

**CABEZON COMMUNITIES PHASE 2
DRAINAGE MANAGEMENT PLAN
UNIT 16**

August 2004

PREPARED FOR:

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SUBMITTED TO:

**City Of Rio Rancho &
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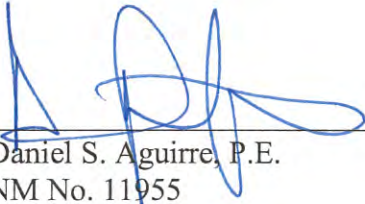
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WCEA File No. X4-218-012

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August 2004

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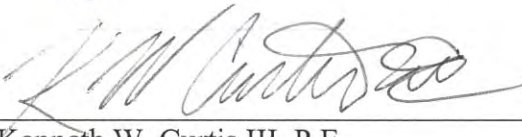
CABEZON COMMUNITIES PHASE 2

DRAINAGE MANAGEMENT PLAN

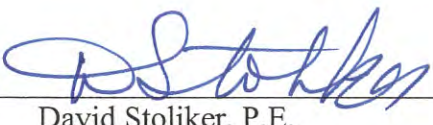
UNIT 16

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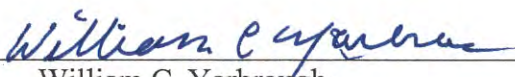
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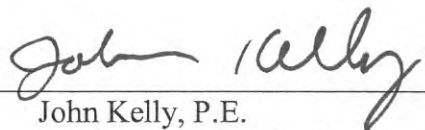
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DRAINAGE MANAGEMENT PLAN – CABEZON PHASE 2 DEVELOPMENT

Introduction

This report is based on the drainage section of the approved Cabezon Communities Master Plan (Master Plan), 2003, and specifically outlines the drainage plan for Phase 2 of Cabezon development. It addresses requirements of the Master Plan and is consistent with both the Black Arroyo Drainage Management Plan (BLWMP) (ASCG, 2002) and the Cabezon Phase 1 Drainage Management Plan. A Drainage Implementation Plan, detailing the major infrastructure proposed for the development and identifying its phasing, has also been submitted.

Although the Master Plan for the 912 acre community scheduled three phases of development, Phases 2 and 3 will now be combined into Phase 2. Phase 2 comprises approximately 625 acres of the Cabezon Communities Development. *Figure 1* shows the entire Cabezon Community Development, with Phase 2 development in green. Phase 1 development is in yellow, while an alternate area, in orange, is not currently part of Cabezon but could be included in the future. Finally, the two large tracts in the southwest corner of Unit 16, uncolored in *figure 1*, are not part of the Cabezon development.

Drainage Constraints

Drainage conditions placed on Cabezon come from two sources. First, although the Southern Sandoval County Arroyo Flood Control Authority (SSCAFCA) Board of Directors approved the Master Plan, they left two items for discussion. Second, the BLWMP, which has been approved by SSCAFCA, the Albuquerque Metropolitan Arroyo Flood Control Authority (AMAFCA), and the City of Rio Rancho (CORR), governs how drainage within the Black Arroyo Watershed will be managed. Therefore, new development must address BLWMP requirements, and any changes to it must be approved by all three entities.

The two discussion items the SSCAFCA Board left from the Master Plan were proposed improvements for the East Branch of the Black Arroyo, and conveyance of flows through the project from the West Branch of Black Arroyo. This DMP proceeds with the assumption that a hard-lined channel capable of conveying the 100-year, 24-hour storm on the East Branch is acceptable. Further, it assumes that the Modified BLWMP Ultimate Conditions Model approved for use in the Phase 1 DMP is also valid for this Phase 2 DMP. The Phase 1 DMP altered the percent land treatment types for BLWMP sub-basin 211 (*figure 2*), and also modeled several off-site commercial basins within Unit 16 with ponds that limit runoff to historic levels. These basins were 211B (Southern Plaza), Off_1A, Off_1B, Off_2A, and Off_2B. This was only done for properties where field investigation verified the existence of the detention facilities. Photographic documentation and a map are provided in the Phase 1 DMP.

The West Branch briefly crosses Cabezon, before entering the off-site southwest corner of Unit 16 (shown uncolored in *figure 2*). The Cabezon developers have agreed to provide a means of insuring the safety of this crossing. Two options are available. One is to build a structure with the capacity to convey the ultimate conditions flow downstream of Unser Boulevard. The other is to provide an upstream means of attenuating peak flows before they reach this point, most likely by expanding or creating a detention facility. The decision on how to proceed will be made during later discussions with SSCAFCA and CORR.

Finally, the BLWMP places two drainage constraints on Cabezon development. First is that the Black Dam shall not, in the present nor under assumed ultimate build-out conditions, be permitted to overtop its emergency spillway in a 100-year 24-hour storm event. This means that the amount of runoff that may be directed to the Black Dam, owned by AMAFCA, must not exceed available storage capacity. This criterion must be met not only at the conclusion of total build-out of the Cabezon Community, but also at any time during construction. The other requirement is that the “first flush” (initial 0.25 inches of runoff) be treated to the maximum extent practicable to remove floatables and sediment.

Hydrology Methodology

Hydrologic Analysis for Phase 2 conforms to Section 22.2, Hydrology, of the Development Process Manual, Volume 2, Design Criteria for the City of Albuquerque, New Mexico, January 1993 (COA DPM), and to the BLWMP. Hydrologic modeling was performed using the Arid-lands Hydrologic Model (AHYMO_97), distributed by Anderson Hydro. The 100-year 24-hour return frequency storm was used as the basis of this analysis. Assumptions regarding land treatments, storm duration and intensity, and water quality requirements established in the BLWMP were followed in this analysis. The sediment bulk rate and routing method differed from the BLWMP, and are discussed further in the *Proposed Conditions Hydrology* section below.

Existing Conditions Hydrology

Existing conditions are taken from the the FEMA floodplain mapping study (RTI, 1994). The original AHYMO files created for that study were used as a foundation for further detailed analysis by the BLWMP, which modeled developed existing conditions. Developed existing conditions assume full development, but with existing platting and facilities. A summary of the FEMA floodplains and key flowrates from RTI's FIS model for the area are shown in *figure 4. Table 1* compares historic, developed existing, and fully developed flows for key locations in the area.

Table 1: Historic, Developed Existing, and Fully Developed Flows at Key Locations

Location	Historic Conditions from FIS	Devex Conditions from BLWMP, Aug 02	Fully Developed Conditions from Cabezon model
West Branch at Unser	2687	5105	5004
West Branch at Dam/ Westside Boulevard	2986	5934	5991
East Branch at Southern Blvd.	1406	2137	2252
East Branch at Dam/ Westside Boulevard	1876	3160	3733

Figure 7 is the Black Dam's current topography. The corresponding table in this figure shows the stage-storage relationship of the facility. Of note is that the existing storage in the Dam, 294 AF, is only slightly less than the State Engineer's permitted storage volume

of 304 AF, which was used in the Modified BLWMP Ultimate Conditions Model.

Proposed Conditions Hydrology

The Modified BLWMP Ultimate Conditions Model, dated January 20, 2004, provides the basis for the Cabezon Phase 2 Model. The Modified BLWMP is based on the FEMA study, but adjusts routing and land treatment types of some sub-basins to represent managed full development in the Black Arroyo Watershed. In an attempt to assess the effect that Cabezon development will have on the Black Dam, both Phase 1 and 2 development were added to the Modified BLWMP model. *Appendix A* contains a printout of the Cabezon Phase 2 Model summary output file, as well the electronic file on diskette.

The Phase 1 DMP described other changes made to the Modified BLWMP Model in Phase 1 to reflect fully developed, current conditions in the watershed. For Phase 2, BLWMP sub-basins 160, 161, 218A, 218B, 219, 220, 253, 255, 256, and 620 were removed to account for the insertion of Phase 2 development. Also, parts of BLWMP sub-basins 550 and 650, which overlap Cabezon at its southern border, were removed to match proposed boundaries. *Figure 2* shows overlapping Cabezon and BLWMP sub-basin boundaries. *Figures 5A* and *5B* are routing schematics for the Cabezon Phase 2 Model, including the Modified BLWMP Model, with the portions pasted in for Phase 1 and 2 circled in *figure 5B*.

The initial Cabezon Phase 2 DMP, submitted May 2004, asked for approval of two methodology differences from the Modified BLWMP. These were a reduced sediment bulk rate, and use of the Muskingum-Cunge, rather than the Variable Storage Coefficient (VSC), routing method. Discussion with SSCAFCA and CORR on July 22, 2004, determined what would be used in Cabezon's final hydrology.

As a result of that discussion, two changes to the BLWMP were agreed upon for Cabezon

modeling. First, sediment bulk rates for the Cabezon model will be set to 6% to represent fully developed conditions with paved roads. This differs from the Modified BLWMP, which uses sediment bulk rates of 6% and 18%.

Second, all flow routing in the Cabezon Phase 2 Model uses the *ROUTE MCUNGE* command in AHYMO. In the Modified BLWMP, the two commands *COMPUTE TRAVEL TIME* and then *ROUTE* are used almost exclusively. At the July meeting, Clifford Anderson—developer of AHYMO_97—presented results from a report he prepared at SSCAFCA’s request comparing the two methods. Following Mr. Anderson’s suggestion, the Cabezon model uses the *ROUTE MCUNGE* command, but decreases the time step from 0.05 hr (3 minutes) to 0.01 hr (36 seconds) for obtaining peak flows.

This change should more accurately catch peak flow for a given hydrograph. This is because many reach lengths are short, while flow velocity is high. Therefore, flow may leave some reaches in less than three minutes, and hence those peak flows will not be accurately represented using the three minute time step. Because AHYMO_97 can only store 600 points for each hydrograph, however, this model does not accurately depict runoff volume, which is important in assessing Cabezon’s effect on the Black Dam.

Therefore, two models were developed for Cabezon design. The two are identical in all ways, except that the first, QP72204.txt, uses a time step of 0.01 hours while the second, VOL72204.txt, uses a time step of 0.05 hours. The first was used to characterize peak flow within the watershed, while the second was used to assess runoff volume. The AHYMO summary output files for both models are in *Appendix A*.

These changes affect flow throughout the entire model, not only within Cabezon. *Table 2* presents the differences for locations discussed in an April 9, 2004, meeting between SSCAFCA, ASCG, and Wilson & Company representatives.

Table 2: Comparison of BLWMP and Cabezon Off-site Flows

Location	BLWMP	Cab Ph 2 Flow,cfs	Cab Ph 2 Flow,cfs
	Flow, cfs	dt = 0.05 hr	dt = 0.01 hr
East Branch South of Southern	2167	2099	2252
Golf Course Rd SD North	75	75	77
Golf Course Rd SD South	77	81	83
23rd Avenue Ponds North	50	53	54
24th Avenue Ponds South	48	48	48
West Branch at Unser	4978	4210	5004
Gateway at Unser	656	600	604
West Branch at Dam	5879	5097	5991
East Branch at Dam	5194	3485	3748

Flow on the West Branch is more strongly influenced by the lower sediment bulk rate, which can reduce peaks by as much as 12%. On the East Branch, however, the routing method is primarily responsible for the change in peak flows. Most East Branch sub-basins upstream from Cabezon are developed, so sediment bulking rates in the Modified BLWMP were already 6%.

The results of the hydrologic analysis are presented below. The allowable discharge from each Phase 2 tract is given, as well as modeling parameters and assumptions used to derive that discharge. Currently undeveloped or partially developed sub-basins were modeled for developed conditions following methodology established in the BLWMP, as indicated in the final column of *Table 3*.

Table 3. Cabezon Drainage Basins-Phase 2

Sub-basin	Acres	DIUs/Acre	T _P	Land Treatments				Q _{peak} (cfs)	Volume (ac-ft)	Methodology/Notes
				A	B	C	D			
5B	12.5	6.00	0.13	0.0	28.1	15.0	56.9	46	1.9	D per DPM; B & C per SSCAFCA
5C	18.5	6.00	0.13	0.0	28.1	15.0	56.9	67	2.8	"
7D	50.8	5.20	0.13	0.0	31.9	17.1	51.0	178	5.9	"
1	71.5	4.00	0.13	0	30.0	28.0	42.0	242	9.0	"
2	20.6	4.00	0.13	0	30.0	28.0	42.0	70	3.0	"
6	61.2	6.00	0.13	0.0	28.1	15.0	56.9	222	9.3	"
8	19.0	6.06	0.13	0.0	27.8	14.9	57.3	69	2.9	"
9	28.7	6.18	0.13	0.0	27.2	14.6	58.2	105	4.4	"
10	83.1	6.00	0.13	0.0	28.1	15.0	56.9	301	12.6	"
12	9.7	Commercial	0.13	0	0	15	85	43	1.9	Free Discharge Allowed
13	50.5	Off-site Commercial	0.13	0	0	15	85	218	10.0	BLWMP
14	58.2	Offsite	0.13	0	10	10	80	231	10.9	BLWMP
15	14.7	Mixed Use	0.13	0	10	10	80	61	2.8	BLWMP
16	19.8	School	0.13	0	25	25	50	70	2.8	Free Discharge Allowed
18	5.0	Park	0.13	0.0	85.0	0.0	15.0	13	0.4	SSCAFCA
19	5.0	Park	0.13	0.0	85.0	0.0	15.0	13	0.4	SSCAFCA
20	5.0	Park	0.13	0	85	0	15	13	0.4	SSCAFCA
21	15.0	WWTP	0.13	0	10	10	80	62	2.8	Wastewater Treatment Plant
OFF_4	31.9	Off-site	0.13	1	29	28	42	108	4.2	BLWMP
OFF_5	16.3	Off-site	0.13	3	20	25	52	58	2.4	BLWMP
OFF_6	16.8	Off-site	0.13	1	29	28	42	57	2.2	BLWMP
OFF_7	6.8	Off-site	0.13	1	29	28	42	23	0.9	BLWMP
OFF_8	9.6	School	0.13	1	29	28	42	32	1.3	BLWMP
A_1	20.3	Arroyo/Channel	0.13	0	20	30	50	73	2.9	Based on arroyo cross-section
A_2	5.2	Arroyo/Channel	0.13	0	20	30	50	19	0.8	"
A_3	5.1	Arroyo/Channel	0.13	0	20	30	50	18	0.7	"
A_4	4.0	Arroyo/Channel	0.13	0	20	30	50	14	0.6	"
A_5	7.7	Arroyo/Channel	0.13	0	20	30	50	28	1.1	"
A_6	29.6	Arroyo/Channel	0.13	0	20	30	50	107	4.3	"
R_4	6.3	Roadway	0.13	0	5	29	66	26	1.1	Based on roadway cross-section
R_5	4.9	Roadway	0.13	0	5	29	66	19	0.8	"
R_7	1.1	Roadway	0.13	0	3	17	80	5	0.2	"
R_8	7.6	Roadway	0.13	0	4	22	74	31	1.4	"
R_9	9.9	Roadway	0.13	0	4	22	74	41	1.8	"

Peak flow directions and quantities for both on and off-site sub-basins used in the hydrologic modeling are presented graphically in *figure 6*. The major off-site flow entering Phase 2 is in the East Branch of Black Arroyo, crossing Southern Boulevard and entering north of off-site sub-basin 6 (Off_6 in *figure 6*). As this modeling is intended to represent conditions with the Cabezon development, flows listed correspond to fully developed conditions.

Phase 2 of Cabezon contains only one commercially zoned tract, Tract 12. One other change from the initial submission of the Phase 2 DMP is that it erroneously held commercial properties to historic discharge. This is not required by CORR, and the sole commercial tract in Phase 2, Tract 12, is therefore allowed free discharge.

Hydraulics

Phase 2 has several significant hydraulic features, including two storm drains. Haestad Methods' StormCAD v5.5 was used to perform a hydraulic grade line analysis. Friction losses were calculated using Manning's equation, while junction and bend losses were calculated using StormCAD's Standard Method, which multiplies a user-input loss coefficient by the velocity head. Loss coefficients were determined using the COA DPM procedure.

The main Phase 2 storm drain connects to an existing 60 inch RCP, which carries Phase 1 outflow from the pond in Tract 17. Prior to Phase 2 construction, this outflow will be released into Tributary B near the southwest corner of Tract 15 (*figure 3*). In Phase 2, 66 to 72 inch RCP will connect to two 40" x 65" RCP arch pipes approximately 200 feet before flow is released to the East Branch Channel (*figure 8*). The of the storm drain line varies between 1.9% and 2.8%. This storm drain, in the Trail Side Road R-O-W and an easement between tracts, will also collect flow from Tracts 7C, 7D, 15, 16, 18, and 8. It will enter the East Branch Channel between Tracts 8 and 9. *Figure 3* shows the location of these facilities, and *figure 8* is a plan and profile of the line.

The other storm drain consists of 36 inch RCP that follows the Cabezon Boulevard R-O-W. It will begin near the southern-most corner of Tract 5C, and convey flows to the release point in the East Branch Channel as it crosses Cabezon Boulevard. The slope of the storm drain line is initially 2.1%, and then approximately 3% to its terminus. Flow from Tract 5C and Cabezon Boulevard is collected in this line. Again, refer to *figure 3* for locations. *Figure 9* is a plan and profile of the storm drain. *Appendix B* contains further design details for both storm drain lines.

For subdivision design, allowable peak flowrates and their entrance locations into the storm drain network are shown in *figure 6*. Each subdivision is permitted free discharge to the major drainage network. If a subdivision drainage plan should call for a higher discharge rate than identified in this plan, the subdivision plan must receive approval

from CORR, SSCAFCA, and AMAFCA for this excess discharge, or else use on-site detention. In the former case, the subdivision drainage plan must show that downstream systems can safely convey this additional flow, and also that the water surface elevation at Black Dam will not be increased. The latter case requires meeting the drainage policies of the CORR and SSCAFCA.

Most of the off-site flows that enter Cabezon Phase 2 are conveyed to the Black Dam in the East Branch Channel. The largest flow, 2252 cfs, is in the East Branch Channel itself, entering Cabezon on the north, near 27th Street. The other East Branch flows enter Cabezon along its eastern edge, and cross one of its sub-basins before entering the East Branch (*figure 6*). The *Golf Course Road Improvements Final Drainage Report* (Wilson & Company, February 2002) was consulted to insure that Cabezon improvements would enhance previously constructed facilities.

As mentioned previously, the East Branch, which carries these flows, will be improved per the discussion surrounding the approval of the Cabezon Master Plan. The proposed trapezoidal channel will be concrete, with a 10 foot bottom, 2:1 side slopes, and a total width between 28 and 34 feet. A multi-use trail will be constructed in the channel R-O-W. The channel was designed to convey the 100 year, 24 hour storm, while the overbank area will provide the necessary freeboard. *Figure 12* shows a typical cross-section.

Based on BLWMP requirements, a structure will be incorporated into Phase 2 to both improve water quality and detain runoff, reducing peak flow into the Black Dam. The Water Quality Structure will be off-site, immediately upstream of the Black Dam, and will treat flow from the entire Black Arroyo Watershed. The structure is designed to remove both floatables and sediment.

Water Quality facilities are generally designed to treat what is called the “first flush” of a storm. The first flush is considered to be the initial 1/4” of runoff. As the Cabezon Development encompasses approximately 900 acres, the volume of runoff that must be treated can be quantified in this way:

$$\text{WQ Volumetric Runoff (acre-ft)} = \frac{\frac{1}{4} \text{ in}}{12 \text{ in/ft}} \times 900 \text{ acres} = 18.75 \text{ AF}$$

The approved Cabezon Master Plan calls for 43.3 AF of water quality. Water quality features were originally master-planned in three possible locations: 1) 2 AF adjacent to Tract 19, 2) 7 AF within Tract 17, and 3) 25 AF immediately upstream of Black Dam within AMAFCA right-of-way.

Aggressive interest from homebuilders has accelerated the development schedule from 7 years to 3-4 years. This unforeseen market demand influenced the final locations of the water quality structures. First, Tract 17, originally planned to treat 7 AF, has been designed and approved for 26.5 AF as part of Phase 1 construction. Second, a preliminary drainage study of the 2 AF structure adjacent to Tract 19 showed it was not cost effective and it will not be constructed. Finally, the water quality structure upstream of the Black Dam will remain, and will provide a minimum of 25 AF (*figure 10*).

The total volumetric runoff to be treated within Cabezon when it is fully developed is approximately 50 AF. That number exceeds both the initial volume from the Cabezon Master Plan and also the first flush from the Cabezon Development.

The Water Quality Structure in Phase 2, near the Black Dam, is designed to treat runoff from both the West and East Branch (*figure 10*). The structure will detain a volume of +/- 25 AF using a +/- 350-foot long, stepped weir, 15 feet wide at its top (*Appendix B*). It will be constructed of soil cement. Again, the majority of floatables and sediment will be held behind the weir, and can later be removed from the WQ structure.

In addition, this structure will also increase both detention time and storage volume, serving multiple purposes. The increased detention time again gives opportunity for natural processes to treat runoff to the maximum extent practicable. Also, the volume of runoff entering the Black Dam is reduced for several reasons. Initial abstractions will increase, and the structure also serves as a settling pond, reducing the sediment load that

reaches the Black Dam. More importantly, the structure increases available detention storage. This is because, when the water surface rises above the top of the stepped weir, both the WQ Structure and the Black Dam act to detain stormwater in a single, larger dam.

For this reason, the stage-storage-discharge curve for the Black Dam was adjusted in the Cabezon Phase 2 Model. A 20" x 28" arch pipe allows low flows to exit the new structure and enter the Black Dam relatively unaffected by the WQ Structure. As the water surface rises above the pipe, the WQ Structure will detain water to the top of its weir, 5165'. However, once the water surface elevation overtops the weir, the weir no longer affects the Black Dam hydraulically, and the WQ Structure acts to enlarge storage behind the Black Dam.

Also of note is that the Black Dam stage elevations, originally given in NGVD29, were adjusted to NAVD88, which is used in all work within Cabezon. Using the more current NAVD88 vertical datum adjusts NGVD29 elevations up by 2.8 feet in this geographic area. Current survey data can be reviewed in *figure 7*. Further details can be found in the AHYMO model on diskette in *Appendix A*.

Water Quality Structure Maintenance and Operation

While the Cabezon Development is located within Sandoval County, some of its infrastructure is in Bernalillo County. For example, the Black Dam—to which the East Branch Channel drains—is in Bernalillo County and hence owned by AMAFCA. The proposed +/- 25 AF Water Quality Structure will be located within AMAFCA right-of-way. AMAFCA will own the structure and will be responsible for the structural inspection and maintenance, as well as sediment monitoring and removal.

The East Branch Channel is in Sandoval County, and therefore SSCAFCA and CORR will most likely maintain it, to include trash and debris removal within the channel reach.

The developer, Curb North LLC, is working closely with all agencies in preparation for a turnkey agreement that will outline the details of design, construction, ownership, and M&O of the proposed facility. Final responsibilities for the Water Quality Structure are contingent upon the final agreement.

Conclusion

One of the most important objectives of the Cabezon Communities' Drainage Management Plan is minimizing impact on the Black Dam, both currently and in the BLWMP ultimate build-out scenario. The Black Dam is near its permitted volume when the Modified BLWMP is used to model ultimate conditions. As large portions of the watershed remain undeveloped, however, the Dam is not at risk under current conditions. To help minimize Cabezon's impact, Phase 1 provided 25 AF of detention in Tract 17.

The true measure of impact on the Black Dam is the water surface elevation at the Dam, as predicted for the 100 year, 24 hour storm. *Table 4* compares this water surface elevation as predicted by the Modified BLWMP Ultimate Conditions Model and both the Cabezon Phase 1 and Phase 2 Models. Note that the elevation listed for full development of Cabezon is from the AHYMO model using the 0.05 hour time step (VOL72204.txt). Also, the vertical datum used below is NAVD88, which differs from that used in the Modified BLWMP (NGVD29). The Modified BLWMP Ultimate Conditions Model—essentially the standard—places it at 5167.02 feet, 1.53 feet below the emergency spillway.

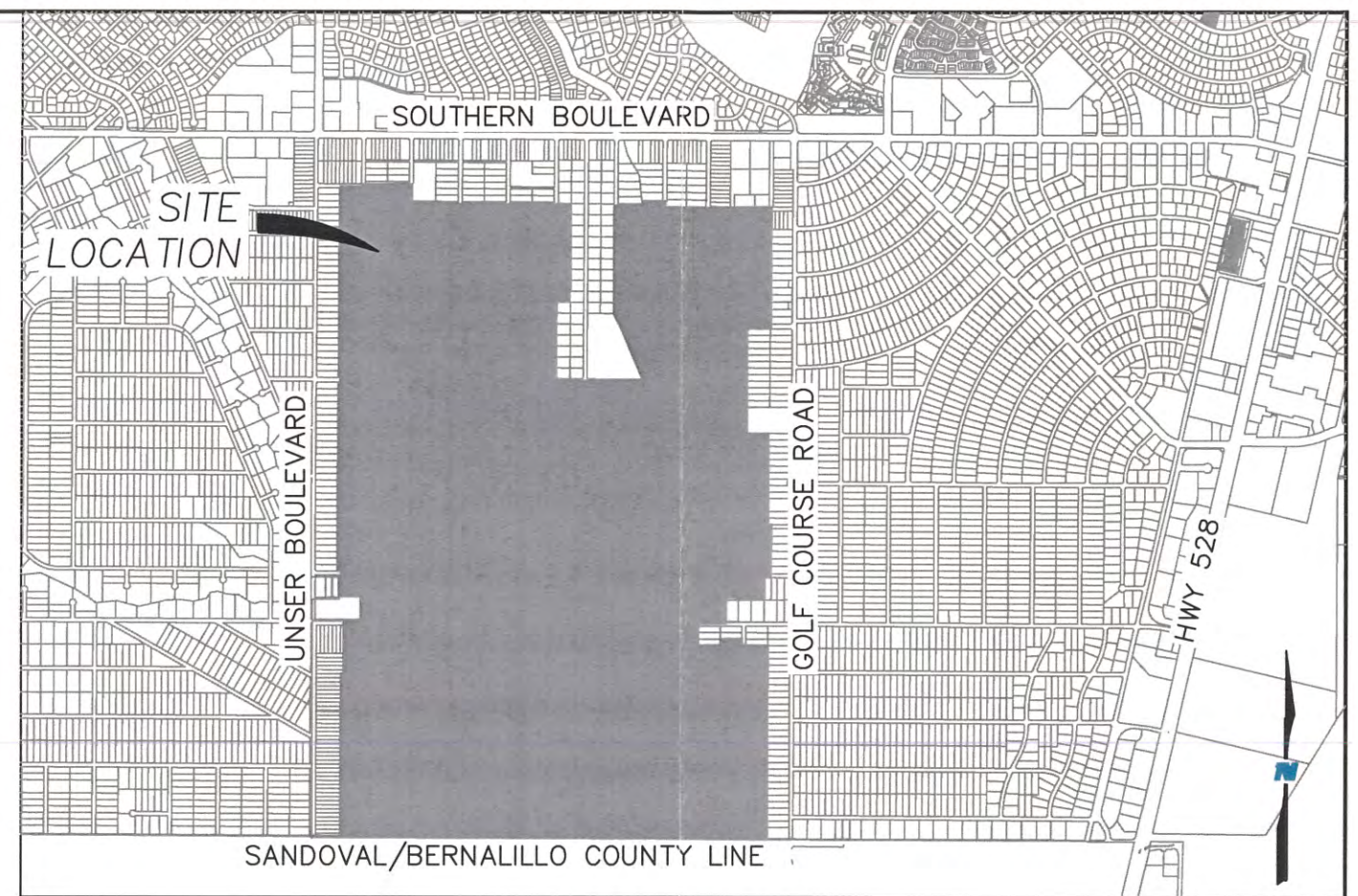
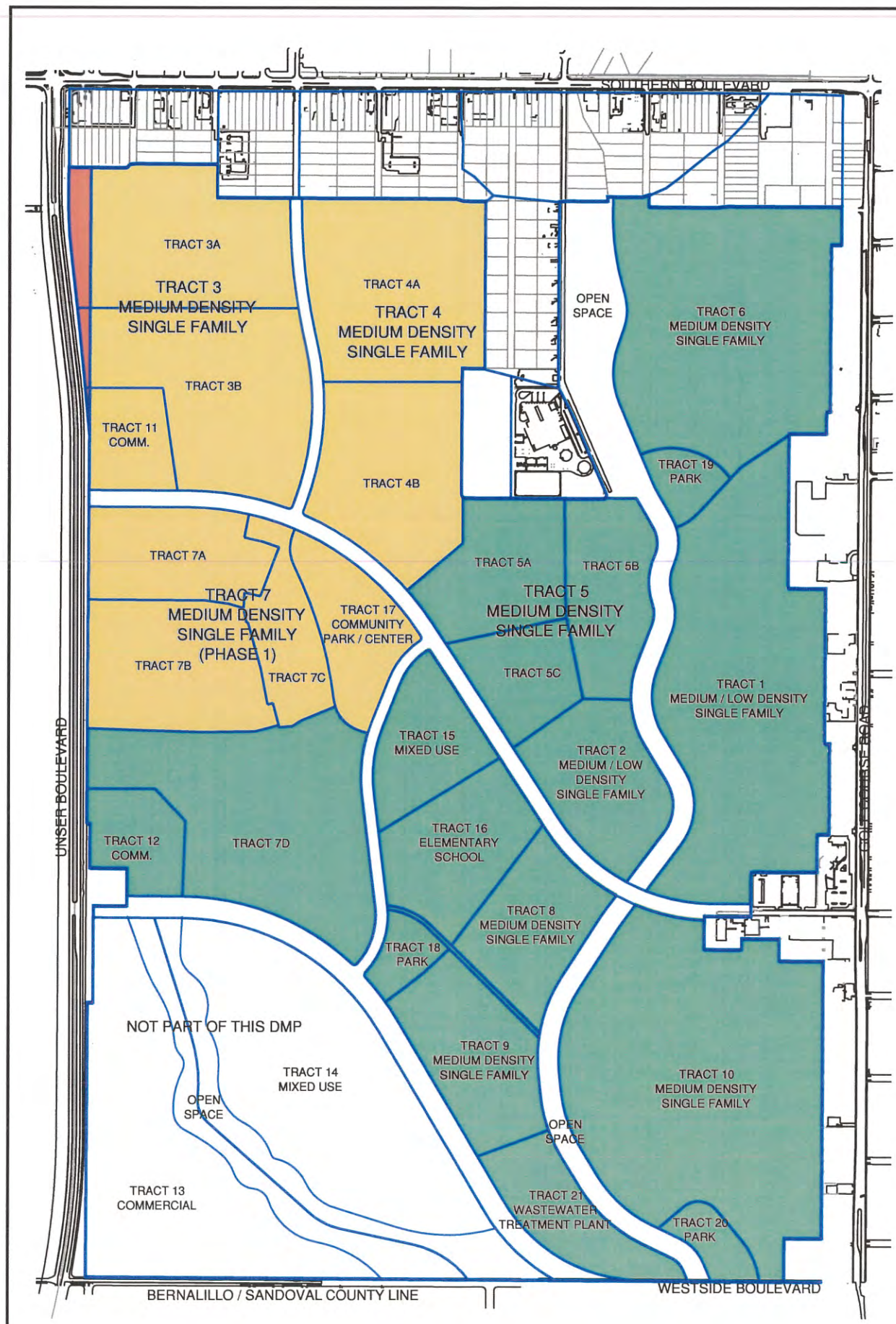
Table 4 - Comparison of Water Surface Elevations at Black Dam

Emergency Spillway Elevation	5168.55	Remaining Storage Depth Prior to Overflow
NOTE: All elevations in NAVD88		
MAX. WATER SURFACE ELEVATION for:	Elevation	
	(ft)	(ft)
BLWMP Ultimate Conditions Model	5167.02	1.53
Cabezon Model (Mod. BLWMP w/Ph 1 only)	5167.81	0.74
Cabezon Model (Mod. BLWMP w/Ph 1 and 2)	5165.13	3.42

The Cabezon Model (Phase 1) shows a water surface elevation of 5167.81 feet, an increase of 0.79 feet, leaving 0.74 feet of freeboard. Finally, the Cabezon Phase 2 Model has a water surface elevation of 5165.13 feet. This lowers the water surface by 1.89 feet, as compared to the Modified BLWMP Model.




This is accomplished by the addition of the two large detention ponds, the Phase 1 pond in Tract 17 and the Water Quality Structure adjacent to the Black Dam. Together, these facilities increase storage in the watershed by approximately 50 AF. Just as with the Tract 17 pond, the Office of the State Engineer must also approve the facility, and preliminary contact has already been made.


Together, these facilities should not only improve the quality of runoff from the Black Arroyo Watershed, but also increase the capacity of the Black Dam. This will result in a lower water surface elevation at the Dam. Therefore, the improvements outlined in this document will protect the Cabezon Communities from flooding and erosion damage, and will further safeguard the entire watershed.

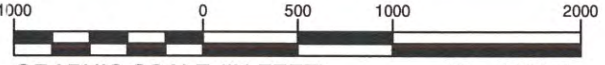





VICINITY MAP

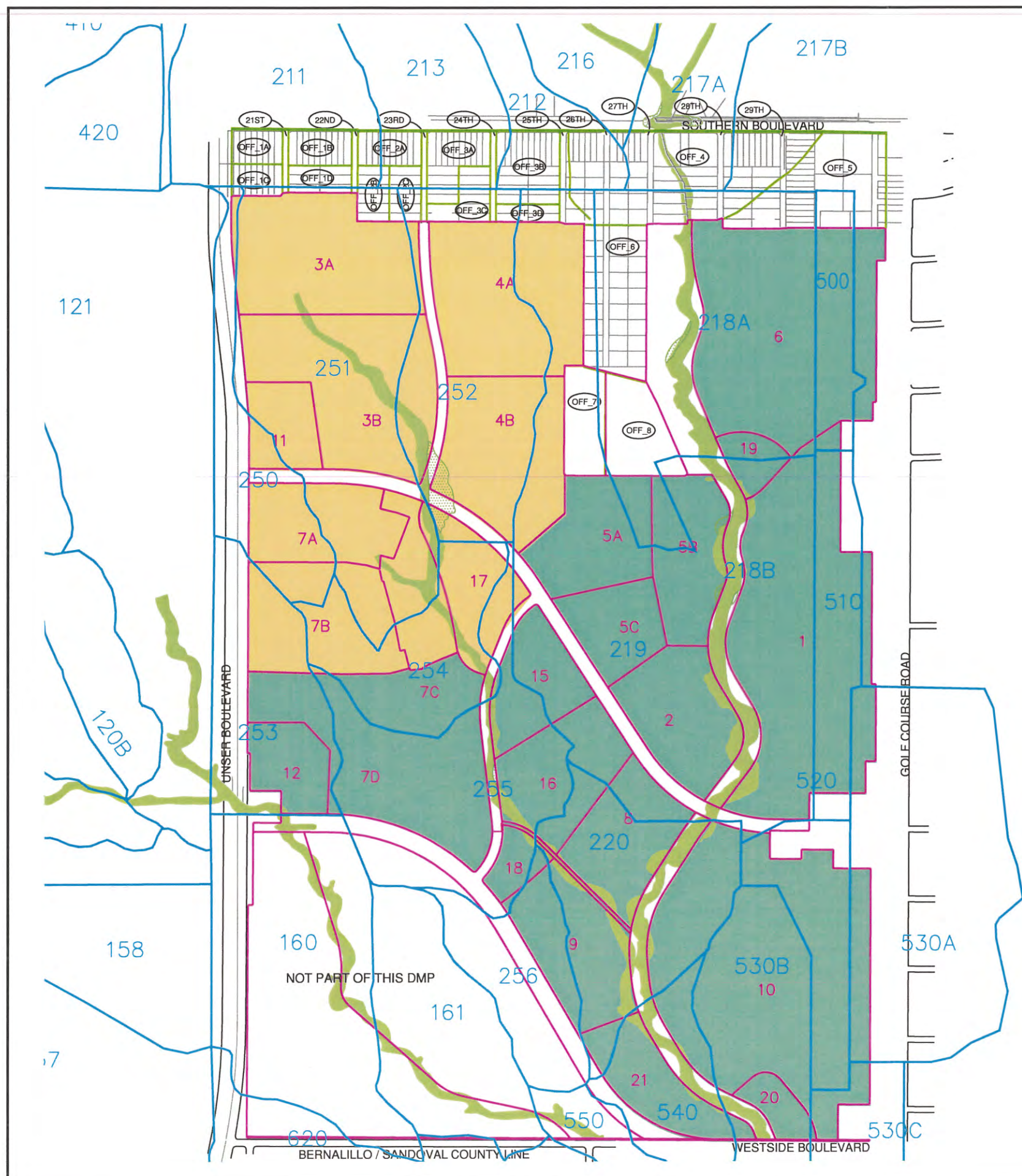
LEGEND

	ALTERNATE
	PHASE 1
	PHASE 2




GRAPHIC SCALE (IN FEET) 1" = 1000 ft.

	CITY OF RIO RANCHO	
 WILSON & COMPANY 2600 THE AMERICAN ROAD S.E. SUITE 100 RIO RANCHO, NEW MEXICO 87124 (505) 898-8021	FIGURE 1 CABEZON - PHASE 2 DRAINAGE MANAGEMENT PLAN	
	CABEZON VICINITY MAP	



LEGEND

SPECIAL FLOOD HAZARD AREAS
INUNDATED BY 100-YEAR FLOOD (ZONE AE)
AS DEFINED BY FEMA

OTHER FLOOD AREAS
(AREAS OF 500 YEAR FLOOD)

NOTE: TAKEN FROM FLOOD INSURANCE RATE MAP (FIRM)
MAP NUMBER: 35043C0894 C
EFFECTIVE DATE: JULY 16, 1996

CABEZON PHASE 1

CABEZON PHASE 2

CABEZON SITE BOUNDARY

CABEZON SUB-BASIN BOUNDARY

BLWMP SUB-BASIN BOUNDARY

CABEZON OFF-SITE SUB-BASIN BOUNDARY

17

CABEZON TRACT/SUB-BASIN LABEL

254

BLWMP SUB-BASIN LABEL

OFF_5

CABEZON OFF-SITE SUB-BASIN LABEL

10000
0
500
1000
2000
GRAPHIC SCALE (IN FEET)
1" = 1000 ft.

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FIGURE 2
CABEZON - PHASE 2
DRAINAGE MANAGEMENT PLAN
BLWMP SUB-BASINS
THAT OVERLAP CABEZON



PHASE 1
PHASE 2

EXISTING SD LINE
PROPOSED SD LINE

WQ/DETENTION FACILITY BOUNDARY

SITE/SUB-BASIN BOUNDARY

EAST BRANCH CONCRETE CHANNEL



CITY OF RIO RANCHO

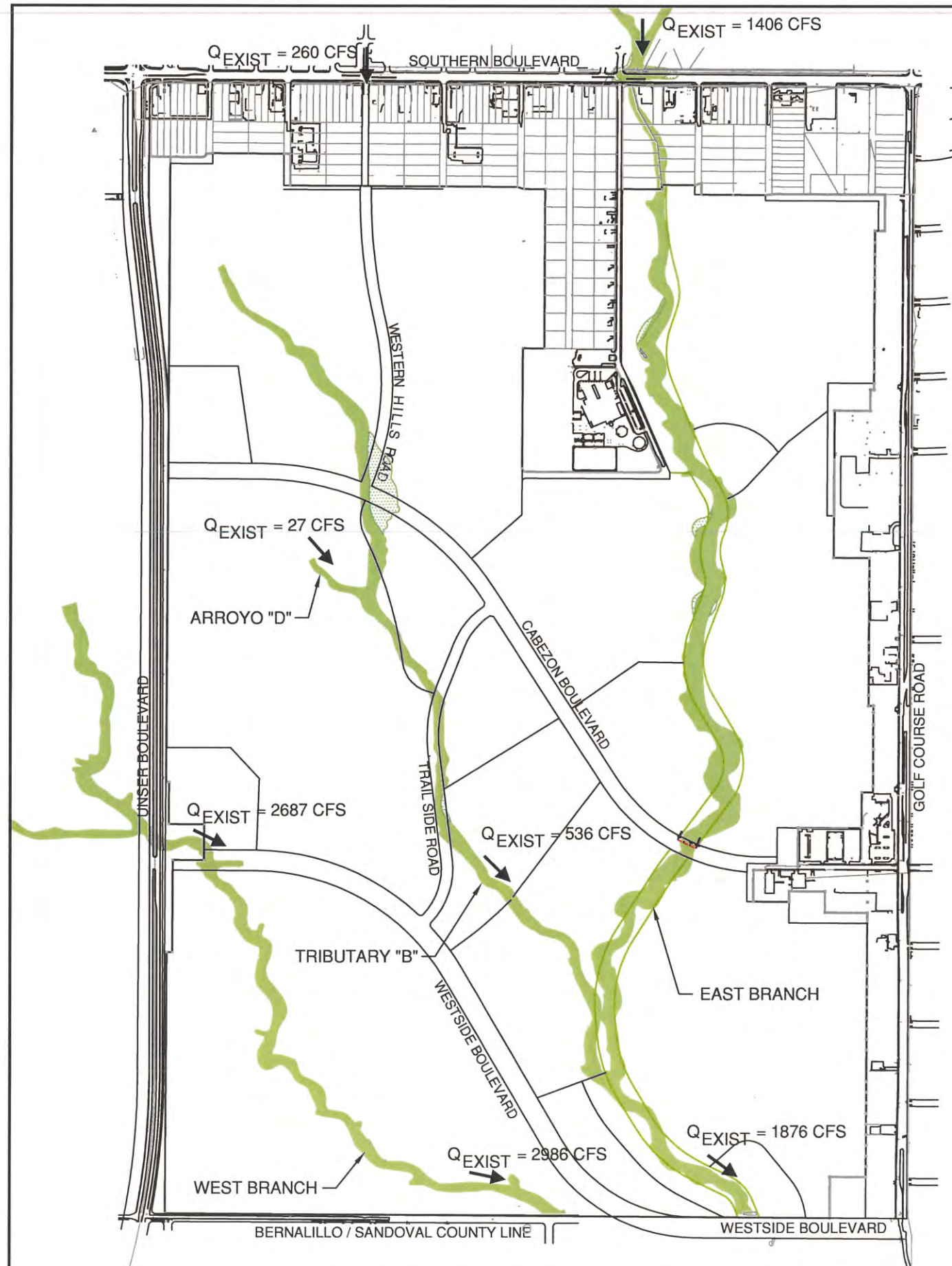


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FIGURE 3

CABEZON - PHASE 2
DRAINAGE MANAGEMENT PLAN

PROPOSED
IMPROVEMENTS



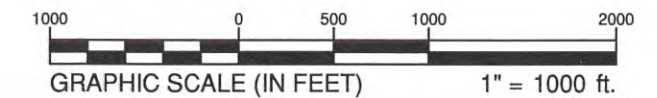
LEGEND

- SPECIAL FLOOD HAZARD AREAS
INUNDATED BY 100-YEAR FLOOD (ZONE AE)
AS DEFINED BY FEMA
- OTHER FLOOD AREAS
(AREAS OF 500 YEAR FLOOD)

NOTE: TAKEN FROM FLOOD INSURANCE RATE MAP (FIRM)
MAP NUMBER: 35043C0894 C
EFFECTIVE DATE: JULY 16, 1996

NOTE

EXISTING FLOWS BASED ON FLOOD INSURANCE STUDY
PERFORMED BY RESOURCE TECHNOLOGY INC., 1994



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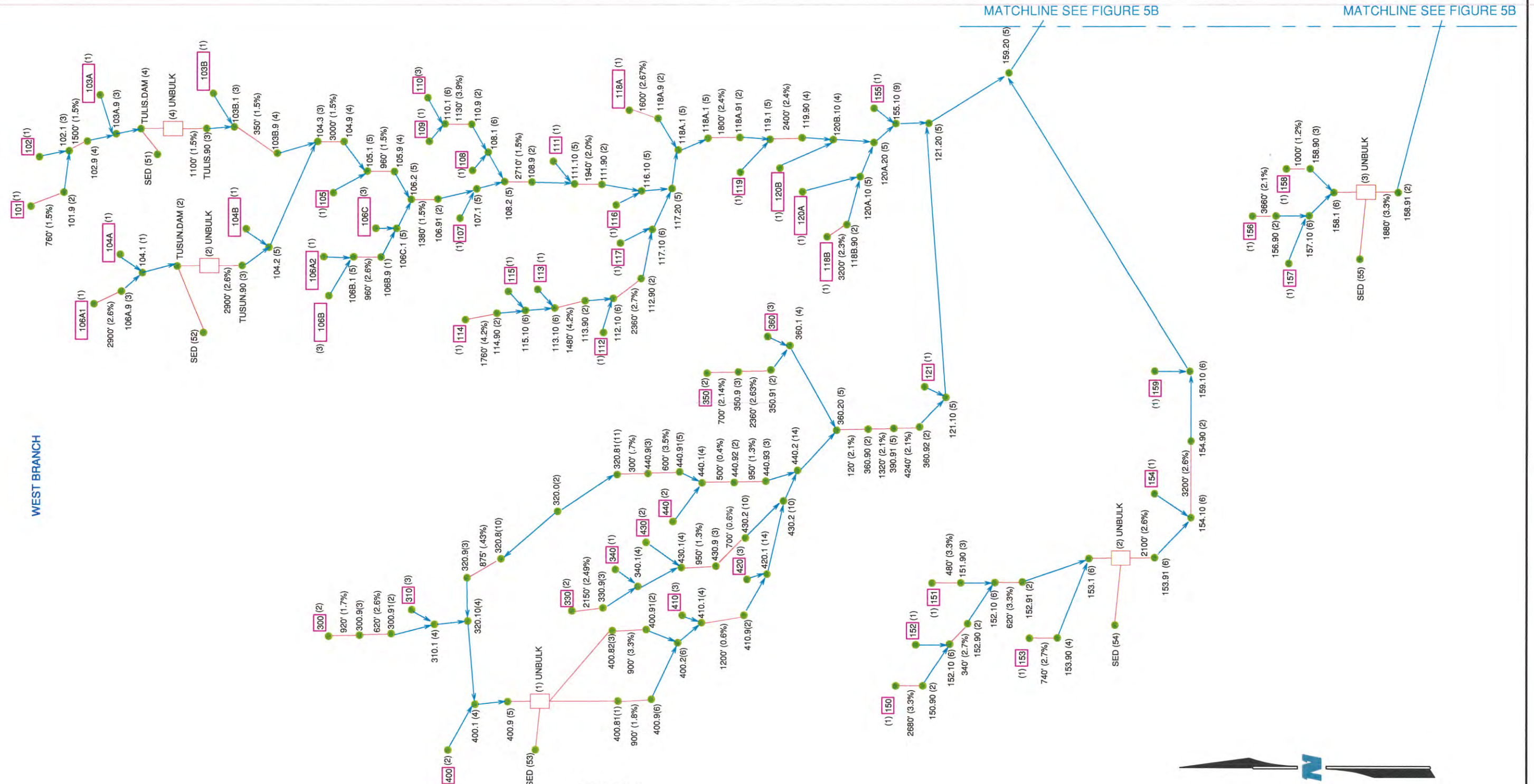


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FIGURE 4
CABEZON - PHASE 2
DRAINAGE MANAGEMENT PLAN

EXISTING FLOWS &
FEMA FLOOD PLAINS

WEST BRANCH



LEGEND



ADD



ROUTE

11

COMPUTE HYD

3.10 (4)

HYD ID

HYD NAME



DETENTION BASIN



WQ SEDIMENT BASIN



DIVIDE HYD



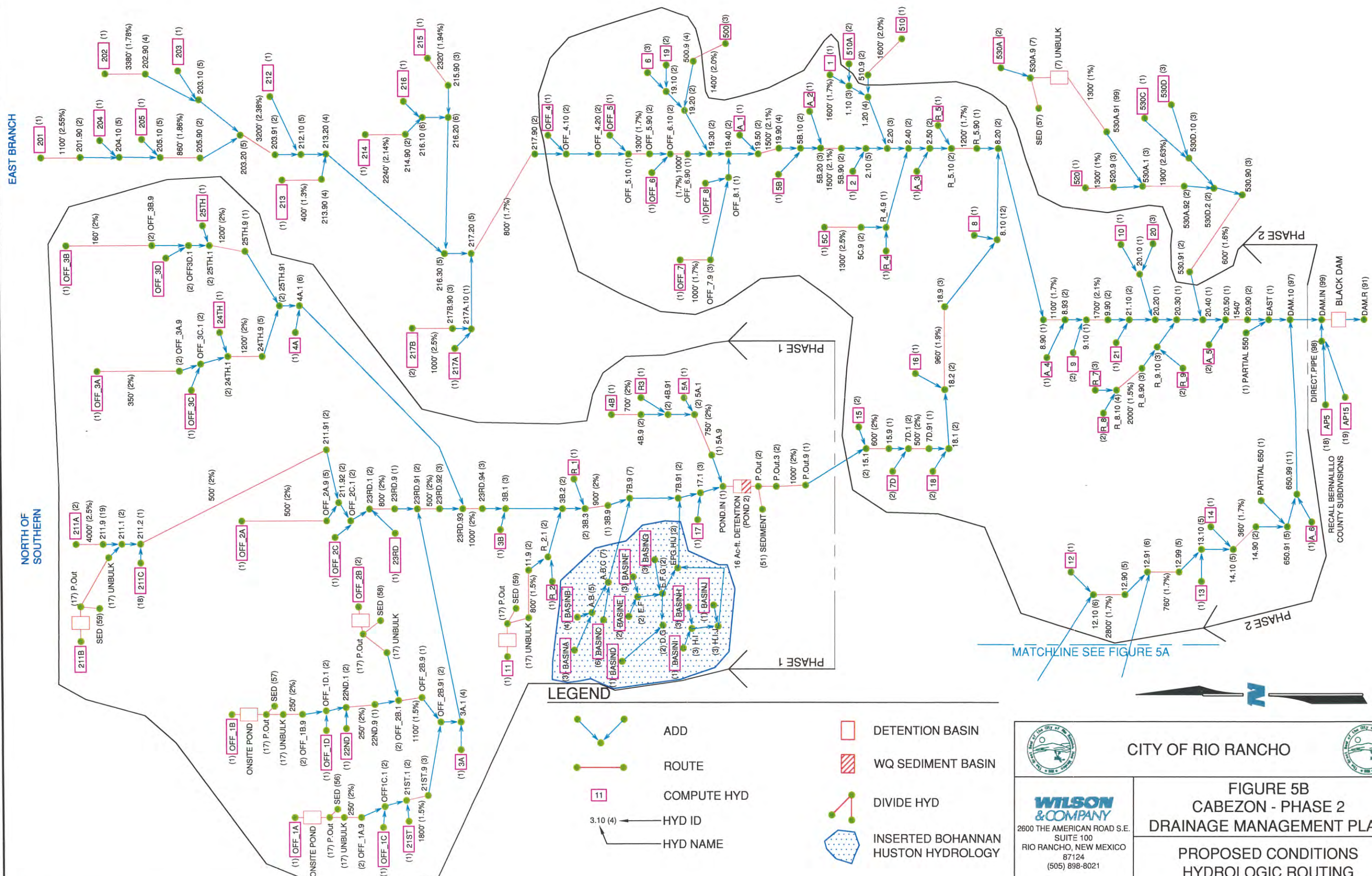
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FIGURE 5A
CABEZON - PHASE 2
DRAINAGE MANAGEMENT PLAN

PROPOSED CONDITIONS
HYDROLOGIC ROUTING



EAST BRANCH

NORTH OF SOUTHERN

LEGEND

- ADD
- ROUTE
- COMPUTE HYD
- HYD ID
- HYD NAME
- DETENTION BASIN
- WQ SEDIMENT BASIN
- DIVIDE HYD
- INSERTED BOHANNAN HUSTON HYDROLOGY

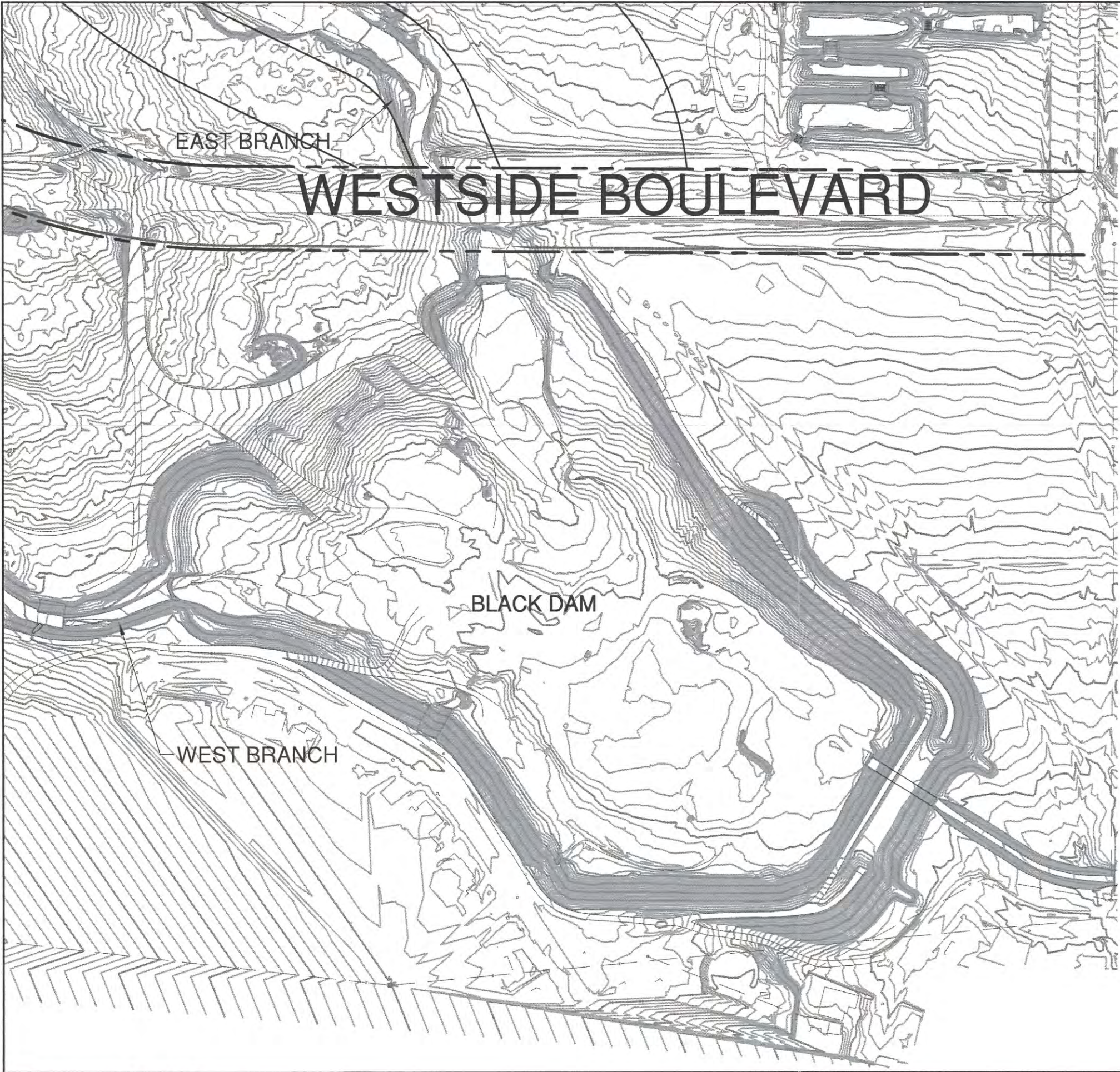


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FIGURE 5B
CABEZON - PHASE 2
DRAINAGE MANAGEMENT PLAN

PROPOSED CONDITIONS
HYDROLOGIC ROUTING

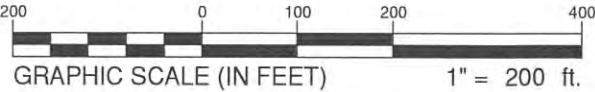


STORAGE RATING CURVE TABLE

Elevation (feet)	Incremental Volume (cubic feet)	Cumulative Volume (cubic feet)	Acre-Feet (feet)	Surface Area (square feet)
5148.00	2902.10	2902.10	0.10	8935.60
5149.00	207701.40	210603.50	4.80	205637.90
5150.00	220139.60	430743.10	9.90	319357.00
5151.00	393872.70	824615.70	18.90	451569.50
5152.00	406166.30	1230782.00	28.30	494995.40
5153.00	451813.90	1682595.80	38.60	530895.70
5154.00	500511.30	2183107.10	50.10	572649.40
5155.00	543290.50	2726397.60	62.60	603091.20
5156.00	581581.60	3307979.20	75.90	633021.10
5157.00	617944.30	3925923.60	90.10	670280.10
5158.00	655630.60	4581554.10	105.20	712476.40
5159.00	693088.10	5274642.20	121.10	752977.90
5160.00	723941.80	5998584.00	137.70	771818.90
5161.00	747001.30	6745585.30	154.90	788731.90
5162.00	767851.00	7513436.30	172.50	808768.80
5163.00	788759.50	8302195.80	190.60	828446.70
5164.00	811694.80	9113890.60	209.20	857403.10
5165.00	832995.70	9946886.30	228.30	889818.60
5166.00	853634.40	10800520.80	247.90	914272.00
5167.00	876263.40	11676784.10	268.10	936044.60
5168.00	896379.80	12573163.90	288.60	952232.30
5168.25	226971.30	12800135.30	293.90	956111.60

*ELEVATIONS IN NAVD88

SPILLWAY



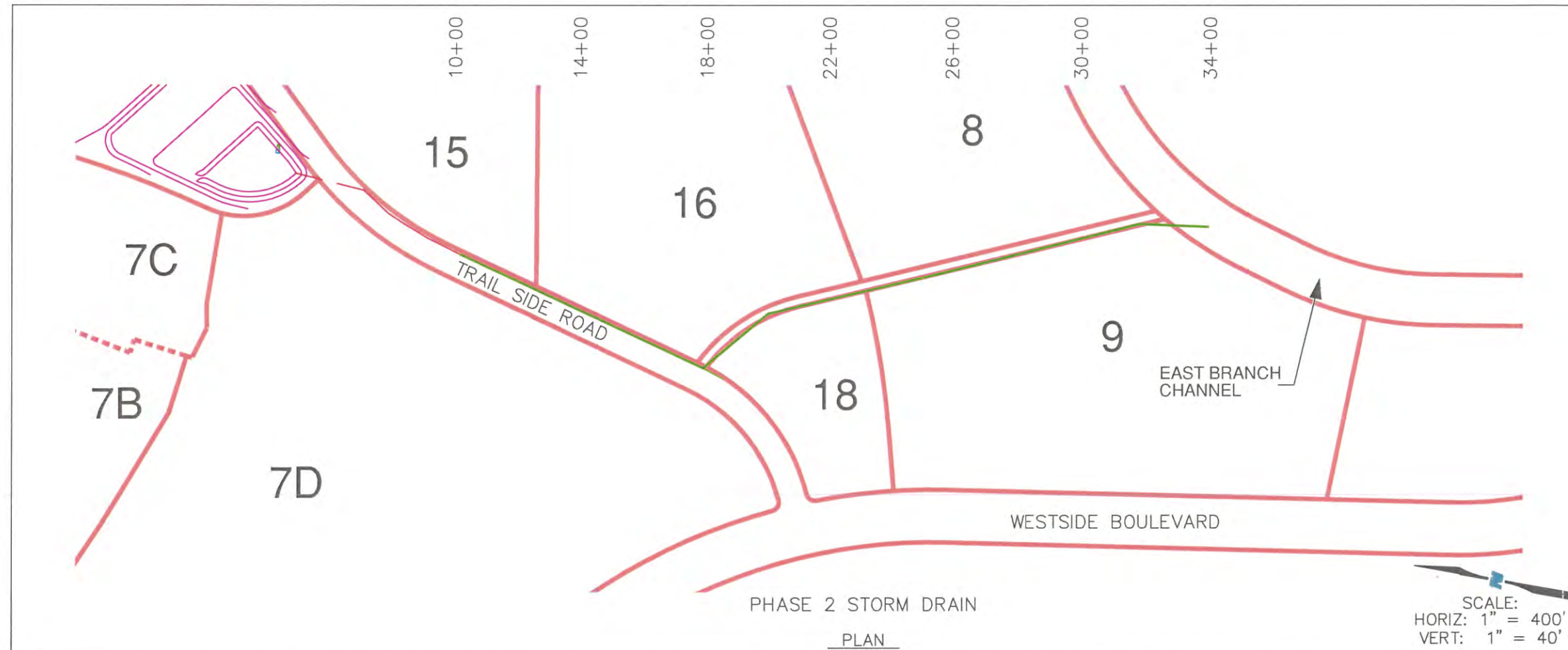
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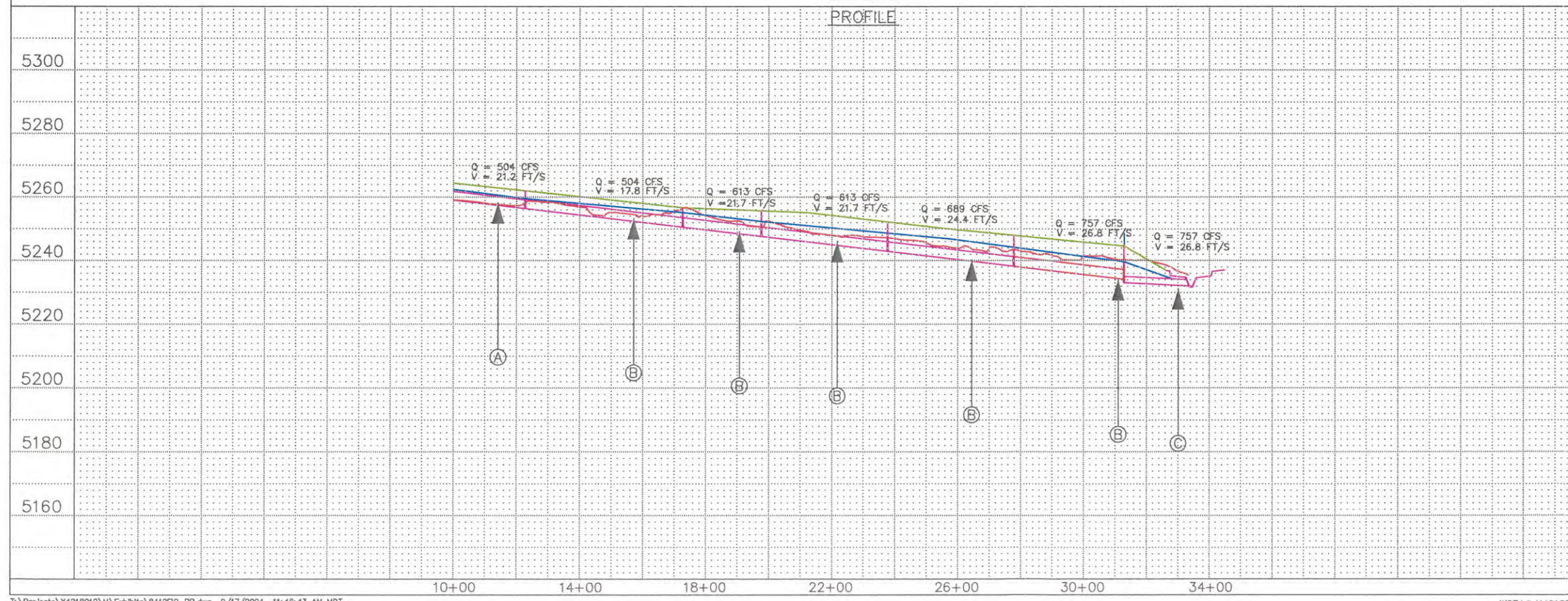
FIGURE 7
CABEZON - PHASE 2
DRAINAGE MANAGEMENT PLAN

BLACK DAM
CURRENT TOPOGRAPHY



- LEGEND (PLAN)
- STORM DRAIN
 - POND EXTENTS
 - EXISTING STORM DRAIN

- KEYED NOTES:
- Ⓐ 66" STORM DRAIN @ 2.42%
 - Ⓑ 72" STORM DRAIN @ 2.80% - 1.94%
 - Ⓒ 2 - 40" X 65" STORM DRAIN @ 0.54%



- LEGEND (PROFILE)
- STORM DRAIN
 - EXISTING GRADE
 - HYDRAULIC GRADE LINE
 - FINISH GRADE (APPROXIMATE)

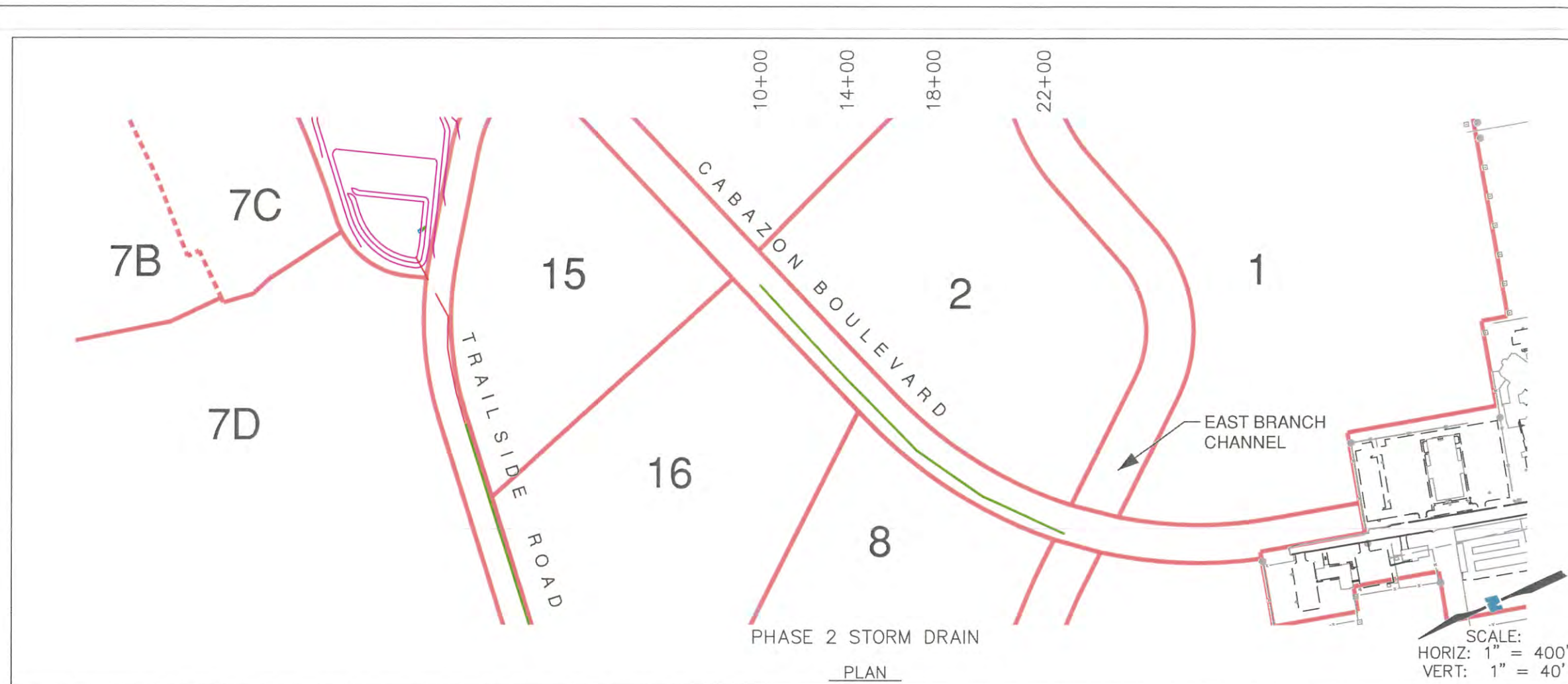
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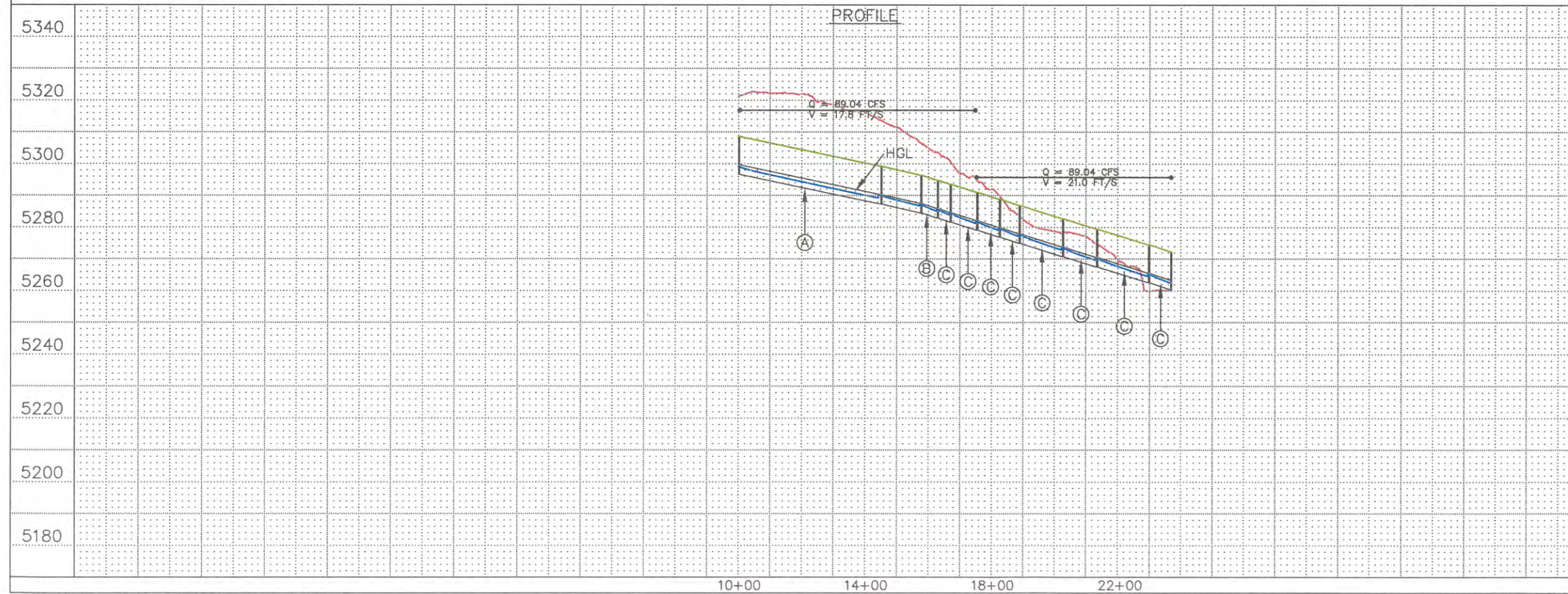
FIGURE 8
CABEZON-PHASE 2
DRAINAGE MANAGEMENT PLAN

PHASE 2 STORM DRAIN
STA 10+00 TO STA 34+06.11



- LEGEND (PLAN)**
- STORM DRAIN
 - POND EXTENTS
 - EXISTING STORM DRAIN

- KEYED NOTES:**
- Ⓐ 36" STORM DRAIN @ 2.1%
 - Ⓑ 36" STORM DRAIN @ 2.2%
 - Ⓒ 36" STORM DRAIN @ 3.0%



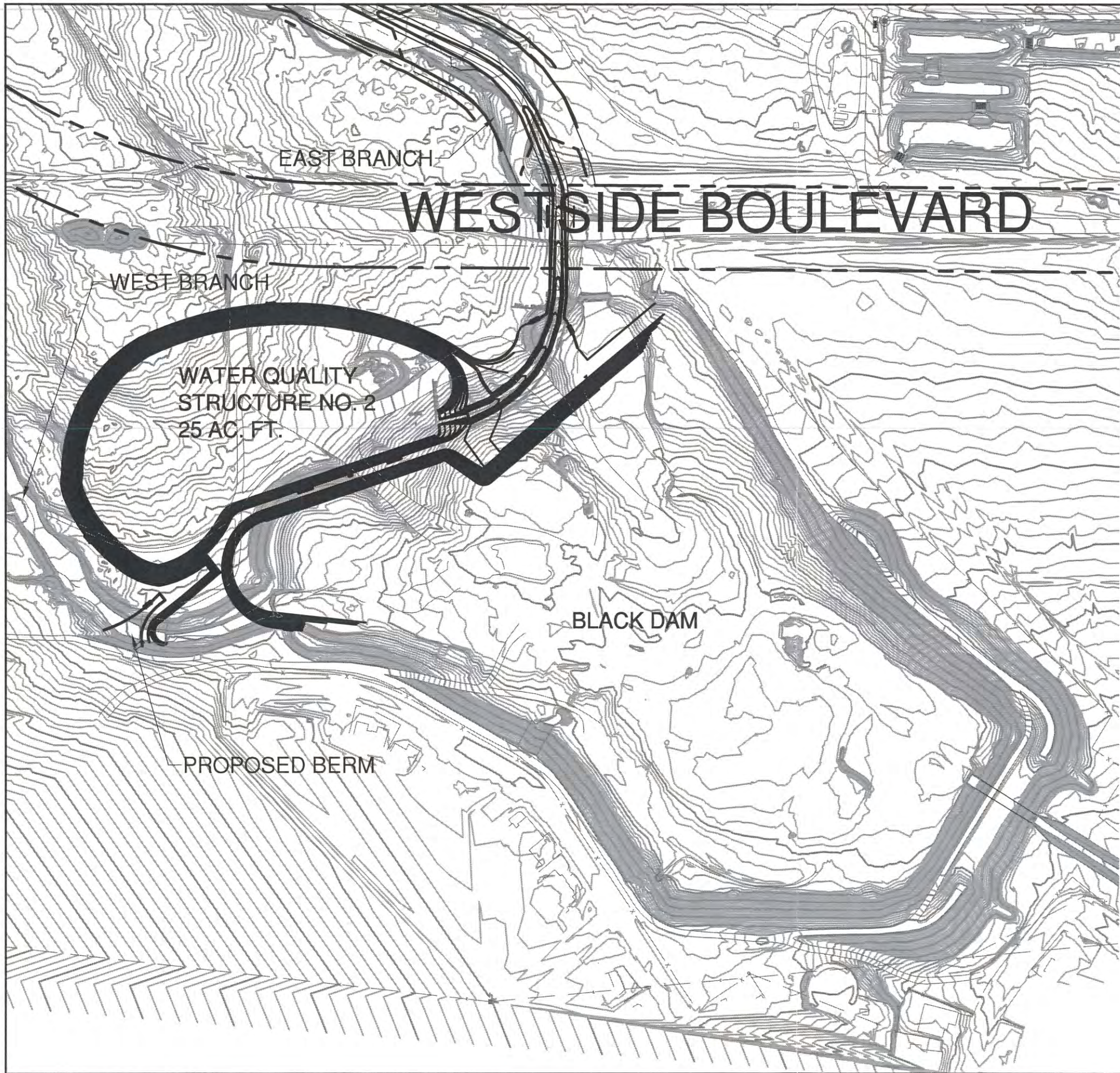
- LEGEND (PROFILE)**
- STORM DRAIN
 - EXISTING GRADE
 - HYDRAULIC GRADE LINE
 - FINISH GRADE (APPROXIMATE)

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**FIGURE 9
 CABEZON-PHASE 2
 DRAINAGE MANAGEMENT PLAN**

**PHASE 2 STORM DRAIN
 STA 10+00 TO STA 23+67.59**

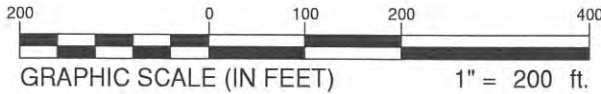


STORAGE RATING CURVE TABLE

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5149.00	207701.40	210603.50	4.80	205637.90
5150.00	220139.60	430743.10	9.90	319357.00
5151.00	393872.70	824615.70	18.90	451569.50
5152.00	406166.30	1230782.00	28.30	494995.40
5153.00	451813.90	1682595.80	38.60	530895.70
5154.00	500511.30	2183107.10	50.10	572649.40
5155.00	543290.50	2726397.60	62.60	603091.20
5156.00	581581.60	3307979.20	75.90	633021.10
5157.00	617944.30	3925923.60	90.10	670280.10
5158.00	655630.60	4581554.10	105.20	712476.40
5159.00	693088.10	5274642.20	121.10	752977.90
5160.00	723941.80	5998584.00	137.70	771818.90
5161.00	747001.30	6745585.30	154.90	788731.90
5162.00	767851.00	7513436.30	172.50	808768.80
5163.00	788759.50	8302195.80	190.60	828446.70
5164.00	811694.80	9113890.60	209.20	857403.10
5165.00	832995.70	9946886.30	228.30	889818.60
5166.00	853634.40	10800520.80	247.90	914272.00
5167.00	876263.40	11676784.10	268.10	936044.60
5168.00	896379.80	12573163.90	288.60	952232.30
5168.25	226971.30	12800135.30	293.90	956111.60

*ELEVATIONS IN NAVD88

SPILLWAY

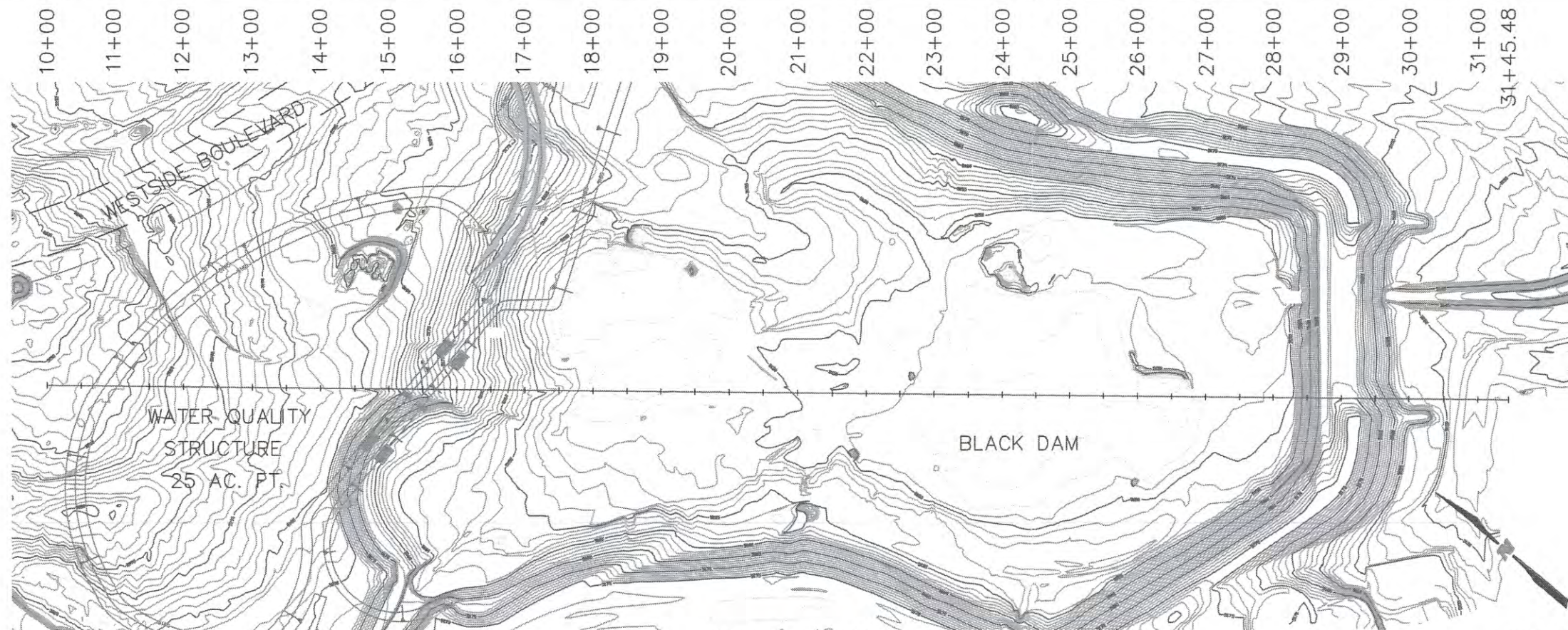


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FIGURE 10
CABEZON - PHASE 2
DRAINAGE MANAGEMENT PLAN
BLACK DAM
PROPOSED WATER QUALITY
STRUCTURE



WATER QUALITY STRUCTURE

PLAN
PROFILE

SCALE:
HORIZ: 1" = 200'
VERT: 1" = 40'

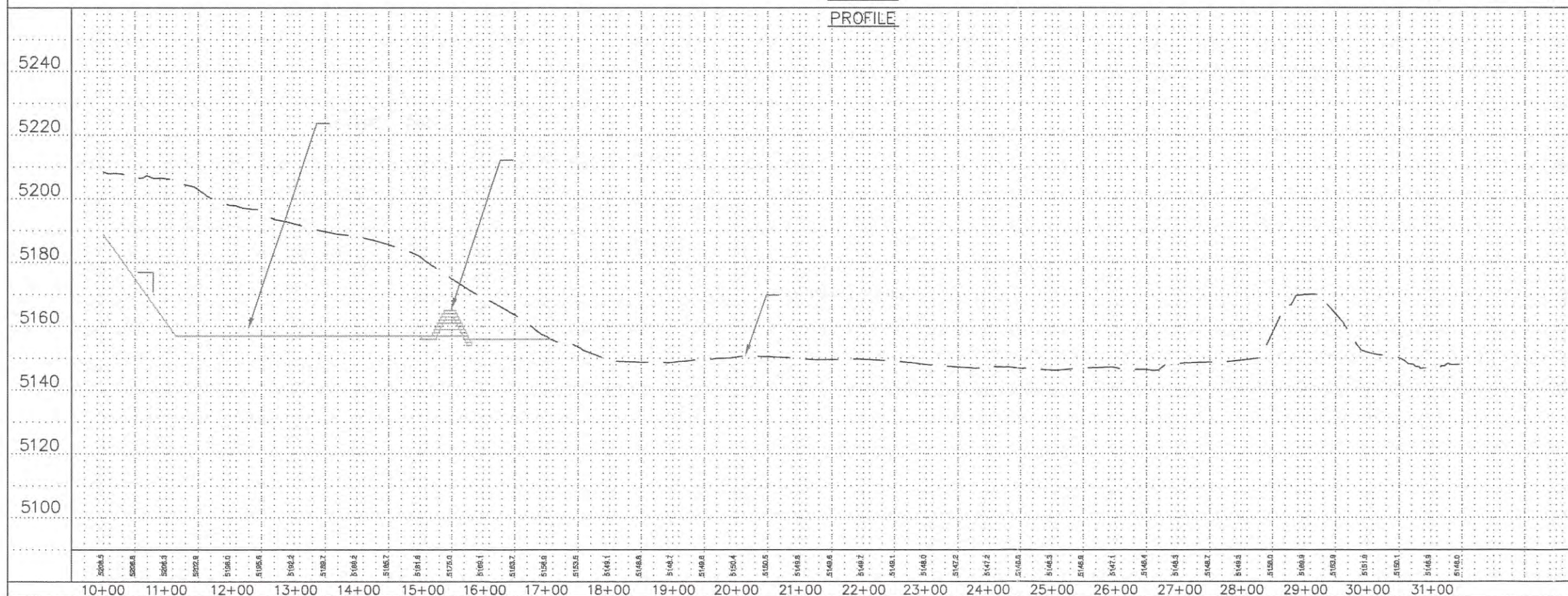
LEGEND (PLAN)

— POND EXTENTS

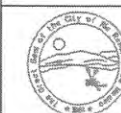
LEGEND (PROFILE)

--- EXISTING GRADE

— FINISH GRADE (APPROXIMATE)



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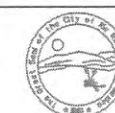
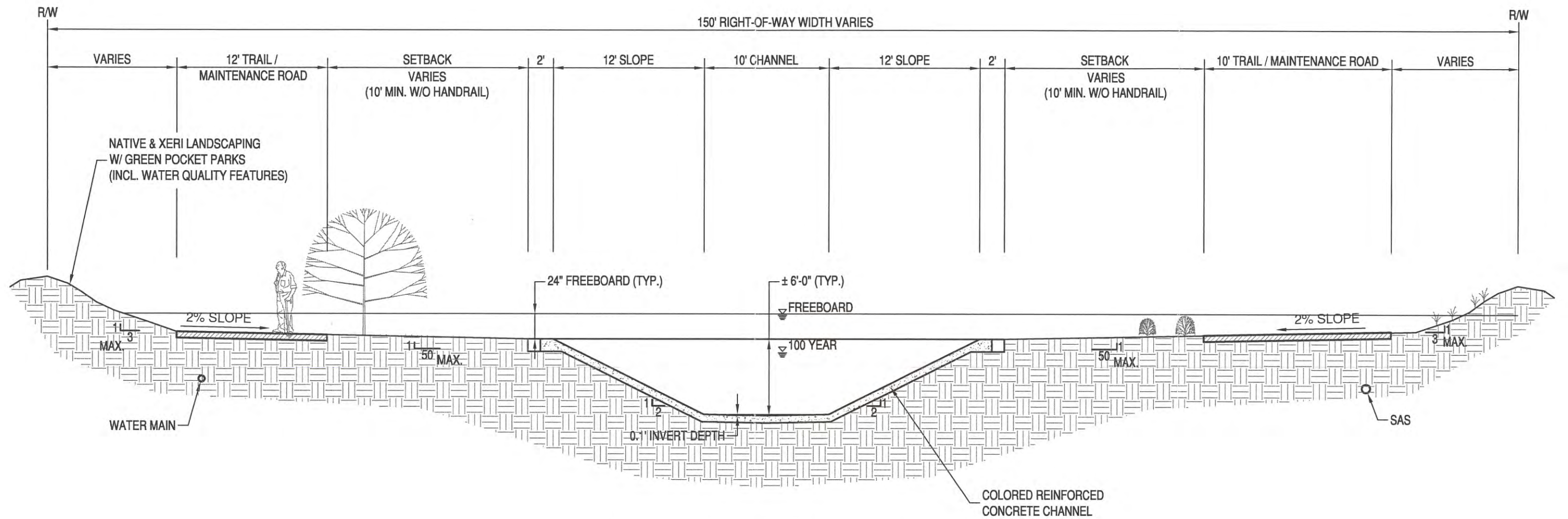


FIGURE 11
CABEZON-PHASE 2
DRAINAGE MANAGEMENT PLAN

WATER QUALITY STRUCTURE
STA 10+00 TO STA 31+45.48



NATURALIZED COMPOSITE CHANNEL SECTION
 SCALE: NTS
 (CHANNEL MEANDERS WITHIN R-O-W)



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FIGURE 12
CABEZON - PHASE 2
DRAINAGE MANAGEMENT PLAN
BLACK ARROYO EAST BRANCH
TYPICAL CHANNEL SECTION

APPENDIX A

Hydrology

QP81604.SUM												
ADD HYD	103B.10	1&3	3	.84018	165.89	6.610	.14751	1.520	.309			
*S ROUTE 103B.10 THRU 104B TO 103B.90	103B.90	3	4	.84018	165.68	6.603	.14736	1.520	.308	CCODE =	.2	
*S												
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID	TO ID	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	2	NOTATION
*S START OF SUNSET CHANNEL												
SEDIMENT BULK	106A1	-	1	.11660	174.60	7.012	1.12758	1.570	2.340	PK BF =	1.06	
ROUTE MCUNGE	106A.90	1	3	.11660	174.55	7.006	1.12660	1.600	2.339	CCODE =	.2	
ROUTE MCUNGE	104A	-	1	.18340	383.74	20.084	1.33762	1.520	3.269	PER IMP=	45.00	
ADD HYD	104.10	3&1	1	.30000	524.32	20.090	1.25560	1.540	2.731			
*S												
*S ROUTE 104.10 THROUGH PROPOSED SUNSET @ TULIP POND/DAM												
*S												
ROUTE RESERVOIR TUSON DAM	1	2		30000	4.28	1.507	.09419	3.570	.022	AC-FT=	18.814	
*S												
DIVIDE HYD	UNBULK	2		.29100	4.15	1.462	.09419	3.570	.022			
*S												
ROUTE IN PIPE TO LISBON CHANNEL	2	3		.29100	4.15	1.428	.09202	3.650	.022	CCODE =	.2	
ROUTE MCUNGE	104B	-	1	.03550	74.14	2.533	1.33768	1.520	3.263	PK BF =	1.06	
SEDIMENT BULK	104.20	1&3	5	.32650	74.28	3.961	.22746	1.520	.355	PER IMP=	45.00	
ADD HYD	*S LISBON CHANNEL AFTER SUNSET CHANNEL											
ROUTE MCUNGE	104.30	5&4	3	1.16668	239.96	10.564	.16978	1.520	.321	CCODE =	.2	
SEDIMENT BULK	104.90	3	4	1.16668	239.73	10.491	.16861	1.560	.321	PK BF =	1.06	
ROUTE MCUNGE	105.00	-	1	.15090	235.54	11.059	1.37411	1.620	2.439	PER IMP=	44.00	
ADD HYD	*S LISBON CHANNEL AFTER SUB-BASIN 105											
ROUTE MCUNGE	105.10	1&4	5	1.31758	461.84	21.550	.30667	1.580	.548	CCODE =	.2	
*S							.30630	1.590	.548	CCODE =	.2	
*S START OF SUGAR CHANNEL AT TULIP												
*S												
ROUTE MCUNGE	106A2	-	1	.13590	231.95	8.178	1.12830	1.540	2.667	PER IMP=	33.00	
SEDIMENT BULK	106A2	-	1	.13590	231.95	8.178	1.12830	1.540	2.667	PER IMP=	33.00	
*S BALI CHANNEL												
*S												
ROUTE MCUNGE	106B	-	3	.15220	267.63	10.944	.30667	1.580	.548	CCODE =	.2	
*S							.30630	1.590	.548	CCODE =	.2	
*S SUGAR CHANNEL INCLUDING CONFLUENCE WITH BALI CHANNEL												
ADD HYD	106B.10	1&3	5	.28810	494.45	19.122	1.24448	1.550	2.682			
ROUTE MCUNGE	106C.90	(TO CONFLUENCE OF LISBON & SUGAR CHLS)										
ROUTE MCUNGE	106B.90	5	1	.28810	494.44	19.117	1.24413	1.560	2.682	CCODE =	.2	
ADD HYD	106C	-	3	.04840	64.56	2.372	.91889	1.550	2.084	PER IMP=	22.00	
ROUTE MCUNGE	106C.10	1&3	5	.33650	558.92	21.488	1.19735	1.560	2.595			
*S												
*S AP 106.90												
*S												
*S LISBON CHANNEL AFTER CONFLUENCE WITH SUGAR CHANNEL												
ADD HYD	106.20	5&4	5	1.65408	1009.09	43.012	.48757	1.570	.953	CCODE =	.1	
ROUTE MCUNGE	106.91	5	2	1.65408	1007.70	42.964	.48702	1.600	.952	CCODE =	.1	
ROUTE MCUNGE	107.00	-	1	.03580	79.05	2.732	1.43071	1.520	3.450	PER IMP=	49.00	
*S												
*S LISBON CHANNEL AFTER ADDING SUB-BASIN 107												
*S												

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID	TO ID	NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION
ADD HYD	107.10	1& 2	5		1.68988	1068.93	45.696	.50702	1.590	.988		
COMPUTE NM HYD	109.00	-	1		.08640	146.45	6.552	1.42186	1.600	2.648	PER IMP=	49.00
*S												
*S	BALTIC CHANNEL											
*S	FLOW AT CASCADE RD @ 600 FT. W. OF COMANCHE RD. (HYD. 109)											
*S												
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID	TO ID	NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION
COMPUTE NM HYD	110.00	-	3		.05090	96.74	3.758	1.38444	1.550	2.970	PER IMP=	46.00
*S	ARKANSAS CHANNEL INCLUDING FLOW FROM BALTIC CHANNEL											
*S												
ADD HYD	110.10	1& 3	6		.13730	239.38	10.310	1.40799	1.580	2.724		
ROUTE MCUNGE	110.90	6	2		.13730	239.35	10.306	1.40739	1.590	2.724	CCODE =	.2
COMPUTE NM HYD	108.00	-	1		.06720	130.16	5.542	1.54624	1.570	3.026	PER IMP=	59.00
*S												
*S	ARKANSAS CHANNEL INCLUDING FLOW FROM BALTIC CHANNEL BEFORE CONFLUENCE											
*S	WITH LISBON CHANNEL											
*S	LISBON AVE. @ 250 FT. N. OF HOOD RD.											
*S												
ADD HYD	108.10	1& 2	6		.20450	368.93	15.848	1.45302	1.580	2.819		
*S	AP 108.91											
*S	LISBON CHANNEL AFTER ADDING ARKANSAS CHANNEL FLOWS											
*S												
ADD HYD	108.20	5& 6	5		1.89438	1437.01	61.543	.60914	1.590	1.185		
ROUTE MCUNGE	108.90	5	2		1.89438	1435.64	61.468	.60839	1.610	1.184	CCODE =	.2
COMPUTE NM HYD	111.00	-	1		.11590	214.48	9.107	1.47330	1.570	2.891	PER IMP=	54.00
*S												
*S	LISBON CHANNEL DISCHARGE @ SOUTHERN BLVD											
*S												
ADD HYD	111.10	1& 2	5		2.01028	1641.75	70.575	.65826	1.610	1.276		
*S												
*S	START OF LISBON ARROYO											
*S												
ROUTE MCUNGE	111.90	5	2		2.01028	1640.72	70.511	.65766	1.620	1.275	CCODE =	.2
SEDIMENT BULK											PK BF =	1.06
COMPUTE NM HYD	116.00	-	1		.03190	75.61	2.687	1.57953	1.520	3.703	PER IMP=	61.00
ADD HYD	116.10	1& 2	5		2.04218	1691.28	73.198	.67206	1.620	1.294		
*S												
*S	END LISBON CHANNEL AND LISBON ARROYO WATERSHED											
*S												
*S												
*S	START IVORY WATERSHED											
*S												
SEDIMENT BULK											PK BF =	1.06
*S	PECOS/RODEO CHANNEL											
COMPUTE NM HYD	114.00	-	1		.06980	126.88	4.917	1.32086	1.560	2.840	PER IMP=	41.00
ROUTE MCUNGE	114.90	1	2		.06980	126.67	4.912	1.31960	1.600	2.836	CCODE =	.1
*S												
*S	SPUR CHANNEL											
*S												
COMPUTE NM HYD	115.00	-	1		.12520	216.57	9.752	1.46049	1.600	2.703	PER IMP=	52.00
ADD HYD	115.10	1& 2	6		.19500	343.24	14.665	1.41005	1.600	2.750		
*S												
*S	IVORY CHANNEL											
*S												
COMPUTE NM HYD	113.00	-	1		.04770	107.66	3.867	1.52010	1.520	3.527	PER IMP=	57.00

OP81604.SUM

*S ADD THE TOTAL FLOW IN 20TH STREET AT THE NORTH SIDE OF SOUTHERN TO THE
*S TOTAL FLOW ROUTED TO THE INTERSECTION FROM THE NORTH AND THE WEST
*S THIS FLOW IS ROUTED UNDER SOUTHERN TO THE UNSEER CHANNEL

*S *****
ADD HYD 360.20 4814 5 57424 652.14 50.375
ROUTE MCUNGE 360.90 5 2 57424 652.14 50.375

*S CONCRETE LINED PORTION OF UNSEER CHANNEL
ROUTE MCUNGE 360.91 2 5 57424 651.95 50.342

*S EARTH LINED PORTION OF UNSEER CHANNEL
ROUTE MCUNGE 360.92 5 2 57424 650.85 50.196

SEDIMENT BULK
COMPUTE NM HYD 121.00 - 1 25810 541.88 23.545
ADD HYD 121.10 1& 2 5 83234 1086.71 73.740

*S *****
*S ***** CONFLUENCE OF UNSEER CHANNEL WITH WEST BRANCH ARROYO *****
*S *****

COMMAND HYDROGRAPH FROM TO PEAK DISCHARGE RUNOFF
ID NO. ID NO. (SQ MI) (CFS) (AC-FT)

ADD HYD 121.20 5& 9 5 3.97714 4554.17 226.004
*S *****
*S ***** START OF TRIBUTARY "A" *****
*S *****

COMPUTE NM HYD 153.00 - 1 14660 191.66 9.880
ROUTE MCUNGE 153.90 1 4 14660 191.67 9.877

COMPUTE NM HYD 150.00 - 1 08730 162.70 5.319
ROUTE MCUNGE 150.90 1 2 08730 162.53 5.315

COMPUTE NM HYD 152.00 - 1 19840 297.64 12.195
ADD HYD 152.10 1& 2 6 28570 453.53 17.510

ROUTE MCUNGE 152.90 6 2 28570 453.51 17.505
COMPUTE NM HYD 151.00 - 1 15130 286.88 9.701

ROUTE MCUNGE 151.90 1 3 15130 286.57 9.699
ADD HYD 152.10 2& 3 6 43700 729.64 27.204

ROUTE MCUNGE 152.91 6 2 43700 729.23 27.198
*S *****
*S ***** AP 153.10 *****

ADD HYD 153.10 4& 2 6 58360 884.06 37.075
*S *****

*S ROUTE HYD. THROUGH TRIBUTARY "A" DAM
*S *****

ROUTE RESERVOIR TRIBA.DAM 6 2 58360 3.58 1.233
*S *****
*S ***** DIVIDE HYD TO UNBULK BY 3% *****

UNBULK 2 2 56609 3.48 1.196
SEDIMENT and 54 01751 .037

ROUTE MCUNGE 153.91 2 6 56609 3.48 1.175
COMPUTE NM HYD 154.00 - 1 21910 357.58 13.089

ADD HYD 154.10 1& 6 6 78519 357.73 14.263
ROUTE MCUNGE 154.90 6 2 78519 357.31 14.231

COMPUTE NM HYD 159.00 - 1 06000 146.57 5.303
ADD HYD 159.10 1& 2 6 84519 479.84 19.534

*S *****
*S ***** CONFLUENCE OF TRIB. "A" WITH WEST BRANCH ARROYO *****
*S *****

*S BLACK ARROYO @ UNSEER BLVD. (WEST BRANCH)
*S *****
*S ***** BLWMP AP 159.20 *****

ADD HYD 159.20 5& 6 5 4.82233 5003.86 245.537
*S *****

*S PUNCH AND ADJUST HYDROGRAPH TO DELETE "FIRST FLUSH" RUNOFF AND SEND TO
*S WATER QUALITY PONDS WHICH IS ESSENTIALLY OUT OF THE SYSTEM THROUGH TIMING.
RECALL HYD 159.20 - 5 4.82230 5003.86 245.537

*S CABEZON REVISIONS PHASE 2 BEGIN HERE; BLWMP SUBBASINS 253,160 ARE REMOVED
*S 253 REPLACED BY CABEZON COMMERCIAL TRACT 12 (DRAINS TO WEST BRANCH)
*S AND 7A, 7B, 7C (ALL DRAIN TO POND IN TRACT 17 WHICH GOES TO EAST

1.64483 1.620 1.774 CCODE = .0
1.64483 1.620 1.774 CCODE = .0

1.64377 1.630 1.774 CCODE = .2
1.63899 1.710 1.771 CCODE = .2

1.71042 1.570 3.280 PK BF = 1.06
1.66114 1.630 2.040 PER IMP= 70.00

TIME TO CFS PAGE = 6
PEAK PER ACRE NOTATION
(HOURS) 1.620 1.789

1.06548 1.620 1.789
1.26361 1.660 2.043 PER IMP= 38.00
1.26328 1.670 2.043 CCODE = 32.00

1.14230 1.520 2.912 PER IMP= 32.00
1.14149 1.540 2.909 CCODE = 32.00

1.15248 1.580 2.344 PER IMP= 32.00
1.14913 1.560 2.480 CCODE = 32.00

1.14883 1.570 2.480 CCODE = 32.00
1.20217 1.530 2.963 PER IMP= 34.00

1.20191 1.530 2.959 CCODE = 34.00
1.16721 1.560 2.609 CCODE = 34.00

1.16695 1.560 2.607 CCODE = 34.00
1.19115 1.580 2.367 CCODE = 34.00

1.19115 1.580 2.367 CCODE = 34.00
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1.19115 1.580 2.367 CCODE = 34.00

QP81604.SUM

*S BRANCH); 160 IS WEST BRANCH, REPLACED BY A_6

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* S Commercial Unit 12
  COMPUTE NM HYD 12.00 - 1 .01560 43.14 1.592
  ADD HYD 12.10 1& 5 6 4.83790 5032.68 247.129
  ROUTE MCUNGE 12.90 6 4.83790 5031.78 246.904
* S BLWMP FILE RESUMES BELOW
  COMPUTE NM HYD 156.00 - 1 .22940 467.47 15.354
  ROUTE MCUNGE 156.90 1 2 .22940 465.95 15.337
  COMPUTE NM HYD 137.00 - 1 .18890 395.16 13.688
  ADD HYD 157.10 1& 2 6 .41830 849.19 29.025
  COMPUTE NM HYD 158.00 - 1 .08160 210.24 7.766
  ROUTE MCUNGE 158.90 1 3 .08160 210.24 7.761
  ADD HYD 158.10 3& 6 6 .49990 1057.67 36.786
* S UNDER GATEWAY DAM
  ROUTE RESERVOIR GATE.POND 6 3 .49990 622.62 36.697
* S *****DIVIDE HYD TO UNBULK BY 3% *****
  DIVIDE HYD UNBULK 3 3 .48490 603.94 35.596
  SEDIMENT and 55 .01500 18.68 1.101
  ROUTE MCUNGE 158.91 3 2 .48490 603.98 35.581
* S CABEZON REVISIONS PHASE 2 RESUME BELOW; BLWMP SUBBASINS 620,161 REMOVED

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COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE	NOTATION
*S 620 REPLACED BY OFFSITE TRACT 13, 161 REPLACED BY OFFSITE TRACT 14										7	
*S (ALL DRAIN TO WEST BRANCH); PART OF BLWMP 650 ALSO REMOVED											
*S THIS TAKES WEST BRANCH TO DAM											
ADD HYD 12.91 5& 2 6				5.32280	5612.00	282.486	.99508	1.630	1.647		.2
ROUTE MCUNGE 12.99 6 5				5.32280	5613.00	282.387	.99473	1.640	1.648		
*S ADJUST SEDIMENT BULK											
*S COMPUTE CABEZON SUBBASIN 13											
COMPUTE NM HYD 13.00 - 1				.07890	217.79	8.050	1.91294	1.510	4.313		PER IMP= 85.00
ADD HYD 13.10 1& 5 5				5.40170	5738.23	290.437	1.00814	1.640	1.660		
*S COMPUTE CABEZON SUBBASIN 14											
COMPUTE NM HYD 14.00 - 1				.09090	231.21	8.837	1.82276	1.520	3.974		PER IMP= 80.00
ADD HYD 14.10 1& 5 5				5.49260	5887.80	299.273	1.02162	1.630	1.675		
ROUTE MCUNGE 14.90 5 2				5.49260	5887.27	299.192	1.02135	1.640	1.675		CCODE = .1
*S Area of 650 is reduced by area that it overlaps											
*S CABEZON basins											
COMPUTE NM HYD 650.00 - 1				.03730	64.55	1.866	.93821	1.520	2.704		PER IMP= 9.00
ADD HYD 650.91 1& 2 5				5.52990	5928.51	301.059	1.02079	1.640	1.675		
*S WEST BRANCH ARROYO BETWEEN 13 AND 14, SOUTH FROM WESTSIDE BLVD											
COMPUTE NM HYD A_6 - 1				.04620	106.58	3.618	1.46839	1.510	3.605		PER IMP= 50.00
*S BLACK'S ARROYO (WEST BRANCH) @ DAM											
ADD HYD 650.99 1& 5 11				5.57610	5991.48	304.677	1.02450	1.640	1.679		
*S END OF THE BLACK'S ARROYO WEST BRANCH											
*S BEGINNING OF THE BLACK'S ARROYO EAST BRANCH											
*S End of West Branch- Beginning of East Branch											
*S THE FOLLOWING ARE CABEZON PHASE 1 REVISIONS											
*S BEGIN WITH CABEZON SUBBASINS THAT DRAIN TO WESTERN HILLS SD											
*S WHICH REPLACE TRIBUTARY B AND ARROYO D											
*S BLWMP SUBBASINS 251,252,250,254 REMOVED											
*S 251 REPLACED BY TRACTS 3A,3B; 252 REPLACED BY TRACTS 4A,4B;											
*S 250 REPLACED BY TRACTS 3B,11,7A; 254 REPLACED BY 17,7A,7C											
SEDIMENT BULK											
*S Following is the Northwest corner of offsites and Subbasin 3A											
*S It will be held on ID=4											
COMPUTE NM HYD off_1A - 1				.00540	14.95	.551	1.91298	1.510	4.324		PER IMP= 85.00

*S ROUTE OFF_1A through existing pond
 *S Pond Exists in field; volume and outflow assumed to
 *S limit flowrate to predevelopment level

```

ROUTE RESERVOIR      P.Out  1  17  .00540  5.19
*****DIVIDE HYD TO UNBULK BY 3% *****
DIVIDE HYD           UNBULK  17  17  .00524  5.03
                      SEDIMENT and 56  .00016  .16
ROUTE MCUNGE         OFF_1A.9  17  2  .00524  5.03
COMPUTE NM HYD       OFF_1C  -  1  .00540  11.21
ADD HYD              OFF1C.1  1& 2  2  .01064  15.26
COMPUTE NM HYD       21ST  -  1  .00100  2.83
ADD HYD              21ST.1  1& 2  2  .01164  18.07
ROUTE MCUNGE         21ST.9  2  3  .01164  18.08
COMPUTE NM HYD       OFF_1B  -  1  .00560  15.50
*****DIVIDE HYD TO UNBULK BY 3% *****
DIVIDE HYD           UNBULK  17  17  .00543  5.11
                      SEDIMENT and 57  .00017  .16

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*S ROUTE OFF_1B through existing pond
 *S Pond Exists in field; Total volume = 0.22 ac-ft
 *S limited flowrate to predevelopment level

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ROUTE RESERVOIR      P.Out  1  17  .00560  5.26
*****DIVIDE HYD TO UNBULK BY 3% *****
DIVIDE HYD           UNBULK  17  17  .00543  5.11
                      SEDIMENT and 57  .00017  .16

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□

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION
ROUTE MCUNGE	Off_1B.9	17	2	.00543	5.11	.554	1.91282	1.469	8	
COMPUTE NM HYD	Off_1D	-	1	.00470	8.90	.279	1.11394	2.959		CCODE =
ADD HYD	Off1D.1	1& 2	2	.01013	13.03	.832	1.54038	2.010		PER IMP= 27.00
COMPUTE NM HYD	22ND	-	1	.00100	2.83	.105	1.56588	4.423		PER IMP= 90.00
ADD HYD	22ND.1	1& 2	2	.01113	15.83	.937	1.57860	2.222		CCODE =
ROUTE MCUNGE	22ND.9	2	1	.01113	15.83	.937	1.57768	4.325		PER IMP= 85.00
COMPUTE NM HYD	Off_2B	-	2	.00470	13.01	.480	1.91299	1.510		
*S ROUTE OFF_2B through existing pond										
*S Pond Exists in field; Total volume = 0.18 ac-ft										
*S limited flowrate to predevelopment level										
ROUTE RESERVOIR	P.Out 2 17			.00470	4.90	.479	1.91284	1.629		AC-FT= .163
ROUTE RESERVOIR	UNBULK 17 17			.00456	4.75	.465	1.91282	1.629		
DIVIDE HYD	SEDIMENT and 58			.00014	.15	.014	1.91282	1.629		
ADD HYD	Off2B.1	1&17	2	.01569	20.06	1.401	1.67445	1.540		
ROUTE MCUNGE	Off2B.9	2	1	.01569	20.08	1.398	1.67014	1.600		CCODE = .2
*S ADD 21ST and 22ND STS offsite routed flows										
ADD HYD	Off2B.91	1& 3	2	.02733	38.07	2.393	1.64154	2.177		
COMPUTE NM HYD	Off2B.3A	-	1	.03440	125.52	4.343	1.49678	3.605		PER IMP= 55.40
ADD HYD	3A.1	1& 2	4	.08173	144.75	6.735	1.54519	2.767		
*S Area coming down 24th to project										
COMPUTE NM HYD	Off_3A	-	1	.00880	24.34	.898	1.91297	4.322		PER IMP= 85.00
*S Use roadway cross-section to route off_3A thru off_3c although there is										
*S not one presently there										
ROUTE MCUNGE	Off3A.9	1	2	.00880	24.32	.897	1.91128	4.318		CCODE =
COMPUTE NM HYD	Off_3C	-	1	.00630	11.93	.374	1.11393	2.958		PER IMP= 27.00
ADD HYD	Off3C.1	1& 2	2	.01510	36.21	1.271	1.57862	3.747		
COMPUTE NM HYD	24th	-	1	.00140	3.96	.147	1.96585	4.415		PER IMP= 90.00
ADD HYD	24TH.1	1& 2	2	.01650	40.15	1.418	1.61147	3.802		
ROUTE MCUNGE	24TH.9	2	5	.01650	40.12	1.416	1.60898	3.799		CCODE =
COMPUTE NM HYD	Off_3B	-	1	.01190	32.91	1.214	1.91297	4.322		PER IMP= 85.00
ROUTE MCUNGE	Off_3B.9	1	2	.01190	32.90	1.214	1.91227	4.320		CCODE =

QP81604.SUM

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COMPUTE NM HYD          OFF_3D          1          .00310          .184
ADD HYD                 OFF3D.1 1& 2 2          .01500          1.398
COMPUTE NM HYD          25th          1          .00140          .147
ADD HYD                 25TH.1 1& 2 2          .01640          1.545
ROUTE MCUNGE            25TH.9 2 1          .01640          1.542
ADD HYD                 25TH.91 1& 5 2          .03290          1.560
COMPUTE NM HYD          4A          1          .05920          1.68574
ADD HYD                 4A.1 1& 2 6          .09710          1.47738
*S *****
*S STORM DRAIN MAIN LINE
*S *****
*S SUBBASIN 211 from BLWMP (Modified 9/03)
COMPUTE NM HYD          211A          2          .13920          12.909
ROUTE MCUNGE            211.90 2 19          .13920          12.533
*S Run predevelopment for 211B
*S Field investigation shows extensive detention/retention
*S on this site
COMPUTE NM HYD          211B          1          .03670          .917
*S Current condition of 211B
COMPUTE NM HYD          211B          1          .03670          3.744
*S ROUTE 211B through EXISTING POND
*S Southern Plaza has ponds, as do the other
*S individual businesses
*S Limited flowrate to predevelopment level
*S
ROUTE RESERVOIR          P.Out 1 17          .03670          32.62
*S *****DIVIDE HYD TO UNBULK BY 3% *****

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COMMAND      HYDROGRAPH  IDENTIFICATION  FROM TO  ID NO.  NO.  AREA  PEAK  RUNOFF  TIME TO  CFS  PAGE = 9
              IDENTIFICATION  NO. NO.  (SQ MI)  DISCHARGE  VOLUME  (HOURS)  PER  NOTATION
              HYDROGRAPH  NO. NO.  (SQ MI)  (CFS)  (AC-FT)

DIVIDE HYD    UNBULK      17 17          .03560          31.64          3.631
              SEDIMENT    and 59          .00110          .112
COMPUTE NM HYD 211C      18 18          .00520          14.48          1.389
ADD HYD        211.10 17&19 2          .17480          288.69          1.840
ROUTE MCUNGE    211.20 2&18 1          .18000          294.62          1.510
COMPUTE NM HYD 211.91 1 2          .18000          294.62          1.740
ROUTE MCUNGE    OFF_2A 1 2          .00560          15.50          2.581
ADD HYD        OFF2A.9 1 5          .00560          15.49          1.73948
COMPUTE NM HYD 211.92 5& 2 2          .18560          301.20          1.73899
ADD HYD        OFF_2C 1 2          .00470          8.90          1.91298
COMPUTE NM HYD OFF2C.1 1& 2 2          .19030          304.53          1.91029
ADD HYD        23RD      2 2          .00140          3.96          1.74416
COMPUTE NM HYD 23RD.1 1& 2 2          .19170          306.12          1.11394
ROUTE MCUNGE    23RD.9 2 1          .19170          305.88          1.72860
ADD HYD        23RD.91 1& 4 2          .27343          428.94          1.510
ROUTE MCUNGE    23RD.92 2 3          .27343          428.74          1.73033
*S Bring in the Flow from Subbasin 4A
ADD HYD        23RD.93 3& 6 2          .36553          625.87          1.72961
ROUTE MCUNGE    23RD.94 2 3          .36553          622.63          1.67449
COMPUTE NM HYD 3B          1          .06210          143.86          1.580
ADD HYD        3B.1 1& 3 3          .42763          742.99          1.67413
*S Run a predevelopment for commercial lot (11) to determine
  the maximum permissible pond outflow
COMPUTE NM HYD 11.00 1          .01560          14.32          1.64331
*S Real Unit 11
COMPUTE NM HYD 11.00 1          .01560          43.14          1.64218
*S ROUTE Unit 11 through pond that will be required
*S limit flowrate to predevelopment level

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[illegible]

QP81604.SUM

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ADD HYD ***** H.I. 1& 3 3 .01859 ***** 41.08 ***** 1.417
*S ***** BASIN J *****
COMPUTE NM HYD ***** BASIN J ***** 3.84 ***** 133
*****
ADD HYD ***** H.I.J 1& 3 3 .02029 ***** 44.92 ***** 1.551
*****
ADD HYD ***** EFG.HIJ 2& 3 2 .06200 ***** 139.58 ***** 4.860
*****
*S ***** ADD BASINS D,E,F,G AND H,I,J (INTO MH 18)
*****
ADD HYD ***** 7B.91 2& 7 2 .54826 ***** 962.16 ***** 46.990
*****
COMPUTE NM HYD ***** 17.00 - 1 .02340 ***** 37.57 ***** 1.110
*****
ADD HYD ***** 17.10 1& 2 3 .57166 ***** 996.91 ***** 2.725
*****
COMPUTE NM HYD ***** 4B - 1 .04810 ***** 110.52 ***** 3.816
*****
*S ***** Route 4B to the Intersection of Cabezon and Trailside
*****
ROUTE MCUNGE ***** 4B.9 1 2 .04810 ***** 110.33 ***** 3.814
*****
COMPUTE NM HYD ***** R_3 - 1 .00520 ***** 13.28 ***** .469
*****
ADD HYD ***** 4B.91 1& 2 2 .05330 ***** 123.35 ***** 4.283
*****
COMPUTE NM HYD ***** 5A - 1 .03130 ***** 72.52 ***** 2.513
*****
*S ***** Add 4B.91 and 5A at Intersection of Cabezon and Trailside
*****
ADD HYD ***** 5A.1 1& 2 2 .08460 ***** 195.66 ***** 6.797
*****
ROUTE MCUNGE ***** 5A.9 1 2 .08460 ***** 195.09 ***** 6.793
*****
ADD HYD ***** POND.IN 1& 3 1 .65626 ***** 1189.09 ***** 54.893
*****
*S ***** ROUTE FLOWS THROUGH Pond/Park in Unit 17
*****
*S ***** Pond Based on final design grades with 7 ac-ft of
*****
*S ***** low storage/WQ and then filling remainder of park/field
*****
*S ***** graded at 2%
*****
ROUTE RESERVOIR ***** P.Out 1 2 .65626 ***** 475.42 ***** 54.264
*****
*S ***** DIVIDE HYD TO UNBULK BY 3% *****
*****
COMMAND HYDROGRAPH FROM TO AREA PEAK
IDENTIFICATION NO. NO. (SQ MI) DISCHARGE (CFS)
TIME TO CFS PER ACRE PAGE = 11
(P.EAK (HOURS) NOTATION)

DIVIDE HYD P.Out.3 2 2 .63657 461.15 1.132
SEDIMENT and 51 .01969 1.628 1.132
*S ***** Route unbulked pond outflow at 17 to east end of 15
*****
*S ***** through a 60" pipe
*****
ROUTE MCUNGE P.Out.9 2 1 .63657 460.35 1.130
*****
*S ***** END OF CABEZON PHASE 1, BEGIN PHASE 2 DEVELOPMENT
*****
*S ***** BLWMP SUBBASINS 255,256,540,530B REMOVED;
*****
*S ***** 255 REPLACED BY TRACTS 15,16; 256 REPLACED BY 8,9,18;
*****
*S ***** 540 REPLACED BY 10,20; 530B REPLACED BY 10,20
*****
COMPUTE NM HYD ***** 15.00 - 2 .02300 ***** 61.11 ***** 4.152
*****
ADD HYD ***** 15.10 1& 2 2 .65957 ***** 53.399 ***** 1.128
*****
ROUTE MCUNGE ***** 15.90 2 1 .65957 ***** 53.382 ***** 1.128
*****
COMPUTE NM HYD ***** 7D.1 1& 2 2 .07932 ***** 178.24 ***** 3.511
*****
ADD HYD ***** 7D.91 2 1 .73889 ***** 59.474 ***** 1.245
*****
ROUTE MCUNGE ***** 18.00 - 2 .00780 ***** 588.25 ***** 1.244
*****
COMPUTE NM HYD ***** 18.10 1& 2 2 .74669 ***** 59.462 ***** 1.560
*****
ADD HYD ***** 16.00 - 1 .03090 ***** 59.832 ***** 2.511
*****
COMPUTE NM HYD ***** 18.20 1& 2 2 .77759 ***** 2.392 ***** 1.255
*****
ADD HYD ***** 18.20 1& 2 2 .77759 ***** 664.23 ***** 3.560
*****
*S ***** Route combined flow at 18 to East Branch
*****
*S ***** through a 78" pipe
*****
ROUTE MCUNGE ***** 18.90 2 3 .77759 ***** 62.198 ***** 1.332
*****
COMPUTE NM HYD ***** 8.00 - 1 .02970 ***** 69.29 ***** 1.332
*****
ADD HYD ***** 8.10 3& 1 12 .80729 ***** 723.38 ***** 3.645
*****

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*S ABOVE IS ALL FLOW TO EAST BRANCH VIA TRIBUTARY B CONTRIBUTING AREA

*S RESUME BLWMP FILE

*S *****

*S East Branch Main Channel

*S *****

*S * * * START OF LEMA CHANNEL

COMMAND	HYDROGRAPH IDENTIFICATION	FROM TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 12	NOTATION
ADD HYD	201.00	1	.24840	492.25	19.609	1.48017	1.550	3.096	PK BF =	1.06
ROUTE MCUNGE	201.90	1	.24840	492.14	19.597	1.47927	1.570	3.096	PER IMP=	54.00
ROUTE MCUNGE	204.00	1	.01500	36.36	1.303	1.62914	1.520	3.096	CCODE =	.2
ADD HYD	204.10	1& 2	.26340	523.81	20.901	1.48780	1.560	3.788	PER IMP=	65.00
*S * * * START OF SNEAD CHANNEL	205.00	1	.09140	163.45	7.382	1.51440	1.590	2.794	PER IMP=	57.00
ADD HYD	205.10	5& 1	.35480	684.20	28.283	1.49466	1.570	3.013		
ROUTE MCUNGE	205.90	5	.35480	683.84	28.269	1.49394	1.580	3.012	CCODE =	.2
ROUTE MCUNGE	202.00	1	.12390	238.31	11.112	1.68166	1.600	3.005	PER IMP=	69.00
ROUTE MCUNGE	202.90	1	.12390	238.17	11.073	1.67562	1.680	3.004	CCODE =	.2
ROUTE MCUNGE	203.00	1	.05390	89.39	4.549	1.58239	1.640	2.591	PER IMP=	62.00
*S * * * WESTERN HILLS DR. @ BLACK'S ARROYO (EAST BRANCH)	203.10	4& 1	.17780	325.61	15.621	1.64736	1.670	2.861		
ADD HYD	203.20	5& 2	.53260	954.01	43.891	1.54516	1.610	2.799		
ROUTE MCUNGE	203.91	5	.53260	952.98	43.836	1.54325	1.640	2.796	CCODE =	.2
ROUTE MCUNGE	212.00	1	.09950	182.73	8.389	1.58080	1.600	2.870	PER IMP=	62.00
ADD HYD	212.10	1& 2	.63210	1129.66	52.225	1.54916	1.630	2.792		
ROUTE MCUNGE	213.00	1	.10800	199.46	9.345	1.62238	1.600	2.886	PER IMP=	65.00
ROUTE MCUNGE	213.90	1	.10800	199.45	9.342	1.62184	1.610	2.886	CCODE =	.2
ADD HYD	213.20	5& 4	.74010	1326.76	61.567	1.55976	1.630	2.801		
*S * * * START OF NICKLAUS CHANNEL	214.00	1	.19090	318.14	15.689	1.54100	1.630	2.604	PER IMP=	59.00
ROUTE MCUNGE	214.90	1	.19090	317.53	15.670	1.53906	1.680	2.599	CCODE =	.1
ROUTE MCUNGE	216.00	1	.09660	179.81	7.821	1.51801	1.580	2.908	PER IMP=	57.00
*S * * * COMBINE HYD. 'S	214.9	AND 216	AT 216.1							

*S CASPER DR. @ 150 FT. W. OF NICKLAUS DR.

COMMAND	HYDROGRAPH IDENTIFICATION	FROM TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 12	NOTATION
ADD HYD	216.10	1& 2	.28750	471.74	23.490	1.53199	1.650	2.564		
ROUTE MCUNGE	215.00	1	.11020	170.19	9.130	1.55347	1.670	2.413	PER IMP=	60.00
ROUTE MCUNGE	215.90	1	.11020	170.15	9.109	1.54986	1.730	2.413	CCODE =	.2
ADD HYD	216.20	6& 3	.39770	626.16	32.600	1.53694	1.670	2.460		
*S * * * AFTER SNEAD AND NICKLAUS CONFLUENCE	216.30	AP 216.30								
ADD HYD	216.30	6& 4	1.13780	1938.16	94.167	1.55179	1.640	2.662		
ROUTE MCUNGE	217B	2	.06660	73.79	3.741	1.05324	1.660	1.731	PER IMP=	26.00
ROUTE MCUNGE	217B.90	2	.06660	73.79	3.738	1.05223	1.690	1.731	CCODE =	.2
ROUTE MCUNGE	217A	1	.19020	243.63	12.120	1.19479	1.650	2.001	PER IMP=	36.00
*S * * * COMBINE HYD. 'S	217A AND 217B AT PLAYERS CHANNEL									
ADD HYD	217A.10	1& 3	.25680	315.58	15.857	1.15782	1.660	1.920		
*S * * * EAST BRANCH CROSSING SOUTHERN BLVD.	217.20	5& 1								
*S * * * SOUTHERN BLVD. @ 2100 FT. W. OF GOLF COURSE RD.	217.20	5& 1								
*S * * * BLWMP AP 217.20	217.20	5& 1								
ADD HYD	217.20	5& 1	1.39460	2251.93	110.024	1.47924	1.640	2.523		
*S * * * CABEZON PHASE 2 REVISIONS RESUME BELOW; FLOW FROM EAST BRANCH NORTH OF										
*S * * * SOUTHERN BLVD ROUTED IN IMPROVED EAST BRANCH										

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*S SEDIMENT BULK AT 6% FOR CABEZON LINED CHANNEL

SEDIMENT BULK	217.90	5	2	1.39460	2251.58	109.989	1.47877	1.660	2.523	PK BF = 1.06	CCODE = .1
ROUTE MCUNGE											
*S CABEZON PHASE 2 REVISIONS: BLWMP SUBBASINS 218A, 218B, 219, 220 REMOVED;											
*S 218A REPLACED BY OFF_4, OFF_5, TRACT 6; 218B REPLACED BY TRACTS 19, 1;											
*S 219 REPLACED BY TRACTS 5A, 5B, 5C, 2, OFF_4, OFF_6, OFF_7, OFF_8, A_1 (CHANNEL);											
*S 220 REPLACED BY TRACTS 8, 2											
COMPUTE NM HYD	Off_4	-	1	.04980	107.82	3.574	1.34573	1.510	3.383	PER IMP=	42.00
ADD HYD	Off_4.10	2& 1	2	1.44440	2309.92	113.564	1.47419	1.660	2.499		
COMPUTE NM HYD	Off_5	-	1	.02540	58.18	1.991	1.46970	1.510	3.579	PER IMP=	52.00
ADD HYD	Off_5.10	2& 1	1	1.46980	2341.40	115.554	1.47411	1.680	2.489		
ROUTE MCUNGE	Off_5.90	1	2	1.46980	2341.46	115.500	1.47341	1.510	3.383	CCODE =	.2
COMPUTE NM HYD	Off_6	-	1	.02620	56.73	1.880	1.34573	1.510	3.383	PER IMP=	42.00
ADD HYD	Off_6.10	2& 1	2	1.49600	2369.40	117.380	1.47118	1.680	2.475		
ROUTE MCUNGE	Off_6.90	2	1	1.49600	2369.15	117.342	1.47070	1.690	2.474	CCODE =	.1
COMPUTE NM HYD	6.00	-	3	.09570	222.48	7.737	1.51585	1.510	3.632	PER IMP=	56.90
ADD HYD	19.00	-	2	.00780	12.54	.370	1.88924	1.520	2.511	PER IMP=	15.00
COMPUTE NM HYD	19.10	3& 2	2	.10350	234.96	8.107	1.46863	1.510	3.547		
ADD HYD											
*S * * * START OF GOLF COURSE CHANNEL											

SEDIMENT BULK										PK BF =	1.06
*S GOLF COURSE ROAD STORM DRAIN SYSTEM WITH TWO OUTFALLS UPSTREAM OF											
*S 23RD AVENUE PONDS											
*S BLWMP SUBBASIN 500, SW CORNER OF SOUTHERN AND GOLF COURSE											
COMPUTE NM HYD	500.00	-	3	.02610	53.84	2.200	1.58042	1.560	3.223	PER IMP=	60.00
*S ROUTE 500 IN TYPICAL ROADWAY CROSS-SECTION TO EAST BRANCH											
ROUTE MCUNGE	500.90	3	4	.02610	53.83	2.196	1.57762	1.600	3.223	CCODE =	.2
*S COMBINE 19.10 AND 500.90 AT 19.20											
ADD HYD	19.20	4& 2	2	.12960	272.92	10.303	1.49058	1.530	3.290		
ADD HYD	19.30	2& 1	2	1.62560	2523.49	127.645	1.47229	1.690	2.426		
COMPUTE NM HYD	Off_7	-	1	.01060	22.96	.761	1.34574	1.510	3.385	PER IMP=	42.00
*S Route off_7 through off_8 to the East Branch											
ROUTE MCUNGE	Off_7.90	1	3	.01060	22.98	.760	1.34353	1.560	3.387	CCODE =	.2
COMPUTE NM HYD	Off_8	-	1	.01500	32.49	1.077	1.34573	1.510	3.384	PER IMP=	42.00
ADD HYD	Off_8.1	1& 3	1	.02560	53.52	1.836	1.34482	1.540	3.267		
ADD HYD	19.40	2& 1	2	1.65120	2553.46	129.481	1.47031	1.690	2.416		
COMPUTE NM HYD	A_1	-	1	.03170	73.14	2.483	1.46839	1.510	3.605	PER IMP=	50.00
ADD HYD	19.50	2& 1	2	1.68290	2587.76	131.964	1.47027	1.690	2.403		
*S ROUTE UNBULKED THROUGH A_2 (EAST BRANCH) TO SOUTHERN END OF 5											

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION
ROUTE MCUNGE	19.90	2	4	1.68290	2586.90	131.884	1.46938	1.700	2.402	CCODE =	.2
COMPUTE NM HYD	5B	-	1	.01960	45.62	1.585	1.51588	1.510	3.637	PER IMP=	56.90
ADD HYD	5B.10	4& 1	2	1.70250	2607.48	133.468	1.46991	1.700	2.393		
*S PORTION OF EAST BRANCH WITHIN CABEZON											
COMPUTE NM HYD	A_2	-	1	.00810	18.70	.634	1.46840	1.510	3.608	PER IMP=	50.00
ADD HYD	5B.20	2& 1	3	1.71060	2615.90	134.102	1.46990	1.700	2.389		
*S ROUTE 5B.20 TO EAST BRANCH CROSSING CABEZON BLVD VIA A_3											
ROUTE MCUNGE	5B.90	3	2	1.71060	2616.12	134.041	1.46923	1.710	2.390	CCODE =	.2
COMPUTE NM HYD	2.00	-	1	.03220	69.92	2.317	1.34900	1.510	3.393	PER IMP=	42.00
ADD HYD	2.10	2& 1	5	1.74280	2646.29	136.358	1.46701	1.710	2.373		
COMPUTE NM HYD	1.00	-	1	.11170	242.40	8.036	1.34898	1.510	3.391	PER IMP=	42.00
*S 510A is small area between Cabazon Subbasin 1 and											
*S BLWMP Subbasin 510- Used same treatments as 510											
COMPUTE NM HYD	510A	-	2	.01320	32.89	1.186	1.68464	1.520	3.894	PER IMP=	68.00
ADD HYD	1.10	1& 2	3	.12490	275.29	9.222	1.38445	1.510	3.444		
COMPUTE NM HYD	510.00	-	1	.04080	76.81	3.129	1.43810	1.560	2.941	PER IMP=	51.00
*S ROUTE 510 IN TYPICAL ROADWAY CROSS-SECTION TO EAST BRANCH											
ROUTE MCUNGE	510.90	1	2	.04080	76.75	3.124	1.43579	1.600	2.939	CCODE =	.2

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ADD HYD	1.20	3& 2	4	1.6570	329.73	12.347	1.530	3.109		
ADD HYD	2.20	4& 5	3	1.90850	2824.94	148.704	1.710	3.313		
COMPUTE NM HYD	5C	-	1	.02890	67.27	2.336	1.510	3.637	PER IMP=	56.90
ROUTE MCUNGE	5C.9	1	2	.02890	67.16	2.334	1.530	3.631	CCODE =	.2
COMPUTE NM HYD	R_4	-	1	.00990	25.27	.894	1.510	3.988	PER IMP=	66.00
ADD HYD	R_4.9	1& 2	1	.03880	91.93	3.228	1.530	3.702		
ADD HYD	2.40	3& 1	2	1.94730	2868.96	151.933	1.700	2.302	PER IMP=	50.00
COMPUTE NM HYD	A_3	-	1	.00800	18.47	.627	1.510	3.608	PER IMP=	66.00
ADD HYD	2.50	2& 1	2	1.95530	2877.27	152.559	1.700	2.299		
COMPUTE NM HYD	R_5	-	1	.00760	19.40	.686	1.510	3.989	PER IMP=	66.00
ADD HYD	R_5.10	2& 1	2	1.96290	2885.98	153.245	1.700	2.297		
**S ROUTE R_5.10 TO R_5.90 VIA EAST BRANCH PROPOSED CHANNEL										
*S TO DOWNSTREAM END OF SUBBASIN 8										
ROUTE MCUNGE	R_5.90	2	1	1.96290	2885.87	153.212	1.720	2.297	CCODE =	.2
**S CONFLUENCE OF TRIBUTARY B AND EAST BRANCH										
ADD HYD	8.20	1&12	2	2.77019	3487.16	217.819	1.710	1.967		
*S ROUTE 8.20 TO END OF SUBBASIN 9 VIA EAST BRANCH CHANNEL (8.90)										
ROUTE MCUNGE	8.90	2	1	2.77019	3486.92	217.749	1.730	1.967	CCODE =	.2
COMPUTE NM HYD	A_4	-	2	.00620	14.32	.486	1.510	3.609	PER IMP=	50.00
ADD HYD	8.93	2& 1	1	2.77639	3492.66	218.234	1.730	1.966		
COMPUTE NM HYD	9.00	-	2	.04480	105.06	3.662	1.510	3.664	PER IMP=	58.20
ADD HYD	9.10	2& 1	1	2.82119	3535.08	221.896	1.730	1.958		
*S ROUTE 9.10 TO 9.90 (DS end of CAB SUBBASIN 21 in EAST BRANCH)										
ROUTE MCUNGE	9.90	1	2	2.82119	3533.75	221.787	1.750	1.957	CCODE =	.2
COMPUTE NM HYD	21.00	-	1	.02340	62.17	2.276	1.510	4.152	PER IMP=	80.00
ADD HYD	21.10	2& 1	2	2.84459	3557.91	224.062	1.750	1.954		
COMPUTE NM HYD	10.00	-	1	.12980	301.44	10.494	1.510	3.629	PER IMP=	56.90
COMPUTE NM HYD	20.00	-	3	.00780	12.54	.370	1.510	3.565	PER IMP=	15.00
ADD HYD	20.10	1& 3	1	2.13760	313.93	10.864	1.510	4.117	PER IMP=	74.00
ADD HYD	20.20	2& 1	1	2.98219	3678.33	234.926	1.510	4.232	PER IMP=	80.00
COMPUTE NM HYD	R_8	-	2	.01180	31.10	1.121	1.740	1.927		
COMPUTE NM HYD	R_7	-	3	.00170	4.60	.168	1.510	4.232	PER IMP=	80.00
ADD HYD	R_8.10	2& 3	4	.01350	35.70	1.288	1.510	4.132		
*S Route combined flows at R_8.10 through 36" pipe IN ROADWAY TO DS END OF 14										
ROUTE	R_8.90	4	3	.01350	32.64	1.285	1.550	3.778		
COMPUTE NM HYD	R_9	-	2	.01540	40.58	1.463	1.510	4.117	PER IMP=	74.00
ADD HYD	R_9.10	3& 2	3	.02890	72.01	2.747	1.530	3.893		
ADD HYD	20.30	1& 3	9	3.01109	3711.14	237.673	1.740	1.926		
*S RESUME BLWMP WITH SUBBASINS WEST OF GOLF COURSE, IN UNIT 16 BUT										
*S NOT PART OF CABEZON										
*S REMAINDER OF GOLF COURSE ROAD STORM DRAIN SYSTEM										
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID	TO ID	NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 14
				NO.						NOTATION
SEDIMENT BULK										
COMPUTE NM HYD	520.00	-	1	.04090	84.56	2.923	1.34014	1.520	3.230	PK BF = 1.06
*S ROUTE 520 TO 530C AT 520.90										
ROUTE MCUNGE	520.90	1	3	.04090	82.67	2.912	1.33507	1.570	3.158	CCODE = .2
COMPUTE NM HYD	530A	-	2	.14730	298.97	10.484	1.33454	1.530	3.171	PER IMP= 41.00
*S ***** AP 530A.90 (20PP.IN) *****										
*S ROUTE 530A THROUGH 20TH AVENUE PARK POND SIZE AND VOLUME ARE ASSUMED										
*S BASED ON FIELD INVESTIGATION BUT NOT ON A COMPREHENSIVE SURVEY.										
*S THIS POND HAS AN OVERFLOW ON THE TWO LOTS ON THE SOUTH EDGE AND										
*S IS MODELED WITH THE PROPOSED EXPANSION.										
ROUTE RESERVOIR	530A.90	2	7	.14730	61.60	10.476	1.33349	1.980	.653	AC-FT= 5.400
*S*****DIVIDE HYD TO UNBULK TO 3% *****										
DIVIDE HYD	UNBULK	7	7	.14288	59.75	10.162	1.33349	1.980	.653	
*S ***** and 57 *****										
*S ***** AP 20PP.OUT *****										

*S ROUTE 530A.90 "UNBULKED" THROUGH STORM DRAIN TO GOLF COURSE ROAD SYSTEM.
 *S OUTFALL PIPE IS 48" CMP.

ROUTE MCUNGE 530A.91 7 99 .14288 59.75 10.147
 *S PUNCH HYDROGRAPH FOR GOLF COURSE ROAD STORM DRAIN DESIGN MODEL
 *S COMBINE 530A.91 AND 520.90 AT STORM DRAIN OUTFALL TO GCR SYSTEM
 ADD HYD 530A.10 99& 3 3 .18378 139.51 13.059
 *S ROUTE COMBINED HYDROGRAPHS IN PIPE TO 23RD AVENUE
 ROUTE MCUNGE 530A.92 3 2 .18378 139.39 13.047
 *S COMPUTE 530C 530C - 1 .02530 51.48 1.688
 *S COMPUTE 530D 23RD AVE. POND BASIN 530D - 3 .01000 16.25 .443
 *S ADD 530D TO 530C 530D.10 1& 3 3 .03530 67.72 2.131
 ADD HYD 530D.20 2& 3 2 .21908 193.84 15.178
 *S *****
 *S ROUTE COMBINED FLOW THROUGH 23RD AVENUE PONDS
 *S THE PONDS ARE COMBINED AND TREATED AS ONE TEN ACRE FOOT POND FOR
 *S FOR THIS MODEL.

ROUTE RESERVOIR 530.90 2 3 .21908 47.87 10.254
 *S THIS RESERVOIR NOT UNBULKED
 ROUTE MCUNGE 530.91 3 2 .21908 47.87 10.186
 *S CABEZON PHASE 2 RESUMES BELOW: PART OF BLWMP SUBBASIN 550 IS REPLACED BY
 *S TRACT 21 AND A-5 (WEST BRANCH)

*S COMBINE ROUTED FLOW WITH EAST BRANCH FLOW:
 *S ADD 20.30 AND 530.91 AT 20.40

ADD HYD 20.40 9& 2 1 3.23017 3728.28 247.859
 COMPUTE NM HYD A-5 - 2 .01210 27.93 .948
 ADD HYD 20.50 1& 2 1 3.24227 3739.07 248.807
 *S ROUTE IN EAST BRANCH TO BLACK DAM

ROUTE MCUNGE 20.90 1 2 3.24227 3733.05 248.512
 *S Area of 550 is reduced by area that it overlaps

*S CABEZON basins
 COMPUTE NM HYD 550.00 - 1 .02760 48.65 1.440
 ADD HYD EAST 2& 1 1 3.26987 3747.95 249.952
 ADD HYD DAM.10 1&11 97 8.84598 9313.70 554.629

*S RECALL HYDROGRAPHS FROM BERNALILLO COUNTY SUBDIVISIONS
 *S THESE ARE PUNCH HYDROGRAPHS AND FLOWS DRAIN DIRECTLY TO THE DAM POOL
 *S VIA PIPES.

TEXT TAKEN FROM MODEL RECEIVED 1/9/02 * * * * *
 *S Ridgeview Village(DB4), Los Suenos(DB3), and the Park Hill(DB2)
 *S Subdivisions have free developed discharge based on R-1, 5 du/acre density.
 *S Flow from some commercial sites east of Unser between McMahon and
 *S Black Arroyo Blvd. is restricted to historic as per Ridgeview Unit 1 Plan.

*S developed flow is accommodated from the residential tracts and
 *S other commercial tracts. * * * * *
 RECALL HYD AP5 - 18 .38090 850.60 31.937
 *S STONEBRIDGE SUBDIVISION FROM MODEL RECEIVED 1/15/02
 RECALL HYD AP15 - 19 .23850 359.51 17.620
 *S ADD RECALL HYDROGRAPHS
 ADD HYD DIRECT PIPE 18&19 98 .61940 1191.72 49.556
 *S ADD RECALL HYDS TO EAST AND WEST BRANCH FLOWS FOR TOTAL INTO BLACK DAM
 ADD HYD DAM.IN 98&97 99 9.46538 10152.29 603.502
 *S ROUTE FLOWS THROUGH WQ STRUCTURE NO. 2
 *S BEFORE ENTERING BLACK DAM

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*S
*S
ROUTE RESERVOIR          P-Out  99  98  9.46538  10142.62  582.419
*S *****DIVIDE HYD TO UNBULK BY 3% *****
DIVIDE HYD              P-Out.3  98  98  9.18141  9838.34  564.946
                        SEDIMENT and 51  .28396  304.28  17.473
*S ROUTE FLOWS THROUGH BLACK DAM RATING CURVE TAKEN FROM BLACK DAM
*S FILING SHEET RECORD DRAWINGS - BLARD-51 Stamp dated 9/14/91
*S Record Dwg Stamp 11/9/92 AMAFCA Ref # NW-04-114 Catlabacillas
*S THIS IS THE FUTURE CONDITIONS RATING CURVE
*S 5/04/04 BLACK DAM RATING CURVE ADJUSTED FOR CABEZON MODEL:
*S ELEVATIONS CONVERTED TO NAVD88 FROM NGVD29; ALSO
*S STORAGE INCREASED TO REFLECT WQ STRUCTURE NO.2
ROUTE RESERVOIR          DAM.R  98  91  9.18141  2419.22  564.920
*S EMERGENCY SPILLWAY CREST IS AT ELEV 5168.55 FT (NAVD88)
FINISH
0($10H
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D(s16.66H

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AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
INPUT FILE = T:\Projects\X4218012\Eng\AHYMO\rev_dmp\vol72204.txt - VERSION: 1997.02c
RUN DATE (MON/DAY/YR) =08/16/2004
USER NO.= AHYMO-I-9702a01000C05-AH

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION
START	7/22/04									1	
*S	WILSON & CO.'S CABEZON COMMUNITIES DRAINAGE MASTER PLAN, PHASE 2 OF DEVELOPMENT: THIS MODEL TAKES BOTH CABEZON PHASE 1 AND 2 INTO THE MODIFIED BLWMP MODEL DEVELOPED BY ASCG (1/20/04) TO ASSESS CABEZON'S IMPACT ON BLACK DAM. IT MODELS DEVELOPED CONDITIONS IN ALL SUBBASINS; SEDIMENT BULKING ADJUSTED TO 6% REFLECT THIS; ALSO, MUSKINGHAM CUNGE ROUTING (COMMAND: ROUTE MCUNGE) CONSISTENTLY USED										
*S	THIS MODEL USES A STEP OF 0.05 HR (3 MIN) SO THAT THE ENTIRE 24 HR HYDROGRAPH IS CAPTURED AND VOLUMETRIC RUNOFF IS MORE COMPLETELY ACCOUNTED FOR										
*S	01/20/2004 ADJUSTMENTS TO THIS MODEL FROM THE BLWMP "DOUBLE" COUNTING OF STREETS IN LAND TREATMENT REMOVED										
*S	SUB-BASIN 211 ROUTED ADJUSTED TO EXISTING FIELD CONDITIONS (XING SOUTHERN) NOTHING ELSE HAS BEEN ADJUSTED - USER ACCEPTS THIS MODEL AS IS AND TAKES THE RESPONSIBILITY FOR CHECKING IT FOR ACCURACY PRIOR TO USE...										
*S	FUTURE CONDITIONS MODEL - ALTERNATE B										
*S	3 DAMS ON THE WEST BRANCH										
*S	UNSER GATEWAY DAM, AND WATER QUALITY DIVERSIONS										
*S	ROUTING WITH MCUNGE METHOD AFTER WATER QUALITY DIVERSIONS ARE UTILIZED TO ADJUST FOR THE UNSTABLE HYDROGRAPHS WITH A STEEP SLOPE										
*S	AFTER MODIFICATION TO REDIRECT THE FIRST FLUSH OF 0.25" RUNOFF FOR SWQ RAINFALL TYPE= 2										
*S	BEGINNING OF THE BLACK ARROYO WEST BRANCH										
*S	LISBON CHANNEL NORTH OF TULIP										
*S	SEDIMENT BULK										
*S	COMPUTE NM HYD	101.00	-	1	33970	533.20	1.60274	1.600	2.453	PK BF =	1.06
*S	ROUTE MCUNGE	101.90	1	2	33970	531.48	1.60002	1.600	2.445	PER IMP=	48.00
*S	ADD HYD	102.00	-	1	25390	342.13	1.16946	1.550	2.105	CCODE =	26.00
*S	ROUTE MCUNGE	102.10	1& 2	3	59360	865.45	1.41586	1.600	2.278	PER IMP=	26.00
*S	COMPUTE NM HYD	102.90	3	4	59360	864.33	1.41606	1.600	2.275	CCODE =	.2
*S	103A	-	1	18030	273.36	12.146	1.26312	1.550	2.369	PER IMP=	28.00
*S	START OF LISBON CHANNEL AT TULIP AND INFLOW TO DAM										
*S	ADD HYD	103A.90	1& 4	3	77390	1121.03	1.38043	1.600	2.263		
*S	ROUTE 103A.90 THRU LISBON @ TULIP DAM/POND										
*S	ROUTE RESERVOIR TULIS.DAM	3	4	77390	4.12	9.428	.22843	20.750	.008	AC-FT=	49.486
*S	DIVIDE HYD	UNBULK	4	3%	75068	4.00	.22842	20.750	.008		
*S	SEDIMENT and 51				.02322	.283					
*S	ROUTE IN PIPE TO LISBON CHANNEL										
*S	AP=TULIS.90										
*S	ROUTE MCUNGE	TULIS.90	4	3	75068	4.00	.22805	20.800	.008	CCODE =	.2
*S	START OF LISBON CHANNEL AT TULIP										
*S	SEDIMENT BULK										
*S	COMPUTE NM HYD	103B	-	1	.08950	162.97	1.26312	1.500	2.845	PK BF =	1.06
						6.029				PER IMP=	28.00

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*S ADD 103B TO PREVIOUS HYDROGRAPHS FOR TOTAL Q IN LISBON CHANNEL AT
 *S DOWNSTREAM END OF BASIN 103B
 ADD HYD 103B.10 1& 3 3 .84018 163.13 15.160
 *S ROUTE 103B.10 THRU 104B TO 103B.90

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION
ROUTE MCUNGE	103B.90	3	4	.84018	163.13	15.160	.33831	1.500	.303	CCODE =	.0
*S START OF SUNSET CHANNEL											
*S *****											
SEDIMENT BULK											
COMPUTE NM HYD	106A1	-	1	.11660	172.56	8.114	1.30471	1.550	2.312	PK BF =	1.06
ROUTE MCUNGE	106A.90	1	3	.11660	171.74	8.116	1.30509	1.600	2.301	PER IMP=	33.00
COMPUTE NM HYD	104A	-	1	.18340	376.90	15.452	1.57974	1.500	3.211	CCODE =	.2
ADD HYD	104.10	3& 1	1	.30000	506.36	23.568	1.47299	1.500	2.637	PER IMP=	45.00
*S *****											
*S ROUTE 104.10 THROUGH PROPOSED SUNSET @ TULIP POND/DAM											
*S *****											
ROUTE RESERVOIR	TUSUN.DAM	1	2	.30000	4.27	9.143	.57141	3.600	.022	AC-FT=	18.802
*S *****											
DIVIDE HYD	UNBULK	2	BY	.29100	4.14	8.868	.57141	3.600	.022		
*S *****											
*S ROUTE IN PIPE TO LISBON CHANNEL	TUSUN.90	2	3	.29100	4.14	8.840	.56960	3.650	.022	CCODE =	.2
ROUTE MCUNGE											
SEDIMENT BULK											
COMPUTE NM HYD	104B	-	1	.03550	72.78	2.991	1.57974	1.500	3.203	PK BF =	1.06
ADD HYD	104.20	1& 3	5	.32650	72.92	11.831	.67943	1.500	.349	PER IMP=	45.00
*S LISBON CHANNEL AFTER SUNSET CHANNEL											
ADD HYD	104.30	5& 4	3	CONFLUENCE (HYD=104B.1)							
ROUTE MCUNGE	104.90	3	4	1.16668	236.05	26.991	.43377	1.500	.316	CCODE =	.1
SEDIMENT BULK											
COMPUTE NM HYD	105.00	-	1	1.16668	232.85	26.915	.43256	1.600	.312	PK BF =	1.06
*S LISBON CHANNEL AFTER SUB-BASIN 105											
ADD HYD	105.10	1& 4	5	.15090	233.80	12.980	1.61284	1.600	2.421	PER IMP=	44.00
ROUTE MCUNGE	105.90	5	4	1.31758	466.65	39.895	.56774	1.600	.553	CCODE =	.2
*S *****											
*S START OF SUGAR CHANNEL AT TULIP											
*S *****											
COMPUTE NM HYD	106A2	-	1	.13590	224.60	9.457	.56740	1.600	.552	CCODE =	.2
*S *****											
*S BALI CHANNEL											
COMPUTE NM HYD	106B	-	3	.15220	265.08	12.921	1.30471	1.500	2.582	PER IMP=	33.00
*S *****											
*S SUGAR CHANNEL INCLUDING CONFLUENCE WITH BALI CHANNEL											
*S *****											
ADD HYD	106B.10	1& 3	5	.28810	484.54	22.377	1.45634	1.550	2.628		
*S ROUTE 106B.10 TO 106C.90 (TO CONFLUENCE OF LISBON & SUGAR CHLS)											
ROUTE MCUNGE	106B.90	5	1	CONFLUENCE OF LISBON & SUGAR CHLS (106C)							
COMPUTE NM HYD	106C	-	3	.28810	484.54	22.377	1.45634	1.550	2.628	CCODE =	.0
ADD HYD	106C.10	1& 3	5	.04840	63.20	2.672	1.03493	1.550	2.040	PER IMP=	22.00
*S *****											
*S AP 106.90				.33650	547.74	25.049	1.39573	1.550	2.543		
*S *****											
*S LISBON CHANNEL AFTER CONFLUENCE WITH SUGAR CHANNEL											
*S *****											
ADD HYD	106.20	5& 4	5	1.65408	952.87	64.920	.73591	1.600	.900	CCODE =	.1
ROUTE MCUNGE	106.91	5	2	1.65408	949.11	64.825	.73483	1.600	.897	PER IMP=	49.00
COMPUTE NM HYD	107.00	-	1	.03580	77.45	3.234	1.69355	1.500	3.380	CCODE =	.1
*S *****											

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COMMAND	HYDROGRAPH IDENTIFICATION	FROM TO ID NO.	ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	CFS PER ACRE	PAGE = NOTATION
*S *	*	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	COMPUTE NM HYD	-	3	.05090	94.74	4.431	2.908	IMP= 46.00
*S *	*	*	*	*	*	*	*	*
*S *	ARKANSAS CHANNEL INCLUDING FLOW FROM BALTIC CHANNEL	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	ADD HYD	110.10	1&3	.13730	236.46	12.207	2.691	
*S *	ROUTE MCUNGEE	110.90	6	.13730	234.54	12.207	2.669	CCODE = .2
*S *	COMPUTE NM HYD	108.00	-	.06720	128.69	6.686	2.992	PER IMP= 59.00
*S *	*	*	*	*	*	*	*	*
*S *	ARKANSAS CHANNEL INCLUDING FLOW FROM BALTIC CHANNEL BEFORE CONFLUENCE	*	*	*	*	*	*	*
*S *	WITH LISBON CHANNEL	*	*	*	*	*	*	*
*S *	LISBON AVE. @ 250 FT. N. OF HOOD RD.	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	ADD HYD	108.10	1&2	.20450	363.23	18.893	2.775	
*S *	* AP 108.91	*	*	*	*	*	*	*
*S *	LISBON CHANNEL AFTER ADDING ARKANSAS CHANNEL FLOWS	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	ADD HYD	108.20	5&6	1.89438	1356.80	86.952	1.119	
*S *	ROUTE MCUNGEE	108.90	5	1.89438	1339.62	86.911	1.105	CCODE = .2
*S *	COMPUTE NM HYD	111.00	-	.11590	212.18	10.915	2.861	PER IMP= 54.00
*S *	*	*	*	*	*	*	*	*
*S *	LISBON CHANNEL DISCHARGE @ SOUTHERN BLVD	AP 111.10	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	ADD HYD	111.10	1&2	2.01028	1534.69	97.826	1.193	
*S *	*	*	*	*	*	*	*	*
*S *	S START OF LISBON ARROYO	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	ROUTE MCUNGEE	111.90	5	2.01028	1532.02	97.721	1.191	CCODE = .1
*S *	SEDIMENT BULK	*	*	*	*	*	*	PK BF = 1.06
*S *	COMPUTE NM HYD	116.00	-	.03190	74.06	3.245	3.628	PER IMP= 61.00
*S *	ADD HYD	116.10	1&2	2.04218	1572.19	100.966	1.203	
*S *	*	*	*	*	*	*	*	*
*S *	END LISBON CHANNEL AND LISBON ARROYO WATERSHED	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	START IVORY WATERSHED	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	SEDIMENT BULK	*	*	*	*	*	*	*
*S *	PECOS/RODEO CHANNEL	-	1	.06980	124.84	5.739	2.795	PER IMP= 41.00
*S *	COMPUTE NM HYD	114.00	*	.	124.44	5.737	2.786	CCODE = .1
*S *	ROUTE MCUNGEE	114.90	1	.06980	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	SPUR CHANNEL	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*
*S *	COMPUTE NM HYD	115.00	-	.12520	212.43	11.634	2.651	PER IMP= 52.00
*S *	ADD HYD	115.10	1&2	.19500	336.86	17.372	2.699	
*S *	Ivory Channel	*	*	*	*	*	*	*
*S *	*	*	*	*	*	*	*	*

[illegible]

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 *S 253 REPLACED BY CABEZON COMMERCIAL TRACT 12 (DRAINS TO WEST BRANCH)
 *S AND 7A, 7B, 7C (ALL DRAIN TO POND IN TRACT 17 WHICH GOES TO EAST
 *S BRANCH); 160 IS WEST BRANCH, REPLACED BY A_6
 *S Commercial Unit 12

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)
COMPUTE NM HYD	12.00	-	1	.01560	42.02	1.972
ADD HYD	12.10	1& 5	6	4.83790	4232.10	315.601
ROUTE MCUNGE	12.90	6	5	4.83790	4228.84	315.448
*S BLWMP FILE RESUMES BELOW						
COMPUTE NM HYD	156.00	-	1	.22940	458.88	17.717
ROUTE MCUNGE	156.90	1	2	.22940	456.44	17.722
COMPUTE NM HYD	157.00	-	1	.18890	387.95	16.128
ADD HYD	157.10	1& 2	6	.41830	811.07	33.850
COMPUTE NM HYD	158.00	-	1	.08160	205.84	9.569
ROUTE MCUNGE	158.90	1	3	.08160	203.95	9.569
ADD HYD	158.10	3& 6	6	.49990	1013.35	43.419
*S UNSER GATEWAY DAM						
ROUTE RESERVOIR	GATE.POND	6	3	.49990	619.15	43.419
*S *****DIVIDE HYD TO UNBULK BY 3% *****						

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION
DIVIDE HYD	UNBULK	3	3	.48490	600.58	42.116	1.650	1.935	7	
ROUTE MCUNGE	SEDIMENT	and 55	2	.01500	18.57	1.303	1.650	1.935		
*S CABEZON REVISIONS PHASE 2 RESUME BELOW; BLWMP SUBBASINS 620,161 REMOVED				.48490	600.32	42.119	1.650	1.934		CCODE = .2
*S 620 REPLACED BY OFFSITE TRACT 13, 161 REPLACED BY OFFSITE TRACT 14										
*S (ALL DRAIN TO WEST BRANCH); PART OF BLWMP 650 ALSO REMOVED										
*S THIS TAKES WEST BRANCH TO DAM										
ADD HYD	12.91	5& 2	6	5.32280	4824.85	357.567	1.700	1.416		
ROUTE MCUNGE	12.99	6	5	5.32280	4824.85	357.567	1.700	1.416		CCODE = .0
*S ADJUST SEDIMENT BULK										
SEDIMENT BULK										
*S COMPUTE CABEZON SUBBASIN 13										
COMPUTE NM HYD	13.00	-	1	.07890	212.18	9.974	1.500	4.202		PK BF = 1.06
ADD HYD	13.10	1& 5	5	5.40170	4917.75	367.541	1.700	1.423		PER IMP= 85.00
*S COMPUTE CABEZON SUBBASIN 14										
COMPUTE NM HYD	14.00	-	1	.09090	226.41	10.926	1.500	3.892		PER IMP= 80.00
ADD HYD	14.10	1& 5	5	5.49260	5025.36	378.467	1.700	1.430		
ROUTE MCUNGE	14.90	5	2	5.49260	5025.36	378.467	1.700	1.430		CCODE = .0
*S Area of 650 is reduced by area that it overlaps										
*S CABEZON basins										
COMPUTE NM HYD	650.00	-	1	.03730	63.36	1.959	1.500	2.654		PER IMP= 9.00
ADD HYD	650.91	1& 2	5	5.52990	5052.43	380.427	1.700	1.428		
*S WEST BRANCH ARROYO BETWEEN 13 AND 14, SOUTH FROM WESTSIDE BLVD										
COMPUTE NM HYD	A_6	-	1	.04620	104.14	4.279	1.500	3.522		PER IMP= 50.00
*S BLACK'S ARROYO (WEST BRANCH) @ DAM										
ADD HYD	650.99	1& 5	11	5.57610	5097.04	384.705	1.700	1.428		
*S END OF THE BLACK'S ARROYO WEST BRANCH										
*S *****										
*S BEGINNING OF THE BLACK'S ARROYO EAST BRANCH										
*S End of West Branch- Beginning of East Branch										
*S THE FOLLOWING ARE CABEZON PHASE 1 REVISIONS										
*S BEGIN WITH CABEZON SUBBASINS THAT DRAIN TO WESTERN HILLS SD										
*S WHICH REPLACE TRIBUTARY B AND ARROYO D										
*S BLWMP SUBBASINS 251,252,250,254 REMOVED										
*S 251 REPLACED BY TRACTS 3A,3B; 252 REPLACED BY TRACTS 4A,4B;										
*S 250 REPLACED BY TRACTS 3B,11,7A; 254 REPLACED BY 17,7A,7C										
SEDIMENT BULK										
*S Following is the Northwest corner of offsites and Subbasin 3A										PK BF = 1.06

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* S It will be held on ID=4
* S COMPUTE NM HYD Off_1A - 1 .00540 14.55 .683 1.500 4.211 PER IMP= 85.00
* S ROUTE OFF_1A through existing pond
* S Pond Exists in field; Volume and outflow assumed to
* S limit flowrate to predevelopment level
* S
* S ROUTE RESERVOIR P.Out 1 17 .00540 5.18 .682 1.800 1.499 AC-FT= .200
* S *****DIVIDE HYD TO UNBULK BY 3% *****
* S DIVIDE HYD UNBULK 17 17 .00524 5.03
* S SEDIMENT and 56 .00016 .16
* S ROUTE MCUNGE Off_1A.9 17 2 .00524 5.02
* S COMPUTE NM HYD Off_1C 1 1 .00540 10.98
* S ADD HYD Off_1C.1 1& 2 2 .01064 14.08
* S COMPUTE NM HYD 21ST 1 1 .00100 2.75
* S ADD HYD 21ST.1 1& 2 2 .01164 16.84
* S ROUTE MCUNGE 21ST.9 2 3 .01164 16.40
* S COMPUTE NM HYD Off_1B - 1 .00560 15.09
* S ROUTE OFF_1B through existing pond
* S Pond Exists in field; Total volume = 0.22 ac-ft
* S limited flowrate to predevelopment level
* S

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COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID	TO ID	NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION
ROUTE RESERVOIR	P.Out	1	17		.00560	5.26	.709	2.37246	1.800	1.467	8	.211
* S *****DIVIDE HYD TO UNBULK BY 3% *****												
DIVIDE HYD	UNBULK	17	17		.00543	5.10	.687	2.37245	1.800	1.467		
ROUTE MCUNGE	SEDIMENT	and	57		.00017	.16	.021	2.37245	1.800	1.467		
COMPUTE NM HYD	Off_1B.9	17	2		.00543	5.10	.687	2.37182	1.800	1.467		
ADD HYD	Off_ID	-	1		.00470	8.76	.316	1.25884	1.500	2.911		CCODE = 27.00
COMPUTE NM HYD	Off_ID.1	1& 2	2		.01013	11.92	1.003	1.85535	1.500	1.838		PER IMP= 90.00
ADD HYD	22ND		1		.00100	2.75	.131	2.45016	1.500	4.303		PER IMP= 90.00
ROUTE MCUNGE	22ND.1	1& 2	2		.01113	14.67	1.133	1.90875	1.500	2.059		CCODE = 85.00
COMPUTE NM HYD	22ND.9	2	1		.01113	14.42	1.133	1.90904	1.550	2.025		PER IMP= 85.00
ROUTE OFF_2B through existing pond	Off_2B	-	2		.00470	12.67	.594	2.37033	1.500	4.212		PER IMP= 85.00
* S Pond Exists in field; Total volume = 0.18 ac-ft												
* S limited flowrate to predevelopment level												
ROUTE RESERVOIR	P.Out	2	17		.00470	4.88	.595	2.37213	1.800	1.623		AC-FT= .160
* S *****DIVIDE HYD TO UNBULK BY 3% *****												
DIVIDE HYD	UNBULK	17	17		.00456	4.73	.577	2.37212	1.800	1.623		
ADD HYD	SEDIMENT	and	58		.00014	.15	.018	2.37212	1.800	1.623		
ROUTE MCUNGE	Off_2B.1	1&17	2		.01569	18.74	1.710	2.04352	1.550	1.866		CCODE = .1
* S ADD 21ST and 22ND STs offsite routed flows												
ADD HYD	Off_2B.91	1& 3	2		.02733	33.41	2.912	1.99788	1.750	1.910		PER IMP= 55.40
COMPUTE NM HYD	3A	-	1		.05440	122.81	5.207	1.79465	1.500	3.528		PER IMP= 55.40
ADD HYD	3A.1	1& 2	4		.08173	126.90	8.119	1.86261	1.500	2.426		
* S Area coming down 24th to project												
COMPUTE NM HYD	Off_3A	-	1		.00880	23.71	1.112	2.37034	1.500	4.210		PER IMP= 85.00
* S Use roadway cross-section to route off_3A thru off_3c although there is												
* S not one presently there												
ROUTE MCUNGE	Off_3A.9	1	2		.00880	23.55	1.112	2.36943	1.550	4.182		CCODE = .1
COMPUTE NM HYD	Off_3C	-	1		.00630	11.73	.423	1.25884	1.500	2.909		PER IMP= 27.00
ADD HYD	Off_3C.1	1& 2	2		.01510	33.98	1.535	1.90601	1.550	3.517		PER IMP= 27.00
COMPUTE NM HYD	24th	-	1		.00140	3.85	.183	2.45015	1.500	4.297		PER IMP= 90.00
ADD HYD	24TH.1	1& 2	2		.01650	37.29	1.718	1.95216	1.550	3.531		PER IMP= 90.00
ROUTE MCUNGE	24TH.9	2	5		.01650	36.94	1.715	1.94857	1.650	3.498		CCODE = .1

ROUTE RESERVOIR	P.Out	1	17	.01560	14.14	1.961	2.35714	1.800	1.416	AC-FT=	.614
*S *****	DIVIDE HYD TO UNBULK BY 3%	17		*****	*****						
DIVIDE HYD	UNBULK	17		.0047	13.72	1.902	2.35714	1.800	1.416		
	SEDIMENT	59		.0047	.42	.059	2.35714	1.800	1.416		
ROUTE MCUNGE	11.90	17		.01513		1.900	2.35714	1.800	1.416		
COMPUTE NM HYD	R_2	1		.01513	13.71	.732	2.04713	1.500	3.890	CCODE =	.1
ADD HYD	R_2.1	1		.00670	16.68		2.26033	1.500	3.890	PER IMP=	66.00
ADD HYD	1& 2	2		.02183	23.95	2.632	2.26033	1.500	1.714		
COMPUTE NM HYD	3B.2	2& 3	2	.49496	720.80	48.056	2.00472	1.550	2.506		
ADD HYD	R_1	1		.00660	17.36	.802	2.27858	1.500	4.111	PER IMP=	80.00
ROUTE MCUNGE	3B.3	1& 2	2	.45606	735.75	48.858	2.00868	1.550	2.521		
*S *****	3B.9	2	1	.45606	735.75	48.858	2.00868	1.550	2.521	CCODE =	.0
*S INSERT BHI HYDROLOGY											
COMPUTE NM HYD	BASINA	-	3	.00680	15.00	.636	1.75423	1.500	3.447	PER IMP=	53.20
*S *****	BASIN B			*****	*****	*****					
COMPUTE NM HYD	BASINB	-	4	.01506	33.20	1.409	1.75423	1.500	3.445	PER IMP=	53.20
*S *****	ADD BASINS A AND B			*****	*****	*****					
ADD HYD	A.B	3& 4	5	.02186	48.20	2.045	1.75421	1.500	3.445		
*S *****	BASIN C			*****	*****	*****					
COMPUTE NM HYD	BASINB	-	6	.00834	18.40	.780	1.75423	1.500	3.446	PER IMP=	53.20
*S *****	ADD BASINS A, B, AND C (INTO MH 15)			*****	*****	*****					
ADD HYD	A.B.C	5& 6	7	.03020	66.60	2.825	1.75420	1.500	3.446		
*S *****				*****	*****	*****					

[illegible]

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*****
*S *****
*S ADD BASINS H AND I
  H,I 1& 3 3 0.01859 40.28 1.685
*****
*S *****
*S COMPUTE NM HYD BASIN J 1 0.00170 3.76 .159
*****
*S *****
*S ADD BASINS H,I AND J
  H,I,J 1& 3 3 0.02029 44.04 1.844
*****
*S *****
*S ADD BASINS D,E,F,G AND H,I,J (INTO MH 18)
  EFG,H,IJ 2& 3 2 0.06200 136.84 5.808
*****
*S *****
*S END BHI HYDROLOGY, FOLLOWING WCEA BASINS OMITTED
  ADD BHI EFG,H,IJ AND PREVIOUSLY ADDED 78.9
*****
*S *****
*S ADD HYD 78.91 2& 7 2 .54826 916.39 57.491
  COMPUTE NM HYD 17.00 1 1 .02340 36.85 1.209
  ADD HYD 17.10 1& 2 3 .57166 949.67 58.699
  COMPUTE NM HYD 48 1 1 .04810 108.15 4.571
  *S Route 48 to the Intersection of Cabezon and Trailside
  ROUTE MCUNGE 48.9 1 2 .04810 107.17 4.571
  COMPUTE NM HYD R_3 1 1 .00520 12.95 .568
  *S Add 48 and Road Section 3
  ADD HYD 48.91 1& 2 2 .05330 120.12 5.139
  COMPUTE NM HYD 5A 1 1 .03130 70.94 3.017
  *S Add 48.91 and 5A at Intersection of Cabezon and Trailside
  ADD HYD 5A.1 1& 2 2 .08460 191.06 8.156
  ROUTE MCUNGE 5A.9 2 1 .08460 187.66 8.156
  ADD HYD POND.IN 1& 3 1 .65626 1131.32 66.855
  *S ROUTE FLOWS THROUGH Pond/Park in Unit 17
  *S Pond Based on final design grades with 7 ac-ft of
  *S low storage/wq and then filling remainder of park/field

COMMAND HYDROGRAPH FROM TO AREA PEAK RUNOFF
IDENTIFICATION NO. ID NO. (SQ MI) DISCHARGE (CFS) VOLUME (AC-FT)

*S graded at 2%
ROUTE RESERVOIR P.Out 1 2 .65626 474.74 66.541
*S *****
DIVIDE HYD HYD TO UNBULK BY 3% *****
  P.Out.3 2 2 .63657 460.50 64.545
  SEDIMENT and 51 .01969 14.24 1.996
*S Route unbulked pond outflow at 17 to east end of 15
  through a 60" pipe
ROUTE MCUNGE P.Out.9 2 1 .63657 460.50 64.545
*S END OF CABEZON PHASE 1, BEGIN PHASE 2 DEVELOPMENT
*S BLWMP SUBBASINS 255,256,540,530B REMOVED;
*S 255 REPLACED BY TRACTS 15,16; 256 REPLACED BY 8,9,18;
*S 540 REPLACED BY 10,20; 530B REPLACED BY 10,20
COMPUTE NM HYD 15.00 2 2 .02300 59.57 2.765
ADD HYD 15.10 1& 2 2 .65957 477.95 66.947
ROUTE MCUNGE 15.90 2 1 .65957 477.95 66.947
COMPUTE NM HYD 7D 1 2 2 .07932 174.52 7.251
ADD HYD 7D.1 1& 2 2 .73889 586.79 74.198
ROUTE MCUNGE 7D.91 2 1 .73889 586.79 74.198
COMPUTE NM HYD 18.00 2 2 .00780 12.29 .403
ADD HYD 18.10 1& 2 2 .74669 597.90 74.601
COMPUTE NM HYD 16.00 1 1 .03090 68.82 2.834
ADD HYD 18.20 1& 2 2 .77759 660.77 77.435
*S Route combined flow at 18 to East Branch
  through a 78" pipe
ROUTE MCUNGE 18.90 2 3 .77759 660.77 77.435
*****

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COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =
COMPUTE NM HYD	8.00	-	1	.02970						12
ADD HYD	8.10	3& 1	12	.80729						
\$S ABOVE IS ALL FLOW TO EAST BRANCH VIA TRIBUTARY B CONTRIBUTING AREA										
\$S RESUME BLWMP FILE										
\$*****										
\$S East Branch Main Channel]										
\$*****										
\$S ** START OF LEMA CHANNEL										
SEDIMENT BULK										
COMPUTE NM HYD	201.00	-	1	.24840						
ROUTE MCUNGE	201.90	1	2	.24840						
COMPUTE NM HYD	204.00	-	1	.01500						
ADD HYD	204.10	1& 2	5	.26340						
\$S ** START OF SNEAD CHANNEL										
COMPUTE NM HYD	203.00	-	1	.09140						
\$S ** CONFLUENCE OF LEMA AND SNEAD										
ADD HYD	205.10	5& 1	5	.35480						
ROUTE MCUNGE	205.90	5	2	.35480						
COMPUTE NM HYD	202.00	-	1	.12390						
ROUTE MCUNGE	202.90	1	4	.12390						
COMPUTE NM HYD	203.00	-	1	.05390						
\$S WESTERN HILLS DR. @ BLACK'S ARROYO (EAST BRANCH)										
\$S ** AP 203.10										
ADD HYD	203.10	4& 1	5	.17780						
ADD HYD	203.20	5& 2	5	.53260						
ROUTE MCUNGE	203.91	5	2	.53260						
COMPUTE NM HYD	212.00	-	1	.09950						
ADD HYD	212.10	1& 2	5	.63210						
COMPUTE NM HYD	213.00	-	1	.10800						
ROUTE MCUNGE	213.90	1	4	.10800						
ADD HYD	213.20	5& 4	4	.74010						
\$S ** START OF NICKLAUS CHANNEL										
COMPUTE NM HYD	214.00	-	1	.19090						
ROUTE MCUNGE	214.90	1	2	.19090						
COMPUTE NM HYD	216.00	-	1	.09660						
\$S COMBINE HYD. 'S	214.9	AND	216	AT	216.1					
\$*****										
\$S CASPER DR. @ 150 FT. W. OF NICKLAUS DR.										
\$S ** AP 216.10										
ADD HYD	216.10	1& 2	6	.28750						
COMPUTE NM HYD	215.00	-	1	.11020						
ROUTE MCUNGE	215.90	1	3	.11020						
ADD HYD	216.20	6& 3	6	.39770						
\$S ** AFTER SNEAD AND NICKLAUS CONFLUENCE										
\$*****										
ADD HYD	216.30	6& 4	5	1.13780						
COMPUTE NM HYD	217B	-	2	.06660						
\$S ROUTE 217B DOWN SOUTHERN TO THE PLAYERS CHANNEL										
ROUTE MCUNGE	217B.90	2	3	.06660						
COMPUTE NM HYD	217A	-	1	.19020						
\$S COMBINE HYD. 'S	217A AND 217B AT PLAYERS CHANNEL									
ADD HYD	217A.10	1& 3	1	.25680						
\$S ** EAST BRANCH CROSSING SOUTHERN BLVD.										
\$S SOUTHERN BLVD. @ 2100 FT. W. OF GOLF COURSE RD.										
\$*****										
ADD HYD	217.20	5& 1	5	1.39460						

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*S CABEZON PHASE 2 REVISIONS RESUME BELOW; FLOW FROM EAST BRANCH NORTH OF
 *S SOUTHERN BLVD ROUTED IN IMPROVED EAST BRANCH
 *S SEDIMENT BULK AT 6% FOR CABEZON LINED CHANNEL

ROUTE MCUNGE 217.90 5 2 1.39460 2098.80 132.342
 *S CABEZON PHASE 2 REVISIONS: BLWMP SUBBASINS 218A,218B,219,220 REMOVED;
 *S 218A REPLACED BY OFF_4, OFF_5, TRACT 6; 218B REPLACED BY TRACTS 19,1;
 *S 219 REPLACED BY TRACTS 5A,5B,5C,2, OFF_4, OFF_7, OFF_8, A_1(CHANNEL);
 *S 220 REPLACED BY TRACTS 8,2

COMPUTE NM HYD 217.90 5 2 1.39460 2098.80 132.342
 ADD HYD OFF_4 1 1 1.04980 105.55 4.171
 COMPUTE NM HYD OFF_4 1 1 1.44440 2154.93 136.514
 ADD HYD OFF_5 1 1 1.02540 56.89 2.369
 ROUTE MCUNGE OFF_5 1 1 1.46980 2185.06 138.882
 COMPUTE NM HYD OFF_5 1 1 1.46980 2185.06 138.882
 ADD HYD OFF_6 1 1 1.02620 55.54 2.195
 ROUTE MCUNGE OFF_6 1 1 1.49600 2212.28 141.072
 COMPUTE NM HYD OFF_6 1 1 1.49600 2205.75 141.047
 ADD HYD 6.00 1 1 1.09570 217.66 9.299
 COMPUTE NM HYD 19.00 1 1 1.00780 12.29 4.403
 ADD HYD 19.10 1 1 1.10350 229.95 9.701
 *S * * * START OF GOLF COURSE CHANNEL * * * * *

SEDIMENT BULK

*S GOLF COURSE ROAD STORM DRAIN SYSTEM WITH TWO OUTFALLS UPSTREAM OF

*S 23RD AVENUE PONDS
 *S BLWMP SUBBASIN 500, SW CORNER OF SOUTHERN AND GOLF COURSE
 COMPUTE NM HYD 500.00 3 3 1.02610 52.98 2.651
 *S ROUTE 500 IN TYPICAL ROADWAY CROSS-SECTION TO EAST BRANCH
 ROUTE MCUNGE 500.90 3 4 1.02610 52.79 2.653
 ADD HYD 19.20 4 2 1.12960 268.57 12.354
 ADD HYD 19.30 2 1 1.62560 2375.40 153.401
 COMPUTE NM HYD OFF_7 1 1 1.01060 22.48 .888
 *S Route off_7 through off_8 to the East Branch
 ROUTE MCUNGE OFF_7 1 1 1.01060 21.99 .886
 COMPUTE NM HYD OFF_8 1 1 1.01500 31.80 1.256
 ADD HYD OFF_8 1 1 1.02560 41.81 2.143

COMMAND FROM TO HYDROGRAPH ID NO. ID NO. AREA (SQ MI) PEAK DISCHARGE (CFS) RUNOFF VOLUME (AC-FT)
 ADD HYD 19.40 2 1 2 1.65120 2414.30 155.543
 COMPUTE NM HYD A_1 1 1 1.03170 71.46 2.936
 ADD HYD 19.50 2 1 2 1.68290 2452.08 158.479
 *S ROUTE UNBULKED THROUGH A_2 (EAST BRANCH) TO SOUTHERN END OF 5
 ROUTE MCUNGE 19.90 2 4 1.68290 2446.60 158.469
 COMPUTE NM HYD 58 1 1 1.01960 44.63 1.904
 ADD HYD 58.10 4 1 2 1.70250 2465.82 160.374
 *S PORTION OF EAST BRANCH WITHIN CABEZON
 COMPUTE NM HYD A_2 1 1 1.00810 18.27 .750
 ADD HYD 58.20 2 1 3 1.71060 2473.65 161.124
 *S ROUTE 58.20 TO EAST BRANCH CROSSING CABEZON BLVD VIA A_3
 ROUTE MCUNGE 58.90 3 2 1.71060 2453.09 161.133
 COMPUTE NM HYD 2.00 1 1 1.03220 68.44 2.703
 ADD HYD 2.10 2 1 5 1.74280 2482.24 163.836
 COMPUTE NM HYD 1.00 1 1 1.11170 237.29 9.376
 *S 510A is small area between Cabazon subbasin 1 and
 *S BLWMP Subbasin 510- used same treatments as 510
 COMPUTE NM HYD 510A 2 2 1.01320 32.19 1.443
 ADD HYD 1.10 1 2 3 1.12490 269.49 10.820
 COMPUTE NM HYD 510.00 1 1 1.04080 75.92 3.729

1.77930 1.650 2.351 CCODE = 1.06
 1.57058 1.500 3.312 PER IMP= 42.00
 1.77211 1.650 2.331
 1.74862 1.500 3.500 PER IMP= 52.00
 1.77170 1.650 2.323
 1.77164 1.650 2.320 CCODE = .2
 1.57059 1.500 3.312 PER IMP= 42.00
 1.76811 1.650 2.311
 1.76780 1.650 2.304 CCODE = .2
 1.82184 1.500 3.554 PER IMP= 56.90
 1.96836 1.500 2.462 PER IMP= 15.00
 1.75752 1.500 3.472

PK BF = 1.06

1.90437 1.550 3.172 PER IMP= 60.00
 1.90565 1.600 3.161 CCODE = .2
 1.78734 1.500 3.238
 1.76935 1.650 2.283
 1.57058 1.500 3.313 PER IMP= 42.00
 1.56759 1.650 3.241 CCODE = .1
 1.57059 1.500 3.313 PER IMP= 42.00
 1.56930 1.600 2.552

CFS PER ACRE NOTATION
 TIME TO PEAK (HOURS)
 RUNOFF (INCHES)
 1.76625 1.650 2.285
 1.73643 1.500 3.522 PER IMP= 50.00
 1.76569 1.650 2.277
 1.76558 1.700 2.272 CCODE = .1
 1.82184 1.500 3.558 PER IMP= 56.90
 1.76623 1.700 2.263
 1.73643 1.500 3.524 PER IMP= 50.00
 1.76609 1.700 2.259
 1.76619 1.700 2.241 CCODE = .2
 1.57390 1.500 3.321 PER IMP= 42.00
 1.76263 1.700 2.225
 1.57391 1.500 3.319 PER IMP= 42.00
 2.05017 1.500 3.811 PER IMP= 68.00
 1.62423 1.500 3.371
 1.71381 1.550 2.907 PER IMP= 51.00

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*S ROUTE 510 IN TYPICAL ROADWAY CROSS-SECTION TO EAST BRANCH									
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 14
ADD HYD	510.90	1	2	.04080	74.66	3.722	1.71059	2.859	CCODE =
ADD HYD	1.20	3& 2	4	.16570	287.12	14.542	1.64549	2.707	.1
ADD HYD	2.20	4& 5	3	1.90850	2672.22	178.377	1.75246	2.188	
COMPUTE NM HYD	5C	-	1	.02890	65.80	2.808	1.82184	3.557	PER IMP=
COMPUTE NM HYD	5C.9	1	2	.02890	64.44	2.808	1.82205	3.484	CCODE =
ADD HYD	R_4	-	1	.00990	24.64	1.081	2.04713	3.889	PER IMP=
ADD HYD	R_4.9	1& 2	1	.03880	89.08	3.889	1.87945	3.587	
COMPUTE NM HYD	A_3	-	1	.00800	18.05	182.267	1.75499	2.178	
ADD HYD	2.40	3& 1	2	1.94730	2713.83	182.267	1.73643	3.524	PER IMP=
COMPUTE NM HYD	A_3	-	1	.00800	18.05	183.007	1.75492	2.175	50.00
ADD HYD	2.50	2& 1	2	1.95530	2721.56	183.007	1.75492	2.175	
COMPUTE NM HYD	R_5	-	1	.00760	18.92	.830	2.04712	3.890	PER IMP=
ADD HYD	R_5.10	2& 1	2	1.96290	2729.73	183.837	1.75605	2.173	66.00
*S ROUTE R_5.10 TO R_5.90 VIA EAST BRANCH PROPOSED CHANNEL									
ROUTE MCUNGE	R_5.90	2	1	1.96290	2721.59	183.831	1.75599	2.166	CCODE =
ADD HYD	8.20	1&12	2	2.77019	3311.29	264.163	1.78798	1.868	.1
*S ROUTE 8.20 TO END OF SUBBASIN 9 VIA EAST BRANCH CHANNEL (8.90)									
ROUTE MCUNGE	8.90	2	1	2.77019	3311.29	264.163	1.78798	1.868	
COMPUTE NM HYD	A_4	-	2	.00620	13.99	.574	1.73643	3.525	CCODE =
ADD HYD	8.93	2& 1	1	2.77639	3316.32	264.737	1.78787	1.866	PER IMP=
COMPUTE NM HYD	9.00	-	2	.04480	102.75	4.410	1.84577	3.584	50.00
ADD HYD	9.10	2& 1	1	2.82119	3353.69	269.147	1.78879	1.857	PER IMP=
*S ROUTE 9.10 TO 9.90 (DS end of CAB SUBBASIN 21 in EAST BRANCH)									
ROUTE MCUNGE	9.90	1	2	2.82119	3335.75	269.124	1.78863	1.847	CCODE =
COMPUTE NM HYD	21.00	-	1	.02340	60.61	2.813	2.25374	4.047	PER IMP=
ADD HYD	21.10	2& 1	2	2.84459	3356.16	271.937	1.79246	1.843	80.00
COMPUTE NM HYD	10.00	-	1	.12980	294.96	12.612	1.82184	3.551	PER IMP=
COMPUTE NM HYD	20.00	-	3	.00780	12.29	.403	.96836	2.462	56.90
ADD HYD	20.10	1& 3	1	2.98219	307.25	13.015	1.77345	3.489	PER IMP=
ADD HYD	20.20	2& 1	1	2.98219	3451.24	284.952	1.79158	4.013	PER IMP=
COMPUTE NM HYD	R_8	-	2	.01180	30.31	1.371	2.17883	4.120	PER IMP=
COMPUTE NM HYD	R_7	-	3	.00170	4.48	.207	2.27858	4.120	PER IMP=
ADD HYD	R_8.10	2& 3	4	.01350	34.79	1.578	2.19135	4.027	80.00
*S Route combined flows at R_8.10 through 36" pipe IN ROADWAY TO DS END OF 14									
ROUTE	R_8.90	4	3	.01350	32.28	1.578	2.19140	3.736	
COMPUTE NM HYD	R_9	-	2	.01540	39.55	1.790	2.17882	4.013	PER IMP=
ADD HYD	R_9.10	3& 2	3	.02890	70.47	3.367	2.18467	3.810	74.00
*S ROUTE 20.30 1& 3 9 3.01109 3477.62 288.319									
ADD HYD	20.30	1& 3	9	3.01109	3477.62	288.319	1.79536	1.805	
*S RESUME BLWMP WITH SUBBASINS WEST OF GOLF COURSE, IN UNIT 16 BUT									
*S NOT PART OF CABEZON									
*S REMAINDER OF GOLF COURSE ROAD STORM DRAIN SYSTEM									
SEDIMENT BULK									
COMPUTE NM HYD	520.00	-	1	.04090	82.95	3.427	1.57126	3.169	PK BF =
*S ROUTE 520 TO 530C AT 520.90	520.90	1	3	.04090	81.34	3.423	1.56905	3.107	PER IMP=
ROUTE MCUNGE	530A	-	2	.14730	291.77	12.212	1.55444	3.095	43.00
COMPUTE NM HYD	530A	-	2	.14730	291.77	12.212	1.55444	3.095	CCODE =
*S *****AP 530A.90 (20PP.IN) *****									
*S ROUTE 530A THROUGH 20TH AVENUE PARK POND SIZE AND VOLUME ARE ASSUMED									
*S BASED ON FIELD INVESTIGATION BUT NOT ON A COMPREHENSIVE SURVEY.									
*S THIS POND HAS AN OVERFLOW ON THE TWO LOTS ON THE SOUTH EDGE AND									
*S IS MODELED WITH THE PROPOSED EXPANSION.									
ROUTE RESERVOIR	530A.90	2	7	.14730	61.58	12.212	1.55444	.653	AC-FT=
*S *****DIVIDE HYD TO UNBULK TO 3% *****	530A.90	2	7	.14730	61.58	12.212	1.55444	.653	5.377
DIVIDE HYD	UNBULK	7	7	.14288	59.73	11.845	1.55444	.653	


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SEDIMENT and 57 VOL81604.SUM
***** AP 20PP.OUT ***** 00442 1.85 .366
*S ROUTE 530A.90 "UNBULKED" THROUGH STORM DRAIN TO GOLF COURSE ROAD SYSTEM.
*S OUTFALL PIPE IS 48" CMP.
ROUTE MCUNGE 530A.91 7 99 .14288 59.73 11.842
*S PUNCH HYDROGRAPH FOR GOLF COURSE ROAD STORM DRAIN DESIGN MODEL
*S COMBINE 530A.91 AND 520.90 AT STORM DRAIN OUTFALL TO GCR SYSTEM
ADD HYD 530A.10 99& 3 3 .18378 137.78 15.264
*S ROUTE COMBINED HYDROGRAPHS IN PIPE TO 23RD AVENUE
ROUTE MCUNGE 530A.92 3 2 .18378 136.48 15.249
*S COMPUTE 530C
COMPUTE NM HYD 530C - 1 .02530 50.49 1.940
*S COMPUTE 530D 23RD AVE. POND BASIN
COMPUTE NM HYD 530D - 3 .01000 15.95 .442
*S ADD 530D TO 530C
ADD HYD 530D.10 1& 3 3 .03530 66.44 2.383
*S ADD ROUTED 520 AND 530A TO 530C
ADD HYD 530D.20 2& 3 2 .21908 174.23 17.631
*S ***** AP 530.90 (GC.OUT) *****
*S ROUTE COMBINED FLOW THROUGH 23RD AVENUE PONDS
*****
*S THE PONDS ARE COMBINED AND TREATED AS ONE TEN ACRE FOOT POND FOR
*S FOR THIS MODEL.
ROUTE RESERVOIR 530.90 2 3 .21908 47.77 17.607
*S THIS RESERVOIR NOT UNBULKED
ROUTE MCUNGE 530.91 3 2 .21908 47.77 17.606
*S CABEZON PHASE 2 RESUMES BELOW: PART OF BLWMP SUBBASIN 550 IS REPLACED BY
*S TRACT 21 AND A_5 (WEST BRANCH)
*S COMBINE ROUTED FLOW WITH EAST BRANCH FLOW:
ADD HYD 20.40 9& 2 1 3.23017 3495.49 305.925
ADD HYD A_5 - 2 .01210 27.29 1.121
ADD HYD 20.50 1& 2 1 3.24227 3503.88 307.045
*S ROUTE IN EAST BRANCH TO BLACK DAM
ROUTE MCUNGE 20.90 1 2 3.24227 3474.91 306.973
*S Area of 550 is reduced by area that it overlaps
*S CABEZON basins
COMPUTE NM HYD 550.00 - 1 .02760 47.77 1.540
ADD HYD EAST 2& 1 1 3.26987 3484.61 308.513
ADD HYD DAM.10 1&1 97 8.84598 8392.24 693.218
*S RECALL HYDROGRAPHS FROM BERNALILLO COUNTY SUBDIVISIONS
*S THESE ARE PUNCH HYDROGRAPHS AND FLOWS DRAIN DIRECTLY TO THE DAM POOL
*S VIA PIPES.

```

TEXT TAKEN FROM MODEL RECEIVED 1/9/02 * * * * *

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)
*S	Ridgeview Village(DB4), Los Suenos(DB3), and the Park Hill(DB2)					
*S	subdivisions have free developed discharge based on R-1, 5 du/acre density.					
*S	Flow from some commercial sites east of Unser between McMahon and					
*S	Black Arroyo Blvd. is restricted to historic as per Ridgeview Unit 1 Plan.					
*S	Developed flow is accommodated from the residential tracts and					
*S	other commercial tracts. * * * * *					
RECALL HYD	AP5	-	18	.38090	850.60	31.937
*S	STONEBRIDGE SUBDIVISION FROM MODEL RECEIVED 1/15/02					
RECALL HYD	API5	-	19	.23850	359.51	17.620
*S	ADD RECALL HYDROGRAPHS					
ADD HYD	DIRECT PIPE 18&19	98		.61940	1191.72	49.556
*S	ADD RECALL HYDS TO EAST AND WEST BRANCH FLOWS FOR TOTAL INTO BLACK DAM				9047.84	742.774
ADD HYD	DAM.IN 98&97	99		9.46538		

VOL81604.SUM

*S ROUTE FLOWS THROUGH WQ STRUCTURE NO. 2
*S BEFORE ENTERING BLACK DAM
*S

ROUTE RESERVOIR

*S *****DIVIDE HYD P.Out 99 98 9.46538 9352.09 762.355
DIVIDE HYD P.Out.3 98 98 9.18141 9071.53 739.484
SEDIMENT and 51 .28396 280.56 22.871

*S ROUTE FLOWS THROUGH BLACK DAM RATING CURVE TAKEN FROM BLACK DAM

*S FILING SHEET RECORD DRAWINGS - BLARD-51 Stamp dated 9/14/91

*S Record Dwg Stamp 11/9/92 AMAFCA Ref # NW-04-114 Calabacillas

*S THIS IS THE FUTURE CONDITIONS RATING CURVE

*S 5/04/04 BLACK DAM RATING CURVE ADJUSTED FOR CABEZON MODEL:

*S ELEVATIONS CONVERTED TO NAVD88 FROM NGVD29; ALSO

*S STORAGE INCREASED TO REFLECT WQ STRUCTURE NO.2

ROUTE RESERVOIR DAM.R 98 91 9.18141 2524.35 739.084

*S EMERGENCY SPILLWAY CREST IS AT ELEV 5168.55 FT (NAVD88)

FINISH
0(S10H

1.51015 1.700 1.544 AC-FT= 30.625

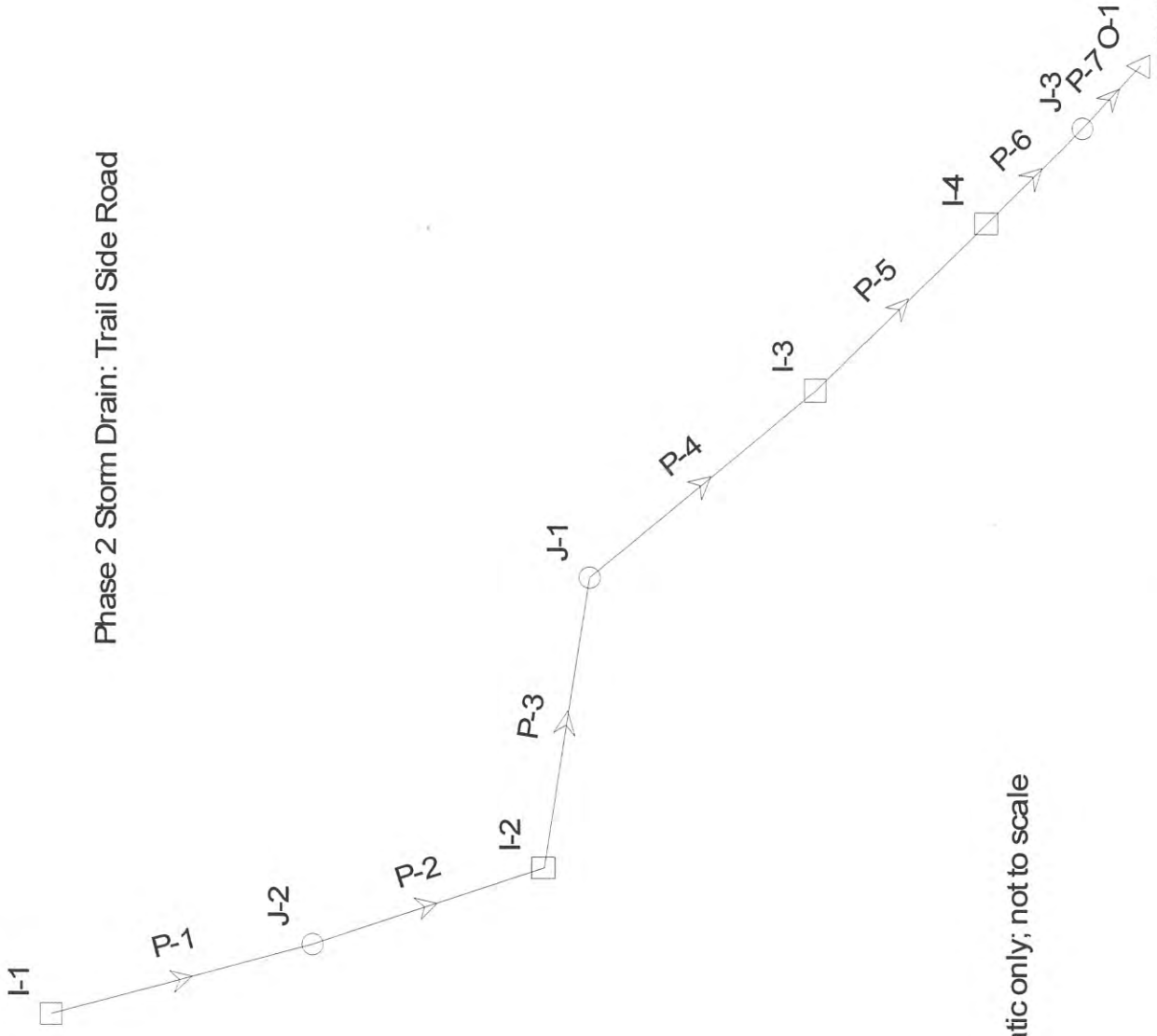
1.51015 1.700 1.544
1.51015 1.700 1.544

1.50933 2.400 .430 AC-FT= 314.594

APPENDIX B

Hydraulics

Scenario: Base



Schematic only; not to scale

Scenario: Base

Pipe Report

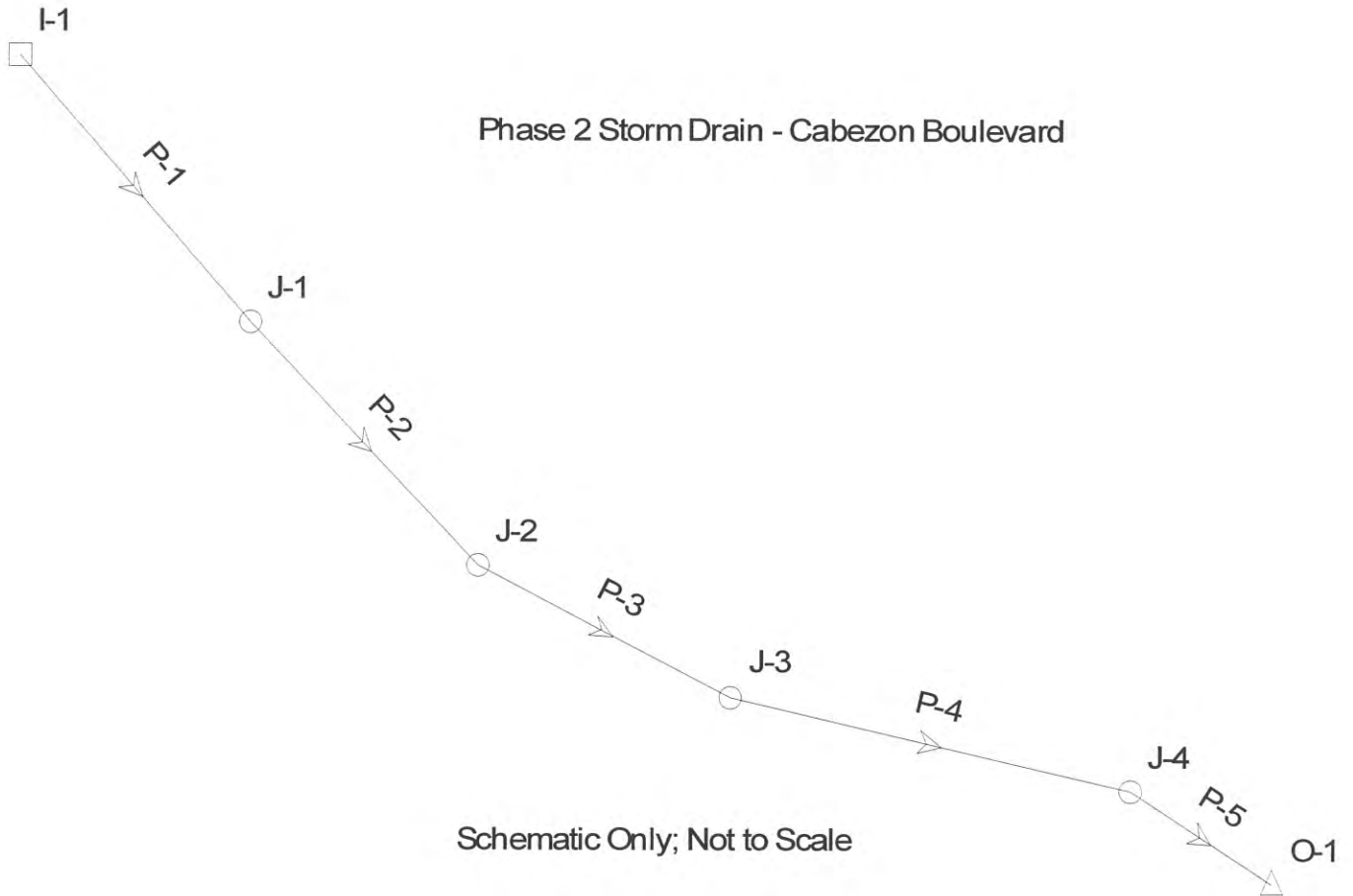
Label	Length (ft)	Section Size	Constructed Slope (ft/ft)	Bend Angle (degrees)	Average Velocity (ft/s)	Total System Flow (cfs)	Depth In (ft)	Depth Out (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Downstream Ground Elevation (ft)	Upstream Ground Elevation (ft)	Gravity Element Headloss (ft)	Mannings n
P-1	300.00	66 inch	0.022567	0.00	21.21	504.00	5.55	5.56	5,265.05	5,258.29	5,259.50	5,252.73	5,263.63	5,270.00	6.76	0.013
P-2	500.00	72 inch	0.024460	64.00	25.78	504.00	5.96	11.12	5,258.19	5,251.12	5,252.23	5,240.00	5,253.00	5,263.63	7.07	0.013
P-3	252.00	72 inch	0.022659	26.00	21.68	613.00	9.88	10.31	5,249.88	5,244.60	5,240.00	5,234.29	5,251.09	5,253.00	5.28	0.013
P-4	500.00	72 inch	0.027420	1.00	21.68	613.00	9.36	12.59	5,243.65	5,233.17	5,234.29	5,220.58	5,239.55	5,251.09	10.48	0.013
P-5	502.50	72 inch	0.021453	0.00	24.37	689.00	12.32	9.79	5,232.90	5,219.59	5,220.58	5,209.80	5,229.75	5,239.55	13.30	0.013
P-6	93.00	72 inch	0.019355	0.00	26.77	757.00	9.68	8.51	5,219.48	5,216.51	5,209.80	5,208.00	5,228.75	5,229.75	2.97	0.013
P-7	200.00	8 x 4 ft	0.017500	0.00	23.66	757.00	6.34	4.00	5,214.34	5,208.50	5,208.00	5,204.50	5,217.00	5,228.75	5.84	0.013

Scenario: Base

Junction Report

Label	Ground Elevation (ft)	Rim Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Structure Diameter (ft)	Headloss Coefficient	Headloss Method	Depth In (ft)	Depth Out (ft)
J-1	5,251.09	5,251.09	5,244.60	5,243.65	4.00	0.13	Standard	10.31	9.36
J-2	5,263.63	5,263.63	5,258.29	5,258.19	4.00	0.02	Standard	6.06	5.96
J-3	5,228.75	5,228.75	5,216.51	5,214.34	4.00	0.25	Standard	8.51	6.34

Scenario: Base



Scenario: Base

Inlet Report

Label	Ground Elevation (ft)	Rim Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Sump Elevation (ft)	Known Flow (cfs)	Headloss Method	Headloss Coefficient	Depth In (ft)	Depth Out (ft)
I-4	5,229.75	5,229.75	5,219.59	5,219.48	5,209.80	757.00	Standard	0.01	9.79	9.68
I-3	5,239.55	5,239.55	5,233.17	5,232.90	5,220.58	689.00	Standard	0.03	12.59	12.32
I-2	5,253.00	5,253.00	5,251.12	5,249.88	5,240.00	613.00	Standard	0.17	11.12	9.88
I-1	5,270.00	5,270.00	5,265.40	5,265.05	5,259.50	504.00	Standard	0.05	5.90	5.55

Scenario: Base

Pipe Report

Label	Length (ft)	Section Size	Constructed Slope (ft/ft)	Bend Angle (degrees)	Average Velocity (ft/s)	Total System Flow (cfs)	Depth In (ft)	Depth Out (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Downstream Ground Elevation (ft)	Upstream Ground Elevation (ft)	Gravity Element Headloss (ft)	Mannings n
P-1	375.00	36 inch	0.028987	2.00	17.78	89.04	2.84	2.92	5,285.42	5,274.63	5,282.58	5,271.71	5,279.54	5,287.08	10.79	0.013
P-2	350.00	36 inch	0.029000	3.00	17.79	89.04	2.84	3.05	5,274.55	5,264.61	5,271.71	5,261.56	5,268.62	5,279.54	9.94	0.013
P-3	250.00	36 inch	0.044000	10.00	20.97	89.04	2.84	3.05	5,264.40	5,253.61	5,261.56	5,250.56	5,260.36	5,268.62	10.79	0.013
P-4	290.00	36 inch	0.044000	17.00	20.97	89.04	2.84	3.12	5,253.40	5,240.92	5,250.56	5,237.80	5,253.09	5,260.36	12.48	0.013
P-5	65.00	36 inch	0.044000	0.00	20.97	89.04	2.84	2.02	5,240.64	5,236.96	5,237.80	5,234.94	5,248.00	5,253.09	3.68	0.013

Scenario: Base

Inlet Report

Label	Ground Elevation (ft)	Rim Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Sump Elevation (ft)	Known Flow (cfs)	Headloss Method	Headloss Coefficient	Depth In (ft)	Depth Out (ft)
I-1	5,287.08	5,287.08	5,285.45	5,285.42	5,282.58	89.04	Standard	0.01	2.87	2.84

Scenario: Base

Junction Report

Label	Ground Elevation (ft)	Rim Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Structure Diameter (ft)	Headloss Coefficient	Headloss Method	Depth In (ft)	Depth Out (ft)
J-4	5,253.09	5,253.09	5,240.92	5,240.64	4.00	0.11	Standard	3.12	2.84
J-3	5,260.36	5,260.36	5,253.61	5,253.40	4.00	0.08	Standard	3.05	2.84
J-2	5,268.62	5,268.62	5,264.61	5,264.40	4.00	0.08	Standard	3.05	2.84
J-1	5,279.54	5,279.54	5,274.63	5,274.55	4.00	0.03	Standard	2.92	2.84

