	177.76	20.39	
3.15	5.00	9.12	8.74	2.10	183.86	20.16	
3.33	5.38	9.44	9.42	1.53	185.36	19.63	
3.50	6.28	9.62	11.00	0.00	172.51	17.93	Full

Circular Pipe Flow			Alameda Bou	levard	Sec. A. Common Sec.	
Diameter (ftin)	3.50	42	Station 29+80) to Station	31+45	
Slope	0.0294	ft/ft			1.	
Manning's N	0.013					
Percent full	69%					
Depth	2.43	ft				
theta	3.94					
Area	7.13					
Wetted Perimeter	6.89					
Surface Width	3.226					
Q	142.81					
V	20.04	fps				
Depth	theta	A		Т	Q	V
0.18	0.90	0.18	1.58	1.53	0.83	4.61
0.35	1.29	0.50	2.25	2.10	3.60	7.19
0.53	1.59	0.90	2.78	2.50	8.39	9.27
0.70	1.85	1.37	3.25	2.80	15.11	11.03
0.88	2.09	1.88	3.67	3.03	23.63	12.56
1.05	2.32	2.43	4.06	3.21	33.78	13.92
1.23	2.53	3.00	4.43	3.34	45.36	15.11
1.40	2.74	3.59	4.79	3.43	58.13	16.18
1.58	2.94	4.20	5.15	3.48	71.86	17.11
1.75	3.14	4.81	5.50	3.50	86.25	17.93
1.93	3.34	5.42	5.85	3.48	101.04	18.64
2.10	3.54	6.03	6.20	3.43	115.90	19.23
2.28	3.75	6.62	6.56	3.34	130.49	19.71
2.45	3.96	7.19	6.94	3.21	144.43	20.08
2.63	4.19	7.74	7.33	3.03	157.31	20.32
2.80	4.43	8.25	7.75	2.80	168.62	20.44
2.98	4.69	8.72	8.21	2.50	177.76	20.39
3.15	5.00	9.12	8.74	2.10	183.86	20.16
3.33	5.38	9.44	9.42	1.53	185.36	19.63
3.50	6.28	9.62	11.00	0.00	172.51	17.93 Full

cular Pipe Flow			Alameda Bo	ulevard		
Diameter (ftin)	3.50	42	Station 31+4	5 to Station	33+50	
Slope	0.0218	ft/ft				
Manning's N	0.013			· · · · · · · · · · · · · · · · · · ·		
Percent full	74%					
Depth	2.59	ft				
theta	4.15					
Area	7.64					
Wetted Perimeter	7.26	ft				
Surface Width	3.067	ft	-			
Q	133.51	cfs				
V	17.47	fps				
Depth	theta	A		т	Q	V
0.18	0.90	0.18	1.58	1.53	0.71	3.97
0.35	1.29	0.50	2.25	2.10	3.10	6.19
0.53	1.59	0.90	2.78	2.50	7.22	7.98
0.70	1.85	1.37	3.25	2.80	13.01	9.50
0.88	2.09	1.88	3.67	3.03	20.35	10.82
1.05	2.32	2.43	4.06	3.21	29.09	11.98
1.23	2.53	3.00	4.43	3.34	39.06	13.02
1.40	2.74	3.59	4.79	3.43	50.06	13.93
1.58	2.94	4.20	5.15	3.48	61.87	14.74
1.75	3.14	4.81	5.50	3.50	74.27	15.44
1.93	3.34	5.42	5.85	3.48	87.01	16.05
2.10	3.54	6.03	6.20	3.43	99.80	16.56
2.28	3.75	6.62	6.56	3.34	112.36	16.97
2.45	3.96	7.19	6.94	3.21	124.37	17.29
2.63	4.19	7.74	7.33	3.03	135.46	17.50
2.80	4.43	8.25	7.75	2.80	145.20	17.60
2.98	4.69	8.72	8.21	2.50	153.07	17.56
3.15	5.00	9.12	8.74	2.10	158.32	17.36
3.33	5.38	9.44	9.42	1.53	159.62	16.91
3.50	6.28	9.62	11.00	0.00	148.55	15.44 Full

Circular Pipe Flow		Second and a	Alameda Bo	ulevard	· · · · · · · · · · · · · · · · · · ·	
Diameter (ftin)	3.50	42	Station 33+5	50 to Station	36+67	
Slope	0.0210	ft/ft				
Manning's N	0.013	s			· = 111	
Percent full	75%			·		
Depth	2.63	ft				
theta	4.20					
Area	7.77					
Wetted Perimeter	7.35	ft				
Surface Width	3.020	ft				
Q	133.50	cfs				
V	17.18	fps				
Depth	theta	A		Т	Q	V
0.18	0.90	0.18	1.58	1.53	0.70	3.89
0.35	1.29	0.50	2.25	2.10	3.04	6.08
0.53	1.59	0.90	2.78	2.50	7.09	7.83
0.70	1.85	1.37	3.25	2.80	12.77	9.32
0.88	2.09	1.88	3.67	3.03	19.97	10.62
1.05	2.32	2.43	4.06	3.21	28.55	11.76
1.23	2.53	3.00	4.43	3.34	38.34	12.77
1.40	2.74	3.59	4.79	3.43	49.13	13.67
1.58	2.94	4.20	5.15	3.48	60.73	14.46
1.75	3.14	4.81	5.50	3.50	72.90	15.15
1.93	3.34	5.42	5.85	3.48	85.40	15.75
2.10	3.54	6.03	6.20	3.43	97.95	16.25
2.28	3.75	6.62	6.56	3.34	110.28	16.66
2.45	3.96	7.19	6.94	3.21	122.07	16.97
2.63	4.19	7.74	7.33	3.03	132.95	17.18
2.80	4.43	8.25	7.75	2.80	142.51	17.27
2.98	4.69	8.72	8.21	2.50	150.24	17.24
3.15	5.00	9.12	8.74	2.10	155.39	17.04
3.33	5.38	9.44	9.42	1.53	156.66	16.59
3.50	6.28	9.62	11.00	0.00	145.80	15.15 Full

Circular Pipe Flow			Alameda Bou	levard		
Diameter (ftin)	3.00	36	Station 36+67	7 to Station 3	38+04	
Slope	0.0643	ft/ft				
Manning's N	0.013				(f	
Percent full	45%					
Depth	1.36	ft				
theta	2.95					
Area	3.12	sf				
Wetted Perimeter	4.43	ft				
Surface Width	2.987	ft				
Q	71.39	cfs				
V	22.91	fps				
Depth	theta	A		т	Q	V
0.15	0.90		1.35	1.31	0.81	6.15
0.30	1.29	0.37	1.93	1.80	3.53	9.60
0.45	1.59	0.66	2.39	2.14	8.22	12.37
0.60	1.85	1.01	2.78	2.40	14.81	14.72
0.75	2.09	1.38	3.14	2.60	23.17	16.76
0.90	2.32	1.78	3.48	2.75	33.12	18.57
1.05	2.53	2.20	3.80	2.86	44.47	20.17
1.20	2.74	2.64	4.11	2.94	56.99	21.59
1.35	2.94	3.09	4.41	2.98	70.45	22.84
1.50	3.14	3.53	4.71	3.00	84.57	23.93
1.65	3.34	3.98	5.01	2.98	99.06	24.87
1.80	3.54	4.43	5.32	2.94	113.63	25.66
1.95	3.75	4.86	5.63	2.86	127.93	26.30
2.10	3.96	5.29	5.95	2.75	141.60	26.79
2.25	4.19	5.69	6.28	2.60	154.23	27.12
2.40	4.43	6.06	6.64	2.40	165.32	27.27
2.55	4.69	6.40	7.04	2.14	174.28	27.22
2.70	5.00	6.70	7.49	1.80	180.26	26.90
2.85	5.38		8.07	1.31	181.73	26.20
3.00	6.28	7.07	9.42	0.00	169.13	23.93 Full

Circular Pipe Flow			Alameda Bo	oulevard	· · · · · · · · · · · · · · · · · · ·		
Diameter (ftin)	3.00	36	Station 38+	10 to Station	40+77		
Slope	0.0254	ft/ft	1				1
Manning's N	0.013			I	1		
Percent full	56%	1			·		
Depth	1.67	ft					
theta	3.36						
Area	4.03						
Wetted Perimeter	5.04	ft					
Surface Width	2.982	ft					1
Q	63.18	cfs					
V	15.68	fps					
Depth	theta	A		Т	Q	V	
0.15	0.90	0.13	1.35	1.31	0.51	3.86	
0.30	1.29	0.37	1.93	1.80	2.22	6.03	
0.45	1.59	0.66	2.39	2.14	5.17	7.77	
0.60	1.85	1.01	2.78	2.40	9.31	9.25	
0.75	2.09	1.38	3.14	2.60	14.56	10.54	
0.90	2.32	1.78	3.48	2.75	20.82	11.67	
1.05	2.53	2.20	3.80	2.86	27.95	12.68	
1.20	2.74	2.64	4.11	2.94	35.82	13.57	
1.35	2.94	3.09	4.41	2.98	44.28	14.35	
1.50	3.14	3.53	4.71	3.00	53.15	15.04	
1.65	3.34	3.98		2.98	62.26	15.63	
1.80	3.54	4.43	5.32	2.94	71.42	16.13	
1.95	3.75	4.86	5.63	2.86	80.41	16.53	
2.10	3.96	5.29	5.95	2.75	89.00	16.84	
2.25	4.19	5.69	6.28	2.60	96.93	17.05	
2.40	4.43	6.06	6.64	2.40	103.90	17.14	
2.55	4.69	6.40	7.04	2.14	109.54	17.11	
2.70	5.00	6.70	7.49	1.80	113.29	16.91	
2.85	5.38	6.94	8.07	1.31	114.22	16.47	
3.00	6.28	7.07	9.42	0.00	106.30	15.04	Full

rcular Pipe Flow			Louisiana B	oulevard		
Diameter (ftin)	3.00	36	Station 11+		12+74	
Slope	0.0080					
Manning's N	0.013	1.		· · · · · · · · · · · · · · · · · · ·		
Percent full	84%					
Depth	2.52	ft				
theta	4.64	1				
Area	6.34	sf				
Wetted Perimeter	6.95					
Surface Width	2.201	ft				
Q	60.90	cfs				
V	9.61	fps				
Depth	theta	A		Т	Q	V
0.15	0.90	0.13	1.35	1.31	0.29	2.17
0.30	1.29	0.37	1.93	1.80	1.25	3.39
0.45	1.59	0.66	2.39	2.14	2.90	4.36
0.60	1.85	1.01	2.78	2.40	5.22	5.19
0.75	2.09	1.38	3.14	2.60	8.17	5.91
0.90	2.32	1.78	3.48	2.75	11.68	6.55
1.05	2.53	2.20	3.80	2.86	15.69	7.11
1.20	2.74	2.64	4.11	2.94	20.10	7.61
1.35	2.94	3.09	4.41	2.98	24.85	8.05
1.50	3.14	3.53	4.71	3.00	29.83	8.44
1.65	3.34	3.98	5.01	2.98	34.94	8.77
1.80	3.54	4.43	5.32	2.94	40.08	9.05
1.95	3.75	4.86	5.63	2.86	45.12	9.28
2.10	3.96	5.29	5.95	2.75	49.95	9.45
2.25	4.19	5.69	6.28	2.60	54.40	9.57
2.40	4.43	6.06	6.64	2.40	58.31	9.62
		6.40	7.04	2.14	61.47	9.60
				1.80	63.58	9.49
	5.38	6.94	8.07	1.31	64.10	9.24 8.44 Full
2.40 2.55 2.70 2.85 3.00	4.69 5.00	6.40 6.70	7.04 7.49	2.14 1.80	61.47 63.58	

cular Pipe Flow			Louisiana Be	oulevard			
Diameter (ftin)	3.00	36	Station 7+54	to Station	11+10		
Slope	0.0065	ft/ft					
Manning's N	0.013		·		1		
Percent full	91%		· · · · · · · · · · · · · · · · · · ·				
Depth	2.72	ft					
theta	5.05						
Area	6.74						
Wetted Perimeter	7.58	ft	1				
Surface Width	1.734	ft	1				
Q	57.50	cfs	· · · · · · · · · · · · · · · · · · ·				
V	8.53	fps					
Depth	theta	A		Т	Q	V	
0.15	0.90	0.13	1.35	1.31	0.26	1.95	
0.30	1.29	0.37	1.93	1.80	1.12	3.05	
0.45	1.59	0.66	2.39	2.14	2.61	3.93	
0.60	1.85	1.01	2.78	2.40	4.71	4.68	
0.75	2.09	1.38	3.14	2.60	7.37	5.33	
0.90	2.32	1,78	3.48	2.75	10.53	5.90	1
1.05	2.53	2.20	3.80	2.86	14.14	6.41	
1.20	2.74	2.64	4.11	2.94	18.12	6.86	G
1.35	2.94	3.09	4.41	2.98	22.40	7.26	h
1.50	3.14	3.53	4.71	3.00	26.89	7.61	
1.65	3.34	3.98	5.01	2.98	31.50	7.91	1
1.80	3.54	4.43	5.32	2.94	36.13	8.16	
1.95	3.75	4.86	5.63	2.86	40.68	8.36	
2.10	3.96	5.29	5.95	2.75	45.02	8.52	
2.25	4.19	5.69	6.28	2.60	49.04	8.62	
2.40	4.43	6.06	6.64	2.40	52.56	8.67	
2.55	4.69	6.40	7.04	2.14	55.41	8.65	
2.70	5.00	6.70	7.49	1.80	57.31	8.55	
2.85	5.38	6.94	8.07	1.31	57.78	8.33	
3.00	6.28	7.07	9.42	0.00	53.77	7.61	Full

Circular Pipe Flow			Louisiana B			
Diameter (ftin)	3.00		Station 7+5	4 to Station	11+10	
Slope	0.0188					
Manning's N	0.013					
Percent full	58%					
Depth	1.73	ft				
theta	3.44					
Area	4.21	sf			-	1
Wetted Perimeter	5.16	ft		1		
Surface Width	2.966	ft				
Q	57.51					
V	13.67	fps				
Depth	theta	A		Т	Q	V
0.15	0.90	0.13		1.31	0.44	3.32
0.30	1.29			1.80	1.91	5.19
0.45	1.59			2.14	4.45	6.69
0.60	1.85			2.40	8.01	7.96
0.75	2.09	1.38		2.60	12.53	9.07
0.90	2.32	1.78		2.75	17.91	10.04
1.05	2.53	2.20	3.80	2.86	24.05	10.91
1.20	2.74	2.64	4.11	2.94	30.82	11.67
1.35	2.94			2.98	38.09	12.35
1.50	3.14	3.53	4.71	3.00	45.73	12.94
1.65	3.34	3.98	5.01	2.98	53.56	13.45
1.80	3.54	4.43		2.94	61.44	13.87
1.95	3.75	4.86	5.63	2.86	69.18	14.22
2.10	3.96	5.29	5.95	2.75	76.57	14.49
2.25	4.19	5.69	6.28	2.60	83.39	14.66
2.40	4.43	6.06	6.64	2.40	89.39	14.75
2.55	4.69	6.40	7.04	2.14	94.24	14.72
2.70	5.00	6.70	7.49	1.80	97.47	14.55
2.85	5.38	6.94	8.07	1.31	98.27	14.17
3.00	6.28	7.07	9.42	0.00	91.45	12.94

rcular Pipe Flow			Louisiana Bo	oulevard			· · · · · · · · · · · · · · · · · · ·
Diameter (ftin)	2.00	24	Station 12+7	4 to Station	13+59		
Slope	0.0142	ft/ft					
Manning's N	0.013						
Percent full	15%						
Depth	0.30	ft					
theta	1.60						
Area	0.30						
Wetted Perimeter	1.60						
Surface Width	1.432						
Q	1.33	cfs					
V	4.45	fps					
Depth	theta	A		т	Q	V	
0.10	0.90	0.06	0.90	0.87	0.13	2.20	
0.20	1.29	0.16	1.29	1.20	0.56	3.44	
0.30	1.59	0.30	1.59	1.43	1.31	4.43	
0.40	1.85	0.45	1.85	1.60	2.36	5.28	
0.50	2.09	0.61	2.09	1.73	3.69	6.01	
0.60	2.32	0.79	2.32	1.83	5.28	6.66	
0.70	2.53	0.98	2.53	1.91	7.09	7.23	f
0.80	2.74	1.17	2.74	1.96	9.08	7.74	
0.90	2.94	1.37	2.94	1.99	11.23	8.19	
1.00	3.14	1.57	3.14	2.00	13.48	8.58	
1.10	3.34	1.77	3.34	1.99	15.79	8.92	
1.20	3.54	1.97	3.54	1.96	18.11	9.20	
1.30	3.75	2.16	3.75	1.91	20.39	9.43	
1.40	3.96	2.35	3.96	1.83	22.57	9.61	
1.50	4.19	2.53	4.19	1.73	24.58	9.73	
1.60	4.43	2.69	4.43	1.60	26.35	9.78	
1.70	4.69	2.85	4.69	1.43	27.78	9.76	
1.80	5.00	2.98	5.00	1.20	28.73	9.65	
1.90	5.38	3.08	5.38	0.87	28.97	9.40	· · · · · · · · · · · · · · · · · · ·
2.00	6.28	3.14	6.28	0.00	26.96	8.58	Full

 $\kappa_{i} = 0$

						SUMN	ARY C	DF H	DRAU	LIC	CAL	CULAT	IONS								BY:	1	
					CL	OSED	CONE	DUIT	- HEAI	D LO	SS	AT MAN	HOLI	ES							DATE		
SEXTERE	ALAMEDA	-	1000	SPER 2		L		1	LAUNAN		L		L								SHEE	T: 1 of 1	
00 year	ALAMEDA	FROI	VI SAN	PEDRO	TOEA	STOFL	OUISIAN	AND	LOUISIA	NAFR	COM S	IGNAL TO	ALAME	DA			ļ						
1	2	3	4	5	6	7	8	9	10	-	11	12	13	14		15	16	17	18	19	21	23	
	-		4	U	0				10	-		CTION	LOSSE			15	10	1/	10	13	21	23	
STATION	STRUCT	D	Q	A	V	K	Sf	E	DELTA	Q	D	ANGLE	hf	hb	Aavg	hj	hmh	ht	hmisc	SUM	hv	GROUND ELEV.	
5+50	MH	-			-		-			-			-						0.00	0.00	7.36	5244.00	
5150	N/11	48	205	12.57	21.77	1437.2	0.0203	450		-			-	-	-				0.00	0.00	7.36		
20+00	MH		200	12.01	21.11	1401.2	0.0200	400		20	24	80	-		12.57	1.60	0.33	0.00		1.92	6.53		*****
		48	185	12.57	20.51	1437.2	0.0166	450								-				0.00			
24+50	MH			1		1	2		1.1.1	20	24	80	-	-	11.09	1.27	0.31	0.00		1.58	6.29		
		42	165	9.62	20.12	1006.6	0.0269	260		_			_							0.00	6.29		
27+10	MH	10	160	0.00	20.01	1000 0	0.0050	100		5	24	80	-	-	9.62	0.38	0.31	0.00		0.69	6.22	5277.00	
29+00	MH	42	160	9.62	20.01	1006.6	0.0253	190		7	24	80	-		9.62	0.32	0.32	0.00	-	0.00	6.22	5282.00	
3.00	IVILI	42	153	9.62	20.25	1006.6	0.0231	80		1	24	80	-	-	9.02	0.32	0.32	0.00		0.64		5282.00	
29+80	MH	76	100	0.02	20.20	1000.0	0.0201	00		10	24	80		-	9.62	0.73	0.31	0.00	-	1.04	6.24	5284.00	
		42	143	9.62	20.04	1006.6	0.0202	165					-		0.02	0.10	0.01	0.00		0.00	6.24		
31+45	MH				1	1				9	24	80		-	9.62	1.68	0.24	0.00		1.92	4.74		******
		42	134	9.62	17.47	1006.6	0.0177	205												0.00	4.74		
33+50	MH									0			_		9.62	0.00	0.23	0.00		0.23	4.58		
36+67	MH	42	134	9.62	17.18	1006.6	0.0177	318		00	- 20	00		1	0.04	0.54	0.11	0.00		0.00	4.58		
0+07	MIT	36	71	7.07	22.01	667.28	0.0113	137		63	36	90			8.34	2.51	0.41	0.00	-	2.92	8.15	5307.00	
88+04	MH	50		1.01	22.31	007.20	0.0113	151	-	8	24	90		-	7.07	2.56	0.21	0.00		2.77	4.27	5311.00	
		36	63	7.07	16.58	667.28	0.0089	267			~ 1		-	-	1.01	2.00	0.21	0.00		0.00	4.27	3311.00	*****
1 1 1 1 1										-													
1																			1			5307.00	
2+75	MH													0.00					0.00	0.00	1.43		
		36	60.9	7.07	9.61	667.28	0.0083	164					-	0.00		-	-		0.00	0.00	1.43		
1+10	MH				0.01		0.0000	104		3.4	24	80		0.00	7.07	0.41	0.06	0.00		0.47	1.43		
		36	57.5	7.07	8.52	667.28	0.0074	355	-	0.4	+	30	-	0.00	1.01	0.41	0.00	0.00		0.47	1.13		
7+55	мн	50	51.5	1.01	0.33	007.20	0.0074	-355	90	-				0.50	7.07	0.00	0.45	0.00					
+00	M.CI	20	67.F	7.07	10.07	007.00	0.0074		90	0				0.58	7.07	0.00	0.15	0.00		0.73	2.90	5309.00	
		36	57.5	7.07	13.67	667.28	0.0074	50					-			-			-	0.00	2.90		
+05	MH			_	-		-			4.5			1.1.1	0.00	7.07	0.00	0.15	0.00		0.15	2.90	5310.00	
		36	53	7.07	13.67	667.28	0.0063	0	1					-				10.00		0.00	2.90		
)+00	MH			-						53				0.00	3.53	0.00	0.00	-0.58		-0.58	0.00		
REMARKS:					1					1. 1	Mann	ning's n: 0.0	013			1					2.5		*****

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