



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

March 26, 2001

Lyle Losack, PE
Community Sciences Corporation
PO Box 1328
Corrales, NM 87048

Re: Fineland Development Drainage Report
Engineer's Stamp dated 2-19-00, (A11/D1E)

Dear Mr. Losack,

Based on information contained in your submittal dated 2-20-01, the above referenced plan cannot be approved for Site Development Plan for Subdivision, Preliminary Plat or Final Plat until all downstream easements are recorded since the location of the easement may affect your drainage plan. In addition, the infrastructure required in the Ridgeview project must be financially guaranteed in order to grant the bulk land variance.

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham
Bradley L. Bingham, PE
Sr. Engineer, Hydrology

C: file



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

October 9, 2000

Dr. Jeffrey L. Fine, PhD CEDS, Fineland, LLC
401 West End Avenue
New York, New York 10024

SUBJECT: FINELAND DEVELOPMENT
EPC Case No: Z-98-31-1

Dear Dr. Fine:

This letter of agreement pertains solely to the 40-acre parcel commonly referred to as the Fineland Development adjoining McMahon Boulevard between Unser Boulevard and Bandelier Drive in North West Albuquerque. As you are aware, the City is pursuing the improvement of McMahon Boulevard from Golf Course Road through the intersection of Unser Boulevard. Although such improvements, including the dedication of rights-of-way is a standard requirement of the development process, the City is willing to agree to construct the ultimate roadway section of McMahon at our expense if the right-of-way is dedicated. In this case, since you have already initiated the development process by the preparation of a bulk land plat, we are proposing the acceleration of the filing of that plat in exchange for construction of the roadway.

In pursuit of a timely extension to McMahon Boulevard, the City agrees to exempt the Fineland Development of all roadway and roadway related storm drainage costs (including sidewalks, bike trails, bike lanes, streetscaping, and street lighting) associated with McMahon Boulevard that might normally be attached as a condition of the development of your property. In consideration of this wavier, you the developer, agree to file immediately with the City, a bulk land plat conveying a 156-foot wide right-of-way for McMahon Boulevard through the Fineland Development. The filing of the bulk land plat with the City's Development Review Board shall occur within 30 calendar days of your acknowledgement and agreement with this proposal.

Please acknowledge your acceptance below and return this letter to Mr. Ed Adams of my staff at the following address:

Mr. Ed Adams, Manager
Public Works Department
Transportation Division
P.O. Box 1293
Albuquerque, New Mexico 87103

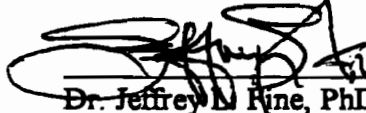
PAGE 2

Should you have any questions or comments regarding this proposal, I can be reached at 505-768-3650.

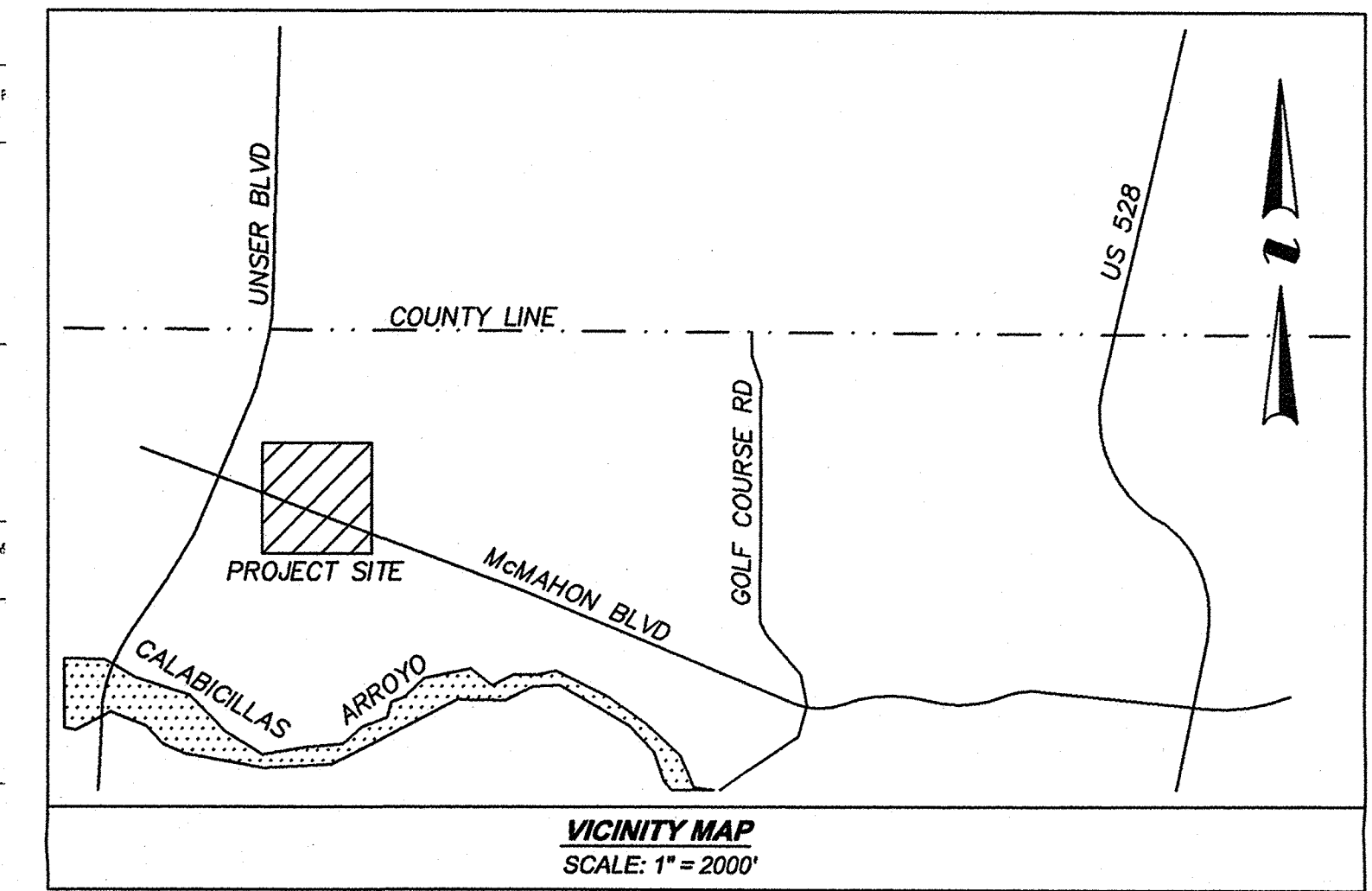
Thank you for your cooperation on this matter.

Sincerely,


Larry L. Blair, Director
Public Works Department

 Date: 10/17/00
Dr. Jeffrey M. Fine, PhD CEDS, Fineland, LLC

- c: Alan B. Armijo, City Councilor, District 1
Lawrence Rael, Chief Administrative Officer
John R. Castillo, Assistant Public Works Director
Ed Adams, Transportation Division Manager
Annette Baca, Transportation Division
Richard Dourte, Development Services, PWD
Community Sciences



GENERAL NOTES:
LEGAL DESCRIPTION: NE1/4, SE1/4, SEC. 2, T11N, R2E, NMPM
SITE AREA: 40.06 ACRES
BENCHMARK: USGS BRASS CAP "SANDBERN", ELEVATION=5456.92

LEGEND
FLOW DIRECTION
EXISTING BASIN ID
100 YR. STORM
PROPOSED SITE BOUNDARY
MASTER DRAIN BASIN BOUNDARY

SCALE: 1" = 100'

FINELAND BASINS (EXISTING)									
BASIN	AREA SQ. FT.	AREA SQ. MI.	%A	%B	%C	%D	Q ₁₀₀ cfs*	V ₁₀₀ AC FT.*	
EA1	189961.97	0.0068	95	5	0	0	5.80	0.163	
EA2.1	120174.79	0.0043	95	5	0	0	3.67	0.103	
EA2.2	45501.75	0.0016	95	5	0	0	1.37	0.038	
EA2	165682.54	0.0059	-	-	-	-	5.04	0.141	
EA3.1	96858.37	0.0035	95	5	0	0	2.99	0.084	
EA3.2	28168.80	0.0010	95	5	0	0	0.86	0.024	
EA3	125027.17	0.0045	-	-	-	-	3.85	0.108	
EA	480665.68	0.0172	-	-	-	-	14.69	0.412	
EB1.1	131184.44	0.0047	95	5	0	0	4.01	0.113	
EB1.2	200498.77	0.0072	95	5	0	0	6.14	0.172	
EB1.3	127107.89	0.0046	95	5	0	0	3.93	0.110	
EB	458791.10	0.0165	-	-	-	-	14.08	0.395	
EC1	124553.95	0.0045	95	5	0	0	3.84	0.108	
EC2.1	262056.96	0.0094	95	5	0	0	3.93	0.110	
EC2.2	133512.98	0.0048	95	5	0	0	4.10	0.115	
EC2.3	122840.67	0.0044	95	5	0	0	3.76	0.105	
EC2	459123.37	0.0165	-	-	-	-	17.86	0.388	
EC3.1	89287.01	0.0032	95	5	0	0	2.73	0.077	
EC3.2	76434.14	0.0027	95	5	0	0	2.31	0.065	
EC3.3	56168.08	0.0020	95	5	0	0	1.71	0.048	
EC3	221889.23	0.0079	-	-	-	-	6.75	0.190	
EC	805566.55	0.0311	-	-	-	-	24.61	0.686	
OFFSITE BASINS (EXISTING)									
ED1	430019.96	0.0088	95	5	0	0	7.33	0.206	
ED2	239938.74	0.0154	95	5	0	0	13.13	0.369	
ED3	137718.54	0.0049	0	0	10	90	13.25	0.488	
ED4	77912.93	0.0028	0	0	10	90	7.58	0.279	
ED	885590.17	0.0317	-	-	-	-	41.29	1.342	

*COMMERCIAL BASINS TO BE PONDED TO HISTORIC RATES.



FINELAND DEVELOPEMENT
Bulkland Plat
Existing Drainage Map

community sciences corporation

LAND PLANNING ENGINEERING SURVEYING

DATE: 12/2000
SCALE: AS Shown
DESIGNED: LCL
DRAWN: PJM
JOB NO: 448-01-030

DATE: 12/2000
SCALE: AS Shown
DESIGNED: LCL
DRAWN: PJM
JOB NO: 448-01-030

SHEET
1
2

**FINAL
DRAINAGE REPORT
FOR
FINELAND DEVELOPMENT**

Prepared For:

**Fineland Development
401 West End Ave.
New York, NY 10024
Ph: 212-724-8025
Fax: same as above**

Prepared By:

**Community Sciences Corporation
PO Box 1328
Corrales, NM 87048
Ph: 505-897-0000
Fax: 505-897-5195
Job: N291-33-130**



Lyle C. Losack P.E.
Lyle C. Losack, PE
2/19/01

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1. Purpose and Scope

This parcel is now proposed as a bulk land plat to facilitate the development of the parcel in accordance with the present land plan, and to provide the required corridor for McMahon Blvd. The approximate 40-acre parcel is also in accordance with the recommendation of the Unser/McMahon Village Center Plan.

The planned development consist of three major tracts; Parcels A, B, & E – Commercial and Office (SU1 for C1), Parcel E & F – Multi-Family Residential (SU1 for R-2); and Parcel C – Single-Family Residential (R-LT). The property is bisected by the future construction of McMahon Boulevard.

This report presents an overall Drainage Management and Conceptual Grading Plan for Approval by the City of Albuquerque in order that the subsequent subdivision and development may proceed.

2. Site Description/ Existing Drainage Conditions

The Fineland Development is located east of the Unser Blvd and McMahon Blvd intersection. It is bounded by the Stonebridge Subdivision on the east, Tuscan Ridge Subdivision on the south, with undeveloped lands to the north and west, and bisected by the McMahon Boulevard corridor. In addition, no existing offsite flows impact this site. However, there are some combined flows along the west side to be negotiated.

The natural drainage divide between the Arroyo de las Calabacillas and Black Arroyo meanders. See Plate E1 of 1.

The FEMA Floodway Boundary and Floodway Map dated September 20, 1996 (panel no. 35001C104) shows the site to be outside Flood Hazard Zone (500-year floodway).

3. Design Criteria

The drainage plan presented in this report has been prepared in accordance with the City of Albuquerque Drainage Ordinances and Chapter 22 of the Development Process Manual (DPM).

The hydrological analysis is based on the 100-year frequency, 6-hour duration storm, as represented in Section 22, Part A, Hydrology, of the "Development Process Manual. Storage ponds are to be sized for the 100-year, 24-hour storm per the DPM.

Rainfall intensities per this report are as follows:

Zone 1	P ₆₀	P ₃₆₀	P ₁₄₄₀
1	1.87	2.20	2.66

LAND TREATMENT

Residential (DPM-Eqn a-4, pg 22-n)

$$N = \text{Resident Units/ Acre} = 63 \text{ (DU's est.)}/10.53 = 5.98$$

$$D = 7 * \text{SQ RT} [(n)(n) + 5(n)] = 7 * \text{SQ RT} [(5.98)(5.98) + 5(5.98)]$$

$$= 56.73 \Rightarrow \text{use } 57 \%$$

(similar to multi-family)

Treatment Type	A	B	C	D
Residential	0	15	22	57
Commercial	0	0	10	90
McMahon Corridor	0	0	10	90
Multi Family	0	15	15	70

4. DRAINAGE MANAGEMENT PLAN

The drainage is to be broken into three parts; residential, commercial, and multi-family.

The residential parcel is to be graded to the NE corner where it is proposed to accumulate in street flows and additional drop inlets be provided for these flows at the intersection of Crooked Creek Ave. and Stonebridge Drive in the Stone Bridge Subdivision. Initially, approximately 20.4 cfs was planned for this area per the Stonebridge drainage report. As the calculations now show, 37.51 cfs is required, a 17.11 cfs increase. Two additional inlets will capture this increase.

With the surge pond downstream from this, the extended time to peak, and street

capacity available, the additional flows will have no impact on the present system (See Plate U1 of 1).

The multi-family parcel is to be accumulated and routed southeast along McMahon Blvd to a 36" outfall provided by the Tuscan Ridge Unit 2 construction. The Tuscan Ridge Unit 2 drainage report restricted flows to 24.0 cfs from the multi-family and commercial lots combined south of the McMahon corridor. The combined developed flows will be 73.59 cfs. An increase of 49.59 cfs which will result in a required storage pond volume of 1.976 AC.-FT. for the 100 year – 6 hour storm. Pond sized to carry the 100 year – 24 hour storm.

The commercial parcel north of the McMahon corridor is proposed to be ponded until development downstream can provide for a storm drain outlet. Additional developed flows beyond historic flows are to be ponded and throttled to historic levels. Per the proposed Ridgeview subdivision drainage plan a 24" storm drain carrying 25.4 cfs is allocated for the Fineland and Smith Properties.

5. Conclusion

Per the overall drainage management plan for this area, no downstream impact will result from this bulk land plat. When development of these parcels proceed, detailed drainage plans will still be required for approval by the city of Albuquerque. The City may at this time utilize the proposed drainage plan, or modify it to accommodate ongoing master drainage planning in this area.


```
*
*
*FINELAND
*100 YEAR EXISTING CONDITIONS
*****
TIME=0.0 HR PUNCH CODE=0 PRINT LINES=-6
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RAIN DAY=2.66 IN DT=0.0333 HRS
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ID=5 CODE=1
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*****
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* PRINT HYD
* ID=18 CODE=1
* *****
* COMPUTE NM HYD
* ID=19 HYD NO=ED2 DA=0.0086 SQ MI
* *****

```

```
*
PRINT HYD
*
COMPUTE NM HYD

PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1
*****
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*****
ID=20 HYD NO=ED3 DA=0.0049 SQ MI
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TP=-0.1333 HR MASS RAIN=-1
*****
ID=20 CODE=1
*****
ID=21 HYD NO=ED4 DA=0.0028 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
*****
ID=21 CODE=1
PRINT HYD
FINISH
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- VERSION: 1997.02c

RUN DATE (MON/DAY/YR) = 02/19/2001
USER NO. = AHYMO-I-9702c01000Q29-AH

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1	NOTATION
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RAINFALL	TYPE= 1										
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COMPUTE NM HYD	EA2.2	-	3	.00160	1.37	.038	.44896	1.532	1.337 PER IMP=		.00
COMPUTE NM HYD	EA3.1	-	4	.00350	2.99	.084	.44896	1.532	1.334 PER IMP=		.00
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COMPUTE NM HYD	EC2.2	-	11	.00480	4.10	.115	.44896	1.532	1.333 PER IMP=		.00
COMPUTE NM HYD	EC2.3	-	12	.00440	3.76	.105	.44896	1.532	1.334 PER IMP=		.00
COMPUTE NM HYD	EC3.1	-	13	.00320	2.73	.077	.44896	1.532	1.334 PER IMP=		.00
COMPUTE NM HYD	EC3.2	-	14	.00270	2.31	.065	.44896	1.532	1.335 PER IMP=		.00
COMPUTE NM HYD	EC3.3	-	15	.00200	1.71	.048	.44896	1.532	1.336 PER IMP=		.00
COMPUTE NM HYD	ED1	-	18	.01540	13.13	.369	.44896	1.532	1.332 PER IMP=		.00
COMPUTE NM HYD	ED2	-	19	.00860	7.33	.206	.44896	1.532	1.333 PER IMP=		.00
COMPUTE NM HYD	ED3	-	20	.00490	13.25	.488	1.86834	1.499	4.226 PER IMP=		90.00
COMPUTE NM HYD	ED4	-	21	.00280	7.58	.279	1.86834	1.499	4.230 PER IMP=		90.00
FINISH											

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- Version: 1997.02c

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*
*
*
*
*FINELAND
*100 YEAR EXISTING CONDITIONS
*****
TIME=0.0 HR PUNCH CODE=0 PRINT LINES=-6
TYPE=1 RAIN QUARTER=0.0
RAIN ONE=1.87 IN RAIN SIX=2.2 IN
RAIN DAY=2.66 IN DT=0.033 HRS
*****
START
RAINFALL

```

COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.
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0.000	0.016	0.033	0.050	0.067	0.085	0.103
0.021	0.140	0.160	0.136	0.200	0.221	0.243
0.065	0.288	0.312	0.330	0.387	0.414	0.436
0.042	0.471	0.501	0.533	0.566	0.600	0.636
0.0674	0.714	0.757	0.808	0.863	0.922	1.044
1.1323	1.754	2.374	3.221	4.335	5.756	7.527
0.9690	1.1767	1.2619	1.3336	1.3972	1.4551	1.5088
1.15579	1.6041	1.6474	1.6881	1.7266	1.7629	1.7973
1.18298	1.8607	1.8900	1.9178	1.9442	1.9515	1.9573
1.19627	1.9680	1.9729	1.9777	1.9823	1.9867	1.9909
1.19950	1.9990	2.0029	2.0066	2.0102	2.0137	2.0172
2.0205	2.0238	2.0269	2.0300	2.0331	2.0360	2.0389
2.0418	2.0446	2.0473	2.0500	2.0526	2.0552	2.0578
2.0603	2.0627	2.0651	2.0675	2.0698	2.0721	2.0744
2.0766	2.0788	2.0810	2.0832	2.0853	2.0873	2.0894
2.0914	2.0934	2.0954	2.0974	2.0993	2.1012	2.1031
2.1050	2.1068	2.1086	2.1104	2.1122	2.1140	2.1157
2.1174	2.1191	2.1208	2.1225	2.1242	2.1258	2.1274
2.1290	2.1306	2.1322	2.1338	2.1353	2.1369	2.1384
2.1399	2.1414	2.1429	2.1444	2.1459	2.1473	2.1487
2.1502	2.1516	2.1530	2.1544	2.1558	2.1571	2.1585
2.1599	2.1612	2.1625	2.1639	2.1652	2.1665	2.1678
2.1691	2.1703	2.1716	2.1729	2.1741	2.1754	2.1766
2.1778	2.1791	2.1803	2.1815	2.1827	2.1839	2.1850
2.1862	2.1874	2.1886	2.1897	2.1909	2.1920	2.1931
2.1943	2.1954	2.1965	2.1976	2.1987	2.1998	2.2009

```

*****
*
*      COMPUTE NM HYD
*      ID=1 HYD NO=EAL DA=0.0068 SQ MI
*      PER A=95 PER B=5 PER C=0 PER D=0
*      TP=0.1333 HR MASS RAIN=-1
*****

```

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 14.067 CFS UNIT VOLUME = .9987 B = 275.76 P60 = 1.8700
AREA = .006800 SQ MI IA = .64350 INCHES INF = 1.64900 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*

PRINT HYD ID=1 CODE=1

HYDROGRAPH FROM AREA EA1

RUNOFF VOLUME = .44896 INCHES = .1628 ACRE-FEET
PEAK DISCHARGE RATE = 5.80 CFS AT 1.532 HOURS BASIN AREA = .0068 SQ. MI.

*

COMPUTE NM HYD ID=2 HYD NO=EA2.1 DA=0.0043 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 8.8954 CFS UNIT VOLUME = .9981 B = 275.76 P60 = 1.8700
AREA = .004300 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*

PRINT HYD ID=2 CODE=1

HYDROGRAPH FROM AREA EA2.1

RUNOFF VOLUME = .44896 INCHES = .1030 ACRE-FEET
PEAK DISCHARGE RATE = 3.67 CFS AT 1.532 HOURS BASIN AREA = .0043 SQ. MI.

*

COMPUTE NM HYD ID=3 HYD NO=EA2.2 DA=0.0016 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 3.3099 CFS UNIT VOLUME = .9954 B = 275.76 P60 = 1.8700
AREA = .001600 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*

PRINT HYD ID=3 CODE=1

HYDROGRAPH FROM AREA EA2.2

RUNOFF VOLUME = .44896 INCHES = .0383 ACRE-FEET
PEAK DISCHARGE RATE = 1.37 CFS AT 1.532 HOURS BASIN AREA = .0016 SQ. MI.

```

*
*****
COMPUTE NM HYD
ID=4 HYD NO=EA3.1 DA=0.0035 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 7.2404 CFS UNIT VOLUME = .9977 B = 275.76 P60 = 1.8700
AREA = .003500 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD
ID=4 CODE=1

HYDROGRAPH FROM AREA EA3.1

RUNOFF VOLUME = .44896 INCHES = .0838 ACRE-FEET
PEAK DISCHARGE RATE = 2.99 CFS AT 1.532 HOURS BASIN AREA = .0035 SQ. MI.

*
*****
COMPUTE NM HYD
ID=5 HYD NO=EA3.2 DA=0.0010 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 2.0687 CFS UNIT VOLUME = .9928 B = 275.76 P60 = 1.8700
AREA = .001000 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD
ID=5 CODE=1

HYDROGRAPH FROM AREA EA3.2

RUNOFF VOLUME = .44896 INCHES = .0239 ACRE-FEET
PEAK DISCHARGE RATE = .86 CFS AT 1.532 HOURS BASIN AREA = .0010 SQ. MI.

*
*****
COMPUTE NM HYD
ID=6 HYD NO=EB1.1 DA=0.0047 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 9.7229 CFS UNIT VOLUME = .9982 B = 275.76 P60 = 1.8700
AREA = .004700 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

```

```
*
*****
PRINT HYD
ID=6 CODE=1

HYDROGRAPH FROM AREA EB1.1

RUNOFF VOLUME = .44896 INCHES = .1125 ACRE-FEET
PEAK DISCHARGE RATE = 4.01 CFS AT 1.532 HOURS BASIN AREA = .0047 SQ. MI.

*
*****
COMPUTE NM HYD
ID=7 HYD NO=EB1.2 DA=0.0072 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 14.895 CFS UNIT VOLUME = .9988 B = 275.76 P60 = 1.8700
AREA = .007200 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD
ID=7 CODE=1

HYDROGRAPH FROM AREA EB1.2

RUNOFF VOLUME = .44896 INCHES = .1724 ACRE-FEET
PEAK DISCHARGE RATE = 6.14 CFS AT 1.532 HOURS BASIN AREA = .0072 SQ. MI.

*
*****
COMPUTE NM HYD
ID=8 HYD NO=EB1.3 DA=0.0046 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 9.5160 CFS UNIT VOLUME = .9982 B = 275.76 P60 = 1.8700
AREA = .004600 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD
ID=8 CODE=1

HYDROGRAPH FROM AREA EB1.3

RUNOFF VOLUME = .44896 INCHES = .1101 ACRE-FEET
PEAK DISCHARGE RATE = 3.93 CFS AT 1.532 HOURS BASIN AREA = .0046 SQ. MI.
```

```

*
* COMPUTE NM HYD
* *****
ID=9 HYD NO=EC1 DA=0.0045 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 9.3091 CFS UNIT VOLUME = .9982 B = 275.76 P60 = 1.8700
AREA = .004500 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
* PRINT HYD
* *****
ID=9 CODE=1

HYDROGRAPH FROM AREA EC1

RUNOFF VOLUME = .44896 INCHES = .1078 ACRE-FEET
PEAK DISCHARGE RATE = 3.84 CFS AT 1.532 HOURS BASIN AREA = .0045 SQ. MI.

*
* COMPUTE NM HYD
* *****
ID=10 HYD NO=EC2.1 DA=0.0094 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 19.446 CFS UNIT VOLUME = .9989 B = 275.76 P60 = 1.8700
AREA = .009400 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
* PRINT HYD
* *****
ID=10 CODE=1

HYDROGRAPH FROM AREA EC2.1

RUNOFF VOLUME = .44896 INCHES = .2251 ACRE-FEET
PEAK DISCHARGE RATE = 8.02 CFS AT 1.532 HOURS BASIN AREA = .0094 SQ. MI.

*
* COMPUTE NM HYD
* *****
ID=11 HYD NO=EC2.2 DA=0.0048 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 9.9297 CFS UNIT VOLUME = .9983 B = 275.76 P60 = 1.8700
AREA = .004800 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300
```

```
*
*****
PRINT HYD
ID=11 CODE=1

HYDROGRAPH FROM AREA EC2.2

RUNOFF VOLUME = .44896 INCHES = .1149 ACRE-FEET
PEAK DISCHARGE RATE = 4.10 CFS AT 1.532 HOURS BASIN AREA = .0048 SQ. MI.

*
*****
COMPUTE NM HYD
ID=12 HYD NO=EC2.3 DA=0.0044 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 9.1023 CFS UNIT VOLUME = .9981 B = 275.76 P60 = 1.8700
AREA = .004400 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD
ID=12 CODE=1

HYDROGRAPH FROM AREA EC2.3

RUNOFF VOLUME = .44896 INCHES = .1054 ACRE-FEET
PEAK DISCHARGE RATE = 3.76 CFS AT 1.532 HOURS BASIN AREA = .0044 SQ. MI.

*
*****
COMPUTE NM HYD
ID=13 HYD NO=EC3.1 DA=0.0032 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 6.6198 CFS UNIT VOLUME = .9976 B = 275.76 P60 = 1.8700
AREA = .003200 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD
ID=13 CODE=1

HYDROGRAPH FROM AREA EC3.1

RUNOFF VOLUME = .44896 INCHES = .0766 ACRE-FEET
PEAK DISCHARGE RATE = 2.73 CFS AT 1.532 HOURS BASIN AREA = .0032 SQ. MI.
```

*

COMPUTE NM HYD
ID=14 HYD NO=EC3.2 DA=0.0027 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 5.5855 CFS UNIT VOLUME = .9971 B = 275.76 P60 = 1.8700
AREA = .002700 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*

PRINT HYD
ID=14 CODE=1

HYDROGRAPH FROM AREA EC3.2

RUNOFF VOLUME = .44896 INCHES = .0647 ACRE-FEET
PEAK DISCHARGE RATE = 2.31 CFS AT 1.532 HOURS BASIN AREA = .0027 SQ. MI.

*

COMPUTE NM HYD
ID=15 HYD NO=EC3.3 DA=0.0020 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 4.1374 CFS UNIT VOLUME = .9962 B = 275.76 P60 = 1.8700
AREA = .002000 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*

PRINT HYD
ID=15 CODE=1

HYDROGRAPH FROM AREA EC3.3

RUNOFF VOLUME = .44896 INCHES = .0479 ACRE-FEET
PEAK DISCHARGE RATE = 1.71 CFS AT 1.532 HOURS BASIN AREA = .0020 SQ. MI.

*

COMPUTE NM HYD
ID=18 HYD NO=ED1 DA=0.0154 SQ MI
PER A=95 PER B=5 PER C=0 PER D=0
TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
UNIT PEAK = 31.858 CFS UNIT VOLUME = .9993 B = 275.76 P60 = 1.8700
AREA = .015400 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*

PRINT HYD ID=18 CODE=1

HYDROGRAPH FROM AREA ED1

RUNOFF VOLUME = .44896 INCHES = .3687 ACRE-FEET
 PEAK DISCHARGE RATE = 13.13 CFS AT 1.532 HOURS BASIN AREA = .0154 SQ. MI.

*
 COMPUTE NM HYD
 ID=19 HYD NO=ED2 DA=0.0086 SQ MI
 PER A=95 PER B=5 PER C=0 PER D=0
 TP=-0.1333 HR MASS RAIN=-1

K = .162049HR TP = .133300HR K/TP RATIO = 1.215673 SHAPE CONSTANT, N = 2.926304
 UNIT PEAK = 17.791 CFS UNIT VOLUME = .9989 B = 275.76 P60 = 1.8700
 AREA = .008600 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
 PRINT HYD ID=19 CODE=1

HYDROGRAPH FROM AREA ED2

RUNOFF VOLUME = .44896 INCHES = .2059 ACRE-FEET
 PEAK DISCHARGE RATE = 7.33 CFS AT 1.532 HOURS BASIN AREA = .0086 SQ. MI.

*
 COMPUTE NM HYD
 ID=20 HYD NO=ED3 DA=0.0049 SQ MI
 PER A=0 PER B=0 PER C=10 PER D=90
 TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 17.411 CFS UNIT VOLUME = .9987 B = 526.28 P60 = 1.8700
 AREA = .004410 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
 PRINT HYD ID=20 CODE=1

HYDROGRAPH FROM AREA ED3

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
 UNIT PEAK = 1.4268 CFS UNIT VOLUME = .9917 B = 388.14 P60 = 1.8700
 AREA = .000490 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

RUNOFF VOLUME = 1.86834 INCHES = .4883 ACRE-FEET
PEAK DISCHARGE RATE = 13.25 CFS AT 1.499 HOURS BASIN AREA = .0049 SQ. MI.

*

COMPUTE NM HYD
ID=21 HYD NO=ED4 DA=0.0028 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 9.9491 CFS UNIT VOLUME = .9982 B = 526.28 P60 = 1.8700
AREA = .002520 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = .81530 CFS UNIT VOLUME = .9840 B = 388.14 P60 = 1.8700
AREA = .000280 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*

PRINT HYD
ID=21 CODE=1

HYDROGRAPH FROM AREA ED4

RUNOFF VOLUME = 1.86834 INCHES = .2790 ACRE-FEET
PEAK DISCHARGE RATE = 7.58 CFS AT 1.499 HOURS BASIN AREA = .0028 SQ. MI.

FINISH

NORMAL PROGRAM FINISH
END TIME (HR:MIN:SEC) = 15:59:18

```
*****
* *FINELAND
* *100 YEAR DEVELOPED CONDITIONS
* *****
START TIME=0.0 HR PUNCH CODE=0 PRINT LINES=-6
RAINFALL TYPE=1 RAIN QUARTER=0.0
RAIN ONE=1.87 IN RAIN SIX=2.2 IN
RAIN DAY=2.66 IN DT=0.0333 HRS
* *****
* COMPUTE NM HYD ID=1 HYD N0=DAl DA=0.0068 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=1 CODE=1
* *****
* COMPUTE NM HYD ID=2 HYD N0=DA2 DA=0.0059 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=2 CODE=1
* *****
* COMPUTE NM HYD ID=3 HYD N0=DA3 DA=0.0045 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=3 CODE=1
* *****
* COMPUTE NM HYD ID=4 HYD N0=DB DA=0.0165 SQ MI
PER A=0 PER B=20 PER C=23 PER D=57
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=4 CODE=1
* *****
* COMPUTE NM HYD ID=5 HYD N0=DC1 DA=0.0045 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=5 CODE=1
* *****
* COMPUTE NM HYD ID=6 HYD N0=DC2 DA=0.0164
PER A=0 PER B=15 PER C=15 PER D=70
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=6 CODE=1
* *****
* COMPUTE NM HYD ID=7 HYD N0=DC3 DA=0.0080
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=7 CODE=1
* *****
* COMPUTE NM HYD ID=8 HYD N0=DD1 DA=0.0086 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=8 CODE=1
* *****
* COMPUTE NM HYD ID=9 HYD N0=DD2 DA=0.0154 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=9 CODE=1
* *****
* COMPUTE NM HYD ID=10 HYD N0=DD3 DA=0.0049
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=10 CODE=1
* *****
* COMPUTE NM HYD ID=11 HYD N0=DD4 DA=0.0028
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1
* *****
* PRINT HYD ID=11 CODE=1
FINISH
```

□(s16-67h8-5v0T□&1&D

AHYMO PROGRAM (AHYMO_97) -

- Version: 1997.02c

RUN DATE (MON/DAY/YR) = 12/15/2000

START TIME (HR:MIN:SEC) = 08:55:20

USER NO. = AHYMO-I-9702c01000429-AH

INPUT FILE = F:\N448\01\030\100PROP6.DAT

```

* *****
* *FINELAND
* *100 YEAR DEVELOPED CONDITIONS
* *****
START TIME=0.0 HR PUNCH CODE=0 PRINT LINES=-6
RAINFALL TYPE=1 RAIN QUARTER=0.0
RAIN ONE=1.87 IN RAIN SIX=2.2 IN
RAIN DAY=2.66 IN DT=0.0333 HRS

```

COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.
DT = .033300 HOURS END TIME = 5.994000 HOURS

.0000	.0016	.0033	.0050	.0067	.0085	.0103
.0121	.0140	.0160	.0180	.0200	.0221	.0243
.0265	.0288	.0312	.0336	.0361	.0387	.0414
.0442	.0471	.0501	.0533	.0566	.0600	.0636
.0674	.0714	.0757	.0808	.0863	.0922	.1044
.1323	.1754	.2374	.3221	.4335	.5756	.7527
.9690	1.1767	1.2619	1.3336	1.3972	1.4551	1.5084
1.5579	1.6041	1.6474	1.6881	1.7266	1.7629	1.7973
1.8298	1.8607	1.8900	1.9178	1.9442	1.9515	1.9573
1.9627	1.9680	1.9729	1.9777	1.9823	1.9867	1.9909
1.9950	1.9990	2.0029	2.0066	2.0102	2.0137	2.0172
2.0205	2.0238	2.0269	2.0300	2.0331	2.0360	2.0389
2.0418	2.0446	2.0473	2.0500	2.0526	2.0552	2.0578
2.0603	2.0627	2.0651	2.0675	2.0698	2.0721	2.0744
2.0766	2.0788	2.0810	2.0832	2.0853	2.0873	2.0894
2.0914	2.0934	2.0954	2.0974	2.0993	2.1012	2.1031
2.1050	2.1068	2.1086	2.1104	2.1122	2.1140	2.1157
2.1174	2.1191	2.1208	2.1225	2.1242	2.1258	2.1274
2.1290	2.1306	2.1322	2.1338	2.1353	2.1369	2.1384
2.1399	2.1414	2.1429	2.1444	2.1459	2.1473	2.1487
2.1502	2.1516	2.1530	2.1544	2.1558	2.1571	2.1585
2.1599	2.1612	2.1625	2.1639	2.1652	2.1665	2.1678
2.1691	2.1703	2.1716	2.1729	2.1741	2.1754	2.1766
2.1778	2.1791	2.1803	2.1815	2.1827	2.1839	2.1850
2.1862	2.1874	2.1886	2.1897	2.1909	2.1920	2.1931
2.1943	2.1954	2.1965	2.1976	2.1987	2.1998	

```

* *****
* COMPUTE NM HYD ID=1 HYD NO=DA1 DA=0.0068 SQ MI
* PER A=0 PER B=0 PER C=10 PER D=90
* TP=-0.1333 HR MASS RAIN=-1

```

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 24.162 CFS UNIT VOLUME = .9989 B = 526.28 P60 = 1.8700
AREA = .006120 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = 1.9800 CFS UNIT VOLUME = .9941 B = 388.14 P60 = 1.8700
AREA = .000680 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

```

* *****
* PRINT HYD ID=1 CODE=1

```

HYDROGRAPH FROM AREA DA1

RUNOFF VOLUME = 1.86834 INCHES = .6776 ACRE-FEET
PEAK DISCHARGE RATE = 18.38 CFS AT 1.499 HOURS BASIN AREA = .0068 SQ. MI.

```

* *****
* COMPUTE NM HYD ID=2 HYD NO=DA2 DA=.0059 SQ MI
* PER A=0 PER B=0 PER C=10 PER D=90
* TP=-0.1333 HR MASS RAIN=-1

```

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 20.964 CFS UNIT VOLUME = .9988 B = 526.28 P60 = 1.8700
AREA = .005310 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = 1.7180 CFS UNIT VOLUME = .9926 B = 388.14 P60 = 1.8700
AREA = .000590 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR

```

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD ID=2 CODE=1

HYDROGRAPH FROM AREA DA2

RUNOFF VOLUME = 1.86834 INCHES = .5879 ACRE-FEET
PEAK DISCHARGE RATE = 15.95 CFS AT 1.499 HOURS BASIN AREA = .0059 SQ. MI.

*
*****
COMPUTE NM HYD ID=3 HYD NO=DA3 DA=0.0045 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 15.990 CFS UNIT VOLUME = .9986 B = 526.28 P60 = 1.8700
AREA = .004050 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = 1.3103 CFS UNIT VOLUME = .9907 B = 388.14 P60 = 1.8700
AREA = .000450 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD ID=3 CODE=1

HYDROGRAPH FROM AREA DA3

RUNOFF VOLUME = 1.86834 INCHES = .4484 ACRE-FEET
PEAK DISCHARGE RATE = 12.17 CFS AT 1.499 HOURS BASIN AREA = .0045 SQ. MI.

*
*****
COMPUTE NM HYD ID=4 HYD NO=DB DA=0.0165 SQ MI
PER A=0 PER B=20 PER C=23 PER D=57
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 37.131 CFS UNIT VOLUME = .9991 B = 526.28 P60 = 1.8700
AREA = .009405 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .117553HR TP = .133300HR K/TP RATIO = .881867 SHAPE CONSTANT, N = 4.024364
UNIT PEAK = 18.990 CFS UNIT VOLUME = .9997 B = 356.79 P60 = 1.8700
AREA = .007095 SQ MI IA = .41977 INCHES INF = 1.02535 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD ID=4 CODE=1

HYDROGRAPH FROM AREA DB

RUNOFF VOLUME = 1.47593 INCHES = 1.2988 ACRE-FEET
PEAK DISCHARGE RATE = 37.51 CFS AT 1.499 HOURS BASIN AREA = .0165 SQ. MI.

*
*****
COMPUTE NM HYD ID=5 HYD NO=DC1 DA=0.0045 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 15.990 CFS UNIT VOLUME = .9986 B = 526.28 P60 = 1.8700
AREA = .004050 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = 1.3103 CFS UNIT VOLUME = .9907 B = 388.14 P60 = 1.8700
AREA = .000450 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD ID=5 CODE=1

```

HYDROGRAPH FROM AREA DC1

RUNOFF VOLUME = 1.86834 INCHES = .4484 ACRE-FEET
 PEAK DISCHARGE RATE = 12.17 CFS AT 1.499 HOURS BASIN AREA = .0045 SQ. MI.

```

*
*****
COMPUTE NM HYD ID=6 HYD NO=DC2 DA=0.0164
PER A=0 PER B=15 PER C=15 PER D=70
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 45.324 CFS UNIT VOLUME = .9991 B = 526.28 P60 = 1.8700
AREA = .011480 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .118429HR TP = .133300HR K/TP RATIO = .888442 SHAPE CONSTANT, N = 3.992480
UNIT PEAK = 13.091 CFS UNIT VOLUME = .9994 B = 354.67 P60 = 1.8700
AREA = .004920 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD ID=6 CODE=1

```

HYDROGRAPH FROM AREA DC2

RUNOFF VOLUME = 1.62055 INCHES = 1.4174 ACRE-FEET
 PEAK DISCHARGE RATE = 39.79 CFS AT 1.499 HOURS BASIN AREA = .0164 SQ. MI.

```

*
*****
COMPUTE NM HYD ID=7 HYD NO=DC3 DA=0.0080
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 28.426 CFS UNIT VOLUME = .9990 B = 526.28 P60 = 1.8700
AREA = .007200 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = 2.3294 CFS UNIT VOLUME = .9947 B = 388.14 P60 = 1.8700
AREA = .000800 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD ID=7 CODE=1

```

HYDROGRAPH FROM AREA DC3

RUNOFF VOLUME = 1.86834 INCHES = .7972 ACRE-FEET
 PEAK DISCHARGE RATE = 21.63 CFS AT 1.499 HOURS BASIN AREA = .0080 SQ. MI.

```

*
*****
COMPUTE NM HYD ID=8 HYD NO=DD1 DA=0.0086 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 30.558 CFS UNIT VOLUME = .9990 B = 526.28 P60 = 1.8700
AREA = .007740 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = 2.5041 CFS UNIT VOLUME = .9953 B = 388.14 P60 = 1.8700
AREA = .000860 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

*
*****
PRINT HYD ID=8 CODE=1

```

HYDROGRAPH FROM AREA DD1

RUNOFF VOLUME = 1.86834 INCHES = .8569 ACRE-FEET
 PEAK DISCHARGE RATE = 23.25 CFS AT 1.499 HOURS BASIN AREA = .0086 SQ. MI.

```

*
* COMPUTE NM HYD *****
ID=9 HYD NO=DD2 DA=0.0154 SQ MI
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 54.720 CFS UNIT VOLUME = .9991 B = 526.28 P60 = 1.8700
AREA = .013860 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

```

```

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = 4.4842 CFS UNIT VOLUME = .9977 B = 388.14 P60 = 1.8700
AREA = .001540 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

```

```

*
PRINT HYD *****
ID=9 CODE=1

```

HYDROGRAPH FROM AREA DD2

```

RUNOFF VOLUME = 1.86834 INCHES = 1.5345 ACRE-FEET
PEAK DISCHARGE RATE = 41.61 CFS AT 1.499 HOURS BASIN AREA = .0154 SQ. MI.

```

```

*
* COMPUTE NM HYD *****
ID=10 HYD NO=DD3 DA=0.0049
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 17.411 CFS UNIT VOLUME = .9987 B = 526.28 P60 = 1.8700
AREA = .004410 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

```

```

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = 1.4268 CFS UNIT VOLUME = .9917 B = 388.14 P60 = 1.8700
AREA = .000490 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

```

```

*
PRINT HYD *****
ID=10 CODE=1

```

HYDROGRAPH FROM AREA DD3

```

RUNOFF VOLUME = 1.86834 INCHES = .4883 ACRE-FEET
PEAK DISCHARGE RATE = 13.25 CFS AT 1.499 HOURS BASIN AREA = .0049 SQ. MI.

```

```

*
* COMPUTE NM HYD *****
ID=11 HYD NO=DD4 DA=0.0028
PER A=0 PER B=0 PER C=10 PER D=90
TP=-0.1333 HR MASS RAIN=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 7.9491 CFS UNIT VOLUME = .9982 B = 526.28 P60 = 1.8700
AREA = .002520 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

```

```

K = .105867HR TP = .133300HR K/TP RATIO = .794199 SHAPE CONSTANT, N = 4.514851
UNIT PEAK = .81530 CFS UNIT VOLUME = .9840 B = 388.14 P60 = 1.8700
AREA = .000280 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033300

```

```

*
PRINT HYD *****
ID=11 CODE=1

```

HYDROGRAPH FROM AREA DD4

```

RUNOFF VOLUME = 1.86834 INCHES = .2790 ACRE-FEET
PEAK DISCHARGE RATE = 7.56 CFS AT 1.499 HOURS BASIN AREA = .0028 SQ. MI.

```

FINISH

100prop6

NORMAL PROGRAM FINISH
□(s0p10h4099T□&16D

END TIME (HR:MIN:SEC) = 08:55:20

□(s16-67h8-5v0T□&16)
 AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
 YR) =12/15/2000
 INPUT FILE = F:\N448\01\030\100PROP6.DAT
 702c010000229-AH

- VERSION: 1997.02c

RUN DATE (MON/DAY/

USER NO.= AHYMO-I-9

PAGE = 1	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE
START									
TIME= .00									
RAINFALL TYPE= 1									
RAINb= 2.200									
COMPUTE NM HYD	DA1	-	1	.00680	18.38	.678	1.86834	1.499	4.224
PER IMP= 90.00									
COMPUTE NM HYD	DA2	-	2	.00590	15.95	.588	1.86834	1.499	4.225
PER IMP= 90.00									
COMPUTE NM HYD	DA3	-	3	.00450	12.17	.448	1.86834	1.499	4.226
PER IMP= 90.00									
COMPUTE NM HYD	DB	-	4	.01650	37.51	1.299	1.47593	1.499	3.552
PER IMP= 57.00									
COMPUTE NM HYD	DC1	-	5	.00450	12.17	.448	1.86834	1.499	4.226
PER IMP= 90.00									
COMPUTE NM HYD	DC2	-	6	.01640	39.79	1.417	1.62055	1.499	3.791
PER IMP= 70.00									
COMPUTE NM HYD	DC3	-	7	.00800	21.63	.797	1.86834	1.499	4.224
PER IMP= 90.00									
COMPUTE NM HYD	DD1	-	8	.00860	23.25	.857	1.86834	1.499	4.224
PER IMP= 90.00									
COMPUTE NM HYD	DD2	-	9	.01540	41.61	1.535	1.86834	1.499	4.222
PER IMP= 90.00									
COMPUTE NM HYD	DD3	-	10	.00490	13.25	.488	1.86834	1.499	4.226
PER IMP= 90.00									
COMPUTE NM HYD	DD4	-	11	.00280	7.58	.279	1.86834	1.499	4.230
PER IMP= 90.00									
FINISH									
□(s0p10h4099T□&16)									

POND CALCULATIONS

DA1

EXISTING - 0.163 AC-FT
ULTIMATE - 0.628 AC-FT
DIFFERENCE - 0.628 - 0.163 = 0.465 AC-F

PER D.P.M. pg. 22-14, EQN a-7

$$\begin{aligned} V1440 &= V360 + Ad *(P1440-P360)/12''/FT \\ &= 0.465 + [0.0068(640)] (2.66-2.20/12) \\ &= 0.632 \text{ AC-FT (43560/1.5 DEEP) } = 18348.25 \text{ FT}^3 \\ \text{SIZE} &= (\text{SQ RT } 18348.25) \\ &= 135.5' \text{ EACH SIDE MIN.} \end{aligned}$$

DA2

EXISTING - 0.103 + 0.038 = 0.141 AC-FT
ULTIMATE - 0.888 AC-FT
DIFFERENCE - 0.888 - 0.141 = 0.747 AC-F

$$\begin{aligned} V1440 &= 0.888 + [0.0059(640)] (2.66-2.20/12) \\ &= 1.033 \text{ AC-FT (43560/1.5) } = 29990.96 \text{ FT}^3 \\ \text{SIZE} &= (\text{SQ RT } 29990.96) \\ &= 173.2' \text{ EACH SIDE MIN.} \end{aligned}$$

DA3

EXISTING - 0.084 + 0.024 = 0.108 AC-FT

ULTIMATE - 0.448 AC-FT

DIFFERENCE - 0.448 - 0.108 = 0.340 AC-F

$$\begin{aligned} V1440 &= 0.448 + [0.0045(640)] (2.66-2.20/12) \\ &= 0.558 \text{ AC-FT } (43560/1.5) = 16215.9 \text{ FT}^3 \end{aligned}$$

$$\begin{aligned} \text{SIZE} &= (\text{SQ RT } 16215.9) \\ &= 127.3' \text{ EACH SIDE MIN.} \end{aligned}$$

DC1

EXISTING - 0.108 AC-FT

ULTIMATE - 0.448 AC-FT

DIFFERENCE - 0.448 - 0.108 = 0.340 AC-F

$$\begin{aligned} V1440 &= 0.448 + [0.0045(640)] (2.66-2.20/12) \\ &= 0.558 \text{ AC-FT } (43560/1.5) = 16215.9 \text{ FT}^3 \end{aligned}$$

$$\begin{aligned} \text{SIZE} &= (\text{SQ RT } 16215.9) \\ &= 127.3' \text{ EACH SIDE MIN.} \end{aligned}$$

DC2

EXISTING - 0.110 + 0.115 + 0.105 + 0.024 + 0.034
= 0.388 AC-FT

ULTIMATE - 1.447 AC-FT

DIFFERENCE - 1.059 AC-F

$$\begin{aligned} V1440 &= 1.447 + [0.0164(640)] (2.66-2.20/12) \\ &= 1.85 \text{ AC-FT } (43560/1.5) = 53705.0 \text{ FT}^3 \end{aligned}$$

$$\begin{aligned} \text{SIZE} &= (\text{SQ RT } 53705.0) \\ &= 231.7' \text{ EACH SIDE MIN.} \end{aligned}$$

STORM DRAIN CALCULATIONS

I. Along McMahon to Tuscany Ridge Unit II.

Existing - 36" storm drain McMahon Blvd.
- 24 cfs allowed from Fineland Development

Proposed – pipe size (full flow)

$$Q = 24.0 \text{ cfs max.}$$

$$n = 0.013$$

$$S = .05\%$$

$$\begin{aligned} D_n &= 1.335 (nq/\text{sq rt } S) \\ &= 1.335 (0.013 (24)/\text{sq rt } .005) = 2.35' (12) \\ &= 28" \text{ min} \rightarrow \textbf{use 30" min} \end{aligned}$$

II. Outlet to Ridgeview Subdivision for Fineland Commercial Lots and Smith Properties.

Proposed - 24" storm drain in Ridgeview Subdivision
- 25.4 cfs allocated from Smith and Fineland Properties

$$Q = 25.4 \text{ cfs max}$$

$$n = 0.013$$

$$S = 1.7\% \text{ average}$$

$$\begin{aligned} D_n &= 1.335 (0.013 (25.4)/\text{sq rt } 0.017)^{3/8} = 1.89(12) \\ &= 22.70" \rightarrow \textbf{use 24" min} \end{aligned}$$

III. Street Flow/Inlet Calculations
(Crooked Creek Avenue)

$$Q = 37.51 \text{ cfs}$$

$$S = 2.33 \%$$

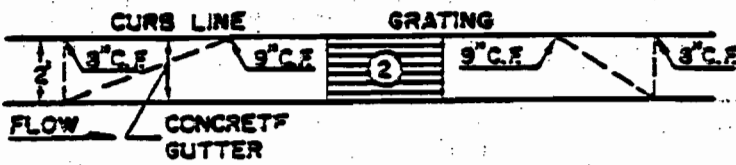
$$@ 2.33 \% \text{ Road Capacity} = 125.79 \text{ cfs}$$

$$@ 37.51 \text{ cfs Depth} = 4.58'' = 0.38''$$

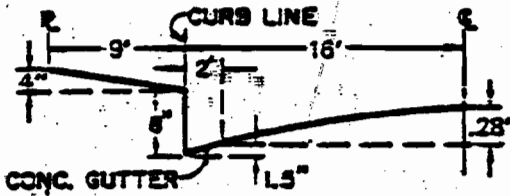
Chart Nomo – Plate 22.3 D-5
Shows 5.1 cfs/grate

- Stonebridge Drainage Plan allowed 20.4 cfs
- Required per bulk land plat 37.51 cfs
- Difference = $37.51 - 20.4 = 17.11 \text{ cfs}$
- @ 2 sides of street $17.11/2 = 8.56 \text{ cfs}$
- @ 5.1 cfs/grate use minimum 2 grates each side of street. This will capture additional flows plus some already allocated for the system.

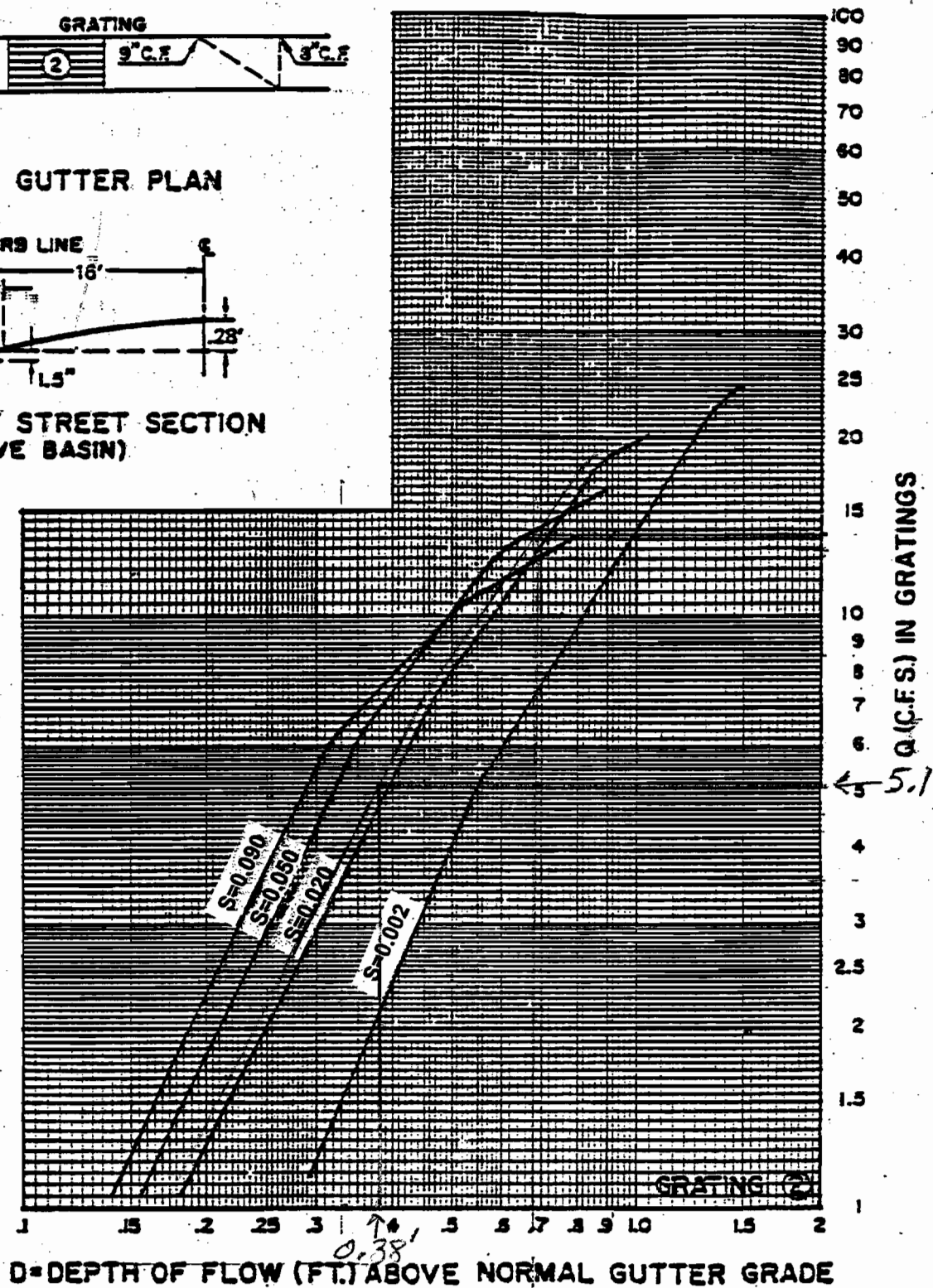
GRATING CAPACITIES FOR TYPE "A" , "C" and "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION
(ABOVE BASIN)



Channel Calculator

Given Input Data:

Shape	Trapezoidal
Solving for	Depth of Flow
Flowrate	37.5100 cfs
Slope	0.0233 ft/ft
Manning's n	0.0170
Height	8.0000 in
Bottom width	336.0000 in
Left slope	0.0200 ft/ft
Right slope	0.0200 ft/ft

Computed Results:

Depth	3.0427 in
Velocity	5.2823 fps
Flow area	7.1010 ft ²
Flow perimeter	342.0867 in
Hydraulic radius	2.9892 in
Top width	336.1217 in
Area	18.6756 ft ²
Perimeter	352.0032 in
Percent full	38.0344 %

Critical Information

Critical depth	4.5846 in
Critical slope	0.0060 ft/ft
Critical velocity	3.5055 fps
Critical area	10.7003 ft ²
Critical perimeter	345.1710 in
Critical hydraulic radius	4.4640 in
Critical top width	336.1834 in
Specific energy	0.6872 ft
Minimum energy	0.5731 ft
Froude number	1.8496
Flow condition	Supercritical

8-inch Max. Depth (8" CURB)

[illegible]

FINELAND COMMERCIAL PIPE SIZING
Worksheet for Circular Channel

Project Description	
Worksheet	FINELAND
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Capacity

Input Data	
Mannings Coefficient	0.013
Slope	0.012000 ft/ft
Diameter	24 in

Results	
Depth	2.00 ft
Discharge	24.78 cfs
Flow Area	3.1 ft²
Wetted Perimeter	6.28 ft
Top Width	0.00 ft
Critical Depth	1.76 ft
Percent Full	100.0 %
Critical Slope	0.010823 ft/ft
Velocity	7.89 ft/s
Velocity Head	0.97 ft
Specific Energy	2.97 ft
Froude Number	0.00
Maximum Dischar	26.66 cfs
Discharge Full	24.78 cfs
Slope Full	0.012000 ft/ft
Flow Type	N/A

>25.4 OK

←

AT MIN. SLOPE,
HGL < PROPOSED GRADE (OK)
(5' MIN. COVER)

FINELAND COMMERCIAL PIPE SIZING
Worksheet for Circular Channel

Project Description	
Worksheet	FINELAND
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Capacity

Input Data	
Mannings Coefficient	0.013
Slope	0.032000 ft/ft
Diameter	24 in

Results	
Depth	2.00 ft
Discharge	40.47 cfs
Flow Area	3.1 ft²
Wetted Perimeter	6.28 ft
Top Width	0.00 ft
Critical Depth	1.95 ft
Percent Full	100.0 %
Critical Slope	0.028486 ft/ft
Velocity	12.88 ft/s
Velocity Head	2.58 ft
Specific Energy	4.58 ft
Froude Number	0.00
Maximum Dischar	43.53 cfs
Discharge Full	40.47 cfs
Slope Full	0.032000 ft/ft
Flow Type	N/A

>25.4 OK
←

AT MAX. SLOPE
HGL < PROPOSED GRADE (OK)
(5' MIN. COVER)

