

CITY OF ALBUQUERQUE

Planning Department
David Campbell, Director



Mayor Timothy M. Keller

June 14, 2018

Diane Hoelzer, P.E.
Mark Goodwin & Associates
PO Box 90606
Albuquerque, NM, 87199

RE: Anasazi Ridge Unit 3
Drainage Report, Engineer's Stamp Date: 05/09/18
Supplemental Rundown Calculations, Engineer's Stamp Date: 05/09/18
Grading and Drainage Plan, Engineer's Stamp Date: 05/09/18
Hydrology File: A10D002G

Dear Ms. Hoelzer:

Based upon the information provided in your submittal received 05/14/18, the Drainage Report, Supplemental Rundown Calculations, and Grading and Drainage Plan which were originally approved on March 12, 2015 is re-approved for action by the DRB on the Preliminary Plat.

If you have any questions, please contact me at 924-3995 or rbrissette@cabq.gov.

Sincerely,

Renée C. Brissette, P.E. CFM
Senior Engineer, Hydrology
Planning Department

Anasazi Ridge Unit 3
Subdivision

Supplemental Information
To
Drainage Management Plan
(dated 1-12-15)

- Revised Spillway Design
- Revised Drainage Easements



Prepared by
Mark Goodwin & Associates, PA
February 2015



D. Mark Goodwin & Associates, P.A.

Consulting Engineers

P.O. BOX 90606, ALBUQUERQUE, NM 87199

(505) 828-2200

FAX 797-9539

~ 2012 ACEC/NM Award Winner for Engineering Excellence ~

~ 2008 ACEC/NM Award Winner for Engineering Excellence ~

February 3, 2015

Ms. Lynn Mazur
AMAFCA
2600 Prospect NE
Albuquerque, NM 87107

Re: Anasazi Ridge Unit 3 – Revised Drainage Management Plan (2-2-15)

Dear Ms. Mazur:

A supplemental information report and revised grading plan have been submitted to City hydrology. Accompanying this letter is a copy of what is being submitted to the City. Below is the response to your earlier comment letter dated October 28, 2014:

1. Agreed. There is a triangular parcel of property at the southeast corner of McMahon Blvd. and Kayenta Blvd. that is owned by someone other than AMAFCA. The proposed rundown improvements will remain outside this parcel of property and remain within the public McMahon Blvd. right of way as shown on the revised grading plan.
2. The temporary 10' wide channel rundown has been added to the city infrastructure list. Whoever is maintaining the existing temporary asphalt rundown should maintain the concrete rundown. I assume this is and will be the City of Albuquerque.
3. The proposed channel is entirely within the McMahon Blvd right of way, so a license should not be necessary.
4. Ok.
5. Ok.
6. Ok. These details can be worked out during DRC approval process.

Sincerely,

MARK GOODWIN & ASSOCIATES, PA

Diane Hoelzer, PE
Senior Project Engineer

DLH/dlh

Ronald D. Brown, Chair
Danny Hernandez, Vice Chair
Bruce M. Thomson P.E., Secretary-Treasurer
Tim Eichenberg, Assistant Secretary-Treasurer
Daniel F. Lyon, Director

Jerry M. Lovato, P.E.
Executive Engineer



**Albuquerque
Metropolitan
Arroyo
Flood
Control
Authority**

2600 Prospect N.E., Albuquerque, NM 87107
Phone: (505) 884-2215 Fax: (505) 884-0214
Website: www.amafca.org

October 28, 2014

Ms. Diane Hoelzer, P.E.
D. Mark Goodwin & Associates, P.A.
P.O. Box 90606
Albuquerque, NM 87199

Via: Electronic Mail

Re: Anasazi Ridge Unit 3 Drainage Report, Engineer's Stamp Dated 10/24/14

Dear Ms. Hoelzer:

I have reviewed the referenced report and approve the drainage concept. I have the following comments on the drainage rundown connection to the Calabacillas Arroyo.

1. The Bernalillo County Assessor's Office shows AMAFCA ownership of the tract at the southeast corner of McMahon and Kayenta. That is incorrect. The plat for Saltillo Unit 1 Subdivision granted a blanket drainage easement to AMAFCA with future dedication of fee right-of-way to City Open Space. I'm not sure who owns it.
2. I don't see the temporary 10-foot wide channel rundown connection from the McMahon/Kayenta intersection to the Calabacillas Arroyo on the Infrastructure List. Who will maintain the facility?
3. If the rundown is maintained by the City, AMAFCA will prepare a license with the City for the facility in AMAFCA's easement.
4. AMAFCA will require a Temporary Construction and Access License with the owner and the owner's contractor for work in AMAFCA's easement.
5. The expansion joint on the Drainage Channel Connection Detail is not approved by AMAFCA. The connection will be similar to AMAFCA's standard detail for a pipe penetration through a wall. See attached detail. The Plastazote filler will run the entire length of the connection with NP-1 sealant at both ends.
6. AMAFCA will require a removable trash screen close to the removable bollards to collect large debris before it flows into the arroyo. See attached detail.

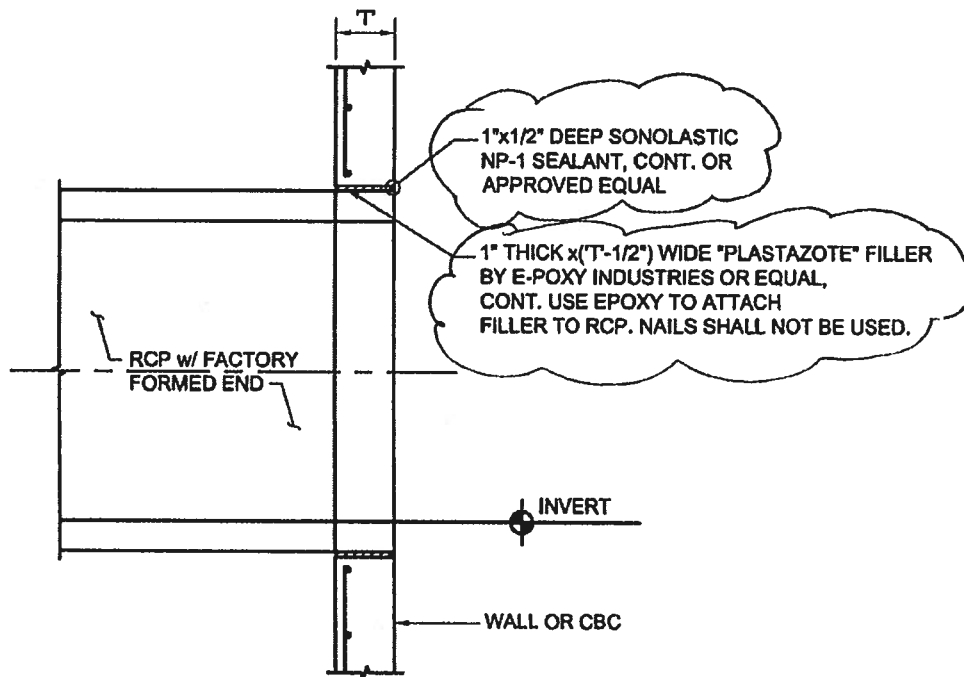
If you have any questions, please call me at 884-2215.

Sincerely,
AMAFCA

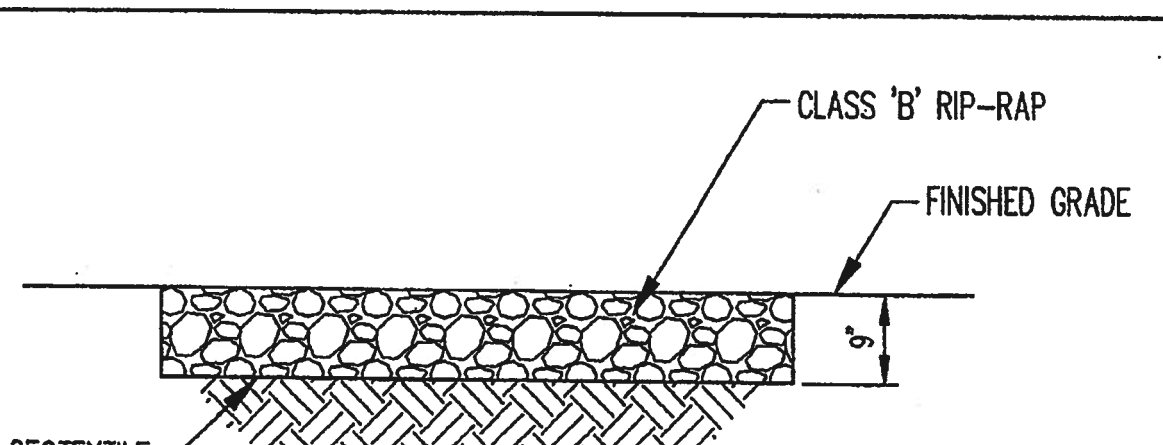
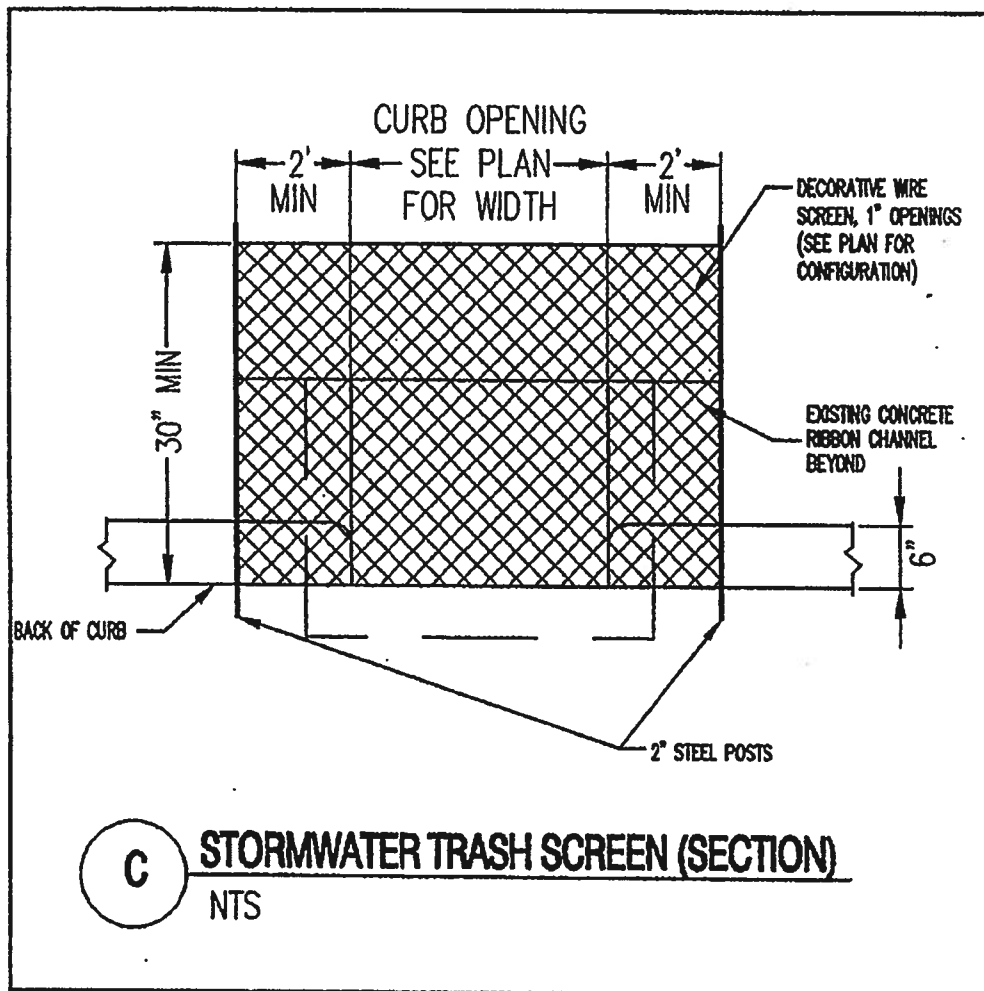
Lynn M. Mazur, P.E., C.F.M.
Development Review Engineer

C: Rita Harmon, City Hydrology

PTED BARS.
EAR FROM



PIPE PENETRATION SECTION A-A



Anasazi Ridge Unit 3

Hydraulic Analysis of the Spillway to Vizcaya Road Transition

A HEC-2 model was developed from the top of the overflow spillway to approximately 100 feet down Vizcaya Road. The 8 ft. wide channel spillway at a slope of 3:1 (0.3%) transitions to an 28' FF Vizcaya Road that is at an existing slope of 2.0%.

The flow regime in the spillway is supercritical and the flow regime in Vizcaya Road is also supercritical at a $Q=10.87$ cfs. Within the section of this analysis subcritical flow never occurs, so there should be no hydraulic jump.

The results of the HEC-2 analysis indicate that the WSEL in Vizcaya immediately downstream will be between 0.34' to 0.39'. While this is above the top of curb height for mountable curb. It is within the maximum 0.53' height that would typically exist at the property line.

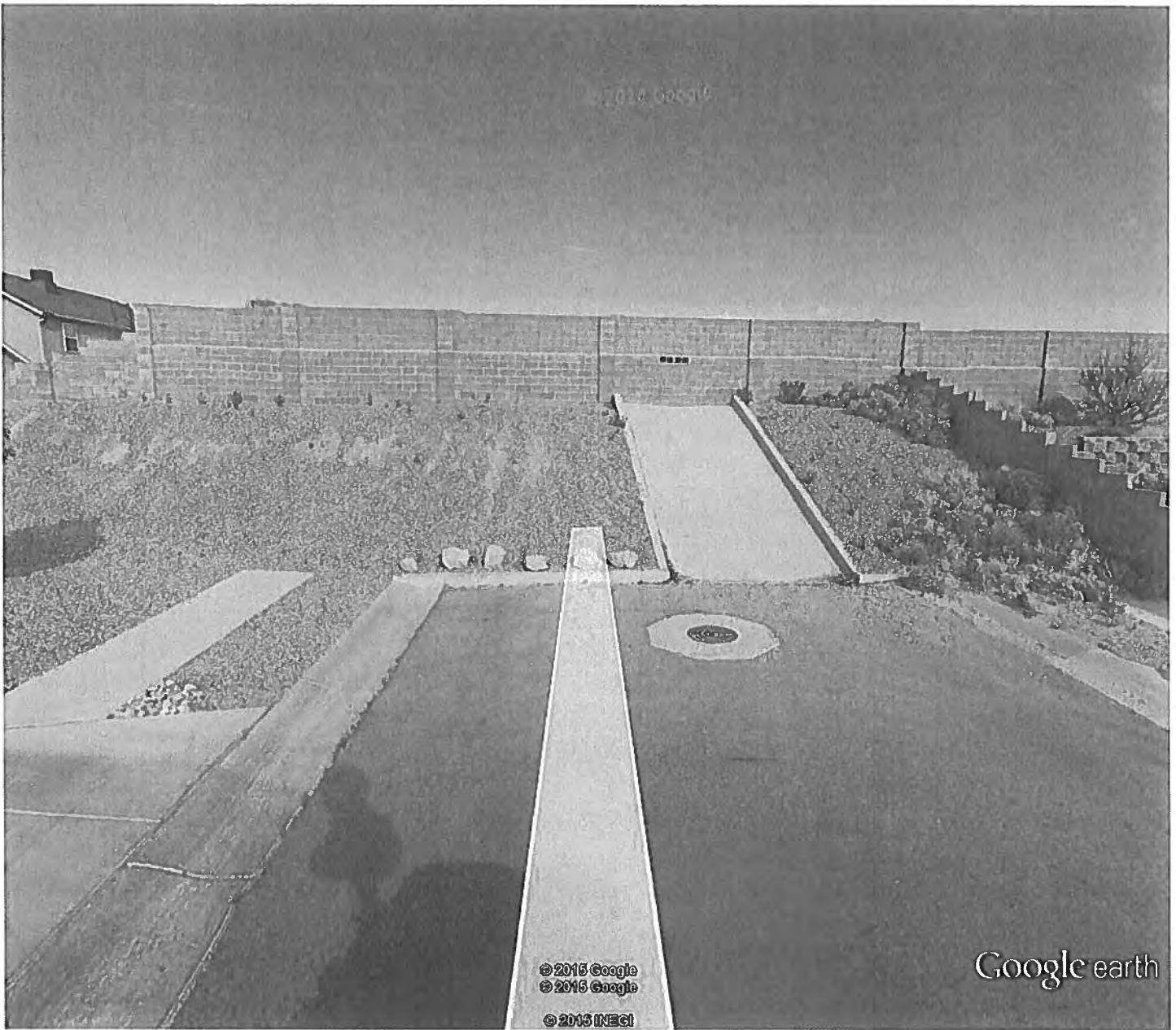
RECOMMENDATION:

It is proposed that the 8' wide channel be constructed to line up with the flow along the north side of Vizcaya Road and that the landscape rock along this side of the road be replaced with 4" concrete section from the spillway channel all the way to the intersection of Calle Gandia Road, which is a distance of approximately 80 lineal feet. This should provide adequate protection against any flow that may top the curb in this area.

Because the channel is being constructed away from the homes located on the south side of Vizcaya Road, and there will be some distance downstream before the spread of runoff would extend all the way to the south side of the road, it should not be necessary to replace the landscape rock on the south side.

See attached HEC-2 output, plan and profile exhibit and google earth photos of the existing field conditions.

It is also recommended that the first flush ponds and swales on Lots 23 and 16 be lined with landscape rock.



Google earth

feet 9
meters 2





Google earth



1 *****
* HEC-2 WATER SURFACE PROFILES
*
* Version 4.6.2; May 1991
*
* RUN DATE 21JAN15 TIME 16:00:33

* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET, SUITE D
* DAVIS, CALIFORNIA 95616-4687
* (916) 756-1104

X	X	XXXXXXX	XXXXX	XXXXX
X	X	X	X	X
X	X	X	X	X
XXXXXXX	XXXX	X	XXXXX	XXXXX
X	X	X	X	X
X	X	X	X	X

THIS RUN EXECUTED 21JAN15 16:00:33

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

Supercritical Flow
Regime Q = 10.87cfs

T1 SEVILLE UNIT 7 - STREET CAPACITY CALCULATIONS
T2 49' ROW 28' F-F MTB CURB AND GUTTER WITH CROWN
T3 VIZCAYA AVENUE

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	1	0	0	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	43	1	2	26	4	68	3
NC	.017	.017	.017	.1	.3		
QT	1	10.87	0	8.2	0	0	0
X1	1	4	0	89.25	8.1	90.25	8.2
GR	90.25	0	89.25	.1	89.25	20	0
X1	2	4	0	8.2	20	82.85	0
GR	82.85	0	81.85	.1	81.85	8.2	0
X1	3	4	0	8.2	25	25	0
GR	82.75	0	81.75	.1	81.75	8.2	0
X1	4	9	24.5	49	46	46	0
X3	10	0	0	0	0	0	0
GR	81.86	0	81.66	9.87	81.33	81.455	12.5
GR	81.455	36.5	81.33	37.53	81.66	81.86	81.695
X1	5	9	24.5	49	67	67	49
X3	10	0	0	0	0	0	0
GR	81.44	0	81.24	9.87	80.91	81.035	12.5
GR	81.035	36.5	80.91	37.53	81.24	81.44	81.275
X1	6	9	24.5	49	85	85	49
X3	10	0	0	0	0	0	0
GR	81.08	0	80.88	9.87	80.55	80.675	12.5
GR	80.675	36.5	80.55	37.53	80.88	81.08	80.915
X1	7	9	24.5	49	125	125	49

VIZCAYA AVENUE

SUMMARY PRINTOUT

Row

Depth } Channel Spillway

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG	Depth
* 1.000	10.87	89.63	89.63	3.53	8.08	1.01	89.83	0.38
* 2.000	10.87	81.92	82.23	21.55	8.01	15.15	89.13	0.07
* 3.000	10.87	81.93	82.13	7.50	8.04	3.12	82.80	0.18
* 4.000	10.87	81.70	81.72	2.43	32.77	1.19	81.80	0.37
* 5.000	10.87	81.30	81.30	2.08	34.83	.98	81.37	0.39
* 6.000	10.87	80.94	80.94	2.05	35.06	.96	81.01	0.39
* 7.000	10.87	80.12	80.14	2.34	33.27	1.13	80.22	0.37

81.86
81.44
81.08
80.28

1 21JAN15 16:00:33

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION SECNO=	1.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION SECNO=	2.000	PROFILE=	1	SLOPE TOO STEEP
WARNING SECNO=	2.000	PROFILE=	1	CONVEYANCE CHANGE OUTSIDE ACCEPTABLE RANGE
WARNING SECNO=	3.000	PROFILE=	1	CONVEYANCE CHANGE OUTSIDE ACCEPTABLE RANGE
CAUTION SECNO=	4.000	PROFILE=	1	WSEL ASSUMED BASED ON MIN DIFF
CAUTION SECNO=	4.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION SECNO=	5.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION SECNO=	5.000	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO=	5.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION SECNO=	6.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION SECNO=	6.000	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO=	6.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION SECNO=	7.000	PROFILE=	1	WSEL ASSUMED BASED ON MIN DIFF
CAUTION SECNO=	7.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL

1*****
* HEC-2 WATER SURFACE PROFILES *
* *
* Version 4.6.2; May 1991 *
* *
* RUN DATE 20JAN15 TIME 13:52:12 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

THIS RUN EXECUTED 20JAN15 13:52:12

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

Supercritical Flow
Vizcaya Road
Q = 11.87 cfs
S = 2.0%

T1 SEVILLE UNIT 7 - STREET CAPACITY CALCULATIONS
T2 49' ROW 28' F-F MTB CURB AND GUTTER WITH CROWN
T3 VIZCAYA AVENUE

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	1	.02	0	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	43	1	2	26	4	68	3
NC	.017	.017	.1	.3			
QT	1	10.87					
X1	1	9	0	49	0	0	0
GR	.53	0	.33	9.87	0	11.47	12.5
GR	.125	36.5	0	37.53	.33	39.13	49

SECCNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

3265 DIVIDED FLOW

1.000	.34	.34	.39	.00	.49	.15	.00	.00	.53
10.9	.0	10.9	.0	.0	3.5	.0	.0	.0	.53
.00	.00	3.08	.00	.000	.017	.000	.000	.00	9.24
.020084	0.	0.	0.	0	14	7	.00	28.29	39.76

THIS RUN EXECUTED 20JAN15 13:52:12

 HEC-2 WATER SURFACE PROFILES
 Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

VIZCAYA AVENUE

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
1.000	10.87	.34	.39	3.08	28.29	1.60	.49

RESULTS:
 WSEL = 0.34'
 V = 3.08 fps
 EG = 0.49'

SUMMARY OF ERRORS AND SPECIAL NOTES

CONCLUSION: The water surface .01' above top of curb.
 The energy grade line below 0.53' at property line

INFRASTRUCTURE LIST

EXHIBIT "A"

TO SUBDIVISION IMPROVEMENTS AGREEMENT

DEVELOPMENT REVIEW BOARD (D.R.B.) REQUIRED INFRASTRUCTURE LIST

Anasazi Ridge Unit 3

PROPOSED NAME OF PLAT AND/OR SITE DEVELOPMENT PLAN

Portions of Lot 3, 4-9, Blk 7, Lots 9-13 Blk 8, Lot 12, Block 9, and Lots 2-10, Blk 14

EXISTING LEGAL DESCRIPTION PRIOR TO PLATTING ACTION

Following is a summary of PUBLIC/PRIVATE Infrastructure required to be constructed or financially guaranteed for the above development. This Listing is not necessarily a complete listing. During the SIA process and/or in the review of the construction drawings, if the DRC Chair determines that appurtenant items and/or unforseen items have not been included in the infrastructure listing, the DRC Chair may include those items in the listing and related financial guarantee. Likewise, if the DRC Chair determines that appurtenant or non-essential items can be deleted from the listing, those items may be deleted as well as the related portions of the financial guarantees. All such revisions require approval by the DRC Chair, the User Department and agent/owner. If such approvals are obtained, those revisions to the listing will be incorporated administratively. In addition, any unforseen items which arise during construction which are necessary to complete the project and which normally are the Subdivider's responsibility will be required as a condition of project acceptance and close out by the City.

SIA Sequence #	COA DRC Project #	Size	Type of Improvement	Location	From	To	Private Inspector	City Inspector	City Enst Engineer
		32' FF	PAVING Perm Pvmnt	Atlant Drive NW	Westside Blvd	McMahon Blvd	/	/	/
		4'	C&G (both sides) Sidewalk (both sides)				/	/	/
		28' FF	Perm Pvmnt	Westside Blvd	End culdesac (Tract C)	Sipapu Drive NW	/	/	/
		4'	C&G (both sides) Sidewalk (North Side) (1)				/	/	/
		28' FF	Perm Pvmnt	Sipapu Drive NW	Westside Blvd	End Culdesac (Lot 16)	/	/	/
		4'	C&G (both sides) Sidewalk (both sides) (1)				/	/	/
		4'	Sidewalk Connection	McMahon Blvd ROW	Sipapu culdesac sidewalk	McMahon sidewalk	/	/	/
		28' FF	Perm Pvmnt	Canty Ct.	End culdesac (Lot 10)	Sipapu Drive NW	/	/	/
		4'	C&G (both sides) Sidewalk (both sides) (1)				/	/	/
		32' FF	Perm Pvmnt	McMahon Blvd.	West prop. Line (Tract C)	East Prop. Line (Lot 16)	/	/	/
			C&G (Southside) Median C&G 6' Sidewalk (Southside)				/	/	/

WATER

8" Waterline

Atlatl Drive NW

Westside Blvd

Exist. 12" WL
McMahon Blvd

8" Waterline

Westside Blvd

South P.L.
Parsons Row

Sipapu Drive NW

6" Waterline

Sipapu Drive NW

Westside Blvd

Exist. 12" WL
McMahon Blvd

6" Waterline

Canty Ct.

Cul-de-Sac

Sipapu Drive NW

12" Waterline

McMahon Blvd

Atlatl Drive NW

East P.L. (Lot 16)

SANITARY SEWER

8" Sanitary Sewer

Westside Blvd

Lot 24 /Parson Blvd

Sipapu Drive NW

8" Sanitary Sewer

Sipapu Drive NW

Westside Blvd

End culdesac
(Lot 16)

6" Sanitary Sewer

Canty Ct.

End Culdesac
(Lot 10)

Sipapu Drive NW

8" Sanitary Sewer

20 ft. Public sanitary
sewer easement

Sipapu Drive NW

Exist. 8" SAS
Calle Vizcaya

DRAINAGE

Per design Channel / swales & ponds

Tract A

Sipapu Dr. NW

Calle Vizcaya ROW

Per design Sidewalk culverts / channel / shallow pond

Lot 16

Sipapu Dr. NW

McMahan

Per design Concrete rundown / spillway

Calle Vizcaya ROW

Tract A

Calle Vizcaya Ave.

Per design Concrete rundown

McMahon Blvd ROW

Kayenta Blvd.

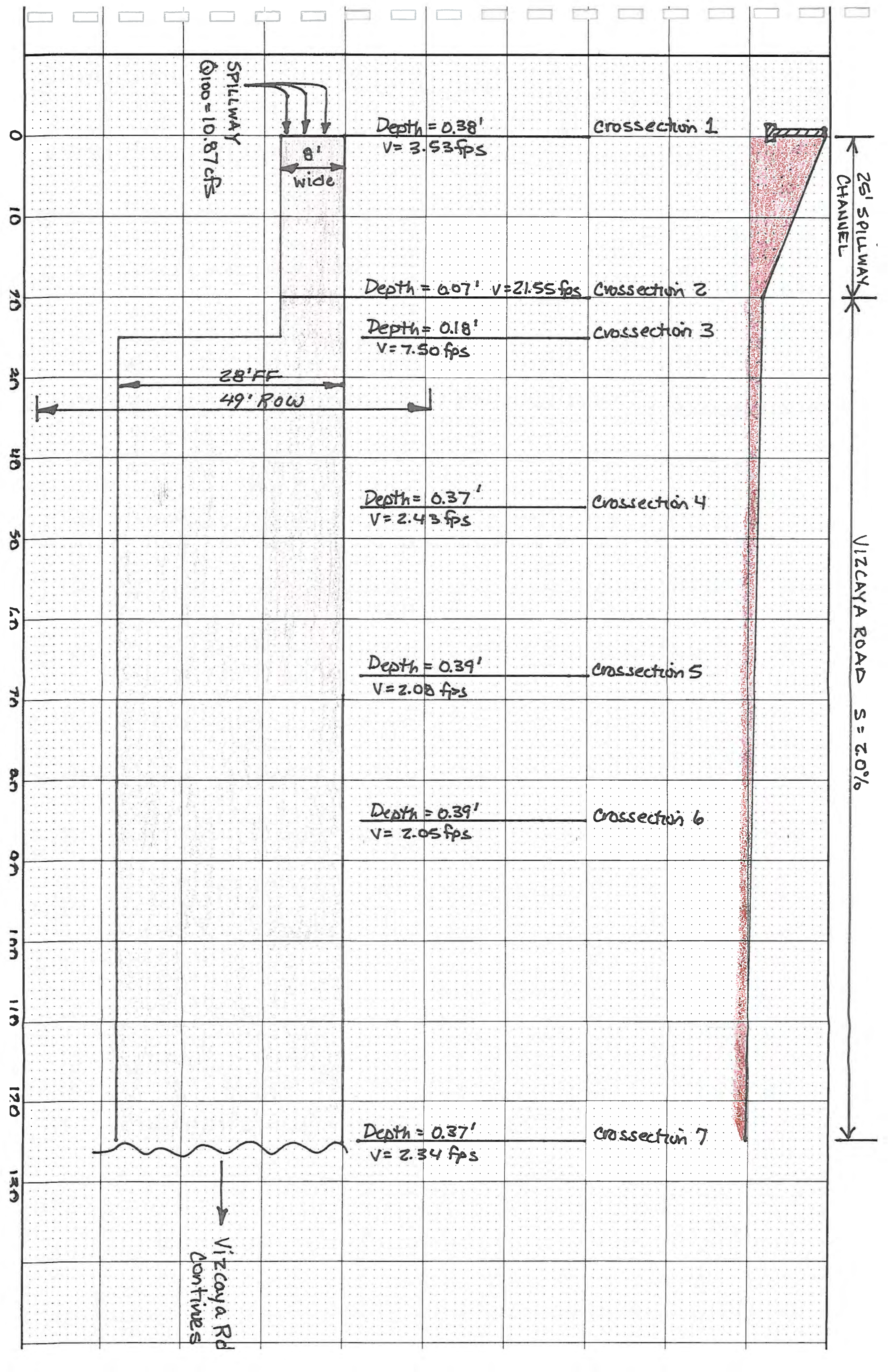
AMAFCA ROW
Calabacillas Arroyo

The items listed below are on the CCIP and approved for Impact Fee credits. Signatures from the Impact Fee Administrator and the City User Department is required prior to DRB approval of							
Financially Guaranteed DRC #	Constructed Under DRC #	Type of Improvement	Location	From	To	Construction Certification	
						Private Inspector P.E.	City Cnst Engineer
						/	/
						/	/
Approval of Creditable Items:						Approval of Creditable Items:	
Impact Fee Administrator Signature						City User Dept. Signature	
Date						Date	

- 1 Deferred sidewalk to comply with approved sidewalk exhibit
- 2 Waterline Infrastructure to include valves, fittings, service connections and fire hydrants
- 3 Storm Drain Infrastructure to include manholes and inlets
- 4 Grading & Drainage Certification required per DPM (Prior to release of Financial Guaranty) to include retaining walls as defined on the approved Grading Plan
- 5 SAS Infrastructure include manholes and service connections.
- 6

AGENT / OWNER		DEVELOPMENT REVIEW BOARD MEMBER APPROVALS	
Diane Hoelzer, PE		PARKS & GENERAL SERVICES - date	
NAME (print)			
MARK GOODWIN & ASSOCIATES		AMAFCA - date	
FIRM			
SIGNATURE - date		- date	
MAXIMUM TIME ALLOWED TO CONSTRUCT THE IMPROVEMENTS WITHOUT A DRB		CITY ENGINEER - date	
EXTENSION: N/A			
DESIGN REVIEW COMMITTEE REVISIONS			

REVISION	DATE	DRC CHAIR	USER DEPARTMENT	AGENT / OWNER



*Anasazi Ridge Unit 3
Subdivision*

Drainage Management Plan

*Prepared by
Mark Goodwin & Associates, P.A.*

January 2015



Anasazi Ridge Unit 3

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 - FIGURE 3** Preliminary Plat
 - FIGURE 4** Infrastructure List
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 - AHYMO output file 100 year storm
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-
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I. PROJECT DESCRIPTION

Anasazi Ridge Unit 3 covers an area of approximately 6.76 acres. This project involves the construction of supporting infrastructure to develop 24 single family residential lots. The project site is bounded by McMahon Blvd. to the north, Seville Unit 7 subdivision to the east and an open tract of land to the south and west. The north half of McMahon Blvd. is complete. This project will construct the south half of McMahon Blvd. connecting to the existing pavement at the east end and ending at the west property line, thus covering their frontage.

II. DESIGN CRITERIA AND PREVIOUS REPORTS AND DEVELOPMENT

The design criteria used in this report was in accordance with Section 22.2 Hydrology of the Development Process Manual, Volume 2, Design Criteria, January 1993 edition. The 100-year 24-hour storm event was analyzed to determine street capacities and sizing of the storm drain system using $P(1 \text{ hr})=1.72"$, $P(6 \text{ hr})=2.25"$ and $P(24 \text{ hr})=2.59"$. The onsite Land Treatment values used were based on Table A-5, in the DPM.

A previous approved drainage plan was prepared for the adjacent Seville Unit 7 subdivision (Wilson & Co.). Appendix D shows the existing conditions sub basin boundary map and the proposed sub basin boundary map from the Seville Unit 7 drainage report. As indicated on these exhibits, a portion of this project site drains to the north towards McMahon Blvd. and the southern portion flows to the east towards Seville Unit 7 subdivision. The developed conditions map indicates that Seville Unit 7 was designed to accept an allowable peak discharge (100 year) of 10.87 cfs from our project site. This project was graded so that this allowable discharge would spill to the east into Calle Vizcaya Avenue. The remainder of the site will drain north and into McMahon Blvd. ($Q(\text{design})=6.57 \text{ cfs}$, from the Wilson Report). Thus, the Anasazi Ridge Unit 3 drainage management plan will be in substantial conformance with the previously approved Seville Unit 7 drainage management plan.

III. EXISTING DRAINAGE CONDITIONS

Under existing drainage conditions, most of the project site drains towards McMahon Blvd. to the north. There is a 3 to 6 foot bluff along the south to southwest boundary of the project site that prevents any cross boundary drainage onto or from our site. The vacant land to the south drains primarily in an east to southeast direction. Along the northern boundary is the McMahon Blvd. and the drainage in this area continues eastward crossing through Kayenta Blvd. intersection to a temporary asphalt rundown that spills into the Calabacillas Arroyo. Appendix E has aerial photos of the Kayenta / McMahon intersection that shows the existing asphalt rundown. From these photos it is evident that the rundown is only a temporary drainage solution until the east side of Kayenta and the south side of McMahon Blvd. are widened.

IV. DEVELOPED DRAINAGE CONDITIONS

A. Onsite Drainage

Under developed conditions, the majority of the site ($Q=10.80$ cfs) drains to Tract A via a series of (4) 24" wide sidewalk culverts (@ 1% slope) and then passes through a meandering channel / shallow pond area before spilling over a vertical drop into an 8' wide concrete channel in the Seville Unit 7 subdivision and then eastward into Calle Vizcaya Avenue. The intent of the shallow ponding area will be to capture the first flush up to 6-8 inches deep as shown on the grading plan and shown in more detail in Appendix C. The velocities through this area are low so only minor landscape rock protection is being proposed.

Much of the kinetic velocity energy from the vertical drop spillway will be dissipated once the runoff hits the 8' wide concrete channel below and is redirected to the east into Calle Vizcaya Avenue. The high retaining sidewalls along the channel adjacent to the spillway drop will contain splash and facilitate in the transition back to normal depth flow when it reaches Calle Vizcaya Avenue. Refer to the conceptual design of this structure in Appendix C.

As previously discussed in the approved Seville Unit 7 drainage management plan, the allowable discharge from our project site is 10.87 cfs for the 100 year storm event.

B. McMahon Blvd. Drainage

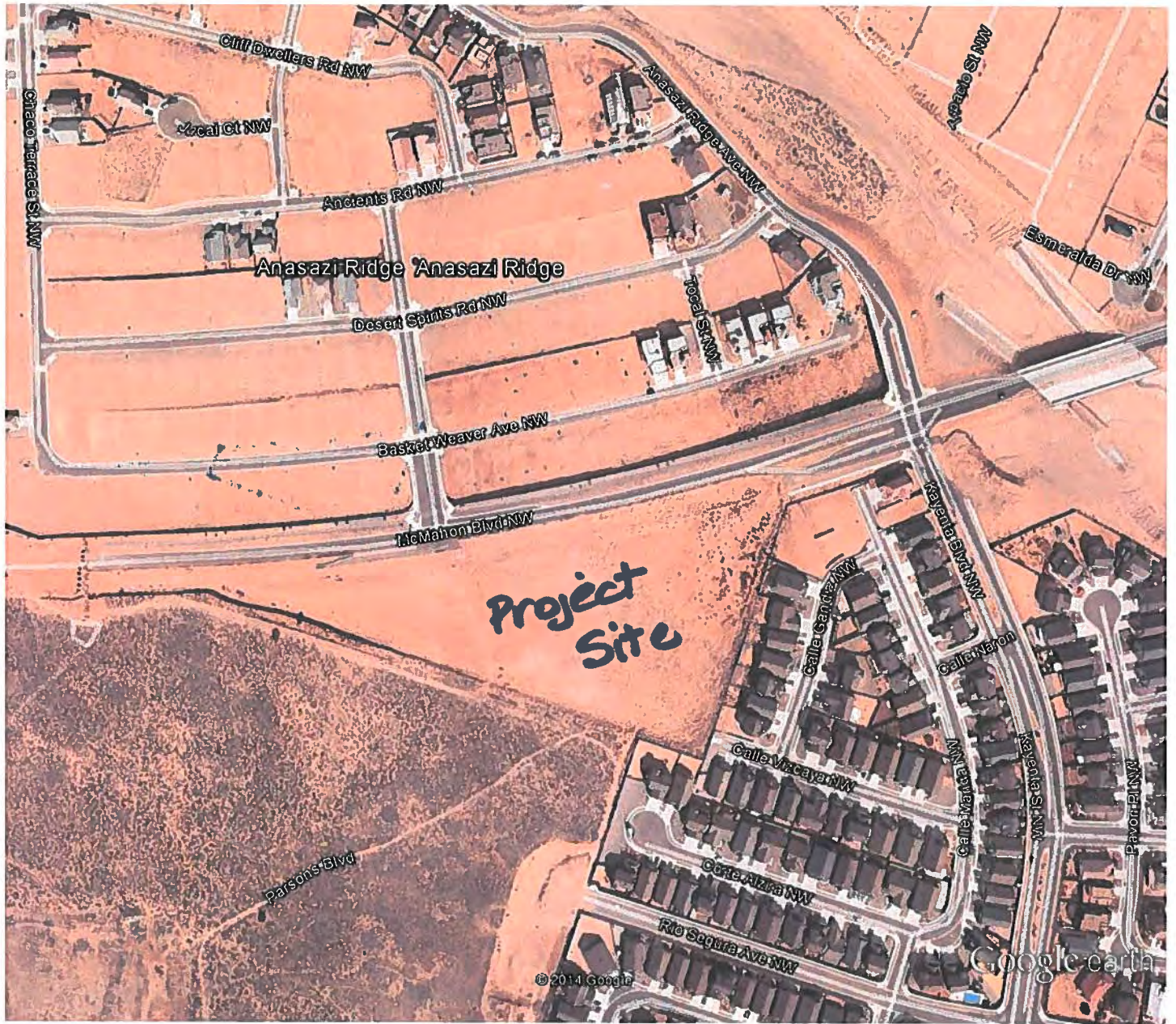
A total of 7.19 cfs will flow from the project site into McMahon Blvd. At the west end, 1.02 cfs will flow from Atlatl Drive and through a couple of wall blocks turned on their side to allow a small amount of discharge to flow into the landscape ROW area from the back yards. At the east end, 5.69 cfs will be conveyed down Canty Court to Sipapu Drive to a drainage swale adjacent to McMahon Blvd and into a shallow pond that will serve to intercept the first flush of runoff before spilling through a couple of sidewalk culverts into McMahon Blvd. This shallow pond is designed to retain no more than 6 inches of runoff before spilling into the sidewalk culverts. A 24" wide sidewalk culvert at a 1.4% slope will carry 5.69 cfs at a depth of 0.55'. It is proposed to add an additional 12" wide sidewalk culvert as a safety factor. A drainage easement will be dedicated on the plat and will be maintained by the H.O.A for Tracts A, B and C. It is proposed that Tract A and C will be protected with landscape rock and or seeded.

Developed conditions runoff within the future fully developed McMahon Blvd., were taken from the McMahon Boulevard Extension Drainage Report, July 2009, prepared by URS Corporation. Their calculated runoff flow rates within the future McMahon Blvd. is 48.32 cfs (Q100) and 29.95 cfs (Q10) for the combined north and south lanes. These flow rates have been reduced and incorporated into the current analysis to determine the McMahon Blvd. street flow capacity so the dry lane width for the 10 year storm event could be determined. The calculations, assumptions and results of this analysis are in Appendix E. For the worst case scenario; with a calculated discharge of 10.83 cfs (10 year storm) at a slope of 0.50% at the flattest section, resulted in dry lane width of 10.12 feet assuming a 32' FF half section roadway width.

The off-site runoff is conveyed via surface flow on McMahon Blvd. to the southeast corner of the McMahon Blvd. and Kayenta Blvd. intersection. It is propose that the existing curb cut be widened to 26 ft. with removable bollards in place and connected to a temporary 10' wide asphalt channel. The proposed channel conveys runoff towards the Calabacillas Arroyo and is proposed to end at the right of way line where the channel will end at a wired enclosed rip rap blanket.

As shown and calculated in Figure 4 (Appendix E) the 100-year flow rate at the McMahon Blvd. / Kayenta Blvd. intersection is 18.13 cfs. This flow is for the south half of McMahon Blvd. only and the valley gutter in this section is at 0.45% slope. Because this area from survey information indicates such a flat longitudinal slope as well as as a cross section slope, the runoff spread may be up to 55' wide as indicated on the HEC-2 output analysis. The spread has been sketched on the topographic survey exhibit in Appendix E.

According to the URS McMahon Blvd. Extension Report the flow from McMahon Blvd ultimate section is supposed to be intercepted by inlets located east of Calabacillas Arroyo bridge as indicated in excerpts from the report in Appendix E.



Google earth





Google earth



Quota Totals					Quota C	Quota L
Case #	Length	Index	Quota	Quota	Quota C	Quota L
C27	120.81	300.00	26.231%	87.733%	136.42	
C28	120.81	250.00	20.792%	71.733%	114.42	
C29	40.00	25.00	10.703%	23.644%	40.00	
C30	21.86	15.00	6.867%	12.671%	21.86	
C31	11.24	7.50	6.679%	11.907%	11.24	
C32	56.39	40.00	70.793%	44.903%	56.39	
C33	56.39	40.00	70.793%	44.903%	56.39	
C34	43.45	30.00	69.237%	34.713%	43.45	
C35	43.45	30.00	69.237%	34.713%	43.45	
C36	1.87	1.00	53.476%	53.476%	1.87	
C37	37.14	25.00	67.315%	43.737%	37.14	
C38	17.54	12.50	70.793%	67.315%	17.54	
C39	41.65	34.00	81.654%	75.000%	41.65	
C40	36.40	30.00	82.170%	75.000%	36.40	
C41	36.40	30.00	82.170%	75.000%	36.40	
C42	27.25	25.00	91.743%	88.235%	27.25	

Order #	Length	Radius	Curve Factor		Offset B	Offset L
			Inside	Outside		
C01	21.62	41.52	179.702	149.731	149.731	41.52
C02	15.14	50.926	171.86	146.722	146.722	131.41
C03	21.5	50.926	646.23	146.722	146.722	21.5
C04	31.8	50.926	673.34	146.722	146.722	31.8
C05	31.8	50.926	673.34	146.722	146.722	31.8
C06	31.8	50.926	673.34	146.722	146.722	31.8
C07	71.1	50.926	670.13	146.722	146.722	71.1
C08	48.17	50.926	670.13	146.722	146.722	48.17
C09	48.17	50.926	670.13	146.722	146.722	48.17
C10	180.78	43.05	83.745	130.77	130.77	43.05
C11	48.17	43.05	83.745	130.77	130.77	48.17
C12	62	43.05	214.747	130.77	130.77	62
C13	8.31	43.05	214.747	130.77	130.77	8.31
C14	54	43.05	180.57	130.77	130.77	54
C15	117.84	43.05	180.57	130.77	130.77	117.84
C16	54	43.05	180.57	130.77	130.77	54
C17	73.37	43.05	180.57	130.77	130.77	73.37

NEW EASEMENTS:

- ① NEW 10' PUBLIC UTILITY EASEMENT GRANTED WITH THIS PLAT
- ② NEW 20' SANITARY SEWER EASEMENT GRANTED WITH THIS PLAT
- ③ NEW BLANKET DRAINAGE EASEMENT ON TRACTS "A" & "B" GRANTED WITH THIS PLAT

1. TRACTS "A", "B" & "C" TO BE OWNED AND MAINTAINED

1. TRACTS "A", "B" & "C" TO BE OWNED AND MAINTAINED

Line Table		
Line #	Starting	Distance
1	467541018"	77.00'
2	508911344"	0.86'
3	525494608"	10.18'
4	529446880"	26.50'
5	529446880"	13.46'
6	568911344"	57.67'
7	568912368"	37.87'
8	579341008"	31.80'
9	579341008"	56.01'
10	579341008"	1.80'
11	529446880"	36.80'
12	568912368"	18.50'
13	529446880"	1.87'

ADRS Aluminum Cap stamped "7-A10 2003"
from the intersection of Living Boulevard NW and Koyuk Street NW,
go north on Koyuk Street NW 0.20 miles to the station on the left.
It is the 1339 feet mark on the centerline of Burgeon Avenue NW and 2.6 feet
apart of the north side of centerline.

Geographic Position (in feet) M4033
N.M.M. State Plane Coordinates (Central Zone)
N = 1520345.638, E = 1409909.436
Distances (in feet) NAD83 = 5382.970

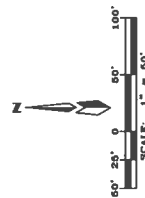
1-PI	LOT NUMBER	▲	CENTER LINE MONUMENT	R/W	RIGHT-OF-WAY
------	------------	---	----------------------	-----	--------------

SURVEYOR
WILDRICH LAND SURVEYING
P.O. BOX 3001
ALBUQUERQUE, NEW MEXICO 87190
505/884-1980

ENGINEERS
J. MARK GOODWIN & ASSOCIATES, P.A.
CONSULTING INC ENGINEERS
P.O. BOX 90008
INDIANAPOLIS, IN 46206-0008

OWNERS
MASATI RIDGE LLC
P.O. BOX 12317
BUENOS AIRES, ARGENTINA
(561) 555 5555

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Current DRC
Project Number: _____

FIGURE 12

Date Submitted: 16-Dec-14
Date Site Plan Approved: _____
Date Preliminary Plat Approved: _____
Date Preliminary Plat Expires: _____
DRB Project No.: 1004245
DRB Application No.: _____

INFRASTRUCTURE LIST

EXHIBIT "A"

**TO SUBDIVISION IMPROVEMENTS AGREEMENT
DEVELOPMENT REVIEW BOARD (D.R.B.) REQUIRED INFRASTRUCTURE LIST**

Anasazi Ridge Unit 3

PROPOSED NAME OF PLAT AND/OR SITE DEVELOPMENT PLAN

Portions of Lot 3, 4-9, Blk 7, Lots 9-13 Blk 8, Lot 12, Block 9, and Lots 2-10, Blk

14

EXISTING LEGAL DESCRIPTION PRIOR TO PLATTING ACTION

Following is a summary of PUBLIC/PRIVATE Infrastructure required to be constructed or financially guaranteed for the above development. This Listing is not necessarily a complete listing. During the SIA process and/or in the review of the construction drawings, if the DRC Chair determines that appurtenant items and/or unforeseen items have not been included in the infrastructure listing, the DRC Chair may include those items in the listing and related financial guarantee. Likewise, if the DRC Chair determines that appurtenant or non-essential items can be deleted from the listing, those items may be deleted as well as the related portions of the financial guarantees. All such revisions require approval by the DRC Chair, the User Department and agent/owner. If such approvals are obtained, these revisions to the listing will be incorporated administratively. In addition, any unforeseen items which arise during construction which are necessary to complete the project and which normally are the Subdivider's responsibility will be required as a condition of project acceptance and close out by the City.

SIA Sequence #	COA DRC Project #
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>
<input type="text"/>	<input type="text"/>

Size	Type of Improvement PAVING	Location	From	To	Private Inspector	City Inspector	City Cnst Engineer
32' FF	Perm Pvmt	Atlatl Drive NW	Westside Blvd	McMahon Blvd	/	/	/
4'	C&G (both sides) Sidewalk (both sides)				/	/	/
28' FF	Perm Pvmt	Westside Blvd	End culdesac (Tract E)	Sipapu Drive NW	/	/	/
4'	C&G (both sides) Sidewalk (North Side) (1)				/	/	/
28' FF	Perm Pvmt	Sipapu Drive NW	Westside Blvd	End Culdesac (Lot 16)	/	/	/
4'	C&G (both sides) Sidewalk (both sides) (1)				/	/	/
28' FF	Perm Pvmt	Canty Ct.	End culdesac (Lot 10)	Sipapu Drive NW	/	/	/
4'	C&G (both sides) Sidewalk (both side) (1)				/	/	/
32' FF	Perm Pvmt	McMahon Blvd.	West prop. Line (Tract E)	East Prop.Line (Lot 16)	/	/	/
	C&G (Southside) Median C&G 6' Sidewalk (Southside)				/	/	/

WATER

8" Waterline

/ / /

Exist. 12" WL
McMahon Blvd

8" Waterline

/ / /

Sipapu Drive NW

6" Waterline

/ / /

Exist. 12" WL
McMahon Blvd

6" Waterline

/ / /

Sipapu Drive NW

12" Waterline

/ / /

East P.L. (Lot 16)

SANITARY SEWER

8" Sanitary Sewer

/ / /

Sipapu Drive NW

8" Sanitary Sewer

/ / /

End culdesac
(Lot 16)

6" Sanitary Sewer

/ / /

Sipapu Drive NW

8" Sanitary Sewer

/ / /

Exist. 8" SAS
Calle Vizcaya

DRAINAGE

Per design Sidewalk culverts / meandering channel

/ / /

Calle Vizcaya
Spillway
McMahan

Per design Sidewalk culverts / channel / shallow pond

/ / /

Sipapu Dr. NW

Per design Concrete runoff / spillway

/ / /

Calle Vizcaya

The items listed below are on the CCIP and approved for Impact Fee credits. Signatures from the Impact Fee Administrator and the City User Department is required prior to DRB approval of								
Financially Guaranteed DRC #	Constructed Under DRC #	Size	Type of Improvement	Location	From	To	Construction Certification	
							Private Inspector P.E.	City Cnst Engineer
							/	/
							/	/
Approval of Creditable Items:							Approval of Creditable Items:	
Impact Fee Administrator Signature							City User Dept. Signature	
Date							Date	

- Deferred sidewalk to comply with approved sidewalk exhibit
- Waterline Infrastructure to include valves, fittings, service connections and fire hydrants
- Storm Drain Infrastructure to include manholes and inlets
- Grading & Drainage Certification required per DPM (Prior to release of Financial Guaranty) to include retaining walls as defined on the approved Grading Plan
- SAS Infrastructure include manholes and service connections.
-

AGENT / OWNER DEVELOPMENT REVIEW BOARD MEMBER APPROVALS

NAME (print) Diane Hoelzer, PE

MARK GOODWIN & ASSOCIATES

Diane Hoelzer 12-16-14

SIGNATURE - date

MAXIMUM TIME ALLOWED TO CONSTRUCT THE IMPROVEMENTS WITHOUT A DRB EXTENSION: N/A

DRB CHAIR - date

TRANSPORTATION DEVELOPMENT - date

UTILITY DEVELOPMENT - date

CITY ENGINEER - date

PARKS & GENERAL SERVICES - date

AMAFCA - date

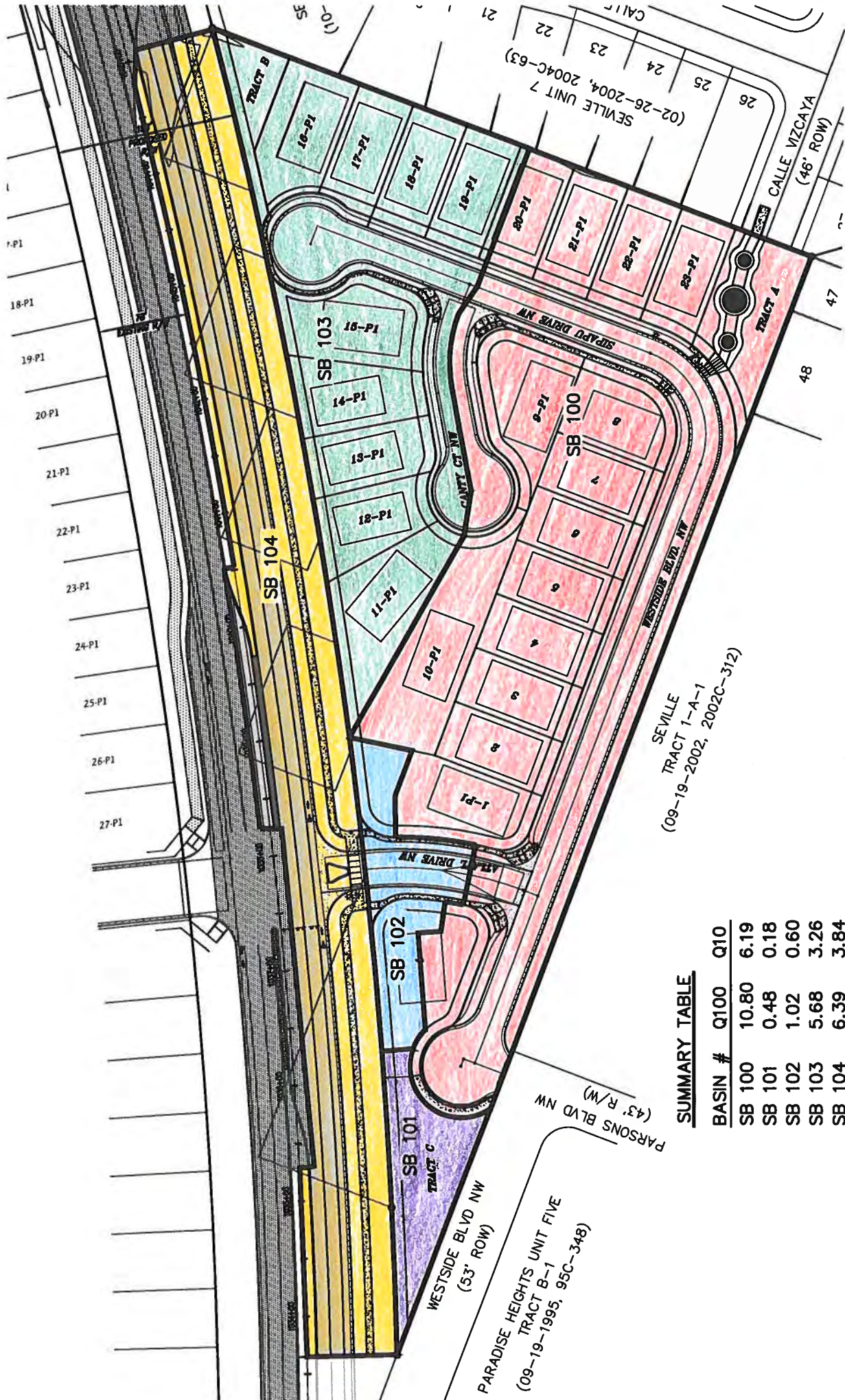
DESIGN REVIEW COMMITTEE REVISIONS

REVISION	DATE	DRC CHAIR	USER DEPARTMENT	AGENT /OWNER

APPENDIX A - HYDROLOGY

Sub Basin Boundary Exhibit

AHYMO Output



SEVILLE
TRACT 1-A-1
(09-19-2002, 2002C-312)

PARADISE HEIGHTS UNIT FIVE
TRACT B-1
(09-19-1995, 95C-348)

SUMMARY TABLE

BASIN #	Q100	Q10
SB 100	10.80	6.19
SB 101	0.48	0.18
SB 102	1.02	0.60
SB 103	5.68	3.26
SB 104	6.39	3.84

**ANASAZI RIDGE UNIT 3
SUB BASIN BOUNDARY EXHIBIT**

100 YEAR STORM

AHYMO PROGRAM (AHYMO_97) - - Version: 1997.02d
 RUN DATE (MON/DAY/YR) = 01/09/2015
 START TIME (HR:MIN:SEC) = 09:22:04 USER NO. = AHYMO-I-9702dGoodwinM-AH
 INPUT FILE = AR3_R3.DAT

 *S
 *S ANASAZI RIDGE UNIT 3
 *S 100 YEAR 24 HOUR STORM EVENT
 *S
 *S FILE: AR3_R3.DAT
 *S LAST REVISED: 1-8-15
 *S NOAA ATLAS 2, VOL IV ZONE: A 10
 *S TIME=0.0 HR PUNCH CODE=0 PRINT LINES=-6
 *S
 *S NEW MEXICO
 *S
 *S State of New Mexico soil infiltration values (LAND FACTORS) used for computations.
 *S LOCATION
 *S Land Treatment Initial Abstr.(in) Unif. Infiltr.(in/hour)
 *S A 0.65 1.67
 *S B 0.50 1.25
 *S C 0.35 0.83
 *S D 0.10 0.04
 *S

RAINFALL
 TYPE=2 RAIN QUARTER=0.0
 RAIN ONE=1.72 IN RAIN SIX=2.25 IN
 RAIN DAY=2.59 IN DT=0.0333 HRS

COMPUTED 24-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.
 DT = .033300 HOURS END TIME = 19.946700 HOURS

.0000	.0044	.0089	.0135	.0182	.0230	.0279
.0329	.0380	.0432	.0485	.0540	.0597	.0654
.0713	.0774	.0837	.0901	.0968	.1036	.1107
.1181	.1257	.1335	.1417	.1503	.1592	.1685
.1782	.1885	.1993	.2042	.2093	.2147	.2259
.2516	.2912	.3482	.4261	.5286	.6594	.8223
1.0212	1.2122	1.2906	1.3565	1.4151	1.4683	1.5173
1.5628	1.6053	1.6451	1.6826	1.7180	1.7514	1.7830
1.8130	1.8414	1.8683	1.8939	1.9182	1.9255	1.9315
1.9372	1.9428	1.9481	1.9533	1.9584	1.9633	1.9680
1.9727	1.9772	1.9816	1.9859	1.9901	1.9943	1.9983
2.0023	2.0062	2.0100	2.0137	2.0174	2.0211	2.0246
2.0281	2.0316	2.0350	2.0384	2.0417	2.0450	2.0482
2.0514	2.0545	2.0576	2.0607	2.0637	2.0667	2.0697
2.0726	2.0755	2.0783	2.0812	2.0840	2.0868	2.0895
2.0922	2.0949	2.0976	2.1002	2.1029	2.1055	2.1080
2.1106	2.1131	2.1156	2.1181	2.1206	2.1230	2.1254
2.1279	2.1302	2.1326	2.1350	2.1373	2.1396	2.1419
2.1442	2.1465	2.1487	2.1510	2.1532	2.1554	2.1576
2.1598	2.1620	2.1641	2.1662	2.1684	2.1705	2.1726
2.1747	2.1767	2.1788	2.1809	2.1829	2.1849	2.1869
2.1889	2.1909	2.1929	2.1949	2.1968	2.1988	2.2007
2.2027	2.2046	2.2065	2.2084	2.2103	2.2122	2.2140
2.2159	2.2178	2.2196	2.2214	2.2233	2.2251	2.2269
2.2287	2.2305	2.2323	2.2340	2.2358	2.2376	2.2393
2.2411	2.2428	2.2445	2.2463	2.2480	2.2497	2.2508
2.2518	2.2528	2.2537	2.2547	2.2557	2.2566	2.2576

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2.3431 2.3439 2.3447 2.3455 2.3462 2.3470 2.3478
2.3486 2.3493 2.3501 2.3509 2.3516 2.3524 2.3531
2.3539 2.3546 2.3554 2.3562 2.3569 2.3577 2.3584
2.3592 2.3599 2.3607 2.3614 2.3621 2.3629 2.3636
2.3644 2.3651 2.3658 2.3666 2.3673 2.3680 2.3688
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2.3796 2.3803 2.3810 2.3817 2.3824 2.3831 2.3838
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2.4084 2.4091 2.4098 2.4104 2.4111 2.4117 2.4124
2.4130 2.4137 2.4144 2.4150 2.4157 2.4163 2.4170
2.4176 2.4183 2.4189 2.4195 2.4202 2.4208 2.4215
2.4221 2.4228 2.4234 2.4240 2.4247 2.4253 2.4260
2.4266 2.4272 2.4279 2.4285 2.4291 2.4297 2.4304
2.4310 2.4316 2.4323 2.4329 2.4335 2.4341 2.4348
2.4354 2.4360 2.4366 2.4372 2.4379 2.4385 2.4391
2.4397 2.4403 2.4409 2.4415 2.4422 2.4428 2.4434
2.4440 2.4446 2.4452 2.4458 2.4464 2.4470 2.4476
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2.4524 2.4530 2.4536 2.4542 2.4548 2.4554 2.4560
2.4566 2.4572 2.4578 2.4583 2.4589 2.4595 2.4601
2.4607 2.4613 2.4619 2.4624 2.4630 2.4636 2.4642
2.4648 2.4653 2.4659 2.4665 2.4671 2.4676 2.4682
2.4688 2.4694 2.4699 2.4705 2.4711 2.4717 2.4722
2.4728 2.4734 2.4739 2.4745 2.4751 2.4756 2.4762
2.4767 2.4773 2.4779 2.4784 2.4790 2.4796 2.4801
2.4807 2.4812 2.4818 2.4823 2.4829 2.4834 2.4840
2.4846 2.4851 2.4857 2.4862 2.4868 2.4873 2.4879
2.4884 2.4889 2.4895 2.4900 2.4906 2.4911 2.4917
2.4922 2.4928 2.4933 2.4938 2.4944 2.4949 2.4955
2.4960 2.4965 2.4971 2.4976 2.4981 2.4987 2.4992
2.4997 2.5003 2.5008 2.5013 2.5019 2.5024 2.5029
2.5035 2.5040 2.5045 2.5050 2.5056 2.5061 2.5066
2.5071 2.5077 2.5082 2.5087 2.5092 2.5097 2.5103
2.5108 2.5113 2.5118 2.5123 2.5129 2.5134 2.5139
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2.5180 2.5185 2.5190 2.5195 2.5200 2.5205 2.5210

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2.5251 2.5256 2.5261 2.5266 2.5271 2.5276 2.5281
2.5286 2.5291 2.5296 2.5301 2.5306 2.5311 2.5315
2.5320 2.5325 2.5330 2.5335 2.5340

*S*****
*** TOTAL SITE
*S DEVELOPED CONDITIONS
***
*** SUB BASIN 100
*** AREA = 3.522 ACRES
*** PROJECT SITE
***
COMPUTE NM HYD ID=1 HYD NO=100. AREA= 0.00550 SQ MI
PER A=0 PER B=28.5 PER C=28.5 PER D=43.
TP=-.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 9.3371 CFS UNIT VOLUME = .9982 B = 526.28 P60 = 1.7200
AREA = .002365 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .118903HR TP = .133300HR K/TP RATIO = .891996 SHAPE CONSTANT, N = 3.975497
UNIT PEAK = 8.3145 CFS UNIT VOLUME = .9989 B = 353.53 P60 = 1.7200
AREA = .003135 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 100.00

RUNOFF VOLUME = 1.41951 INCHES = .4164 ACRE-FEET
PEAK DISCHARGE RATE = 10.80 CFS AT 1.499 HOURS BASIN AREA = .0055 SQ. MI.

*S*****
*S* ROUTE THRU FIRST FLUSH POND
*S*****
ROUTE RESERVOIR ID=12 HYD=POND.12 INFLOW=1 CODE=5
OUTFLOW(CFS) STORAGE(ACFT) ELEV(FT)
0.00 0.000000 89.00
0.01 0.010023 89.25
2.15 0.010170 89.45
6.07 0.010501 89.65
11.15 0.011015 89.85

* * * * *
TIME INFLOW ELEV VOLUME OUTFLOW
(HRS) (CFS) (FEET) (AC-FT) (CFS)

```

.00	.00	89.00	.000	.00
.17	.00	89.00	.000	.00
.33	.00	89.00	.000	.00
.50	.00	89.00	.000	.00
.67	.01	89.00	.000	.00
.83	.22	89.04	.002	.00
1.00	.32	89.13	.005	.01
1.17	.26	89.24	.009	.01
1.33	2.36	89.45	.010	2.22
1.50	10.80	89.84	.011	10.84
1.67	5.52	89.62	.010	5.52
1.83	2.92	89.49	.010	2.95
2.00	1.92	89.43	.010	1.92
2.16	.95	89.34	.010	.96
2.33	.50	89.30	.010	.50
2.50	.32	89.28	.010	.33
2.66	.22	89.27	.010	.22
2.83	.16	89.26	.010	.16
3.00	.13	89.26	.010	.13
3.16	.10	89.26	.010	.11
3.33	.09	89.26	.010	.09
3.50	.08	89.26	.010	.08
3.66	.07	89.26	.010	.07
3.83	.07	89.26	.010	.07
4.00	.07	89.26	.010	.07
4.16	.07	89.26	.010	.07
4.33	.07	89.26	.010	.07
4.50	.07	89.26	.010	.07
4.66	.07	89.26	.010	.07
4.83	.07	89.26	.010	.07
5.00	.07	89.26	.010	.07
5.16	.07	89.26	.010	.07
5.33	.07	89.26	.010	.07
5.49	.07	89.26	.010	.07
5.66	.07	89.26	.010	.07
5.83	.07	89.26	.010	.07
5.99	.08	89.26	.010	.08
6.16	.06	89.25	.010	.06
6.33	.05	89.25	.010	.05
6.49	.05	89.25	.010	.05
6.66	.04	89.25	.010	.04
6.83	.04	89.25	.010	.04
6.99	.04	89.25	.010	.04
7.16	.04	89.25	.010	.04
7.33	.04	89.25	.010	.04
7.49	.04	89.25	.010	.04
7.66	.04	89.25	.010	.04
7.83	.04	89.25	.010	.04
7.99	.04	89.25	.010	.04
8.16	.04	89.25	.010	.04
8.33	.04	89.25	.010	.04
8.49	.04	89.25	.010	.04
8.66	.04	89.25	.010	.04
8.82	.04	89.25	.010	.04

8.99	.04	89.25	.010	.04
9.16	.04	89.25	.010	.04
TIME	INFLOW	ELEV	VOLUME	OUTFLOW
(HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)
9.32	.04	89.25	.010	.04
9.49	.04	89.25	.010	.04
9.66	.04	89.25	.010	.04
9.82	.04	89.25	.010	.04
9.99	.04	89.25	.010	.04
10.16	.03	89.25	.010	.03
10.32	.03	89.25	.010	.03
10.49	.03	89.25	.010	.03
10.66	.03	89.25	.010	.03
10.82	.03	89.25	.010	.03
10.99	.03	89.25	.010	.03
11.16	.03	89.25	.010	.03
11.32	.03	89.25	.010	.03
11.49	.03	89.25	.010	.03
11.66	.03	89.25	.010	.03
11.82	.03	89.25	.010	.03
11.99	.03	89.25	.010	.03
12.15	.03	89.25	.010	.03
12.32	.03	89.25	.010	.03
12.49	.03	89.25	.010	.03
12.65	.03	89.25	.010	.03
12.82	.03	89.25	.010	.03
12.99	.03	89.25	.010	.03
13.15	.03	89.25	.010	.03
13.32	.03	89.25	.010	.03
13.49	.03	89.25	.010	.03
13.65	.03	89.25	.010	.03
13.82	.03	89.25	.010	.03
13.99	.03	89.25	.010	.03
14.15	.03	89.25	.010	.03
14.32	.03	89.25	.010	.03
14.49	.03	89.25	.010	.03
14.65	.03	89.25	.010	.03
14.82	.03	89.25	.010	.03
14.99	.03	89.25	.010	.03
15.15	.03	89.25	.010	.03
15.32	.03	89.25	.010	.03
15.48	.03	89.25	.010	.03
15.65	.03	89.25	.010	.03
15.82	.03	89.25	.010	.03
15.98	.03	89.25	.010	.03
16.15	.03	89.25	.010	.03
16.32	.03	89.25	.010	.03
16.48	.03	89.25	.010	.03
16.65	.03	89.25	.010	.03
16.82	.03	89.25	.010	.03
16.98	.03	89.25	.010	.03
17.15	.02	89.25	.010	.02
17.32	.03	89.25	.010	.03

17.48	.02	89.25	.010	.02
17.65	.02	89.25	.010	.02
17.82	.02	89.25	.010	.02
17.98	.02	89.25	.010	.02
18.15	.02	89.25	.010	.02
18.32	.02	89.25	.010	.02
18.48	.02	89.25	.010	.02

TIME	INFLOW	ELEV	VOLUME	OUTFLOW
(HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)

18.65	.02	89.25	.010	.02
18.81	.02	89.25	.010	.02
18.98	.02	89.25	.010	.02
19.15	.02	89.25	.010	.02
19.31	.02	89.25	.010	.02
19.48	.02	89.25	.010	.02
19.65	.02	89.25	.010	.02
19.81	.02	89.25	.010	.02

PEAK DISCHARGE = 10.845 CFS - PEAK OCCURS AT HOUR 1.50

MAXIMUM WATER SURFACE ELEVATION = 89.838

MAXIMUM STORAGE = .0110 AC-FT INCREMENTAL TIME= .033300HRS

PRINT HYD ID=12 CODE=50

HYDROGRAPH FROM AREA POND.12

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	3.996	.1	7.992	.0	11.988	.0
.666	.0	4.662	.1	8.658	.0	12.654	.0
1.332	2.2	5.328	.1	9.324	.0	13.320	.0
1.998	1.9	5.994	.1	9.990	.0	13.986	.0
2.664	.2	6.660	.0	10.656	.0	14.652	.0
3.330	.1	7.326	.0	11.322	.0	15.318	.0

RUNOFF VOLUME = 1.38534 INCHES = .4064 ACRE-FEET

PEAK DISCHARGE RATE = 10.84 CFS AT 1.499 HOURS BASIN AREA = .0055 SQ. MI.

*** SUB BASIN 101

*** AREA = .24367 ACRES

*** TRACT E

COMPUTE NM HYD

ID=1 HYD NO=101. AREA= 0.0003807 SQ MI
PER A=0 PER B=100 PER C=0 PER D=0
TP=-.1333 HR MASS RAIN=-1

K = .133631HR TP = .133300HR K/TP RATIO = 1.002485 SHAPE CONSTANT, N = 3.521459
UNIT PEAK = .91931 CFS UNIT VOLUME = .9852 B = 321.89 P60 = 1.7200
AREA = .000381 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 101.00

RUNOFF VOLUME = .63581 INCHES = .0129 ACRE-FEET
PEAK DISCHARGE RATE = .48 CFS AT 1.499 HOURS BASIN AREA = .0004 SQ. MI.

*** *****

*** SUB BASIN 102

*** AREA = 0.3162 ACRES

*** PROJECT SITE ENTRANCE ROAD

*** *****

COMPUTE NM HYD ID=1 HYD NO=102 AREA= 0.000494 SQ MI
PER A=0 PER B=25 PER C=25 PER D=50
TP=-.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = .97517 CFS UNIT VOLUME = .9880 B = 526.28 P60 = 1.7200
AREA = .000247 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .118903HR TP = .133300HR K/TP RATIO = .891996 SHAPE CONSTANT, N = 3.975497
UNIT PEAK = .65508 CFS UNIT VOLUME = .9792 B = 353.53 P60 = 1.7200
AREA = .000247 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 102.00

RUNOFF VOLUME = 1.52481 INCHES = .0402 ACRE-FEET
PEAK DISCHARGE RATE = 1.02 CFS AT 1.499 HOURS BASIN AREA = .0005 SQ. MI.

*** *****

*** SUB BASIN 103

*** AREA = 1.8420 ACRES

*** PROJECT SITE

*** *****

COMPUTE NM HYD ID=1 HYD NO=103. AREA= 0.002878 SQ MI
PER A=0 PER B=28.15 PER C=28.15 PER D=43.7
TP=-.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 4.9654 CFS UNIT VOLUME = .9969 B = 526.28 P60 = 1.7200
AREA = .001258 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .118903HR TP = .133300HR K/TP RATIO = .891996 SHAPE CONSTANT, N = 3.975497
 UNIT PEAK = 4.2973 CFS UNIT VOLUME = .9975 B = 353.53 P60 = 1.7200
 AREA = .001620 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 103.00

RUNOFF VOLUME = 1.43004 INCHES = .2195 ACRE-FEET
 PEAK DISCHARGE RATE = 5.68 CFS AT 1.499 HOURS BASIN AREA = .0029 SQ. MI.

*S*****
 S ROUTE THRU FIRST FLUSH POND
 *S*****

ROUTE RESERVOIR ID=13 HYD=POND.13 INFLOW=1 CODE=5
 OUTFLOW(CFS) STORAGE(ACFT) ELEV(FT)
 0.00 .000000 85.5
 0.01 .009617 86.0
 5.69 .022792 86.5
 5.70 .040087 87.0

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	85.50	.000	.00
.17	.00	85.50	.000	.00
.33	.00	85.50	.000	.00
.50	.00	85.50	.000	.00
.67	.01	85.50	.000	.00
.83	.12	85.54	.001	.00
1.00	.17	85.65	.003	.00
1.17	.14	85.76	.005	.01
1.33	1.25	86.04	.011	.50
1.50	5.68	86.45	.021	5.13
1.67	2.90	86.30	.017	3.36
1.83	1.54	86.15	.014	1.70
2.00	1.02	86.09	.012	1.09
2.16	.50	86.05	.011	.60
2.33	.26	86.02	.010	.29
2.50	.17	86.02	.010	.18
2.66	.11	86.01	.010	.12
2.83	.08	86.01	.010	.09
3.00	.07	86.01	.010	.07
3.16	.05	86.00	.010	.05
3.33	.04	86.00	.010	.05
3.50	.04	86.00	.010	.04
3.66	.04	86.00	.010	.04
3.83	.04	86.00	.010	.04

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
4.00	.04	86.00	.010	.04
4.16	.04	86.00	.010	.04
4.33	.04	86.00	.010	.04
4.50	.04	86.00	.010	.04
4.66	.04	86.00	.010	.04
4.83	.04	86.00	.010	.04
5.00	.04	86.00	.010	.04
5.16	.04	86.00	.010	.04
5.33	.04	86.00	.010	.04
5.49	.04	86.00	.010	.04
5.66	.04	86.00	.010	.04
5.83	.04	86.00	.010	.04
5.99	.04	86.00	.010	.04
6.16	.03	86.00	.010	.03
6.33	.03	86.00	.010	.03
6.49	.02	86.00	.010	.02
6.66	.02	86.00	.010	.02
6.83	.02	86.00	.010	.02
6.99	.02	86.00	.010	.02
7.16	.02	86.00	.010	.02
7.33	.02	86.00	.010	.02
7.49	.02	86.00	.010	.02
7.66	.02	86.00	.010	.02
7.83	.02	86.00	.010	.02
7.99	.02	86.00	.010	.02
8.16	.02	86.00	.010	.02
8.33	.02	86.00	.010	.02
8.49	.02	86.00	.010	.02
8.66	.02	86.00	.010	.02
8.82	.02	86.00	.010	.02
8.99	.02	86.00	.010	.02
9.16	.02	86.00	.010	.02
9.32	.02	86.00	.010	.02
9.49	.02	86.00	.010	.02
9.66	.02	86.00	.010	.02
9.82	.02	86.00	.010	.02
9.99	.02	86.00	.010	.02
10.16	.02	86.00	.010	.02
10.32	.02	86.00	.010	.02
10.49	.02	86.00	.010	.02
10.66	.02	86.00	.010	.02
10.82	.02	86.00	.010	.02
10.99	.02	86.00	.010	.02
11.16	.02	86.00	.010	.02
11.32	.02	86.00	.010	.02
11.49	.02	86.00	.010	.02
11.66	.02	86.00	.010	.02
11.82	.02	86.00	.010	.02
11.99	.02	86.00	.010	.02
12.15	.02	86.00	.010	.02
12.32	.02	86.00	.010	.02

12.49	.02	86.00	.010	.02
12.65	.02	86.00	.010	.02
12.82	.02	86.00	.010	.02
12.99	.02	86.00	.010	.02
13.15	.02	86.00	.010	.02
13.32	.02	86.00	.010	.02
13.49	.02	86.00	.010	.02
13.65	.02	86.00	.010	.02
13.82	.02	86.00	.010	.02
13.99	.02	86.00	.010	.02
14.15	.02	86.00	.010	.02
14.32	.01	86.00	.010	.01
14.49	.02	86.00	.010	.02
14.65	.01	86.00	.010	.01
14.82	.01	86.00	.010	.01
14.99	.01	86.00	.010	.01
15.15	.01	86.00	.010	.01
15.32	.01	86.00	.010	.01
15.48	.01	86.00	.010	.01
15.65	.01	86.00	.010	.01
15.82	.01	86.00	.010	.01
15.98	.01	86.00	.010	.01
16.15	.01	86.00	.010	.01
16.32	.01	86.00	.010	.01
16.48	.01	86.00	.010	.01
16.65	.01	86.00	.010	.01
16.82	.01	86.00	.010	.01
16.98	.01	86.00	.010	.01
17.15	.01	86.00	.010	.01
17.32	.01	86.00	.010	.01
17.48	.01	86.00	.010	.01
17.65	.01	86.00	.010	.01
17.82	.01	86.00	.010	.01
17.98	.01	86.00	.010	.01
18.15	.01	86.00	.010	.01
18.32	.01	86.00	.010	.01
18.48	.01	86.00	.010	.01

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
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18.65	.01	86.00	.010	.01
18.81	.01	86.00	.010	.01
18.98	.01	86.00	.010	.01
19.15	.01	86.00	.010	.01
19.31	.01	86.00	.010	.01
19.48	.01	86.00	.010	.01
19.65	.01	86.00	.010	.01
19.81	.01	86.00	.010	.01

PEAK DISCHARGE = 5.465 CFS - PEAK OCCURS AT HOUR 1.53
 MAXIMUM WATER SURFACE ELEVATION = 86.480
 MAXIMUM STORAGE = .0223 AC-FT INCREMENTAL TIME= .033300HRS

PRINT HYD ID=13 CODE=50

HYDROGRAPH FROM AREA POND.13

[illegible]

RUNOFF VOLUME = 1.36736 INCHES = .2099 ACRE-FEET
PEAK DISCHARGE RATE = 5.47 CFS AT 1.532 HOURS BASIN AREA = .0029 SQ. MI.

*** SUB BASIN 104

*** AREA = 5.6738 ACRES

*** MCMAHON BLVD NEW PAVEMENT

COMPUTE NM HYD

ID=1 HYD NO=104. AREA= 0.003012 SQ MI

PER A=0 PER B=20 PER C=023.5 PER D=56.5

TP=-.1333 HR MASS RAIN=-1

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K = .072649HR    TP = .133300HR    K/TP RATIO = .545000    SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 6.7187    CFS    UNIT VOLUME = .9975    B = 526.28    P60 = 1.7200
AREA = .001702 SQ MI    IA = .10000 INCHES    INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

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K = .117718HR  TP = .133300HR  K/TP RATIO = .883106  SHAPE CONSTANT, N = 4.018318
UNIT PEAK = 3.5030  CFS  UNIT VOLUME = .9967  B = 356.39  P60 = 1.7200
AREA = .001310 SQ MI  IA = .41897 INCHES  INF = 1.02310 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

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PRINT HYD
ID=1 CODE=1
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PARTIAL HYDROGRAPH 104.00

RUNOFF VOLUME = 1.62763 INCHES = .2615 ACRE-Feet
 PEAK DISCHARGE RATE = 6.39 CFS AT 1.499 HOURS BASIN AREA = .0030 SQ. MI.

FINISH

NORMAL PROGRAM FINISH

10 YEAR STORM

AHYMO PROGRAM (AHYMO_97) - - Version: 1997.02d
RUN DATE (MON/DAY/YR) = 01/09/2015
START TIME (HR:MIN:SEC) = 09:32:17
INPUT FILE = AR3_R10.DAT
USER NO. = AHYMO-I-9702dGoodwinM-AH

*S
*S ANASAZI RIDGE UNIT 3
*S 10 YEAR 6 HOUR STORM EVENT
*S
*S
*S FILE: AR3_R1.DAT
*S LAST REVISED: 1-8-15
*S NOAA ATLAS 2, VOL IV ZONE: A 10
*S
START TIME=0.0 HR PUNCH CODE=0 PRINT LINES=-6
LOCATION NEW MEXICO
State of New Mexico soil infiltration values (LAND FACTORS) used for computations.
Land Treatment Initial Abstr.(in) Unif. Infiltr.(in/hour)
A 0.65 1.67
B 0.50 1.25
C 0.35 0.83
D 0.10 0.04

RAINFALL
TYPE=1 RAIN QUARTER=0.0
RAIN ONE=1.147 IN RAIN SIX=1.500 IN
RAIN DAY=1.728 IN DT=0.0333 HRS

COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.
DT = .033300 HOURS END TIME = 5.994000 HOURS
.0000 .0029 .0059 .0090 .0121 .0153 .0185
.0219 .0253 .0287 .0323 .0359 .0397 .0435
.0475 .0515 .0557 .0600 .0644 .0690 .0737
.0785 .0836 .0888 .0943 .1000 .1059 .1121
.1186 .1254 .1326 .1359 .1393 .1429 .1503
.1675 .1939 .2319 .2839 .3522 .4394 .5480
.6807 .8081 .8603 .9043 .9433 .9788 1.0115
1.0419 1.0702 1.0968 1.1218 1.1453 1.1676 1.1887
1.2087 1.2276 1.2456 1.2627 1.2789 1.2837 1.2877
1.2916 1.2953 1.2988 1.3023 1.3057 1.3089 1.3121
1.3152 1.3182 1.3211 1.3240 1.3268 1.3296 1.3323
1.3349 1.3375 1.3401 1.3426 1.3450 1.3474 1.3498
1.3522 1.3545 1.3567 1.3590 1.3612 1.3634 1.3655
1.3676 1.3697 1.3718 1.3739 1.3759 1.3779 1.3798
1.3818 1.3837 1.3856 1.3875 1.3894 1.3912 1.3931
1.3949 1.3967 1.3985 1.4002 1.4020 1.4037 1.4054
1.4071 1.4088 1.4105 1.4121 1.4138 1.4154 1.4170
1.4186 1.4202 1.4218 1.4234 1.4249 1.4265 1.4280
1.4295 1.4310 1.4325 1.4340 1.4355 1.4370 1.4384
1.4399 1.4413 1.4428 1.4442 1.4456 1.4470 1.4484
1.4498 1.4512 1.4526 1.4539 1.4553 1.4566 1.4580
1.4593 1.4607 1.4620 1.4633 1.4646 1.4659 1.4672
1.4685 1.4697 1.4710 1.4723 1.4735 1.4748 1.4760
1.4773 1.4785 1.4797 1.4810 1.4822 1.4834 1.4846
1.4858 1.4870 1.4882 1.4894 1.4905 1.4917 1.4929
1.4941 1.4952 1.4964 1.4975 1.4987 1.4998

*S*****

*** TOTAL SITE

*S DEVELOPED CONDITIONS

*** SUB BASIN 100

*** AREA = 3.522 ACRES

*** PROJECT SITE

COMPUTE NM HYD

ID=1 HYD NO=100. AREA= 0.00550 SQ MI

PER A=0 PER B=28.5 PER C=28.5 PER D=43.

TP=-.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420

UNIT PEAK = 9.3371 CFS UNIT VOLUME = .9982 B = 526.28 P60 = 1.1470

AREA = .002365 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .126379HR TP = .133300HR K/TP RATIO = .948077 SHAPE CONSTANT, N = 3.728417

UNIT PEAK = 7.9172 CFS UNIT VOLUME = .9985 B = 336.64 P60 = 1.1470

AREA = .003135 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 100.00

RUNOFF VOLUME = .71342 INCHES = .2093 ACRE-FEET

PEAK DISCHARGE RATE = 6.19 CFS AT 1.499 HOURS BASIN AREA = .0055 SQ. MI.

*S*****

*S ROUTE THRU FIRST FLUSH POND

ROUTE RESERVOIR

ID=12 HYD=POND.12 INFLOW=1 CODE=5

OUTFLOW(CFS) STORAGE(ACFT) ELEV(FT)

0.00 0.000000 89.00

0.01 0.010023 89.25

2.15 0.010170 89.45

6.07 0.010501 89.65

11.15 0.011015 89.85

* * * * *

TIME INFLOW ELEV VOLUME OUTFLOW

(HRS) (CFS) (FEET) (AC-FT) (CFS)

.00 .00 89.00 .000 .00

.17 .00 89.00 .000 .00

.33 .00 89.00 .000 .00

.50 .00 89.00 .000 .00

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.67	.00	89.00	.000	.00
.83	.00	89.00	.000	.00
1.00	.14	89.02	.001	.00
1.17	.14	89.07	.003	.00
1.33	1.27	89.25	.010	.01
1.50	6.19	89.68	.011	6.83
1.67	3.01	89.48	.010	2.68
1.83	1.62	89.42	.010	1.82
2.00	1.14	89.34	.010	1.02
2.16	.55	89.31	.010	.63
2.33	.27	89.27	.010	.23
2.50	.17	89.27	.010	.20
2.66	.12	89.26	.010	.10
2.83	.08	89.26	.010	.09
3.00	.06	89.25	.010	.05
3.16	.05	89.25	.010	.05
3.33	.04	89.25	.010	.04
3.50	.04	89.25	.010	.04
3.66	.03	89.25	.010	.03
3.83	.03	89.25	.010	.03
4.00	.03	89.25	.010	.03
4.16	.03	89.25	.010	.03
4.33	.03	89.25	.010	.03
4.50	.03	89.25	.010	.03
4.66	.04	89.25	.010	.04
4.83	.04	89.25	.010	.04
5.00	.04	89.25	.010	.04
5.16	.04	89.25	.010	.04
5.33	.04	89.25	.010	.04
5.49	.04	89.25	.010	.04
5.66	.05	89.25	.010	.05
5.83	.05	89.25	.010	.05
5.99	.05	89.25	.010	.05
6.16	.02	89.25	.010	.02
6.33	.01	89.25	.010	.01
6.49	.00	89.25	.010	.01
6.66	.00	89.24	.010	.01
6.83	.00	89.24	.010	.01
6.99	.00	89.24	.010	.01
7.16	.00	89.23	.009	.01
7.33	.00	89.23	.009	.01
7.49	.00	89.23	.009	.01
7.66	.00	89.23	.009	.01
7.83	.00	89.22	.009	.01
7.99	.00	89.22	.009	.01
8.16	.00	89.22	.009	.01
8.33	.00	89.21	.009	.01
8.49	.00	89.21	.008	.01
8.66	.00	89.21	.008	.01
8.82	.00	89.20	.008	.01
8.99	.00	89.20	.008	.01
9.16	.00	89.20	.008	.01

9.32 .00 89.20 .008 .01
 9.49 .00 89.19 .008 .01
 9.66 .00 89.19 .008 .01
 9.82 .00 89.19 .008 .01
 9.99 .00 89.19 .007 .01
 10.16 .00 89.18 .007 .01
 10.32 .00 89.18 .007 .01
 10.49 .00 89.18 .007 .01
 10.66 .00 89.18 .007 .01
 10.82 .00 89.17 .007 .01
 10.99 .00 89.17 .007 .01
 11.16 .00 89.17 .007 .01
 11.32 .00 89.17 .007 .01
 11.49 .00 89.16 .007 .01
 11.66 .00 89.16 .006 .01
 11.82 .00 89.16 .006 .01
 11.99 .00 89.16 .006 .01
 12.15 .00 89.16 .006 .01
 12.32 .00 89.15 .006 .01
 12.49 .00 89.15 .006 .01
 12.65 .00 89.15 .006 .01
 12.82 .00 89.15 .006 .01
 12.99 .00 89.15 .006 .01
 13.15 .00 89.14 .006 .01
 13.32 .00 89.14 .006 .01
 13.49 .00 89.14 .006 .01
 13.65 .00 89.14 .006 .01
 13.82 .00 89.14 .005 .01
 13.99 .00 89.13 .005 .01
 14.15 .00 89.13 .005 .01
 14.32 .00 89.13 .005 .01
 14.49 .00 89.13 .005 .01
 14.65 .00 89.13 .005 .01
 14.82 .00 89.12 .005 .00

PEAK DISCHARGE = 6.835 CFS - PEAK OCCURS AT HOUR 1.50
 MAXIMUM WATER SURFACE ELEVATION = 89.680
 MAXIMUM STORAGE = .0106 AC-FT INCREMENTAL TIME= .033300HRS

PRINT HYD ID=12 CODE=50

HYDROGRAPH FROM AREA POND.12

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	3.996	.0	7.992	.0	11.988	.0
.666	.0	4.662	.0	8.658	.0	12.654	.0
1.332	.0	5.328	.0	9.324	.0	13.320	.0
1.998	1.0	5.994	.0	9.990	.0	13.986	.0
2.664	.1	6.660	.0	10.656	.0	14.652	.0
3.330	.0	7.326	.0	11.322	.0	15.318	.0

RUNOFF VOLUME = .70220 INCHES = .2060 ACRE-Feet
 PEAK DISCHARGE RATE = 6.83 CFS AT 1.499 HOURS BASIN AREA = .0055 SQ. MI.

*** *****

*** *****

*** SUB BASIN 101

*** AREA = .24367 ACRES

*** TRACT E

*** *****

COMPUTE NM HYD ID=1 HYD NO=101. AREA= 0.0003807 SQ MI

PER A=0 PER B=100 PER C=0 PER D=0

TP=-.1333 HR MASS RAIN=-1

K = .143714HR TP = .133300HR K/TP RATIO = 1.078121 SHAPE CONSTANT, N = 3.276560
UNIT PEAK = .86720 CFS UNIT VOLUME = .9837 B = 303.64 P60 = 1.1470
AREA = .000381 SQ MI IA = .50000 INCHES INF = 1.25000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 101.00

RUNOFF VOLUME = .21940 INCHES = .0045 ACRE-FEET
PEAK DISCHARGE RATE = .18 CFS AT 1.532 HOURS BASIN AREA = .0004 SQ. MI.

*** *****

*** SUB BASIN 102

*** AREA = 0.3162 ACRES

*** PROJECT SITE ENTRANCE ROAD

*** *****

COMPUTE NM HYD ID=1 HYD NO=102 AREA= 0.000494 SQ MI

PER A=0 PER B=25 PER C=25 PER D=50

TP=-.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = .97517 CFS UNIT VOLUME = .9880 B = 526.28 P60 = 1.1470
AREA = .000247 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 102.00

RUNOFF VOLUME = .77980 INCHES = .0205 ACRE-FEET
PEAK DISCHARGE RATE = .60 CFS AT 1.499 HOURS BASIN AREA = .0005 SQ. MI.

*** *****

*** SUB BASIN 103

*** AREA = 1.8420 ACRES

*** PROJECT SITE

*** *****

COMPUTE NM HYD

ID=1 HYD NO=103. AREA= 0.002878 SQ MI

PER A=0 PER B=28.15 PER C=28.15 PER D=43.7

TP=-.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420

UNIT PEAK = 4.9654 CFS UNIT VOLUME = .9969 B = 526.28 P60 = 1.1470

AREA = .001258 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .126379HR TP = .133300HR K/TP RATIO = .948077 SHAPE CONSTANT, N = 3.728417

UNIT PEAK = 4.0920 CFS UNIT VOLUME = .9968 B = 336.64 P60 = 1.1470

AREA = .001620 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD

ID=1 CODE=1

PARTIAL HYDROGRAPH 103.00

RUNOFF VOLUME = .72006 INCHES = .1105 ACRE-FEET
PEAK DISCHARGE RATE = 3.26 CFS AT 1.499 HOURS BASIN AREA = .0029 SQ. MI.

*S*****

S ROUTE THRU FIRST FLUSH POND

*S*****

ROUTE RESERVOIR

ID=13 HYD=POND.13 INFLOW=1 CODE=5

OUTFLOW (CFS) STORAGE (ACFT) ELEV (FT)

0.00 .000000 85.5

0.01 .009617 86.0

5.69 .022792 86.5

5.70 .040087 87.0

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
---------------	-----------------	----------------	-------------------	------------------

.00	.00	85.50	.000	.00
-----	-----	-------	------	-----

.17	.00	85.50	.000	.00
-----	-----	-------	------	-----

.33	.00	85.50	.000	.00
-----	-----	-------	------	-----

.50	.00	85.50	.000	.00
-----	-----	-------	------	-----

.67	.00	85.50	.000	.00
-----	-----	-------	------	-----

.83	.00	85.50	.000	.00
-----	-----	-------	------	-----

1.00	.07	85.52	.000	.00
------	-----	-------	------	-----

1.17	.08	85.58	.002	.00
------	-----	-------	------	-----

1.33	.67	85.78	.005	.01
1.50	3.26	86.25	.016	2.88
1.67	1.59	86.16	.014	1.87
1.83	.86	86.08	.012	.94
2.00	.61	86.06	.011	.64
2.16	.29	86.03	.010	.35
2.33	.14	86.01	.010	.16
2.50	.09	86.01	.010	.10
2.66	.06	86.00	.010	.06
2.83	.04	86.00	.010	.04
3.00	.03	86.00	.010	.03
3.16	.02	86.00	.010	.03
3.33	.02	86.00	.010	.02
3.50	.02	86.00	.010	.02
3.66	.02	86.00	.010	.02
3.83	.02	86.00	.010	.02
4.00	.02	86.00	.010	.02
4.16	.02	86.00	.010	.02
4.33	.02	86.00	.010	.02
4.50	.02	86.00	.010	.02
4.66	.02	86.00	.010	.02
4.83	.02	86.00	.010	.02
5.00	.02	86.00	.010	.02
5.16	.02	86.00	.010	.02
5.33	.02	86.00	.010	.02
5.49	.02	86.00	.010	.02
5.66	.02	86.00	.010	.02
5.83	.03	86.00	.010	.03
5.99	.03	86.00	.010	.03
6.16	.01	86.00	.010	.01
6.33	.00	86.00	.010	.01
6.49	.00	85.99	.009	.01
6.66	.00	85.98	.009	.01
6.83	.00	85.98	.009	.01
6.99	.00	85.97	.009	.01
7.16	.00	85.96	.009	.01
7.33	.00	85.96	.009	.01
7.49	.00	85.95	.009	.01
7.66	.00	85.94	.009	.01
7.83	.00	85.94	.008	.01
7.99	.00	85.93	.008	.01
8.16	.00	85.93	.008	.01
8.33	.00	85.92	.008	.01
8.49	.00	85.91	.008	.01
8.66	.00	85.91	.008	.01
8.82	.00	85.90	.008	.01
8.99	.00	85.90	.008	.01
9.16	.00	85.89	.008	.01
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
9.32	.00	85.89	.007	.01
9.49	.00	85.88	.007	.01
9.66	.00	85.87	.007	.01

9.82 .00 85.87 .07 .01
 9.99 .00 85.86 .07 .01
 10.16 .00 85.86 .07 .01
 10.32 .00 85.85 .07 .01
 10.49 .00 85.85 .07 .01
 10.66 .00 85.84 .07 .01
 10.82 .00 85.84 .07 .01
 10.99 .00 85.83 .06 .01
 11.16 .00 85.83 .06 .01
 11.32 .00 85.82 .06 .01
 11.49 .00 85.82 .06 .01
 11.66 .00 85.82 .06 .01
 11.82 .00 85.81 .06 .01
 11.99 .00 85.81 .06 .01
 12.15 .00 85.80 .06 .01
 12.32 .00 85.80 .06 .01
 12.49 .00 85.79 .06 .01
 12.65 .00 85.79 .06 .01
 12.82 .00 85.79 .05 .01
 12.99 .00 85.78 .05 .01
 13.15 .00 85.78 .05 .01
 13.32 .00 85.77 .05 .01
 13.49 .00 85.77 .05 .01
 13.65 .00 85.76 .05 .01
 13.82 .00 85.76 .05 .01
 13.99 .00 85.76 .05 .01
 14.15 .00 85.75 .05 .01
 14.32 .00 85.75 .05 .01
 14.49 .00 85.75 .05 .00

PEAK DISCHARGE = 3.128 CFS - PEAK OCCURS AT HOUR 1.53
 MAXIMUM WATER SURFACE ELEVATION = 86.274
 MAXIMUM STORAGE = .0168 AC-FT INCREMENTAL TIME= .033300HRS

PRINT HYD ID=13 CODE=50

HYDROGRAPH FROM AREA POND.13

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	3.996	.0	11.988	.0
.666	.0	4.662	.0	12.654	.0
1.332	.0	5.328	.0	13.320	.0
1.998	.6	5.994	.0	13.986	.0
2.664	.1	6.660	.0	14.652	.0
3.330	.0	7.326	.0	15.318	.0

RUNOFF VOLUME = .70060 INCHES = .1075 ACRE-FEET
 PEAK DISCHARGE RATE = 3.13 CFS AT 1.532 HOURS BASIN AREA = .0029 SQ. MI.

*** *****
 *** *****
 *** SUB BASIN 104
 *** AREA = 5.6738 ACRES

*** MCMAHON BLVD NEW PAVEMENT

*** *****

COMPUTE NM HYD

ID=1 HYD NO=104. AREA= 0.003012 SQ MI

PER A=0 PER B=20 PER C=023.5 PER D=56.5

TP=-.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 6.7187 CFS UNIT VOLUME = .9975 B = 526.28 P60 = 1.1470
AREA = .001702 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .124984HR TP = .133300HR K/TP RATIO = .937613 SHAPE CONSTANT, N = 3.771697
UNIT PEAK = 3.3385 CFS UNIT VOLUME = .9961 B = 339.65 P60 = 1.1470
AREA = .001310 SQ MI IA = .41897 INCHES INF = 1.02310 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 104.00

RUNOFF VOLUME = .84479 INCHES = .1357 ACRE-FEET
PEAK DISCHARGE RATE = 3.84 CFS AT 1.499 HOURS BASIN AREA = .0030 SQ. MI.

FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 09:32:17

APPENDIX B – HYDRAULICS

Channel Summary Exhibit

HEC-2 Printouts



D. Mark Goodwin & Associates, P.A.
Consulting Engineers

P.O. BOX 90606, ALBUQUERQUE, NM 87199
(505) 828-2200 FAX 797-9539

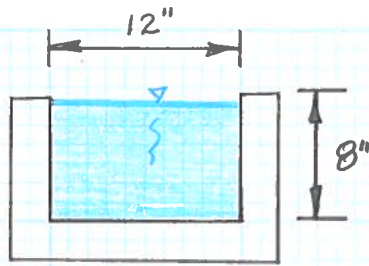
PROJECT ANASAZI RIDGE

SUBJECT Channel - Summary

BY Dut DATE 1-7-15

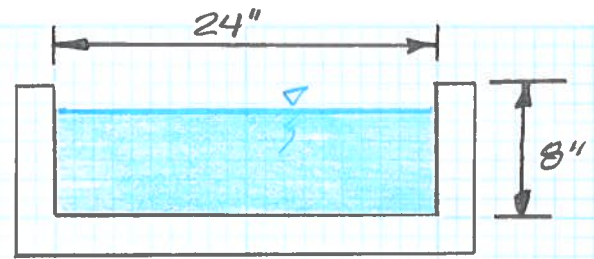
CHECKED _____ DATE _____

SHEET _____ OF _____



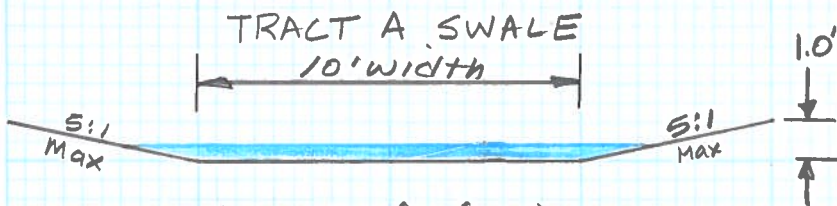
$$Q = 2.7 \text{ cfs}$$
$$S = 1.4\%$$
$$WSEL = 0.61'$$
$$V = 4.46 \text{ fps}$$

12" SIDEWALK CULVERT
(TRACT B)



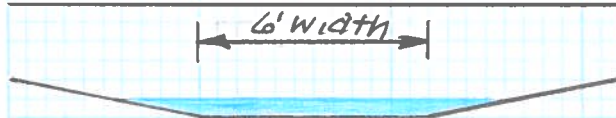
$$Q = 5.69 \text{ cfs}$$
$$S = 1.4\%$$
$$WSEL = 0.55'$$
$$V = 5.24 \text{ fps}$$

24" SIDEWALK CULVERT
(TRACT B)



$$Q = 10.87 \text{ cfs (max)}$$
$$S = 1.0\%$$
$$WSEL = 0.39'$$
$$V = 2.36 \text{ fps}$$

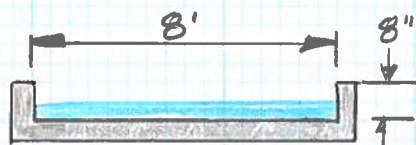
($n = .03 \Rightarrow$ USE LANDSCAPE GRAVEL)



TRACT A SWALE

$$Q = 10.87 \text{ cfs (max)}$$
$$S = 1.0\%$$
$$WSEL = 0.5'$$
$$V = 2.58 \text{ fps}$$

($n = .03 \Rightarrow$ USE LANDSCAPE GRAVEL)



SPILLWAY CHANNEL

Concrete channel.

$$Q = 10.87 \text{ cfs (max)}$$
$$S = 1.0\%$$
$$WSEL = 0.34'$$
$$V = 4.03 \text{ fps}$$


```

*****
1 *****
* HEC-2 WATER SURFACE PROFILES *
* *
* Version 4.6.2; May 1991 *
* *
* RUN DATE 15DEC14 TIME 15:46:07 *
*****
U.S. ARMY CORPS OF ENGINEERS *
HYDROLOGIC ENGINEERING CENTER *
609 SECOND STREET, SUITE D *
DAVIS, CALIFORNIA 95616-4687 *
(916) 756-1104 *
*****

```

[illegible]

THIS RUN EXECUTED 15DEC14 15:46:07

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

T1	CHANNEL CAPACITY CALCULATIONS
T2	ANASAZI RIDGE
T3	1 FOOT WIDE SHALLOW CHANNEL -

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	0	2	0	1	.014	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

	38	43	1	2	26	4	68	3
NC	.017	.017	.017	.1	.3			
QT	1	2.70						
X1	4	1	0	1.1	0	0	0	0
GR	.67	0	0	.1	0	1.	.67	1.1

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	CLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

***PROF 1**

CCHV=	.100	CEHV=	.300
-------	------	-------	------

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED	1.000	.61	.63
---	-------	-----	-----

.67

2.7	.0	2.7	.0	.0	.6	.0	.0	.0	.67
.00	.00	4.46	.00	.000	.017	.000	.000	.00	.01
.013992	0.	0.	0.	0	14	5	1.08	1.09	

THIS RUN EXECUTED 15DEC14 15:46:07

 HEC-2 WATER SURFACE PROFILES
 Version 4.6.2; May 1991

 NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

1 FOOT WIDE SHALLOW

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRIS	VCH	TOPWID	FRCH	EG
1.000	2.70	.61	.63	4.46	1.08	1.05	.92

SUMMARY OF ERRORS AND SPECIAL NOTES

.00	.00	5.24	.00	.000	.017	.000	.000	.00	.02
.013978	0.	0.	0.	0	14	5	.00	2.06	2.08

THIS RUN EXECUTED 15DEC14 15:47:31

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

2 FOOT WIDE SHALLOW

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRISW	VCH	TOPWID	FRCH	EG
1.000	5.69	.55	.64	5.24	2.06	1.27	.97

SUMMARY OF ERRORS AND SPECIAL NOTES

1*****
* HEC-2 WATER SURFACE PROFILES *
* *
* Version 4.6.2; May 1991 *
* *
* RUN DATE 15DEC14 TIME 16:38:40 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

X X XXXXXXXX XXXXX XXXXX
X X X X X
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XXXXXXXX XXXX XXXXX
X X X X
X X X X X
X X XXXXXXXX XXXXX
X X XXXXXXXX XXXXX

THIS RUN EXECUTED 15DEC14 16:38:40

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

T1 CHANNEL CAPACITY CALCULATIONS
T2 ANASAZI RIDGE
T3 10 FOOT WIDE SHALLOW CHANNEL - FIRST FLUSH CAPTURE

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	0	.01	0	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	43	1	2	26	4	68	3			
NC	.03	.03	.03	.1	.3					
QT	1	10.87								
X1	1	4	0	20.	0	0	0	0	0	0
GR	1.	0	0	5.	0	15.	0	1.	20.	

SECNO	DEPTH	CWSEL	CRIS	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV= .100 CEHV= .300
*SECNO 1.000
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED
1.000 .39 .00
10.9 .0 10.9 .0

.47 .09 .00 .00
4.6 .0 1.00 1.00

.00	.00	2.36	.00	.00	.030	.000	.000	.00	3.07
.009939	0.	0.	0.	0	0	.000	.00	13.86	16.93

THIS RUN EXECUTED 15DEC14 16:38:40

 HEC-2 WATER SURFACE PROFILES
 Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

10 FOOT WIDE SHALLOW

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
1.000	10.87	.39	.00	2.36	13.86	.72	.47

SUMMARY OF ERRORS AND SPECIAL NOTES


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*****
1*****
* HEC-2 WATER SURFACE PROFILES*****
*
*
* Version 4.6.2; May 1991
*
*
* RUN DATE 15DEC14 TIME 16:38:25
*****
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET, SUITE D
*
* DAVIS, CALIFORNIA 95616-4687
*
* (916) 756-1104
*****
*****

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[illegible]

THIS RUN EXECUTED 15DEC14 16:38:25

HEC-2 WATER SURFACE PROFILES

Version 4.6.2: May 1991

T1 CHANNEL CAPACITY CALCULATIONS

ANASAZI RIDGE

T3 6 FOOT WIDE SHALLOW CHANNEL - FIRST FLUSH CAPTURE

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	2	0	0	.01	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	43	1	2	26	4	68	3
----	----	---	---	----	---	----	---

	NC	QT	X1	X2	GR
NC	.03				
QT	1	.03			
X1	1	10.87	.1		
X2	1	4	16.	.3	
GR	1.	0	5.	0	0
		0	11.	0	0
			1.	0	16.

[illegible]

***PROF 1**

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

Variable	Mean	SD	Min	Max	Skewness	Kurtosis
Age	1.000	.50	.50	1.50	.00	.60
Gender	1.000	.50	.50	1.50	.00	.60
Marital Status	1.000	.50	.50	1.50	.00	.60
Education	1.000	.50	.50	1.50	.00	.60
Income	1.000	.50	.50	1.50	.00	.60
Health	1.000	.50	.50	1.50	.00	.60
Stress	1.000	.50	.50	1.50	.00	.60
Depression	1.000	.50	.50	1.50	.00	.60
Loneliness	1.000	.50	.50	1.50	.00	.60
Life Satisfaction	1.000	.50	.50	1.50	.00	.60
Resilience	1.000	.50	.50	1.50	.00	.60
Optimism	1.000	.50	.50	1.50	.00	.60
Gratitude	1.000	.50	.50	1.50	.00	.60
Forgiveness	1.000	.50	.50	1.50	.00	.60
Compassion	1.000	.50	.50	1.50	.00	.60
Empathy	1.000	.50	.50	1.50	.00	.60
Kindness	1.000	.50	.50	1.50	.00	.60
Generosity	1.000	.50	.50	1.50	.00	.60
Patience	1.000	.50	.50	1.50	.00	.60
Humility	1.000	.50	.50	1.50	.00	.60
Modesty	1.000	.50	.50	1.50	.00	.60
Self-control	1.000	.50	.50	1.50	.00	.60
Emotional Stability	1.000	.50	.50	1.50	.00	.60
Conscientiousness	1.000	.50	.50	1.50	.00	.60
Openness	1.000	.50	.50	1.50	.00	.60
Agreeableness	1.000	.50	.50	1.50	.00	.60
Neuroticism	1.000	.50	.50	1.50	.00	.60
Extraversion	1.000	.50	.50	1.50	.00	.60
Conscientiousness	1.000	.50	.50	1.50	.00	.60
Openness	1.000	.50	.50	1.50	.00	.60
Agreeableness	1.000	.50	.50	1.50	.00	.60
Neuroticism	1.000	.50	.50	1.50	.00	.60
Extraversion	1.000	.50	.50	1.50	.00	.60
Conscientiousness	1.000	.50	.50	1.50	.00	.60
Openness	1.000	.50	.50	1.50	.00	.60
Agreeableness	1.000	.50	.50	1.50	.00	.60
Neuroticism	1.000	.50	.50	1.50	.00	.60
Extraversion	1.000	.50	.50	1.50	.00	.60
Conscientiousness	1.000	.50	.50	1.50	.00	.60
Openness	1.000	.50	.50	1.50	.00	.60
Agreeableness	1.000	.50	.50	1.50	.00	.60
Neuroticism	1.000	.50	.50	1.50	.00	.60
Extraversion	1.000	.50	.50	1.50	.00	.60
Conscientiousness	1.000	.50	.50	1.50	.00	.60
Openness	1.000	.50	.50	1.50	.00	.60
Agreeableness	1.000	.50	.50	1.50	.00	.60
Neuroticism	1.000	.50	.50	1.50	.00	.60
Extraversion	1.000	.50	.50	1.50	.00	.60
Conscientiousness	1.000	.50	.50	1.50	.00	.60
Openness	1.000	.50	.50	1.50	.00	.60
Agreeableness	1.000	.50	.50	1.50	.00	.60
Neuroticism	1.000	.50	.50	1.50	.00	.60
Extraversion	1.000	.50	.50	1.50	.00	.60
Conscientiousness	1.000	.50	.50	1.50	.00	.60
Openness	1.000	.50	.50	1.50	.00	.60
Agreeableness	1.000	.50	.50	1.50	.00	.60
Neuroticism	1.000	.50	.50	1.50	.00	.60
Extraversion	1.000	.50	.50	1.50	.00	.60
Conscientiousness	1.000</					

.009857 0. 0. 0. 0 3 .00 10.96 13.48

THIS RUN EXECUTED 15DEC14 16:38:25

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST
6 FOOT WIDE SHALLOW

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
1.000	10.87	.50	.00	2.58	10.96	.73	.60

SUMMARY OF ERRORS AND SPECIAL NOTES

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1*****
* HEC-2 WATER SURFACE PROFILES *****
*
* Version 4.6.2; May 1991
*
* RUN DATE 10DEC14 TIME 15:15:57
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET, SUITE D
* DAVIS, CALIFORNIA 95616-4687
* (916) 756-1104
*****

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X X X XXXXXXXX XXXXX
X X X X X
X X X X
XXXXXXXX XXXX
X X X X
X X X X
X X XXXXXXXX XXXXX

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THIS RUN EXECUTED 10DEC14 15:15:57

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*****
HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991
*****

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```

T1 CHANNEL CAPACITY CALCULATIONS
T2 ANASAZI RIDGE
T3 6 FOOT WIDE SHALLOW CHANNEL - FIRST FLUSH CAPTURE

```

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	0	0	.01	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

	38	43	1	2	26	4	68	3	
NC	.03	.03	.03	.1	.3				
QT	2	11.87	11.87						
X1	1	4	0	16.	0	0	0	0	0
GR	1.	0	0	5.	0	11.	1.	16.	

SECNO	DEPTH	CWSEL	CRIS	QROB	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

```

CCHV= .100 CEHV= .300
*SECNO 1.000
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED
1.000 .52 .00
11.9 .0 11.9 .0
.63 .11 .00 .00 .00 .00
4.5 4.5 .0 .0 .0 .0

```

.00 .00 2.66 .00 .00 .030 .000 .000 .00 2.41
.009993 0. 0. 0. 0 0 0 5 11.18 13.59

T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STPT	METRIC	HVINS	Q	WSEL	FQ
0		3	0	1	.01					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
2		0	-1	0	0	0	0	0	0	0
SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV	
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV	
TIME	VLOB	VCH	VROB	XLNL	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

*PROF 2

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

3720 CRITICAL DEPTH ASSUMED

1.000	.43	.43	.43	.00	.61	.17	.00	.00	1.00
11.9	.0	11.9	.0	.0	3.6	.0	.0	.0	1.00
.00	.00	3.34	.00	.000	.030	.000	.000	.00	2.83
.019115	0.	0.	0.	0	11	5	.00	10.35	13.17

THIS RUN EXECUTED 10DEC14 15:15:57

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

6 FOOT WIDE SHALLOW

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRISW	VCH	TOPWID	FRCH	EG
1.000	11.87	.52	.00	2.66	11.18	.74	.63
*	1.000	11.87	.43	3.34	10.35	1.00	.61

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION SECNO= 1.000 PROFILE= 2 CRITICAL DEPTH ASSUMED

1 *****
* HEC-2 WATER SURFACE PROFILES *****
* *
* Version 4.6.2; May 1991 *
* *
* RUN DATE 10DEC14 TIME 15:14:11 *

***** U.S. ARMY CORPS OF ENGINEERS *****
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

X X X XXXXXXXX XXXXX XXXXX
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X X X X X
XXXXXXXX XXXX XXXXX
X X X X X
X X X X X

THIS RUN EXECUTED 10DEC14 15:14:11

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

T1 CHANNEL CAPACITY CALCULATIONS

T2 ANASAZI RIDGE

T3 10 FOOT WIDE SHALLOW CHANNEL - FIRST FLUSH CAPTURE

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	0	0	.01	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	43	1	2	26	4	68	3
NC	.03	.03	.03	.1	.3		
QT	2	11.87	11.87				
X1	1	4	0	20.	0	0	0
GR	1.	0	0	5.	0	1.	20.

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	ARO	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV=.100 CEHV=.300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

1.000	.41	.41	.00	.00	.50	.09	.00	.00	1.00
11.9	.0	11.9	.0	.0	4.9	.0	.0	.0	1.00
.00	.00	2.43	.00	.000	.030	.000	.000	.00	2.97

.009965 0. 0. 0. 0. 0 0 5 .00 14.06 17.03

T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0		3	0	1	.01					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
2		0	-1	0	0	0	0	0	0	0
SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	OLOSS	HL	L-BANK ELEV	
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	TWA	VOL	R-BANK ELEV	
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	ELMIN	WTN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	TOPWID	CORAR	ENDST	

*PROF 2

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

3720 CRITICAL DEPTH ASSUMED

1.000	.33	.33	.33	.00	.48	.15	.00	.00	1.00
11.9	.0	11.9	.0	.0	3.9	.0	.0	.0	1.00
.00	.00	3.07	.00	.000	.030	.000	.000	.000	3.34
.020179	0.	0.	0.	0	14	5	.00	13.31	16.66

THIS RUN EXECUTED 10DEC14 15:14:11

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

10 FOOT WIDE SHALLOW

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
1.000	11.87	.41	.00	2.43	14.06	.73	.50
* 1.000	11.87	.33	.33	3.07	13.31	1.01	.48

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION SECNO= 1.000 PROFILE= 2 CRITICAL DEPTH ASSUMED

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1*****
* HEC-2 WATER SURFACE PROFILES*****
*
* Version 4.6.2; May 1991
*
* RUN DATE 06JAN15 TIME 09:34:49
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X X XXXXXXXX XXXXX XXXXX
X X X X X X
X X X X X
XXXXXXXX XXXX XXXXX
X X X X X
X X X X X

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THIS RUN EXECUTED 06JAN15 09:34:49
*****
HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991
*****

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T1 SEVILLE UNIT 7 - STREET CAPACITY CALCULATIONS
T2 49'ROW 28'F-F MTB CURB AND GUTTER WITH CROWN
T3 VIZCAYA AVENUE

```

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	1	.02	0	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

	38	43	1	2	26	4	68	3
NC	.017	.017	.017	.1	.3			
QT	1	11.9						
X1	1	9	0	49	0	0	0	0
GR	.53	0	.33	9.87	0	11.47	.125	12.5
GR	.125	36.5	0	37.53	.33	39.13	.53	49

SECNO	DEPTH	CWSEL	CRIS	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

```

CCHV= .100 CEHV= .300
*SECNO 1.000
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

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3265 DIVIDED FLOW

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*****
* U.S. ARMY CORPS OF ENGINEERS
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* DAVIS, CALIFORNIA 95616-4687
* (916) 756-1104
*****

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1.000	.35	.35	.40	.00	.50	.15	.00	.00	.53
11.9	.0	11.9	.0	.0	3.8	.0	.0	.0	.53
.00	.00	3.13	.00	.000	.017	.000	.000	.00	8.77
.020385	0.	0.	0.	0	14	7	.00	30.17	40.23

THIS RUN EXECUTED 06JAN15 09:34:49

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

VIZCAYA AVENUE

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
1.000	11.90	.35	.40	3.13	30.17	1.59	.50

SUMMARY OF ERRORS AND SPECIAL NOTES

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*****
1 *****
* HEC-2 WATER SURFACE PROFILES *
* *
* Version 4.6.2; May 1991 *
* *
* RUN DATE 09JAN15 TIME 14:14:24 *
*****
*****
U.S. ARMY CORPS OF ENGINEERS *
HYDROLOGIC ENGINEERING CENTER *
609 SECOND STREET, SUITE D *
DAVIS, CALIFORNIA 95616-4687 *
(916) 756-1104 *
*****
*****

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[illegible]

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***** 14:14:24 *****
THIS RUN EXECUTED 09JAN15
*****
HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991
*****

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T1 Anasazi Ridge Subdivision - STREET CAPACITY CALCULATIONS 10YR-6HR ST
T2 32' HALF SECTION
T3 MCMAHON BLVD.

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	0	2	0	0	.005	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

[illegible][illegible]

***PROF 1**

CCHV= .100 CEHV= .300

*SECNO	1.000		
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED			
	1.000	.55	.55
			.00

1.39

12.6 .0 12.6 .0 5.5 .0 .0 1.39
 .00 .00 2.32 .00 .017 .000 .00 35.92
 .004986 0. 0. 0. 0 6 .00 23.20 59.12

T1
 T2
 T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0		3	0	0	.005					

J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
2		0	-1	0	0	0	0	0	0	0

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	CORAR	TOPWID	ENDST

*PROF 2

CCHV= .100 CEHV= .300
 *SECNO 1.000
 2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED
 1.000 .60 .60 .00 .00 .69 .09 .00 .00 1.39
 16.4 .0 16.4 .0 .0 6.7 .0 .0 1.39
 .00 .00 2.46 .00 .000 .017 .000 .00 35.91
 .004926 0. 0. 0. 0 5 .00 25.66 61.57

THIS RUN EXECUTED 09JAN15 14:14:24

 HEC-2 WATER SURFACE PROFILES
 Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

MCMAHON BLVD.

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
1.000	12.64	.55	.00	2.32	23.20	.84	.63
1.000	16.37	.60	.00	2.46	25.66	.85	.69

SUMMARY OF ERRORS AND SPECIAL NOTES

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

[illegible]

THIS RUN EXECUTED 09JAN15 13:56:21

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

T1 Anasazi Ridge Subdivision - STREET CAPACITY CALCULATIONS 10YR-6HR ST
T2 32' HALF SECTION
T3 MCMAHON BLVD.

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	2	0	0	.0054	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

	38	43	1	2	26	4	68	3
NC	.017	.017						
QT	2	12.64	16.37	.1	.3			
X1	1	6	0	68.1	0	0	0	0
GR	1.39	0	.67	35.9	0	36.0	0.125	38.0
GR	1.395	68.1						68.

SECNO	DEPTH	CWSEL	CRIS	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPMID	ENDST

***PROF 1**

CCHV=	.100	CEHV=	.300
-------	------	-------	------

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

1.000	.54	.54	.00
-------	-----	-----	-----

12.6	.0	12.6	.0	5.3	.0	1.39
12.6	.0	12.6	.0	5.3	.0	1.39

.00 .00 2.39 .00 .00 .017 .000 .000 .00 35.92
.005381 0. 0. 0. 0 6 .00 22.86 58.78

T1
T2
T3

J1 ICHECK INQ NINV IDIR STPT METRIC HVINS Q WSEL FQ

0 3 0 0 .0054

J2 NPROF IPLOT PRFVS XSECV XSECH FN ALLDC IBW CHNIM ITRACE

2 0 -1 0 0 0 0 0 0 0

SECNO DEPTH CWSEL CRIWS WSELK EG HV HL L-BANK ELEV
Q QLOB QCH QROB ALOB ACH AROB VOL TWA R-BANK ELEV
TIME VLOB VCH VROB XNL XNCH XNR WTN SSTA
SLOPE XLOBL XLCH XLOBR ITRIAL IDC ICNT CORAR TOPWID ENDST

*PROF 2

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

1.000 .59 .59 .00 .00 .69 .10 .00 .00 1.39
16.4 .0 16.4 .0 .0 6.5 .0 .0 1.39
.00 .00 2.53 .00 .00 .017 .000 .00 35.91
.005303 0. 0. 0. 0 5 .00 25.31 61.22

THIS RUN EXECUTED 09JAN15 13:56:21

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

MCMAHON BLVD.

SUMMARY PRINTOUT

SECNO Q CWSEL CRIWS VCH TOPWID FRCH EG
1.000 12.64 .54 .00 2.39 22.86 .87 .63
1.000 16.37 .59 .00 2.53 25.31 .88 .69

SUMMARY OF ERRORS AND SPECIAL NOTES

```

1*****
* HEC-2 WATER SURFACE PROFILES *****
* *
* Version 4.6.2; May 1991
* *
* RUN DATE 09JAN15 TIME 14:09:33 *
*****
***** U.S. ARMY CORPS OF ENGINEERS *****
***** HYDROLOGIC ENGINEERING CENTER *****
***** 609 SECOND STREET, SUITE D *****
***** DAVIS, CALIFORNIA 95616-4687 *****
***** (916) 756-1104 *****
*****

```

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X X XXXXXXX XXXX XXXX
X X X X X X
X X X X X X
XXXXXXX XXXX XXXX
X X X X X X
X X X X X X

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THIS RUN EXECUTED 09JAN15 14:09:33
*****
HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991
*****

```

```

T1 Anasazi Ridge Subdivision - STREET CAPACITY CALCULATIONS 10YR-6HR ST
T2 32' HALF SECTION
T3 MCMAHON BLVD.

```

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	0	0	.0065	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

	38	43	1	2	26	4	68	3
NC	.017	.017	.017	.1	.3			
QT	2	12.64	16.37					
X1	1	6	0	68.1	0	0	0	0
GR	1.39	0	.67	35.9	0	36.0	0.125	38.0
GR	1.395	68.1						0.725
								68.

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV= .100 CEHV= .300

```

*SECNO 1.000
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED
1.000 .52 .00 .63 .10 .00 .00 1.39
12.6 .0 12.6 .0 4.9 .0 0 1.39
.00 .00 2.56 .00 .017 .000 .00 35.92

```

.006463 0. 0. 0. 0. 0 0 6 .00 22.08 58.00

T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0		3	0	0	.0065					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
2		0	-1	0	0	0	0	0	0	0
SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV	
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV	
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

*PROF 2

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

1.000	.57	.57	.00	.00	.69	.12	.00	.00	1.39
16.4	.0	16.4	.0	.0	6.0	.0	.0	.0	1.39
.00	.00	2.73	.00	.000	.017	.000	.000	.00	35.91
.006492	0.	0.	0.	0	0	6	.00	24.35	60.26

THIS RUN EXECUTED 09JAN15 14:09:33

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

MCMAHON BLVD.

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRISW	VCH	TOPWID	FRCH	EG
1.000	12.64	.52	.00	2.56	22.08	.95	.63
1.000	16.37	.57	.00	2.73	24.35	.97	.69

SUMMARY OF ERRORS AND SPECIAL NOTES

1*****
* HEC-2 WATER SURFACE PROFILES *****
* * * * *
* Version 4.6.2; May 1991 *
* * * * *
* RUN DATE 06JAN15 TIME 14:07:08 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

X X X XXXXXXXX XXXX XXXX
X X X X X X
X X X X X
XXXXXXXX XXXX
X X X X X
X X X X X
X X XXXXXXXX XXXX
X X XXXXXXXX XXXX

THIS RUN EXECUTED 06JAN15 14:07:08

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

T1 CHANNEL CAPACITY CALCULATIONS
T2 ANASAZI RIDGE
T3 8 FOOT WIDE SHALLOW CHANNEL - SPILLWAY

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	0	0	.01	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	43	1	2	26	4	68	3
NC	.017	.017	.017	.1	.3		
QT	2	10.87	10.87				
X1	1	4	0	8.2	0	0	0
GR	.67	0	0	.1	0	.67	8.2

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV= .100 CEHV= .300
*SECNO 1.000
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED
3720 CRITICAL DEPTH ASSUMED
1.000 .38 .38 .00 .19 .00 .00 .67

10.9 .0 10.9 .0 3.1 .0 .0 .67
.00 .00 3.51 .00 .017 .000 .04
.006474 0. 0. .0 7 .00 8.11 8.16

T1
T2 SPILLWAY
T3 8' WIDE

J1 ICHECK INQ NINV IDIR STRT METRIC HVINS Q WSEL FQ
0 3 0 1 .01

J2 NPROF IPLOT PRFVS XSECV XSECH FN ALLDC IBW CHNIM ITRACE
2 0 -1 0 0 0 0 0 0 0
SECNO DEPTH CWSEL CRIWS WSELK EG HV HL OLOSS L-BANK ELEV
Q QLOB QCH QROB QROB ALOB ACH AROB VOL TWA R-BANK ELEV
TIME VLOB VCH VROB VROB XNL XNL XNCH XNR WTN ELMIN SSTA
SLOPE XLOBL XLCH XLCH XLOBR XLOBR ITRIAL IDC IDC CORAR TOPWID ENDST

*PROF 2

CCHV= .100 CEHV= .300
*SECNO 1.000
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED
1.000 .34 .34 .38 .00 .59 .25 .00 .00 .67
10.9 .0 10.9 .0 .0 2.7 .0 .0 .0 .67
.00 .00 4.03 .00 .000 .017 .000 .00 .00 .05
.010100 0. 0. 0. 0 7
THIS RUN EXECUTED 06JAN15 14:07:08

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

8 FOOT WIDE SHALLOW

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
*	1.000	10.87	.38	3.51	8.11	1.00	.58
	1.000	10.87	.34	4.03	8.10	1.23	.59

SUMMARY OF ERRORS AND SPECIAL NOTES

APPENDIX C – STORMWATER MANAGEMENT DESIGN

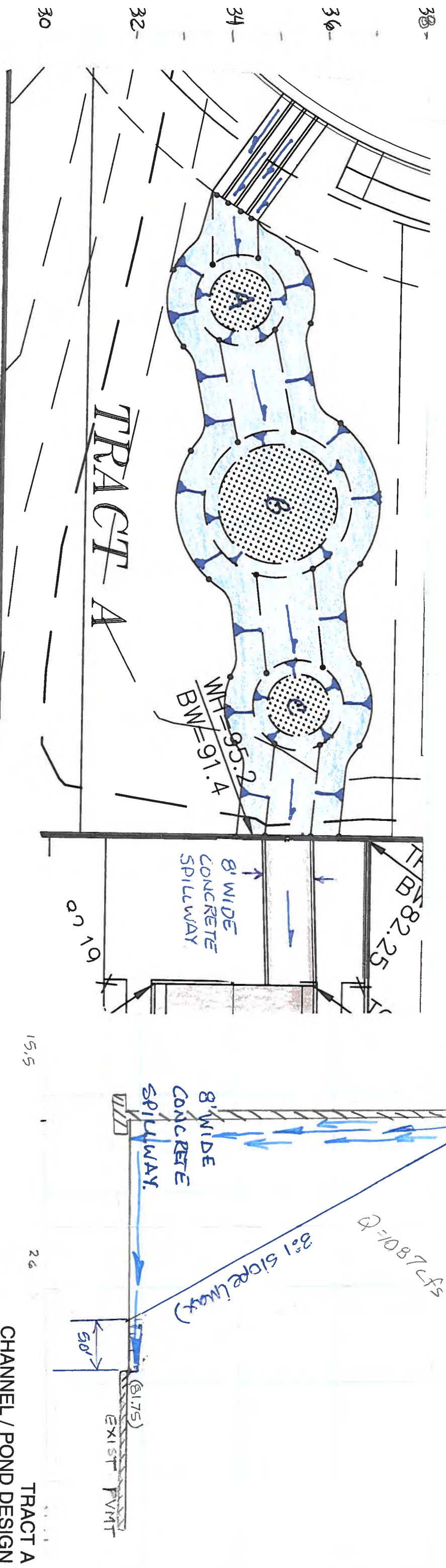
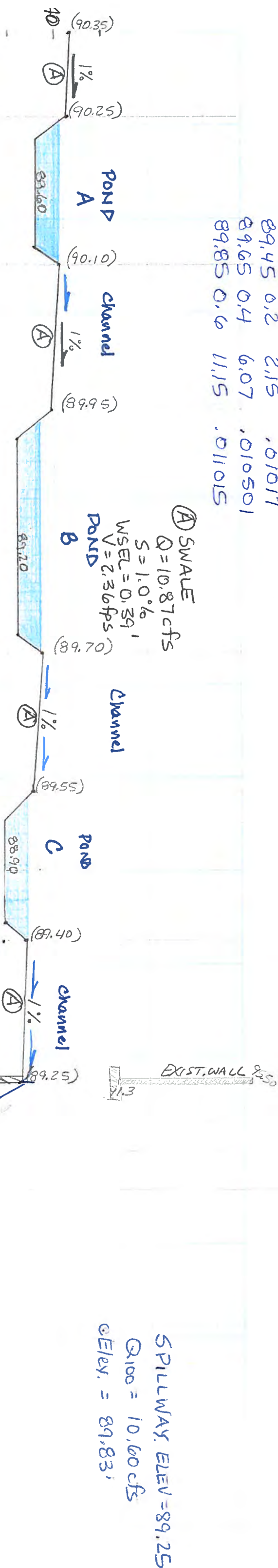
*Tract A Pond / Channel
Spillway /Channel Vizcaya Avenue*

Tract A - Spillway Rating Table (for Attynud rating)

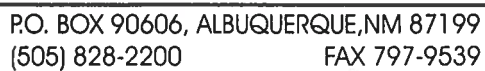
Spillway crest = 89.25
 Spillway crest length = 8'

$$Q = C \cdot L \cdot H^{3/2} = 3(8)H^{3/2}$$

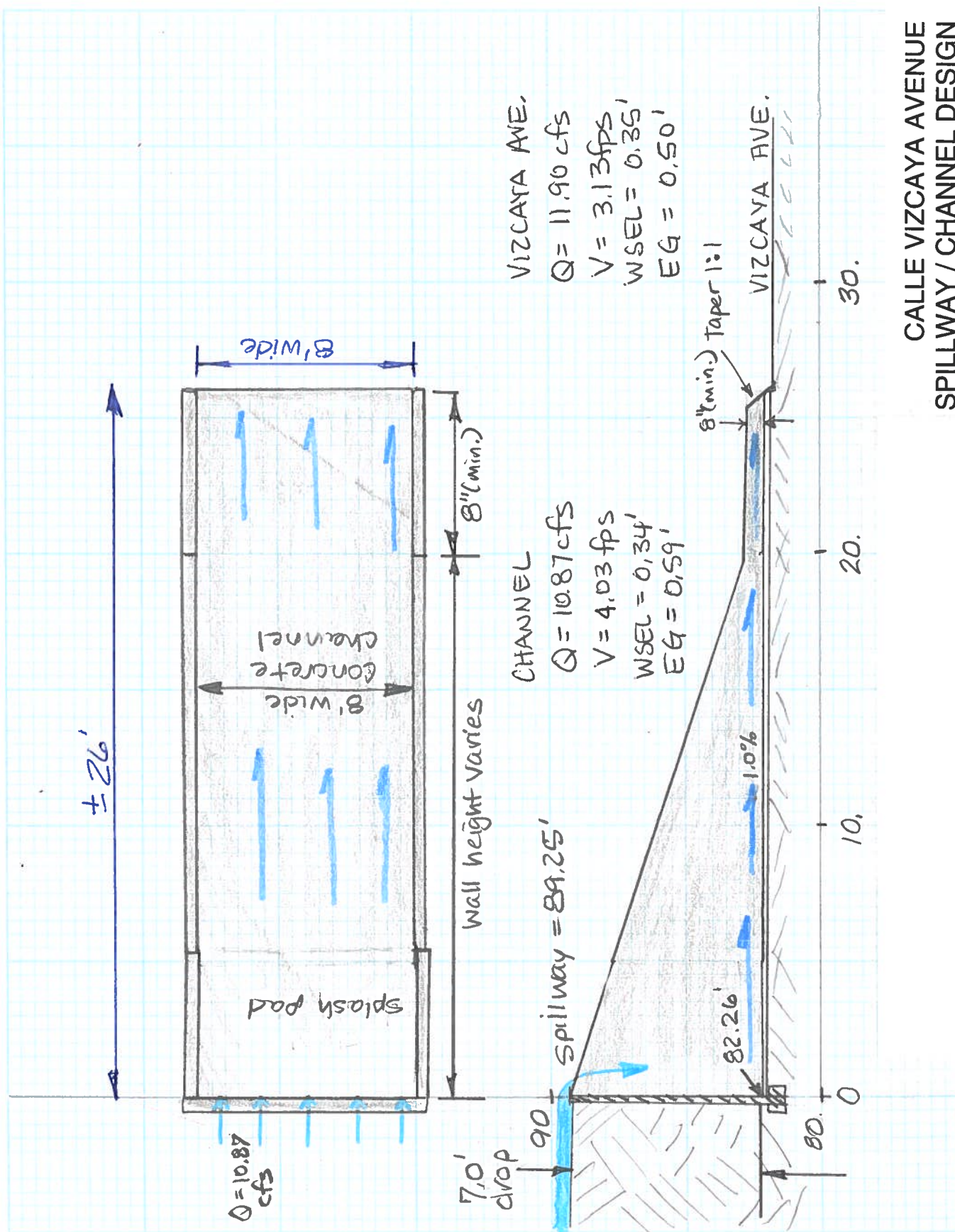
Elev.	H	Q	Storage Vol. (A.F.)
89.25	0	0	
89.45	0.2	2.15	.01017
89.65	0.4	6.07	.010501
89.85	0.6	11.15	.011015



TRACT A
 CHANNEL / POND DESIGN



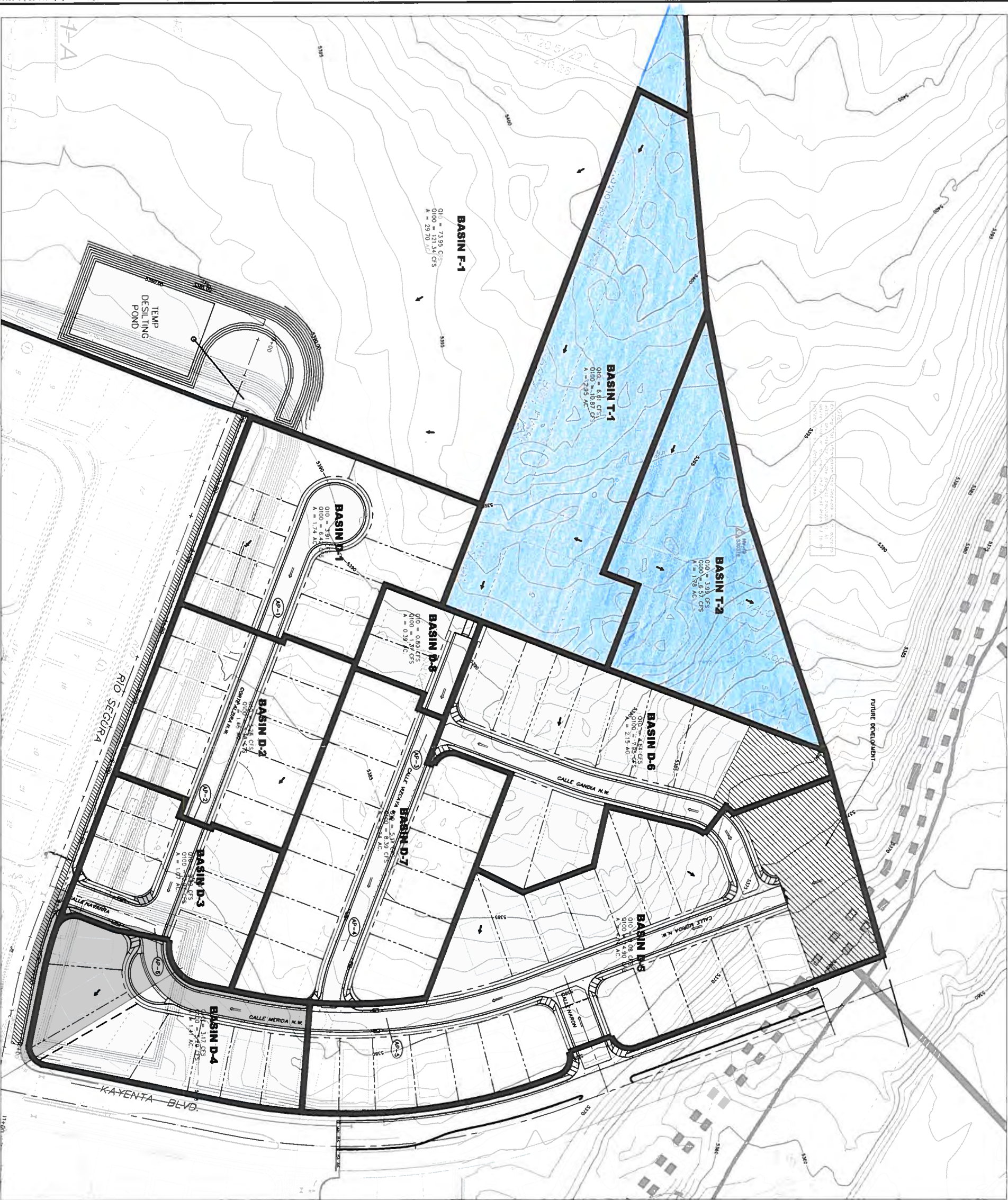
PROJECT Anasazi Ridge
SUBJECT Spillway Design
BY ALT DATE 1-6-15
CHECKED _____ DATE _____
SHEET _____ OF _____



APPENDIX D

Seville Unit 7 Drainage Plan (Wilson & Co.)

- ***Existing Sub Basin exhibit***
- ***Developed Sub Basin exhibit***



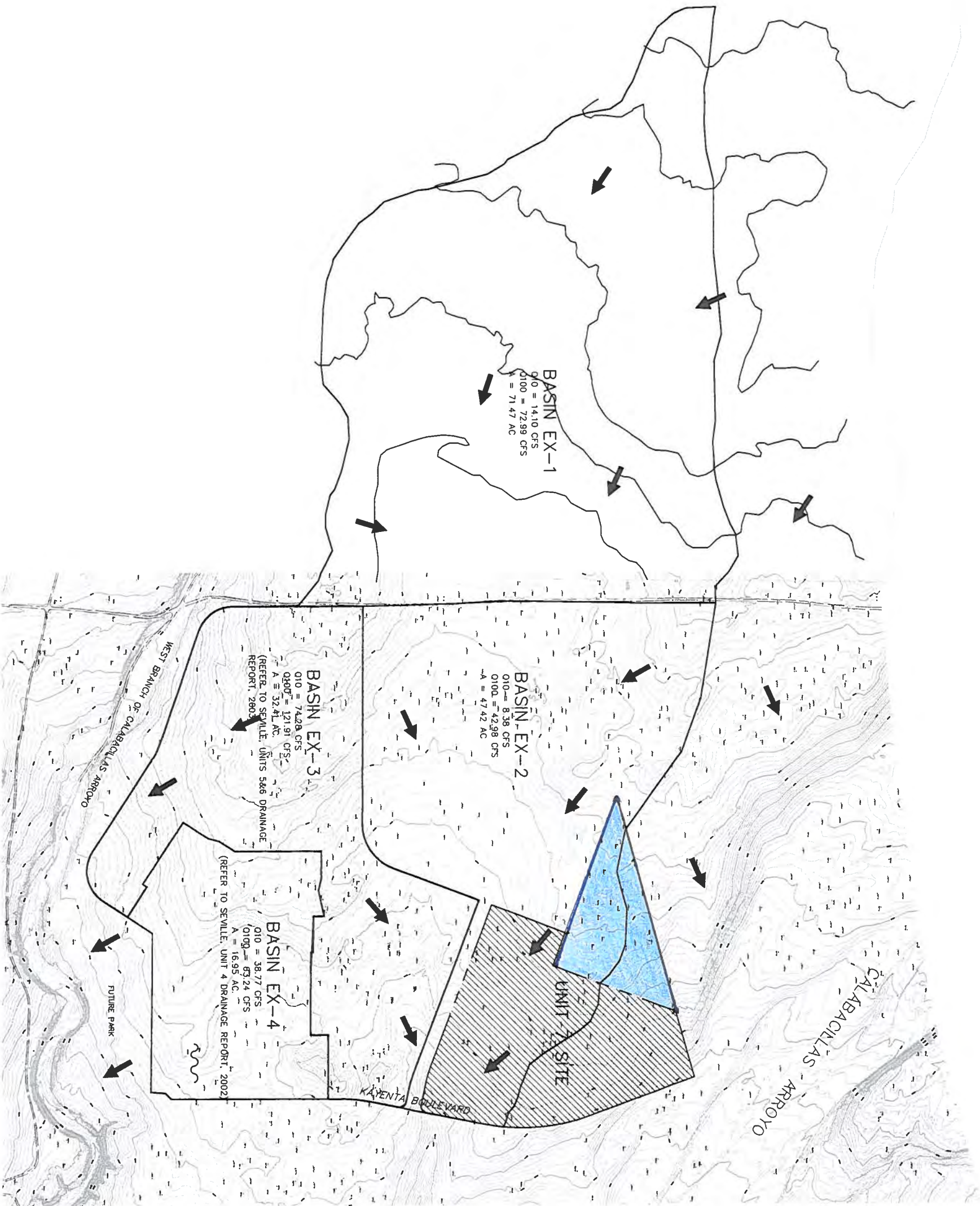
HYDROLOGIC DATA - DEVELOPED

BASIN	AREA (acres)	A	B	C	D	YIELD (cf/acre)	Q ₁₀₀ (cfs)	Q ₁₀ (cfs)	Q ₂ (cfs)
D-1	1.74	0	10	30	60	3.68	8.42	0.22	
D-2	1.46	0	10	30	60	3.68	5.38	0.18	
D-3	1.07	0	10	30	60	3.71	3.92	0.16	
D-4	1.41	0	10	30	60	3.69	5.20	0.18	
D-5	4.04	0	10	30	60	3.69	14.50	0.52	
D-6	2.15	0	10	30	60	3.69	7.95	0.28	
D-7	2.24	0	10	30	60	3.69	8.39	0.29	
D-8	0.39	0	10	30	60	3.36	1.31	0.05	
T-1	2.95	0	10	30	60	3.69	10.87	0.37	
T-2	1.78	0	10	30	60	3.69	6.57	0.22	

STREET HYDRAULIC DATA

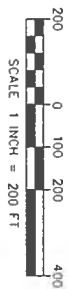
AP	θ INLET (ft)	SLOPE (%)	Q ₁₀₀ (cfs)	Q ₁₀ (cfs)	Q ₂ (cfs)	D ₁₀₀ (ft)	D ₁₀ (ft)	D ₂ (ft)	DNV (ft)	V ₂ (ft/s)
AP-1	-	0.68	6.42	-	-	0.34	1.87	1.07	0.64	0.38
AP-2	-	1.60	11.80	-	-	0.36	2.98	1.07	0.64	0.47
AP-3	-	0.61	10.89	-	-	0.40	2.15	0.88	0.68	0.46
AP-4	1A & 1B	0.81	28.52	28.52	0.00	0.44	2.47	1.09	0.89	0.52
AP-5	2A & 2B	0.65	14.90	14.90	0.00	0.44	2.47	1.09	0.52	
AP-6	3A & 3B	2.02	20.97	20.97	0.00	0.41	3.59	1.64	0.81	

$$V_2 = \left[\frac{V^2}{2g} \right] \times 0.8 + D_{100}$$



HYDROLOGIC DATA - EXISTING									
BASIN	DESCRIPTION	AREA (acres)	LAND TREATMENT PERCENTAGES BY TYPE				YIELD (cu/acre)	Q _{avg} (cfs)	W _{avg} -1 (cfs-ft)
			A	B	C	D			
EX-1	UNDEVELOPED	71.47	85	0	5	0	1.02	72.88	2.83
EX-2	UNDEVELOPED	47.42	85	0	5	0	0.92	42.88	0.91
EX-3	SEWAGE UNIT 3 & 6	32.41	0	10	30	60	3.76	121.91	4.24
EX-4	SEWAGE UNIT 4	18.95	0	10	30	60	3.73	63.24	2.21

- LEGEND**
- DRAINAGE FLOW ARROW
 - BASIN BOUNDARY
 - HIGH POINT IN EXISTING ROADWAY



WILSON & COMPANY		SEVILLE SUBDIVISION UNIT 7	
2600 THE SUITE 100 R.O. BAILEY RD. NEA NE CO 8724 (505) 395-8121		BASIN BOUNDARY MAP EXISTING CONDITIONS	
REVISIONS		BY	
NO	DATE	REMARKS	
DESIGN	JRW	W/E-A NO	X2218030 DATE JULY 2003
DRAWN	JRW	PROJECT NO	N/A
CHECK	DSA	SHEET NO	1 OF 1

APPENDIX E

McMahon Blvd. Extension Report Excerpts

McMahon Blvd. Hydrology

Calculations and Analysis

Google Earth Photos



MCMAHON BOULEVARD EXTENSION

PRELIMINARY DRAINAGE REPORT

July 2009

Prepared for:

City of Albuquerque
Department of Municipal Development
Transportation Division
One Civic Plaza
Albuquerque, New Mexico 87102

Prepared by:

URS Corporation
One Park Square
6501 Americas Parkway NE, Suite 900
Albuquerque, NM 87110

URS Project Number: 24343019

URS

1. INTRODUCTION

This drainage report is for the two lane extension of McMahon Boulevard to Universe Boulevard and the extension of Universe Boulevard to McMahon Boulevard. Both streets will eventually be median-divided, four lane roads with two lanes in each direction. However, this project is providing construction plans for just the west half of Universe Boulevard and the north half of McMahon Boulevard. The purpose of this drainage report is to allow phased construction to proceed. This project is located on City of Albuquerque Zone Atlas page A-10. The project limits are shown on Figure 1 below.

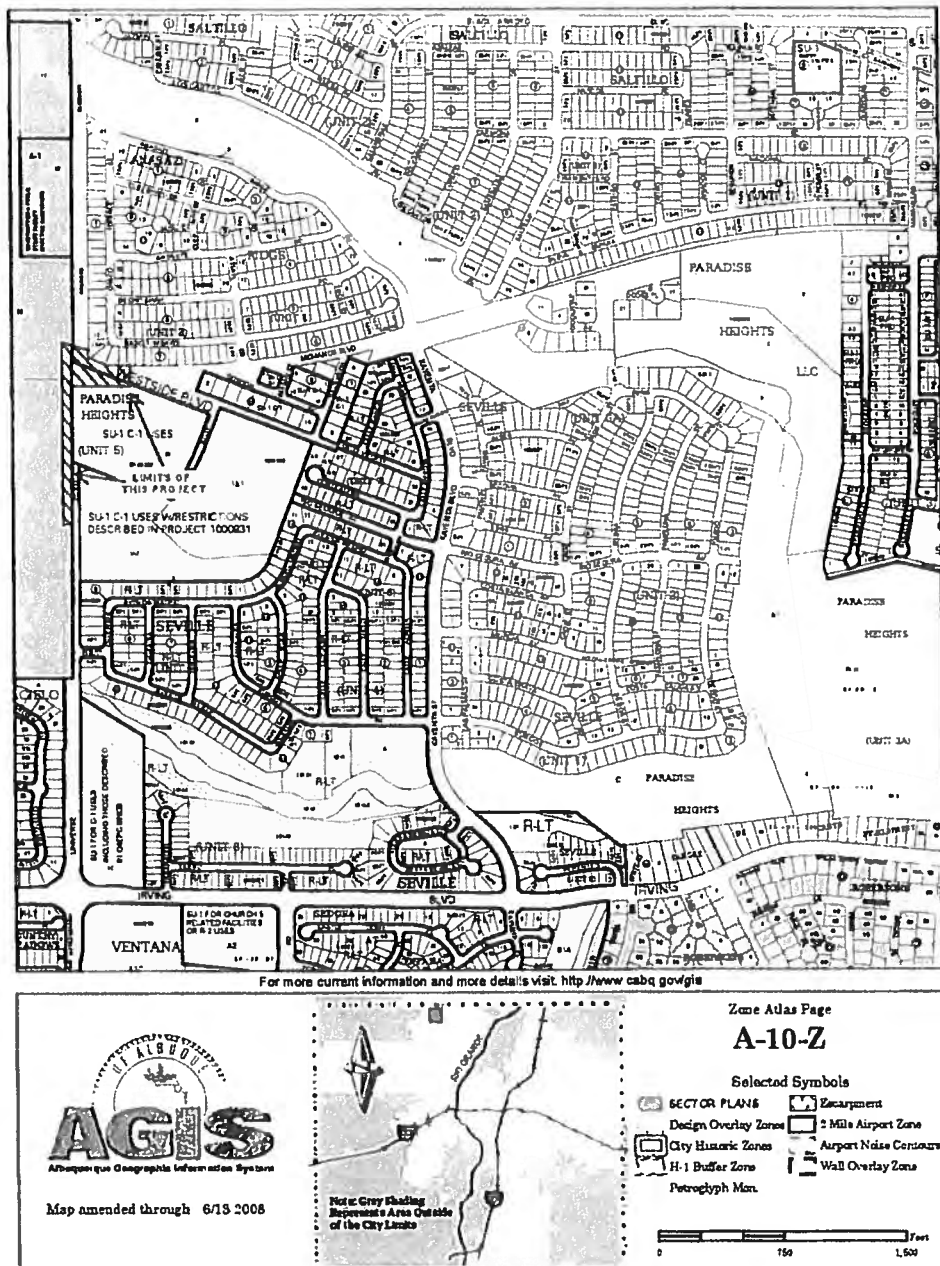


Figure 1 - Vicinity Map

MCMAHON BOULEVARD EXTENSION

DRAINAGE REPORT

Table 1 - Summary of Hydrology

BASIN ID	AREA		LAND TREATMENT (%)				t _p	PEAK 100-YR FLOW ⁽²⁾		PEAK 10-YR FLOW ⁽²⁾	
	(AC)	(SQ MI)	A	B	C	D		(HR)	Inc. (cfs)	Cum (cfs)	Inc. (cfs)
EXISTING CONDITIONS (See Figure 2)											
RW-1	3.7	0.0058	25	0	75	0	0.13	10.15	199.80	4.62	102.32
OS-1	29.9	0.0467	100	0	0	0	0.22	28.90		5.58	
RW-2	5.0	0.0078	85	0	15	0	0.13	8.50	35.67	2.13	7.32
B-3	47.7	0.0745	25	5	30	40	0.13	159.12	189.65	86.79	92.80
OS-1A	12.1	0.0189	90	0	10	0	0.13	19.72		4.61	
OS-1B	3.8	0.0059	90	0	10	0	0.13	6.16		1.44	
RW-1C	11.6	0.0181	20	0	55	25	0.13	37.42	43.58	19.80	21.24
Subtotal	113.8	0.1777									
DEVELOPED CONDITIONS (See Figure 3)											
RW-1	3.7	0.0058	0	0	87	13	0.13	12.71	202.36	7.00	99.80
OS-1	29.9	0.0467	100	0	0	0	0.22	28.90		5.58	
RW-2	5.0	0.0078	85	0	15	0	0.13	8.50	35.67	2.13	7.32
B-3	47.7	0.0745	25	5	30	40	0.13	159.12	189.65	86.79	92.80
OS-1A	12.1	0.0189	90	0	10	0	0.13	19.72		4.61	
OS-1B	3.8	0.0059	90	0	10	0	0.13	6.16		1.44	
RW-1C	11.6	0.0181	20	0	50	30	0.13	38.36	44.52	20.70	22.14
Subtotal	113.8	0.1777									
FUTURE CONDITIONS (See Figure 5)											
RW-1.1	0.38	0.0005	0	0	33	67	0.13	1.39		0.87	
RW-1.2	0.38	0.0005	0	0	33	67	0.13	1.39		0.87	
RW-1.3A	1.64	0.0027	0	0	100	0	0.13	5.56		2.92	
RW-1.3B	0.51	0.0011	0	0	33	67	0.13	2.89		1.82	
RW-1.4	0.50	0.0011	0	0	33	67	0.13	2.89		1.82	
FUTURE CONDITIONS (See Figure 4)											
RW-1	3.7	0.0058	0	0	74	26	0.13	13.48	163.97	7.72	101.62
OS-1	29.9	0.0467	100 ⁽¹⁾	0	0	0	0.22	28.90		5.58	
RW-2	5.0	0.0078	0	0	40	60	0.13	20.83	45.64	12.91	16.80
B-3	35.5	0.0555	0	10	20	70	0.13	150.49	163.97	93.90	101.62
OS-1A	12.1	0.0189	75	0	20	5	0.13	23.49		7.54	
OS-1B	3.8	0.0059	75	0	20	5	0.13	7.35		2.36	
RW-1C	11.6	0.0181	0	0	40	60	0.13	48.32	55.67	29.95	32.31
Subtotal	113.8	0.1777									

Notes:

- ⁽¹⁾ Future conditions OS-1 will be limited to historic runoff rate. Thus Group A is appropriate for Existing, Developed, and Future Conditions.
- ⁽²⁾ All flow rates are bulked by a factor of 1.10 for 10% sediment by volume.

7. HYDRAULIC CALCULATION PROCEDURES

The City's DPM Section 22 is used to establish the drainage design criteria for this project. It requires that the 10-YR water spread will allow for one lane to remain open in both directions. In order to keep one lane open, the allowable depths may not exceed 0.33 foot for 10-YR flows on

OS-1 to the existing historic rate. Since the Rio Rancho annexation, increased flows from the TVI MDP offsite basins are no longer expected.

The *Albuquerque Technical Vocational Institute West Side Campus Phase 2* construction plans, dated 11-17-2005, were prepared by Van H. Gilbert Architect, and the associated Drainage Report, dated 11-18-2005, was prepared by Jeff Mulberry, PE, of Bohannon Huston, Inc. (see Appendix E). The report deviated significantly from the 2001 TVI MDP in that it did not include the second entrance on McMahon Boulevard and it did not provide for construction of any of the frontage improvements.

The *McMahon Blvd Inlet Calculations Affecting both Saltillo and Anasazi Subdivisions*, dated April 21, 2006, prepared by James D. Hughes, PE of Mark Goodwin and Associates, showed a high spot on McMahon Boulevard about 800 feet west of Universe Boulevard (see Appendix F). This implied that Basin OS-1 from the TVI MDP would drain along its historic path through the TVI campus instead of the Master Planned route east in McMahon Boulevard to Universe Boulevard and south in Universe Boulevard to the West Branch of the Calabacillas Arroyo. These calculations served as the basis for constructing the north half of McMahon Boulevard from the current west end of the pavement to the next high point which is located about 4,700 feet east of Universe Boulevard at Rockcliff Drive with very little storm sewer in McMahon Boulevard. The calculations demonstrated that McMahon Boulevard has adequate street drainage capacity in accordance with Section 22 of the City of Albuquerque Development Process Manual (DPM). These calculations have been verified as accurate for this design.

Additional planning history references are located in Appendix A.

3. EXISTING DRAINAGE CONDITIONS

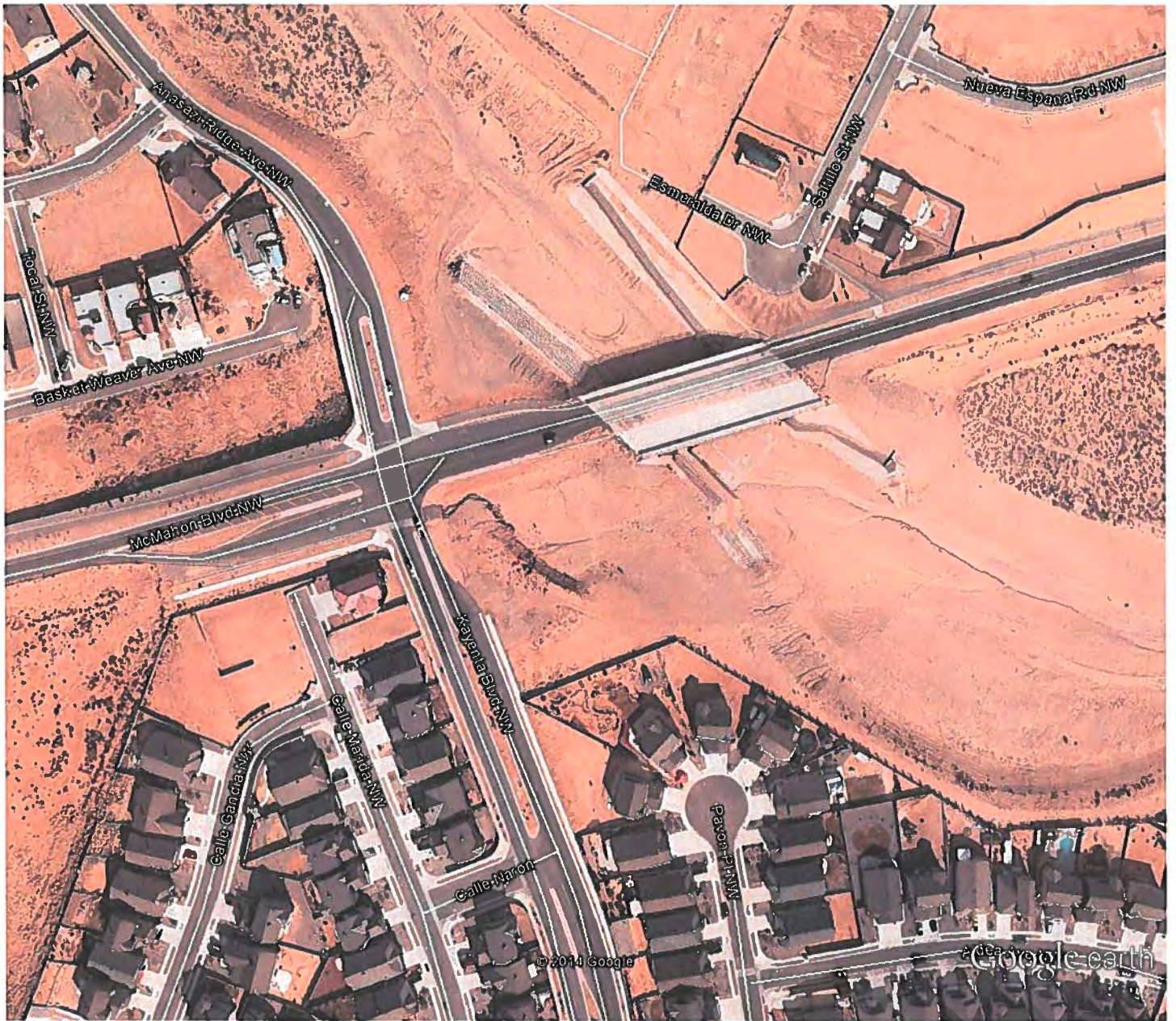
Existing Watershed Boundaries are shown on Figure 2. Four existing drainage outfalls were constructed by previous projects.

1. **Surface drainage in McMahon Boulevard, including runoff from Basins OS-1B and RW-1C (see Figure 3-2 for Existing Drainage Basins), flows east to existing storm inlets located east of the Calabacillas Arroyo, which discharge into the arroyo through a 120 inch storm sewer below the bridge.**
2. Runoff from the Central New Mexico Community College (CNM) Westside Campus basin B-3 and upstream offsite basins OS-1 and RW-2, drain into **an existing 60 inch storm sewer located in Universe Boulevard about 150 feet north of the campus entrance which flows south and discharges into the West Branch of the Calabacillas Arroyo just below the bridge.** This pipe was constructed by CNM as part of the Phase 1 infrastructure as identified in their 2001 Master Drainage Plan. However, when CNM built Phase 2 in 2005 they did not construct any of the Master Planned infrastructure in Universe Boulevard or McMahon Boulevard. Phase 2 provided an onsite conveyance system rather than the Master Planned offsite conveyance system for runoff from offsite Basins OS-1 and RW-2.
3. Runoff from basin RW-1 drains east through the undeveloped property in the southeast corner of the intersection of McMahon Boulevard and Universe Boulevard and flows into **an 18 inch storm sewer at the west end of Rio Segura Avenue.**



Google earth





Google earth

feet
meters



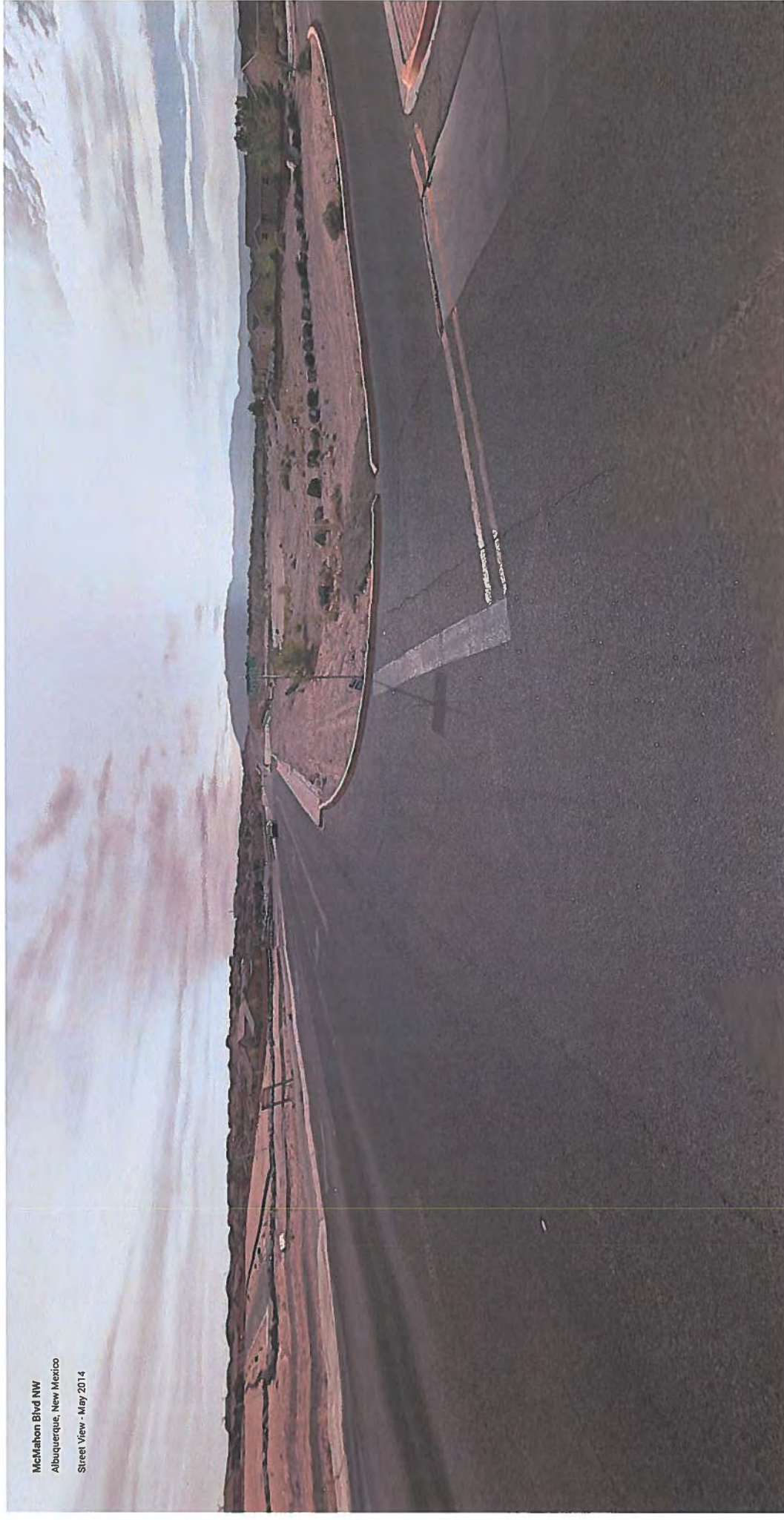




Google earth

feet 7
meters 2





McMahon Blvd NW
Albuquerque, New Mexico
Street View - May 2014

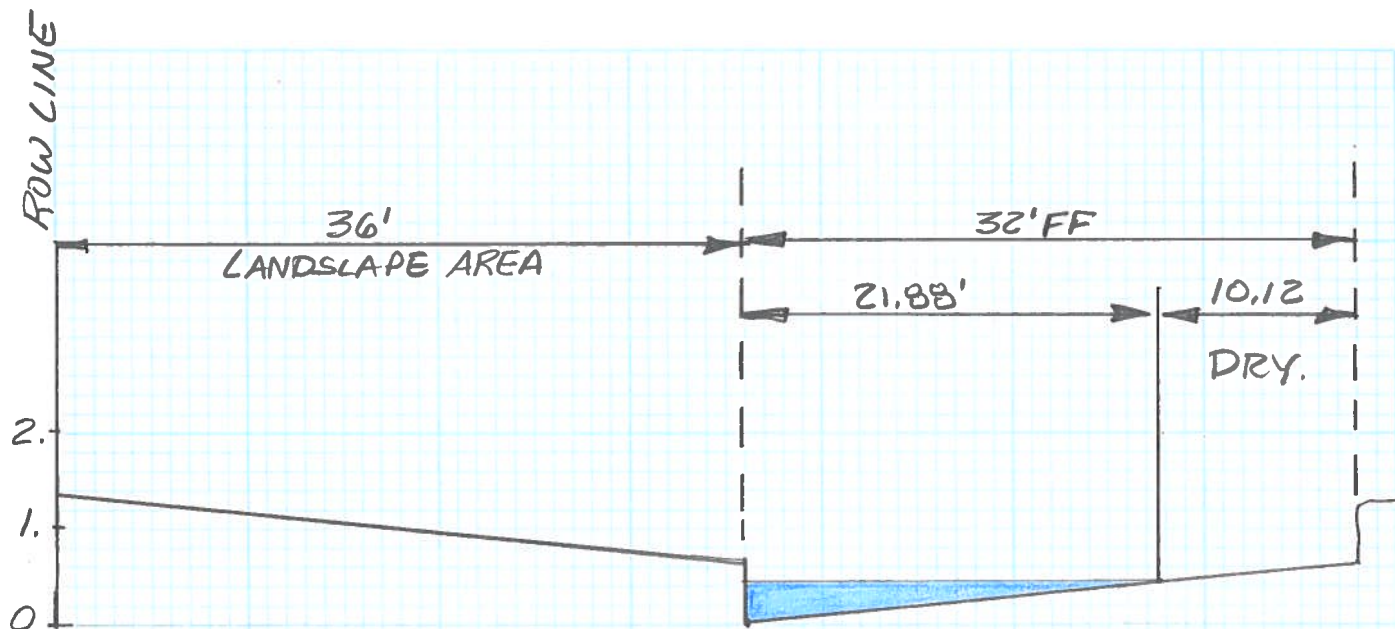
43
(12)
(30)
(32)



D. Mark Goodwin & Associates, P.A.
Consulting Engineers

P.O. BOX 90606, ALBUQUERQUE, NM 87199
(505) 828-2200 FAX 797-9539

PROJECT Anasazi Ridge
SUBJECT McMahon Blvd.
BY DLH DATE 1-12-15
CHECKED _____ DATE _____
SHEET _____ OF _____



FLAT SECTION

WORST CASE SCENARIO

SLOPE = 0.5%

$Q(10 \text{ YEAR}) = 10.83 \text{ cfs}$ (REFER TO FIGURE 4)

WSEL = 0.52'

$V = 2.23 \text{ fps}$

TOPW = 21.88

```
X      X      XXXX
X      X      X
XXXXXX
X      X      XXXX
XXXXXX
X      X      XXXX
XXXXXX
X      X      XXXX
XXXXXX
X      X      XXXX
XXXXXX
```

Version 4.6.2; May 1991

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	2	0	0	.005	0	0	0	0	0

38	43	1	2	26	4	68	3
NC	.017	.017	.1	.3			
QT	3	10.83	10.83				
X1	1	6	68.1	0	0	0	0
GR	1.39	0	35.9	0	36.0	0.125	0.725
		.67				38.0	68.

CCHV= .100 CEHV= .300

*SECNO	1.000	2096	WSEL	NOT	GIVEN,	AVG	OF	MAX,	MIN	USED
	1.000	.52				.52				.00
	10.8	.0				10.8				.0
	.00	.00				2.23				.00
	.004968	.0				.0				.0

T1	T2	T3
----	----	----

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0		3	0	0	.0054					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
2		0	-1	0	0	0	0	0	0	0
SECNO	DEPTH	CWSEL	CRIS	WSELK		EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB		ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL		XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL		IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 2

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

1.000	.51	.51	.00	.00	.60	.08	.00	.00	1.39
10.8	.0	10.8	.0	.0	4.7	.0	.0	.0	1.39
.00	.00	2.29	.00	.000	.017	.000	.00	.00	35.92
.005359	0.	0.	0.	0	0	6	.00	21.57	57.49

T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0		3	0	0	.0065					
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
2		0	-1	0	0	0	0	0	0	0
SECNO	DEPTH	CWSEL	CRIS	WSELK		EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB		ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XNL		XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL		IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 3

CCHV= .100 CEHV= .300

*SECNO 1.000

2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED

1.000	.50	.50	.00	.00	.59	.09	.00	.00	1.39
10.8	.0	10.8	.0	.0	4.4	.0	.0	.0	1.39
.00	.00	2.45	.00	.000	.017	.000	.00	.00	35.93
.006425	0.	0.	0.	0	0	6	.00	20.83	56.75

THIS RUN EXECUTED 12JAN15 09:14:52

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

MCMAHON BLVD.

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
1.000	10.83	.52	.00	2.23	21.88	.83	.60
1.000	10.83	.51	.00	2.29	21.57	.86	.60
1.000	10.83	.50	.00	2.45	20.83	.94	.59

10 YR STORM
0.5% slope

SUMMARY OF ERRORS AND SPECIAL NOTES

McMahon Blvd. - west
of Kayenta along
flat area of Road.

1*****
* HEC-2 WATER SURFACE PROFILES *
* * *
* Version 4.6.2; May 1991 *
* * *
* RUN DATE 12JAN15 TIME 09:56:34 *

***** U.S. ARMY CORPS OF ENGINEERS *****
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *

X X X XXXXXXX XXXXX XXXXX
X X X X X X X
X X X X X X X
XXXXXXXX XXXX XXXXX
X X X X X X
X X X X X X

THIS RUN EXECUTED 12JAN15 09:56:34

HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991

T1 CHANNEL CAPACITY CALCULATIONS
T2 ANASAZI RIDGE at Kayenta Blvd.
T3 VALLEY GUTTER TO 10' WIDE CHANNEL Calabacillas Arroyo

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
0	2	0	0	.0045	0	0	0	0	0	0

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38	43	1	2	26	4	68	3			
NC	.017	.017	.1	.3						
QT	1	18.13								
X1	1	3	0	100	0	0	0	0	0	0
GR	.45	0	0	40	.30	.35	100			

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	OLOSS	L-BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	R-BANK ELEV
TIME	VLOB	VCH	VROB	XLN	KNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV= .100 CEHV= .300

*SECNO 1.000
2096 WSEL NOT GIVEN, AVG OF MAX, MIN USED
3280 CROSS SECTION 1.00 EXTENDED .04 FEET

1.000	.34	.34	.00	.00	.39	.05	.00	.00	.45
-------	-----	-----	-----	-----	-----	-----	-----	-----	-----

```

18.1      .0      18.1      .0      .0      .0      .30
.00      .00      1.85      .00      .000      .000      9.89
.004454    0.      0.      0.      0      0      65.00
                                     THIS RUN EXECUTED 12JAN15 09:56:34

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```

*****
HEC-2 WATER SURFACE PROFILES
Version 4.6.2; May 1991
*****

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NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

VALLEY GUTTER TO 10'

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	VCH	TOPWID	FRCH	EG
1.000	18.13	.34	.00	1.85	55.11	.77	.39

SUMMARY OF ERRORS AND SPECIAL NOTES

McMahon @ Kayenta
Valley Gutter - Low Area

(A) CONSTRUCT HEADER CURB AT EDGE OF NEW PAVEMENT AND C&G, INSTALL TYPE-III BARRICADE

(B) TIE TO EXISTING GROUND, 4:1 MAX. SLOPE

(C) 4:1 SLOPE (MAX), TURN 2 BLOCKS ON SIDE TO ALLOW SMALL DRAINAGE TO PASS FOR TRACT C AND A PORTION OF LOT 1. CREATE 2.0' WIDE GRAVEL PROTECTED RUNDOWN

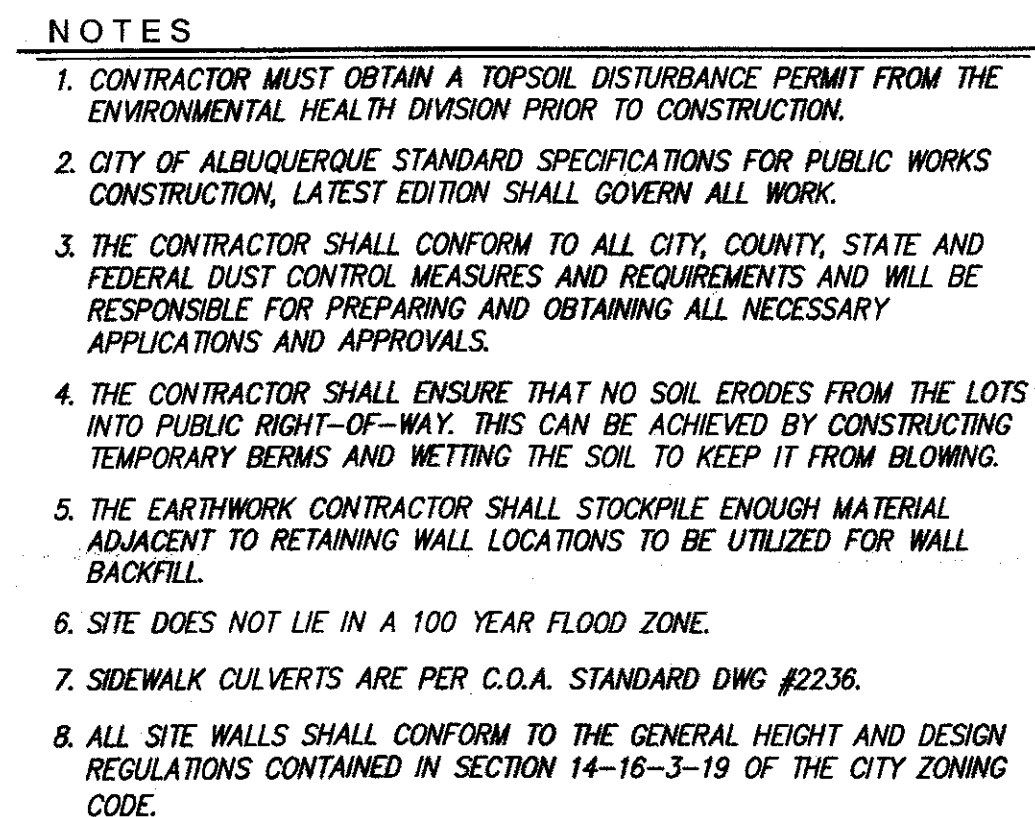
(D) TURN 1 BLOCK SIDEWAYS FOR DRAINAGE OUTLET

(E) CONSTRUCT 8" WIDE CHANNEL SECTION TO BE DESIGNED AT DRC

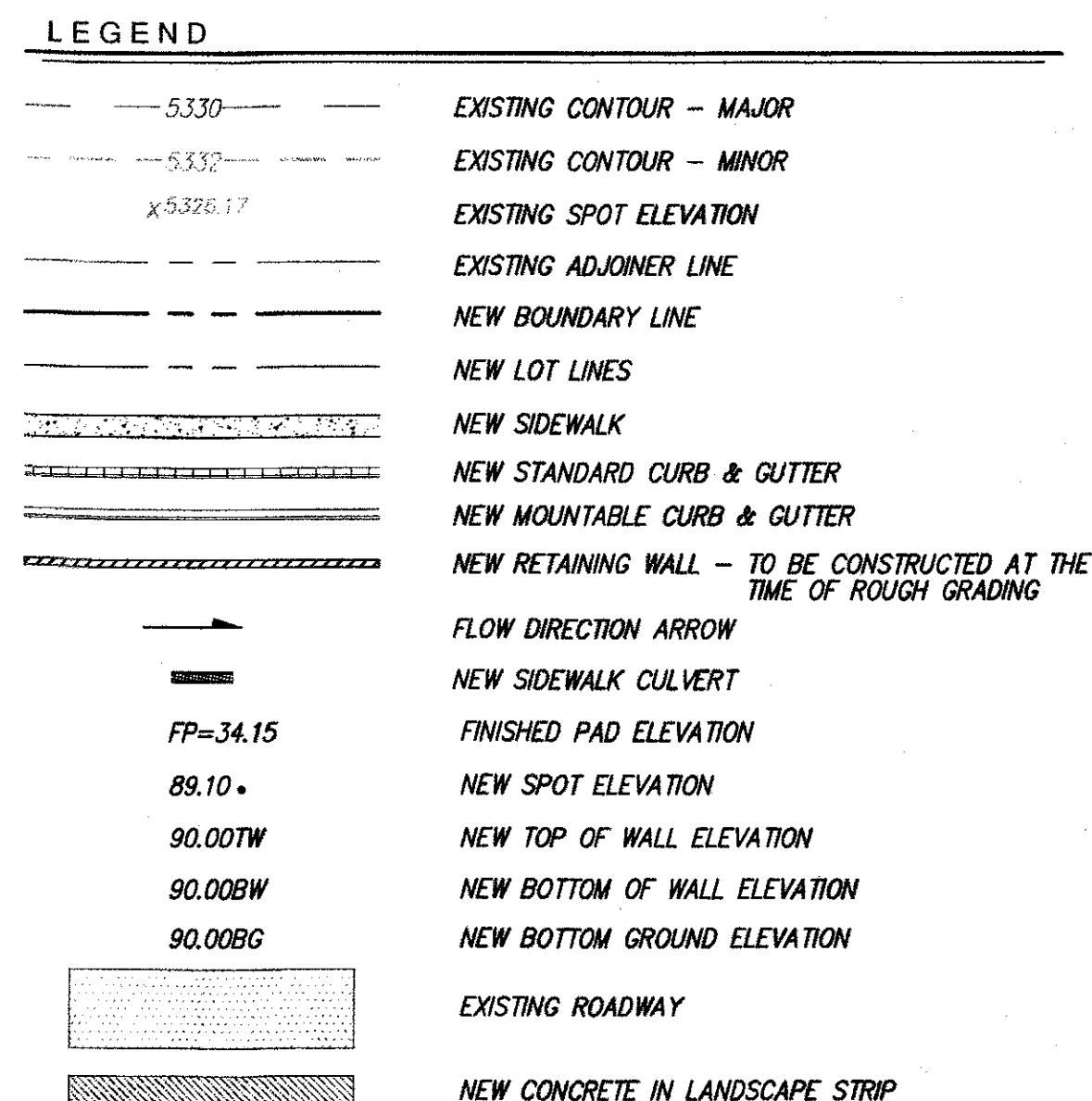
(F) CONSTRUCT HEADER CURB AT EDGE OF NEW PAVEMENT AND C&G

(G) 24" & 12" SIDEWALK CULVERT PER C.O.A. STD. DWG #2236 (DESIGN AT DRC--SEE DRAINAGE REPORT FOR HYDRAULIC CALCULATIONS)


(H) 24" SIDEWALK CULVERT PER C.O.A. STD. DWG #2236




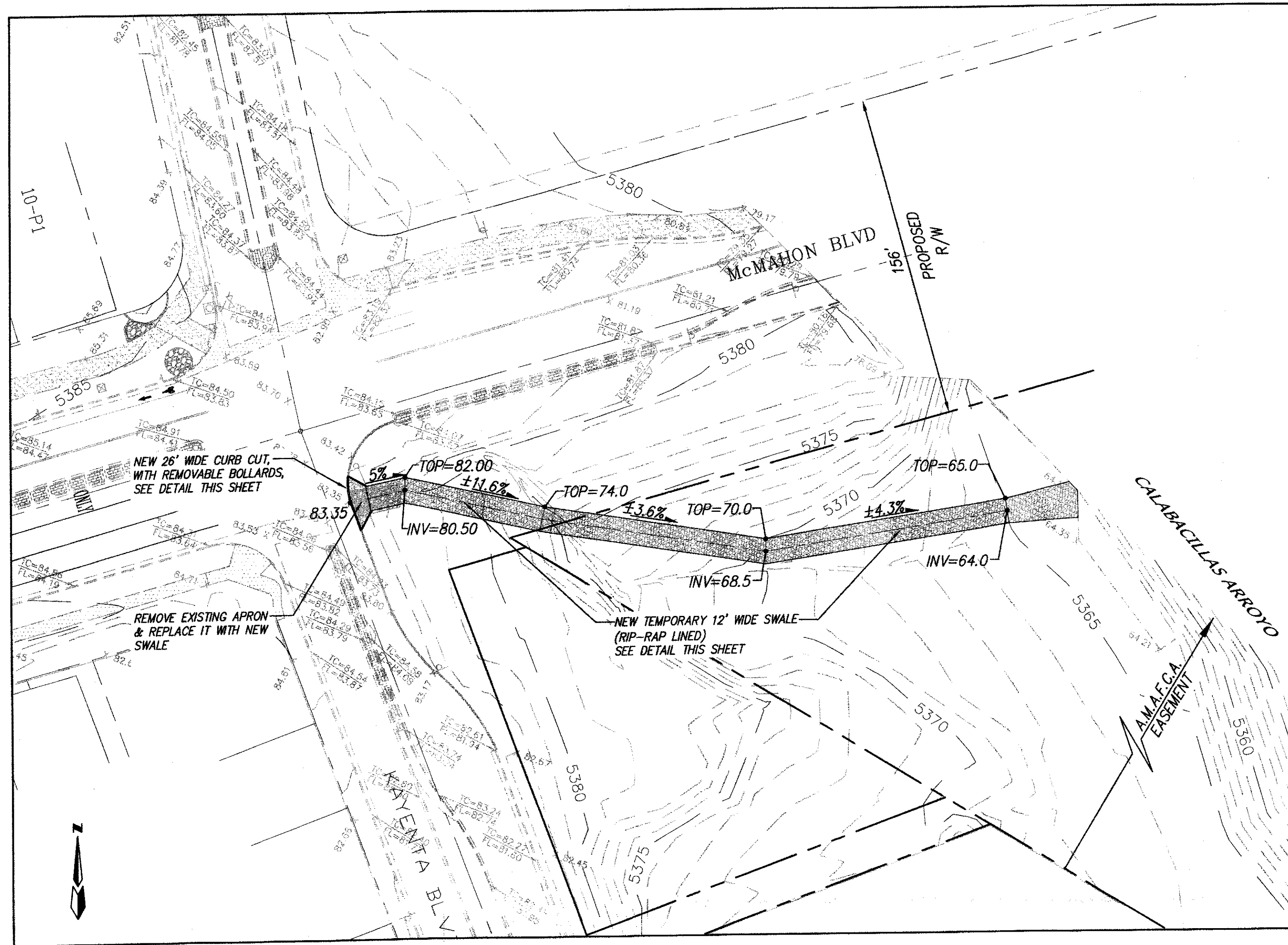
A tract of land situated within the Town of Alameda Grant, projected Section 3, Township 11 North, Range 2 East, New Mexico Principal Meridian, City of Albuquerque, Bernalillo County, New Mexico being a portion of LOT 3 and all of LOTS 4 thru 9, BLOCK 7, all of LOTS 9 thru 13, BLOCK 8, all of LOT 12, BLOCK 9, all of LOTS 1 through 6, BLOCK 10, all of LOTS 1 through 6, BLOCK 11, GORDON AVENUE NW, MASON DRIVE NW, WESTSIDE BOULEVARD NW and McMAHON BOULEVARD NW, PARADISE HEIGHTS UNIT 5, as the same is shown and designated on said plat filed for record in the office of the County Clerk of Bernalillo County, New Mexico, Volume D-1370, in Volume DS, Folio 111 and 112, and containing 6,926 acres more or less.



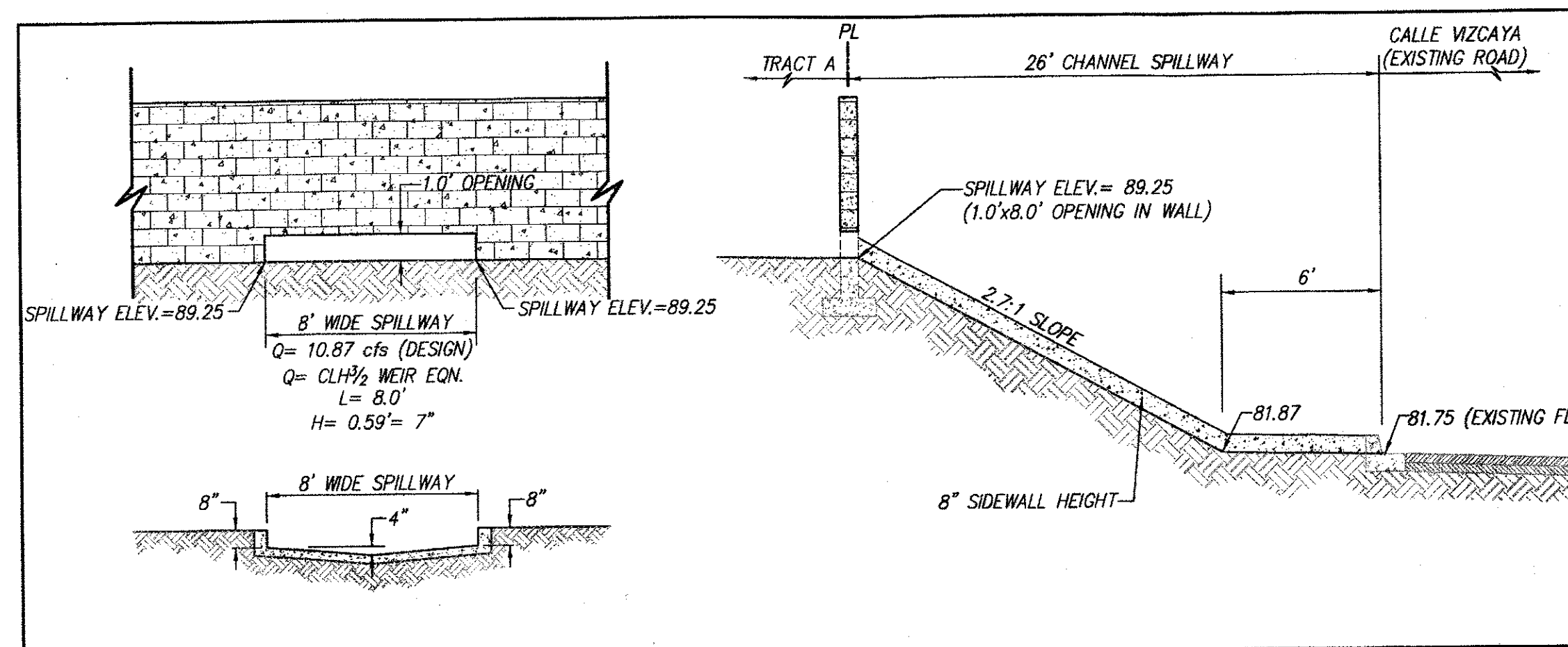
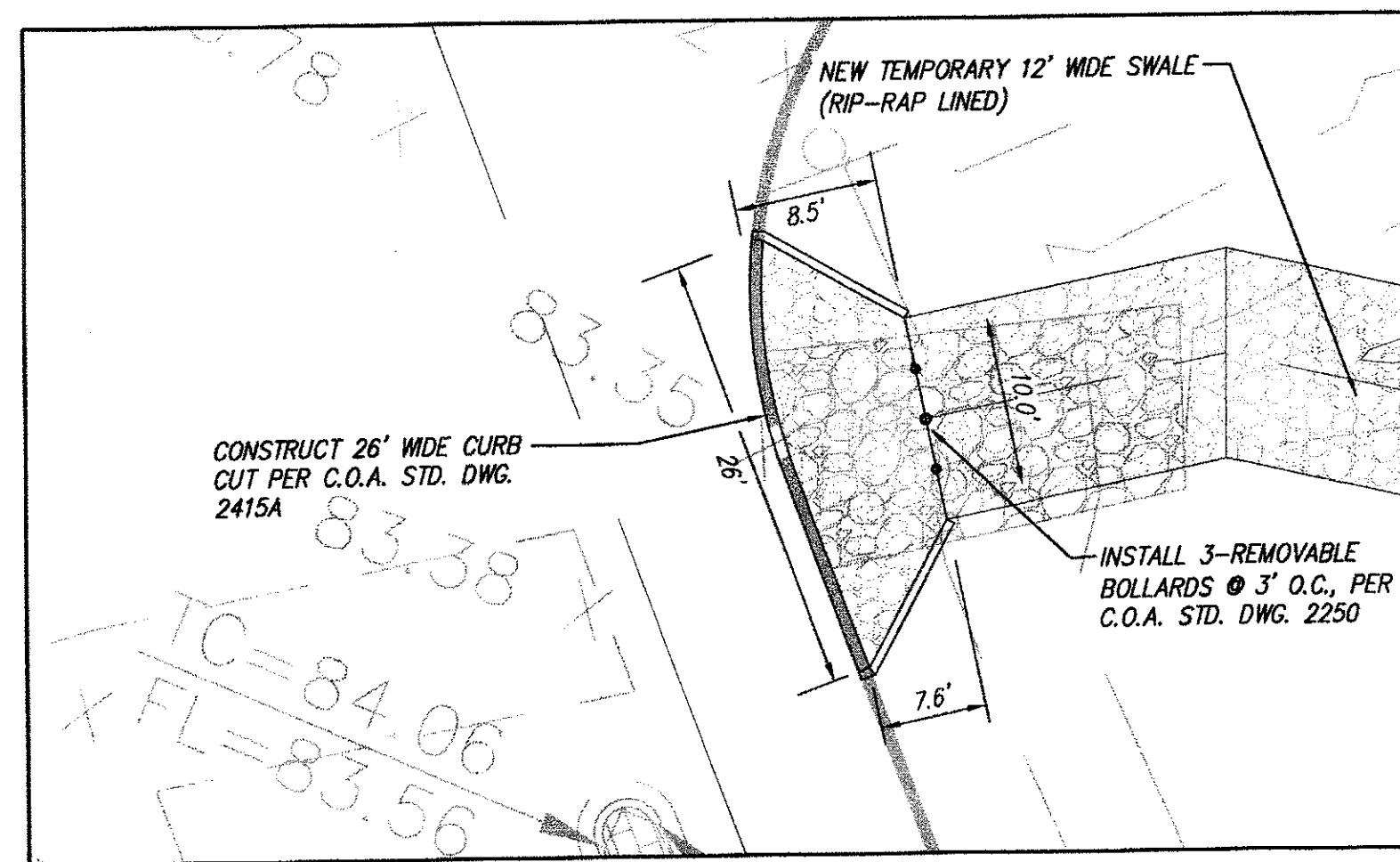
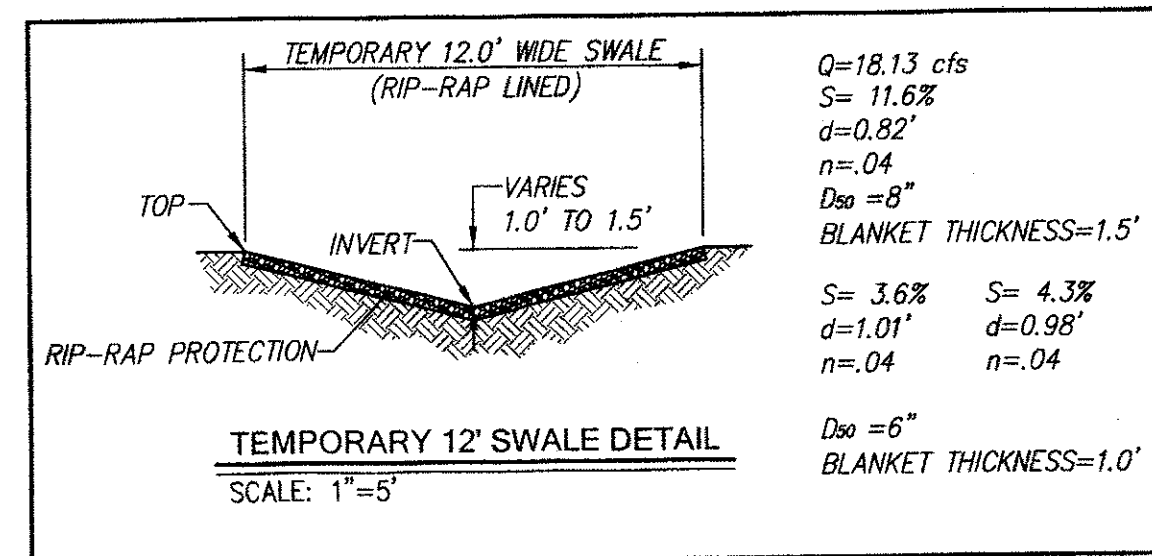
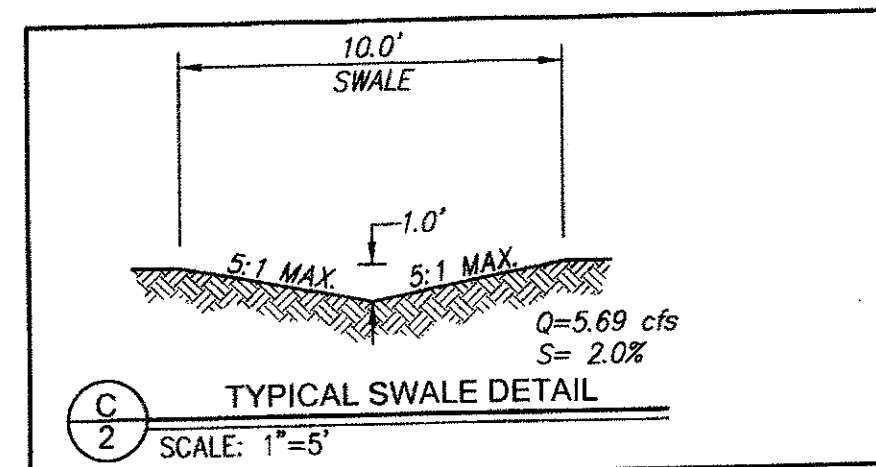
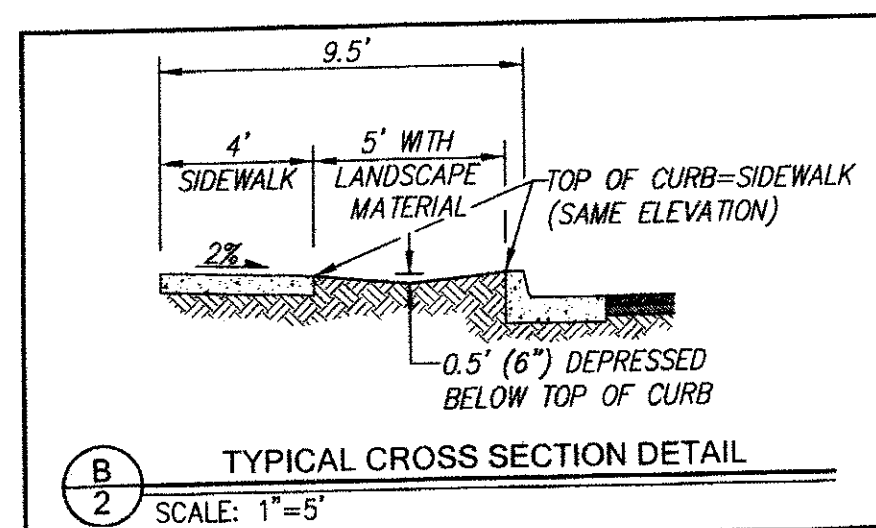
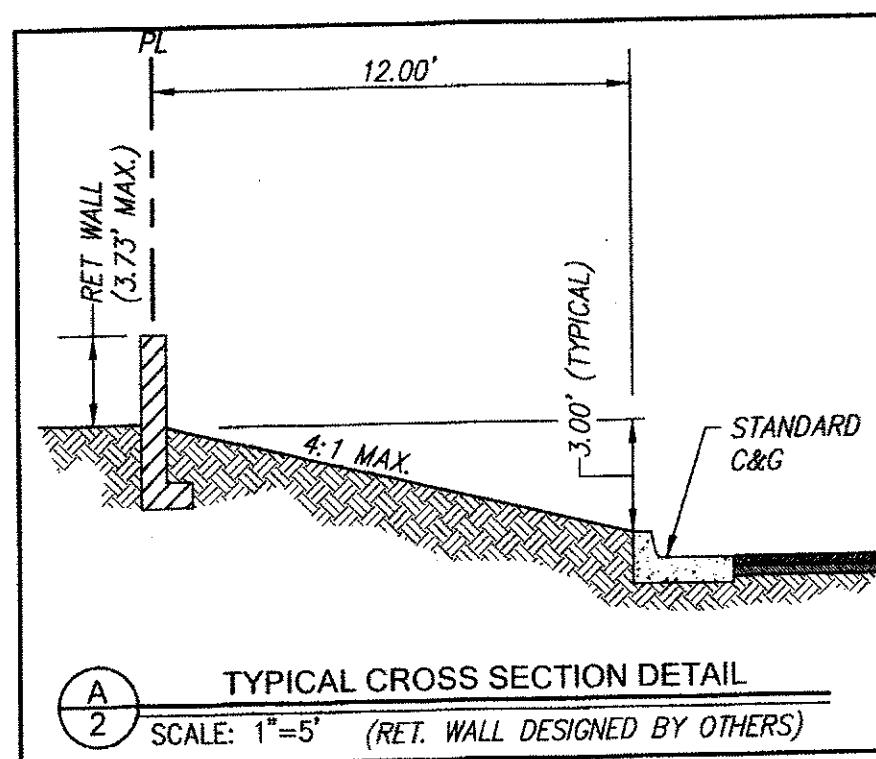
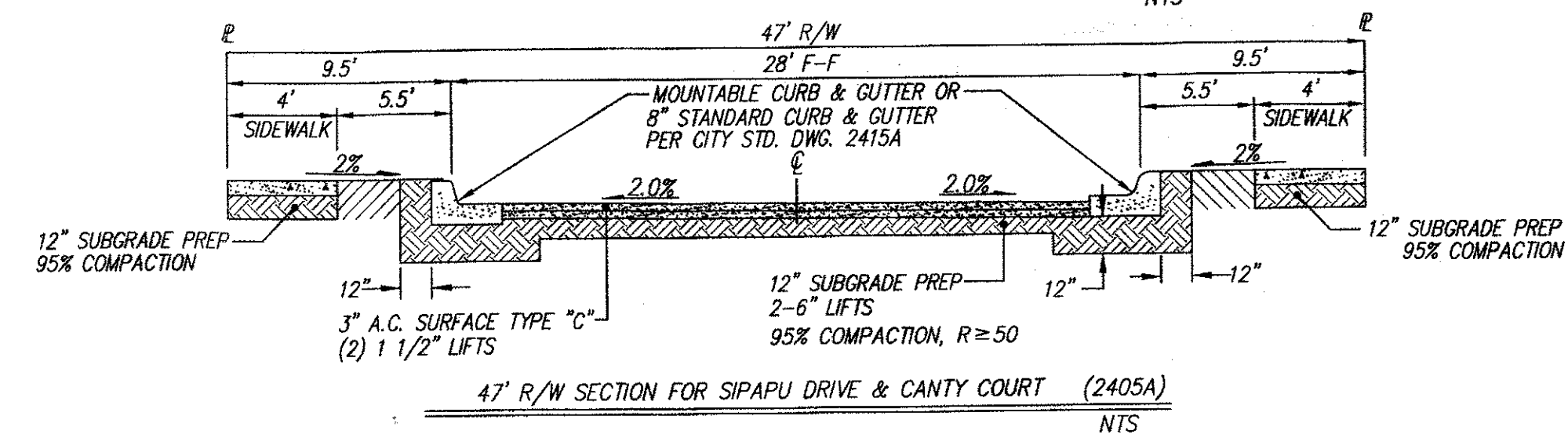
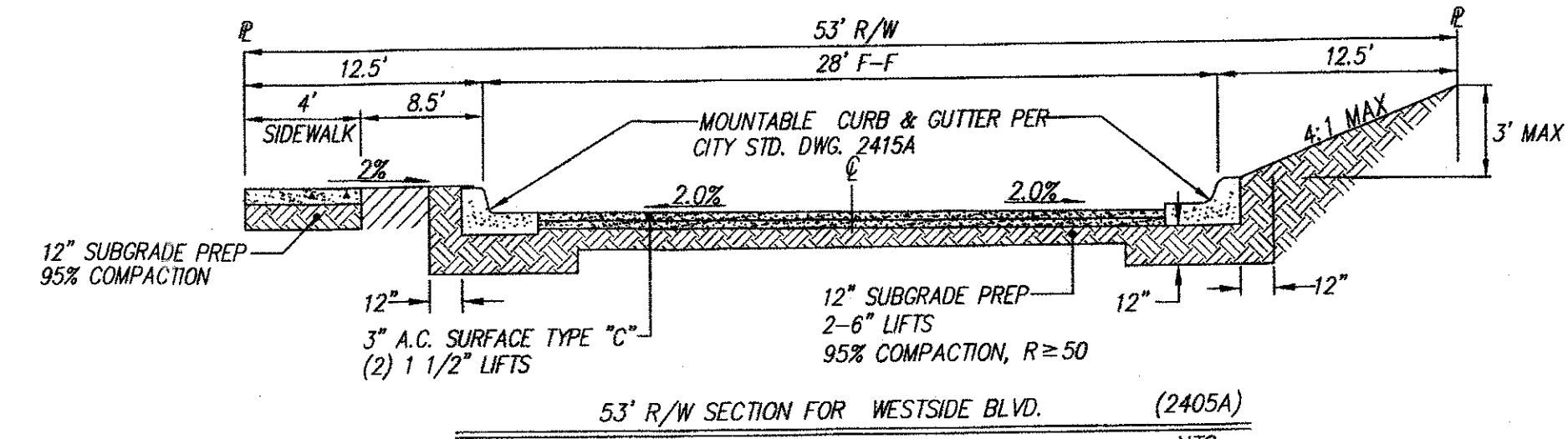
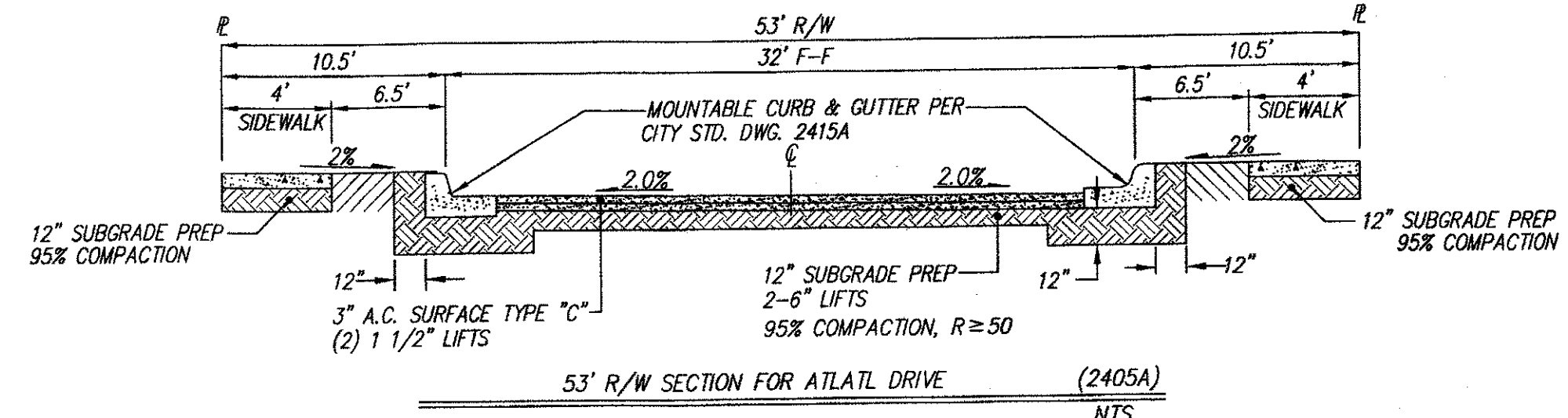
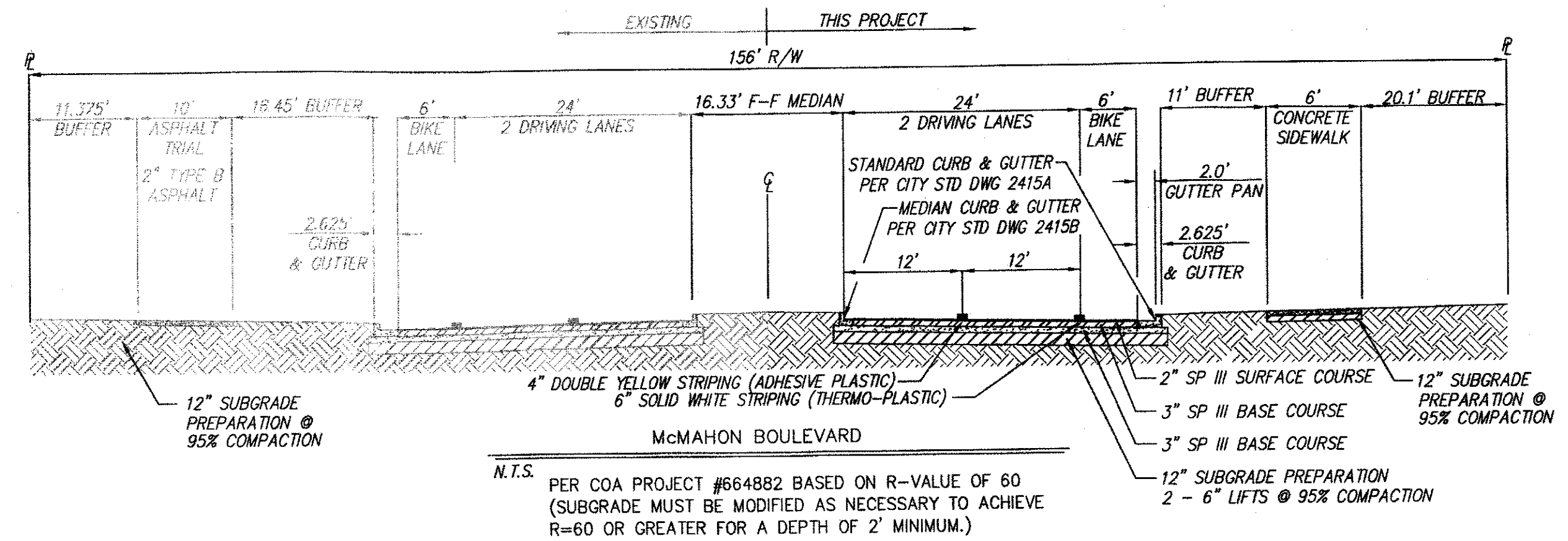
CERTIFICATE OF SUBSTANTIAL COMPLIANCE

 MARK GOODWIN & ASSOCIATES, P.A.
CONSULTING ENGINEERS
P.O. BOX 90606
ALBUQUERQUE, NEW MEXICO 87199
OFFICE (505) 828-2200 FAX (505) 797-9539

	<h2 style="margin: 0;">CITY OF ALBUQUERQUE</h2> <h2 style="margin: 0;">PUBLIC WORKS DEPARTMENT</h2>														
TITLE:	<h3 style="margin: 0;">ANASAZI RIDGE UNIT 3</h3> <h3 style="margin: 0;">GRADING AND DRAINAGE PLAN</h3>														
CITY ENGINEER APPROVAL	LAST DESIGN UPDATE	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="text-align: center;">MO./DAY/YR.</th> </tr> <tr><td> </td></tr> <tr><td> </td></tr> <tr><td> </td></tr> <tr><td> </td></tr> <tr><td> </td></tr> </table>	MO./DAY/YR.						<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="text-align: center;">MO./DAY/YR.</th> </tr> <tr><td> </td></tr> <tr><td> </td></tr> <tr><td> </td></tr> <tr><td> </td></tr> <tr><td> </td></tr> </table>	MO./DAY/YR.					
MO./DAY/YR.															
MO./DAY/YR.															
CITY PROJECT NO.	ZONE MAP NO. <h2 style="margin: 0;">A-10-Z</h2>	SHEET <h2 style="margin: 0;">3.1</h2>	OF												



TEMPORARY SWALE OUTFALL TO CALABACILLAS ARROYO
SCALE: 1"=40'



SPILLWAY & CONCRETE CHANNEL DETAIL - TRACT A
SCALE: 1"=5'
(CHANNEL CONSTRUCTION AT DRC PER
C.O.A. STD. DWG #2260)

AS BUILT INFORMATION		BENCH MARKS		SURVEY INFORMATION		ENGINEER'S SEAL	
CONTRACTOR	DATE	AGRS Aluminum Cap stamped "2-A10 2003"	DATE	NO.	BY		DESIGNED BY DLH DATE 01/15 DRAWN BY DLH DATE 01/15 CHECKED BY DMG DATE 01/15
INSPECTOR	DATE	From the intersection of Irving Boulevard NW and Koyote Street NW, go north on Koyote Street NW 0.20 miles to the station on the left.	DATE	NO.	BY		
FIELD	DATE	It is 339 feet south of the centerline of Burgos Avenue NW & 2.8 feet west of the west back of curb.	DATE	NO.	BY		
VERIFICATION BY	DATE	Geographic Position (in feet) NAD83	DATE	NO.	BY		
MICRO-FILM INFORMATION		RECORDED BY		N.M. State Plane Coordinates (Central Zone)			
				N = 1530345.636, E = 1499909.436			
				Elevation (in feet) NAVD83 = 5362.970			

CERTIFICATE OF SUBSTANTIAL COMPLIANCE	
CITY OF ALBUQUERQUE PUBLIC WORKS DEPARTMENT	
TITLE: ANASAZI RIDGE UNIT 3 GRADING AND DRAINAGE PLAN	
DESIGN REVIEW COMMITTEE	CITY ENGINEER APPROVAL
LAST DESIGN UPDATE	MO./DAY/YR.
CITY PROJECT NO.	ZONE MAP NO.
	A-10-2
SHEET	OF
	3.2