

Appendix I

Detention Pond Data

Existing Detention Ponds

1. **Black Dam** – Source: As-built (1-23-2009) Construction Plans for Regional Water Quality Structure at Black Arroyo Dam, Albuquerque New Mexico. Prepared for AMAFCA by Wilson & Company, 3-10-2008.
2. **Cabazon Subdivision – Tract 17 Detention Pond** - Source: AHYMO_97 Model Input File for - Cabazon Communities Phase I Drainage Management Plan (Unit 16) Wilson & Company, Feb. 2004.
3. **Gateway Pond** - Source: Drainage Analysis Report. Prepared for SSCAFCA by Bohannon-Huston. November 4, 2010.
4. **Sugar Ridge Subdivision Detention Pond** - Source: Based on an as-built topographic survey prepared by Smith Engineering Company and documented in a report titled – Letter of Map Revision (LOMR) for Sugar Channel, Rio Rancho, NM. Prepared for City of Rio Rancho, prepared by Smith Engineering Company December 2009.
5. **Wallen Park Subdivision Detention Pond** – Source: Based on As-Built Plans (2-26-2008). Wallen Park Subdivision. Prepared for Wallen Builders, prepared by Community Sciences Corporation 5-4-2007. Also see Detention Pond Figure 3 prepared by Smith Engineering to assist in the detention pond elevation-area-discharge data preparation.
6. **Sunset Pond** – Source: Based on As-Built Plans (Feb. 2009). Prepared for SSCAFCA, Prepare by ASCG Inc. January 2008.
7. **Wexford Pond** – Source: Obtained from AHYMO from Black Arroyo watershed Management Plan. Prepared for SSCAFCA, prepared by ASCG. Final August 2002.
8. **Stone Bridge Detention Pond (Bernalillo County)** – Source: Developed by Smith Engineering Company based on 2010 Lidar contour mapping along with field observations and measurements.
9. **19th Ave. Retention Pond.** Source: Developed by Smith Engineering Company. Based on 2010 Lidar Contour mapping along with field observations.

Proposed or Possible Detention Ponds

1. **Sugar Pond** – Source : Proposed Construction Plans – Prepared for SSCAFCA, prepared by WH Pacific, June 2011.
2. **Lisbon Dam** – Source : Conceptual Design by Smith Engineering Company, July 2013
3. **19th Ave. Dam (West Branch at west side of Unser Blvd.)** – Source : Conceptual Design by Smith Engineering Company, July 2013

HEC-HMS Output for: Existing Conditions Detention Pond Routings

HEC-HMS Output for: DEVEX Conditions Detention Pond Routings

HEC-HMS Output for: Ultimate Conditions Detention Pond Routings

Existing Detention Ponds

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2. **Cabezon Subdivision – Tract 17 Detention Pond** - Source: AHYMO_97 Model Input File for - Cabezon Communities Phase I Drainage Management Plan (Unit 16) Wilson & Company, Feb. 2004.
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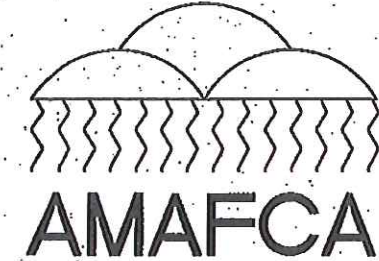


ALBUQUERQUE METROPOLITAN ARROYO FLOOD CONTROL AUTHORITY CONSTRUCTION PLANS FOR



INDEX

REGIONAL WATER QUALITY STRUCTURE AT BLACK ARROYO DAM ALBUQUERQUE, NEW MEXICO



SHEET NO.

DESCRIPTION

- 1
- 2
- 3
- 4
- 5
- 6
- 7
- 8
- 9
- 10
- 11
- 12
- 13
- 14

TITLE SHEET
VICINITY MAP
HYDROLOGY/HYDRAULICS
WATER QUALITY STRUCTURE GRADING PLAN
WEST BRANCH ARROYO DROP STRUCTURE PLAN & PROFILE
EAST BRANCH CHANNEL PLAN & PROFILE
WATER QUALITY STRUCTURE DETAILS
LOW FLOW IN-TAKE STRUCTURE
SITE DETAILS
SITE DETAILS
TESCM EROSION & SEDIMENT CONTROL MEASURES
TESCM SILT FENCE INSTALLATION AND CHECK DAMS
TESCM PIPE SLOPE DRAIN & SEDIMENT TRAPS
DROP INLET & CULVERT PROTECTION

BLACK ARROYO DAM PROPERTIES	
MAXIMUM GRADE ABOVE EXISTING GRADE AT CENTERLINE	22.5 FT
LENGTH	3,273 FT
MAXIMUM WIDTH AT BASE	200 FT
CREST WIDTH	15 FT
SLOPE UPSTREAM FACE	3:1 FT/FT
SLOPE DOWNSTREAM FACE	2.5:1 FT/FT
ELEVATION OF THE DAM CREST (TOD)	5175.0 FT
ELEVATION OF THE EMERGENCY SPILLWAY CREST	5165.75 FT
WATER SURFACE ELEVATION 1/2 PMP, 6-HOUR LOCAL EVENT	5173.25 FT
WATER SURFACE ELEVATION 100-YEAR 24-HOUR EVENT	5160.99 FT
ELEVATION OF THE OUTLET CONDUIT UPSTREAM	5148.00 FT
ELEVATION OF THE OUTLET CONDUIT DOWNSTREAM	5144.08 FT
OUTLET CONDUIT SIZE AND TYPE	2 - 8.5' x 8.5' CBCs
OUTLET CONDUIT CAPACITY AT TOD ELEVATION 5175.0'	3865 CFS
DRAINAGE AREA	6.347 ACRE
HAZARD CLASSIFICATION	HIGH
1 PMP 6 HOUR LOCAL STORM DESIGN RAINFALL	7.12 IN.
FREEBOARD	9.25 FT
LOCATION OF OUTLET WORKS INTAKE STRUCTURE (@ C. OF UPSTREAM HEADWALL)	N 1534254.33 E 1612979.54

STATE OF NEW MEXICO)
COUNTY OF BERNALILLO) SS.
I, JOHN P. KELLY, P.E., BEING FIRST DULY SWORN, UPON MY OATH, STATE THAT I AM THE EXECUTIVE ENGINEER FOR THE ALBUQUERQUE METROPOLITAN ARROYO FLOOD CONTROL AUTHORITY, ALBUQUERQUE, NM; A GOVERNMENTAL ENTITY ORGANIZED UNDER THE LAWS OF THE STATE OF NEW MEXICO. THAT THE ACCOMPANYING CONSTRUCTION DRAWINGS CONSISTING OF 14 SHEETS FOR THE REGIONAL WATER QUALITY STRUCTURE AT BLACK ARROYO DETENTION DAM WERE MADE UNDER THE AUTHORITY OF THE BOARD OF DIRECTORS OF SAID ENTITY AND THAT, IN THEIR BEHALF, I HAVE READ AND EXAMINED THE STATEMENTS AND REPRESENTATIONS AND ALL THAT SHOWN HEREIN IS DONE WITH THEIR FREE CONSENT AND IN ACCORDANCE WITH THEIR WISHES AND STATE THAT THE SAME ARE TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.
John P. Kelly DATE 2-29-08
JOHN P. KELLY, P.E. EXECUTIVE ENGINEER
SUBSCRIBED AND SWORN TO BEFORE ME THIS 29th DAY OF Feb., 2008
Amelia L. Woodruff
NOTARY PUBLIC
MY COMMISSION EXPIRES 9-22-08

AS-BUILT
SURVEYOR'S CERTIFICATION

I, Dan B. Holmes, New Mexico Land Surveyor No. 6245, do hereby certify that the as-built elevations shown on these plans were surveyed under my supervision and that they are true and correct to the best of my knowledge and belief.

Dan B. Holmes
Dan B. Holmes
02-11-09
Date



State of New Mexico)
County of Bernalillo) SS.

I, Daniel S. Aguirre, PE, CFM, state that I am a qualified professional engineer licensed in the state of New Mexico, that I have inspected the REGIONAL WATER QUALITY STRUCTURE AT THE BLACK ARROYO DAM and appurtenant structures and find them to be in accordance with the recent construction drawings and specifications and are now in satisfactory condition for acceptance.

Daniel S. Aguirre
Daniel S. Aguirre, PE, CFM

Date submitted 2/9/09



STATE OF NEW MEXICO)
COUNTY OF BERNALILLO) SS.

I, DANIEL S. AGUIRRE, P.E., CFM HEREBY CERTIFY THAT I AM A PROFESSIONAL ENGINEER LICENSED IN THE STATE OF NEW MEXICO, QUALIFIED IN CIVIL ENGINEERING; THAT THE ACCOMPANYING DESIGN REPORT WAS PREPARED BY ME OR UNDER MY SUPERVISION; THAT THE ACCOMPANYING CONSTRUCTION DRAWINGS CONSISTING OF 14 SHEETS WAS PREPARED BY ME OR UNDER MY SUPERVISION; THAT THE ACCOMPANYING CONSTRUCTION DRAWINGS CONSISTING OF 14 SHEETS IS IN COMPLIANCE WITH THE DAM DESIGN, CONSTRUCTION AND DAM SAFETY REGULATIONS (19.25.12 NMAC) AND THAT THE SAME ARE TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

Daniel S. Aguirre LICENSE 11955,
DANIEL S. AGUIRRE, P.E., CFM
DATE SUBMITTED 3/10/09

STATE OF NEW MEXICO)
COUNTY OF SANTA FE) SS.

HEREBY CERTIFY THAT THE ACCOMPANYING CONSTRUCTION DRAWINGS I FOR THE REGIONAL WATER QUALITY STRUCTURE AT THE BLACK ARROYO DETENTION DAM AND APPURTENANT STRUCTURES HAS BEEN DULY EXAMINED BY ME AND ACCEPTED FOR FILING ON THE _____ DAY OF _____, 200____.

JOHN D'ANTONIO, P.E.
NEW MEXICO STATE ENGINEER

APPROVED FOR CONSTRUCTION

DEVELOPER CURB-NORTH LLC.
CITY OF RIO RANCHO DEPARTMENT OF PUBLIC INFRASTRUCTURE
AMAFCA John P. Kelly EXECUTIVE ENGINEER
SSCAFC Robert Johnson EXECUTIVE DIRECTOR

ALBUQUERQUE METROPOLITAN
ARROYO FLOOD CONTROL
AUTHORITY

WILSON & COMPANY
2600 THE AMERICAN ROAD, SE
SUITE 100
RIO RANCHO, NEW MEXICO
87124
P: (505) 348-4000
F: (505) 348-4072
WWW.WILSONCO.COM

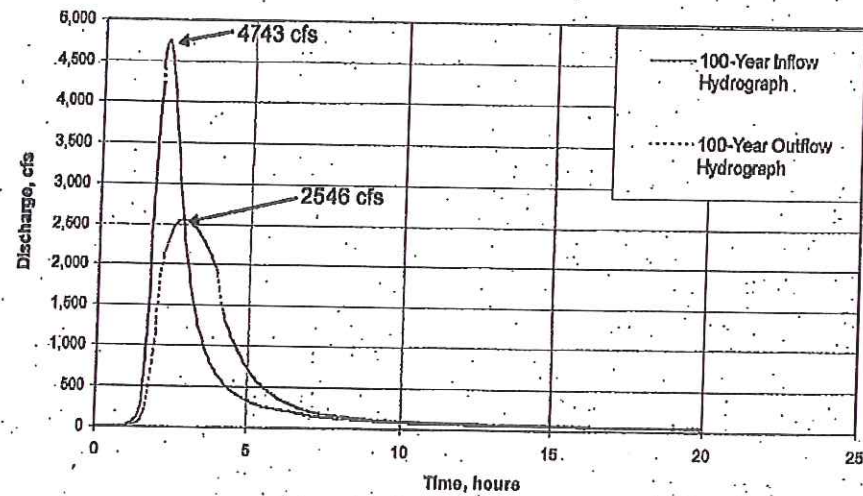
REGIONAL WATER
STRUCTURE AT BI

TITLE SHEET

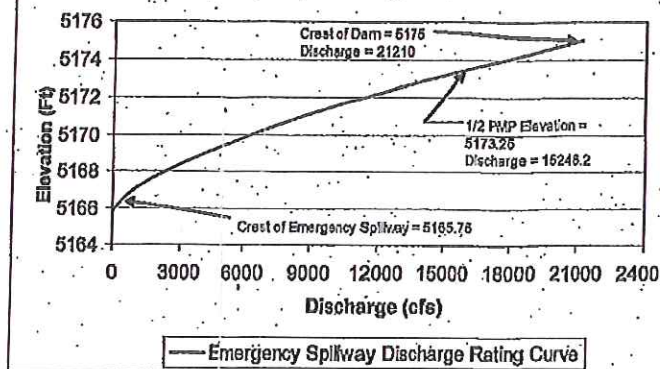
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DRAWN	HLC	PROJECT NO.	
CHECK	MJA		N/A



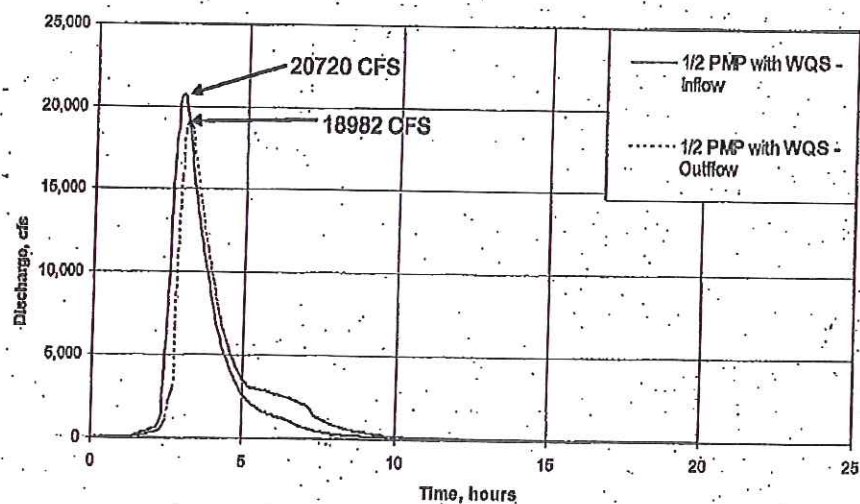
Inflow and Outflow Hydrographs for the Combined Black Arroyo Dam and Water Quality Structure, 100-year 24-hour Storm Event



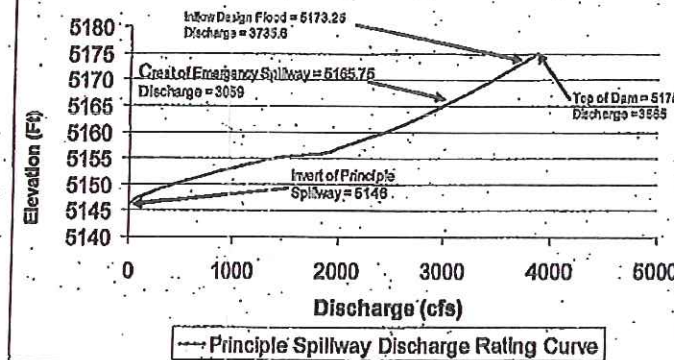
Emergency Spillway Discharge Rating Curve



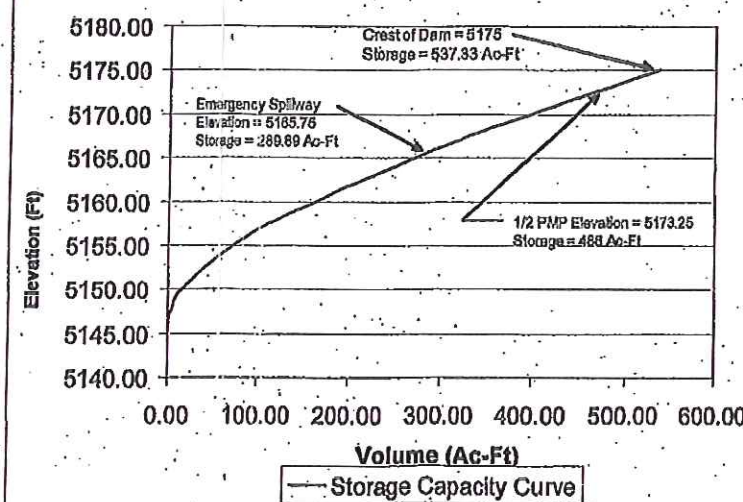
Inflow and Outflow Hydrographs for the Combined Black Arroyo Dam and Water Quality Structure, 1/2 PMP, 6-Hour Local Storm Event



Principle Spillway Discharge Rating Curve



Storage Capacity Curve



BLACK ARROYO DAM PROPERTIES

MAXIMUM GRADE ABOVE EXISTING GRADE AT CENTERLINE
LENGTH
MAXIMUM WIDTH AT BASE
CREST WIDTH
SLOPE UPSTREAM FACE
SLOPE DOWNSTREAM FACE
ELEVATION OF THE DAM CREST (TOD)
ELEVATION OF THE EMERGENCY SPILLWAY CREST
WATER SURFACE ELEVATION 1/2 PMP, 6-HOUR LOCAL EVENT
WATER SURFACE ELEVATION 100-YEAR 24-HOUR EVENT
ELEVATION OF THE OUTLET CONDUIT UPSTREAM
ELEVATION OF THE OUTLET CONDUIT DOWNSTREAM
OUTLET CONDUIT SIZE AND TYPE
OUTLET CONDUIT CAPACITY AT TOD ELEVATION 5175.0'
DRAINAGE AREA
HAZARD CLASSIFICATION
1/2 PMP 6 HOUR LOCAL STORM DESIGN RAINFALL
FREEBOARD
LOCATION OF OUTLET WORKS INTAKE STRUCTURE (at center of upstream headwall)

Proposed Black Arroyo Dam Rating Curve Information With WQS

Elevation (feet)	Surface Area (Acres)	Incremental Volume (Ac-Ft)	Storage (Ac-Ft)	Discharge** (CFS)	
5146.00	0.00	0.00	0.00	0.0	Principle Spillway
5147.00	3.00	1.50	1.50	51.9	
5148.00	3.63	3.32	4.82	140.7	
5149.00	4.25	3.94	8.76	289.4	
5150.00	9.22	6.74	15.49	414.8	
5151.00	10.10	9.68	25.15	579.7	
5152.00	11.23	10.67	35.82	762.0	
5153.00	12.48	11.88	47.67	960.3	
5154.00	13.57	13.03	60.70	1173.2	
5155.00	14.40	13.99	74.68	1400.0	
5156.00	14.48	14.43	89.11	1883.0	
5157.00	15.28/18.9*	14.87	103.98	2018.5	
5158.00	19.39	19.15	123.13	2162.9	
5159.00	19.68	19.64	142.78	2289.2	
5160.00	20.44	20.16	162.92	2428.0	
5161.00	20.97	20.71	183.63	2547.4	
5162.00	21.52	21.25	204.87	2663.2	
5163.00	22.12	21.82	226.69	2774.2	
5164.00	22.76	22.44	249.13	2881.0	
5165.00	23.31	23.04	272.17	2983.0	
5165.76	23.80	23.49	289.89	3059.8	
5166.00	23.96	23.64	295.80	3169.8	
5167.00	24.53	24.25	320.05	4150.7	
5168.00	25.15	24.84	344.89	5644.0	
5169.00	25.84	25.50	370.38	7523.3	
5170.00	26.63	26.19	396.57	9738.9	
5171.00	27.18	26.88	423.42	12255.3	
5172.00	27.88	27.62	450.94	15059.7	
5173.00	28.49	28.18	479.12	18136.9	
5173.25			488.40	18981.8	
5174.00	29.09	28.79	507.91	21477.6	
5175.00	29.76	29.43	537.33	25074.8	
					Design Elevation
					Top of Dam

*There are 2 areas shown at Elevation 5157 for the calculations of the Volume. The 15.28 surface area is used to calculate the incremental volume at elevation 5157. The 18.9 value is the surface area used to calculate the incremental volume at elevation 5168.

**Discharge includes total of Principle and Emergency Spillways

SOUTH 16'-28" S x 20" R CMP			NORTH 16'-28" S x 20" R CMP		
CMP	INVERT WEST	INVERT EAST	CMP	INVERT WEST	INVERT EAST
1	5157.08	5160.00	1	5158.12	5161.21
2	5157.81	5160.00	2	5157.89	5161.18
3	5157.52	5160.08	3	5157.86	5161.39
4	5157.72	5160.99	4	5159.07	5161.28
5	5157.89	5160.08	5	5159.01	5161.20
6	5157.82	5160.87	6	5157.82	5161.17
7	5157.83	5160.84	7	5157.84	5161.18
8	5157.84	5160.86	8	5157.84	5161.12
9	5157.77	5160.88	9	5157.80	5161.13
10	5157.77	5160.81	10	5157.81	5161.17
11	5157.72	5160.87	11	5158.01	5161.11
12	5157.78	5160.91	12	5157.84	5161.10
13	5157.71	5160.88	13	5157.92	5161.14
14	5157.78	5160.89	14	5157.92	5161.15
15	5157.74	5160.97	15	5157.90	5161.13
16	5157.78	5160.99	16	5157.88	5161.11

SOUTH & NORTH CMP's BEGINNING WITH #1 @ SOUTH END OF EACH BATTERY FOR CMP'S & ENDING WITH #16. EQUAL INVERTS WEST & EAST FOR EACH CMP.

ALBUQUERQUE METROPOLITAN ARROYO FLOOD CONTROL AUTHORITY

REGIONAL WATER QUALITY STRUCTURE AT BLACK DAM

HYDROLOGY/HYD

REVISIONS

NO.	DATE	REMARKS

DESIGN: MJJ WCEA NO. X421B
 DRAWN: HLG PROJECT NO.
 CHECK: MJJ N/A

WILSON & COMPANY
 2600 THE AMERICAN ROAD SE
 SUITE 100
 RIO RANCHO, NEW MEXICO
 87124
 (505) 939-8021

RECORD DRAWING
 DATE: 1-23-2009

CABEZON TRACT 17 DETENTION POND
ELEV. STORAGE DISCHARGE DATA

(3 PAGES)

FROM

CABEZON COMMUNITIES PHASE I
DRAINAGE MANAGEMENT PLAN (Unit 16)
Wilson & Company, Feb. 2004

CD in report with AHYMO models

Copy of model beginning text and RESERVOIR ROUTING DATA

```
START                0.0 HRS  PUNCH CODE=0  PRINT LINES=-1
* * * * *
* * * * *
*S      7/22/04
*S      WILSON & CO.'S CABEZON COMMUNITIES DRAINAGE MASTER PLAN, PHASE 2 OF
*S      DEVELOPMENT: THIS MODEL TAKES BOTH CABEZON PHASE 1 AND 2 INTO THE
*S      MODIFIED BLWMP MODEL DEVELOPED BY ASCG (1/20/04) TO ASSESS
CABEZON'S
*S      IMPACT ON BLACK DAM. IT MODELS DEVELOPED CONDITIONS IN ALL
SUBBASINS;
*S      SEDIMENT BULKING ADJUSTED TO 6% REFLECT THIS; ALSO, MUSKINGHAM
CUNGE
*S      ROUTING (COMMAND: ROUTE MCUNGE) CONSISTENTLY USED
*S      THIS MODEL USES A STEP OF 0.05 HR (3 MIN) SO THAT THE ENTIRE 24 HR
*S      HYDROGRAPH IS CAPTURED AND VOLUMETRIC RUNOFF IS MORE COMPLETELY
*S      ACCOUNTED FOR
*S * * * * *
* * * * *
*S 01/20/2004 ADJUSTMENTS TO THIS MODEL FROM THE BLWMP
*S "DOUBLE" COUNTING OF STREETS IN LAND TREATMENT REMOVED
*S SUB-BASIN 211 ROUTED ADJUSTED TO EXISTING FIELD CONDITIONS (XING
SOUTHERN)
*S NOTHING ELSE HAS BEEN ADJUSTED - USER ACCEPTS THIS MODEL AS IS AND
TAKES THE
*S RESPONSIBILITY FOR CHECKING IT FOR ACCURACY PRIOR TO USE...
*****
*      -----HYDROLOGY MODEL-----
*S * * * FUTURE CONDITIONS MODEL - ALTERNATE B * * * * *
* * * * *
*S * * * 3 DAMS ON THE WEST BRANCH * * * * *
*S * * * UNSER GATEWAY DAM, AND WATER QUALITY DIVERSIONS * * * * *
*S * * * ROUTING WITH MCUNGE METHOD AFTER WATER QUALITY DIVERSIONS ARE *
* * * *
```

```

*S * * * UTILIZED TO ADJUST FOR THE UNSTABLE HYDROGRAPHS WITH A STEEP
SLOPE * * *
*S * * * AFTER MODIFICATION TO REDIRECT THE FIRST FLUSH OF 0.25" RUNOFF
FOR SWQ *
* LH
***** * *
*
* LH FILE MODIFIED BY LH/ASCG TO REFLECT FULL DEVELOPMENT WITHIN THE BLACK
*
* LH ARROYO WATERSHED USING THE SSCAFCA LAND TREATMENTS FOR LOTS AND
*
* LH ZONING DEVELOPED FOR THE MONTOYAS ARROYO STUDY.
*
* LH THIS MODEL IS INTENDED TO PROVIDE A BIG PICTURE STUDY FOR THE BLACK
*
* LH ARROYO AND SHOULD NOT BE USED TO DEVELOP DETAILED SOLUTIONS.
*
* LH THE FEMA RESTUDY MODEL HAS BEEN ADDED TO IVORY AND LISBON CROSSING
DESIGN*
* LH MODEL AND CHANGED TO DEVELOPED CONDITIONS.
*
* LH
*
* LH THE FOLLOWING THINGS WERE CHANGED IN THE MODEL:
*
* LH
*
* LH MODIFIED PRINT LINE COMMAND AND ROUTES CHANGED TO MANNINGS ROUTE FOR
*
* LH ALL WELL DEFINED CHANNELS (ALSO CHANGED IN RESTUDY MODEL PORTION)
*
* LH MODIFIED SLOPE FOR ROUTING THRU BASIN 103 FROM 0.0179 TO 0.0214
FT/FT.
*
* LH SEE RUN CHRONOLOGY FOR OTHER CHANGES IN THE MODEL.
*
*
LH*****
* * *
*
* ORIGINAL AHYMO MODEL DEVELOPED FOR:
* FEMA RE-STUDY
* SANDOVAL COUNTY, NEW MEXICO
*
* RESTUDY AREA: CITY OF RIO RANCHO
* FLOODING SOURCE: BLACK ARROYO
*
*****
* LH ALL SEDIMENT BULKING WAS MODIFIED TO USE THE SEDIMENT BULK COMMAND
AND
* NOT THE DIVIDE HYD COMMANDS IN THE PREVIOUS FEMA RESTUDY MODELS.
* SEE RUNCHRONOLOGY FOR AN EXPLANATION OF THE BULKING FACTORS.
*
*S ROUTE FLOWS THROUGH Pond/Park in Unit 17
*S Pond Based on final design grades with 7 ac-ft of
*S low storage/WQ and then filling remainder of park/field
*S graded at 2%
ROUTE RESERVOIR ID=2 HYD NO=P.Out INFLOW ID=1 CODE=4.2

```

OUTFLOW (CFS)	STORAGE (AF)	ELEV (FT)
0.00	0.00	5263.00
0.06	0.25	5263.50
0.46	0.51	5264.00
1.48	0.83	5264.50
3.31	1.15	5265.00
6.04	1.50	5265.50
9.66	1.85	5266.00
14.01	2.22	5266.50
18.71	2.59	5267.00
23.07	2.99	5267.50
25.83	3.39	5268.00
24.31	3.81	5268.50
235.80	4.23	5269.00
254.70	4.68	5269.50
272.28	5.13	5270.00
288.80	5.60	5270.50
304.42	6.08	5271.00
319.28	6.58	5271.50
333.47	7.09	5272.00
347.09	7.62	5272.50
360.19	8.16	5273.00
372.84	8.72	5273.50
385.06	9.29	5274.00
396.91	10.08	5274.50
408.42	10.87	5275.00
419.61	12.09	5275.50
430.51	13.31	5276.00
441.14	14.84	5276.50
451.53	16.36	5277.00
461.67	18.00	5277.50
471.60	19.63	5278.00
481.33	21.33	5278.50
490.86	23.02	5279.00
500.21	24.72	5279.50
509.39	26.41	5280.00

Principal Spillway / Pond Basin

*TOPOG. SFT
CMP
PRINCIPAL
SPILLWAY PIPE*

Top Of Pond - Emergency Spillway

```

*
PRINT HYD          ID=2  CODE=1
*
*
*S *****DIVIDE HYD TO UNBULK BY 3% *****
DIVIDE HYD          ID=2  %=-97  ID I=2  HYD=P.Out.3
                      ID II=51  HYD=SEDIMENT
*
*
*S  Route unbulked pond outflow at 17 to east end of 15
*S  through a 60" pipe

```

GATEWAY POND DRAINAGE ANALYSIS REPORT

NOVEMBER 4, 2010

Prepared for:

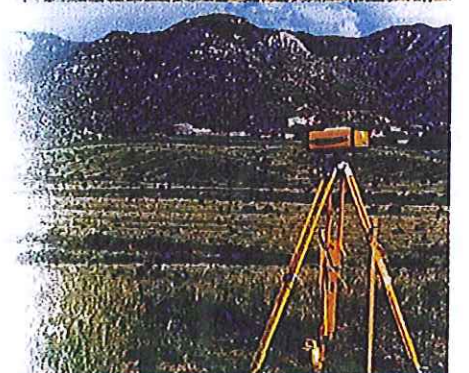
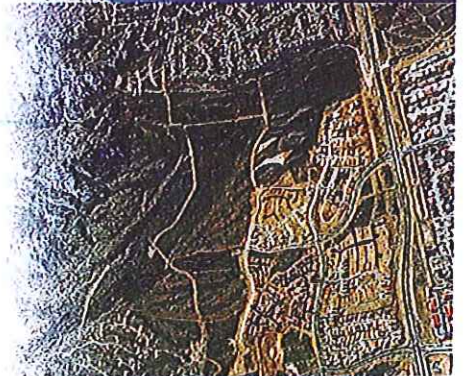
SSCAFCA
1041 Commercial Dr. S.E.
Rio Rancho, NM 87124

Bohannon & Huston INC.

ENGINEERING ▲

SPATIAL DATA ▲

ADVANCED TECHNOLOGIES ▲



**Gateway Dam Elevation-Storage-
Discharge Table**

Elevation (FT)	Storage (AC- FT, see note 1)	Existing Discharge (CFS, see note 2)
5263	0.000	0.000
5264	0.871	58.161
5265	1.976	88.423
5266	3.326	168.753
5267	5.343	244.421
5268	8.507	303.831
5269	11.987	340.404
5270	17.216	371.140
5271	21.619	399.865

Notes:

- 1) DTM created from proposed contours provided by Goodwin, 9/9/10
- 2) 3 Existing 57" x 38" CMP Pipes

TABLE SR 1 CORRECT
ELEVATION - STORAGE-DISCHARGE DATA
SUGAR RIDGE SUBDIVISION DETENTION POND

(Elevations, contours, principal and emergency spillway measurements are based on the "as-built" condition as surveyed by Smith Engineering Company, October 2009)

Contour Elevation	Contour Area	Incremental Volume	Incremental Volume	Cumulative Volume	Principal Spillway Orifice Discharge Curve	Emergency Spillway Discharge	Total Discharge	Comments
Principal Spillway Orifice Diameter (inches)								
Number of Orifices								
(ft)	0				36 1			See Figure For sketch of pond principal and emergency spillways
				(ac-ft)	(cfs)	(cfs)		
				(a) (c)	(b)			
5560	175	0	0.0000	0.0000	0.00	0.0	0.00	The storage volume below the vertical 5 ft. dia. principal spillway crest elevation 5564.42 is dead storage. The 3 ft. dia. CMP horizontal pipe is joined to the 5 ft. dia. vertical pipe. The 3 ft. dia. pipe invert elevation = 5561.13
5561	2633	1404	0.0322	0.0322	0.01	0.0	0.01	
5561.13	2919	361	0.0083	0.0405	0.02	0.0	0.02	
5562	4830	3371	0.0774	0.1179	0.03	0.0	0.03	
5563	6570	5700	0.1309	0.2488	0.04	0.0	0.04	
5564	7958	7264	0.1668	0.4155	0.05	0.0	0.05	
5564.42	8564	3470	0.0797	0.4952	0.06	0.0	0.06	After water overtops the 5 ft. dia. CMP, the 3 ft. dia. CMP outfall pipe joined to 5 ft. CMP will control the discharge.
5565	9401	5210	0.1196	0.6148	7.5	0.0	7.5	
5566	10933	10167	0.2334	0.8482	30.1	0.0	30.1	
5567	12980	11957	0.2745	1.1227	55.9	0.0	55.9	Crest elev. Of emergency spillway is 5567.26
5567.26	13643	3461	0.0795	1.2021	83.0	0.0	83.0	
5568	15529	10794	0.2478	1.4499	87.9	72.6	160.4	
5569	17102	16316	0.3746	1.8244	94.0	261.7	355.7	
5570	18551	17827	0.4092	2.2337	99.8	517.0	616.9	
5571	19977	19264	0.4422	2.6759	105.3	824.5	929.9	
Total Volume (ft³) =				116563				
Total Volume (ac-ft) =				2.6759				

Principal Spillway

Emergency Spillway

Total of Pond

TABLE SR 1

(a) Orifice flows were obtained from the use of Equation 4-10 and Table 4-3 from "Handbook of Hydraulics, Sixth Edition, by Brater and King" 1982."
 $Q = Ca \sqrt{2gh}^{1.5}$ $C=0.591$, $g=32.2 \text{ ft/sec}^2$, $a=\text{area (sq ft)}$ $h=\text{head (ft)}$
 Principal Spillway Elevation is 5561.13

(b) Emergency Spillway flows were computed from the use of equation 5-10 and Table 5-3 from "Handbook of Hydraulics" Sixth Edition, by Brater and King" 1982, and the following data
 $Q = CLH^{1.5}$ $C = \text{discharge coefficient}$, $L = \text{spillway length perp. To flow}$, $H = \text{head (ft)}$

$C = 3$ $L = 38.0000$ Spillway Elev. 5567.26

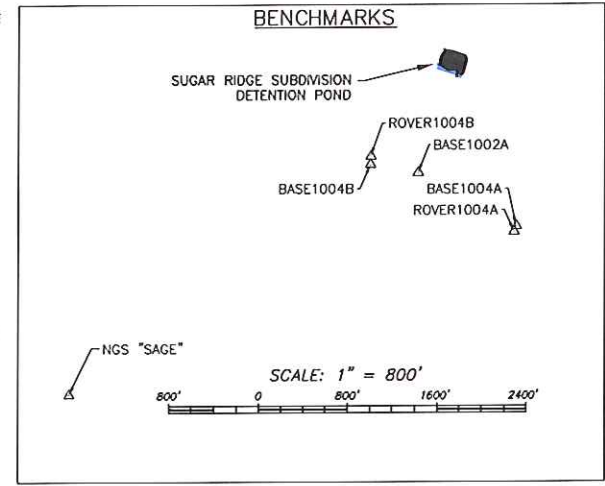
(c) 36-inch CMP principal spillway pipe water areas when the pipe is not full (for orifice equation)

elev.	water depth ft	flow area sq ft	See Note regarding shaded area
5561.13	0.00	0.00	
5562.00	0.87	1.69	
5563.00	1.87	4.64	
5564.00	2.87	6.96	3 ft depth full pipe area = 7.07 sq ft

Note - the principal spillway flows in the shaded area were computed in TABLE SR 2 which computes the discharge as if the 36-inch cmp has head on it from the invert elev.. However, the 36-inch cmp will not take in water until the water depth exceeds the top of the 5 ft. dia. cmp vertical pipe elevation of 5564.42. As water overtops the crest elevation of the 5 ft. dia. cmp, the head on the invert of the 36-inch cmp will increase gradually until the water depth submerges the 5 ft. dia. cmp. Therefore the values from TABLE SR2 were inserted in the shaded area. At elevations greater than the crest of the 5 ft. dia. and greater, assume the full head is available on the 36-inch cmp.

PURPOSE OF THIS POND
AS-BUILT SURVEY WAS TO ASSIST IN
DEVELOPMENT OF THE HYDROLOGIC
MODEL FOR THE TRIBUTARY ARROYO
FOR WHICH THE LOMR APPLIES
BEGINNING DOWNSTREAM OF BALI
ROAD

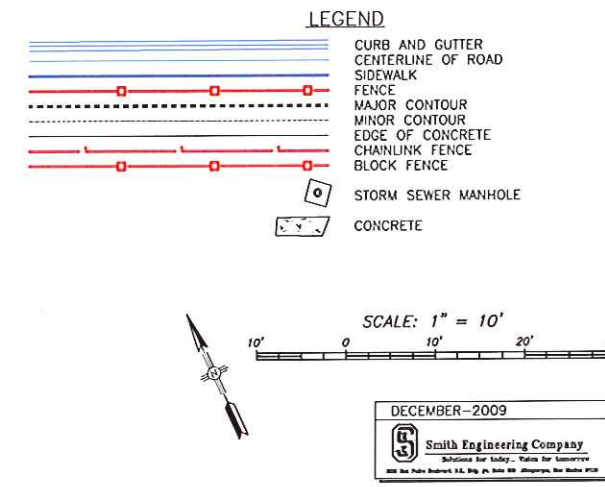
CERTIFICATION
I, W. DANIEL BOVIN, N.M.P.S. NO. 13050, CERTIFY THAT THE TOPOGRAPHIC
MAP WAS DEVELOPED BY ME OR UNDER MY DIRECT SUPERVISION AND IS
CORRECT TO THE BEST OF MY KNOWLEDGE.
W. Daniel Bovin
W. DANIEL BOVIN P.S. NO. 13050
2201 SAN PEDRO DR. NE
ALBUQUERQUE, NM 87110
DATE OF SURVEY: 10/07/2009



BENCHMARK COORDINATE TABLE

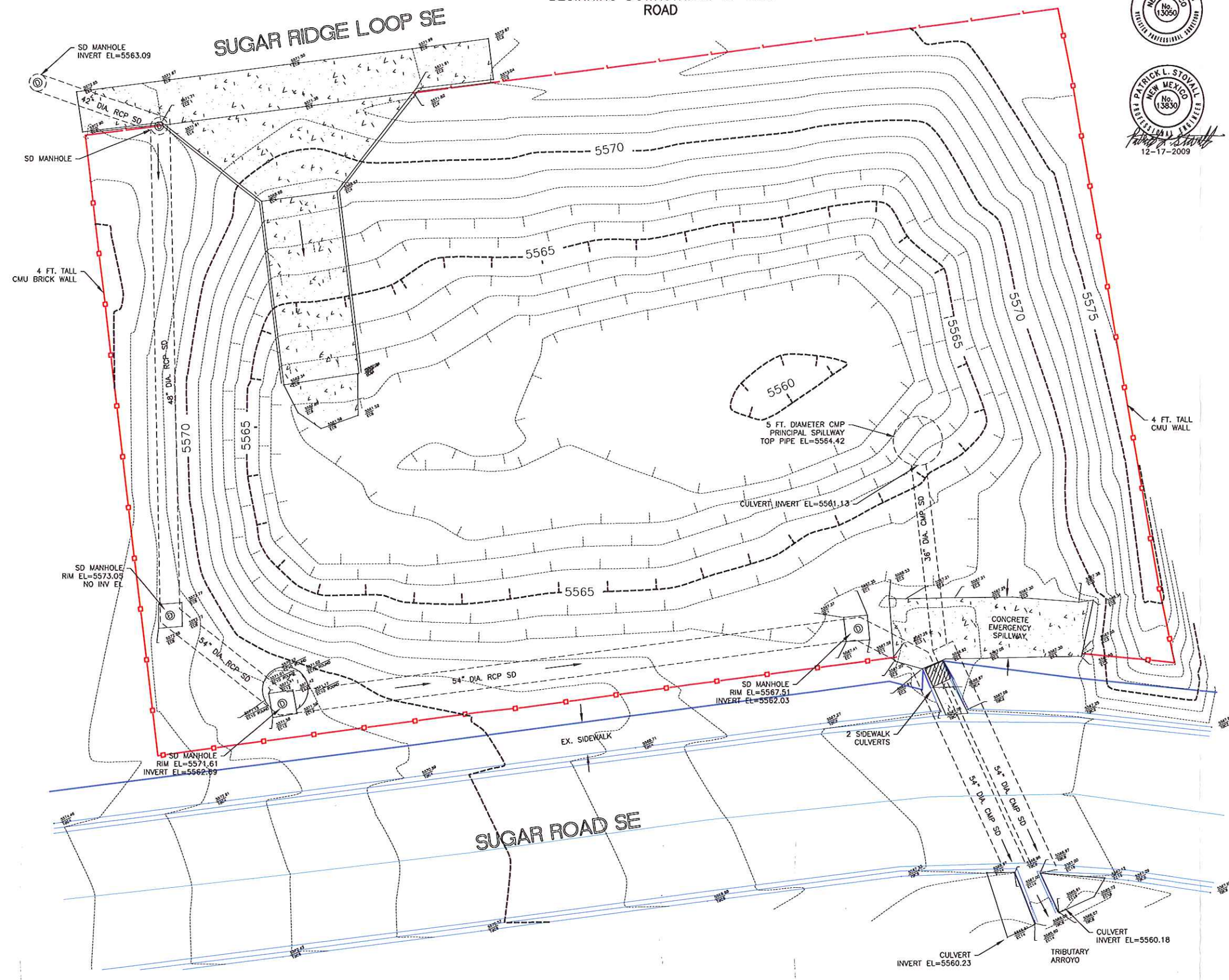
NAME	GROUND N (FT)	GROUND E (FT)	ELEV (FT)
NGS "SAGE"	1546139.353	1499776.710	5676.170
BASE1002A	1548107.370	1502899.131	5559.812
BASE1004B	1548182.352	1502473.570	5571.354
ROVER1004B	1548257.660	1502476.980	5574.178
BASE1004A	1547631.516	1547631.516	5533.270
ROVER1004A	1547583.462	1503758.284	5532.204

COORDINATES SHOWN ARE BASED UPON NEW MEXICO
STATE PLANE COORDINATE SYSTEM, GRID ZONE CENTRAL,
COMBINED SCALE FACTOR = 1.00034146.



6			
5			
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2			
1			
NO.	DESCRIPTION (OR CHANGE NOTICES)	DATE	BY
LETTER OF MAP REVISION FOR SUGAR CHANNEL RIO RANCHO, NEW MEXICO			
CITY OF RIO RANCHO			
SUGAR RIDGE SUBDIVISION DETENTION POND AS BUILT SURVEY BY SMITH ENGINEERING COMPANY			
FIGURE 4 SHEET NO. _____			

NOTES:
ELEVATIONS SHOWN ARE NAVD 88 BASED UPON STATIC G.P.S. OBSERVATION
OF N.G.S. CONTROL POINT "SAGE", ELEVATION = 5676.17'.
THIS IS NOT A BOUNDARY SURVEY.



G:\SEC-PROJECTS\PROJECTS\109119 CORR SUGAR CHAN LOMR REVISION\LOMR APPLICATIONS\MAP POCKET\CD\APP. F2.1 CAD F2.1 DWTURE 4\Figure 4.DWG

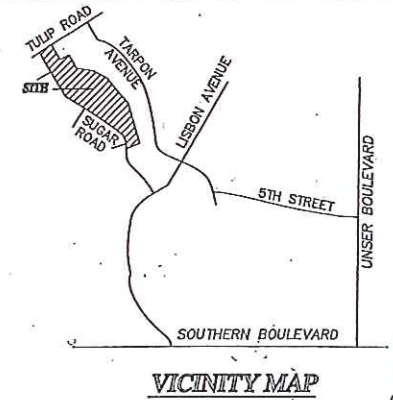
SUGAR RIDGE SUBDIVISION

CITY OF RIO RANCHO, SANDOVAL COUNTY, NEW MEXICO

IMPROVEMENTS FOR
GRADING, DRAINAGE, PAVING, AND UTILITIES

INDEX TO DRAWINGS

SHEET NO.	DESCRIPTION	SHEET NO.	DESCRIPTION
1	COVER SHEET AND INDEX TO DRAWINGS	13	COMPOSITE UTILITY PLAN
2 & 3	PLAT OF GEOMETRY	14	SUGAR RIDGE LOOP (NORTH) UTILITY PLAN AND PROFILE
4	GENERAL NOTES	15	SUGAR RIDGE LOOP (SOUTH) UTILITY PLAN AND PROFILE
5 & 6	GRADING AND EROSION CONTROL PLAN	16	SUGAR RIDGE LOOP CT., CAMEL CT., AND CONFECTION CT. UTILITY PLAN AND PROFILE
7 & 8	GRADING AND DRAINAGE DETAILS	17	WATER AND SANITARY SEWER DETAILS
9	COMPOSITE PAVING PLAN	18 & 19	NM APWA STANDARD DETAILS
10	SUGAR RIDGE LOOP (NORTH) PAVING PLAN AND PROFILE	20	LISBON CHANNEL IMPROVEMENTS (ALT #1)
11	SUGAR RIDGE LOOP (SOUTH) PAVING PLAN AND PROFILE	21	LISBON CHANNEL IMPROVEMENTS (ALT #2)
12	SUGAR RIDGE LOOP CT., CAMEL CT., AND CONFECTION CT. PAVING PLAN AND PROFILE	22	RETAINING WALL DETAILS

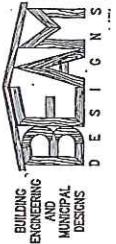


COVER SHEET AND
INDEX TO DRAWINGS

SUGAR RIDGE SUBDIVISION
SANDOVAL COUNTY, NEW MEXICO

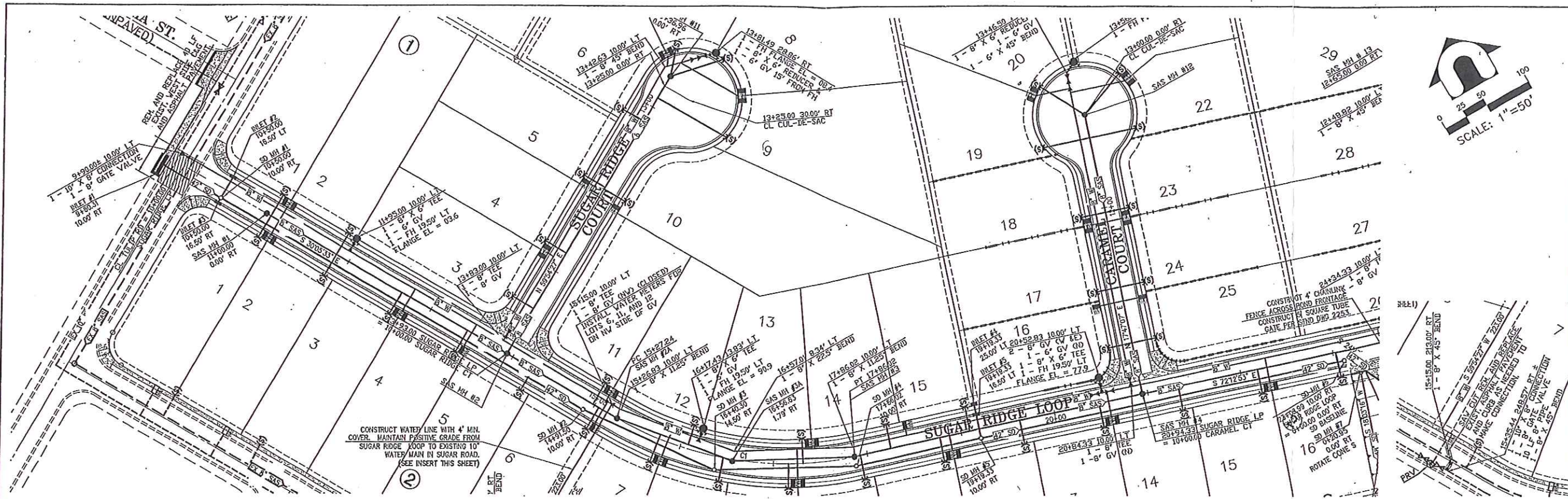
*Sugar Ridge
Hanging File Set*

RES. POLARIS BLVD., SE
RIO RANCHO, NM 87024
PHONE (505) 834-0001
FAX (505) 834-3352
bermudez@beamdesign.com



APPROVED FOR CONSTRUCTION	PROJECT NUMBER: AMRP0002
<i>[Signature]</i> DEPARTMENT OF PUBLIC SAFETY	SHEET NO.
11-13-02 DATE	1
<i>[Signature]</i> CITY ENGINEER	OF 22
12/9/02 DATE	205
<i>[Signature]</i> WATER AND WASTEWATER DEPT.	
11-12-02 DATE	

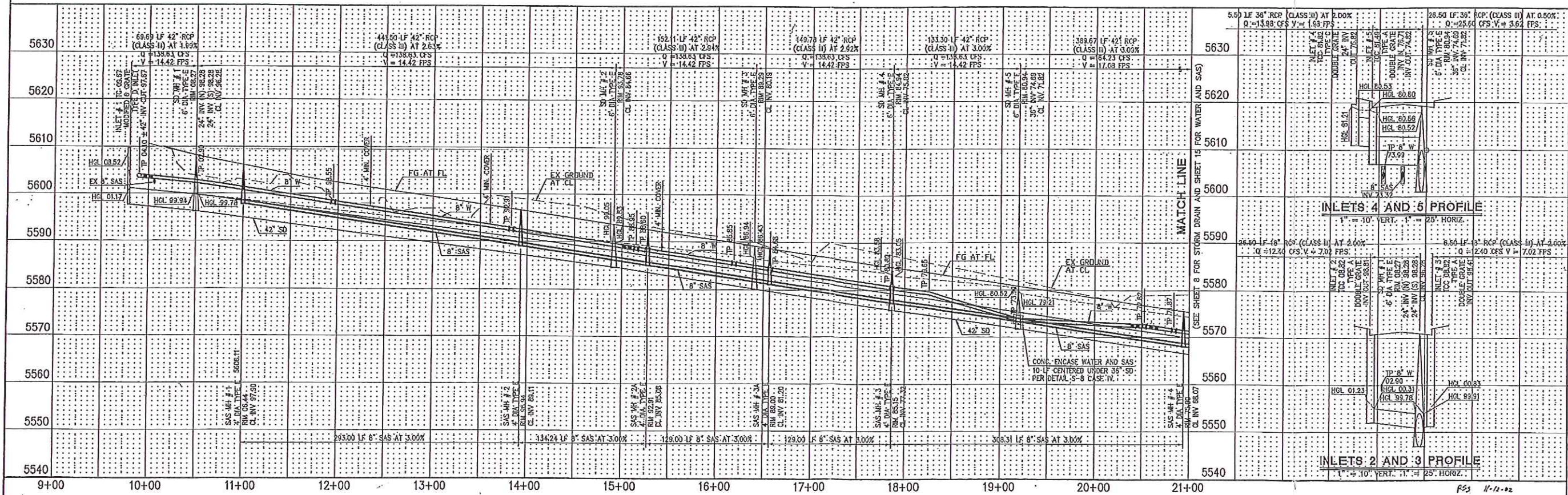
H-File-145



CENTERLINE CURVE DATA			
CURVE ARC (FT)	DELTA (DEG)	RADIUS (FT)	CH. LENGTH (FT)
258.78	42°07'20"	352.00	252.99
S 51°09'13" E			

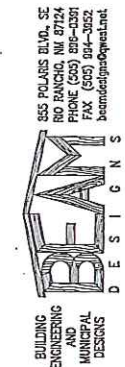
SUGAR RIDGE LOOP

WATER LINE CONNECTION TO SUGAR ROAD



SUGAR RIDGE LOOP
UTILITY PLAN AND PROFILE

SUGAR RIDGE SUBDIVISION
SANDOVAL COUNTY, NEW MEXICO



PROJECT NUMBER:
AMRP0002

SHEET NO.

14

**TABLE WP
ELEVATION - STORAGE-DISCHARGE DATA
WALLEN PARK SUBDIVISION DETENTION POND**

(Elevations, principal and emergency spillway measurements are based on the "as-built" plans (included in this LOMR)

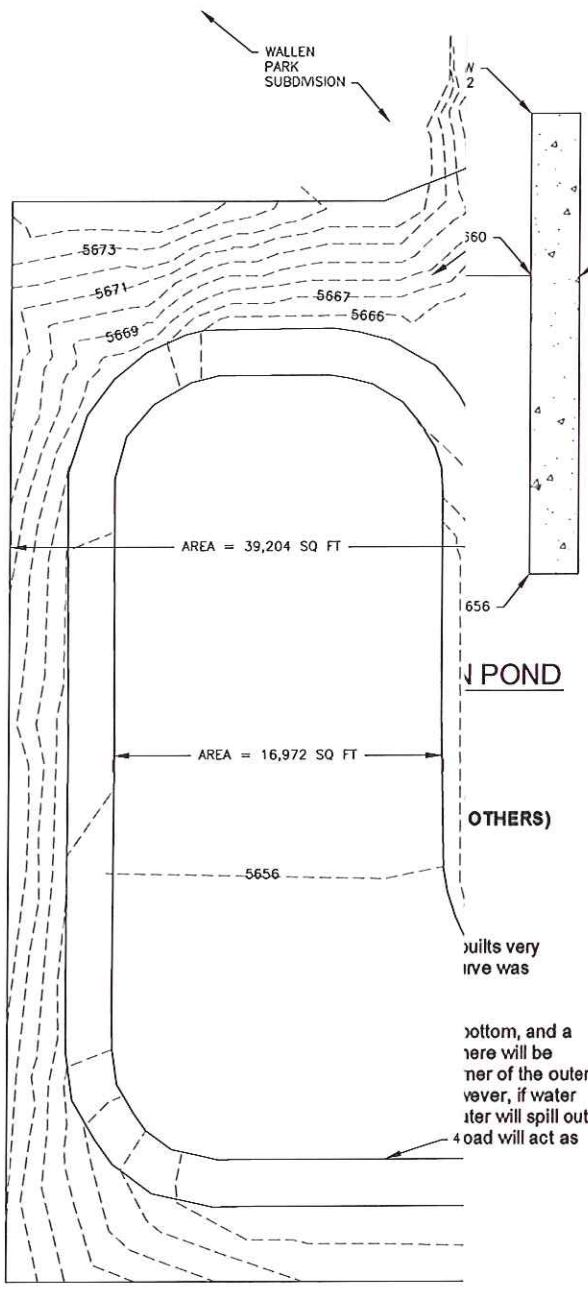
Contour Elevation	Contour Area	Incremental Volume	Incremental Volume	Cumulative Volume	Principal Spillway - Orifice Flow Discharge Curve	Emergency Spillway Discharge	Total Discharge	Comments
Principal Spillway Orifice Diameter (inches)								
Number of Orifices								
(ft)								
	0			0.0000				
5655.88	0	0	0.0000	0.0000	0.0	0.0	0.00	Invert elev. Of 6 - in. dia. PVC principal spillway pipe is 5655.88. Emergency Spillway elevation is 5660
5656	16972	1018	0.0234	0.0234	0.3	0.0	0.3	
5657	16972	16972	0.3896	0.4130	1.0	0.0	1.0	
5658	16972	16972	0.3896	0.8026	1.4	0.0	1.4	
5659	16972	16972	0.3896	1.1922	1.6	0.0	1.6	
5660	16972	16972	0.3896	1.5819	1.9	0.0	1.9	
5661	39204	28088	0.6448	2.2267	2.1	36.0	38.1	Lowest top of outer 6 ft. tall CMU wall at SE corner of pond elev. = 5662
5662	39204	39204	0.9000	3.1267	2.3	101.8	104.1	
5663	39204	39204	0.9000	4.0267	2.5	187.1	189.5	
5664	39204	39204	0.9000	4.9267	2.7	288.0	290.7	
5665	39204	39204	0.9000	5.8267	2.8	402.5	405.3	
Total Volume (ft³) =		253810						
Total Volume (ac-ft) =		5.8267						

(a) Orifice flows were obtained from the use of Equation 4-10 and Table 4-3 from "Handbook of Hydraulics, Sixth Edition, by Brater and King" 1982.

$Q = Ca (2gh)^{1.5}$
 $C=0.591, g=32.2 \text{ ft/sec}^2, a=\text{area (sq ft)} \quad h=\text{head (ft)}$

Principal Spillway Elevation is 5661.13

G:\SEC---PROJECTS\2010\PROJECTS\109119 CORR SUGAR CHAN LOWR REVISION\SEC TOPO SURVEY SUGAR RIDGE POND\WALLENPARKSUP NPOND.DWG



NOTE:
 WATER ELEVATION ABOVE 5660
 WILL SPILL OUT AT GATE OPENING
 BY MAINTENANCE ROAD

2 AREAS
 < 5660 TO 5656 = 16,972 SQ FT
 5660 TO 5662 = 39,204 SQ FT

PLAN VIEW - WALLE

bottom, and a
 here will be
 ner of the outer
 ever, if water
 ster will spill out
 4 road will act as

12 - 2009

Smith Engineering Company
 Solutions For Today... Paths For Tomorrow
 401 San Pedro Boulevard, P.O. Box 26, Suite 200, Broomfield, CO 80020

SEC PROJECT #109119

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NO.	DESCRIPTION	DATE	BY

REVISIONS (OR CHANGE NOTICES)

LETTER OF MAP REVISION
 FOR
 SUGAR CHANNEL
 RIO RANCHO, NEW MEXICO

CITY OF RIO RANCHO

WALLE PARK SUBDIVISION
 DETENTION POND

FIGURE 3

SHEET NO. _____

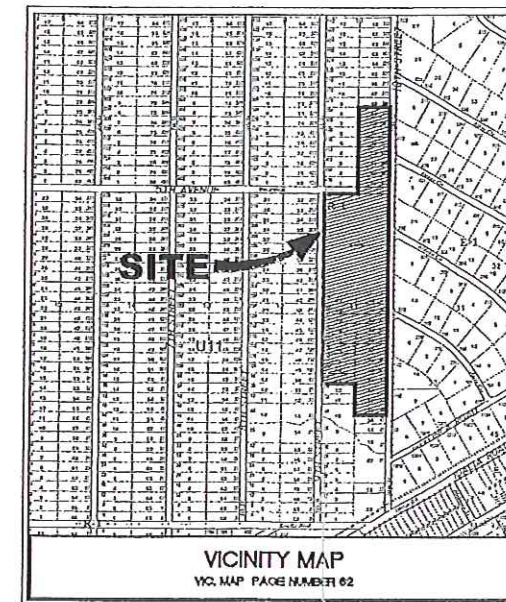
WALLEN PARK SUBDIVISION

CITY OF RIO RANCHO, SANDOVAL COUNTY, NEW MEXICO

IMPROVEMENTS FOR PAVING, DRAINAGE, AND UTILITIES

INDEX TO DRAWINGS

SHEET NO.	DESCRIPTION	UTILITY PLAN & PROFILES
1	COVER	16 OVERALL UTILITY PLAN SOUTH SECTION
2	GENERAL NOTES	17 OVERALL UTILITY PLAN NORTH SECTION
3-5	WALLEN PARK SUBDIVISION PLAT	18 UTILITY DETAILS
6	GRADING AND DRAINAGE PLAN SOUTH SECTION	19 UTILITY DETAILS
7	GRADING AND DRAINAGE PLAN NORTH SECTION	20 LANDING TRAIL UTILITY PLAN AND PROFILE STA. 10+00.00 TO 19+50.00
	<u>PAVING PLAN & PROFILES</u>	21 LANDING TRAIL UTILITY PLAN AND PROFILE STA. 10+00.00 TO 19+50.00
8	OVERALL PAVING PLAN SOUTH SECTION	22 LANDING COURT UTILITY PLAN AND PROFILE
9	OVERALL PAVING PLAN NORTH SECTION	23 GUNPOWDER COURT AND 5TH AVENUE UTILITY PLAN AND PROFILE
10	PAVING DETAILS	24 HUNTER COURT AND CROWN COURT UTILITY PLAN AND PROFILE
11	LANDING TRAIL PAVING PLAN & PROFILE STA. 10+00.00 TO 19+30.00	<u>STORM DRAIN PLAN AND PROFILES</u>
12	LANDING TRAIL PAVING PLAN & PROFILE STA. 19+30.00 TO 30+80.92	25 LANDING TRAIL AND HUNTER COURT STORM SEWER PLAN AND PROFILE
13	LANDING COURT PAVING PLAN AND PROFILE STA. 10+00.00 TO 15+65.02	26 STORM SEWER DETAILS
14	GUN POWDER COURT AND 5TH AVENUE PAVING PLAN AND PROFILE	27 STORM SEWER DETAILS
15	HUNTER COURT AND CROWN COURT PAVING PLAN AND PROFILE	28 POND DETAILS
		29 LANDSCAPE PLAN
		29A LANDSCAPE PLAN



CERTIFICATE OF SUBSTANTIAL COMPLIANCE OF PLANS
 I, Christopher A. Peres of the firm Wilson & Company, a Registered Professional Engineer in the State of New Mexico, NMPE Number 13685, do hereby certify, to the best of my knowledge and belief, that the infrastructure installed as part of this project has been inspected by me or by a qualified person under my direct supervision and has been constructed in accordance with the plans and specifications approved by the City of Rio Rancho Engineers and the original design intent of the approved plans has been met, except as noted by me on the as-built construction drawings. This Certificate is based on the inspections by me or personnel under my direction and survey information provided by Timothy Aldrich NMFS Number 7719.

Christopher A. Peres 5-13-08
 Christopher A. Peres, PE Date

SURVEYOR'S CERTIFICATION
 I, Timothy Aldrich, a duly qualified Registered Professional Land Surveyor under the laws of the State of New Mexico, do hereby certify that the 'as-built' information shown on these drawings was obtained from field construction and 'as-built' surveys performed by me or under my supervision, that the 'as-built' information shown on these drawings was obtained under my supervision, and that this 'as-built' information is true and correct to the best of my knowledge and belief. Aldrich Land Surveys, P.C. is the author of the design concepts, calculations, or methods or content of these drawings.

Timothy Aldrich 5-24-07
 Timothy Aldrich, S.B. No. 7719 Date



DEVELOPER: *Juan Montoya* DATE: *5/8/07*
 WALLEN DEVELOPMENT

CITY OF RIO RANCHO: *Jose Arango* DATE: *5-24-07*
 DEPARTMENT OF PUBLIC INFRASTRUCTURE

CITY OF RIO RANCHO: *P. O. Raza* DATE: *05/11/07*
 DEPARTMENT OF PUBLIC SAFETY TRAFFIC DIVISION

CITY OF RIO RANCHO: *St. Hill* DATE: *05/11/07*
 DEPARTMENT OF PUBLIC SAFETY FIRE

CITY OF RIO RANCHO: *Vanessa W. Conner* DATE: *5/23/07*
 DEPARTMENT OF CULTURAL ENRICHMENT

SSCA/CA: *D. S. Toliver* DATE: *5-27-07*
 EXECUTIVE DIRECTOR

NOTES:
 THIS DOCUMENT, AND THE IDEAS AND DESIGNS INCORPORATED HEREIN, ARE INTENDED FOR USE ON THIS PROJECT AND IS NOT TO BE USED, IN WHOLE OR IN PART, FOR ANY OTHER PROJECT WITHOUT THE WRITTEN AUTHORIZATION OF COMMUNITY SCIENCES CORPORATION. IN THE EVENT OF UNAUTHORIZED USE, THE USER ASSUMES ALL RESPONSIBILITY AND LIABILITY WHICH RESULTS.

THE ENGINEER HAS UNDERTAKEN NO FIELD VERIFICATION OF THE LOCATION, DEPTH, SIZE, OR TYPE OF EXISTING UNDERGROUND UTILITY LINES, MAKES NO REPRESENTATION PERTAINING THERETO AND ASSUMES NO RESPONSIBILITY OR LIABILITY THEREFOR. THE CONTRACTOR SHALL INFORM ITSELF OF THE WORK IN ADVANCE OF AND DURING EXCAVATION WORK. THE CONTRACTOR IS FULLY RESPONSIBLE FOR ANY AND ALL DAMAGE CAUSED BY ITS FAILURE TO LOCATE, IDENTIFY, AND PRESERVE ANY AND ALL EXISTING UTILITIES. THE CONTRACTOR SHALL COMPLY WITH STATE STATUTES, MUNICIPAL AND LOCAL ORDINANCES, RULES AND REGULATIONS PERTAINING TO THE LOCATION OF THESE LINES AND FACILITIES IN PLANNING AND CONDUCTING EXCAVATION, WHETHER BY CALLING OR NOTIFYING THE UTILITIES, COMPLYING WITH NEW MEXICO ONE CALL PROCEDURES, OR OTHERWISE.

CALL BEFORE YOU DIG!

STATEWIDE
1-800-321-ALERT

NM ONE CALL
260-1990

Wallen Builders

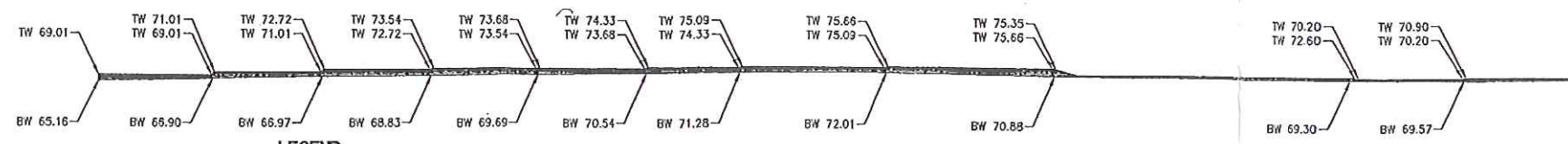
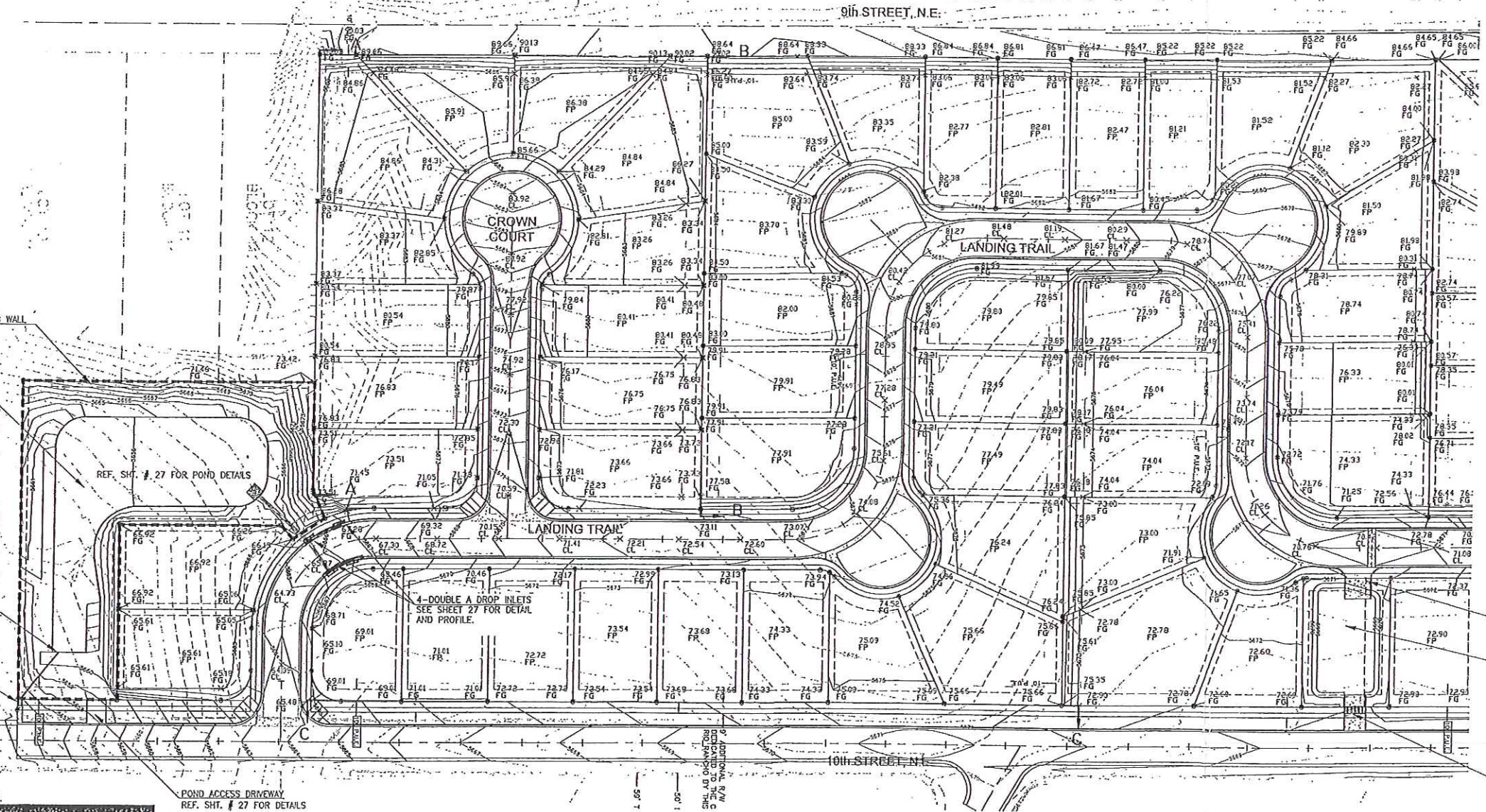
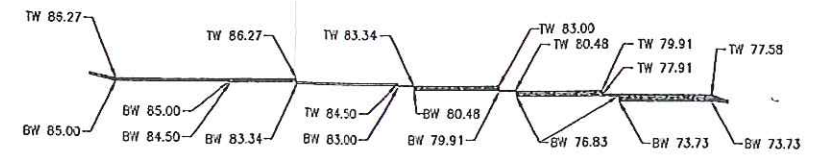
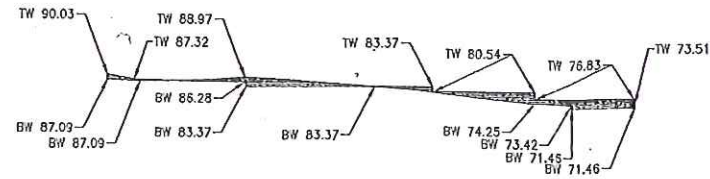
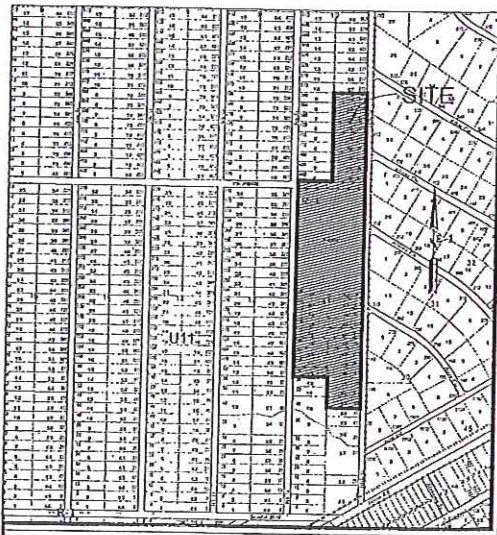
224 B FRONTAGE ROAD
RIO RANCHO, NM 87124 OFFICE: 505-892-2538
FAX: 505-891-8993

WALLEN PARK SUBDIVISION
COVER SHEET AND
INDEX TO DRAWINGS

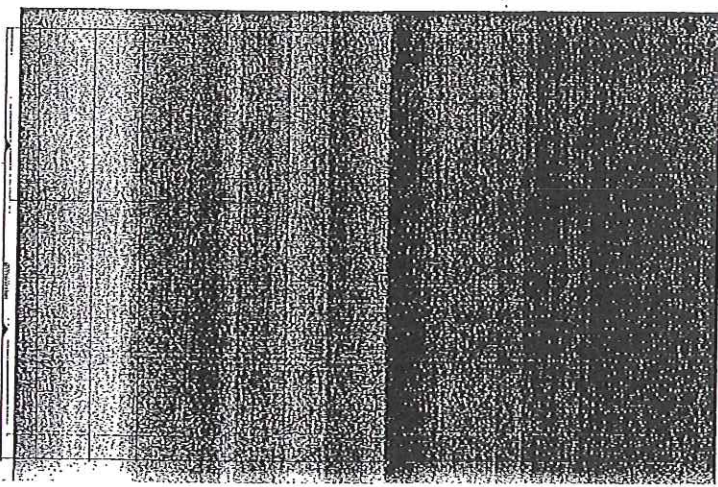
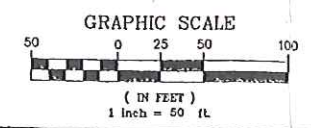
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3/9/06	CORR/ISSUE/COMMENTS	FILE	MW/RLE		
4/1/07	CORR/ISSUE/COMMENTS	FILE			

community sciences corporation
LAND PLANNING ENGINEERING SURVEYING

SHEET 1 OF 29



- LEGEND**
- ✱ 5295.95 PROPOSED SPOT ELEVATION
 - 65.11 EXISTING SPOT ELEVATION (GRID & TC)
 - ▬ PROPOSED CONCRETE VALLEY GUTTER
 - ▬ PROPOSED CURB & GUTTER
 - EXISTING CONTOUR W/ INDEX ELEVATION
 - PROPOSED MANHOLE
 - EXISTING STORM DRAIN
 - SD PROPOSED STORM DRAIN
 - PROPOSED STORM SEWER CATCH BASIN
 - BOUNDARY LINE



WALLEN PARK SUBDIVISION
GRADING AND DRAINAGE

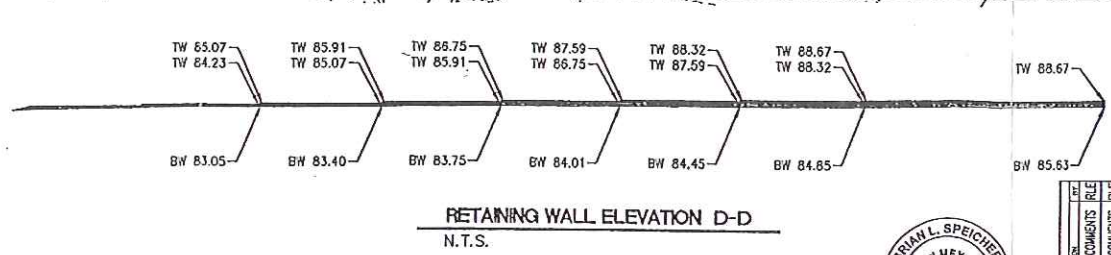
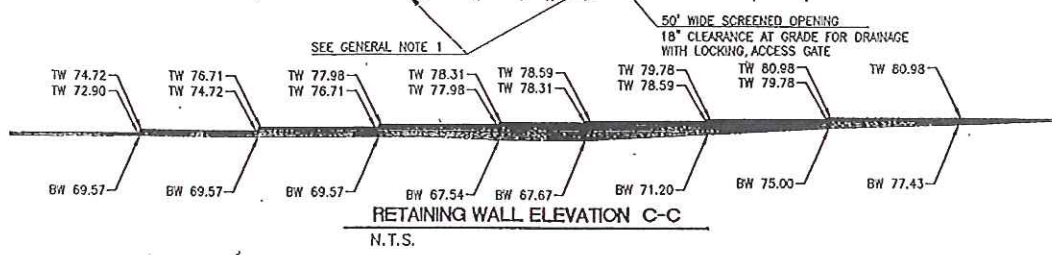
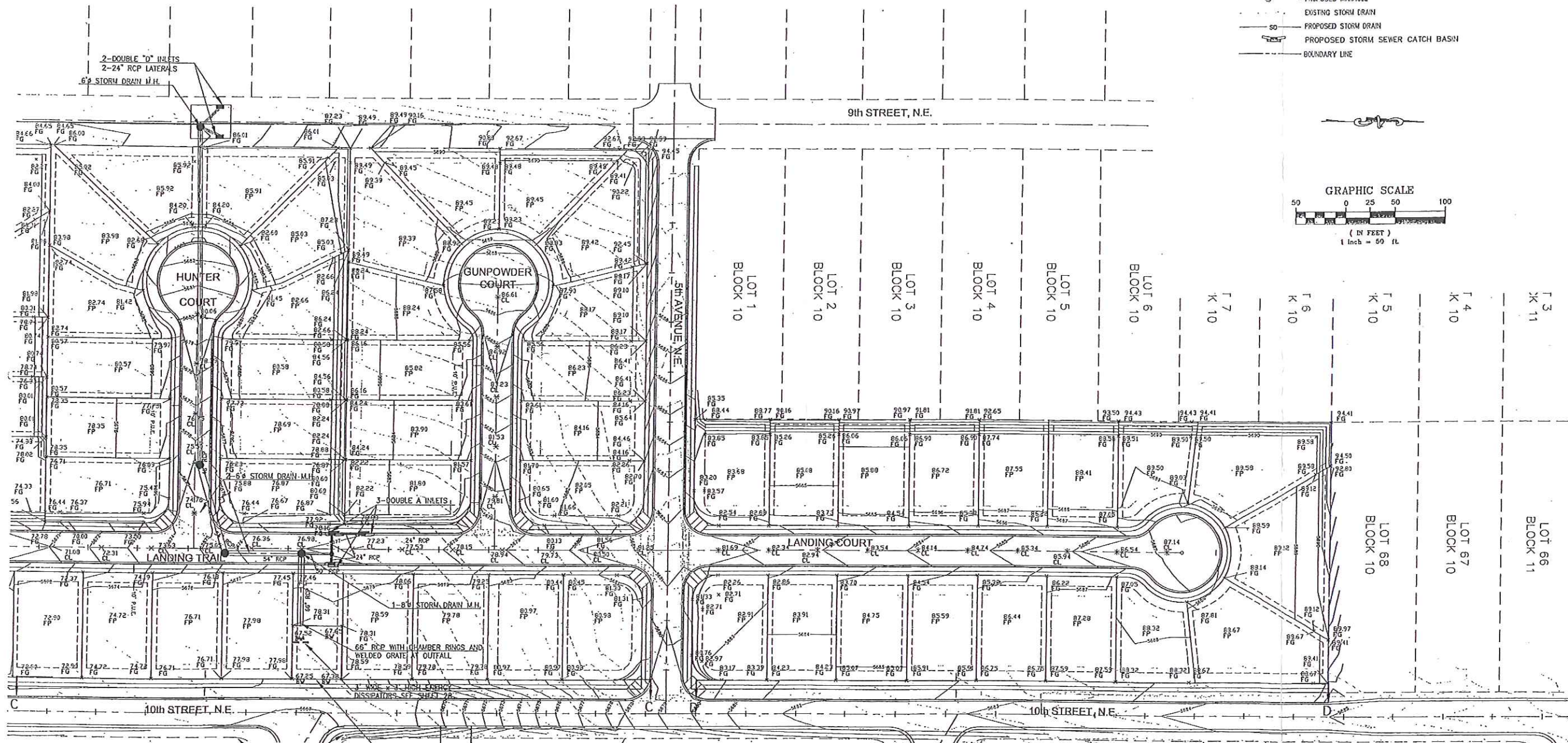
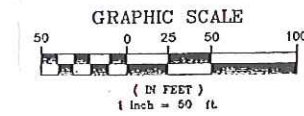
community sciences corporation

DATE: MAY 4, 2007
SCALE: AS SHOWN
DESIGNER: REH
CHECKER: MVH/RLE
JOB NO.: N701-02

SHEET 6 OF 29

LEGEND

- ✕ 5255.98 PROPOSED SPOT ELEVATION
- EXISTING SPOT ELEVATION (GRID & TC)
- ▭ PROPOSED CONCRETE VALLEY GUTTER
- PROPOSED CURB & GUTTER
- EXISTING CONTOUR W/ INDEX ELEVATION
- PROPOSED MANHOLE
- EXISTING STORM DRAIN
- SD PROPOSED STORM DRAIN
- ☐ PROPOSED STORM SEWER CATCH BASIN
- BOUNDARY LINE



GENERAL NOTES

The Contractor and Developer shall coordinate with the property owners to provide a constructed driveway to connect to the finished roadway.

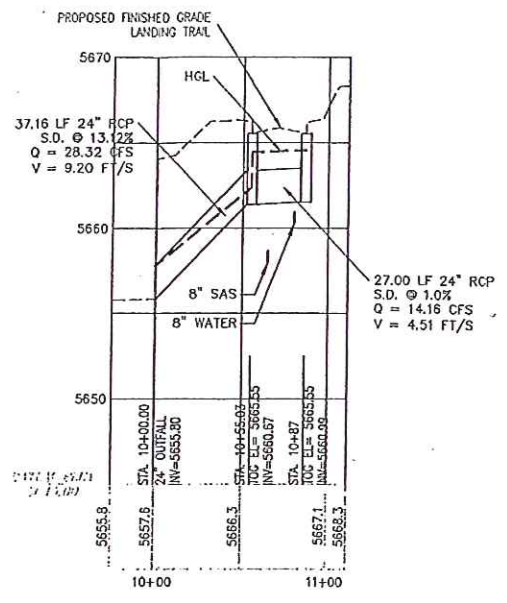
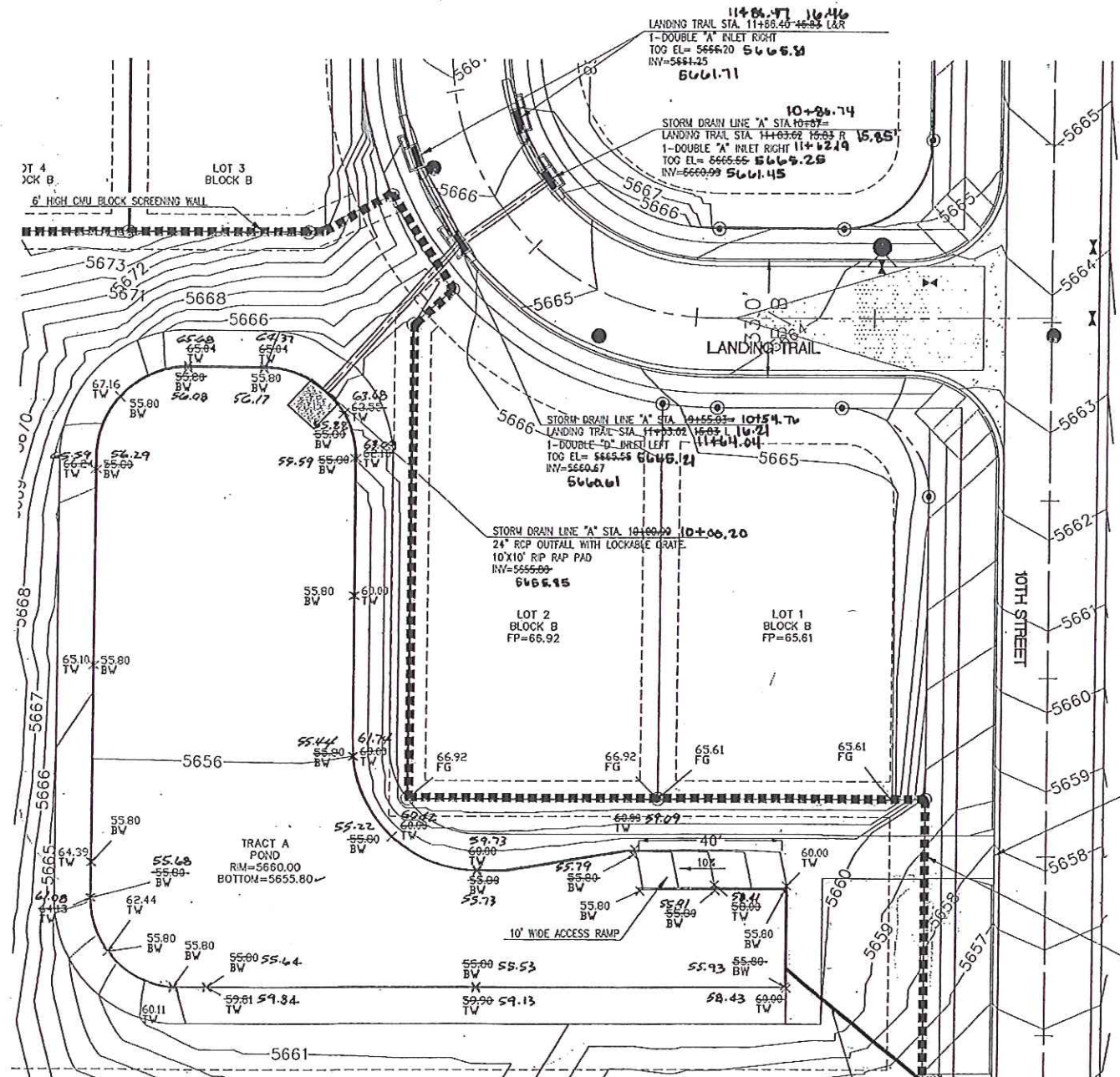


WALLEN PARK SUBDIVISION
GRADING AND DRAINAGE

DATE: May 3, 2007
SCALE: AS SHOWN
DESIGNER: REH
CHECKER: MVH/RLE
JOB NO.: N701-02

community sciences corporation

SHEET 7 OF 29



REBAR SCHEDULE					
	8" WALL REBAR	12" CONC. REBAR	14" WALL REBAR	12" WALL REBAR	FOOTING REBAR
1'-8"	#4 @ 48" O.C.	N/A	N/A	N/A	#4 @ 18" O.C.
2'-4"	#4 @ 48" O.C.	N/A	N/A	N/A	#4 @ 18" O.C.
3'-0"	#4 @ 48" O.C.	N/A	N/A	N/A	#4 @ 18" O.C.
3'-8"	#4 @ 32" O.C.	N/A	N/A	N/A	#4 @ 18" O.C.
4'-4"	#4 @ 16" O.C.	N/A	N/A	N/A	#4 @ 18" O.C.
5'-0"	#5 @ 8" O.C.	N/A	N/A	N/A	#4 @ 18" O.C.
5'-8"	#4 @ 8" VERT. #4 @ 24" HOR.	N/A	N/A	#4 @ 8" VERT. #4 @ 24" HOR.	#4 @ 18" O.C.
6'-4"	#4 @ 8" VERT. #4 @ 24" HOR.	N/A	N/A	#4 @ 8" VERT. #4 @ 24" HOR.	#4 @ 18" O.C.
7'-0"	#4 @ 8" VERT. #4 @ 24" HOR.	N/A	N/A	#5 @ 8" VERT. #4 @ 24" HOR.	#4 @ 9" O.C.
7'-8"	#4 @ 8" VERT. #4 @ 16" HOR.	N/A	#4 @ 8" VERT. #4 @ 16" HOR.	N/A	#4 @ 9" O.C.
8'-4"	#4 @ 8" VERT. #4 @ 16" HOR.	N/A	#5 @ 8" VERT. #4 @ 16" HOR.	N/A	#4 @ 9" O.C.
9'-0"	#4 @ 8" VERT. #4 @ 16" HOR.	#4 @ 8" VERT. #4 @ 16" HOR.	N/A	#4 @ 8" VERT. #4 @ 16" HOR.	#4 @ 9" O.C.
9'-8"	#5 @ 8" VERT. #5 @ 16" HOR.	#5 @ 8" VERT. #4 @ 16" HOR.	N/A	#5 @ 8" VERT. #4 @ 16" HOR.	#4 @ 9" O.C.
10'-4"	#5 @ 8" VERT. #5 @ 16" HOR.	#5 @ 8" VERT. #5 @ 16" HOR.	N/A	#5 @ 8" VERT. #4 @ 16" HOR.	#5 @ 9" O.C.
11'-0"	#5 @ 8" VERT. #5 @ 16" HOR.	#5 @ 8" VERT. #5 @ 16" HOR.	N/A	#5 @ 8" VERT. #5 @ 16" HOR.	#5 @ 9" O.C.

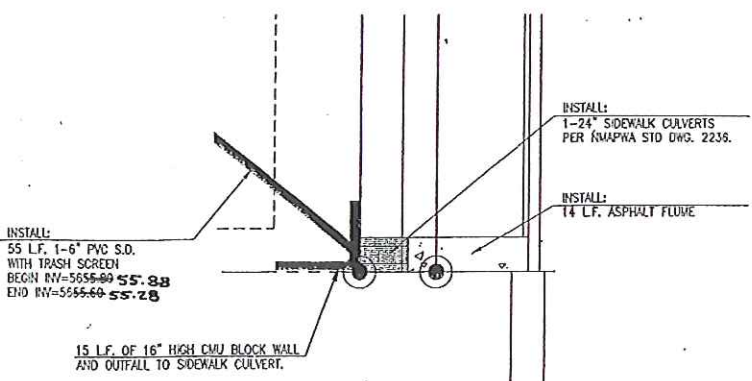
STORM DRAIN LINE 'A'
SCALE: H:1"=50', V:1"=5'

WALL DIMENSIONS TW-BW S (HEIGHT LISTED BELOW)															
	1'-8"	2'-4"	3'-0"	3'-8"	4'-4"	5'-0"	5'-8"	6'-4"	7'-0"	7'-8"	8'-4"	9'-0"	9'-8"	10'-4"	11'-0"
A	5"	1'-0"	1'-0"	1'-0"	1'-8"	2'-0"	2'-3"	1'-10"	2'-11"	2'-0"	2'-6"	2'-9"	3'-3"	4'-3"	4'-3"
B	1'-6"	1'-8"	2'-2"	2'-6"	3'-0"	3'-6"	3'-6"	4'-9"	5'-3"	5'-0"	5'-3"	5'-9"	6'-3"	6'-6"	7'-3"
C	N/A	N/A	N/A	N/A	N/A	2'-0"	2'-3"	1'-10"	1'-10"	2'-11"	2'-11"	2'-10"	2'-10"	4'-11"	4'-11"
D	N/A	N/A	N/A	N/A	N/A	1'-0"	3"	1'-10"	2'-4"	2'-4"	1'-10"	2'-11"	2'-4"	1'-4"	2'-11"
E	N/A	N/A	N/A	N/A	N/A	4"	1'-0"	8"	1'-0"	1'-0"	1'-3"	1'-6"	1'-9"	2'-0"	2'-4"
F	N/A	N/A	N/A	N/A	N/A	6"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"
G	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"	1'-0"
H	1'-0"	1'-0"	1'-0"	1'-0"	1'-3"	1'-3"	1'-3"	1'-3"	1'-3"	1'-3"	1'-3"	1'-3"	1'-3"	1'-4"	1'-4"
I	N/A	N/A	N/A	N/A	N/A	N/A	1'-4"	2'-0"	2'-8"	2'-8"	3'-4"	4'-0"	2'-8"	4'-0"	4'-0"
J	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	2'-0"	2'-0"	2'-0"	2'-0"

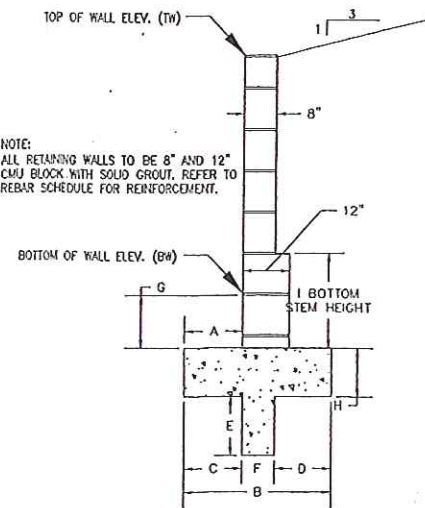
10TH STREET STA. 19+00.00
CENTERLINE RESIDENTIAL DRIVEWAY,
CONSTRUCT PER CORR STD. DWG. DW-01.
CONSTRUCT 12' WIDE, 6" THICK CONC.
DRIVE TO ROW, AND 12' WIDE, 8" OF
AGGREGATE BASE COURSE FOR INTERNAL
DRIVES.

ACCESS GATE AT 6' HIGH CMU BLOCK
SCREENING WALL

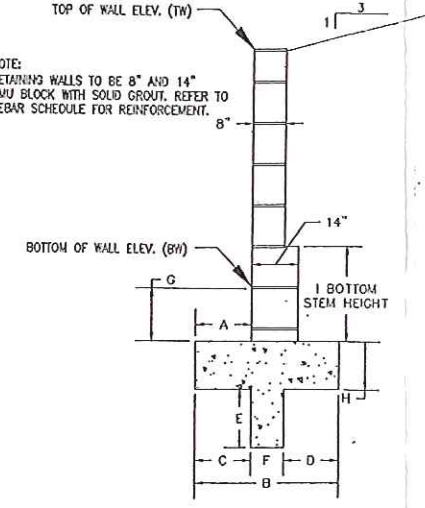
TRACT 'A' DETAILED POND GRADING
SCALE: 1"=20'



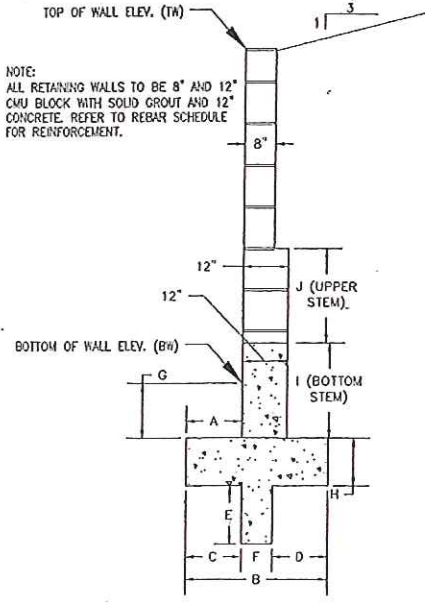
TRACT 'A' POND OUTFALL DETAIL
SCALE: 1"=10'



RETAINING WALL HEIGHT 1'-8" TO 7'-0"
N.T.S.



RETAINING WALL HEIGHT 7'-8" TO 8'-4"
N.T.S.



RETAINING WALL HEIGHT 9'-0" TO 11'-0"
N.T.S.

WALLEN PARK SUBDIVISION
STORM SEWER DETAILS

community sciences corporation

DATE: MAY 4, 2007
SCALE: AS SHOWN
DESIGNED: REH
CHECKED: MVH/RLB
DRAWN: H701-02

SHEET 27 OF 29

1.48

(SEE PLANS FOR ITEMS WITHIN THIS PROJECT)

LEGEND

- SURVEY MONUMENT
- FOUND MONUMENT AS NOTED
- EXISTING GAS LINE MARKER
- EXISTING WATER VALVE
- EXISTING JUNIPER BUSH/TREE
- EXISTING HYDRANT
- EXISTING CATV PEDESTAL
- EXISTING TELEPHONE PEDESTAL
- 10" G EXISTING GAS
- 10" W LINE EXISTING WATER LINE
- EXISTING ELECTRICAL TRANSFORMER
- EXISTING SURVEY MONUMENT
- EXISTING TELEPHONE PEDESTAL
- EXISTING WATER METER
- EXISTING MAIL BOX
- EXISTING EXISTING TV CABLE PEDESTAL
- 5640 DESIGN MAJOR CONTOUR
- DESIGN MINOR CONTOUR
- 5640 EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- RIGHT OF WAY LINE
- EASEMENT LINE
- LOT LINE
- FENCE LINE
- GRADE/SLOPE
- NATURAL GROUND
- COMPACTED SUBGRADE
- RIPRAP / COBBLES / STONE
- CONCRETE
- SELECT SOIL MATERIAL
- SOIL CEMENT
- GRADED DIRT PATH W/ DRAINAGE SWALE
- GRADED DIRT PATH
- SANDSTONE FINISH
- AGGREGATE BASE COURSE PATH
- EXISTING PAVEMENT
- REMOVE AND REPLACE

ABBREVIATIONS

- BOW BOTTOM OF WALL
- ℓ or CL CENTERLINE
- CDA CITY OF ALBUQUERQUE
- CORR CITY OF RIO RANCHO
- CONST CONSTRUCTION
- CMP CORRUGATED METAL PIPE
- DIA DIAMETER
- DIP DUCTILE IRON PIPE
- E EASTING
- EL/ELEV ELEVATION
- EX EXISTING
- FL FLOW LINE
- HORIZ HORIZONTAL
- HP HIGH POINT
- INV INVERT
- L LENGTH
- LP LOW POINT
- LT LEFT
- NAVD NORTH AMERICA VERTICAL DATUM
- N NORTHING
- OC ON CENTER
- PL PROPERTY LINE
- PVC POINT OF VERTICAL CURVATURE
- PVI POINT OF VERTICAL INTERSECTION
- PVT POINT OF VERTICAL TANGENCY
- R RADIUS
- RCP REINFORCED CONCRETE PIPE
- ROW RIGHT OF WAY
- RT RIGHT
- SD STORM DRAIN
- ST STREET
- STA STATION
- SW SIDEWALK
- SWPPP STORM WATER POLLUTION PREVENTION PLAN
- SWP3 STORM WATER POLLUTION PREVENTION PLAN
- T TANGENT
- TBM TEMPORARY BENCH MARK
- TOC TOP OF CURB
- TOW TOP OF WALL
- TYP TYPICAL
- SSCA/CA SOUTHERN SANDOVAL COUNTY ARROYO FLOOD CONTROL AUTHORITY
- VERT VERTICAL
- VC VERTICAL CURVE

SUNSET POND PROPERTIES:

CREST WIDTH: RETAINING WALL - 1' - 4"
 SLOPE UPSTREAM FACE: 17% (8:1)
 SLOPE/DOWNSTREAM FACE: VERTICAL @ 3' RETAINING WALL - 3% TO 5% DOWNSTREAM
 ELEVATION AT EMERGENCY SPILLWAY CREST: 5620
 ELEVATION OF PRINCIPAL OUTLET (FINISH GRADE OF POND): 5603
 WIDTH OF EMERGENCY SPILLWAY CREST: 380'
 DISCHARGE CAPACITY OF EMERGENCY SPILLWAY: 2330 CFS
 OUTLET CONDUIT SIZE AND TYPE: 24" DIP
 OUTLET CONDUIT CAPACITY (ORIFICE CONTROL): 39 CFS
 EVACUATION TIME: 11 HOURS
 STORAGE CAPACITY @ EMERGENCY SPILLWAY: 47.7 ACRE-FT. 15.6 AF
 STORAGE CAPACITY @ ELEVATION 5617 (DOWNSTREAM NATURAL GROUND): 40.9 AF 8.98 AF
 STORAGE CAPACITY @ BETWEEN NATURAL GROUND AND SPILLWAY: 7.4 AF 8.9 AF
 100 YEAR DRAINAGE AREA: 180 ACRES
 100 YEAR 24 HOUR DESIGN RAINFALL: 2.8"
 100 YEAR PEAK INFLOW TO POND: 478 CFS 454 CFS
 100 YEAR DETAINED VOLUME: 44.8 AC-FT. 10.9 AF
 100 YEAR WATER SURFACE ELEVATION: 5618
 100 YEAR PEAK OUTFLOW: 36 CFS
 100 YEAR FREEBOARD: 2'

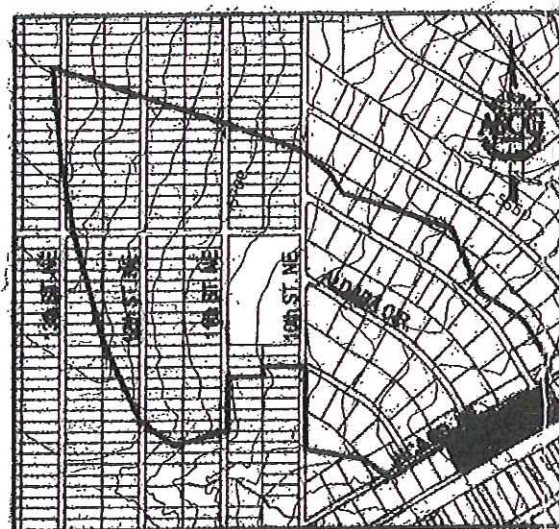
NOTE: THE SUNSET POND IS NOT A STATE ENGINEER PERMITTED FACILITY.

SUNSET POND RATING DATA

ELEVATION	STORAGE (AF)	OUTFLOW (cfs)
5606	0	0
5608	0.14	0.01
5610	0.37	0.15
5612	1.72	20.5
5614	4.11	29
5616	7.16	33
5618	11.01	36
5620	15.82	39
5621	20.5	200
5622	25.5	600

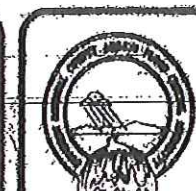
RECORD DRAWING
 Date: February, 2009
 These drawings have been revised to reflect the best information available. Do not use without field verification.
 Note: Design 100yr detained volume was 11.08 ac. ft.
 Note: Design 100yr WSEL was 5617.3.
 Note: Design 100yr Peak Outflow was 35 cfs.

SYMBOLS



SUNSET POND DRAINAGE AREA MAP

THIS SHEET HAS BEEN REDRAWN FOR RECORD PURPOSES. SEE ORIGINAL DRAWING FOR ENGINEER'S SIGNATURE AND SEAL.



SOUTHERN SANDOVAL COUNTY
 ARROYO FLOOD CONTROL
 AUTHORITY

SUNSET POND
 AND STORM DRAIN
 LEGEND, ABBREVIATIONS AND
 DRAINAGE DATA

REVISIONS

NUMBER	DATE

JOB NO: 277207
 DATE: JAN., 2008
 DRAWN BY: RRB
 CHECKED BY: CO
 DRAWING NO: 02

THIS SHEET HAS BEEN REDRAWN FOR RECORD PURPOSES. SEE ORIGINAL DRAWING FOR ENGINEER'S SIGNATURE AND SEAL.

C:\Users\p127\Documents\277207\Drawings\277207-02.dwg 3/7/2008 12:41:36 PM MST

DEVELOPED

CONDITIONS

AHYMO

INPUT

DATA

WEXFORD
DETENTION
POND

FROM

ASCG

BLACK

ARROYO

WATERSHED

MANAGEMENT

PLAN

ASCG

Final

August,

2002

DEVELOPED CONDITIONS AHYMO INPUT DATA
FILE PRINTOUT

FUTURE
COND.

AHYMO

WEXFORD
POND

2 OF 3

BL10D35B

START 0.0 HRS PUNCH CODE=0 PRINT LINES=-1

```

* -----HYDROLOGY MODEL-----
*S * * * FUTURE CONDITIONS MODEL - ALTERNATE B * * * * *
*S * * * 3 DAMS ON THE WEST BRANCH * * * * *
*S * * * UNSER GATEWAY DAM, AND WATER QUALITY DIVERSIONS * * * * *
*S * * * ROUTING WITH MCUNGE METHOD AFTER WATER QUALITY DIVERSIONS ARE * * * * *
*S * * * UTILIZED TO ADJUST FOR THE UNSTABLE HYDROGRAPHS WITH A STEEP SLOPE * * *
*S * * * AFTER MODIFICATION TO REDIRECT THE FIRST FLUSH OF 0.25" RUNOFF FOR SWQ *
* LH *****
* LH FILE MODIFIED BY LH/ASCG TO REFLECT FULL DEVELOPMENT WITHIN THE BLACK *
* LH ARROYO WATERSHED USING THE SSCAFCA LAND TREATMENTS FOR LOTS AND *
* LH ZONING DEVELOPED FOR THE MONTOYAS ARROYO STUDY. *
* LH THIS MODEL IS INTENDED TO PROVIDE A BIG PICTURE STUDY FOR THE BLACK *
* LH ARROYO AND SHOULD NOT BE USED TO DEVELOP DETAILED SOLUTIONS. *
* LH THE FEMA RESTUDY MODEL HAS BEEN ADDED TO IVORY AND LISBON CROSSING DESIGN *
* LH MODEL AND CHANGED TO DEVELOPED CONDITIONS. *
* LH *
* LH THE FOLLOWING THINGS WERE CHANGED IN THE MODEL: *
* LH *
* LH MODIFIED PRINT LINE COMMAND AND ROUTES CHANGED TO MANNINGS ROUTE FOR *
* LH ALL WELL DEFINED CHANNELS (ALSO CHANGED IN RESTUDY MODEL PORTION) *
* LH MODIFIED SLOPE FOR ROUTING THRU BASIN 103 FROM 0.0179 TO 0.0214 FT/FT. *
* LH SEE RUN CHRONOLOGY FOR OTHER CHANGES IN THE MODEL. *
* LH***** * * *
* ORIGINAL AHYMO MODEL DEVELOPED FOR:
* FEMA RE-STUDY
* SANDOVAL COUNTY, NEW MEXICO
*
* RESTUDY AREA: CITY OF RIO RANCHO
* FLOODING SOURCE: BLACK ARROYO
*

```

```

*****
* LH ALL SEDIMENT BULKING WAS MODIFIED TO USE THE SEDIMENT BULK COMMAND AND
* NOT THE DIVIDE HYD COMMANDS IN THE PREVIOUS FEMA RESTUDY MODELS.
* SEE RUNCHRONOLOGY FOR AN EXPLANATION OF THE BULKING FACTORS.
*

```

```

* RAINFALL TYPE=2 RAIN QUARTER=0.0 RAIN ONE=1.799
RAIN SIX=2.205 RAIN DAY=2.703 DT=.05
*

```

```

*S*****
*S BEGINNING OF THE BLACK ARROYO WEST BRANCH
*S*****
*S LISBON CHANNEL NORTH OF TULIP
*S * * * * *
* BULK FOR SEDIMENT

```

```

SEDIMENT BULK CODE=1 BULK FACTOR=1.18
*
COMPUTE LT TP LCODE=1 NK=4 ISLOPE=0
L=400 S=0.025 K=1
L=1300 S=0.014 K=2
L=1100 S=0.029 K=3
L=2200 S=0.023 K=4
KN=0.0 CD=0.0 Qp=420 cfs

```

```

* COMPUTE NM HYD ID=1 HYD=101 DA=0.3397 SQ MI
PER A=17 B=16 C=17 D=50
TP=0.0 HRS RAIN=-1

```

```

* PRINT HYD ID=1 CODE=1
*

```

```

* C ROUTE HYD. 101 TO 101.90
*

```

```

* COMPUTE RATING CURVE CID=1 VS NO=1 NSEGS=3
ELMIN=0 ELMAX=6.3 CH SLP=.015 ft/ft FP SLP=.015ft/ft
N=.045 DIST=15 N=-0.013 DIST=49 N=.045 DIST=64
DIST ELEV
0 6.3
15 6.0
27 0.0
37 0.0
49 6.0
64 6.3

```

CROSS-SECTION

3 OF 3
PAT. M. POWELL
WEXFORD BASIN
400

BL10D35B
COMPUTE RATING CURVE CID=1 VALLEY SECTION=1 NUMBER OF SEGMENTS=3
MINIMUM ELEV=0.0 FT MAXIMUM ELEV=1.5 FT
CHANNEL SLOPE=0.0043 FLOOD PLAIN SLOPE=0.0043
N=0.030 DIST=16.7 N=-0.017 DIST=48.1 N=0.030 DIST=64
DIST ELEV DIST ELE DIST ELEV DIST ELEV
0.0 1.5 8.0 .9 16.7 .7 16.9 0.0
18.9 0.1 32.0 0.4 45.1 0.1 47.9 0.0
48.1 0.7 56.0 0.9 64.0 1.5

COMPUTE TRAVEL TIME ID=3 REACH NO=1 VALLEY SECTIONS=1
LENGTH=875 FT SLOPE=0.0043
ROUTE ID=3 HYD NO=320.90 INFLOW ID=10 DT=0.0
PRINT HYD ID=3 CODE=1

320.90

** ADD THE ROUTED FLOW FROM BASIN 320 TO THE FLOW AT THE INTERSECTION OF
** WEXFORD AND ARCTURUS

ADD HYD ID=4 HYD=320.10 ID I=4 ID II=3
PRINT HYD ID=4 CODE=1

Wexford
Det. Pond

** COMPUTE HYDROGRAPH FOR BASIN 400 THE DETENTION POND SITE
COMPUTE NM HYD ID=2 HYD=400 DA=0.0041 SM
%A=0.0 %B=50.0 %C=50.0 %D=0.0 TP=0.13333
MASS RAINFALL=-1
PRINT HYD ID=2 CODE=1

** ADD THE FLOW IN WEXFORD AT THE INTERSECTION WITH ARCTURUS TO THE DETENTION
** POND TO BE LOCATED ON THE SOUTH SIDE OF WEXFORD

ADD HYD ID=4 HYD=400.1 ID I=4 ID II=2
PRINT HYD ID=4 CODE=1

** ROUTE THE FLOW THROUGH THE DETENTION POND

*S ***** AP 400.30 *****INFLOW INTO WEXFORD POND*****
*S*****

ROUTE RESERVOIR ID=5 HYD NO=400.90 INFLOW ID=4 CODE=24

OUTFLOW(cfs)	STORAGE(ac ft)	ELEV(ft)
0	0.0	31.5
10.00	0.01	32
60.0	0.19	33
78.0	0.60	34
92.0	1.23	35
102.0	2.35	36
120.0	5.52	38
135.0	9.19	40
142.0	11.25	41
145.0	12.50	41.5

WEXFORD
POND

*S ***** AP 400.OUT (BEFORE DIVIDE) *****
PRINT HYD ID=5 CODE=1

*S *****DIVIDE HYD TO UNBULK TO 3% *****
DIVIDE HYD ID=5 %=-97 ID I=1 HYD=UNBULK
ID II=53 HYD=SEDIMENT

*S DIVIDE INTO PIPE AND SPILLWAY FLOWS AP 400.OUT PIPE AND SPILL *****
DIVIDE HYD ID=1 Q=135 ID I=1 HYD NO=400.81 PIPE
ID II=3 HYD NO=400.82 SPILL

NO channel
NO W

** ROUTE THE OUTFLOW FROM THE POND (400.81) THROUGH A 42" STORM DRAIN
** TO THE CHANNEL ADJACENT TO 20TH. (OUTFALL TO CHANNEL BELOW ZARAGOSA ST.)
COMPUTE RATING CURVE CID=1 VALLEY SECTION=1 NUMBER OF SEGMENTS=3
PIPE DIA=42 N=0.013

COMPUTE TRAVEL TIME ID=6 REACH=1 NUMBER OF VALLEY SECTIONS=1
LENGTH=900 FT SLOPE=0.018

ROUTE ID=6 HYD NO=400.9 INFLOW ID=1 DT=0.0
PRINT HYD ID=6 CODE=1

* ROUTE THE FLOW OVER THE SPILLWAY (400.82) THROUGH THE STREET TILL IT DUMPS
* INTO THE STORM DRAIN

COMPUTE RATING CURVE CID=1 VALLEY SECTION=1 NUMBER OF SEGMENTS=3
MINIMUM ELEV=0.0 FT MAXIMUM ELEV=1.5 FT
CHANNEL SLOPE=0.0330 FLOOD PLAIN SLOPE=0.0330
N=0.030 DIST=16.7 N=-0.017 DIST=48.1 N=0.030 DIST=64
DIST ELEV DIST ELE DIST ELEV DIST ELEV
0.0 1.5 8.0 .9 16.7 .7 16.9 0.0
18.9 0.1 32.0 0.4 45.1 0.1 47.9 0.0
48.1 0.7 56.0 0.9 64.0 1.5

COMPUTE TRAVEL TIME ID=2 REACH NO=1 VALLEY SECTIONS=1
LENGTH=900 FT SLOPE=0.0330

ROUTE ID=2 HYD NO=400.91 INFLOW ID=3 DT=0.0
PRINT HYD ID=2 CODE=1

ADD HYD ID=6 HYD=400.20 ID I=2 ID II=6

ADDED
PIPE FLOW
ID=6 TO
EM. SPILL. FLOW
ID=2
NOW TOTAL ID=6

TABLE
Stone Bridge Det. Pond
ELEVATION-STORAGE-DISCHARGE DATA

grey box means must input data

Contour Elevation NAVD 1988	Depth (ft)	Contour Area (sq ft)	Incremental Volume (cu ft)	Incremental Volume (ac-ft)	Cumulative Volume (ac-ft)	Principal Spillway		Emergency Spillway Discharge (cfs)	Total Discharge (cfs)	Comment
						Number of Orifices	Orifice Diameter (inches)			
	(ft)	(sq ft)	(cu ft)	(ac-ft)	(ac-ft)	(cfs)	(cfs)	(cfs)		
5246.00	0	0	0	0.0000	0.0000	0.0	0.0	0.0		
5248.00	2.0	53162	53162	1.2204	1.2204	21.1	0.0	21.1		
5250.00	4.0	76682	129844	2.9808	4.2012	29.9	0.0	29.9		
5252.00	6.0	76823	153505	3.5240	7.7252	36.6	916.4	953.0		
			Total Volume (ft ³) =	336511						Pond bottom. 24" SD pipe invert from field observation
			Total Volume (ac-ft) =	7.73						Emergency spillway (f)
										(f) Length assumed along top of pond and elevations extended above emergency spillway to allow for rating curve to function if flow spills over top

(a) Orifice flows based on Equation 4-10 and Table 4 from Hydraulics 6th Edition, Brater King, 1976

$$Q = Ca\sqrt{2gh}$$

$$a = \frac{\pi D^2}{4}$$

C = 0.591
(full area formula)

g=32.2 ft/sec², a=area (sq ft) h=head (ft)
d = depth of water in the pipe in feet

(b) Emergency Spillway flows were computed based on the following data used in the weir equation
Q = CLH^{1.5} C = discharge coefficient, L = spillway length perp. To flow in ft, H = head (ft)

C = 3 L = 216

(d) Data Source 2010 Lidar topography and Field Observation and Measurements by Smith Engineering Company

TABLE
19 th Ave. RETENTION POND (Existing)
ELEVATION-STORAGE-DISCHARGE DATA (c)

grey box means must input data

Contour Elevation	Depth (ft)	Incremental Depth (ft)	Contour Area (sq ft)	Incremental Volume (cu ft)	Incremental Volume (ac-ft)	Cumulative Volume (ac-ft)	Comment
0			0			0.0000	
5218	0	0	0	0	0.0000	0.0000	Invert elevation of pond (d)
5220	2	2	38146	38146	0.8757	0.8757	
5222	4	2	42518	80664	1.8518	2.7275	
5224	6	2	51049	93567	2.1480	4.8755	
5226	8	2	55204	106253	2.4392	7.3147	
5228	10	2	59430	114634	2.6316	9.9464	
5230	12	2	63660	123090	2.8258	12.7721	
5232	14	2	69960	133620	3.0675	15.8396	Emerg. Spill. Elev. (only soil top of pond)

(d) This pond has no principal spillway pipe and acts as full retention
(C) Area - Elevation Data obtained from contours on the drainage basin map (generated from 2010 Lidar topography)

Proposed or Possible Detention Ponds

1. **Sugar Pond** – Source : Proposed Construction Plans – Prepared for SSCAFCA, prepared by WH Pacific, June 2011.
2. **Lisbon Pond** – Source : Conceptual Design by Smith Engineering Company, July 2013
3. **19th Ave. Dam (West Branch at west side of Unser Blvd.)** – Source : Conceptual Design by Smith Engineering Company, July 2013

Proposed or Possible Detention Ponds

1. Sugar Pond –

Source of Grading Plan:

Proposed Construction Plans – Prepared for SSCAFCA, prepared by WH Pacific, June 2011.

This Section Contains:

Copies of Select Sheets from the Sugar Pond Plans, WH Pacific, June 2011 as follows:

Cover Sheet

Sheet C2

Sheet C3

Sheet G3

Table S1 – Sugar Pond Proposed - Elevation – Volume – Discharge Data and Computations
(computed by Smith Engineering Company, April 2013)

Table S2 – Sugar Pond Very Conceptual Grading Plan Elevation – Area Data
(computed by Smith Engineering Company, April 2013)

SOUTHERN SANDOVAL COUNTY ARROYO FLOOD CONTROL AUTHORITY (SSCAFCA)

SUGAR POND OUTFALL

RIO RANCHO
SANDOVAL COUNTY, NEW MEXICO



JUNE 2011

INDEX OF DRAWINGS

SEQUENCE NO.	SHEET NO.	SHEET TITLE
1	T1	COVER SHEET, INDEX OF SHEETS, VICINITY MAP, LOCATION MAP
2	G1	CITY OF RIO RANCHO GENERAL NOTES
3	G2	PROJECT GENERAL NOTES & GEOTECHNICAL DATA
4	G3	LEGEND, ABBREVIATIONS & DRAINAGE DATA
5	G4	SITE SURVEY
6	C1	POND SITE LAYOUT
7	C2	POND GRADING PLAN
8	C3	POND OUTLET DETAILS
9	C4	FENCE LAYOUT AND DETAILS
10	C5	OUTLET STORM DRAIN PLAN AND PROFILE
11	C6	STORM DRAIN DETAILS
12	C7-C9	POND CROSS SECTIONS

NOTE:
THESE PLANS WERE PREPARED JUNE 2011
TO BE PLACED ON HOLD UNTIL FUNDING
IS AVAILABLE. REVIEW AND UPDATE TO
CURRENT CONDITIONS AT THE TIME OF
CONSTRUCTION.

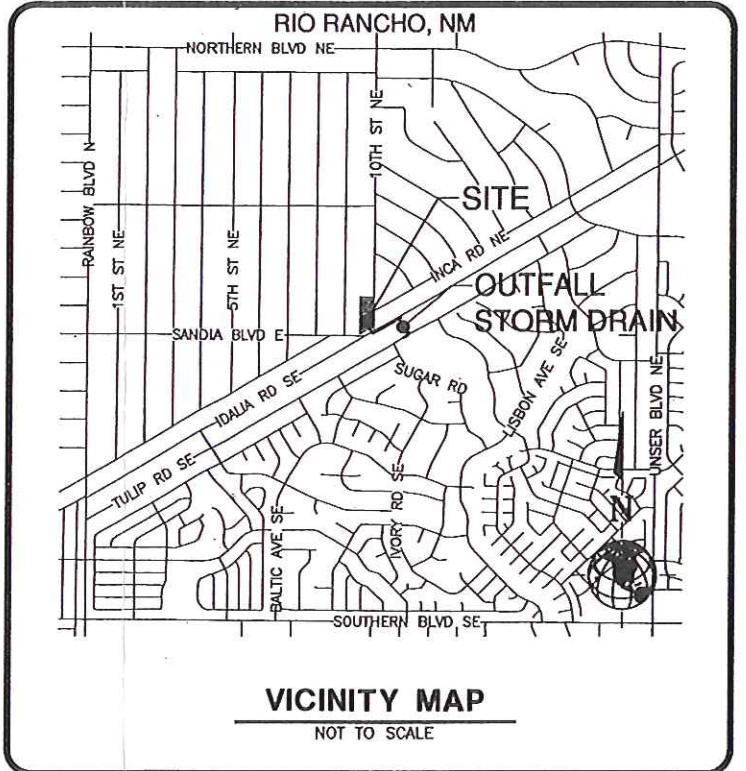
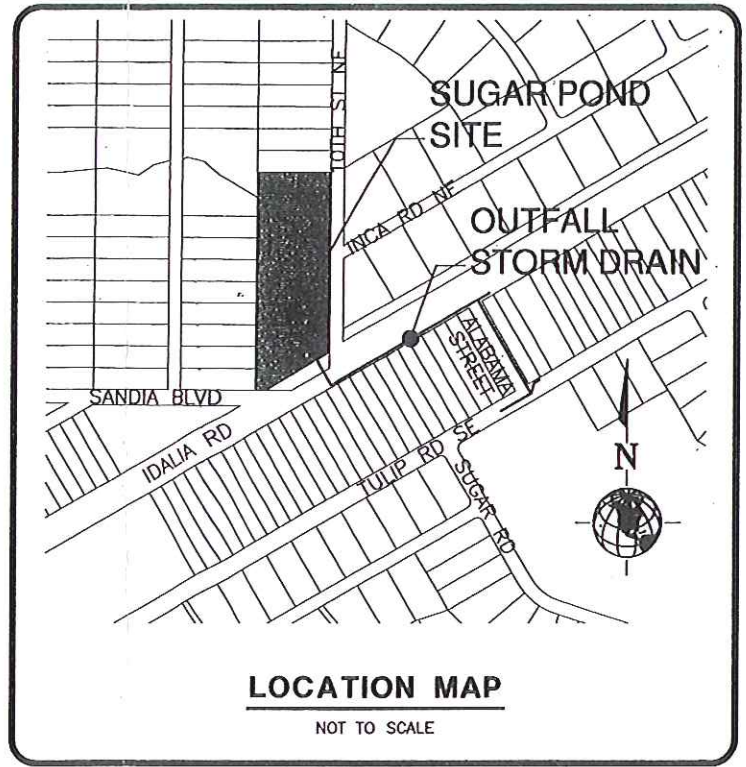


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SSCAFCA EXECUTIVE ENGINEER _____ DATE _____

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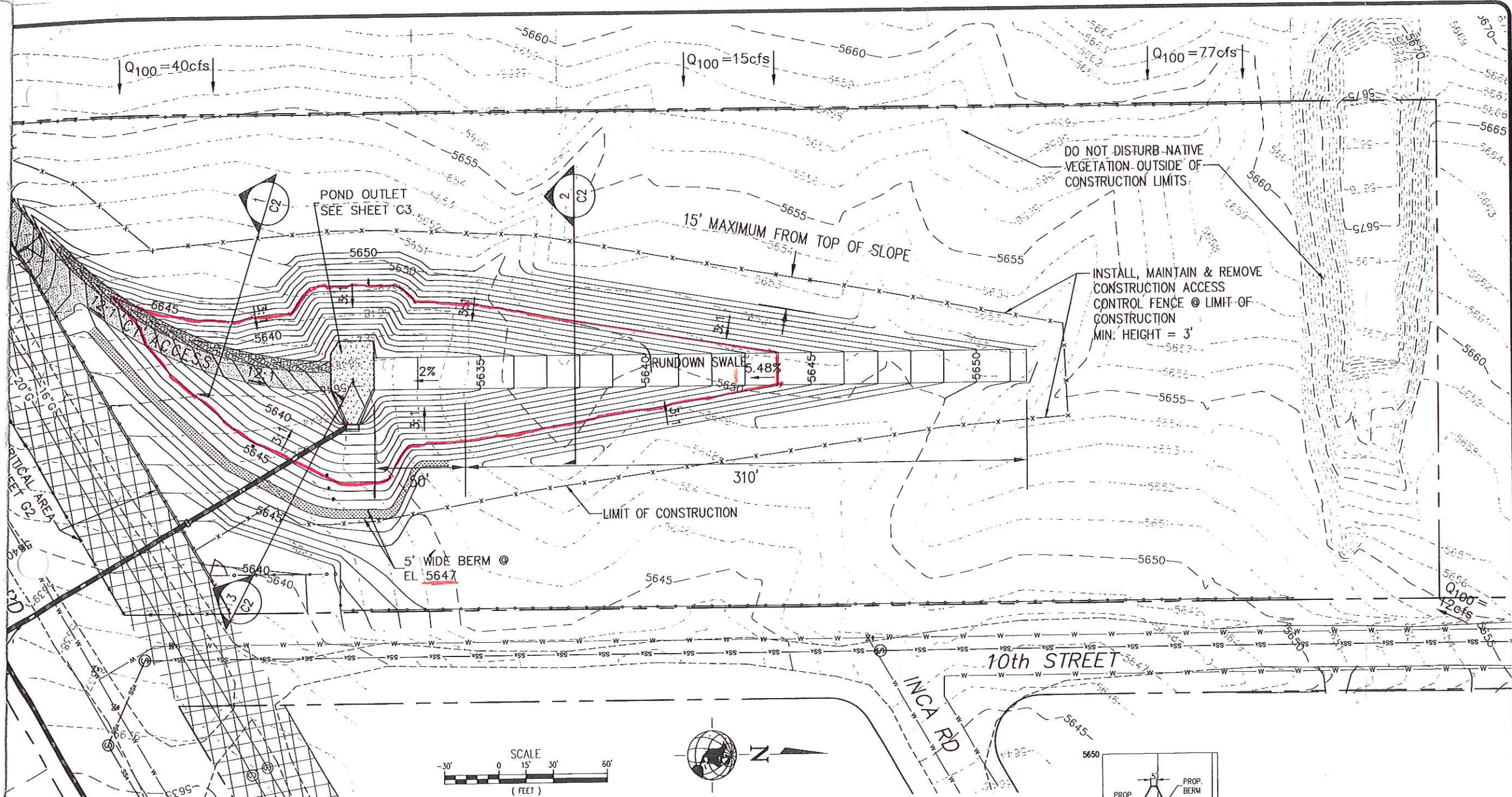
**SOUTHERN SANDOVAL COUNTY
 ARROYO FLOOD CONTROL
 AUTHORITY**

**SUGAR POND
 OUTFALL
 POND GRADING PLAN**

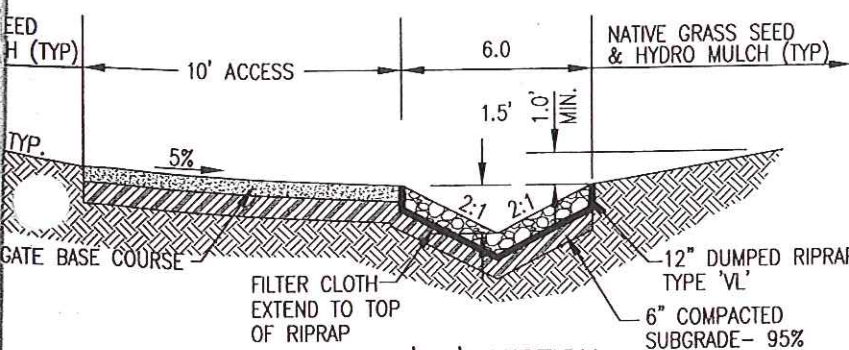
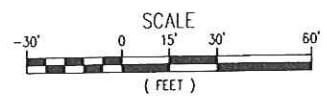
REVISIONS

NUMBER	DATE

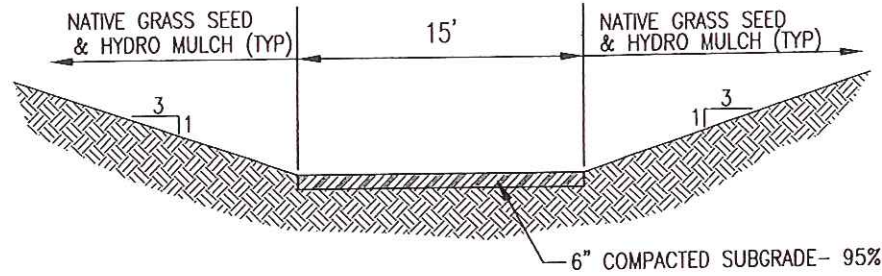
JOB NO: 212821
 DATE: JUNE 2011
 DRAWN BY: KLF
 CHECKED BY: CD
 DRAWING NO: **C2**



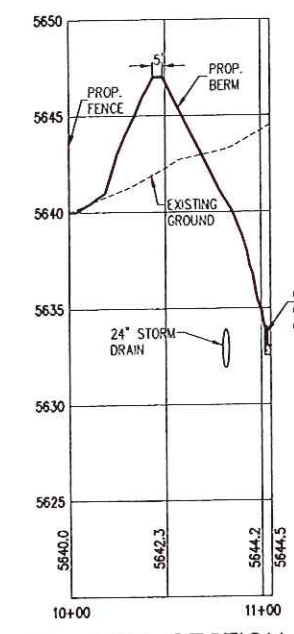
FOR LAYOUT CONTROL.
 FOR FENCE LAYOUT.
 MODEL WILL BE PROVIDED.
 DEVELOPED CONDITION FLOW.



1
C2 ACCESS 'C1' SECTION
 SCALE: NOT TO SCALE

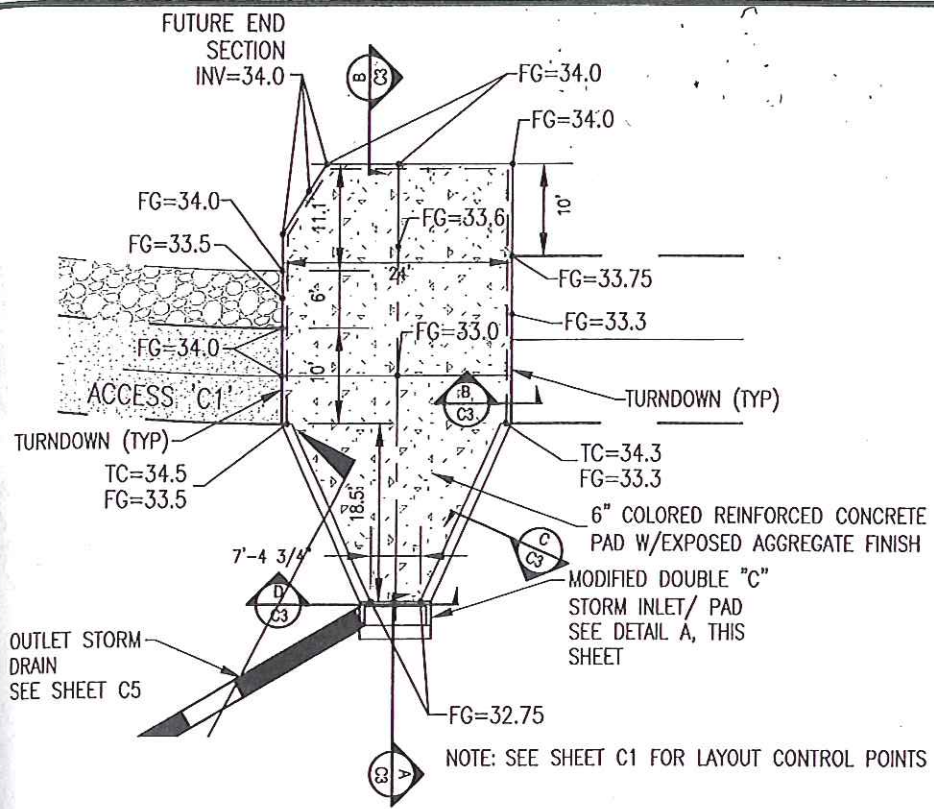


2
C2 RUNDOWN SWALE SECTION
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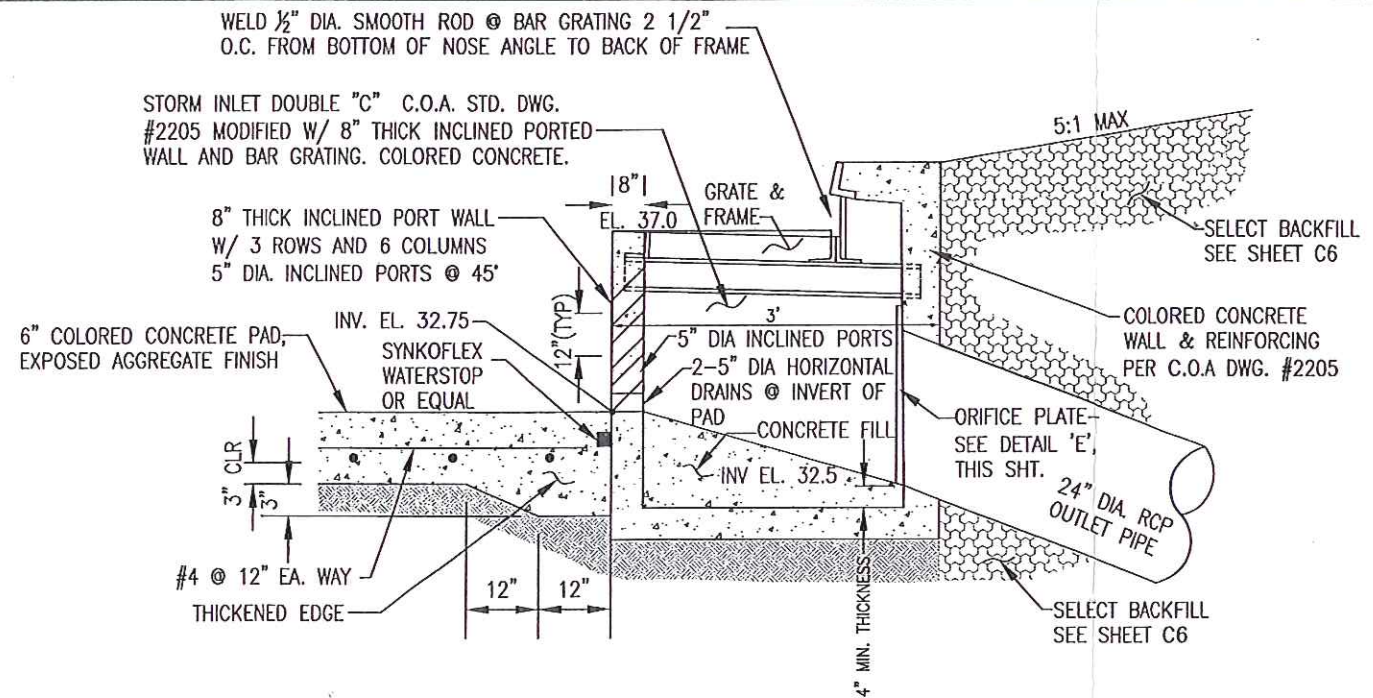


3
C2 DAM SECTION
 SCALE: HORIZ: 1" = 50'
 VERT: 1" = 5'

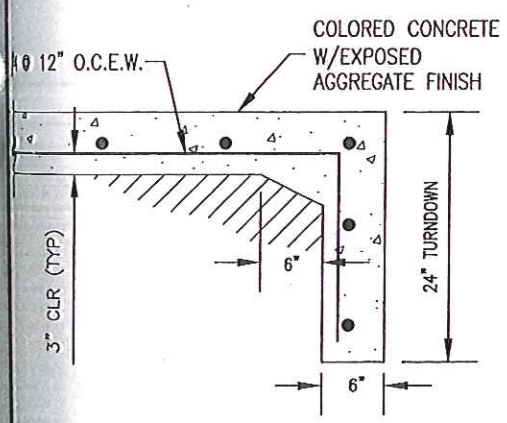




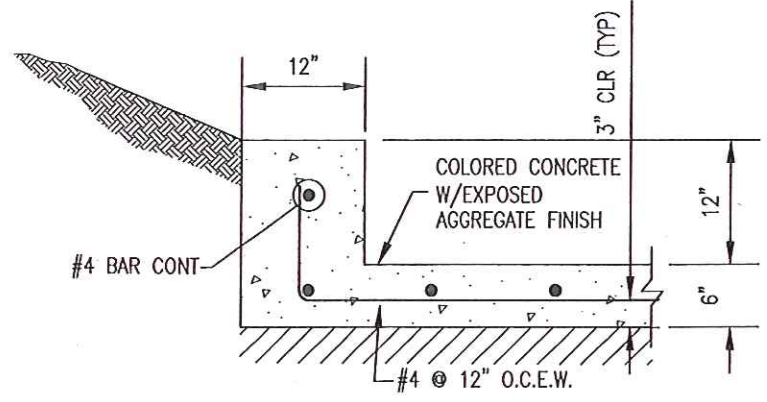
1 POND OUTLET PLAN
C3 SCALE: 1"=10'



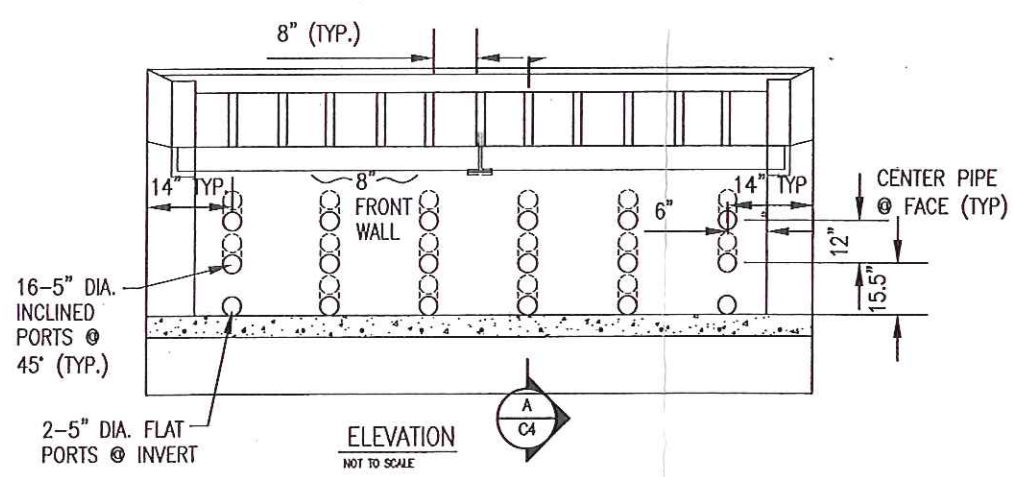
A C3 MODIFIED DOUBLE "C" STORM INLET/ PAD SECTION
SCALE: NOT TO SCALE



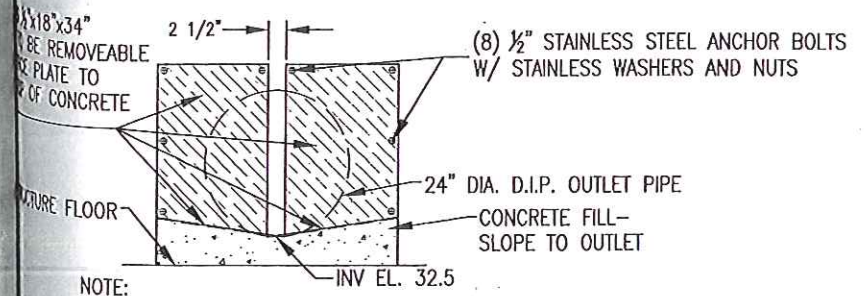
CONCRETE EDGE DETAIL W/O CURB
SCALE: NOT TO SCALE



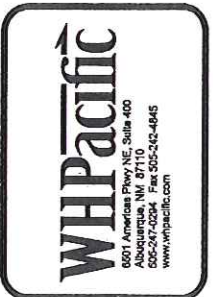
C C3 EDGE CURB DETAIL
SCALE: NOT TO SCALE



D C3 MODIFIED DOUBLE "C" STORM INLET ELEVATION
SCALE: NOT TO SCALE



E C3 ORIFICE PLATE DETAIL
SCALE: NOT TO SCALE



SOUTHERN SANDOVAL COUNTY
ARROYO FLOOD CONTROL
AUTHORITY

SUGAR POND
OUTFALL
POND OUTLET DETAILS

REVISIONS	
NUMBER	DATE

JOB NO.: 212821
DATE: JUNE 2011
DRAWN BY: KLF
CHECKED BY: CD
DRAWING NO.:
C3



LEGEND

- SURVEY MONUMENT
- FOUND MONUMENT AS NOTED
- EXISTING GAS LINE MARKER
- EXISTING WATER VALVE
- EXISTING JUNIPER BUSH/TREE
- G — EXISTING GAS LINE
- W — EXISTING WATER LINE
- S — EXISTING SANITARY SEWER LINE W/ MANHOLE
- EXISTING MAJOR CONTOUR
- EXISTING MINOR CONTOUR
- LOT LINE
- RIGHT OF WAY LINE
- EASEMENT LINE
- EXISTING DIRT/ACCESS ROAD
- FENCE LINE
- NEW STORM DRAIN LINE W/ MANHOLE
- NEW PATH CENTERLINE
- NEW MAJOR CONTOUR
- NEW MINOR CONTOUR
- NEW BUSH/TREE
- NATURAL GROUND
- COMPACTED SUBGRADE
- COMPACTED SUBGRADE PATH
- RIPRAP
- CONCRETE
- AGGREGATE BASE COURSE SURFACE
- SELECT SOIL MATERIAL
- CRUSHER FINES
- GAS LINE CRITICAL AREA
- ASPHALT

SYMBOLS

- SECTION NUMBER
- SHEET NUMBER WHERE SECTION IS DRAWN

DRAINAGE BASIN DATA:

AREA (AC)	DESIGN DISCHARGE (CFS)	DRAINS TO
22.4	72	SUGAR POND
4.2	15	SUGAR POND
11.5	40	SUGAR POND
15.2	52	SUGAR POND/SD (FUTURE)
5.6	30	SUGAR POND SITE
8.6	3.5	WALLEN POND TO 10TH TO SUGAR POND
—	8	SUGAR POND
13.8	32	SD @ IDALIA
9.6	33	SD @ TULIP
6.2	21	SD @ TULIP

ABBREVIATIONS

- AP ANALYSIS POINT
- AT AT
- BC BEGIN CURVE
- BCR BEGIN CURB RETURN
- BK BOOK
- BLDG BUILDING
- BM BENCH MARK
- BOP BEGINNING OF PROJECT
- BVC BEGIN VERTICAL CURVE
- BW BASE OF WALL
- CB CATCH BASIN
- CF CURB FACE
- CG CURB AND GUTTER
- CL CHAIN LINK
- C CENTERLINE
- CMP CORRUGATED METAL PIPE
- CO CLEAN OUT
- CONC CONCRETE
- CORR CITY OF RIO RANCHO
- CP CONTROL POINT
- CY CURB YARDS
- DI DRAINAGE UTILITY EASEMENT
- DUE DROP INLET
- DI DIAMETER
- Δ DELTA
- EA EACH
- EC END CURVE
- ECR END CURB RETURN
- ELEV ELEVATION
- EOP END OF PROJECT
- EP EDGE OF PAVEMENT
- ESMT EASEMENT
- EVC END VERTICAL CURVE
- EW EACH WAY
- EXIST EXISTING
- FF FINISH FLOOR
- FG FINISH GRADE
- FH FIRE HYDRANT
- FL FLOW LINE
- FOC FACE OF CURB
- FP FINISHED PAD
- G GAS
- GB GRADE BREAK
- GM GAS METER
- GV GATE VALVE
- HORIZ HORIZONTAL
- INT INTERSECTION
- INV INVERT
- INV EL INVERT ELEVATION
- LF LINEAR FEET
- LP LIGHT POLE
- LT LEFT
- MH MANHOLE
- NG NATURAL GROUND
- OC ON CENTER
- PB PULL BOX
- PC POINT OF CURVATURE
- PCC POINT OF COMPOUND CURVATURE
- PG PAGE
- PGL PROFILE GRADE LINE PER TYPICAL SECTION
- PI POINT OF INTERSECTION
- PL PROPERTY LINE
- PRC POINT OF REVERSE CURVATURE
- PT POINT OF TANGENCY
- PUE PUBLIC UTILITY EASEMENT
- PVC POLYVINYL CHLORIDE PIPE
- PVMT PAVEMENT
- RAD RADIUS
- RCP REINFORCED CONCRETE PIPE
- RD ROOF DRAIN
- REF REFERENCE
- RT RIGHT
- R/W, ROW RIGHT-OF-WAY
- S SLOPE
- SAS SANITARY SEWER LINE
- SD STORM DRAIN
- SF SQUARE FEET
- STA STATION
- STD STANDARD
- SW SIDEWALK
- SY SQUARE YARDS
- T TANGENT
- TA TOP OF ASPHALT
- TAC TOP OF ASPHALT CURB
- TBC TOP BACK OF CURB
- TC TOP OF CONCRETE
- TEL TELEPHONE LINE, RISER OR BOX
- TP TOP OF PIPE
- TRANS TRANSVERSE
- TW TOP OF WALL
- TYP TYPICAL
- UE UNDERGROUND ELECTRICAL LINE
- UT UNDERGROUND TELEPHONE LINE
- VC VERTICAL CURVE
- VERT VERTICAL
- VPI VERTICAL POINT OF INTERSECTION
- W WATERLINE
- WM WATER METER
- WSEL WATER SURFACE ELEVATION
- WV WATER VALVE

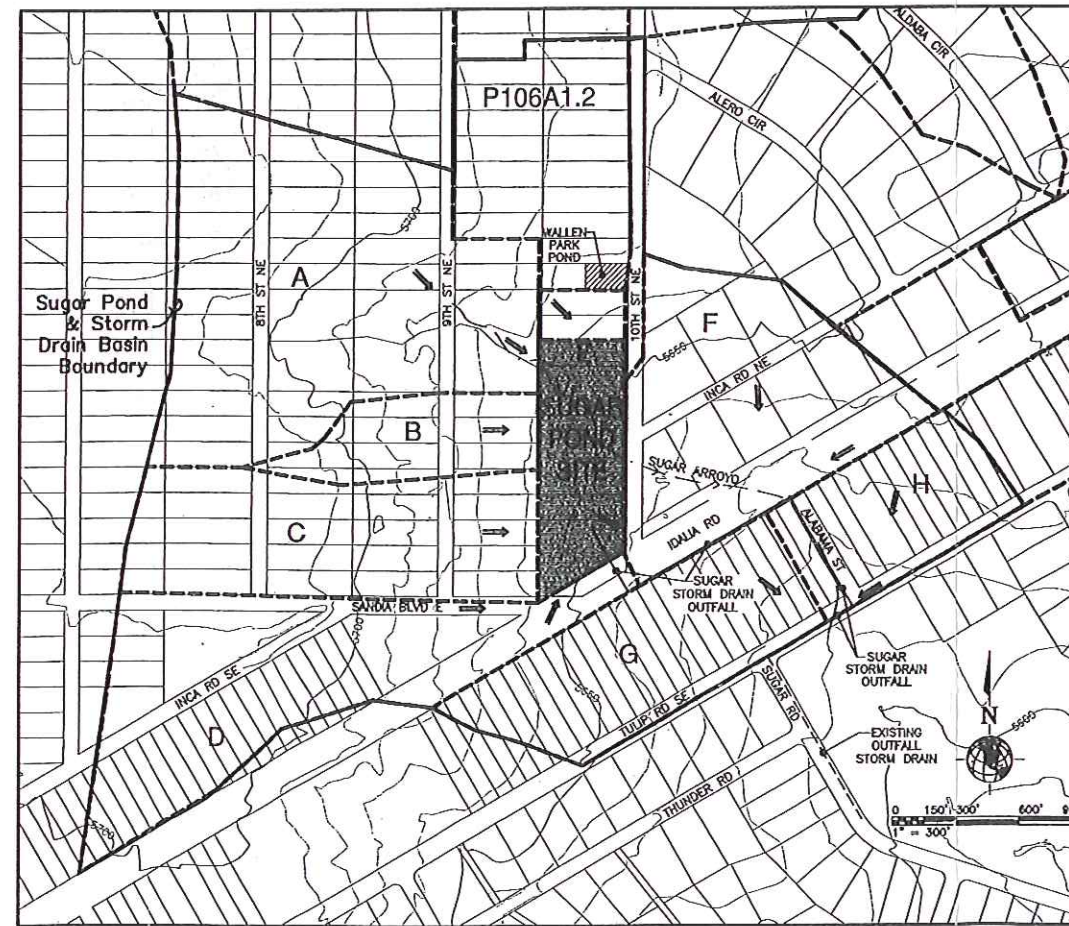
FUTURE SUGAR POND PROPERTIES:

- (NOT PART OF THIS PROJECT)
- CREST WIDTH 6 FEET RIPRAP
 - SLOPE UPSTREAM FACE 6H:1V (VARIES)
 - SLOPE DOWNSTREAM FACE 20H:1V (VARIES)
 - ELEVATION AT EMERGENCY SPILLWAY CREST 5644 FEET
 - ELEVATION OF PRINCIPAL OUTLET 5633 FEET
 - WIDTH OF EMERGENCY SPILLWAY CREST 100 FEET
 - DISCHARGE CAPACITY OF EMERGENCY SPILLWAY W 2' FB 350 CFS
 - OUTLET CONDUIT SIZE AND TYPE 24" DIP
 - OUTLET CONDUIT CAPACITY (W/ ORIFICE) 7.1 CFS
 - EVACUATION TIME 46 HOURS
 - STORAGE CAPACITY @ ELEV: 5644 9.9 ACRE FEET
 - 100 YEAR DRAINAGE AREA 75 ACRES
 - 100 YEAR 24 HOUR DESIGN RAINFALL 2.8" IN 24 HOURS
 - 100 YEAR PEAK INFLOW TO POND 220 CFS
 - 100 YEAR OUTLET FLOW FROM POND 6.5 CFS
 - 100 YEAR DETAINED VOLUME 6.5 ACRE FEET
 - 100 YEAR WATER SURFACE ELEVATION 5642
- FOR DETAILED INFORMATION SEE "SUGAR POND DESIGN ANALYSIS REPORT" DATED JANUARY, 2006.
REVISED JANUARY 2009.

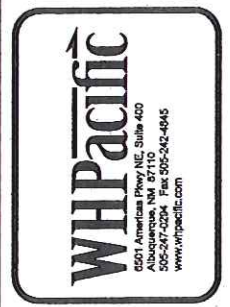
RATING DATA:

ELEV.	AREA (AC)	DISCHARGE (CFS)	VOLUME (AF)	NOTES
5633	0	0	0	OUTLET POND
5634	0.15	2.1	0	POND BOTTOM
5635	0.34	3.0	0	SEDIMENT POOL
5636	0.55	3.7	0.4	X
5637	0.69	4.3	1.1	X
5638	0.84	4.8	1.8	X
5639	1.00	5.3	2.7	X
5640	1.16	5.7	3.8	X
5641	1.33	6.1	5.1	X
5642	1.52	6.5	6.5	100 YR WSEL
5643	1.70	6.8	8.1	X
5644	1.88	7.1	9.9	SPILLWAY CREST
5645	2.06	350	11.9	X
5646	2.24	1000	14.0	X
5647	2.44	2000	16.4	EMBANKMENT TOP

NOTE: ASSUMES 1± SEDIMENT (EL 35.0 +/-).



DRAINAGE BASIN MAP



**SOUTHERN SANDOVAL COUNTY
ARROYO FLOOD CONTROL
AUTHORITY**

**SUGAR POND
OUTFALL**
LEGEND, ABBREVIATIONS
AND DRAINAGE DATA

REVISIONS

NUMBER	DATE

JOB NO.: 212821
DATE: JUNE 2011
DRAWN BY: KLF
CHECKED BY: CD
DRAWING NO.:
G3

TABLE S1
SUGAR POND (Proposed) OPTION 2
 Elevation - Volume - Discharge Data and Computations
 grey box means must input data

Contour Elevation NAVD 1988	Depth	Contour Area	Incremental Volume	Incremental Volume	Cumulative Volume	(A)		(A)		Principal Spillway Outfall Pipe Discharge	Total Discharge Spillway / Outfall Pipe Discharge	Emergency Spillway Discharge	Total Discharge Rating Curve	Comment
						1st Row of Reverse Incline Ports Discharge	2nd Row of Reverse Incline Ports Discharge	Principal Spillway / Outfall Pipe Discharge	(cfs)					
(ft)	(g)	(sq ft)	(cu ft)	(ac-ft)	(ac-ft)	(cfs)	(a)	(cfs)	(b)	(cfs)	(a)	(cfs)	(b)	(cfs)
5633	0	300	0	0.0000	0.0000	0.0	0.0	0.0	0.0	0.0	0.0	0	0	0
5634	1.0	3885	2093	0.0480	0.0480	0.0	0.0	0.0	0.0	0.0	0.0	0	0	0
5634.5	1.5	4521	2102	0.0482	0.0963	2.6	0.0	0.0	0.0	0.0	3	1	1	4
5635	2.0	5157	2420	0.0555	0.1518	3.7	0.0	0.0	0.0	0.0	4	0	0	4
5636	3.0	6501	5829	0.1338	0.2856	5.3	3.7	0.0	0.0	0.0	9	0	0	9
5637	4.0	7917	7209	0.1655	0.4511	6.4	5.3	0.0	0.0	0.0	12	0	0	12
5638	5.0	9405	8661	0.1988	0.6500	7.4	6.4	45.0	45.0	19	19	0	0	19
5639	6.0	10965	10185	0.2338	0.8838	8.3	7.4	127.3	127.3	20	20	0	0	20
5640	7.0	12597	11781	0.2705	1.1542	9.1	8.3	233.8	233.8	22	22	0	0	22
5641	8.0	14301	13449	0.3087	1.4630	9.8	9.1	360.0	360.0	24	24	0	0	24
5642	9.0	16077	15189	0.3487	1.8117	10.5	9.8	503.1	503.1	25	25	0	0	25
5643	10.0	17925	17001	0.3903	2.2020	11.2	10.5	661.4	661.4	26	26	0	0	26
5644	11.0	19845	18885	0.4335	2.6355	11.8	11.2	833.4	833.4	28	28	0	0	28
5645	12.0	21837	20841	0.4784	3.1139	12.3	11.8	1018.2	1018.2	29	29	0	0	29
5646	13.0	23901	22869	0.5250	3.6389	12.9	12.3	1215.0	1215.0	30	30	0	0	30
5647	14.0	26037	24969	0.5732	4.2122	13.4	12.9	1423.0	1423.0	31	31	0	0	31
5647.5	14.5	26038	13019	0.2989	4.5110	13.7	13.1	1531.1	1531.1	32	32	239	0	271

(a) Office equation and coefficient were obtained from Equation 4-10 and Table 4-3 from "Handbook of Hydraulics" Sixth Edition, by Brater & King, 1976.
 $Q = C a \sqrt{2gh}$
 $a = \frac{\pi D^2}{4}$
 (full area formula)
 $a = \frac{1}{2} r^2 \left[2 \cos^{-1} \left(\frac{r-d}{r} \right) \right] \frac{\pi}{180} - \sin \left[2 \cos^{-1} \left(\frac{r-d}{r} \right) \right] \frac{\pi}{180}$
 (partial area formula)
 (e) The combined discharge of the reverse incline ports and the grate (A), will govern the discharge until the principal spillway outfall pipe becomes fully submerged. When the sum of (A)s is greater than outfall pipe capacity then outfall pipe capacity governs the discharge

(b) Principal Spill. Pipe radius r in feet = 0.75
 d = depth of water in the pipe in feet
 Emergency Spillway flows were computed based on the following data used in the weir equation
 $Q = CLH^{1.5}$ C = discharge coefficient, L = spillway length perp. to flow (ft), H = head (ft)
 (b) Emergency Spillway C = 2.60 L = 260 Emer. Spill. EI 5647
 (b) Grate / Weir C = 3.00 L = 15 EI. 5'x5' grate 5637
 (g) Data Source : See Table S2 for Rectangular Pond 1V:3H computations for contour area calculations and Sheet C2 Grading Plan from WH Pacific Sugar Pond Plans dated June 2011.
 (b) Weir equation and "C" coefficients were obtained from Equation 5-10 and Table 5-3 from "Handbook of Hydraulics" Sixth Edition, by Brater & King, 1976.

TABLE S2					
Sugar Pond Very Conceptual Grading Plan (See Note "A" below)					
Elevation - Area Data					
Assume Rectangular Pond Shape with 1V:3H side slopes -					
Generally Following the WH Pacific June 2011 Sugar Pond Grading Plan (Sheet C2) attached. Note that Sheet C2 is drawn to scale and was used as the basis to set up this spreadsheet to generally follow the contour shape of this pond on Sheet C2.					
Elevation	Length	Width	Contour Area	Contour Area	COMMENT
ft	ft	ft	sq ft	acres	
5632.75	0	0	0	0.0000	Invert Elevation at Modified Double C storm inlet as shown on Sheet C3 of WH Pacific Plans (June 2011)
5633	20	15	300	0.0069	ASSUME Starting Elevation as 5633 for this Conceptual Level Pond Routing
5634	185	21	3,885	0.0892	
5635	191	27	5,157	0.1184	
5636	197	33	6,501	0.1492	
5637	203	39	7,917	0.1817	
5638	209	45	9,405	0.2159	
5639	215	51	10,965	0.2517	
5640	221	57	12,597	0.2892	
5641	227	63	14,301	0.3283	
5642	233	69	16,077	0.3691	
5643	239	75	17,925	0.4115	
5644	245	81	19,845	0.4556	
5645	251	87	21,837	0.5013	
5646	257	93	23,901	0.5487	
5647	263	99	26,037	0.5977	SEE NOTE "A" - BELOW
A - The WH Pacific Plans presents Rating Curve Data on Sheet G3 (attached). The area shown at the 5647 contour = 2.44 acres and this is much to large compared to measurement on Sheet C2. At SSCAFCA's direction, Smith Engineering was directed to spend very little effort refining the Sugar Pond design or pond routing. Therefore, the simplified rectangular pond assumptions / computations were developed and computed in this spreadsheet. These values are adopted for the Ultimate conditions Sugar Pond detention pond routing and are included in Table S1					

Proposed or Possible Detention Ponds

2. Lisbon Pond –

Lisbon Pond Conceptual Design (Conceptual Level Grading Plan)
(prepared by Smith Engineering Company, July 2013)

Table L1 - Lisbon Pond - Elevation – Volume – Discharge Data and Computations
(computed by Smith Engineering Company, July 2013)

TABLE L1
LISBON POND (Proposed) REVISED -36-in cul mas rat curve/ new areas
Elevation - Volume - Discharge Data and Computations

Option Description - Embankment height 8 ft. tall relative to Inca Rd. Max. pond depth to top emankment = 13 ft. Pond bottom slope = 0.5 %, Pond inside side slopes mainly 1V:6H. See below for Principal, Emergency and Outfall Pipe information.

grey box means must input data

Contour Elevation NAVD 1988	Depth	Contour Area (grading plan of 5-30-13)	Incremental Volume	Incremental Volume	Cumulative Volume	(A)			(A)		Total Principal Spillway / Outfall Pipe Discharge	Emergency Spillway Discharge	Total Discharge Rating Curve	Comment
						1st Row of Reverse Incline Ports Discharge	2nd Row of Reverse Incline Ports Discharge	Principal Spillway Gate Discharge	Principal Spillway 36-in. Outfall Pipe Discharge	(cfs)				
(ft)		(sq ft)	(cu ft)	(ac-ft)	(ac-ft)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)		
5589.00	0	0	0	0.0000	0.0000	0.0	0.0	0.0	0.0	0.0	0.0	0	Pond bottom and principal spillway structure invert	
5590.00	1	46,585	23,293	0.5347	0.5347	0.0	0.0	0.0	4.0	0.0	0.0	0	Highest invert 1st row of reverse incline ports	
5591.00	2	105,063	75,824	1.7407	2.2754	19.8	0.0	0.0	16.0	0.0	0.0	16	Highest invert of 2nd row of reverse incline ports	
5592.00	3	113,329	109,196	2.5068	4.7822	28.0	0.0	0.0	32.0	0.0	0.0	28		
5593.00	4	121,734	117,532	2.6992	7.4803	34.4	19.8	0.0	50.0	0.0	0.0	50		
5594.00	5	130,334	126,034	2.8933	10.3737	39.7	28.0	0.0	61.0	0.0	0.0	61		
5595.00	6	139,113	134,724	3.0928	13.4665	44.3	34.4	0.0	64.0	0.0	0.0	64	Top of principal spillway grate	
5596.00	7	148,116	143,615	3.2989	16.7635	48.6	39.7	96.0	67.0	0.0	0.0	67		
5597.00	8	157,339	152,728	3.5061	20.2696	52.5	44.3	271.5	70.0	0.0	0.0	70		
5598.00	9	166,790	162,065	3.7205	23.9901	56.1	48.6	498.8	72.0	0.0	0.0	72		
5599.00	10	176,505	171,548	3.9405	27.9306	59.5	52.5	768.0	74.0	0.0	0.0	74		
5600.00	11	186,425	181,465	4.1659	32.0964	62.7	56.1	1073.3	77.0	0.0	0.0	77		
5601.00	12	196,606	191,516	4.3966	36.4930	65.8	59.5	1410.9	79.0	0.0	0.0	79	Emergency spillway Elevation	
5601.20	12.2	207,079	40,368	0.9267	37.4198	66.4	60.2	1482.0	81.0	23.3	23.3	104		
5601.40	12.4	207,080	41,416	0.9508	38.3705	67.0	60.8	1554.3	82.0	65.8	65.8	148		
5601.60	12.6	207,081	41,416	0.9508	39.3213	67.5	61.4	1627.7	83.0	120.8	120.8	204		
5601.80	12.8	207,082	41,416	0.9508	40.2721	68.1	62.1	1702.3	84.0	186.0	186.0	270		
5602.00	13.0	207,083	201,845	4.6337	41.1267	68.7	62.7	1777.9	85.0	260.0	260.0	345	Top of Dam	

(a) Office equation and coefficient were obtained from Equation 4-10 and Table 4-3 from "Handbook of Hydraulics" Sixth Edition, by Brater & King, 1976.

$$Q = C a \sqrt{2gh}$$

$$a = \frac{\pi D^2}{4}$$

(full area formula)

Principal Spill. Pipe radius r in feet = 1.50

Emergency Spillway flows were computed based on the following data used in the weir equation

$$Q = CLH^{1.5} \quad C = \text{discharge coefficient, } L = \text{spillway length perp. to flow (ft), } H = \text{head (ft)}$$

$$(b) \text{ Emergency Spillway } C = 2.6 \quad L = 100 \quad \text{Emer. Spill. El. } 5601$$

$$(b) \text{ Gate / Weir } C = 3 \quad L = 32 \quad \text{El. } 8' \times 8' \text{ grate } 5595$$

(d) Data Source : Lidar Contours provided by SSCAFCA

(c) Rating curve computed with Culvert Master - output is attached

(e) The combined discharge of the reverse incline ports and the grate (A), will govern the discharge until the principal spillway outfall pipe becomes fully submerged. When the sum of (A)s is greater than outfall pipe capacity then outfall pipe capacity governs the discharge

(b) Weir equation and "C" coefficients were obtained from Equation 5-10 and Table 5-3 from "Handbook of Hydraulics" Sixth Edition, by Brater & King, 1976.

Table R1

Rating Curve Parameters for Lisbon Pond Outfall Pipe

Depth	Upstream Invert Elevation	Headwater Elevation	Downstream Invert Elevation	Tailwater Elevation	Length	Slope	Manning's 'n'	Pipe Size	Pipe Shape	Computed Discharge from Culvert Master for 1 Box Culvert
ft	ft	ft	ft	ft	ft	ft/ft		ft		cfs
	a	b	c	d	a	a				e
0	5589	5589	5587	5587.0	225	0.01	0.013	3	circular	0
1		5590		5587.7						4
2		5591		5588.3						16
3		5592		5589.0						32
4		5593		5589.7						50
5		5594		5590.3						61
6		5595		5591.0						64
7		5596		5591.7						67
8		5597		5592.3						70
9		5598		5593.0						72
10		5599		5593.7						74
11		5600		5594.3						77
12		5601		5595.0						79
13		5602		5595.7						81

a- Based on SSCAFCA approved conceptual grading plan for Lisbon Pond
 b- Headwater elevation = depth + upstream invert elevation
 c- Based on 2ft contour map provided by SSCAFCA
 d- Tailwater Elevation Assumption = (2/3*depth) + Downstream Invert Elevation
 e- Based on Culvert Master calculations- see output in Appendix I

Culvert Calculator Report HW 1ft

olve For: Discharge

Culvert Summary

Allowable HW Elevation	5,590.00 ft	Headwater Depth/Height	0.33
Computed Headwater Elev:	5,590.00 ft	Discharge	4.39 cfs
Inlet Control HW Elev.	5,589.88 ft	Tailwater Elevation	5,587.70 ft
Outlet Control HW Elev.	5,590.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	0.70 ft
Slope Type	Steep	Normal Depth	0.54 ft
Flow Regime	N/A	Critical Depth	0.65 ft
Velocity Downstream	3.50 ft/s	Critical Slope	0.003969 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,590.00 ft	Upstream Velocity Head	0.23 ft
Ke	0.50	Entrance Loss	0.12 ft

Inlet Control Properties

Inlet Control HW Elev.	5,589.88 ft	Flow Control	Unsubmerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 2ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,591.00 ft	Headwater Depth/Height	0.67
Computed Headwater Elev.	5,591.00 ft	Discharge	15.96 cfs
Inlet Control HW Elev.	5,590.80 ft	Tailwater Elevation	5,588.30 ft
Outlet Control HW Elev.	5,591.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	1.30 ft
Slope Type	Steep	Normal Depth	1.03 ft
Flow Regime	N/A	Critical Depth	1.28 ft
Velocity Downstream	5.44 ft/s	Critical Slope	0.004040 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,591.00 ft	Upstream Velocity Head	0.48 ft
Ke	0.50	Entrance Loss	0.24 ft

Inlet Control Properties

Inlet Control HW Elev.	5,590.80 ft	Flow Control	Unsubmerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 3ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,592.00 ft	Headwater Depth/Height	1.00
Computed Headwater Elev.	5,592.00 ft	Discharge	32.04 cfs
Inlet Control HW Elev.	5,591.80 ft	Tailwater Elevation	5,589.00 ft
Outlet Control HW Elev.	5,592.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	2.00 ft
Slope Type	Steep	Normal Depth	1.52 ft
Flow Regime	N/A	Critical Depth	1.84 ft
Velocity Downstream	6.40 ft/s	Critical Slope	0.004810 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,592.00 ft	Upstream Velocity Head	0.78 ft
Ke	0.50	Entrance Loss	0.39 ft

Inlet Control Properties

Inlet Control HW Elev.	5,591.80 ft	Flow Control	Unsubmerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 4ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,593.00 ft	Headwater Depth/Height	1.33
Computed Headwater Elev.	5,593.00 ft	Discharge	49.61 cfs
Inlet Control HW Elev.	5,592.96 ft	Tailwater Elevation	5,589.70 ft
Outlet Control HW Elev.	5,593.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	2.70 ft
Slope Type	Steep	Normal Depth	2.01 ft
Flow Regime	N/A	Critical Depth	2.29 ft
Velocity Downstream	7.40 ft/s	Critical Slope	0.006374 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,593.00 ft	Upstream Velocity Head	1.14 ft
Ke	0.50	Entrance Loss	0.57 ft

Inlet Control Properties

Inlet Control HW Elev.	5,592.96 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 5ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,594.00 ft	Headwater Depth/Height	1.67
Computed Headwater Elev.	5,594.00 ft	Discharge	61.40 cfs
Inlet Control HW Elev.	5,594.00 ft	Tailwater Elevation	5,590.30 ft
Outlet Control HW Elev.	5,593.97 ft	Control Type	Inlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	Pressure Profile	Depth, Downstream	2.40 ft
Slope Type	N/A	Normal Depth	2.40 ft
Flow Regime	N/A	Critical Depth	2.53 ft
Velocity Downstream	10.14 ft/s	Critical Slope	0.008097 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,593.97 ft	Upstream Velocity Head	1.45 ft
Ke	0.50	Entrance Loss	0.59 ft

Inlet Control Properties

Inlet Control HW Elev.	5,594.00 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 6ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,595.00 ft	Headwater Depth/Height	2.00
Computed Headwater Elev.	5,595.00 ft	Discharge	64.14 cfs
Inlet Control HW Elev.	5,594.27 ft	Tailwater Elevation	5,591.00 ft
Outlet Control HW Elev.	5,595.00 ft	Control Type	Outlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	Pressure Profile	Depth, Downstream	4.00 ft
Slope Type	N/A	Normal Depth	2.52 ft
Flow Regime	N/A	Critical Depth	2.57 ft
Velocity Downstream	9.07 ft/s	Critical Slope	0.008603 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,595.00 ft	Upstream Velocity Head	1.28 ft
Ke	0.50	Entrance Loss	0.64 ft

Inlet Control Properties

Inlet Control HW Elev.	5,594.27 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 7ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,596.00 ft	Headwater Depth/Height	2.33
Computed Headwater Elev.	5,596.00 ft	<u>Discharge</u>	<u>66.50 cfs</u>
Inlet Control HW Elev.	5,594.52 ft	Tailwater Elevation	5,591.70 ft
Outlet Control HW Elev.	5,596.00 ft	Control Type	Outlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	Pressure Profile	Depth, Downstream	4.70 ft
Slope Type	N/A	Normal Depth	2.66 ft
Flow Regime	N/A	Critical Depth	2.61 ft
Velocity Downstream	9.41 ft/s	Critical Slope	0.009075 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,596.00 ft	Upstream Velocity Head	1.38 ft
Ke	0.50	Entrance Loss	0.69 ft

Inlet Control Properties

Inlet Control HW Elev.	5,594.52 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 8ft

olve For: Discharge

Culvert Summary

Allowable HW Elevation	5,597.00 ft	Headwater Depth/Height	2.67
Computed Headwater Elev.	5,597.00 ft	Discharge	69.52 cfs
Inlet Control HW Elev.	5,594.85 ft	Tailwater Elevation	5,592.30 ft
Outlet Control HW Elev.	5,597.00 ft	Control Type	Outlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	Pressure Profile	Depth, Downstream	5.30 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	2.65 ft
Velocity Downstream	9.84 ft/s	Critical Slope	0.009732 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,597.00 ft	Upstream Velocity Head	1.50 ft
Ke	0.50	Entrance Loss	0.75 ft

Inlet Control Properties

Inlet Control HW Elev.	5,594.85 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 9ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,598.00 ft	Headwater Depth/Height	3.00
Computed Headwater Elev:	5,598.00 ft	<u>Discharge</u>	<u>71.71 cfs</u>
Inlet Control HW Elev.	5,595.09 ft	Tailwater Elevation	5,593.00 ft
Outlet Control HW Elev.	5,598.00 ft	Control Type	Outlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	Pressure Profile	Depth, Downstream	6.00 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	2.68 ft
Velocity Downstream	10.14 ft/s	Critical Slope	0.010243 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,598.00 ft	Upstream Velocity Head	1.60 ft
Ke	0.50	Entrance Loss	0.80 ft

Inlet Control Properties

Inlet Control HW Elev.	5,595.09 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 10ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,599.00 ft	Headwater Depth/Height	3.33
Computed Headwater Elev:	5,599.00 ft	Discharge	<u>73.83 cfs</u>
Inlet Control HW Elev.	5,595.34 ft	Tailwater Elevation	5,593.70 ft
Outlet Control HW Elev.	5,599.00 ft	Control Type	Outlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	Pressure Profile	Depth, Downstream	6.70 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	2.71 ft
Velocity Downstream	10.44 ft/s	Critical Slope	0.010769 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,599.00 ft	Upstream Velocity Head	1.70 ft
Ke	0.50	Entrance Loss	0.85 ft

Inlet Control Properties

Inlet Control HW Elev.	5,595.34 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 11ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,600.00 ft	Headwater Depth/Height	3.67
Computed Headwater Elev:	5,600.00 ft	Discharge	<u>76.56 cfs</u>
Inlet Control HW Elev.	5,595.67 ft	Tailwater Elevation	5,594.30 ft
Outlet Control HW Elev.	5,600.00 ft	Control Type	Outlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	Pressure Profile	Depth, Downstream	7.30 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	2.74 ft
Velocity Downstream	10.83 ft/s	Critical Slope	0.011492 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,600.00 ft	Upstream Velocity Head	1.82 ft
Ke	0.50	Entrance Loss	0.91 ft

Inlet Control Properties

Inlet Control HW Elev.	5,595.67 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 12ft

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,601.00 ft	Headwater Depth/Height	4.00
Computed Headwater Elev:	5,601.00 ft	<u>Discharge</u>	<u>78.55 cfs</u>
Inlet Control HW Elev.	5,595.91 ft	Tailwater Elevation	5,595.00 ft
Outlet Control HW Elev.	5,601.00 ft	Control Type	Outlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	PressureProfile	Depth, Downstream	8.00 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	2.76 ft
Velocity Downstream	11.11 ft/s	Critical Slope	0.012049 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,601.00 ft	Upstream Velocity Head	1.92 ft
Ke	0.50	Entrance Loss	0.96 ft

Inlet Control Properties

Inlet Control HW Elev.	5,595.91 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Culvert Calculator Report HW 13ft

olve For: Discharge

Culvert Summary

Allowable HW Elevation	5,602.00 ft	Headwater Depth/Height	4.33
Computed Headwater Elev:	5,602.00 ft	Discharge	80.49 cfs
Inlet Control HW Elev.	5,596.16 ft	Tailwater Elevation	5,595.70 ft
Outlet Control HW Elev.	5,602.00 ft	Control Type	Outlet Control

Grades

Upstream Invert	5,589.00 ft	Downstream Invert	5,587.00 ft
Length	225.00 ft	Constructed Slope	0.008889 ft/ft

Hydraulic Profile

Profile	PressureProfile	Depth, Downstream	8.70 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	2.77 ft
Velocity Downstream	11.39 ft/s	Critical Slope	0.012618 ft/ft

Section

Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	3.00 ft
Section Size	36 inch	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,602.00 ft	Upstream Velocity Head	2.02 ft
Ke	0.50	Entrance Loss	1.01 ft

Inlet Control Properties

Inlet Control HW Elev.	5,596.16 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	7.1 ft ²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

Proposed or Possible Detention Ponds

3. 19th Ave. Dam (West Branch at west side of Unser Blvd.) –

19th Ave. Dam - Conceptual Design (Conceptual Level Grading Plan)
(prepared by Smith Engineering Company, July 2013)

Table - 19th Ave. Dam - Elevation – Volume – Discharge Data and Computations
(computed by Smith Engineering Company, July 2013)

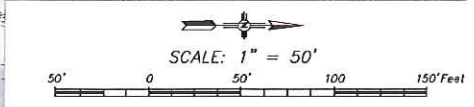
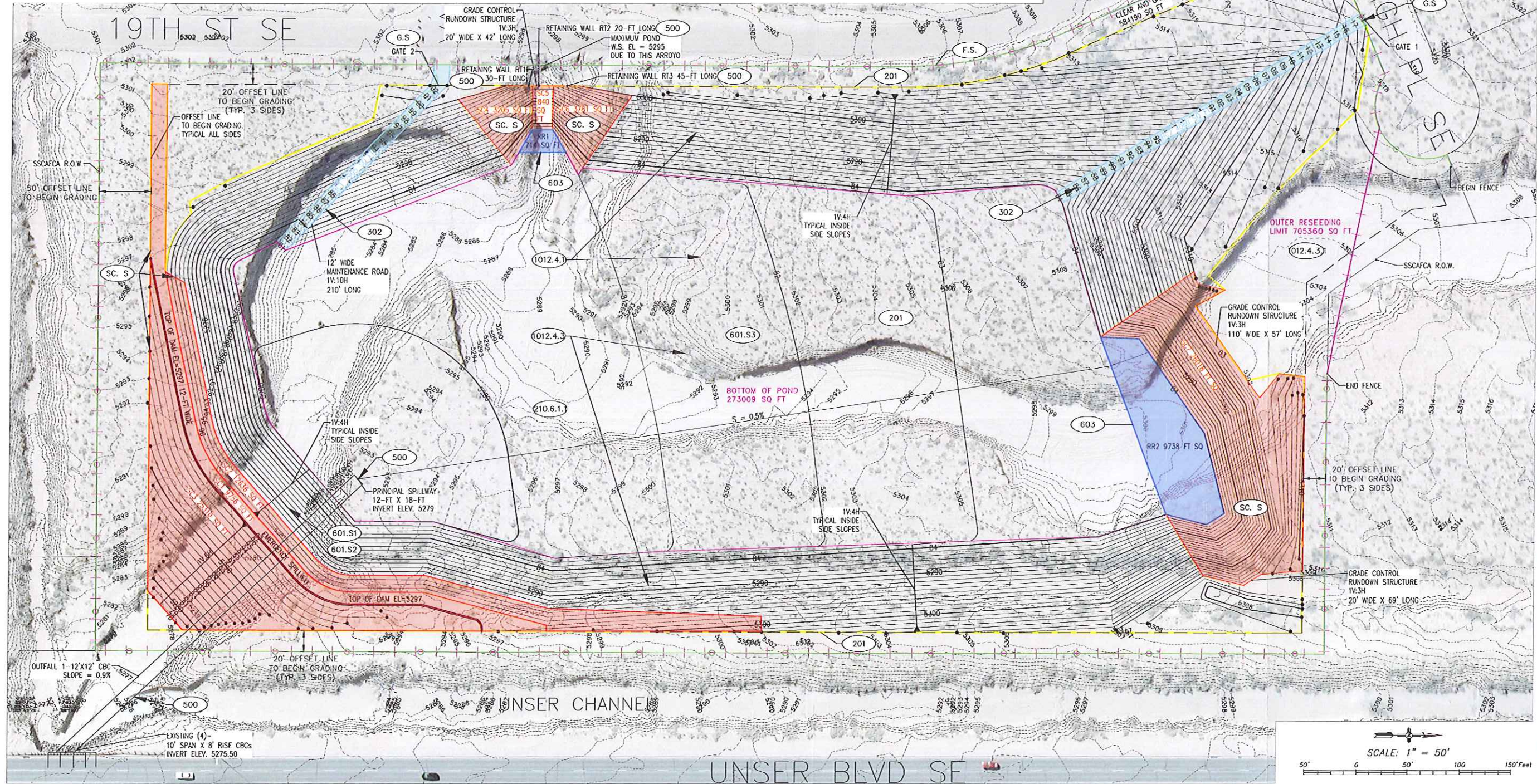
LEGEND

- THREE STRAND NON-BARB WIRE FENCE
- SEEDING LIMIT
- CLEAR AND GRUB
- RIP RAP-TYPE M 2-FT THICK
- BASE COURSE 6-IN THICK
- SOIL CEMENT 1-FT THICK X 8-FT WIDE FOR 1V:4H AND 1V:6H SLOPE AND 6-FT WIDE FOR 1V:3H SLOPES, STAGGERED OVERLAPPED LAYERS TO ACHIEVE SLOPES.

BUILD/PAY NOTES

- 201 CLEARING & GRUBBING: Comp.
- 210.6.1.1 ROUGH GRADING: Pond bottom area and areas outside the top of pond cut slopes, and outside the top of dam slopes. Finished grades shall match plan grades or contours within 0.5 ft. Comp.
- 302 AGGREGATE BASE COURSE: Install 6-inch thick within areas shown on plans. O.P.
- 500 REINFORCED CONCRETE STRUCTURES: Colored reinforced concrete (4,000 psi) including all rebar, principal spillway and concrete boxculvert. C.P.
- 601.S1 SELECT BACKFILL MATERIAL: The Keyway Trench subgrade clay layer. All materials, the clay material, proper soil, and clay/soil mixing to obtain gradation, and subgrade preparation are included with this item. C.P.
- 601.S2 FILL SOIL: Fill soil material for dam embankment when obtained from within the limits of construction, includes blending / mixing to obtain homogenous material / construction in lifts, rough & final grading of dam embankment slopes. C.P.
- 601.S3 UNCLASSIFIED EXCAVATION: Dispose of excess soils off-site to SSCAFCA designated location within 6 mi radius, compact on not required. Comp.
- 603 R/R-RAP: Type M R/R-Rap (Std. Spec. Sect on 109 Table 109A) Install 2 feet thick within areas shown on plans. Assume filter fabric is incidental to r/r-rap. C.P.
- 1012.4.1 NATIVE SEEDS: All disturbed areas including pond bottom and pond side slopes, C.P.
- 1012.4.3 SANTA FE BROWN GRAVEL MULCH: All disturbed areas including pond bottom and pond side slopes, C.P.
- G.S Gate: Install 12 ft. square tube drainage gate. O.P.
- F.S FENCING: Install 5 strand barbed wood post fence. C.P.
- SC.S SOIL CEMENT: Includes all materials (portland cement, native soil) labor, equipment, and placement in 4-foot thick lifts. O.P.

- CS.S CONSTRUCTION STAKING: Includes topographic survey of over excavated surface and final as-built survey preparation, Staking monuments on top of dam. Comp.
- NP.S NPDES PERMITTING: SWPPP preparation, implementation, monitoring, record keeping, including siting fencing (3 ft tall w/ 5-8 steel posts at 10 foot center) and all BMPs including initial installation and maintenance as required. C.P.
- T.S TESTING: Testing and Approval of all Soil Fill, concrete, soil cement, materials, comp.
- PE.S PROFESSIONAL GEOTECHNICAL ENGINEER: Professional Geotechnical Engineer for 2 hours/day during excavation, backfill and compaction of all soils work related to dam and boxculvert construction. Comp.
- MI.S MOBILIZATION
- DM.S DEMOBILIZATION



**PRELIMINARY
NOT FOR
CONSTRUCTION**

PREPARED FOR SSCAFCA

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**ADDENDUM 1
BLACK ARROYO WATERSHED MANAGEMENT PLAN
19TH AVE. POND
CONCEPTUAL DESIGN**

NEW MEXICO TEXAS

JOB NO. 112138
 DATE: June 2013

CS:SEC-PRODUCTS 2012 Project: 112138 SSCAFCA - 1 Black Arroyo (ENGINEERING) CADD PLANSET 19 AVE POND GRADING.dwg Jun 26, 2013 - 8:28am Saved By: Victoria

TABLE
19th Ave. Pond (Proposed) OPTION 6
 Elevation - Volume - Discharge Data and Computations
 grey box means must input data

Contour Elevation NAVD 1988	Depth	Contour Area	Incremental Volume		Cumulative Volume	(A)		(A)		Principal Spillway Outlet 12' X 12' CBC Discharge	Total Principal Spillway / Outfall Pipe Discharge	Emergency Spillway Discharge	Total Discharge Rating Curve	Comment
			(sq ft)	(cu ft)		(ac-ft)	(ac-ft)	1st Row of Reverse Incline Ports Discharge	2nd Row of Reverse Incline Ports Discharge					
(ft)														
(d)														
5279	0	0	0	0.0000	0.0000	0.0	0.0	0.0	0.0	0	0.0	0.0	0	Pond bottom and principal spillway structure invert
5280	1	36.652	18.326	0.4207	0.4207	0.0	0.0	0.0	0.0	27	0.0	0.0	0	Highest Invert - 1st row of reverse incline ports
5281	2	117.745	77.199	1.7722	2.1929	62.0	0.0	0.0	0.0	77	62.0	0.0	62	
5282	3	176.244	146.995	3.3745	5.5675	87.6	0.0	0.0	0.0	141	87.6	0.0	88	Highest Invert - of 2nd row of reverse incline ports
5283	4	234.224	205.234	4.7115	10.2790	107.3	62.0	0.0	0.0	216	169.3	0.0	169	
5284	5	301.658	267.941	6.1511	16.4301	124.0	87.6	0.0	0.0	302	211.6	0.0	212	Top of principal spillway grate
5285	6	311.030	306.344	7.0327	23.4628	138.6	107.3	144.0	144.0	398	389.9	0.0	390	
5286	7	320.502	315.766	7.2490	30.7118	151.8	124.0	407.3	407.3	501	501.0	0.0	501	
5287	8	330.122	325.312	7.4681	38.1799	164.0	138.6	748.2	748.2	612	612.0	0.0	612	
5288	9	339.857	334.989	7.6903	45.8702	175.3	151.8	1,152.0	1,152.0	730	730.0	0.0	730	
5289	10	348.274	344.065	7.8987	53.7689	185.9	164.0	1,610.0	1,610.0	855	855.0	0.0	855	
5290	11	359.680	353.977	8.1262	61.8950	196.0	175.3	2,116.4	2,116.4	987	987.0	0.0	987	
5291	12	369.767	364.723	8.3729	70.2679	205.6	185.9	2,666.9	2,666.9	1125	1,125.0	0.0	1125	
5292	13	379.979	374.873	8.6059	78.8738	214.7	196.0	3,258.3	3,258.3	1288	1,288.0	0.0	1288	
5293	14	390.291	385.135	8.8415	87.7153	223.5	205.6	3,888.0	3,888.0	1417	1,417.0	0.0	1417	
5294	15	400.717	395.504	9.0795	96.7948	231.9	214.7	4,553.7	4,553.7	1572	1,572.0	0.0	1572	
5295	16	411.260	405.989	9.3202	106.1151	240.0	223.5	5,253.5	5,253.5	1731	1,731.0	0.0	1731	
5296	17	421.871	416.566	9.5630	115.6781	247.9	231.9	5,986.0	5,986.0	1896	1,896.0	0.0	1896	
5297	18	432.426	427.149	9.8050	125.4841	255.5	240.0	6,749.6	6,749.6	2007	2,007.0	0.0	2007	Emergency spill. Elev. = lowest top of embankment (f)
5298	19	432.427	432.426	9.9271	135.4112	262.9	247.9	7,543.2	7,543.2	2008	2,008.0	598.0	2606	
5299	20	432.428	432.427	9.9272	145.3384	270.2	255.5	8,365.6	8,365.6	2009	2,009.0	1,691.4	3700	
5300	21	432.429	432.428	9.9272	155.2656	277.2	262.9	9,216.0	9,216.0	2010	2,010.0	3,107.3	5117	

Office equation and coefficient C were obtained from Equation 4-10 and Table 4-3 from "Handbook of Hydraulics" Sixth Edition, by Brater & King, 1976.

$$Q = Ca\sqrt{2gh}$$

$$a = \frac{\pi D^2}{4}$$

(full area formula)

- (a) $C = 0.590$ $g = 32.2 \text{ ft/sec}^2$, $a = \text{area (sq ft)}$ $h = \text{head (ft)}$
- (a) $C = 1.5$ $C = \text{discharge coefficient}$, $L = \text{spillway length perp. to flow (ft)}$, $H = \text{head (ft)}$
- (b) Emergency Spillway $C = 2.6$ $L = 230$ Emer. Spill. Elev. = 5297
- (b) Grate / Weir $C = 3$ $L = 48$ El. 12' X 18' grate Elev. = 5284
- (c) Rating curve obtained from Culvert Master and output is attached
- (d) Data Source : Lidar Contours, provided by SSCAFCA

(e) The combined discharge of the reverse incline ports and the grate (A), will govern the discharge until the principal spillway outfall pipe becomes fully submerged. When the sum of (A)s is greater than outfall pipe capacity then outfall pipe capacity governs the discharge

(b) Weir equation and "C" coefficients were obtained from Equation 5-10 and Table 5-3 from "Handbook of Hydraulics" Sixth Edition, by Brater & King, 1976.

(f) Length assumed along top of pond embankment and elevations extended above emergency spillway to allow for rating curve to function if flow spills over top

Table R**Rating Curve Parameters for 19th Ave Dam Outfall Pipe**

Depth	Upstream Invert Elevation	Headwater Elevation	Downstream Invert Elevation	Tailwater Elevation	Length	Slope	Manning's 'n'	Pipe Size	Pipe Shape	Computed Discharge from Culvert Master for 1 Box Culvert
ft	ft	ft	ft	ft	ft	ft/ft		ft		cfs
	a	b	c	d	a	a				e
0	5279	5279	5275.5	5275.5	375	0.009	0.013	12 X 12	Box	0
1		5280		5276.2						27
2		5281		5276.8						77
3		5282		5277.5						141
4		5283		5278.2						216
5		5284		5278.8						302
6		5285		5279.5						398
7		5286		5280.2						501
8		5287		5280.8						612
9		5288		5281.5						730
10		5289		5282.2						855
11		5290		5282.8						987
12		5291		5283.5						1125
13		5292		5284.2						1268
14		5293		5284.8						1417
15		5294		5285.5						1572
16		5295		5286.2						1731
17		5296		5286.8						1896
18		5297		5287.5						2007

a- Based on SSCAFCA approved conceptual grading plan for 19th Ave Dam

b- Headwater elevation = depth + upstream invert elevation

c- Based on LOMR for West Branch Unser Box Culverts June, 2009

d- Tailwater Elevation Assumption = $(2/3 * \text{depth}) + \text{Downstream Invert Elevation}$

e- Based on Culvert Master calculations- see output in Appendix I

Culvert Calculator Report

1 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,280.00 ft	Headwater Depth/Height	0.08
Computed Headwater Elev.	5,280.00 ft	Discharge	27.05 cfs
Inlet Control HW Elev.	5,279.84 ft	Tailwater Elevation	5,276.20 ft
Outlet Control HW Elev.	5,280.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	0.70 ft
Slope Type	Steep	Normal Depth	0.40 ft
Flow Regime	N/A	Critical Depth	0.54 ft
Velocity Downstream	3.22 ft/s	Critical Slope	0.003392 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,280.00 ft	Upstream Velocity Head	0.27 ft
Ke	0.70	Entrance Loss	0.19 ft

Inlet Control Properties

Inlet Control HW Elev.	5,279.84 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 2 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,281.00 ft	Headwater Depth/Height	0.17
Computed Headwater Elev:	5,281.00 ft	Discharge	76.51 cfs
Inlet Control HW Elev.	5,280.75 ft	Tailwater Elevation	5,276.80 ft
Outlet Control HW Elev.	5,281.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	1.30 ft
Slope Type	Steep	Normal Depth	0.75 ft
Flow Regime	N/A	Critical Depth	1.08 ft
Velocity Downstream	4.90 ft/s	Critical Slope	0.002993 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,281.00 ft	Upstream Velocity Head	0.54 ft
Ke	0.70	Entrance Loss	0.38 ft

Inlet Control Properties

Inlet Control HW Elev.	5,280.75 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

3ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,282.00 ft	Headwater Depth/Height	0.25
Computed Headwater Elev.	5,282.00 ft	Discharge	140.56 cfs
Inlet Control HW Elev.	5,281.66 ft	Tailwater Elevation	5,277.50 ft
Outlet Control HW Elev.	5,282.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	2.00 ft
Slope Type	Steep	Normal Depth	1.11 ft
Flow Regime	N/A	Critical Depth	1.62 ft
Velocity Downstream	5.86 ft/s	Critical Slope	0.002884 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,282.00 ft	Upstream Velocity Head	0.81 ft
Ke	0.70	Entrance Loss	0.57 ft

Inlet Control Properties

Inlet Control HW Elev.	5,281.66 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 4 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,283.00 ft	Headwater Depth/Height	0.33
Computed Headwater Elev.	5,283.00 ft	Discharge	216.40 cfs
Inlet Control HW Elev.	5,282.58 ft	Tailwater Elevation	5,278.20 ft
Outlet Control HW Elev.	5,283.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	2.70 ft
Slope Type	Steep	Normal Depth	1.46 ft
Flow Regime	N/A	Critical Depth	2.16 ft
Velocity Downstream	6.68 ft/s	Critical Slope	0.002871 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,283.00 ft	Upstream Velocity Head	1.08 ft
Ke	0.70	Entrance Loss	0.76 ft

Inlet Control Properties

Inlet Control HW Elev.	5,282.58 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 5 ft HW

olve For: Discharge

Culvert Summary

Allowable HW Elevation	5,284.00 ft	Headwater Depth/Height	0.42
Computed Headwater Elev.	5,284.00 ft	Discharge	302.43 cfs
Inlet Control HW Elev.	5,283.50 ft	Tailwater Elevation	5,278.80 ft
Outlet Control HW Elev.	5,284.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	3.30 ft
Slope Type	Steep	Normal Depth	1.82 ft
Flow Regime	N/A	Critical Depth	2.70 ft
Velocity Downstream	7.64 ft/s	Critical Slope	0.002903 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,284.00 ft	Upstream Velocity Head	1.35 ft
Ke	0.70	Entrance Loss	0.95 ft

Inlet Control Properties

Inlet Control HW Elev.	5,283.50 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 6 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,285.00 ft	Headwater Depth/Height	0.50
Computed Headwater Elev.	5,285.00 ft	Discharge	397.56 cfs
Inlet Control HW Elev.	5,284.43 ft	Tailwater Elevation	5,279.50 ft
Outlet Control HW Elev.	5,285.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	4.00 ft
Slope Type	Steep	Normal Depth	2.19 ft
Flow Regime	N/A	Critical Depth	3.24 ft
Velocity Downstream	8.28 ft/s	Critical Slope	0.002960 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,285.00 ft	Upstream Velocity Head	1.62 ft
Ke	0.70	Entrance Loss	1.14 ft

Inlet Control Properties

Inlet Control HW Elev.	5,284.43 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

7 ft HW

olve For: Discharge

Culvert Summary

Allowable HW Elevation	5,286.00 ft	Headwater Depth/Height	0.58
Computed Headwater Elev:	5,286.00 ft	Discharge	500.98 cfs
Inlet Control HW Elev.	5,285.35 ft	Tailwater Elevation	5,280.20 ft
Outlet Control HW Elev.	5,286.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	4.70 ft
Slope Type	Steep	Normal Depth	2.56 ft
Flow Regime	N/A	Critical Depth	3.78 ft
Velocity Downstream	8.88 ft/s	Critical Slope	0.003033 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,286.00 ft	Upstream Velocity Head	1.89 ft
Ke	0.70	Entrance Loss	1.32 ft

Inlet Control Properties

Inlet Control HW Elev.	5,285.35 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 8 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,287.00 ft	Headwater Depth/Height	0.67
Computed Headwater Elev.	5,287.00 ft	Discharge	612.08 cfs
Inlet Control HW Elev.	5,286.28 ft	Tailwater Elevation	5,280.80 ft
Outlet Control HW Elev.	5,287.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	5.30 ft
Slope Type	Steep	Normal Depth	2.94 ft
Flow Regime	N/A	Critical Depth	4.32 ft
Velocity Downstream	9.62 ft/s	Critical Slope	0.003117 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,287.00 ft	Upstream Velocity Head	2.16 ft
Ke	0.70	Entrance Loss	1.51 ft

Inlet Control Properties

Inlet Control HW Elev.	5,286.28 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 9 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,288.00 ft	Headwater Depth/Height	1.00
Computed Headwater Elev.	5,288.00 ft	Discharge	730.36 cfs
Inlet Control HW Elev.	5,287.27 ft	Tailwater Elevation	5,281.50 ft
Outlet Control HW Elev.	5,288.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	6.00 ft
Slope Type	Steep	Normal Depth	3.32 ft
Flow Regime	N/A	Critical Depth	4.86 ft
Velocity Downstream	10.14 ft/s	Critical Slope	0.003208 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 9 ft	Rise	9.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,288.00 ft	Upstream Velocity Head	2.43 ft
Ke	0.70	Entrance Loss	1.70 ft

Inlet Control Properties

Inlet Control HW Elev.	5,287.27 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	108.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 10 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,289.00 ft	Headwater Depth/Height	0.83
Computed Headwater Elev.	5,289.00 ft	Discharge	855.41 cfs
Inlet Control HW Elev.	5,288.15 ft	Tailwater Elevation	5,282.20 ft
Outlet Control HW Elev.	5,289.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	6.70 ft
Slope Type	Steep	Normal Depth	3.71 ft
Flow Regime	N/A	Critical Depth	5.41 ft
Velocity Downstream	10.64 ft/s	Critical Slope	0.003304 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,289.00 ft	Upstream Velocity Head	2.70 ft
Ke	0.70	Entrance Loss	1.89 ft

Inlet Control Properties

Inlet Control HW Elev.	5,288.15 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

11 ft HW

olve For: Discharge

Culvert Summary

Allowable HW Elevation	5,290.00 ft	Headwater Depth/Height	0.92
Computed Headwater Elev.	5,290.00 ft	Discharge	986.88 cfs
Inlet Control HW Elev.	5,289.08 ft	Tailwater Elevation	5,282.80 ft
Outlet Control HW Elev.	5,290.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	7.30 ft
Slope Type	Steep	Normal Depth	4.11 ft
Flow Regime	N/A	Critical Depth	5.95 ft
Velocity Downstream	11.27 ft/s	Critical Slope	0.003405 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,290.00 ft	Upstream Velocity Head	2.97 ft
Ke	0.70	Entrance Loss	2.08 ft

Inlet Control Properties

Inlet Control HW Elev.	5,289.08 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 12 ft HW

olve For: Discharge

Culvert Summary

Allowable HW Elevation	5,291.00 ft	Headwater Depth/Height	1.00
Computed Headwater Elev:	5,291.00 ft	Discharge	1,124.47 cfs
Inlet Control HW Elev.	5,290.02 ft	Tailwater Elevation	5,283.50 ft
Outlet Control HW Elev.	5,291.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	8.00 ft
Slope Type	Steep	Normal Depth	4.52 ft
Flow Regime	N/A	Critical Depth	6.49 ft
Velocity Downstream	11.71 ft/s	Critical Slope	0.003508 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,291.00 ft	Upstream Velocity Head	3.24 ft
Ke	0.70	Entrance Loss	2.27 ft

Inlet Control Properties

Inlet Control HW Elev.	5,290.02 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

13 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,292.00 ft	Headwater Depth/Height	1.08
Computed Headwater Elev.	5,292.00 ft	Discharge	1,267.92 cfs
Inlet Control HW Elev.	5,290.96 ft	Tailwater Elevation	5,284.20 ft
Outlet Control HW Elev.	5,292.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	8.70 ft
Slope Type	Steep	Normal Depth	4.93 ft
Flow Regime	N/A	Critical Depth	7.03 ft
Velocity Downstream	12.14 ft/s	Critical Slope	0.003615 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,292.00 ft	Upstream Velocity Head	3.51 ft
Ke	0.70	Entrance Loss	2.46 ft

Inlet Control Properties

Inlet Control HW Elev.	5,290.96 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 14 ft HW

olve For: Discharge

Culvert Summary

Allowable HW Elevation	5,293.00 ft	Headwater Depth/Height	1.17
Computed Headwater Elev.	5,293.00 ft	Discharge	1,416.99 cfs
Inlet Control HW Elev.	5,291.90 ft	Tailwater Elevation	5,284.80 ft
Outlet Control HW Elev.	5,293.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	9.30 ft
Slope Type	Steep	Normal Depth	5.35 ft
Flow Regime	N/A	Critical Depth	7.57 ft
Velocity Downstream	12.70 ft/s	Critical Slope	0.003723 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,293.00 ft	Upstream Velocity Head	3.78 ft
Ke	0.70	Entrance Loss	2.65 ft

Inlet Control Properties

Inlet Control HW Elev.	5,291.90 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft ²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

15 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,294.00 ft	Headwater Depth/Height	1.25
Computed Headwater Elev.	5,294.00 ft	Discharge	1,571.50 cfs
Inlet Control HW Elev.	5,292.84 ft	Tailwater Elevation	5,285.50 ft
Outlet Control HW Elev.	5,294.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	10.00 ft
Slope Type	Steep	Normal Depth	5.78 ft
Flow Regime	N/A	Critical Depth	8.11 ft
Velocity Downstream	13.10 ft/s	Critical Slope	0.003833 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,294.00 ft	Upstream Velocity Head	4.05 ft
Ke	0.70	Entrance Loss	2.84 ft

Inlet Control Properties

Inlet Control HW Elev.	5,292.84 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 16 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,295.00 ft	Headwater Depth/Height	1.33
Computed Headwater Elev.	5,295.00 ft	Discharge	1,731.24 cfs
Inlet Control HW Elev.	5,293.78 ft	Tailwater Elevation	5,286.20 ft
Outlet Control HW Elev.	5,295.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	10.70 ft
Slope Type	Steep	Normal Depth	6.21 ft
Flow Regime	N/A	Critical Depth	8.65 ft
Velocity Downstream	13.48 ft/s	Critical Slope	0.003944 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,295.00 ft	Upstream Velocity Head	4.32 ft
Ke	0.70	Entrance Loss	3.03 ft

Inlet Control Properties

Inlet Control HW Elev.	5,293.78 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 17 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,296.00 ft	Headwater Depth/Height	1.42
Computed Headwater Elev:	5,296.00 ft	Discharge	1,896.05 cfs
Inlet Control HW Elev.	5,295.69 ft	Tailwater Elevation	5,286.80 ft
Outlet Control HW Elev.	5,296.00 ft	Control Type	Entrance Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	11.30 ft
Slope Type	Steep	Normal Depth	6.65 ft
Flow Regime	N/A	Critical Depth	9.19 ft
Velocity Downstream	13.98 ft/s	Critical Slope	0.004057 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,296.00 ft	Upstream Velocity Head	4.59 ft
Ke	0.70	Entrance Loss	3.22 ft

Inlet Control Properties

Inlet Control HW Elev.	5,295.69 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report 18 ft HW

Solve For: Discharge

Culvert Summary

Allowable HW Elevation	5,297.00 ft	Headwater Depth/Height	1.50
Computed Headwater Elev.	5,297.00 ft	Discharge	2,006.89 cfs
Inlet Control HW Elev.	5,297.00 ft	Tailwater Elevation	5,287.50 ft
Outlet Control HW Elev.	5,296.66 ft	Control Type	Inlet Control

Grades

Upstream Invert	5,279.00 ft	Downstream Invert	5,275.50 ft
Length	375.00 ft	Constructed Slope	0.009333 ft/ft

Hydraulic Profile

Profile	CompositeS1S2	Depth, Downstream	7.42 ft
Slope Type	Steep	Normal Depth	6.95 ft
Flow Regime	N/A	Critical Depth	9.54 ft
Velocity Downstream	22.54 ft/s	Critical Slope	0.004131 ft/ft

Section

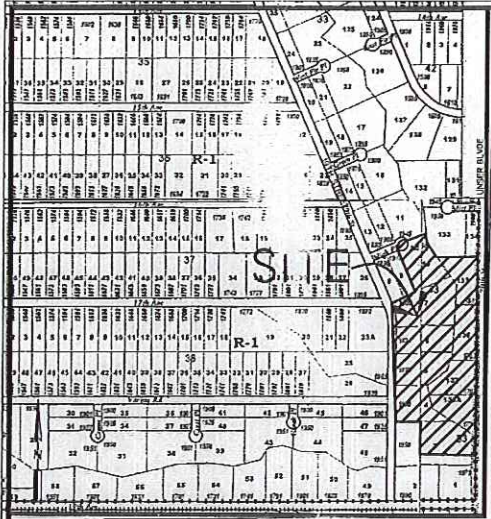
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 12 ft	Rise	12.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	5,296.66 ft	Upstream Velocity Head	4.77 ft
Ke	0.70	Entrance Loss	3.34 ft

Inlet Control Properties

Inlet Control HW Elev.	5,297.00 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	144.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		



VICINITY MAP ZONE AT1 MAP 37 & 38 NOT TO SCALE

- NOTES**
1. BASIS OF BEARINGS FOR THIS SURVEY IS THE VECTORS, INC. GPS REAL TIME NETWORK BEARINGS ARE NEW MEXICO STATE PLANE GRID BEARINGS (CENTR. ZONE, NAD 83); DISTANCES ARE GROUND DISTANCES.
 2. BEARINGS AND DISTANCES SHOWN ON THIS SURVEY IN PARENTHESES () ARE PER THE RIO RANCHO ESTATES UNIT 10 FILED ON MAY 6, 1996, IN BOOK 1, PAGE 73.
 3. BEARING AND DISTANCES SHOWN ON THIS SURVEY IN BRACKETS [] ARE PER THE SUMMARY PLAT OF LOTS 1-A, 3-A, 139-A AND LOT A, RIO RANCHO ESTATES UNIT 10 FILED ON JUNE 17, 1994, PLAT IN BOOK 7, PAGE 44.
 4. DOCUMENTS USED:
 - a. PLAT OF RIO RANCHO ESTATE UNIT 10, FILED ON MAY 6, 1996, IN BOOK 1, PAGE 73.
 - b. SUMMARY PLAT OF LOTS 1-A, 3-A, 139-A AND LOT A, BLOCK 33, RIO RANCHO ESTATES UNIT 10, FILED JUNE 17, 1994, IN BOOK 7, PAGE 49.
 - c. SUMMARY PLAT OF LOTS 1-A-1 AND 2-A, BLOCK 33, RIO RANCHO ESTATES UNIT 10, CREATED BY COMMUNITY SCIENCES CORPORATION, OCTOBER, 2008.
 - d. PLAT OF LOT A 19TH AVENUE DAM RIO RANCHO ESTATES UNIT 1 FILED MAY 24, 2011, IN BOOK 3, PAGE 3378.

CONSENT STATEMENT
 The undersigned owners and proprietors of the properties represented herein do hereby certify and affirm that this replat is created with our free will and consent in accordance with our expressed wishes and desires, and do hereby grant new Public Utility Easements and vacate existing drainage and utility easements and lot lines as shown herein.

of Charles Thomas 12-20-11 Date
 CHARLES THOMAS
 S.S.C.A.F.C.A. EXECUTIVE ENGINEER

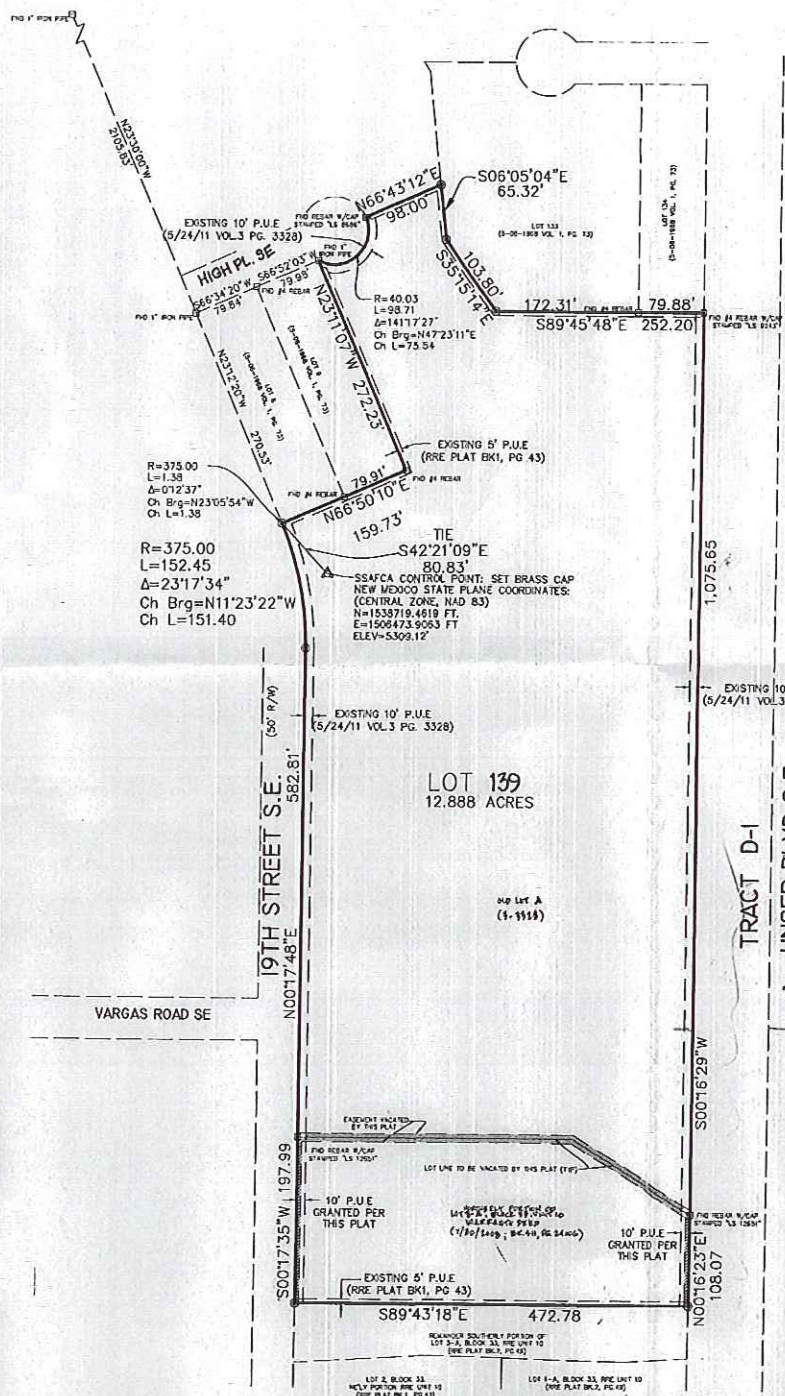
ACKNOWLEDGEMENT
 State of New Mexico)
 County of Sandoval)
 This instrument was acknowledged before me this 10th day of December, 2011.
 by: Charles Thomas
Thomas W. Patrick
 Notary Public
 My Commission Expires: 10-06-2014

JURISDICTIONAL AFFIDAVIT:
 I, THOMAS W. PATRICK, NEW MEXICO PROFESSIONAL SURVEYOR NO. 12651, HEREBY AFFIRM THAT THE PROPERTY DESCRIBED DOES LIE WITHIN THE PLATTING AND SUBDIVISION JURISDICTION OF THE CITY OF RIO RANCHO.
Thomas W. Patrick 12-20-2011 DATE
 THOMAS W. PATRICK
 NEW MEXICO PROFESSIONAL SURVEYOR NO. 12651

SURVEYOR'S CERTIFICATION:
 I, THOMAS W. PATRICK, NEW MEXICO PROFESSIONAL SURVEYOR NO. 12651, HEREBY CERTIFY THAT THIS PLAT WAS PREPARED FROM AN ACTUAL GROUND SURVEY PERFORMED BY ME OR UNDER MY SUPERVISION, THAT I AM RESPONSIBLE FOR THIS PLAT AND THAT THIS PLAT IS TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. THIS PLAT CONFORMS TO THE MINIMUM STANDARDS FOR SURVEYING IN NEW MEXICO AS ADOPTED BY THE NEW MEXICO BOARD OF REGISTRATION FOR PROFESSIONAL ENGINEERS AND SURVEYORS AND TO THE CITY OF RIO RANCHO SUBDIVISION ORDINANCE.
Thomas W. Patrick 12-20-2011 DATE
 THOMAS W. PATRICK
 NEW MEXICO PROFESSIONAL SURVEYOR NO. 12651

SUBJECT PROPERTY DESCRIPTION
 LOT A, RIO RANCHO ESTATE UNIT 10, AS THE SAME ARE SHOWN AND DESIGNATED ON THE PLAT THEREOF FILED IN THE OFFICE OF THE COUNTY CLERK OF SANDOVAL COUNTY, NEW MEXICO, ON MAY 24, 2011, PLAT BOOK 3, PAGE 3378, AND THAT NORTHERLY PORTION OF LOT 3-A, BLOCK 33 RIO RANCHO ESTATES, AS THE SAME IS SHOWN AND DESIGNATED ON THE PLAT THEREOF FILED IN THE OFFICE OF THE COUNTY CLERK OF SANDOVAL COUNTY, NEW MEXICO ON JUNE 17, 1994, PLAT BOOK 7, PAGE 49, SAID NORTHERLY PORTION BEING CONVEYED TO ESCAFCA BY WARRANTY DEED RECORDED JULY 30, 2008 IN BK.411, PG.2406.
 CONTAINS 12.888 ACRES, MORE OR LESS.

DISCLOSURE STATEMENT:
 THE PURPOSE OF THIS PLAT IS TO COMBINE 2 EXISTING LOTS INTO ONE NEW LOT, TO GRANT NEW PUBLIC UTILITY EASEMENT AND TO VACATE EXISTING DRAINAGE AND UTILITY EASEMENTS AND EXISTING LOT LINES AS SHOWN HEREON.



MONUMENT LEGEND
 □ FOUND MONUMENT AS NOTED
 ● SET IS REBAR W/2" ALUMINUM CAP STAMPED "CSO P512651"

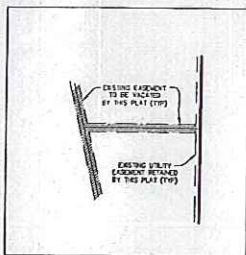
PUBLIC UTILITY EASEMENTS
 PUBLIC UTILITY EASEMENTS shown on this plat are granted for the common and joint use of:
 1. **New Mexico Gas Company** for installation, maintenance and service of natural gas lines, valves and other equipment and facilities reasonably necessary to provide natural gas.
 2. **Public Service Company of New Mexico** for the installation, maintenance, and service of overhead and underground electrical lines, transformers, and other equipment, fixtures, structures and related facilities reasonably necessary to provide electrical service.
 3. **Qwest** for installation, maintenance and service of all buried and aerial communication lines and other related equipment and facilities reasonably necessary to provide communication services, including but not limited to above ground pedestals and closures.
 4. **Cable TV** for installation, maintenance and service of such lines, cable and other related equipment and facilities reasonably necessary to provide Cable TV service.
 Included is the right to build, rebuild, construct, reconstruct, locate, relocate, change, remove, modify, renew, operate and maintain facilities for the purposes described above, together with free access to, from, and over said right of way and easement, with the right and privilege of going upon, over and across adjoining lands of Grantor for the purposes set forth herein and with the right to utilize the right of way and easement to extend services to customers of Grantor, and to trim and remove trees, shrubs or bushes which interfere with the purposes set forth herein. No building, sign, pool (above ground or subsurface), hot tub, concrete or wood pool decking, or other structure shall be erected or constructed on said easements, nor shall any well be drilled or operated thereon.
Disclaimer:
 In approving this plat, the utility companies did not conduct a Title Search of the properties shown hereon. Consequently, the utility companies do not waive or release any easement or easement rights which may have been granted by prior plat, replat or other document and which are not shown on this plat.

New Mexico Gas Company Easement Release Approval
 New Mexico Gas Company, Inc., a Delaware corporation, does hereby release, waive, quitclaim and discharge its right, title and interest in the easement(s) (granted by prior plat, replat or document) shown to be vacated on this plat.
 New Mexico Gas Company
 By: [Signature]
 State of New Mexico
 County of Bernalillo
 This instrument was acknowledged before me on DECEMBER 15, 2011.

My Commission Expires: 03-25-2013
OFFICIAL SEAL
 Brandon Kaufman
 NOTARY PUBLIC
 STATE OF NEW MEXICO
 My Commission Expires: 04-01-2012

STATE OF NEW MEXICO) SS.
 COUNTY OF SANDOVAL)
 THIS INSTRUMENT WAS FILED FOR RECORD ON THIS 16th day of February, 2012 AT 12:33 P.M.
 RECORDED IN VOLUME 3, FOLIO 422 OF RECORDS OF SANDOVAL COUNTY.
[Signature]
 COUNTY CLERK AND RECORDER
 BY: [Signature]

TYPICAL UTILITY EASEMENT VACATION/RETENTION DETAIL



SUMMARY PLAT
 OF
LOT 139
S.S.C.A.F.C.A. 19TH AVENUE DAM
RIO RANCHO ESTATES UNIT 10
 BEING A REPLAT OF
 LOT A AND THE NORTHERLY PORTION OF LOT 3-A, BLOCK 33
 RIO RANCHO ESTATES, UNIT 10
 SITUATE WITHIN
 TOWN OF ALAMEDA GRANT
 CITY OF RIO RANCHO
 SANDOVAL COUNTY, NEW MEXICO
 SEPTEMBER, 2011

SITE DATA

CASE NUMBERS	12-200-00004
FEMA MAP NO.	35043C2102 D
FLOOD ZONE DESIGNATION	ZONE "X"
ZONING	R-1
MILES OF DEDICATED RIGHT OF WAY CREATED	NONE
NO. OF EXISTING LOTS	2
NO. OF LOTS CREATED	1
TOTAL AREA	12.888 ACRES
ACREAGE OF DEDICATED RIGHT-OF-WAY	N/A
PROPOSED LAND USE	R-1

UTILITY APPROVALS

Fernando Vigil 12-14-11 DATE
 PNM ELECTRIC SERVICES

[Signature] 12-15-2011 DATE
 NEW MEXICO GAS COMPANY

Chad Sims 12-15-11 DATE
 CABLEONE

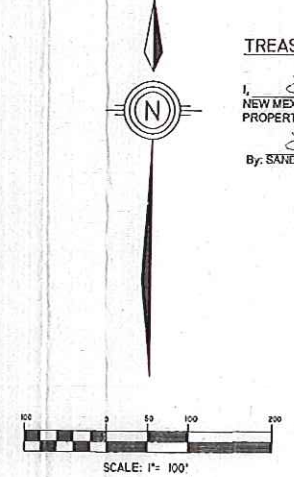
Wilaheli Ramoel 12-14-10 DATE
 QWEST CORPORATION DBS CENTUR LINK QC

Debbie Stork 2-13-12 DATE
 CITY OF RIO RANCHO

RIO RANCHO DEVELOPMENT SERVICES DEPARTMENT
 APPROVED THIS 13 DAY OF FEBRUARY, 2011.
[Signature]
 DIRECTOR

CITY CLERKS CERTIFICATE
 I, ROMAN MONTOYA, CITY CLERK OF THE CITY OF RIO RANCHO, NEW MEXICO DO HEREBY CERTIFY THAT THE PLAT SHOWN HEREON WAS APPROVED ADMINISTRATIVELY BY THE CITY OF RIO RANCHO DEVELOPMENT SERVICES DEPARTMENT DIRECTOR ON THIS 14th DAY OF February, 2012.
 By: [Signature]

TREASURER'S CERTIFICATE
 I, Jannine Dominguez TREASURER OF SANDOVAL COUNTY, NEW MEXICO DO HEREBY CERTIFY THAT THE PREVIOUS TEN (10) YEARS PROPERTY TAXES HAVE BEEN PAID IN FULL.
 By: Jannine Dominguez 2/16/12 DATE
 SANDOVAL COUNTY TREASURER



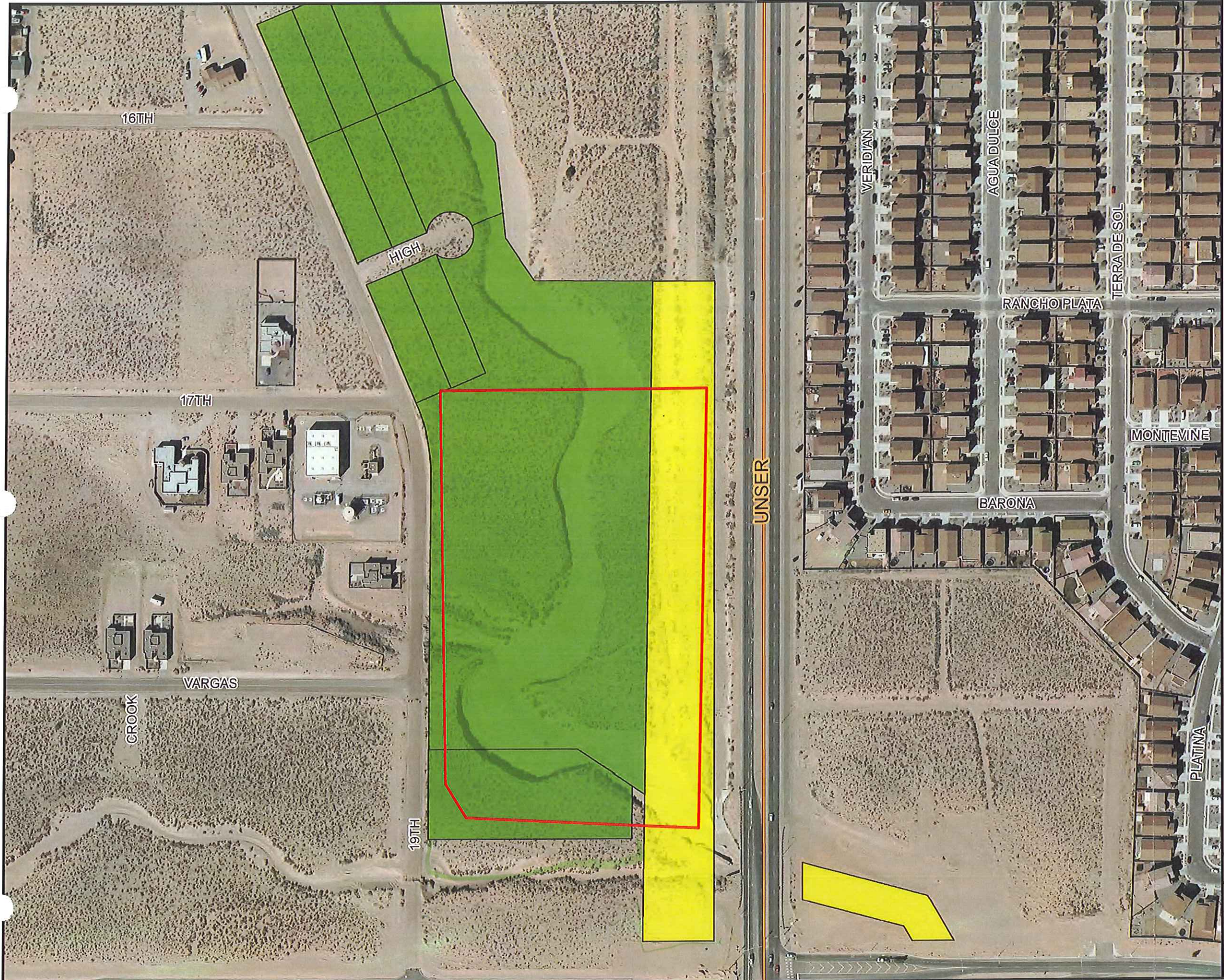
SHEET 1 OF 1

SUMMARY PLAT
LOT 139
19TH AVENUE DAM
RIO RANCHO ESTATES UNIT 10

DATE: 09/29/11
 SCALE: 1" = 100'
 DRAWN: SUN/TWP
 CHECKED: SUN/TWP
 FILE NO: 12337-04-600

LAND PLANNING
 P.O. Box 1328
 Corral, N.M. 87048
 (505) 997-0000

community sciences corporation



Legend

- SSCAFCA Fee Simple
- SSCAFCA Easement



1 inch = 200 feet

ROW



Southern Sandoval County
Arroyo Flood Control Authority

Date: November 2012

Figure 1 of 1

HEC-HMS Output for

Existing Conditions

Detention Pond Routings

Project: Tp Model
Simulation Run: Run 1 Reservoir: Wallen Pond
Start of Run: 01Nov2012, 09:00 Basin Model: Existing Conditions
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:11:25 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	18.6 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:30
Peak Outflow :	1.0 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:09
Total Inflow :	0.5685 (AC-FT)	Peak Storage :	0.4589 (AC-FT)
Total Outflow :	0.5676 (AC-FT)	Peak Elevation :	5657.12 (FT)

Project: Tp Model

Simulation Run: Run 1 Reservoir: Sunset Pond

Start of Run:	01Nov2012, 09:00	Basin Model:	Existing Conditions
End of Run:	02Nov2012, 09:00	Meteorologic Model:	100yr-24hr
Compute Time:	30May2013, 14:11:25	Control Specifications:	Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	296.8 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:36
Peak Outflow :	34.6 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:21
Total Inflow :	15.1475 (AC-FT)	Peak Storage :	9.2063 (AC-FT)
Total Outflow :	15.1470 (AC-FT)	Peak Elevation :	5617.06 (FT)

Project: Tp Model

Simulation Run: Run 1 Reservoir: Sugar Ridge Pond

Start of Run:	01Nov2012, 09:00	Basin Model:	Existing Conditions
End of Run:	02Nov2012, 09:00	Meteorologic Model:	100yr-24hr
Compute Time:	30May2013, 14:11:25	Control Specifications:	Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	105.2 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:30
Peak Outflow :	93.8 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 10:36
Total Inflow :	5.1478 (AC-FT)	Peak Storage :	1.2368 (AC-FT)
Total Outflow :	4.6488 (AC-FT)	Peak Elevation :	5567.36 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: Wexford Pond

Start of Run: 01Nov2012, 09:00 Basin Model: Existing Conditions
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:11:25 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	368.3 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:36
Peak Outflow :	135.3 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:06
Total Inflow :	27.7897 (AC-FT)	Peak Storage :	9.2655 (AC-FT)
Total Outflow :	27.7879 (AC-FT)	Peak Elevation :	40.04 (FT)

Project: Tp Model

Simulation Run: Run 1 Reservoir: Gateway Pond

Start of Run:	01Nov2012, 09:00	Basin Model:	Existing Conditions
End of Run:	02Nov2012, 09:00	Meteorologic Model:	100yr-24hr
Compute Time:	30May2013, 14:11:25	Control Specifications:	Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	503.4 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:33
Peak Outflow :	264.5 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 10:45
Total Inflow :	19.3400 (AC-FT)	Peak Storage :	6.4103 (AC-FT)
Total Outflow :	19.3330 (AC-FT)	Peak Elevation :	5267.34 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: Tract 17 Pond

Start of Run: 01Nov2012, 09:00 Basin Model: Existing Conditions
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:11:25 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	620.0 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:39
Peak Outflow :	403.6 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 10:54
Total Inflow :	45.5576 (AC-FT)	Peak Storage :	10.5393 (AC-FT)
Total Outflow :	44.3973 (AC-FT)	Peak Elevation :	5274.79 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: Stonebridge Pond

Start of Run: 01Nov2012, 09:00 Basin Model: Existing Conditions
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:11:25 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	150.1 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:33
Peak Outflow :	29.3 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:06
Total Inflow :	7.7799 (AC-FT)	Peak Storage :	3.9985 (AC-FT)
Total Outflow :	7.7509 (AC-FT)	Peak Elevation :	5249.86 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: BLACK DAM → *
Start of Run: 01Nov2012, 09:00 Basin Model: Existing Conditions
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 21Aug2013, 17:34:49 Control Specifications: Control 1
Volume Units: AC-FT

Computed Results

Peak Inflow :	8539.2 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:48
Peak Outflow :	3045.2 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:24
Total Inflow :	709.3905 (AC-FT)	Peak Storage :	286.6820 (AC-FT)
Total Outflow :	708.1810 (AC-FT)	Peak Elevation :	5165.61 (FT)

Project: Tp Model
Simulation Run: Run 1 Sink: 19th Ave. Ret. Pond

Start of Run: 01Nov2012, 09:00 Basin Model: Existing Conditions
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:11:25 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Outflow : 691.9 (CFS) Date/Time of Peak Outflow : 01Nov2012, 10:39
Total Outflow : 43.9782 (AC-FT)

HEC-HMS Output for

DEVEX Conditions

Detention Pond Routings

Project: Tp Model
Simulation Run: Run 1 Reservoir: Sunset Pond

Start of Run: 01Nov2012, 09:00 Basin Model: DEVE~~X~~
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:13:17 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	349.4 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:36
Peak Outflow :	36.5 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:21
Total Inflow :	20.3148 (AC-FT)	Peak Storage :	11.8589 (AC-FT)
Total Outflow :	20.3244 (AC-FT)	Peak Elevation :	5618.35 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: Wallen Pond

Start of Run: 01Nov2012, 09:00 Basin Model: DEVE
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:13:17 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	31.5 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:30
Peak Outflow :	1.5 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:12
Total Inflow :	1.3603 (AC-FT)	Peak Storage :	0.9634 (AC-FT)
Total Outflow :	1.3537 (AC-FT)	Peak Elevation :	5658.41 (FT)

Project: Tp Model

Simulation Run: Run 1 Reservoir: Sugar Ridge Pond

Start of Run:	01Nov2012, 09:00	Basin Model:	DEVEX
End of Run:	02Nov2012, 09:00	Meteorologic Model:	100yr-24hr
Compute Time:	30May2013, 14:13:17	Control Specifications:	Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	130.9 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:33
Peak Outflow :	119.6 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 10:36
Total Inflow :	5.2215 (AC-FT)	Peak Storage :	1.3191 (AC-FT)
Total Outflow :	4.7223 (AC-FT)	Peak Elevation :	5567.61 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: Wexford Pond

Start of Run:	01Nov2012, 09:00	Basin Model:	DEVEX
End of Run:	02Nov2012, 09:00	Meteorologic Model:	100yr-24hr
Compute Time:	30May2013, 14:13:17	Control Specifications:	Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	368.3 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:36
Peak Outflow :	135.2 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:06
Total Inflow :	27.6672 (AC-FT)	Peak Storage :	9.2614 (AC-FT)
Total Outflow :	27.6653 (AC-FT)	Peak Elevation :	40.03 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: Tract 17 Pond

Start of Run: 01Nov2012, 09:00 Basin Model: DEVE~~X~~
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:13:17 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	683.5 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:36
Peak Outflow :	420.1 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 10:54
Total Inflow :	50.7490 (AC-FT)	Peak Storage :	12.1417 (AC-FT)
Total Outflow :	49.5170 (AC-FT)	Peak Elevation :	5275.52 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: Gateway Pond

Start of Run: 01Nov2012, 09:00 Basin Model: DEVE
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:13:17 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	783.1 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:33
Peak Outflow :	345.3 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 10:51
Total Inflow :	42.8537 (AC-FT)	Peak Storage :	12.8145 (AC-FT)
Total Outflow :	42.8100 (AC-FT)	Peak Elevation :	5269.16 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: Stonebridge Pond

Start of Run: 01Nov2012, 09:00 Basin Model: DEVE
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 14:13:17 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	161.3 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:33
Peak Outflow :	49.1 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 10:57
Total Inflow :	8.7817 (AC-FT)	Peak Storage :	4.2745 (AC-FT)
Total Outflow :	8.7462 (AC-FT)	Peak Elevation :	5250.04 (FT)

Project: Tp Model
Simulation Run: Run 1 Reservoir: BLACK DAM

Start of Run: 01Nov2012, 09:00 Basin Model: DEVE~~X~~
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 21Aug2013, 17:09:05 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	9863.6 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:48
Peak Outflow :	4649.3 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:15
Total Inflow :	867.4591 (AC-FT)	Peak Storage :	328.3439 (AC-FT)
Total Outflow :	865.7380 (AC-FT)	Peak Elevation :	5167.33 (FT)

HEC-HMS Output for

Ultimate Conditions

Detention Pond Routings

Project: Tp Model
Simulation Run: 100yr-24hr Reservoir: LISBON

Start of Run: 01Nov2012, 09:00 Basin Model: Ultimate 3
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 16:19:00 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	754.8 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:39
Peak Outflow :	73.9 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:27
Total Inflow :	41.8619 (AC-FT)	Peak Storage :	27.7657 (AC-FT)
Total Outflow :	41.1739 (AC-FT)	Peak Elevation :	5598.96 (FT)

Project: Tp Model
Simulation Run: 500yr-24hr Reservoir: LISBON

Start of Run: 01Nov2012, 09:00 Basin Model: Ultimate 3
End of Run: 02Nov2012, 09:00 Meteorologic Model: 500yr-24hr
Compute Time: 30May2013, 16:19:35 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	1088.7 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:39
Peak Outflow :	221.8 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:15
Total Inflow :	58.7775 (AC-FT)	Peak Storage :	39.5777 (AC-FT)
Total Outflow :	58.0762 (AC-FT)	Peak Elevation :	5601.65 (FT)

Project: Tp Model
Simulation Run: 100yr-24hr Reservoir: SUGAR POND

Start of Run:	01Nov2012, 09:00	Basin Model:	Ultimate 3
End of Run:	02Nov2012, 09:00	Meteorologic Model:	100yr-24hr
Compute Time:	30May2013, 16:19:00	Control Specifications:	Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	121.8 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:33
Peak Outflow :	37.2 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 10:54
Total Inflow :	6.9582 (AC-FT)	Peak Storage :	2.6549 (AC-FT)
Total Outflow :	6.8791 (AC-FT)	Peak Elevation :	5640.39 (FT)

Project: Tp Model
Simulation Run: 500yr-24hr Reservoir: SUGAR POND

Start of Run: 01Nov2012, 09:00 Basin Model: Ultimate 3
End of Run: 02Nov2012, 09:00 Meteorologic Model: 500yr-24hr
Compute Time: 30May2013, 16:19:35 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	170.1 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:33
Peak Outflow :	42.1 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:00
Total Inflow :	9.6154 (AC-FT)	Peak Storage :	4.1769 (AC-FT)
Total Outflow :	9.5310 (AC-FT)	Peak Elevation :	5642.03 (FT)

Project: Tp Model
Simulation Run: 100yr-24hr Reservoir: 19th Ave Pond

Start of Run: 01Nov2012, 09:00 Basin Model: Ultimate 3
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 30May2013, 16:19:00 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	3407.8 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:48
Peak Outflow :	1499.3 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:12
Total Inflow :	288.4143 (AC-FT)	Peak Storage :	92.5388 (AC-FT)
Total Outflow :	287.5536 (AC-FT)	Peak Elevation :	5293.53 (FT)

Project: Tp Model
Simulation Run: 500yr-24hr Reservoir: 19th Ave Pond

Start of Run: 01Nov2012, 09:00 Basin Model: Ultimate 3
End of Run: 02Nov2012, 09:00 Meteorologic Model: 500yr-24hr
Compute Time: 30May2013, 16:19:35 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	4983.4 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:45
Peak Outflow :	2421.4 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:09
Total Inflow :	401.4429 (AC-FT)	Peak Storage :	132.3510 (AC-FT)
Total Outflow :	400.5521 (AC-FT)	Peak Elevation :	5297.69 (FT)

Project: Tp Model
Simulation Run: 100yr-24hr Reservoir: BLACK DAM

Start of Run: 01Nov2012, 09:00 Basin Model: Ultimate 3
End of Run: 02Nov2012, 09:00 Meteorologic Model: 100yr-24hr
Compute Time: 21Aug2013, 17:14:42 Control Specifications: Control 1

Volume Units: AC-FT

Computed Results

Peak Inflow :	6923.0 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:45
Peak Outflow :	2955.6 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:30
Total Inflow :	865.8519 (AC-FT)	Peak Storage :	265.8398 (AC-FT)
Total Outflow :	864.1184 (AC-FT)	Peak Elevation :	5164.73 (FT)

Project: Tp Model

Simulation Run: 500yr-24hr Reservoir: BLACK DAM

Start of Run: 01Nov2012, 09:00

Basin Model:

Ultimate.3

End of Run: 02Nov2012, 09:00

Meteorologic Model:

500yr-24hr

Compute Time: 21Aug2013, 17:15:18

Control Specifications:

Control 1

Volume Units:

AC-FT

Computed Results

Peak Inflow :	9497.5 (CFS)	Date/Time of Peak Inflow :	01Nov2012, 10:45
Peak Outflow :	5685.9 (CFS)	Date/Time of Peak Outflow :	01Nov2012, 11:18
Total Inflow :	1156.2996 (AC-FT)	Peak Storage :	345.4586 (AC-FT)
Total Outflow :	1154.4623 (AC-FT)	Peak Elevation :	5168.02 (FT)