



City of Albuquerque
P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

November 27, 2001

Rick Beltramo, PE
Bohannan Huston, Inc
7500 Jefferson NE
Albuquerque, NM 87109

Re: Unser/McMahon Area Master Drainage Study
Engineer's Stamp dated 11-13-01, (A11/D5A)

Dear Mr. Beltramo,

Based upon the information provided in your submittal dated 11-13-01, the above referenced Study is conditionally approved as a Master Study for the subject area to support the Storm Drain Installation project in Black Arroyo and Unser Blvd. Conditions of approval include:

- All reference to the "City Section" should be removed and combined with the East Section. The agreement, once it is signed by your client and the City, denotes what the City contribution will be and nowhere is it noted that any particular reach is the responsibility of the City.
- This approval does not necessarily approve the plan and profile sheets provided; they are a guide (albeit a well-designed guide) and coordination with other departments and as-built conditions will be necessary.

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham
Bradley L. Bingham, PE
Sr. Engineer, PWD
Development and Building Services

C: file

A-11/10005-A

- und sehr
Wichtig!

Mission Blvd.



A-11/DOO 5A

MASTER DRAINAGE STUDY FOR THE UNSER / MCMAHON AREA

BOHANNAN HUSTON

Courtyard One

7500 JEFFERSON NE

Albuquerque

NEW MEXICO 87109

voice 505.823.1000

fax 505.821.0892

July 17, 2001

AMENDED NOVEMBER 13, 2001

PREPARED FOR:

CURB, INC.
6301 INDIAN SCHOOL NE, SUITE 208
ALBUQUERQUE, NM 87109

TABLE OF CONTENTS

	Page
I. INTRODUCTION.....	1
II. PURPOSE.....	1
III. METHODOLOGY	2
IV. LAND TREATMENTS	2
V. PROPOSED DEVELOPED CONDITIONS.....	3
VI. CONCLUSION.....	4

FIGURES

FIGURE 1 - UNSER / MCMAHON AREA VICINITY MAP

FIGURE 2 - DEVELOPED CONDITIONS BASIN MAP

FIGURE 3 - DEVELOPED CONDITIONS LAND TREATMENT EXHIBIT

APPENDICES

APPENDIX A - AHYMO INPUT, OUTPUT AND SUMMARY FILES CONDITIONS

APPENDIX B - STREET FLOW, INLET, AND HYDRAULIC GRADE LINE CALCULATIONS

EXHIBITS

EXHIBIT 1 - DEVELOPED CONDITIONS BASIN MAP

EXHIBIT 2 - UNSER BOULEVARD UTILITY PLAN AND PROFILES

EXHIBIT 3 - BLACK ARROYO BOULEVARD UTILITY PLAN AND PROFILES

MASTER DRAINAGE STUDY
FOR THE
UNSER / MCMAHON AREA

July 17, 2001
November 13, 2001

Prepared for:

CURB INC.
6301 INDIAN SCHOOL NE, SUITE 208
ALBUQUERQUE, NM 87110

By:

BOHANNAN HUSTON, INC.
COURTYARD I
7500 JEFFERSON STREET NE
ALBUQUERQUE, NM 87109

PREPARED BY:

Elizabeth Smith, P.E.

Date

Rick Beltramo, R.E.

Date



I. INTRODUCTION

This drainage study is a Master plan for the McMahon Boulevard and Unser Boulevard drainage area. A regional master plan is required due to the geopolitical boundaries of Rio Rancho and Albuquerque, the drainage impacts of McMahon Boulevard and Unser Boulevard, and the interrelated drainage impacts of several developments. This Master plan will address the developed storm runoff and the necessary facilities to adequately convey the flow from the Unser/McMahon Area to the Black Arroyo Detention Facility. The drainage area addressed in this report includes the land bounded by the Albuquerque/Rio Rancho city boundary to the north, McMahon Boulevard to the south, the Stonebridge Subdivision to the east, and the natural ridgeline to the west. In addition, two commercial tracts south of McMahon are included. See vicinity map for location. (**Figure 1**) The runoff from this area will be conveyed through a storm drain system in McMahon Boulevard, Unser Boulevard, and Black Arroyo Boulevard to the Lands of AMAFCA and the Black Arroyo Detention Facility. The Detention Facility was built with the capacity to handle all of the developed runoff from this region.

II. PURPOSE

The drainage problems associated with this area involve the interests of several public entities and several private developers. Since the Albuquerque/Rio Rancho boundary splits the drainage basins, AMAFCA, SSCAFCA, the City of Albuquerque, and the City of Rio Rancho are all interested in this drainage solution. In addition, the City of Albuquerque is in the process of designing McMahon Boulevard and the drainage in the road must be accommodated. On the private side, four subdivisions are in the process of developing and require a drainage solution. These subdivisions are the Ridgeview Subdivision, Ridgeview Village, Los Suenos, and Park Hill. Finally, several commercial tracts in the Village Center along Unser are involved. These regional drainage issues are too complex for any one development or public agency to solve alone. Therefore, the private developers and the public agencies involved must cooperate. Approval of this Master plan and the associated storm drains provides a basis for determining shared storm drain infrastructure between public and private entities and allows for the phased implementation of the storm drain system. This Master plan will propose a plan to provide a

suitable public storm drain outfall for the following portions of the McMahon/Unser Region:

- Portions of McMahon Boulevard.
- Portions of Unser Boulevard.
- All contributing areas that cross McMahon Boulevard and Unser Boulevard under developed conditions.
- Proposed developments within Albuquerque that historically drain into Rio Rancho.
- Units 1 and 2 of the Ridgeview Subdivision and adjacent land located east of Unser Boulevard and north of McMahon Boulevard.

This Master plan does not address the historic drainage patterns or the interim plans for the individual developments. Refer to the Drainage Studies for the Ridgeview Subdivision, the Los Suenos Subdivision, or the Park Hill Subdivision for historic and interim conditions.

III. METHODOLOGY

Existing and proposed site hydrological conditions were analyzed for the 100-year, 6-hour storm in accordance with the revised Section 22.2, Hydrology, of the Development Process Manual (DPM) for the City of Albuquerque, dated January 1993. Street capacities were analyzed using Manning's equation, consistent with the revised DPM Section 22.2. All data and calculations supporting this study are located in Appendix B. The Arid-lands Hydrologic Model (AHYMO) was utilized to determine peak flow rates for design of the storm drainage improvements within the projects. The 100-year, 6-hour storm is used as the design event. The results are included in Appendix A.

The storm sewer system is analyzed using current DPM methods for gravity flow conditions. Inlet capacity computations, along with all hydraulic computations, are included in Appendix B.

IV. LAND TREATMENTS

The land treatments in this analysis are divided into two sections. The land east of Unser and south of McMahon drains through the Ridgeview Subdivision. Therefore, the lands treatment values used to design the existing storm drain within the Ridgeview Subdivision were generally maintained in this analysis. The residential lands within the Ridgeview analysis were analyzed

using 25% type 'B', 25% type 'C', and 50% type 'D'. The commercial tracts were restricted to historic discharge of 95% type 'A' and 5% type 'B'. The only commercial tracts allowed developed discharge in the Ridgeview report were the Village Center North Tracts because Mr. Smith paid to upsize the Ridgeview storm drain. One amendment was made to the drainage plan proposed by the Ridgeview Subdivision. The runoff from the Fein Residential property that was originally conveyed through the Ridgeview Subdivision and discharged into Black Arroyo Boulevard is now directed through the Stonebridge Subdivision. This change was made due to a subsequent analysis of the Fein property performed by Community Sciences. This analysis determined that there is sufficient capacity in the Stonebridge storm drain to accommodate the 36.3 cfs from the Fein Residential property. Therefore, the contribution from this basin was removed from the Ridgeview storm drain.

The tracts of land west of Unser or south of McMahon do not drain through the Ridgeview Subdivision. The commercial tracts in this area are permitted developed discharge and were analyzed using 90% type 'D' and 10% type 'B'. The residential tracts were analyzed using 20% type 'B', 20% type 'C', and 60% type 'D'. See **Figure 3**, the Developed Conditions Land Treatment Exhibit for an illustration of land treatment values.

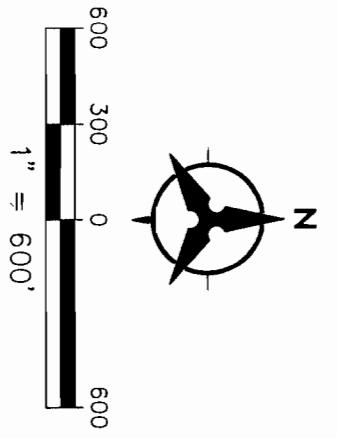
V. PROPOSED DEVELOPED CONDITIONS

There are four major storm drain reaches included in this analysis. First, the southern reach of the analysis consists of basins that contribute flow to McMahon Boulevard and Unser Boulevard south of Black Arroyo Boulevard. Secondly, the West section of the analysis consists of the basins that contribute flow to Black Arroyo Boulevard west of Unser. Thirdly, the east portion of the analysis consists of basins that contribute flow to Black Arroyo Boulevard adjacent to the Ridgeview Subdivision. Finally, the *Lower Reach* of the analysis includes the section of storm drain that conveys the flow from the other reaches east to the Lands of A.M.A.F.C.A. At the top of the southern reach, the runoff from basins DB6 and DC2 south of McMahon combine with the street flow from McMahon Boulevard and the commercial tract DB4-C and is conveyed to the intersection of McMahon and Unser Boulevards. The flow then combines with the Unser street flow and 180 cfs is diverted north in Unser Boulevard. Basin DB5A discharges into the Unser storm drain and is conveyed to the south boundary of the Ridgeview Subdivision. At this point, basin DB5B

discharges into the storm drain and the street flow from Unser is captured. In addition, the southern half of Ridgeview Village, Basin DB4-B, discharges into the main line at this intersection. Then the flow, 288 cfs, continues north to the intersection with Black Arroyo Boulevard. At the intersection, the flow from the West Section of the analysis is added to the flow from the South Section. A discharge of 675 cfs from the residential developments to the west, Basins DB1, DB2, DB3, and DB4-A, is diverted east on Black Arroyo Boulevard. The storm drain system in the Eastern portion of Black Arroyo Boulevard then accepts flow from the land that discharges through Ridgeview Unit 1. A 42" storm drain has been stubbed through the Ridgeview Subdivision to the south to convey this flow to Black Arroyo Boulevard. The storm drain containing 823 cfs continues east to the lands of A.M.A.F.C.A. The remaining street flow is captured just west of the lands of A.M.A.F.C.A., then the storm drain crosses an existing water line and discharges 841 cfs through an energy dissipater into an earthen channel. The earthen channel discharges into the Black Arroyo utilizing a grade control structure. See the Developed Conditions Basin Map, **Plate 1**, for basin locations and **Appendix B** for the calculations for the hydraulic grade line, street capacity, inlet design, and the channel analysis. **Appendix A** contains the AHYMO analysis that was performed to determine the flows created by these basins.

VI. CONCLUSION

The improvements proposed in this Master plan solve regional drainage issues. The plan provides a public storm drain outfall for planned developments including those that currently drain into Rio Rancho. This Master Plan proposes redirecting these flows to the Black Arroyo Detention Facility due to the geopolitical boundaries and the difficulties in obtaining approvals for discharging developed runoff originating in Albuquerque but outfalling in Rio Rancho. Drainage solutions for McMahon Boulevard and Unser Boulevard are identified and an outfall to the Black Arroyo Detention Facility is provided. Approval of this plan provides a basis for requiring storm drains to be funded and constructed by both private and public entities. Approval also allows planning and construction of phased improvements of the ultimate system. Significant work is already in progress that will manifest itself in several drainage reports associated with the proposed subdivisions and construction plans for the storm drain in Black Arroyo Boulevard and Unser Boulevard.



CITY OF
RIO RANCHO

SANDOVAL COUNTY

BERNALILLO COUNTY
BLACK ARROYO BLVD

RIO
RANCHO
ESTATES
UNIT 16

SANDOVAL COUNTY
BERNALILLO COUNTY

PARK HILL
SUBDIVISION
LOS SUEÑOS
SUBDIVISION
RIDGEVIEW
VILLAGE
SUBDIVISION
(CURB INC.)
VILLAGE CENTER
WEST
RIDGEVIEW
SUBDIVISION
(CURB INC.)
STONEBRIDGE
SUBDIVISION
(CENTEX)
LANDS OF
AMAFCA
BLACK
ARROYO
DETENTION
FACILITY

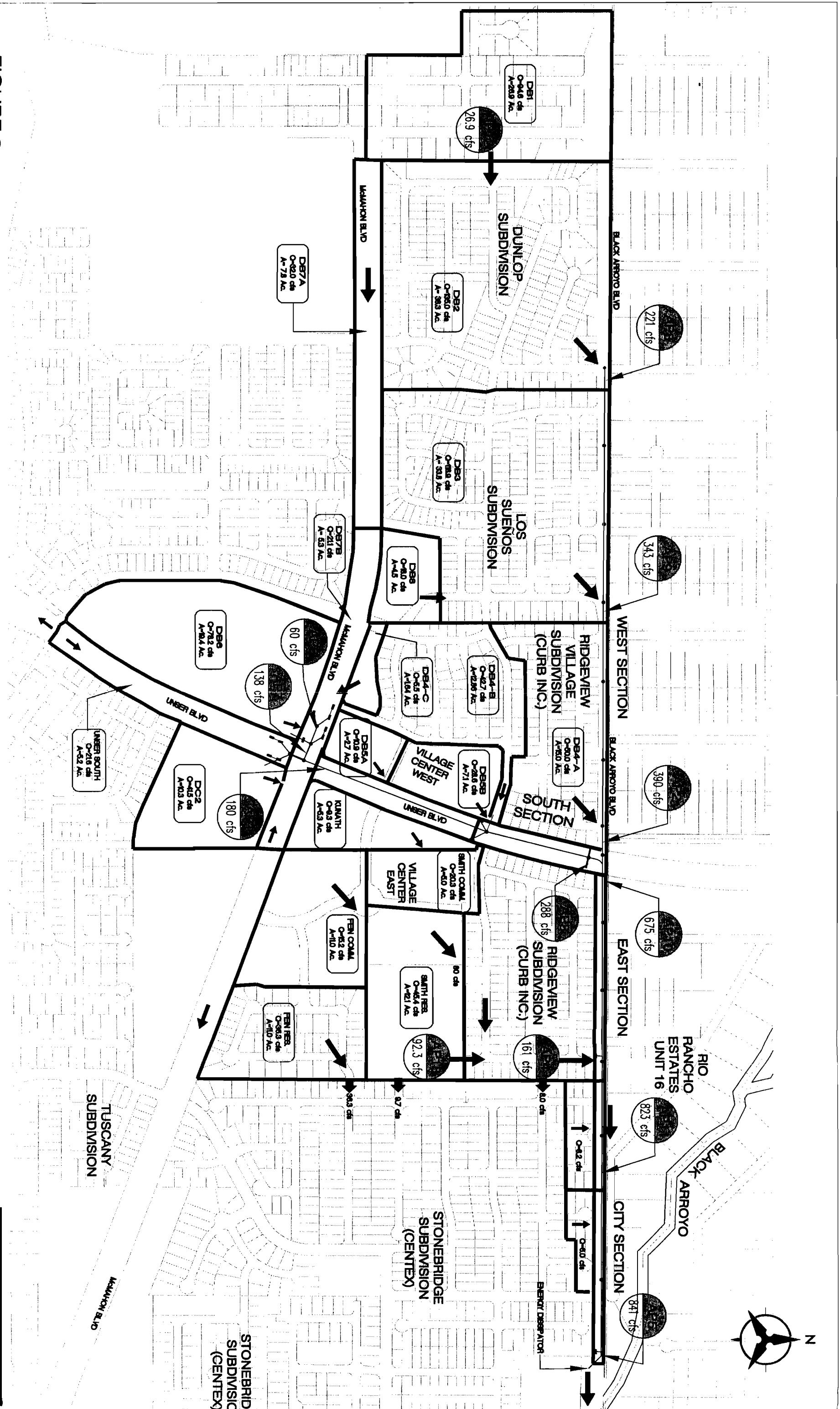
McMAHON BLVD

UNSER BLVD
McMAHON BLVD
TUSCANY
SUBDIVISION
STONEBRIDGE
SUBDIVISION
(CENTEX)
PARADISE
HEIGHTS
SUBDIVISION
BANDELIER ROAD

FIGURE 1
UNSER / McMAHON AREA
VICINITY MAP

**FIGURE 2
DEVELOPED CONDITIONS
BASIN MAP**

P:\01177\CDP\GENERAL\EXHIBITS\MSTR-BASIN.DWG



ROHANNAN HUSTON

Courtyard One

7500 JEFFERSON NE

Albuquerque

NEW MEXICO 87109

voire 505.823.1000

fax 505.823.6812

APPENDICES

- | | |
|-------------------|--|
| APPENDIX A | AHYMO INPUT AND SUMMARY FILES FOR
HISTORIC AND DEVELOPED CONDITIONS |
| APPENDIX B | STREET FLOW IN UNSER, MCMAHON, AND BLACK
ARROYO BLVDS, INLET AND SWALE CAPACITY, AND
HYDRAULIC GRADE LINE CALCULATIONS |

* UNSER/MCMAHON MASTER PLAN
* EXISTING CONDITIONS HYDROLOGIC ANALYSIS

*S HISTORIC DRAINAGE FROM THE UNSER/MCMAHON BASIN

*S Revised 7-20-00

START RAINFALL BEGINS AT 0.00 HOURS
* 100 YEAR RETURN PERIOD

* MISC. DATA
* RAINFALL RETURN PERIOD 100-YEAR
* RAINFALL DURATION 6-HOUR
* ZONE 1
* RAINFALL DEPTHS: 1 HOUR (P60) 1.87 INCHES
* (UNADJUSTED) 6 HOUR (P360) 2.20 INCHES
* 24 HOUR (P1440) 2.66 INCHES

* RAINFALL DATA TAKEN FROM NOAA.

* HYDROGRAPH METHODOLOGY

* CITY OF ALBQ. DPM VOL. 2, SECTION 22.2 July, 1997
* INITIAL ABSTRACTION - INFILTRATION METHOD
* Tc CALCULATIONS PER C.O.A. DPM 22.2-B.4
* AMAFCA AHYMO VERSION MARCH 20, 1992

* BEGIN ANALYSIS

* RAINFALL TYPE=1 RAIN QUARTER=0.0 RAIN ONE=1.87
* RAIN SIX=2.20 RAIN DAY=2.66 DT=0.05

***** COMPUTE AND PRINT NM HYD DATA FOR BASIN OFF1 *****
COMPUTE NM HYD ID=1 HYD=OFF1 AREA=0.157 PER A=50.0 PER B=50.0
PER C=0.0 PER D=0.0 TP=.133 RAINFALL=-1

PRINT HYD ID=1 CODE=1

***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 2 *****
COMPUTE NM HYD ID=2 HYD=OFF2 AREA=0.086 PER A=50.0 PER B=50.0
PER C=0.0 PER D=0.0 TP=.133 RAINFALL=-1

PRINT HYD ID=2 CODE=1

***** COMPUTE AND PRINT NM HYD DATA FOR BASIN OFFSITE BASIN 3 *****
COMPUTE NM HYD ID=3 HYD=OFF3 AREA=0.137 PER A=50.0 PER B=50.0
PER C=0.0 PER D=0.0 TP=.133 RAINFALL=-1

PRINT HYD ID=3 CODE=1

***** COMPUTE AND PRINT NM HYD DATA FOR BASIN OFFSITE BASIN 4 *****
COMPUTE NM HYD ID=4 HYD=OFF4 AREA=0.065 PER A=50.0 PER B=50.0
PER C=0.0 PER D=0.0 TP=.133 RAINFALL=-1

PRINT HYD ID=4 CODE=1

***** COMPUTE AND PRINT NM HYD DATA FOR BASIN OFFSITE BASIN 5 *****
COMPUTE NM HYD ID=5 HYD=OFF5 AREA=0.061 PER A=50.0 PER B=50.0
PER C=0.0 PER D=0.0 TP=.133 RAINFALL=-1

PRINT HYD ID=5 CODE=1

ADD HYD ID=10 HYD=12 ID I=1 ID II=2

PRINT HYD ID=10 CODE=1

ADD HYD ID=12 HYD=34 ID I=4 ID II=3

PRINT HYD ID=12 CODE=1

ADD HYD ID=14 HYD=1234 ID I=10 ID II=12

PRINT HYD ID=14 CODE=1

FINISH

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994
INPUT FILE = ex.txt

RUN DATE (MON/DAY/YR) = 06/14/2001
USER NO. = BOHN_HNM.STE

COMPLAND	HYDROGRAPH IDENTIFICATION	FROM ID	TO ID	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION
*; UNDEVELOPED PROPERTY ORIGINALLY DRAINING TO ARROYO										
*S Revised 6-14-01 for User/McMahon Master Drainage Study										
START	RAINFALL TYPE=	1								
COMPUTE NM HYD	OFF1	-	1	.15700	168.87	4.535	.54156	1.500	1.681 PER IMP=	.00
COMPUTE NM HYD	OFF2	-	2	.08600	89.96	2.484	.54156	1.500	1.635 PER IMP=	.00
COMPUTE NM HYD	OFF3	-	3	.13700	146.21	3.957	.54156	1.500	1.668 PER IMP=	.00
COMPUTE NM HYD	OFF4	-	4	.06500	67.45	1.877	.54156	1.100	1.621 PER IMP=	.00
COMPUTE NM HYD	OFF5	-	5	.06100	63.24	1.762	.54156	1.500	1.620 PER IMP=	.00
ADD HYD	12.00	1& 2	10	.24300	258.83	7.019	.54156	1.500	1.664	
ADD HYD	34.00	4& 3	12	.20200	213.66	5.834	.54156	1.500	1.653	
ADD HYD	1234.00	10&12	14	.44500	472.49	12.853	.54156	1.500	1.659	
FINISH										

UNSER/MCMAHON ANALYSIS POINTS

01177

11/8/2001

<u>ANALYSIS POINT #</u>	<u>Q (CFS)</u>	<u>AREA (MI²)</u>	<u>LOCATION</u>
-----------------------------	--------------------	----------------------------------	-----------------

1	180	0.069	Unser just north of McMahon
2	390	0.185	Black Arroyo Blvd. just west of Unser
3	288	0.121	Unser just south of Black Arroyo Blvd
4	161	0.0664	Ridgeview discharge to Black Arroyo Blvd
5	841	0.3809	Total Discharge to Black Arroyo Dam
6	60	0.0227	McMahon Blvd at first inlets
7	138	0.053	McMahon Blvd just west of Unser
8	221	0.1019	East Boundary of Park Hill
9	343	0.1617	East Boundary of Los Suenos
10	675	0.306	Black Arroyo Blvd. just east of Unser
11	823	0.3725	Black Arroyo Blvd. Adjacent to Stonebridge
12	94.6	0.042	West Boundary of Park Hill
13	92.3	0.048	Smith Discharge to Ridgeview Subdivision

UNSER/MCMAHON BASINS

11/8/2001

01177

<u>BASIN</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>Q (CFS)</u>	<u>AREA (MI^2)</u>	<u>COMMENTS</u>
IN		10		90	21.43	0.0083	Kunath Commercial Outfalls to Unser Blvd.
J1		10		90	20.14	0.0078	Smith Commercial Outfalls to Ridgeview
J2		10		90	16.53	0.0064	Smith Residential Outfalls to Ridgeview
*K		15	20	65	7.45	0.0032	Smith Residential Outfalls to Ridgeview
*L		15	20	65	10.24	0.0044	Smith Residential Outfalls to Ridgeview
*M		15	20	65	11.17	0.0048	Smith Residential Outfalls to Ridgeview
O	95	5			6	0.0072	Fein Commercial - Restricted
P	95	5			4.75	0.0057	Fein Commercial - Restricted
Q	95	5			4.25	0.0051	Fein Commercial - Restricted to Historic Flow per Ridgeview Drainage Plan
*R		25	25	50	12.82	0.006	Fein Residential Outfalls to Stonebridge
*S		25	25	50	23.49	0.011	Fein Residential Outfalls to Stonebridge
A-H		25	25	50	70.76	0.0331	Ridgeview Subdivision
WS				100	5.73	0.0021	Black Arroyo Blvd.
DB1		20	20	60	94.6	0.042	Offsite platted residential lots west of Park Hill
DB2		20	20	60	134.9	0.0599	Park Hill Subdivision
DB3		20	20	60	118.9	0.0528	Los Suenos Subdivision
DB4A		20	20	60	52.72	0.0234	Ridgeview Villiage-Discharge to Black Arroyo
DB4B		20	20	60	45.06	0.02	Ridgeview Villiage-Discharge to Unser
DB4C		10		90	6.62	0.00256	Ridgeview Villiage-office
DB5A		10		90	10.85	0.0042	Village Center West Commercial
DB5B		10		90	28.39	0.011	Village Center West Commercial
DB6		10		90	78.18	0.0303	Comm. Tract south-west of Unser/McMahon
DB7A			10	90	32.03	0.01216	McMahon Blvd West Street Flow
DB7B			10	90	21.08	0.008	McMahon Blvd East Street Flow
DB8		10		90	18.07	0.007	Los Suenos Commercial Tract
N-UNSER			10	90	9.23	0.0035	North portion of Unser Blvd.
MID-UNSER			10	90	13.18	0.005	Middle portion of Unser Blvd.
S-UNSER			10	90	21.61	0.0082	South portion of Unser Blvd.
DC2		10		90	41.55	0.016	Comm. tract south-east of Unser/McMahon
2	25	25	50		2.15	0.001	Ridgeview Subdivision Unit 2
3	25	25	50		3.09	0.00144	Ridgeview Subdivision Unit 2
W2			10	90	2.91	0.0011	Black Arroyo Blvd. W
ROAD			10	90	5.54	0.0021	Black Arroyo Blvd. E
CULSACS		25	25	50	5.97	0.00279	Stonebridge Unit 4 into Black Arroyo Blvd
				TOTAL	0.420		
SUBTRACT FLOW TO STONEBRIDGE					0.040		
				TOTAL	0.380		

Note: Flow is not directly additive due to routing

COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 3 NOTATION	
*S FLOW ADDED TO UNSER AT BLACK ARROYO BLVD FROM WEST											
*S AP 2		AP2	25& 4	26	.18510	389.72	14.952	1.51459	1.550	3.290	
ADD HYD											
*****S ADD FLOWS TO MCMAHON AND UNSER INTERSECTION*****											
ADD HYD		F712	7&12	29	.02016	53.11	2.008	1.86799	1.500	4.116	
*S AP 6		F715	29&15	30	.02272	59.73	2.259	1.86433	1.500	4.108	
ADD HYD											
*S AP 7		F7615	30& 6	31	.05302	137.91	5.225	1.84794	1.500	4.064	
ADD HYD											
*S AP 1		API	31&11	32	.06912	179.46	6.802	1.84507	1.500	4.057	
ADD HYD											
*****S ROUTE UNSER/MCMAHON FLOW TO UNSER/BLACK ARROYO ROUTE*****											
ROUTE		UMC	32	33	.06912	168.73	6.802	1.84508	1.500	3.814	
ADD HYD		5A	33& 5	38	.07332	179.58	7.213	1.84453	1.500	3.827	
ADD HYD		UNSER	10&16	39	.01320	34.79	1.315	1.86797	1.500	4.118	
ADD HYD		SR	38&39	40	.08652	214.37	8.528	1.84811	1.500	3.871	
ADD HYD		USB	40&13	41	.09752	242.76	9.605	1.84670	1.500	3.890	
ADD HYD		UNSER	41&14	42	.11752	287.82	11.207	1.78803	1.500	3.827	
ROUTE		UMC	42	43	.11752	278.09	11.207	1.78804	1.500	3.697	
*S AP 3		AP3	43& 9	44	.12102	287.32	11.556	1.79034	1.500	3.710	
*****S TOTAL FLOW AT UNSER AND BLACK ARROYO*****											
*S AP 10		UBL	44&26	46	.30612	674.89	26.508	1.62360	1.550	3.445	
ADD HYD											
*****S ROUTE UNSER/BLACK ARROYO FLOW TO EAST OF RIDGEVIEW 1*****											
ROUTE		RV1	46	47	.30612	682.28	26.508	1.62361	1.550	3.482	
*****S ADD RIDGEVIEW 1 AND FINELAND VILLAGE CENTER FLOWS TO PIPE*****											
*S AP 11		RV	47&52	48	.37247	823.15	31.231	1.57218	1.550	3.453	
ADD HYD											
*****S COMPUTE RIDGEVIEW 2 AND BLACK ARROYO BLVD FLOWS*****											
*****S 'UVAL STREET FLOW IN BLACK ARROYO BLVD EAST OF RIDGEVIEW UNIT 2*****											
ADD HYD		WEST23	12& 3	14	.00354	8.15	.290	1.53544	1.500	3.596	
*S STONEBRIDGE CONTRIBUTION											
COMPUTE NM HYD		ROAD	2.00	-	2	.00100	2.15	.074	1.38584	1.500	3.357 PER IMP= 50.00
COMPUTE NM HYD		CULSACS	3.00	-	3	.00144	3.09	.106	1.38584	1.500	3.351 PER IMP= 50.00
COMPUTE NM HYD		WEST	-	4	.00110	2.91	.110	.110	1.86802	1.500	4.134 PER IMP= 90.00
ADD HYD		WEST2	4& 2	12	.00210	5.06	.183	.183	1.63816	1.500	3.764
*****S TOTAL FLOW IN BLACK ARROYO BLVD EAST OF RIDGEVIEW UNIT 2*****											
*S AP 5		AP5	16&48	18	.38090	840.49	31.937	1.57211	1.550	3.448	
ADD HYD											
FINISH											

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994
INPUT FILE = Master.TXT

RUN DATE (MON/DAY/YR) =11/05/2001
USER NO. = BOHN_HNM.STE

HYDROGRAPH				PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1
FROM ID	TO ID	AREA (SQ. MI.)	NO.						NOTATION
TENNESSE	CONTRACT	100	1						

*S INPUT = 01177\cdp\hydro\master\commercial developed\Master.TXT
*S Revised 10-17-01 for Master Storm Drain in Unser/McMahon
*S This analysis assumes that McMahon flow is diverted down Unser Blvd
*S and Black Arroyo Blvd without Bonding.
*S Ridgeview Village (DB4), Los Sueños (DB3), and the Park Hill (DB2)
*S Subdivisions have free developed discharge based on R-1, 5 du/acre density.
*S Flow from some commercial sites east of Unser between Mcmahon and
*S Black Arroyo Blvd is restricted to historic as per Ridgeview Unit 1 Plan.
*S Developed flow is accommodated from the residential tracts and
*S other commercial tracts. See Land Treatment Exhibit for specific tracts.

ADD HYD RVAP4 33&35 50

*S ADD SOUTH-EASTERN BASINS
*S S'ONEBRIDGE WILL ACCEPT 9.69 CFS AT FEATHER ROCK
DIVIDE HYD SB2 9 80 .00472 9.69 .394 1.56785 1.450 3.210
M2 AND 81 .00008 1.48 .007 1.56785 1.500 27.530

COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =
										NOTATION
ADD HYD	SR 21&19	54	.01700	36.31	1.256	1.38581	1.500	3.337		
ADD HYD	ML 81& 7	55	.00448	11.72	.375	1.56784	1.500	4.083		
ADD HYD	OK 17& 5	58	.00830	11.70	.388	1.87632	1.500	2.203		
ADD HYD	QK3 58&46	59	.04370	80.55	2.895	1.24216	1.500	2.880		
*S AP 13	RVAP5 59&55	60	.04818	92.27	3.270	1.27247	1.500	2.992		
ADD HYD	5H 60&37	62	.04948	95.05	3.366	1.27544	1.500	3.001		
*S ADD WESTERN TO EASTERN BASINS	RVAP6 62&50	63	.05818	113.65	4.009	1.29194	1.500	3.052		
ADD HYD	DE 29&31	66	.00990	21.16	.732	1.38579	1.500	3.339		
ADD HYD	DE6 66&63	67	.06808	134.81	4.741	1.30558	1.500	3.094		
ADD HYD	A1A2 23&24	64	.00350	7.50	.259	1.38566	1.500	3.348		
ADD HYD	A1A2B 64&25	68	.01130	24.16	.835	1.38576	1.500	3.340		
ADD HYD	A12BC 68&27	70	.01320	28.23	.976	1.38575	1.500	3.341		
ADD HYD	RVAP7 70&67	71	.08128	163.03	5.716	1.31860	1.500	3.134		
ADD HYD	PONDIN 71&39	73	.08338	168.76	5.937	1.33492	1.500	3.162		
*S DIVIDE BASIN S: STONEBRIDGE WILL ACCEPT 8 CFS										
*S AP 4	DIVIDE HYD	SB AND	73 51	.01704	8.00	1.213	1.33492	1.250	.734	
	TOBLACK		52	.06635	160.76	4.724	1.33492	1.500	3.786	
*S BASINS FROM WEST OF UNSER										
*S WEST OF DUNLOP										
*S AP 12	DB1	-	1	.04200	94.60	3.364	1.50198	1.500	3.520 PER IMP= 6.00	
COMPUTE NM HYD	DB2	-	2	.05920	134.92	4.798	1.50198	1.500	3.519 PER IMP= 6.00	
COMPUTE NM HYD	DB3	-	3	.05280	118.93	4.230	1.50198	1.500	3.519 PER IMP= 6.00	
COMPUTE NM HYD	DB4A	-	4	.02240	52.72	1.874	1.50198	1.500	3.520 PER IMP= 6.00	
COMPUTE NM HYD	DB4B	-	14	.02000	45.06	1.602	1.50198	1.500	3.520 PER IMP= 6.00	
COMPUTE NM HYD	DB4C	-	15	.00226	6.62	.251	1.83565	1.500	4.040 PER IMP= 9.00	
COMPUTE NM HYD	DB5A	-	5	.00420	10.85	.411	1.83565	1.500	4.036 PER IMP= 9.00	
COMPUTE NM HYD	DB5B	-	13	.01100	28.39	1.077	1.83565	1.500	4.033 PER IMP= 9.00	
COMPUTE NM HYD	DB6	-	6	.03030	78.18	2.966	1.83565	1.500	4.032 PER IMP= 9.00	
COMPUTE NM HYD	DB7A	-	7	.01216	32.03	1.211	1.86802	1.500	4.116 PER IMP= 9.00	
COMPUTE NM HYD	DB7B	-	12	.00800	21.08	.797	1.86802	1.500	4.117 PER IMP= 9.00	
COMPUTE NM HYD	DB8	-	8	.00700	18.07	.685	1.83565	1.500	4.034 PER IMP= 9.00	
COMPUTE NM HYD	NUNSER	-	9	.00350	9.23	.349	1.86802	1.500	4.120 PER IMP= 9.00	
COMPUTE NM HYD	MUNSER	-	10	.00500	13.18	.498	1.86802	1.500	4.119 PER IMP= 9.00	
COMPUTE NM HYD	SUNSER	-	16	.00820	21.61	.817	1.86802	1.500	4.117 PER IMP= 9.00	
*S COMMERCIAL TRACT ON SE CORNER OF MCMAHON AND UNSER	DC2	-	11	.01610	41.55	1.576	1.83565	1.500	4.032 PER IMP= 9.00	
ADD HYD	LOS 8& 3	17	.05980	137.00	4.915	1.54103	1.500	3.580		
*S ROUTE AND ADD RESIDENTIAL FLOWS ALONG BLACK ARROYO										
*S WEST OF UNSER BLVD.	ROUTE	DB1R	1 20	.04200	88.80	3.364	1.50199	1.550	3.304	
*S AP 8	1R2 20& 2	22	.10190	220.96	8.163	1.50197	1.500	3.388		
ADD HYD	DB2R 22	23	.10190	214.91	8.163	1.50198	1.550	3.295		
ROUTE	123.00 23&17	24	.16170	340.57	13.078	1.51642	1.500	3.291		
*S AP 9	DB3R	24 25	.16170	343.10	13.078	1.51642	1.550	3.315		

```

*S INPUT = 01177\cdp\hydro\master\commercial developed\Master.TXT
*S Revised 10-17-01 for Master Storm Drain in Unser/McMahon
*S This analysis assumes that McMahon flow is diverted down Unser Blvd
*S and Black Arroyo Blvd without ponding.
*S Ridgeview Village(DB4), Los Suenos(DB3), and the Park Hill(DB2)
*S Subdivisions have free developed discharge based on R-1, 5 du/acre density.
*S Flow from some commercial sites east of Unser between McMahon and
*S Black Arroyo Blvd.is restricted to historic as per Ridgeview Unit 1 Plan.
*S Developed flow is accommodated from the residential tracts and
*S other commercial tracts. See Land Treatment Exhibit for specific tracts.
*
START          RAINFALL BEGINS AT 0.00 HOURS
*           100-YEAR RETURN PERIOD
*****
*:
*:          MISC. DATA
*:          RAINFALL RETURN PERIOD _____ 100-YEAR   :::
*:          RAINFALL DURATION _____ 6-HOUR    :::
*:          ZONE 1          :::
*:          RAINFALL DEPTHS: 1 HOUR (P60) 1.85 INCHES      :::
*:          (UNADJUSTED)      6 HOUR (P360) 2.20 INCHES      :::
*:          24 HOUR (P1440) 2.75 INCHES      :::
*:
*:          RAINFALL DATA TAKEN FROM NOAA.      :::
*:
*:          HYDROGRAPH METHODOLOGY      :::
*:
*:          CITY OF ALBQ. DPM VOL. 2, SECTION 22.2 July, 1997      :::
*:          INITIAL ABSTRACTION - INFILTRATION METHOD      :::
*:          Tc CALCULATIONS PER C.O.A. DPM 22.2-B.4      :::
*:          AMAFCA AHYMO VERSION MARCH 20,1992      :::
*:
*:
*:          BEGIN ANALYSIS
*****
*:
RAINFALL          TYPE=1 RAIN QUARTER=0.0 RAIN ONE=1.85
                  RAIN SIX=2.20 RAIN DAY=2.75 DT=0.05
*****
*S*****FINELAND VILLAGE CENTER BASINS
*****
**** COMPUTE AND PRINT NM HYD DATA FOR BASIN J1 *****
COMPUTE NM HYD      ID=3 HYD=J1 AREA=0.0078 PER A=0.0 PER B=10.0
                  PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
PRINT HYD          ID=3 CODE=1
**** COMPUTE AND PRINT NM HYD DATA FOR BASIN J2 *****
COMPUTE NM HYD      ID=4 HYD=J2 AREA=0.0064 PER A=0.0 PER B=10.0
                  PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
PRINT HYD          ID=4 CODE=1
**** COMPUTE AND PRINT NM HYD DATA FOR BASIN K *****
COMPUTE NM HYD      ID=5 HYD=K AREA=0.0032 PER A=0.0 PER B=15.0
                  PER C=20.0 PER D=65.0 TP=.133 RAINFALL=-1
PRINT HYD          ID=5 CODE=1
**** COMPUTE AND PRINT NM HYD DATA FOR BASIN L *****
COMPUTE NM HYD      ID=7 HYD=L AREA=0.0014 PER A=1.0 PER B=15.0

```

```

        PER C=20.0 PER D=65.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=7 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN M *****
COMPUTE NM HYD      ID=9 HYD=M AREA=0.0048 PER A=0.0 PER B=15.0
                    PER C=20.0 PER D=65.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=9 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN IN (KUNATH) *****
COMPUTE NM HYD      ID=11 HYD=IN AREA=0.0083 PER A=0.0 PER B=10.0
                    PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=11 CODE=1
*
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN O *****
COMPUTE NM HYD      ID=13 HYD=O AREA=0.0072 PER A=95.0 PER B=5.0
                    PER C=0.0 PER D=0.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=13 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN P *****
COMPUTE NM HYD      ID=15 HYD=P AREA=0.0057 PER A=95.0 PER B=5.0
                    PER C=0.0 PER D=0.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=15 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN Q *****
COMPUTE NM HYD      ID=17 HYD=Q AREA=0.0051 PER A=95.0 PER B=5.0
                    PER C=0.0 PER D=0.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=17 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN R *****
COMPUTE NM HYD      ID=19 HYD=R AREA=0.006 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=19 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN S *****
COMPUTE NM HYD      ID=21 HYD=S AREA=0.011 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=21 CODE=1
*
*****
*S*****RIDGEVIEW UNIT 1 BASINS
*****
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN A1 *****
COMPUTE NM HYD      ID=23 HYD=A1 AREA=0.0023 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=23 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN A2 *****
COMPUTE NM HYD      ID=24 HYD=A2 AREA=0.0012 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=24 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN B *****
COMPUTE NM HYD      ID=25 HYD=B AREA=0.0078 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=25 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN C *****
COMPUTE NM HYD      ID=27 HYD=C AREA=0.0019 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=27 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN D *****
COMPUTE NM HYD      ID=29 HYD=D AREA=0.0079 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=29 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN E *****
COMPUTE NM HYD      ID=31 HYD=E AREA=0.002 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=31 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN F *****
COMPUTE NM HYD      ID=33 HYD=F AREA=0.0051 PER A=0.0 PER B=25.0
                    PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD      ID=33 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN G *****
COMPUTE NM HYD      ID=35 HYD=G AREA=0.0136 PER A=0.0 PER B=25.0

```

```

PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD ID=35 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN H *****
COMPUTE NM HYD ID=37 HYD=H AREA=0.0013 PER A=0.0 PER B=25.0
PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD ID=37 CODE=1
*
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN WESTSIDE *****
COMPUTE NM HYD ID=39 HYD=WEST AREA=0.0021 PER A=0.0 PER B=0.0
PER C=0.0 PER D=100.0 TP=.133 RAINFALL=-1
PRINT HYD ID=39 CODE=1
*S ADD SOUTH-WESTERN BASINS
ADD HYD ID=40 HYD=OP ID I=13 ID II=15
PRINT HYD ID=40 CODE=1
*
ADD HYD ID=41 HYD=OPIN I=40 ID II=11
PRINT HYD ID=41 CODE=1
*
* ADD BASIN J
*
ADD HYD ID=45 HYD=OPINJ1 ID I=41 ID II=3
PRINT HYD ID=45 CODE=1
*
*S AP #3
ADD HYD ID=46 HYD=RVAP3 ID I=45 ID II=4
PRINT HYD ID=46 CODE=1
*
*S AP#4
* ADD BASIN G
ADD HYD ID=50 HYD=RVAP4 ID I=33 ID II=35
PRINT HYD ID=50 CODE=1
*
*S ****
*S ADD SOUTH-EASTERN BASINS
*S STONEBRIDGE WILL ACCEPT 9.69 CFS AT FEATHER ROCK
DIVIDE HYD ID=9 Q=9.69 IDI=80 HYD=SB2
IDII=81 HYD=M2
*
*S FEIN SUBDIVISION DISCHARGES INTO STONEBRIDGE PER CSC
ADD HYD ID=54 HYD=SR ID I=21 ID II=19
PRINT HYD ID=54 CODE=1
*
ADD HYD ID=55 HYD=ML ID I=81 ID II=7
PRINT HYD ID=55 CODE=1
*
ADD HYD ID=58 HYD=QK ID I=17 ID II=5
PRINT HYD ID=58 CODE=1
*
ADD HYD ID=59 HYD=QK3 ID I=58 ID II=46
PRINT HYD ID=59 CODE=1
*
ADD HYD ID=60 HYD=RVAP5 ID I=59 ID II=55
PRINT HYD ID=60 CODE=1
*
ADD HYD ID=62 HYD=5H ID I=60 ID II=37
PRINT HYD ID=62 CODE=1
*
*S ADD WESTERN TO EASTERN BASINS
*S AP#6
ADD HYD ID=63 HYD=RVAP6 ID I=62 ID II=50
PRINT HYD ID=63 CODE=1
*
ADD HYD ID=66 HYD=DE ID I=29 ID II=31
PRINT HYD ID=66 CODE=1
*
```

```

ADD HYD           ID=67 HYD=DE6 ID I=66 ID II=63
PRINT HYD        ID=67 CODE=1
*
ADD HYD           ID=64 HYD=A1A2 ID I=23 ID II=24
PRINT HYD        ID=64 CODE=1
*
ADD HYD           ID=68 HYD=A1A2B ID I=64 ID II=25
PRINT HYD        ID=68 CODE=1
*
ADD HYD           ID=70 HYD=A12BC ID I=68 ID II=27
PRINT HYD        ID=70 CODE=1
*S AP#7
ADD HYD           ID=71 HYD=RVAP7 ID I=70 ID II=67
PRINT HYD        ID=71 CODE=1
*
ADD HYD           ID=73 HYD=PONDIN ID I=71 ID II=39
PRINT HYD        ID=73 CODE=1
*S DIVIDE BASIN S: STONEBRIDGE WILL ACCEPT 8 CFS
DIVIDE HYD       ID=73 Q=.0      IDI=51 HYD=SB
                           IDII=52 HYD=TOBLACK
*****
*S BASINS FROM WEST OF UNSER
*S WEST OF DUNLOP
COMPUTE NM HYD    ID=1 HYD=DB1 AREA=0.042 PER A=0.0 PER B=20.0
                  PER C=20.0 PER D=60.0 TP=.133 RAINFALL=-1
PRINT HYD         ID=1 CODE=1
*
***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 2 DUNLOP*****
COMPUTE NM HYD    ID=2 HYD=DB2 AREA=0.0599 PER A=0.0 PER B=20.0
                  PER C=20.0 PER D=60.0 TP=.133 RAINFALL=-1
PRINT HYD         ID=2 CODE=1
*
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN OFFSITE BASIN 3 LOS SUENOS *****
COMPUTE NM HYD    ID=3 HYD=DB3 AREA=0.0528 PER A=0.0 PER B=20.0
                  PER C=20.0 PER D=60.0 TP=.133 RAINFALL=-1
PRINT HYD         ID=3 CODE=1
*
*****
COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 4A RIDGEVIEW VILLAGE-BL ARROYO*****
COMPUTE NM HYD    ID=4 HYD=DB4A AREA=0.0234 PER A=0.0 PER B=20.0
                  PER C=20.0 PER D=60.0 TP=.133 RAINFALL=-1
PRINT HYD         ID=4 CODE=1
*
***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 4B RIDGEVIEW VILLAGE-UNSER*****
COMPUTE NM HYD    ID=14 HYD=DB4B AREA=0.02 PER A=0.0 PER B=20.0
                  PER C=20.0 PER D=60.0 TP=.133 RAINFALL=-1
PRINT HYD         ID=14 CODE=1
*
***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 4C RIDGEVIEW VILLAGE OFFICE*****
COMPUTE NM HYD    ID=15 HYD=DB4C AREA=0.00256 PER A=0.0 PER B=10.0
                  PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
PRINT HYD         ID=15 CODE=1
*
* PINON HEIGHTS COMMERCIAL TRACT
***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 5A *****
COMPUTE NM HYD    ID=5 HYD=DB5A AREA=0.0042 PER A=0.0 PER B=10.0
                  PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
PRINT HYD         ID=5 CODE=1
*
* PINON HEIGHTS COMMERCIAL TRACT
***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 5B *****
COMPUTE NM HYD    ID=13 HYD=DB5B AREA=0.011 PER A=0.0 PER B=10.0
                  PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
PRINT HYD         ID=13 CODE=1
*

```

***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 6 TRES ESQUINAS COMMERCIAL *****
 COMPUTE NM HYD ID=6 HYD=DB6 AREA=0.0303 PER A=0.0 PER B=10.0
 PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
 PRINT HYD ID=6 CODE=1
 * (NOT INCL UNSER)
 ***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE MCMAHON WEST *****
 COMPUTE NM HYD ID=7 HYD=DB7A AREA=0.01216 PER A=0.0 PER B=0.0
 PER C=10.0 PER D=90.0 TP=.133 RAINFALL=-1
 PRINT HYD ID=7 CODE=1
 *
 ***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN MCMAHON EAST *****
 COMPUTE NM HYD ID=12 HYD=DB7B AREA=0.008 PER A=0.0 PER B=0.0
 PER C=10.0 PER D=90.0 TP=.133 RAINFALL=-1
 PRINT HYD ID=12 CODE=1
 *
 ***** COMPUTE AND PRINT NM HYD DATA FOR OFFSITE BASIN 8 LOS SUENOS COMMERCIAL*****
 COMPUTE NM HYD ID=8 HYD=DB8 AREA=0.007 PER A=0.0 PER B=10.0
 PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
 PRINT HYD ID=8 CODE=1
 ***** COMPUTE AND PRINT NM HYD DATA FOR BASIN OFFSITE BASIN 9 - NORTH UNSER *****
 COMPUTE NM HYD ID=9 HYD=MUNSER AREA=0.0035 PER A=0.0 PER B=0.0
 PER C=10.0 PER D=90.0 TP=.133 RAINFALL=-1
 PRINT HYD ID=9 CODE=1
 *
 ***** COMPUTE AND PRINT NM HYD DATA FOR BASIN OFFSITE BASIN 10 - MID UNSER *****
 COMPUTE NM HYD ID=10 HYD=MUNSER AREA=0.005 PER A=0.0 PER B=0.0
 PER C=10.0 PER D=90.0 TP=.133 RAINFALL=-1
 PRINT HYD ID=10 CODE=1
 *
 ***** COMPUTE AND PRINT NM HYD DATA FOR BASIN OFFSITE BASIN 16 - SOUTH UNSER *****
 COMPUTE NM HYD ID=16 HYD=SUNSER AREA=0.0082 PER A=0.0 PER B=0.0
 PER C=10.0 PER D=90.0 TP=.133 RAINFALL=-1
 PRINT HYD ID=16 CODE=1
 *
 *S COMMERCIAL TRACT ON SE CORNER OF MCMAHON AND UNSER
 COMPUTE NM HYD ID=11 HYD=DC2 AREA=0.0161 PER A=0.0 PER B=10.0
 PER C=0.0 PER D=90.0 TP=.133 RAINFALL=-1
 PRINT HYD ID=11 CODE=1
 *
 * ADD LOS SUENOS COMMERCIAL TO RESIDENTIAL
 ADD HYD ID=17 HYD=LOS ID I=8 ID II=3
 PRINT HYD ID=17 CODE=1

 *S ROUTE AND ADD RESIDENTIAL FLOWS ALONG BLACK ARROYO
 *S WEST OF UNSER BLVD.
 * ROUTE DB1 ACROSS DUNLOP PROPERTY ON BLACK ARROYO BLVD
 COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.02
 DIAM=2.5 FT N=0.014
 COMPUTE TRAVEL TIME ID=20 REACH NO=1 NO VS=1 L=1305 FT
 SLOPE=0.02
 ROUTE ID=20 HYD NO=DB1R INFLOW ID=1
 *
 * ADD ROUTED DB1 TO DUNLOP DB2
 ADD HYD ID=22 HYD=1R2 ID I=20 ID II=2
 PRINT HYD ID=22 CODE=1
 *
 * ROUTE DB1 + DUNLOP ON BLACK ARROYO ACROSS LOS SUENOS
 COMPUTE RATING CURVE CID=1 VS NO=2 CODE=-1 SLP=0.02
 DIAM=4 FT N=0.014
 COMPUTE TRAVEL TIME ID=23 REACH NO=2 NO VS=1 L=1374 FT
 SLOPE=0.02
 ROUTE ID=23 HYD NO=DB2R INFLOW ID=22
 *
 * ADD LOS SUENOS TO DUNLOP
 ADD HYD ID=24 HYD=123 ID I=23 ID II=17


```

*
*S ROUTE UNSER/BLACK ARROYO FLOW TO EAST OF RIDGEVIEW 1
*
COMPUTE RATING CURVE CID=1 VS NO=5 CODE=-1 SLP=0.02
DIAM=6.5 FT N=0.014
COMPUTE TRAVEL TIME ID=47 REACH NO=5 NO VS=1 L=1226 FT
SLOPE=0.005
ROUTE ID=47 HYD NO=RV1 INFLOW ID=46
*
*S ADD RIDGEVIEW 1 AND FINELAND VILLAGE CENTER FLOWS TO PIPE
ADD HYD ID=48 HYD=RV ID I=47 ID II=52
PRINT HYD ID=48 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN 2 *****
COMPUTE NM HYD ID=2 HYD=2 AREA=0.001 PER A=0.0 PER B=25.0
PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD ID=2 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BASIN 3 *****
COMPUTE NM HYD ID=3 HYD=3 AREA=0.00144 PER A=0.0 PER B=25.0
PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD ID=3 CODE=1
***** COMPUTE AND PRINT NM HYD DATA FOR BLACK ARROYO BLVD ADJ TO RIDGEVIEW 2 *****
COMPUTE NM HYD ID=4 HYD=WEST AREA=0.0011 PER A=0.0 PER B=0.0
PER C=10.0 PER D=90.0 TP=.133 RAINFALL=-1
PRINT HYD ID=4 CODE=1
* ADD BASIN 2 INTO BLACK ARROYO BLVD
ADD HYD ID=12 HYD=WEST2 ID I=4 ID II=2
PRINT HYD ID=12 CODE=1
* ADD BASIN 3 INTO BLACK ARROYO BLVD
*S TOTAL STREET FLOW IN BLACK ARROYO BLVD EAST OF RIDGEVIEW UNIT 2
ADD HYD ID=14 HYD=WEST23 ID I=12 ID II=3
PRINT HYD ID=14 CODE=1
*
*S STONEBRIDGE CONTRIBUTION
**** COMPUTE AND PRINT NM HYD DATA FOR BASIN BLACK ARROYO ADJ TO STONEBRIDGE *****
COMPUTE NM HYD ID=5 HYD=ROAD AREA=0.0021 PER A=0.0 PER B=0.0
PER C=10.0 PER D=90.0 TP=.133 RAINFALL=-1
PRINT HYD ID=5 CODE=1
**** COMPUTE AND PRINT NM HYD DATA FOR STONEBRIDGE CUL-DE-SACS *****
COMPUTE NM HYD ID=6 HYD=CULSACS AREA=0.00279 PER A=0.0 PER B=25.0
PER C=25.0 PER D=50.0 TP=.133 RAINFALL=-1
PRINT HYD ID=6 CODE=1
*
ADD HYD ID=7 HYD=SBROAD ID I=5 ID II=6
PRINT HYD ID=7 CODE=1
*
*S STREET FLOW IN BLACK ARROYO BLVD EAST OF STONEBRIDGE
ADD HYD ID=16 HYD=ESB ID I=7 ID II=14
PRINT HYD ID=16 CODE=1
*
*S TOTAL PIPE FLOW IN BLACK ARROYO BLVD
ADD HYD ID=18 HYD=AP5 ID I=16 ID II=48
PRINT HYD ID=18 CODE=1
*
FINISH

```

UNSER STREET FLOW

ees.

6-14-01

• UNSER SOUTH OF McMAHON

$$Q = 21.9 \text{ cfs}$$

$$S = 0.961\%$$

half street capacity = 30.1 per PC Stream output

See attached cross section for input

Install inlets instead of valley gutters.

$$\text{half street flow} = 10.95 \text{ cfs.}$$

$$\text{depth} = 0.48'$$

$$\text{flow in each grate} = 5.5 \text{ cfs / grate.}$$

use 2 inlets on each side.

• Unser North of McMahon at Southern Boundary of Ridgewood Subdivision

$$Q = 13.18 \text{ cfs. } S = 0.51$$

$$\text{half street capacity} = 37.6 \text{ cfs.}$$

Install inlets instead of valley gutters.

$$\text{half street flow} = 6.6 \text{ cfs.}$$

$$\text{depth} = 0.44' \text{ see PC stream output}$$

$$Q \text{ in each grate} = 3.4 \text{ cfs.}$$

Install two grates on each side of Unser.

Bohannan □ Huston

PROJECT NAME _____

SHEET _____

OF _____

PROJECT NO. _____

BY _____

DATE _____

SUBJECT _____

CH'D _____

DATE _____

ENGINEERS PLANNERS PHOTOGRAPHERS
SURVEYORS SOFTWARE DEVELOPERS



B-8

PC PROGRAM STREAM

SEPTEMBER 1994

UNSER SOUTH

MANNING'S N= .017 SLOPE= .0096

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
(FT)	INC	AREA	RATE	PER	VEL		HEAD	HEAD
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)
1	0.00	0.93	4	15.00	0.13	7	0.00	0.00
2	13.00	0.67	5	53.00	0.89	8	0.00	0.00
3	13.10	0.00	6	53.10	1.22	9	0.00	0.00
0.01	0.01	0.00	0.0	0.16	0.24	0.15	0.00	0.01
0.02	0.02	0.00	0.0	0.31	0.38	0.30	0.00	0.02
0.03	0.03	0.01	0.0	0.47	0.50	0.44	0.00	0.03
0.04	0.04	0.01	0.0	0.63	0.61	0.59	0.01	0.05
0.05	0.05	0.02	0.0	0.78	0.70	0.74	0.01	0.06
0.06	0.06	0.03	0.0	0.94	0.80	0.89	0.01	0.07
0.07	0.07	0.04	0.0	1.10	0.88	1.03	0.01	0.08
0.08	0.08	0.05	0.0	1.25	0.96	1.18	0.01	0.09
0.09	0.09	0.06	0.1	1.41	1.04	1.33	0.02	0.11
0.10	0.10	0.07	0.1	1.57	1.12	1.48	0.02	0.12
0.11	0.11	0.09	0.1	1.72	1.19	1.62	0.02	0.13
0.12	0.12	0.11	0.1	1.88	1.26	1.77	0.02	0.14
0.13	0.13	0.12	0.2	2.04	1.33	1.92	0.03	0.16
0.14	0.14	0.15	0.2	2.55	1.28	2.42	0.03	0.17
0.15	0.15	0.17	0.2	3.06	1.26	2.92	0.02	0.17
0.16	0.16	0.20	0.3	3.57	1.28	3.42	0.03	0.19
0.17	0.17	0.24	0.3	4.08	1.30	3.93	0.03	0.20
0.18	0.18	0.28	0.4	4.59	1.34	4.43	0.03	0.21
0.19	0.19	0.33	0.5	5.10	1.38	4.93	0.03	0.22
0.20	0.20	0.38	0.5	5.61	1.43	5.43	0.03	0.23
0.21	0.21	0.44	0.6	6.12	1.48	5.93	0.03	0.24
0.22	0.22	0.50	0.8	6.63	1.53	6.43	0.04	0.26
0.23	0.23	0.57	0.9	7.14	1.58	6.93	0.04	0.27
0.24	0.24	0.64	1.0	7.65	1.64	7.44	0.04	0.28
0.25	0.25	0.72	1.2	8.16	1.69	7.94	0.04	0.29
0.26	0.26	0.80	1.4	8.67	1.75	8.44	0.05	0.31
0.27	0.27	0.88	1.6	9.18	1.80	8.94	0.05	0.32
0.28	0.28	0.98	1.8	9.69	1.86	9.44	0.05	0.33
0.29	0.29	1.07	2.1	10.20	1.91	9.94	0.06	0.35
0.30	0.30	1.18	2.3	10.71	1.96	10.44	0.06	0.36
0.31	0.31	1.28	2.6	11.22	2.02	10.95	0.06	0.37
0.32	0.32	1.39	2.9	11.73	2.07	11.45	0.07	0.39
0.33	0.33	1.51	3.2	12.24	2.12	11.95	0.07	0.40
0.34	0.34	1.63	3.6	12.75	2.18	12.45	0.07	0.41
0.35	0.35	1.76	3.9	13.26	2.23	12.95	0.08	0.43
0.36	0.36	1.89	4.3	13.77	2.28	13.45	0.08	0.44
0.37	0.37	2.03	4.7	14.28	2.33	13.96	0.08	0.45
0.38	0.38	2.17	5.2	14.79	2.38	14.46	0.09	0.47
0.39	0.39	2.32	5.6	15.30	2.43	14.96	0.09	0.48
0.40	0.40	2.47	6.1	15.81	2.48	15.46	0.10	0.50
0.41	0.41	2.63	6.7	16.32	2.53	15.96	0.10	0.51
0.42	0.42	2.79	7.2	16.83	2.58	16.46	0.10	0.52
0.43	0.43	2.96	7.8	17.34	2.63	16.96	0.11	0.54
0.44	0.44	3.13	8.4	17.85	2.68	17.47	0.11	0.55
0.45	0.45	3.49	9.7	18.37	2.73	18.47	0.12	0.58
0.47	0.47	3.68	10.4	19.38	2.83	18.97	0.12	0.59
0.48	0.48	3.87	11.1	19.89	2.87	19.47	0.13	0.61
0.49	0.49	4.07	11.9	20.40	2.92	19.97	0.13	0.62
0.50	0.50	4.27	12.7	20.91	2.97	20.47	0.14	0.64
0.51	0.51	4.47	13.5	21.42	3.02	20.98	0.14	0.65
0.52	0.52	4.69	14.3	21.93	3.06	21.48	0.15	0.67
0.53	0.53	4.90	15.2	22.44	3.11	21.98	0.15	0.68

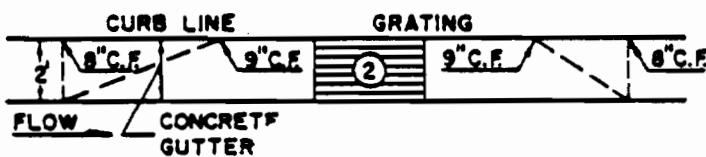
B-10

WSEL (FT)	DEPTH INC (FT)	FLOW AREA SQ. FT.	FLOW RATE (CFS)	WETTED PER (FT)	FLOW VEL (FPS)	TOPWID (FT)	VEL HEAD (FT)	ENERGY HEAD (FT)
0.54	0.54	5.13	16.2	22.95	3.15	22.48	0.15	0.69
0.55	0.55	5.35	17.1	23.46	3.20	22.98	0.16	0.71
0.56	0.56	5.59	18.1	23.97	3.24	23.48	0.16	0.72
0.57	0.57	5.82	19.1	24.49	3.29	23.99	0.17	0.74
0.58	0.58	6.07	20.2	25.00	3.33	24.49	0.17	0.75
0.59	0.59	6.31	21.3	25.51	3.38	24.99	0.18	0.77
0.60	0.60	6.57	22.5	26.02	3.42	25.49	0.18	0.78
0.61	0.61	6.82	23.6	26.53	3.46	25.99	0.19	0.80
0.62	0.62	7.09	24.9	27.04	3.51	26.49	0.19	0.81
0.63	0.63	7.35	26.1	27.55	3.55	26.99	0.20	0.83
0.64	0.64	7.63	27.4	28.06	3.59	27.50	0.20	0.84
0.65	0.65	7.90	28.7	28.57	3.64	28.00	0.21	0.86
0.66	0.66	8.19	30.1	29.08	3.68	28.50	0.21	0.87
0.67	0.67	8.47	31.5	29.59	3.72	29.00	0.21	0.88
0.68	0.68	8.77	32.6	30.59	3.72	30.00	0.22	0.90
0.69	0.69	9.07	33.8	31.59	3.73	31.00	0.22	0.91
0.70	0.70	9.39	35.1	32.59	3.74	32.00	0.22	0.92
0.71	0.71	9.71	36.4	33.59	3.75	33.00	0.22	0.93
0.72	0.72	10.05	37.7	34.59	3.76	34.00	0.22	0.94
0.73	0.73	10.39	39.2	35.59	3.77	35.00	0.22	0.95
0.74	0.74	10.75	40.7	36.59	3.78	36.00	0.22	0.96
0.75	0.75	11.11	42.2	37.59	3.80	37.00	0.22	0.97
0.76	0.76	11.49	43.9	38.59	3.82	38.00	0.23	0.99
0.77	0.77	11.87	45.6	39.59	3.84	39.00	0.23	1.00
0.78	0.78	12.27	47.3	40.59	3.86	40.00	0.23	1.01
0.79	0.79	12.67	49.1	41.59	3.88	41.00	0.23	1.02
0.80	0.80	13.09	51.0	42.59	3.90	42.00	0.24	1.04
0.81	0.81	13.51	53.0	43.59	3.92	43.00	0.24	1.05
0.82	0.82	13.95	55.0	44.59	3.95	44.00	0.24	1.06
0.83	0.83	14.39	57.2	45.59	3.97	45.00	0.24	1.07
0.84	0.84	14.85	59.3	46.59	4.00	46.00	0.25	1.09
0.85	0.85	15.31	61.6	47.59	4.02	47.00	0.25	1.10
0.86	0.86	15.79	63.9	48.59	4.05	48.00	0.25	1.11
0.87	0.87	16.27	66.3	49.59	4.07	49.00	0.26	1.13
0.88	0.88	16.77	68.8	50.59	4.10	50.00	0.26	1.14
0.89	0.89	17.27	71.3	51.59	4.13	51.00	0.26	1.15
0.90	0.90	17.79	74.4	52.10	4.18	51.50	0.27	1.17
0.91	0.91	18.30	77.5	52.61	4.24	52.01	0.28	1.19
0.92	0.92	18.83	80.7	53.12	4.29	52.51	0.29	1.21
0.93	0.93	19.35	84.0	53.63	4.34	53.01	0.29	1.22
0.94	0.94	19.88	87.9	53.64	4.42	53.02	0.30	1.24
0.95	0.95	20.41	91.8	53.65	4.50	53.02	0.31	1.26
0.96	0.96	20.94	95.8	53.67	4.57	53.02	0.32	1.28
0.97	0.97	21.47	99.9	53.68	4.65	53.02	0.34	1.31
0.98	0.98	22.00	104.0	53.69	4.73	53.03	0.35	1.33
0.99	0.99	22.53	108.2	53.70	4.80	53.03	0.36	1.35
1.01	1.01	23.60	116.8	53.72	4.95	53.04	0.38	1.39
1.02	1.02	24.13	121.2	53.73	5.02	53.04	0.39	1.41
1.03	1.03	24.66	125.6	53.74	5.09	53.04	0.40	1.43
1.04	1.04	25.19	130.1	53.75	5.17	53.05	0.41	1.45
1.05	1.05	25.72	134.7	53.76	5.24	53.05	0.43	1.48
1.06	1.06	26.25	139.4	53.77	5.31	53.05	0.44	1.50
1.07	1.07	26.78	144.1	53.78	5.38	53.05	0.45	1.52
1.08	1.08	27.31	148.8	53.79	5.45	53.06	0.46	1.54
1.09	1.09	27.84	153.7	53.80	5.52	53.06	0.47	1.56
1.10	1.10	28.37	158.6	53.81	5.59	53.06	0.49	1.59
1.11	1.11	28.90	163.5	53.82	5.66	53.07	0.50	1.61
1.12	1.12	29.43	168.5	53.83	5.73	53.07	0.51	1.63
1.13	1.13	29.96	173.6	53.84	5.79	53.07	0.52	1.65
1.14	1.14	30.49	178.7	53.85	5.86	53.08	0.53	1.67
1.15	1.15	31.02	183.9	53.86	5.93	53.08	0.55	1.70

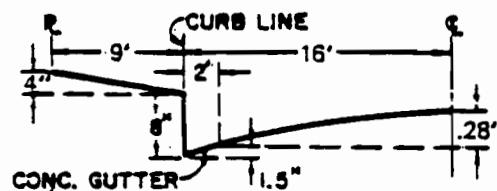
Unser South of McMahon

22.0

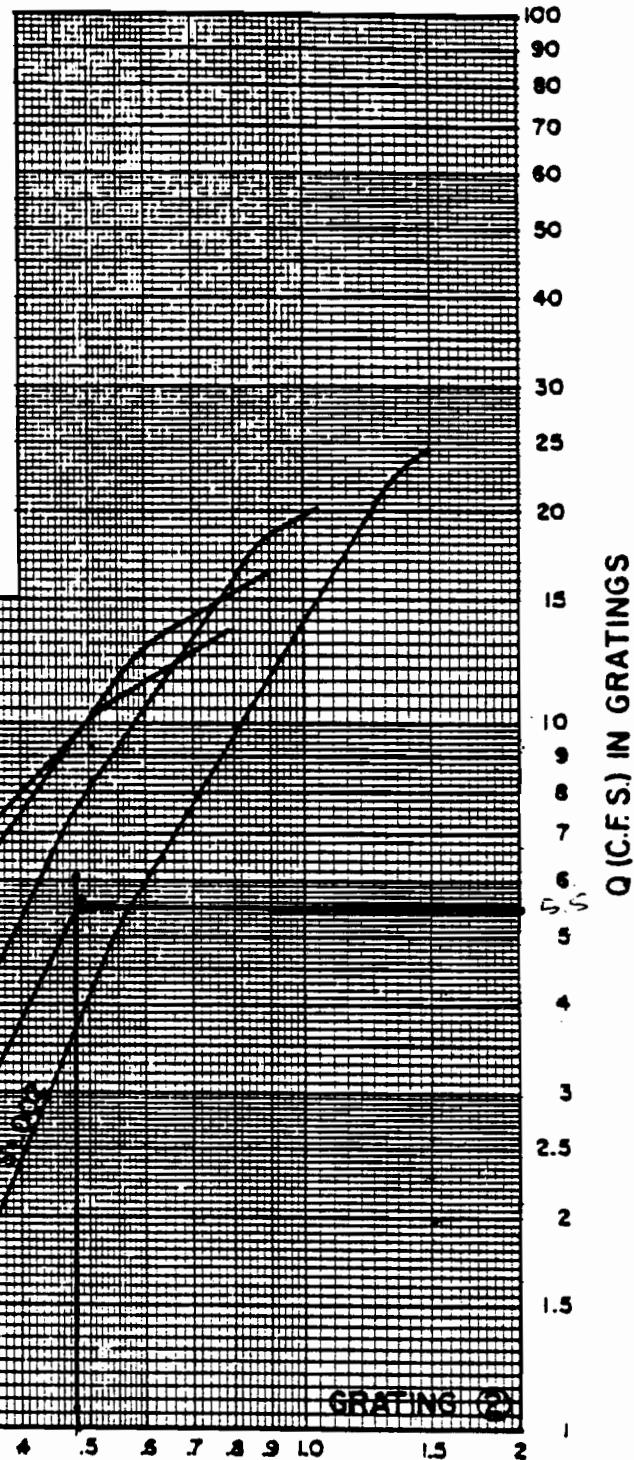
GRATING CAPACITIES FOR TYPE "A", "C" and "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION
(ABOVE BASIN)



D = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

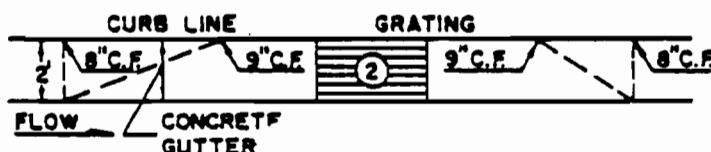
$$d = 0.48$$

$$S = 0.96\%$$

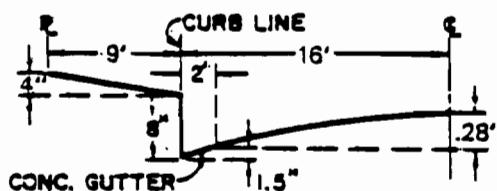
$$Q = 5.5 \text{ cfs/grade}$$

UNSER BWD. at Ridgview

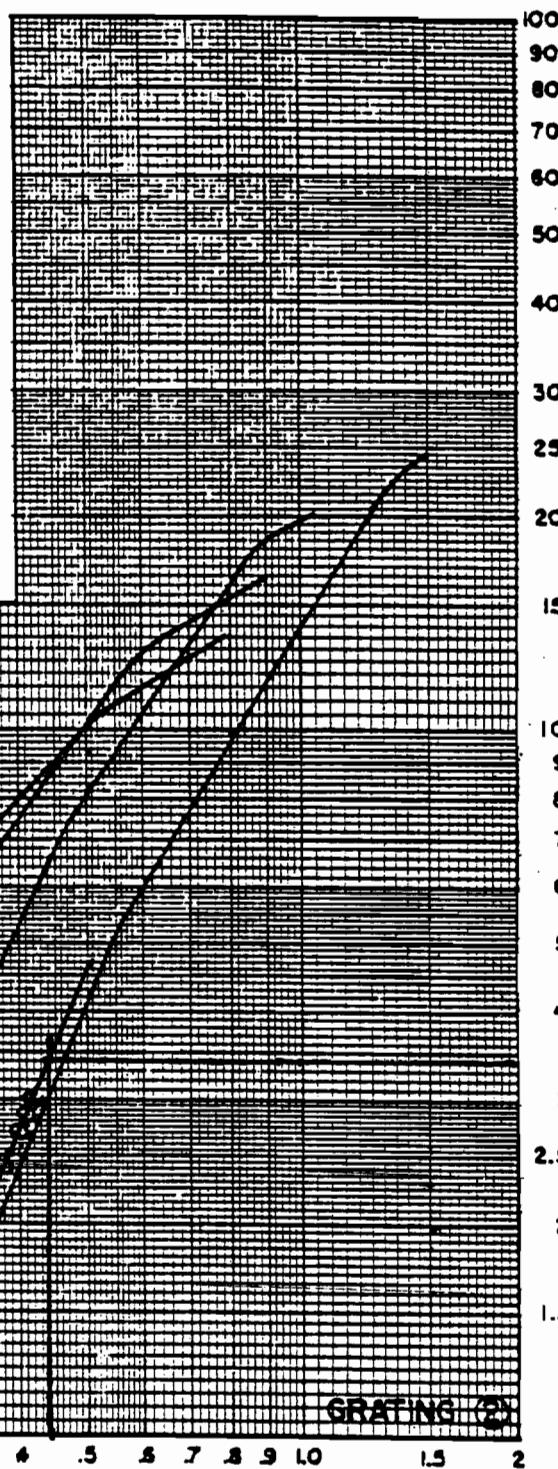
GRATING CAPACITIES FOR TYPE "A", "C" and "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION
(ABOVE BASIN)



D=DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

$$S = 0.51$$

$$\Delta = 0.44$$

$$Q = 3.4 \text{ cfs}$$

PC PROGRAM STREAM

SEPTEMBER 1994

MIDDLE UNSER BLVD.

MANNING'S N= .017 SLOPE= .005

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
	INC	AREA	RATE	PER	VEL		HEAD	HEAD
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)
0.01	0.01	0.00	0.0	0.16	0.17	0.15	0.00	0.01
0.02	0.02	0.00	0.0	0.31	0.28	0.30	0.00	0.02
0.03	0.03	0.01	0.0	0.47	0.36	0.44	0.00	0.03
0.04	0.04	0.01	0.0	0.63	0.44	0.59	0.00	0.04
0.05	0.05	0.02	0.0	0.78	0.51	0.74	0.00	0.05
0.06	0.06	0.03	0.0	0.94	0.57	0.89	0.01	0.07
0.07	0.07	0.04	0.0	1.10	0.64	1.03	0.01	0.08
0.08	0.08	0.05	0.0	1.25	0.70	1.18	0.01	0.09
0.09	0.09	0.06	0.0	1.41	0.75	1.33	0.01	0.10
0.10	0.10	0.07	0.1	1.57	0.81	1.48	0.01	0.11
0.11	0.11	0.09	0.1	1.72	0.86	1.62	0.01	0.12
0.12	0.12	0.11	0.1	1.88	0.91	1.77	0.01	0.13
0.13	0.13	0.12	0.1	2.04	0.96	1.92	0.01	0.14
0.14	0.14	0.15	0.1	2.55	0.92	2.42	0.01	0.15
0.15	0.15	0.17	0.2	3.06	0.91	2.92	0.01	0.16
0.16	0.16	0.20	0.2	3.57	0.92	3.42	0.01	0.17
0.17	0.17	0.24	0.2	4.08	0.94	3.93	0.01	0.18
0.18	0.18	0.28	0.3	4.59	0.97	4.43	0.01	0.19
0.19	0.19	0.33	0.3	5.10	1.00	4.93	0.02	0.21
0.20	0.20	0.38	0.4	5.61	1.03	5.43	0.02	0.22
0.21	0.21	0.44	0.5	6.12	1.07	5.93	0.02	0.23
0.22	0.22	0.50	0.6	6.63	1.10	6.43	0.02	0.24
0.23	0.23	0.57	0.6	7.14	1.14	6.93	0.02	0.25
0.24	0.24	0.64	0.8	7.65	1.18	7.44	0.02	0.26
0.25	0.25	0.72	0.9	8.16	1.22	7.94	0.02	0.27
0.26	0.26	0.80	1.0	8.67	1.26	8.44	0.02	0.28
0.27	0.27	0.88	1.2	9.18	1.30	8.94	0.03	0.30
0.28	0.28	0.98	1.3	9.69	1.34	9.44	0.03	0.31
0.29	0.29	1.07	1.5	10.20	1.38	9.94	0.03	0.32
0.30	0.30	1.18	1.7	10.71	1.42	10.44	0.03	0.33
0.31	0.31	1.28	1.9	11.22	1.46	10.95	0.03	0.34
0.32	0.32	1.39	2.1	11.73	1.49	11.45	0.03	0.35
0.33	0.33	1.51	2.3	12.24	1.53	11.95	0.04	0.37
0.34	0.34	1.63	2.6	12.75	1.57	12.45	0.04	0.38
0.35	0.35	1.76	2.8	13.26	1.61	12.95	0.04	0.39
0.36	0.36	1.89	3.1	13.77	1.65	13.45	0.04	0.40
0.37	0.37	2.03	3.4	14.28	1.68	13.96	0.04	0.41
0.38	0.38	2.17	3.7	14.79	1.72	14.46	0.05	0.43
0.39	0.39	2.32	4.1	15.30	1.76	14.96	0.05	0.44
0.40	0.40	2.47	4.4	15.81	1.79	15.46	0.05	0.45
0.41	0.41	2.63	4.8	16.32	1.83	15.96	0.05	0.46
0.42	0.42	2.79	5.2	16.83	1.87	16.46	0.05	0.47
0.43	0.43	2.96	5.6	17.34	1.90	16.96	0.05	0.49
0.44	0.44	3.13	6.1	17.85	1.94	17.47	0.06	0.50
0.45	0.46	3.49	7.0	18.87	2.01	18.47	0.06	0.52
0.47	0.47	3.68	7.5	19.38	2.04	18.97	0.06	0.53
0.48	0.48	3.87	8.0	19.89	2.07	19.47	0.07	0.55
0.49	0.49	4.07	8.6	20.40	2.11	19.97	0.07	0.56
0.50	0.50	4.27	9.1	20.91	2.14	20.47	0.07	0.57
0.51	0.51	4.47	9.7	21.42	2.18	20.98	0.07	0.58
0.52	0.52	4.69	10.4	21.93	2.21	21.43	0.08	0.60
0.53	0.53	4.90	11.1	22.44	2.24	21.83	0.08	0.61

B-14

Under Bed at the County line

$Q = 9.23 \text{ cfs}$ half street flow = 4.6 cfs .

$S = 3.5\%$

$d = 0.3'$

$Q_{\text{in inlet}} = 3.7 \text{ cfs}$.

Install one inlet on each side

PROJECT NAME _____ SHEET _____ OF _____
PROJECT NO. _____ BY _____ DATE _____
SUBJECT _____ C-H'D _____ DATE _____

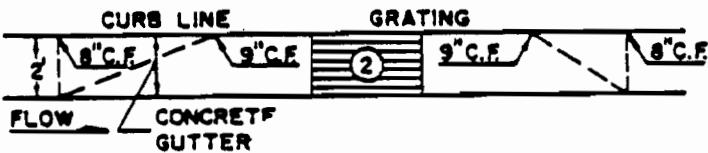


Bohannan & Huston

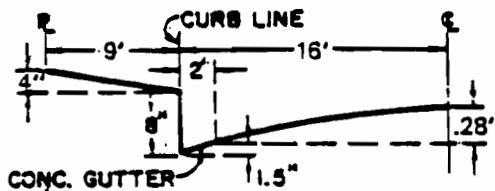
B-15

ENGINEERS PLANNERS PHOTOGRAMMETRISTS
SURVEYORS SOFTWARE DEVELOPERS

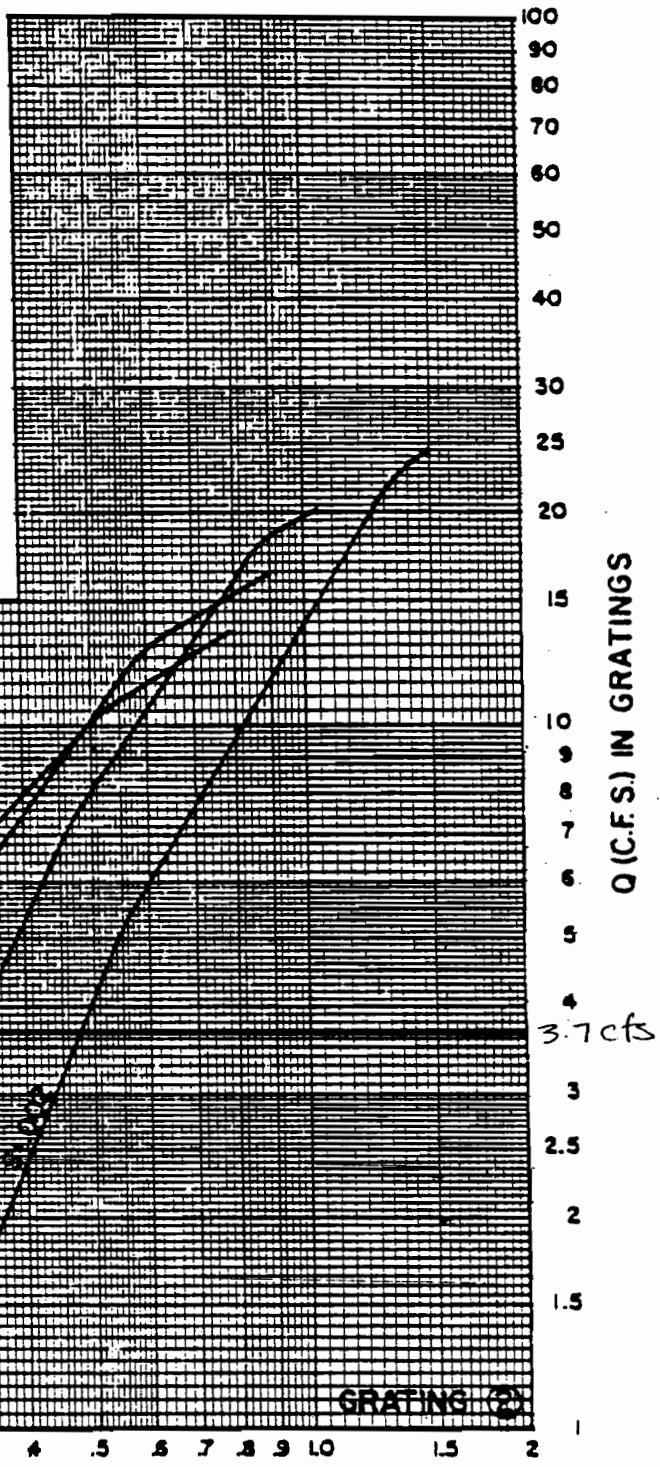
Under at the County Line
GRATING CAPACITIES FOR TYPE "A", "C" and "D"



GRATING & GUTTER PLAN



**TYPICAL HALF STREET SECTION
(ABOVE BASIN)**



D=DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

$$d = 0.3'$$

$$S = 3.5\%$$

$$Q = 3.7 \text{ cfs / grate}$$

PC PROGRAM STREAM

SEPTEMBER 1994

UNSER NORTH

MANNING'S N= .017 SLOPE= .035

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
	INC	AREA	RATE	PER	VEL	HEAD	HEAD	
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	
0.01	0.01	0.00	0.0	0.16	0.46	0.15	0.00	0.01
0.02	0.02	0.00	0.0	0.31	0.73	0.30	0.01	0.03
0.03	0.03	0.01	0.0	0.47	0.96	0.44	0.01	0.04
0.04	0.04	0.01	0.0	0.63	1.16	0.59	0.02	0.06
0.05	0.05	0.02	0.0	0.78	1.34	0.74	0.03	0.08
0.06	0.06	0.03	0.0	0.94	1.52	0.89	0.04	0.10
0.07	0.07	0.04	0.1	1.10	1.68	1.03	0.04	0.11
0.08	0.08	0.05	0.1	1.25	1.84	1.18	0.05	0.13
0.09	0.09	0.06	0.1	1.41	1.99	1.33	0.06	0.15
0.10	0.10	0.07	0.2	1.57	2.13	1.48	0.07	0.17
0.11	0.11	0.09	0.2	1.72	2.27	1.62	0.08	0.19
0.12	0.12	0.11	0.3	1.88	2.41	1.77	0.09	0.21
0.13	0.13	0.12	0.3	2.04	2.54	1.92	0.10	0.23
0.14	0.14	0.15	0.4	2.55	2.44	2.42	0.09	0.23
0.15	0.15	0.17	0.4	3.06	2.41	2.92	0.09	0.24
0.16	0.16	0.20	0.5	3.57	2.43	3.42	0.09	0.25
0.17	0.17	0.24	0.6	4.08	2.49	3.93	0.10	0.27
0.18	0.18	0.28	0.7	4.59	2.56	4.43	0.10	0.28
0.19	0.19	0.33	0.9	5.10	2.64	4.93	0.11	0.30
0.20	0.20	0.38	1.0	5.61	2.73	5.43	0.12	0.32
0.21	0.21	0.44	1.2	6.12	2.82	5.93	0.12	0.33
0.22	0.22	0.50	1.5	6.63	2.92	6.43	0.13	0.35
0.23	0.23	0.57	1.7	7.14	3.02	6.93	0.14	0.37
0.24	0.24	0.64	2.0	7.65	3.13	7.44	0.15	0.39
0.25	0.25	0.72	2.3	8.16	3.23	7.94	0.16	0.41
0.26	0.26	0.80	2.7	8.67	3.33	8.44	0.17	0.43
0.27	0.27	0.88	3.0	9.18	3.44	8.94	0.18	0.45
0.28	0.28	0.98	3.5	9.69	3.54	9.44	0.19	0.47
0.29	0.29	1.07	3.9	10.20	3.65	9.94	0.21	0.50
0.30	0.30	1.18	4.4	10.71	3.75	10.44	0.22	0.52
0.31	0.31	1.28	4.9	11.22	3.85	10.95	0.23	0.54
0.32	0.32	1.39	5.5	11.73	3.95	11.45	0.24	0.56
0.33	0.33	1.51	6.1	12.24	4.06	11.95	0.26	0.59
0.34	0.34	1.63	6.8	12.75	4.16	12.45	0.27	0.61
0.35	0.35	1.76	7.5	13.26	4.26	12.95	0.28	0.63
0.36	0.36	1.89	8.2	13.77	4.36	13.45	0.29	0.65
0.37	0.37	2.03	9.0	14.28	4.45	13.96	0.31	0.68
0.38	0.38	2.17	9.9	14.79	4.55	14.46	0.32	0.70
0.39	0.39	2.32	10.8	15.30	4.65	14.96	0.34	0.73
0.40	0.40	2.47	11.7	15.81	4.74	15.46	0.35	0.75
0.41	0.41	2.63	12.7	16.32	4.84	15.96	0.36	0.77
0.42	0.42	2.79	13.8	16.83	4.93	16.46	0.38	0.80
0.43	0.43	2.96	14.9	17.34	5.03	16.96	0.39	0.82
0.44	0.44	3.13	16.0	17.85	5.12	17.47	0.41	0.85
0.46	0.46	3.49	18.5	18.87	5.31	18.47	0.44	0.90
0.47	0.47	3.68	19.8	19.38	5.40	18.97	0.45	0.92
0.48	0.48	3.87	21.2	19.89	5.49	19.47	0.47	0.95
0.49	0.49	4.07	22.7	20.40	5.58	19.97	0.48	0.97
0.50	0.50	4.27	24.2	20.91	5.67	20.47	0.50	1.00
0.51	0.51	4.47	25.8	21.42	5.76	20.98	0.51	1.02
0.52	0.52	4.69	27.4	21.93	5.85	21.43	0.53	1.05
0.53	0.53	4.90	29.1	22.4	5.93	21.98	0.55	1.08

B - 7

WSEL (FT)	DEPTH INC (FT)	FLOW AREA SQ.FT.	FLOW RATE (CFS)	WETTED PER (FT)	FLOW VEL (FPS)	TOPWID (FT)	VEL HEAD (FT)	ENERGY HEAD (FT)
0.54	0.54	5.13	30.9	22.95	6.02	22.48	0.56	1.10
0.55	0.55	5.35	32.7	23.46	6.11	22.98	0.58	1.13
0.56	0.56	5.59	34.6	23.97	6.19	23.48	0.60	1.16
0.57	0.57	5.82	36.6	24.49	6.28	23.99	0.61	1.18
0.58	0.58	6.07	38.6	25.00	6.36	24.49	0.63	1.21
0.59	0.59	6.31	40.7	25.51	6.45	24.99	0.65	1.24
0.60	0.60	6.57	42.9	26.02	6.53	25.49	0.66	1.26
0.61	0.61	6.82	45.1	26.53	6.61	25.99	0.68	1.29
0.62	0.62	7.09	47.5	27.04	6.70	26.49	0.70	1.32
0.63	0.63	7.35	49.9	27.55	6.78	26.99	0.71	1.34
0.64	0.64	7.63	52.3	28.06	6.86	27.50	0.73	1.37
0.65	0.65	7.90	54.9	28.57	6.94	28.00	0.75	1.40
0.66	0.66	8.19	57.5	29.08	7.02	28.50	0.77	1.43
0.67	0.67	8.47	60.2	29.59	7.10	29.00	0.78	1.45
0.68	0.68	8.77	62.3	30.59	7.11	30.00	0.78	1.46
0.69	0.69	9.07	64.6	31.59	7.12	31.00	0.79	1.48
0.70	0.70	9.39	67.0	32.59	7.13	32.00	0.79	1.49
0.71	0.71	9.71	69.5	33.59	7.15	33.00	0.79	1.50
0.72	0.72	10.05	72.1	34.59	7.17	34.00	0.80	1.52
0.73	0.73	10.39	74.8	35.59	7.20	35.00	0.80	1.53
0.74	0.74	10.75	77.7	36.59	7.23	36.00	0.81	1.55
0.75	0.75	11.11	80.7	37.59	7.26	37.00	0.82	1.57
0.76	0.76	11.49	83.8	38.59	7.29	38.00	0.83	1.59
0.77	0.77	11.87	87.0	39.59	7.33	39.00	0.83	1.60
0.78	0.78	12.27	90.4	40.59	7.37	40.00	0.84	1.62
0.79	0.79	12.67	93.8	41.59	7.41	41.00	0.85	1.64
0.80	0.80	13.09	97.5	42.59	7.45	42.00	0.86	1.66
0.81	0.81	13.51	101.2	43.59	7.49	43.00	0.87	1.68
0.82	0.82	13.95	105.1	44.59	7.54	44.00	0.88	1.70
0.83	0.83	14.39	109.1	45.59	7.58	45.00	0.89	1.72
0.84	0.84	14.85	113.3	46.59	7.63	46.00	0.90	1.74
0.85	0.85	15.31	117.6	47.59	7.68	47.00	0.92	1.77
0.86	0.86	15.79	122.0	48.59	7.73	48.00	0.93	1.79
0.87	0.87	16.27	126.6	49.59	7.78	49.00	0.94	1.81
0.88	0.88	16.77	131.3	50.59	7.83	50.00	0.95	1.83
0.89	0.89	17.27	136.2	51.59	7.88	51.00	0.97	1.86
0.90	0.90	17.79	142.1	52.10	7.99	51.50	0.99	1.89
0.91	0.91	18.30	148.1	52.61	8.09	52.01	1.02	1.93
0.92	0.92	18.83	154.2	53.12	8.19	52.51	1.04	1.96
0.93	0.93	19.35	160.4	53.63	8.29	53.01	1.07	2.00
0.94	0.94	19.88	167.8	53.64	8.44	53.02	1.11	2.05
0.95	0.95	20.41	175.3	53.65	8.59	53.02	1.14	2.09
0.96	0.96	20.94	182.9	53.67	8.73	53.02	1.18	2.14
0.97	0.97	21.47	190.7	53.68	8.88	53.02	1.22	2.19
0.98	0.98	22.00	198.6	53.69	9.02	53.03	1.26	2.24
0.99	0.99	22.53	206.6	53.70	9.17	53.03	1.30	2.29

Black Arroyo Street Capacity

6-14-01
EES.

- Black Arroyo at east boundary of Ridgewood Unit 1

$$Q = 5.73 \text{ cfs}$$

$$S = 6.15\%$$

$D = 0.24'$ < curb height see PC Stream output
no inlets required

- Black Arroyo at east boundary of Ridgewood Unit 2.

$$Q = 5.73 \text{ RVI}$$

$$+ 8.15 \text{ RV2}$$

$$\underline{13.88 \text{ cfs}}$$

$$S = 1.63\%$$

depth = $0.36'$ < curb height
no inlets required

- Black Arroyo at east boundary of Stonebridge 4.

$$13.88 \text{ cfs} \text{ Ridgewood 1+2}$$

$$+ 11.51 \text{ cfs} \text{ Stonebridge 4}$$

$$\underline{25.39 \text{ cfs}}$$

$$S = 0.5\% \text{ depth} = 0.51'$$

and

$$S = 5.88\% \text{ depth} = 0.36'$$

and

$$S = 1.73\% \text{ at outfall depth} = 0.43'$$

Install inlets

Q in each inlet = 5.5 cfs/grate

Install 5 inlets

Bohannan Huston



PROJECT NAME _____ SHEET _____ OF _____

PROJECT NO. _____ BY _____ DATE _____

SUBJECT _____ CH'D _____ DATE _____

B-19

ENGINEERS PLANNERS PHOTOGRAMMETRISTS
SURVEYORS SOFTWARE DEVELOPERS

Black Arroyo Blvd. east of Ridgewood 1

PC PROGRAM STREAM

SEPTEMBER 1994

MANNING'S N= .017 SLOPE= .0615

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
1	0.00	0.87	5	12.00	0.13	9	50.17	0.67
2	9.38	0.67	6	30.00	0.41	10	50.63	0.67
3	9.83	0.67	7	48.00	0.13	11	60.00	0.83
4	10.00	0.00	8	50.00	0.00	12	0.00	0.00
WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
(FT)	(FT)	INC	AREA	RATE	PER	VEL	HEAD	HEAD
0.01	0.01	0.00	0.0	0.33	0.61	0.31	0.01	0.02
0.02	0.02	0.01	0.0	0.66	0.97	0.63	0.01	0.03
0.03	0.03	0.01	0.0	0.99	1.27	0.94	0.03	0.06
0.04	0.04	0.03	0.0	1.32	1.54	1.25	0.04	0.08
0.05	0.05	0.04	0.1	1.64	1.79	1.56	0.05	0.10
0.06	0.06	0.06	0.1	1.97	2.02	1.88	0.06	0.12
0.07	0.07	0.08	0.2	2.30	2.24	2.19	0.08	0.15
0.08	0.08	0.10	0.2	2.63	2.45	2.50	0.09	0.17
0.09	0.09	0.13	0.3	2.96	2.65	2.81	0.11	0.20
0.10	0.10	0.16	0.4	3.29	2.84	3.13	0.13	0.23
0.11	0.11	0.19	0.6	3.62	3.03	3.44	0.14	0.25
0.12	0.12	0.23	0.7	3.95	3.21	3.75	0.16	0.28
0.13	0.13	0.26	0.9	4.28	3.39	4.07	0.18	0.31
0.14	0.14	0.31	1.0	5.58	3.16	5.36	0.16	0.30
0.15	0.15	0.37	1.1	6.89	3.09	6.65	0.15	0.30
0.16	0.16	0.44	1.4	8.20	3.11	7.94	0.15	0.31
0.17	0.17	0.53	1.7	9.50	3.17	9.23	0.16	0.33
0.18	0.18	0.63	2.0	10.81	3.25	10.52	0.16	0.34
0.19	0.19	0.74	2.5	12.12	3.36	11.81	0.18	0.37
0.20	0.20	0.87	3.0	13.42	3.48	13.10	0.19	0.39
0.21	0.21	1.00	3.6	14.73	3.61	14.39	0.20	0.41
0.22	0.22	1.15	4.3	16.04	3.75	15.68	0.22	0.44
0.23	0.23	1.32	5.1	17.34	3.89	16.97	0.23	0.46
0.24	0.24	1.49	6.0	18.65	4.03	18.26	0.25	0.49
0.25	0.25	1.68	7.0	19.95	4.17	19.56	0.27	0.52
0.26	0.26	1.88	8.1	21.26	4.31	20.85	0.29	0.55
0.27	0.27	2.10	9.3	22.57	4.45	22.14	0.31	0.58
0.28	0.28	2.33	10.7	23.87	4.59	23.43	0.33	0.61
0.29	0.29	2.57	12.1	25.18	4.73	24.72	0.35	0.64
0.30	0.30	2.82	13.7	26.49	4.87	26.01	0.37	0.67
0.31	0.31	3.09	15.5	27.79	5.01	27.30	0.39	0.70
0.32	0.32	3.37	17.3	29.10	5.15	28.59	0.41	0.73
0.33	0.33	3.66	19.3	30.41	5.28	29.88	0.43	0.76
0.34	0.34	3.96	21.5	31.71	5.42	31.17	0.46	0.80
0.35	0.35	4.28	23.8	33.02	5.55	32.46	0.48	0.83
0.36	0.36	4.61	26.2	34.33	5.69	33.75	0.50	0.86
0.37	0.37	4.96	28.9	35.63	5.82	35.04	0.53	0.90
0.38	0.38	5.31	31.6	36.94	5.95	36.34	0.55	0.93
0.39	0.39	5.68	34.6	38.25	6.08	37.63	0.57	0.96
0.40	0.40	6.07	37.7	39.55	6.21	38.92	0.60	1.00
0.41	0.41	6.46	41.0	40.86	6.34	40.21	0.62	1.03
0.42	0.42	6.86	45.3	40.88	6.60	40.21	0.68	1.10
0.43	0.43	7.27	49.8	40.90	6.85	40.22	0.73	1.16
0.45	0.45	8.07	59.3	40.94	7.34	40.23	0.84	1.29
0.46	0.46	8.47	64.3	40.96	7.58	40.23	0.89	1.35
0.47	0.47	8.88	69.4	40.98	7.82	40.24	0.95	1.42
0.48	0.48	9.23	74.7	41.00	8.05	40.24	1.01	1.49
0.49	0.49	9.68	80.1	41.02	8.28	40.25	1.06	1.55
0.50	0.50	10.03	85.7	41.04	8.50	40.25	1.12	1.62

B-20

Black Arroyo Blvd at Ridgeview

***** PC PROGRAM STREAM SEPTEMBER 1994 *****

MANNING'S N= .017 SLOPE= .0163

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
1	0.00	0.87	5	12.00	0.13	9	50.17	0.67
2	9.38	0.67	6	30.00	0.41	10	50.63	0.67
3	9.83	0.67	7	48.00	0.13	11	60.00	0.83
4	10.00	0.00	8	50.00	0.00	12	0.00	0.00
WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
(FT)	(FT)	INC	AREA	RATE	PER	VEL	HEAD	HEAD
0.01	0.01	0.00	0.0	0.33	0.32	0.31	0.00	0.01
0.02	0.02	0.01	0.0	0.66	0.50	0.63	0.00	0.02
0.03	0.03	0.01	0.0	0.99	0.66	0.94	0.01	0.04
0.04	0.04	0.03	0.0	1.32	0.80	1.25	0.01	0.05
0.05	0.05	0.04	0.0	1.64	0.92	1.56	0.01	0.06
0.06	0.06	0.06	0.1	1.97	1.04	1.88	0.02	0.08
0.07	0.07	0.08	0.1	2.30	1.15	2.19	0.02	0.09
0.08	0.08	0.10	0.1	2.63	1.26	2.50	0.02	0.10
0.09	0.09	0.13	0.2	2.96	1.37	2.81	0.03	0.12
0.10	0.10	0.16	0.2	3.29	1.46	3.13	0.03	0.13
0.11	0.11	0.19	0.3	3.62	1.56	3.44	0.04	0.15
0.12	0.12	0.23	0.4	3.95	1.65	3.75	0.04	0.16
0.13	0.13	0.26	0.5	4.28	1.74	4.07	0.05	0.18
0.14	0.14	0.31	0.5	5.58	1.63	5.36	0.04	0.18
0.15	0.15	0.37	0.6	6.89	1.59	6.65	0.04	0.19
0.16	0.16	0.44	0.7	8.20	1.60	7.94	0.04	0.20
0.17	0.17	0.53	0.9	9.50	1.63	9.23	0.04	0.21
0.18	0.18	0.63	1.1	10.81	1.68	10.52	0.04	0.22
0.19	0.19	0.74	1.3	12.12	1.73	11.81	0.05	0.24
0.20	0.20	0.87	1.6	13.42	1.79	13.10	0.05	0.25
0.21	0.21	1.00	1.9	14.73	1.86	14.39	0.05	0.26
0.22	0.22	1.15	2.2	16.04	1.93	15.68	0.06	0.28
0.23	0.23	1.32	2.6	17.34	2.00	16.97	0.06	0.29
0.24	0.24	1.49	3.1	18.65	2.07	18.26	0.07	0.31
0.25	0.25	1.68	3.6	19.95	2.15	19.56	0.07	0.32
0.26	0.26	1.88	4.2	21.26	2.22	20.85	0.08	0.34
0.27	0.27	2.10	4.8	22.57	2.29	22.14	0.08	0.35
0.28	0.28	2.33	5.5	23.87	2.36	23.43	0.09	0.37
0.29	0.29	2.57	6.3	25.18	2.44	24.72	0.09	0.38
0.30	0.30	2.82	7.1	26.49	2.51	26.01	0.10	0.40
0.31	0.31	3.09	8.0	27.79	2.58	27.30	0.10	0.41
0.32	0.32	3.37	8.9	29.10	2.65	28.59	0.11	0.43
0.33	0.33	3.66	10.0	30.41	2.72	29.88	0.11	0.44
0.34	0.34	3.96	11.1	31.71	2.79	31.17	0.12	0.46
0.35	0.35	4.28	12.2	33.02	2.86	32.46	0.13	0.48
0.36	0.36	4.61	13.5	34.33	2.93	33.75	0.13	0.49
0.37	0.37	4.96	14.9	35.63	3.00	35.04	0.14	0.51
0.38	0.38	5.31	16.3	36.94	3.06	36.34	0.15	0.53
0.39	0.39	5.68	17.8	38.25	3.13	37.63	0.15	0.54
0.40	0.40	6.07	19.4	39.55	3.20	38.92	0.16	0.56
0.41	0.41	6.46	21.1	40.86	3.26	40.21	0.17	0.58
0.42	0.42	6.86	23.3	40.88	3.40	40.21	0.18	0.60
0.43	0.43	7.27	25.6	40.90	3.53	40.22	0.19	0.62
0.45	0.45	8.07	30.5	40.94	3.78	40.23	0.22	0.67
0.46	0.46	8.47	33.1	40.96	3.90	40.23	0.24	0.70
0.47	0.47	8.88	35.7	40.98	4.02	40.24	0.25	0.72
0.48	0.48	9.28	38.5	41.00	4.14	40.24	0.27	0.75
0.49	0.49	9.68	41.3	41.02	4.26	40.25	0.28	0.77
0.50	0.50	10.08	44.1	41.04	4.38	40.25	0.30	0.80
0.51	0.51	10.49	47.1	41.07	4.49	40.26	0.31	0.82
0.52	0.52	10.89	50.1	41.09	4.60	40.26	0.33	0.85
0.53	0.53	11.29	53.2	41.11	4.72	40.27	0.35	0.88
0.54	0.54	11.69	56.4	41.13	4.83	40.27	0.36	0.90

Black Arroyo Blvd. Adjacent to Stonebridge 4

***** PC PROGRAM STREAM SEPTEMBER 1994 *****

MANNING'S N= .017 SLOPE= .05875

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
1	0.00	0.87	5	12.00	0.13	9	50.17	0.67
2	9.38	0.67	6	30.00	0.41	10	50.63	0.67
3	9.83	0.67	7	48.00	0.13	11	60.00	0.83
4	10.00	0.00	8	50.00	0.00	12	0.00	0.00
WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
	INC	AREA	RATE	PER	VEL		HEAD	HEAD
(FT)	(FT)	SQ.FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)	(FT)
0.01	0.01	0.00	0.0	0.33	0.60	0.31	0.01	0.02
0.02	0.02	0.01	0.0	0.66	0.95	0.63	0.01	0.03
0.03	0.03	0.01	0.0	0.99	1.25	0.94	0.02	0.05
0.04	0.04	0.03	0.0	1.32	1.51	1.25	0.04	0.08
0.05	0.05	0.04	0.1	1.64	1.75	1.56	0.05	0.10
0.06	0.06	0.06	0.1	1.97	1.98	1.88	0.06	0.12
0.07	0.07	0.08	0.2	2.30	2.19	2.19	0.07	0.14
0.08	0.08	0.10	0.2	2.63	2.40	2.50	0.09	0.17
0.09	0.09	0.13	0.3	2.96	2.59	2.81	0.10	0.19
0.10	0.10	0.16	0.4	3.29	2.78	3.13	0.12	0.22
0.11	0.11	0.19	0.6	3.62	2.96	3.44	0.14	0.25
0.12	0.12	0.23	0.7	3.95	3.14	3.75	0.15	0.27
0.13	0.13	0.26	0.9	4.28	3.31	4.07	0.17	0.30
0.14	0.14	0.31	1.0	5.58	3.09	5.36	0.15	0.29
0.15	0.15	0.37	1.1	6.89	3.02	6.65	0.14	0.29
0.16	0.16	0.44	1.3	8.20	3.03	7.94	0.14	0.30
0.17	0.17	0.53	1.6	9.50	3.09	9.23	0.15	0.32
0.18	0.18	0.63	2.0	10.81	3.18	10.52	0.16	0.34
0.19	0.19	0.74	2.4	12.12	3.29	11.81	0.17	0.36
0.20	0.20	0.87	2.9	13.42	3.41	13.10	0.18	0.38
0.21	0.21	1.00	3.5	14.73	3.53	14.39	0.19	0.40
0.22	0.22	1.15	4.2	16.04	3.66	15.68	0.21	0.43
0.23	0.23	1.32	5.0	17.34	3.80	16.97	0.22	0.45
0.24	0.24	1.49	5.9	18.65	3.93	18.26	0.24	0.48
0.25	0.25	1.68	6.8	19.95	4.07	19.56	0.26	0.51
0.26	0.26	1.88	7.9	21.26	4.21	20.85	0.28	0.54
0.27	0.27	2.10	9.1	22.57	4.35	22.14	0.29	0.56
0.28	0.28	2.33	10.4	23.87	4.49	23.43	0.31	0.59
0.29	0.29	2.57	11.9	25.18	4.62	24.72	0.33	0.62
0.30	0.30	2.82	13.4	26.49	4.76	26.01	0.35	0.65
0.31	0.31	3.09	15.1	27.79	4.90	27.30	0.37	0.68
0.32	0.32	3.37	16.9	29.10	5.03	28.59	0.39	0.71
0.33	0.33	3.66	18.9	30.41	5.16	29.88	0.41	0.74
0.34	0.34	3.96	21.0	31.71	5.30	31.17	0.44	0.78
0.35	0.35	4.28	23.2	33.02	5.43	32.46	0.46	0.81
0.36	0.36	4.61	25.6	34.33	5.56	33.75	0.48	0.84
0.37	0.37	4.96	28.2	35.63	5.69	35.04	0.50	0.87
0.38	0.38	5.31	30.9	36.94	5.82	36.34	0.53	0.91
0.39	0.39	5.68	33.8	38.25	5.94	37.63	0.55	0.94
0.40	0.40	6.07	36.8	39.55	6.07	38.92	0.57	0.97
0.41	0.41	6.46	40.0	40.86	6.20	40.21	0.60	1.01
0.42	0.42	6.86	44.3	40.88	6.45	40.21	0.65	1.07
0.43	0.43	7.27	48.7	40.90	6.70	40.22	0.70	1.13
0.45	0.45	8.07	57.9	40.94	7.18	40.23	0.80	1.25
0.46	0.46	8.47	62.8	40.96	7.41	40.23	0.85	1.31
0.47	0.47	8.88	67.8	40.98	7.64	40.24	0.91	1.38
0.48	0.48	9.29	73.0	41.00	7.87	40.24	0.96	1.44
0.49	0.49	9.68	78.3	41.02	8.09	40.25	1.02	1.51
0.50	0.50	10.08	83.8	41.04	8.31	40.25	1.07	1.57
0.51	0.51	10.49	89.4	41.07	8.53	40.26	1.13	1.64

B-22

Black Arroyo Blvd Adjacent to Stonebridge 4

***** PC PROGRAM STREAM SEPTEMBER 1994 *****

MANNING'S N= .017 SLOPE= .005

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
1	0.00	0.87	5	12.00	0.13	9	50.17	0.67
2	9.38	0.67	6	30.00	0.41	10	50.63	0.67
3	9.83	0.67	7	48.00	0.13	11	60.00	0.83
4	10.00	0.00	8	50.00	0.00	12	0.00	0.00
WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
(FT)	(FT)	INC	AREA	RATE	PER	(FT)	HEAD	HEAD
0.01	0.01	0.00	0.0	0.33	0.17	0.31	0.00	0.01
0.02	0.02	0.01	0.0	0.66	0.28	0.63	0.00	0.02
0.03	0.03	0.01	0.0	0.99	0.36	0.94	0.00	0.03
0.04	0.04	0.03	0.0	1.32	0.44	1.25	0.00	0.04
0.05	0.05	0.04	0.0	1.64	0.51	1.56	0.00	0.05
0.06	0.06	0.06	0.0	1.97	0.58	1.88	0.01	0.07
0.07	0.07	0.08	0.0	2.30	0.64	2.19	0.01	0.08
0.08	0.08	0.10	0.1	2.63	0.70	2.50	0.01	0.09
0.09	0.09	0.13	0.1	2.96	0.76	2.81	0.01	0.10
0.10	0.10	0.16	0.1	3.29	0.81	3.13	0.01	0.11
0.11	0.11	0.19	0.2	3.62	0.86	3.44	0.01	0.12
0.12	0.12	0.23	0.2	3.95	0.92	3.75	0.01	0.13
0.13	0.13	0.26	0.3	4.28	0.97	4.07	0.01	0.14
0.14	0.14	0.31	0.3	5.58	0.90	5.36	0.01	0.15
0.15	0.15	0.37	0.3	6.89	0.88	6.65	0.01	0.16
0.16	0.16	0.44	0.4	8.20	0.89	7.94	0.01	0.17
0.17	0.17	0.53	0.5	9.50	0.90	9.23	0.01	0.18
0.18	0.18	0.63	0.6	10.81	0.93	10.52	0.01	0.19
0.19	0.19	0.74	0.7	12.12	0.96	11.81	0.01	0.20
0.20	0.20	0.87	0.9	13.42	0.99	13.10	0.02	0.22
0.21	0.21	1.00	1.0	14.73	1.03	14.39	0.02	0.23
0.22	0.22	1.15	1.2	16.04	1.07	15.68	0.02	0.24
0.23	0.23	1.32	1.5	17.34	1.11	16.97	0.02	0.25
0.24	0.24	1.49	1.7	18.65	1.15	18.26	0.02	0.26
0.25	0.25	1.68	2.0	19.95	1.19	19.56	0.02	0.27
0.26	0.26	1.88	2.3	21.26	1.23	20.85	0.02	0.28
0.27	0.27	2.10	2.7	22.57	1.27	22.14	0.02	0.29
0.28	0.28	2.33	3.0	23.87	1.31	23.43	0.03	0.31
0.29	0.29	2.57	3.5	25.18	1.35	24.72	0.03	0.32
0.30	0.30	2.82	3.9	26.49	1.39	26.01	0.03	0.33
0.31	0.31	3.09	4.4	27.79	1.43	27.30	0.03	0.34
0.32	0.32	3.37	4.9	29.10	1.47	28.59	0.03	0.35
0.33	0.33	3.66	5.5	30.41	1.51	29.88	0.04	0.37
0.34	0.34	3.96	6.1	31.71	1.55	31.17	0.04	0.38
0.35	0.35	4.28	6.8	33.02	1.58	32.46	0.04	0.39
0.36	0.36	4.61	7.5	34.33	1.62	33.75	0.04	0.40
0.37	0.37	4.96	8.2	35.63	1.66	35.04	0.04	0.41
0.38	0.38	5.31	9.0	36.94	1.70	36.34	0.04	0.42
0.39	0.39	5.68	9.9	38.25	1.73	37.63	0.05	0.44
0.40	0.40	6.07	10.7	39.55	1.77	38.92	0.05	0.45
0.41	0.41	6.46	11.7	40.86	1.81	40.21	0.05	0.46
0.42	0.42	6.86	12.9	40.88	1.88	40.21	0.05	0.47
0.43	0.43	7.27	14.2	40.90	1.95	40.22	0.06	0.49
0.45	0.45	8.07	16.9	40.94	2.09	40.23	0.07	0.52
0.46	0.46	8.47	18.3	40.96	2.16	40.23	0.07	0.53
0.47	0.47	8.88	19.8	40.98	2.23	40.24	0.08	0.55
0.48	0.48	9.28	21.3	41.00	2.30	40.24	0.08	0.56
0.49	0.49	9.68	22.9	41.02	2.36	40.25	0.09	0.58
0.50	0.50	10.08	24.4	41.04	2.42	40.25	0.09	0.59
0.51	0.51	10.49	25.1	41.07	2.49	40.25	0.10	0.61
0.52	0.52	12.89	27.3	41.09	2.55	40.25	0.10	0.63

Black Arroyo Blvd east of Stonesbridge

***** PC PROGRAM STREAM SEPTEMBER 1994 *****

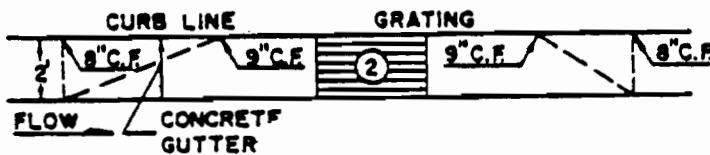
MANNING'S N= .017 SLOPE= .0173

POINT	DIST	ELEV	POINT	DIST	ELEV	POINT	DIST	ELEV
1	0.00	0.87	5	12.00	0.13	9	50.17	0.67
2	9.38	0.67	6	30.00	0.41	10	50.63	0.67
3	9.83	0.67	7	48.00	0.13	11	60.00	0.83
4	10.00	0.00	8	50.00	0.00	12	0.00	0.00
WSEL	DEPTH	FLOW	FLOW	WETTED	FLOW	TOPWID	VEL	ENERGY
(FT)	(FT)	INC	AREA	RATE	PER	VEL	HEAD	HEAD
		(FT)	SQ. FT.	(CFS)	(FT)	(FPS)	(FT)	(FT)
0.01	0.01	0.00	0.0	0.33	0.33	0.31	0.00	0.01
0.02	0.02	0.01	0.0	0.66	0.52	0.63	0.00	0.02
0.03	0.03	0.01	0.0	0.99	0.68	0.94	0.01	0.04
0.04	0.04	0.03	0.0	1.32	0.82	1.25	0.01	0.05
0.05	0.05	0.04	0.0	1.64	0.95	1.56	0.01	0.06
0.06	0.06	0.06	0.1	1.97	1.07	1.88	0.02	0.08
0.07	0.07	0.08	0.1	2.30	1.19	2.19	0.02	0.09
0.08	0.08	0.10	0.1	2.63	1.30	2.50	0.03	0.11
0.09	0.09	0.13	0.2	2.96	1.41	2.81	0.03	0.12
0.10	0.10	0.16	0.2	3.29	1.51	3.13	0.04	0.14
0.11	0.11	0.19	0.3	3.62	1.61	3.44	0.04	0.15
0.12	0.12	0.23	0.4	3.95	1.70	3.75	0.05	0.17
0.13	0.13	0.26	0.5	4.28	1.80	4.07	0.05	0.18
0.14	0.14	0.31	0.5	5.58	1.68	5.36	0.04	0.18
0.15	0.15	0.37	0.6	6.89	1.64	6.65	0.04	0.19
0.16	0.16	0.44	0.7	8.20	1.65	7.94	0.04	0.20
0.17	0.17	0.53	0.9	9.50	1.68	9.23	0.04	0.21
0.18	0.18	0.63	1.1	10.81	1.73	10.52	0.05	0.23
0.19	0.19	0.74	1.3	12.12	1.78	11.81	0.05	0.24
0.20	0.20	0.87	1.6	13.42	1.85	13.10	0.05	0.25
0.21	0.21	1.00	1.9	14.73	1.92	14.39	0.06	0.27
0.22	0.22	1.15	2.3	16.04	1.99	15.68	0.06	0.28
0.23	0.23	1.32	2.7	17.34	2.06	16.97	0.07	0.30
0.24	0.24	1.49	3.2	18.65	2.14	18.26	0.07	0.31
0.25	0.25	1.68	3.7	19.95	2.21	19.56	0.08	0.33
0.26	0.26	1.88	4.3	21.26	2.28	20.85	0.08	0.34
0.27	0.27	2.10	5.0	22.57	2.36	22.14	0.09	0.36
0.28	0.28	2.33	5.7	23.87	2.43	23.43	0.09	0.37
0.29	0.29	2.57	6.4	25.18	2.51	24.72	0.10	0.39
0.30	0.30	2.82	7.3	26.49	2.58	26.01	0.10	0.40
0.31	0.31	3.09	8.2	27.79	2.66	27.30	0.11	0.42
0.32	0.32	3.37	9.2	29.10	2.73	28.59	0.12	0.44
0.33	0.33	3.66	10.3	30.41	2.80	29.88	0.12	0.45
0.34	0.34	3.96	11.4	31.71	2.87	31.17	0.13	0.47
0.35	0.35	4.28	12.6	33.02	2.95	32.46	0.13	0.48
0.36	0.36	4.61	13.9	34.33	3.02	33.75	0.14	0.50
0.37	0.37	4.96	15.3	35.63	3.09	35.04	0.15	0.52
0.38	0.38	5.31	16.8	36.94	3.16	36.34	0.15	0.53
0.39	0.39	5.68	18.3	38.25	3.23	37.63	0.16	0.55
0.40	0.40	6.07	20.0	39.55	3.29	38.92	0.17	0.57
0.41	0.41	6.46	21.7	40.86	3.36	40.21	0.18	0.59
0.42	0.42	6.86	24.0	40.88	3.50	40.21	0.19	0.61
0.43	0.43	7.27	26.4	40.90	3.63	40.22	0.21	0.64
0.45	0.45	8.07	31.4	40.94	3.89	40.23	0.24	0.69
0.46	0.46	8.47	34.1	40.96	4.02	40.23	0.25	0.71
0.47	0.47	8.88	36.8	40.98	4.15	40.24	0.27	0.74
0.48	0.48	9.29	39.5	41.00	4.27	40.24	0.28	0.76
0.49	0.49	9.68	42.5	41.02	4.39	40.25	0.30	0.79
0.50	0.50	10.08	45.5	41.04	4.51	40.25	0.32	0.82

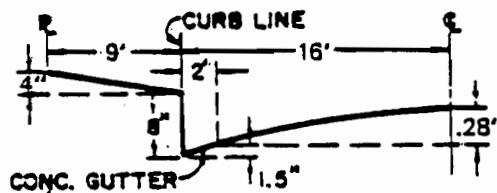
Black Arrows at east end of Stonebridge

4400

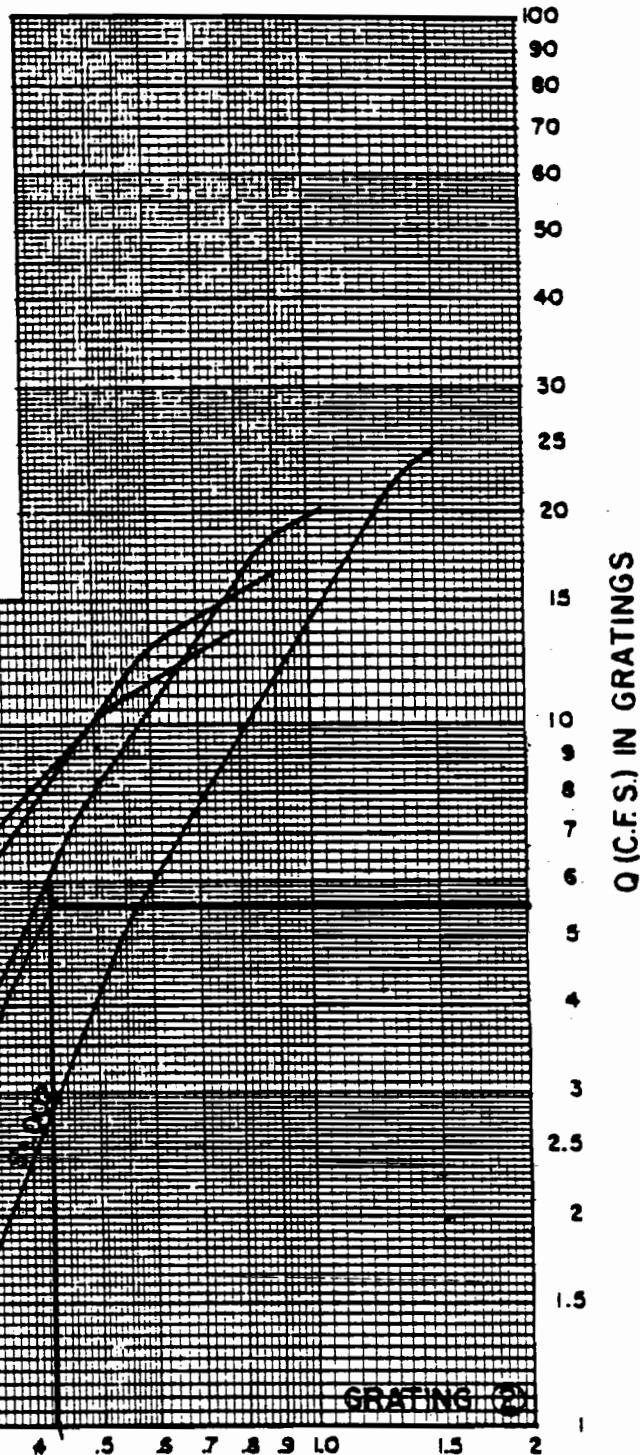
GRATING CAPACITIES FOR TYPE "A", "C" and "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION
(ABOVE BASIN)



d = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

$$d = 0.43'$$

$$S = 1.73\%$$

$$Q = 5.5 \text{ cfs}$$

REV. 3-83

74

PLATE 223 D-5

B-25

analyzer Report

=====

Rainage Structure Analyzer

i : Hydraulic Analysis

Date: Tuesday, November 06, 2001 02:03:58 PM

=====

Input Data

=====

ipe	Circular
aterial	RC C76-A
oughness	0.013000
ethod	Manning
l w Rate	675.0 cfs
l pe	2.600%
ize (W x T):	72.00 x 6.0000

Output Results

=====

low Rate	675.0 cfs
ipe	2.600%
/	0.81
apacity	682.9 cfs
elocity	27.53 ft/s
th	4.86 ft
r tical Depth	5.89 ft
ize (W x T):	72.00 x 6.0000

alyzer Report

ainage Structure Analyzer

Hydraulic Analysis

Date: Tuesday, November 06, 2001 02:05:41 PM

Input Data

i pe	Circular
i erial	RC C76-A
oughness	0.013000
ethod	Manning
l w Rate	675.0 cfs
l pe	3.840%
ize (W x T):	72.00 x 6.0000

put Results

low Rate	675.0 cfs
l pe	3.840%
/	0.68
apacity	829.9 cfs
elocity	32.71 ft/s
= th	4.11 ft
r tical Depth	5.89 ft
ize (W x T):	72.00 x 6.0000

lyzer Report

ainage Structure Analyzer

Hydraulic Analysis

Date: Tuesday, November 06, 2001 02:06:06 PM

Input Data

ipe	Circular
rial	RC C76-A
roughness	0.013000
ethod	Manning
flow Rate	675.0 cfs
ipe	2.810%
ize (W x T):	72.00 x 6.0000

put Results

low Rate	675.0 cfs
ipe	2.810%
/	0.78
apacity	709.9 cfs
elocity	28.57 ft/s
e th	4.67 ft
r tical Depth	5.89 ft
ize (W x T):	72.00 x 6.0000

Analyzer Report

Drainage Structure Analyzer

Hydraulic Analysis

Date: Tuesday, November 06, 2001 02:09:56 PM

Input Data

Shape	Circular
Atrial	RC C76-A
roughness	0.013000
Method	Manning
Flow Rate	830.0 cfs
Loss	4.910%
Size (W x T):	84.00 x 7.0000

Output Results

Flow Rate	830.0 cfs
Loss	4.910%
/	0.55
Capacity	1415.6 cfs
Velocity	38.25 ft/s
Depth	3.85 ft
Vertical Depth	6.75 ft
Size (W x T):	84.00 x 7.0000

Analyzer Report

=====
rainage Structure Analyzer

nel Hydraulic Analysis

ate: Tuesday, November 06, 2001 02:11:47 PM
=====

put Data

ne	Trapezoidal
rial	Bare Soil
roughness	0.020000
ottom Width	10.00 ft
e : Slope	33.000%
nt Slope	33.000%
ed Slope	0.500%
ow Rate	841.0 cfs

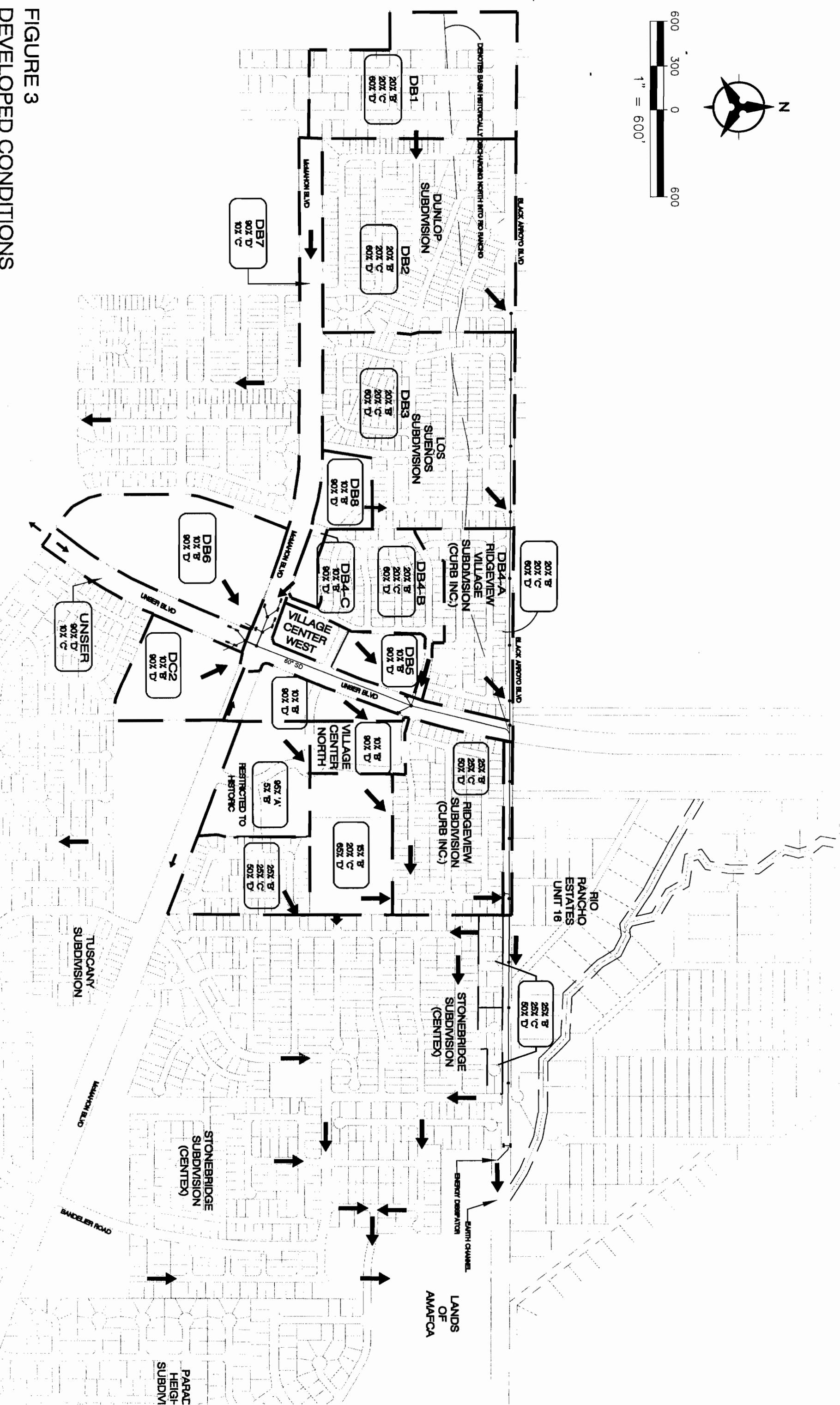
put Results

flow Rate	841.0 cfs
depth	3.97 ft
elocity	9.61 ft/s
op Width	34.07 ft
critical Depth	4.09 ft

uper Critica

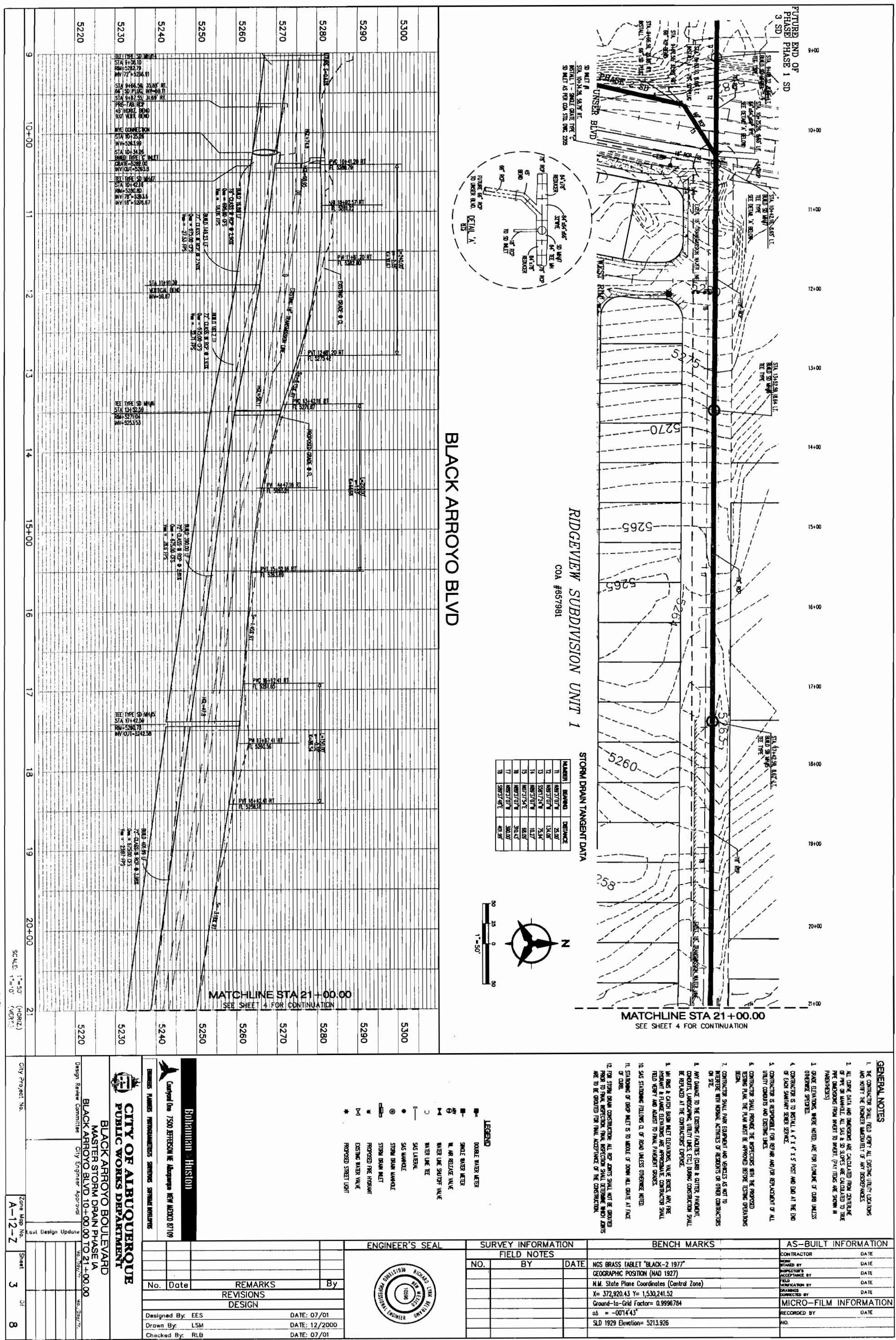
**FIGURE 3
DEVELOPED CONDITIONS
LAND TREATMENT EXHIBIT**

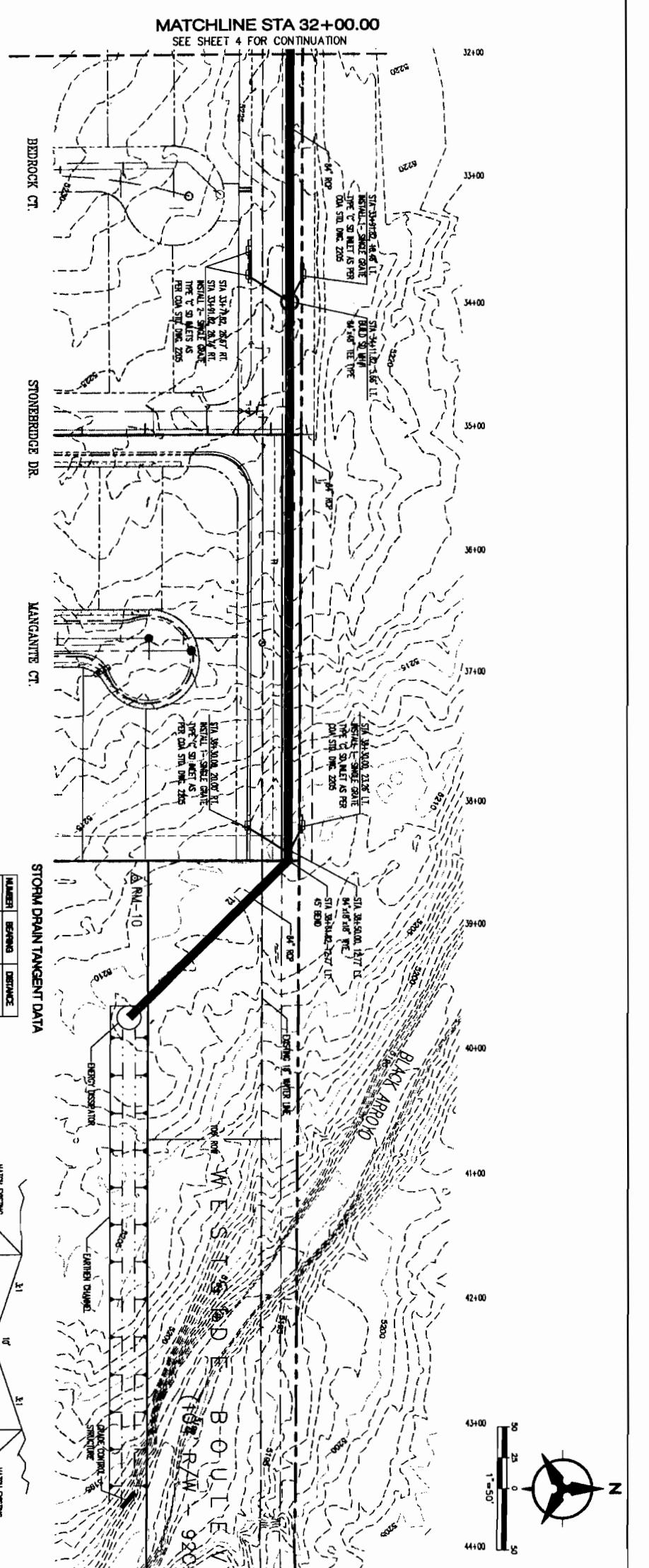
P:\01177\CDP\GENERAL\EXHIBITS\MSTR-LANDTREAT.DWG



...aded cells require user input. Non-shaded cells cannot be edited.***

MCK ARROYO STORM DRAIN with FREE DISCHARGE FROM COMMERCIAL TRACTS





GENERAL NOTES

104

ATION
E
E
E
E
E
ATION
E

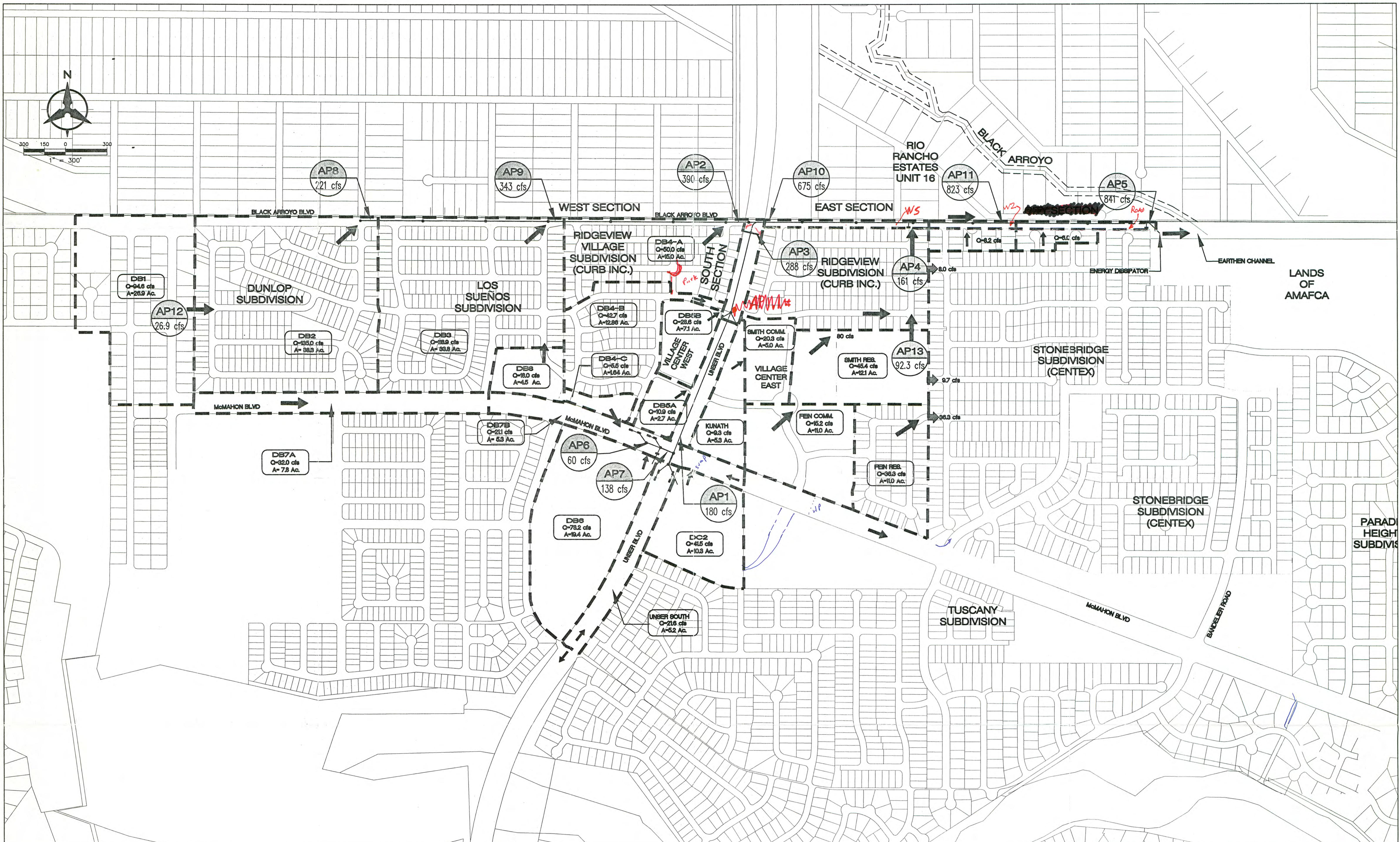
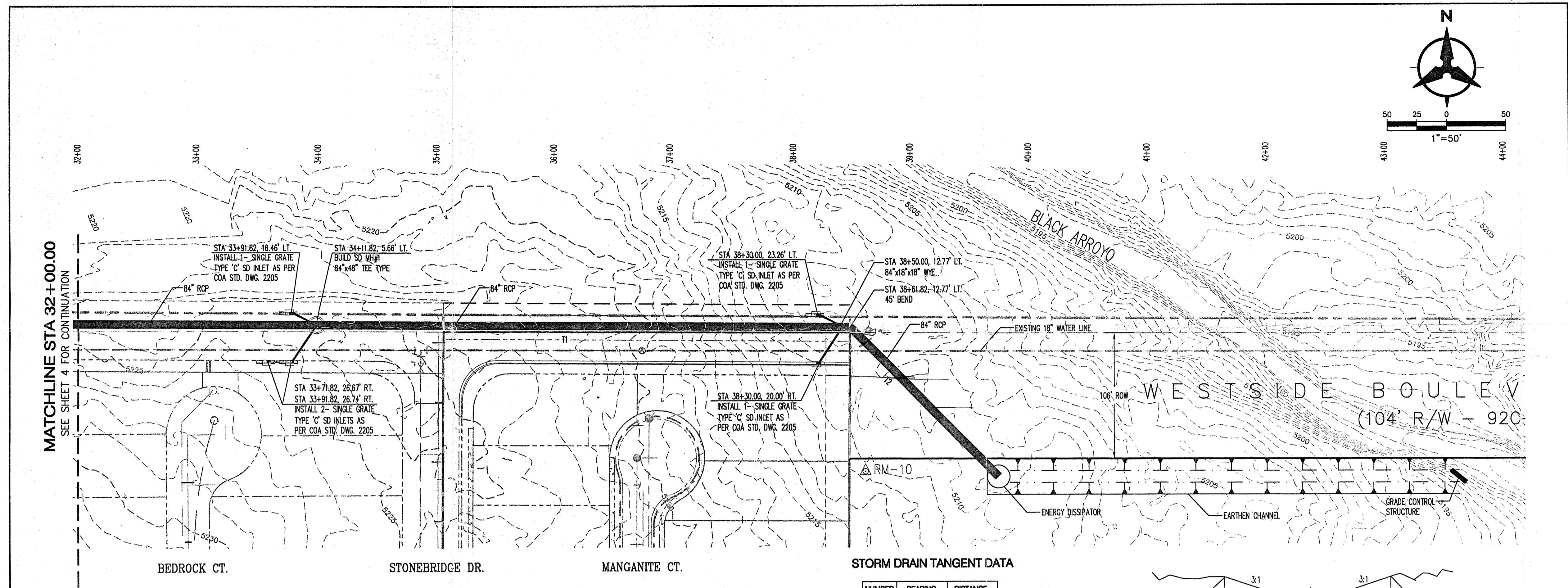


EXHIBIT 1

DEVELOPED CONDITIONS BASIN MAP



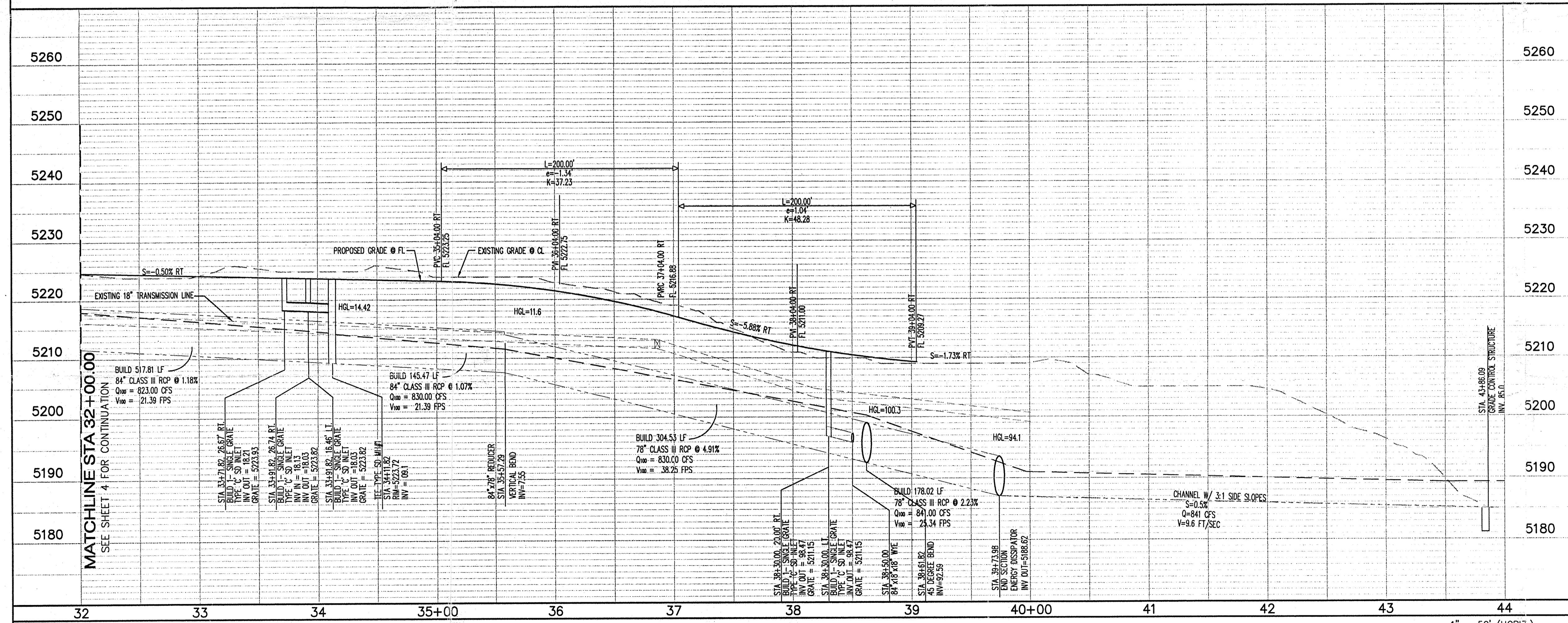
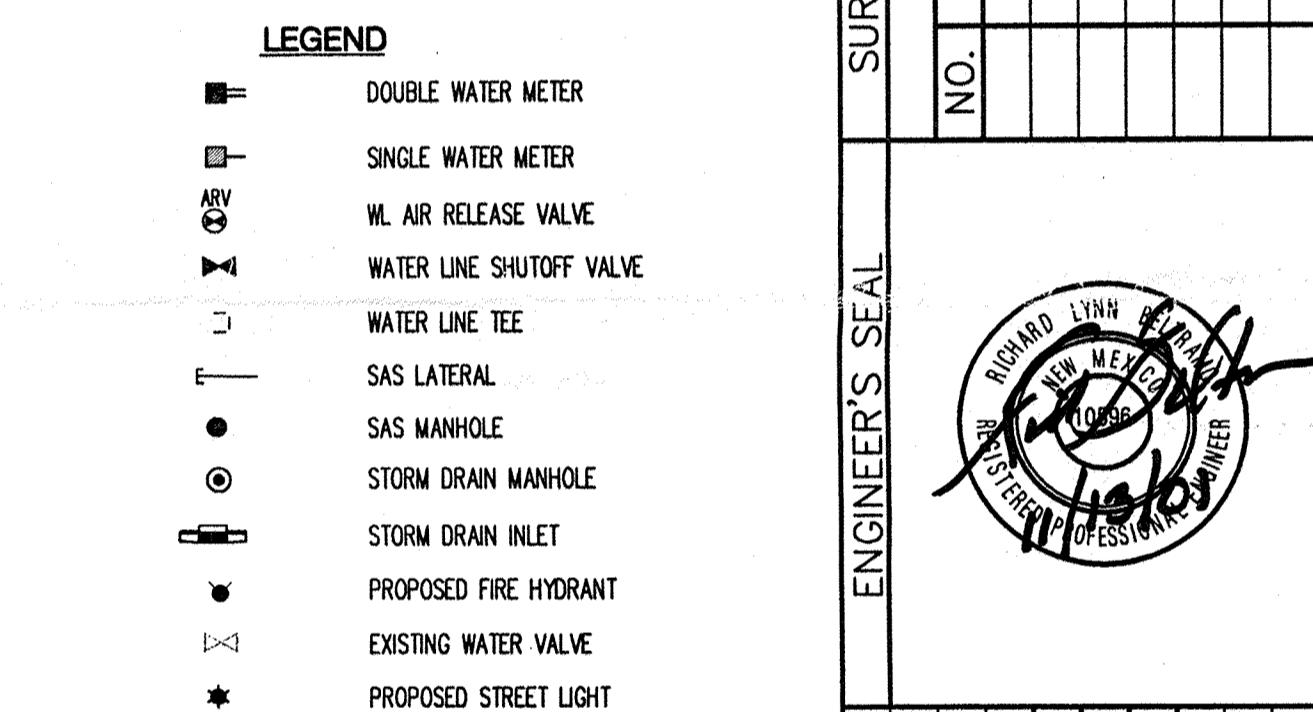
GENERAL NOTES

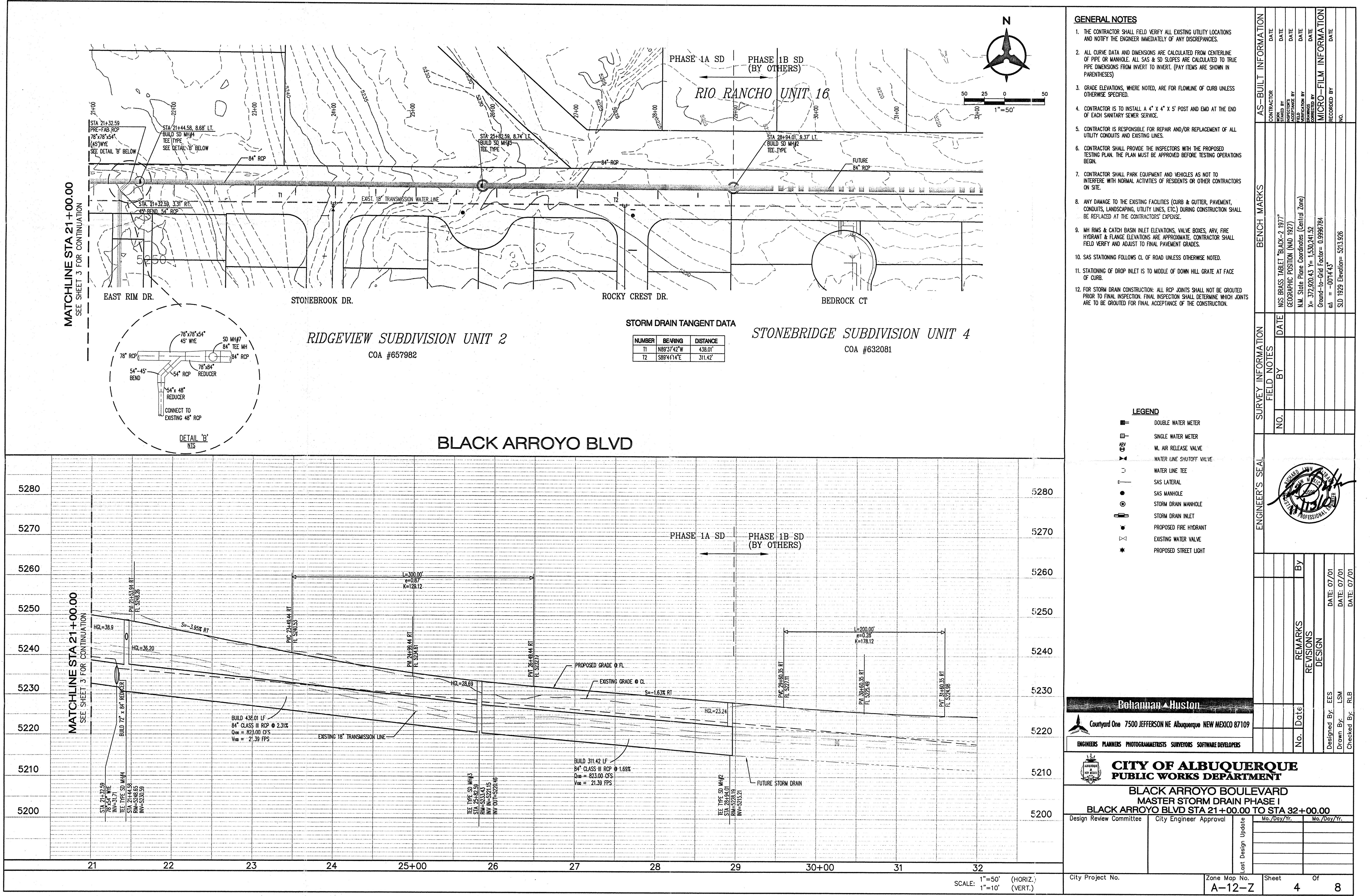
- THE CONTRACTOR SHALL FIELD VERIFY ALL EXISTING UTILITY LOCATIONS AND NOTIFY THE ENGINEER IMMEDIATELY OF ANY DISCREPANCIES.
- ALL CURVE DATA AND DIMENSIONS ARE CALCULATED FROM CENTERLINE OF PIPE OR MANHOLE. ALL SAS & SD SLOPES ARE CALCULATED TO TRUE PIPE DIMENSIONS FROM INVERT TO INVERT. (PAY ITEMS ARE SHOWN IN PARENTHESES)
- GRADE ELEVATIONS, WHERE NOTED, ARE FOR FLOWLINE OF CURB UNLESS OTHERWISE SPECIFIED.
- CONTRACTOR IS TO INSTALL A 4" X 4" X 5' POST AND END AT THE END OF EACH SANITARY SEWER SERVICE.
- CONTRACTOR IS RESPONSIBLE FOR REPAIR AND/OR REPLACEMENT OF ALL UTILITY CONDUITS AND EXISTING LINES.
- CONTRACTOR SHALL PROVIDE THE INSPECTORS WITH THE PROPOSED TESTING PLAN. THE PLAN MUST BE APPROVED BEFORE TESTING OPERATIONS BEGIN.
- CONTRACTOR SHALL PARK EQUIPMENT AND VEHICLES AS NOT TO INTERFERE WITH NORMAL ACTIVITIES OF RESIDENTS OR OTHER CONTRACTORS ON SITE.
- ANY DAMAGE TO THE EXISTING FACILITIES (CURB & GUTTER, PAVEMENT, CONDUITS, LANDSCAPING, UTILITY LINES, ETC.) DURING CONSTRUCTION SHALL BE REPAIRED AT THE CONTRACTORS EXPENSE.
- MH RIMS & CATCH BASIN INLET ELEVATIONS, VALVE BOXES, ARV, FIRE HYDRANT & FLANGE ELEVATIONS ARE APPROXIMATE. CONTRACTOR SHALL FIELD VERIFY AND ADJUST TO FINAL PAVEMENT GRADES.
- SAS STATIONING FOLLOWS CL OF ROAD UNLESS OTHERWISE NOTED.
- STATIONING OF DROP INLET IS TO MIDDLE OF DOWN HILL GRATE AT FACE OF CURB.
- FOR STORM DRAIN CONSTRUCTION: ALL RCP JOINTS SHALL NOT BE GROUTED PRIOR TO FINAL INSPECTION. FINAL INSPECTION SHALL DETERMINE WHICH JOINTS ARE TO BE GROUTED FOR FINAL ACCEPTANCE OF THE CONSTRUCTION.

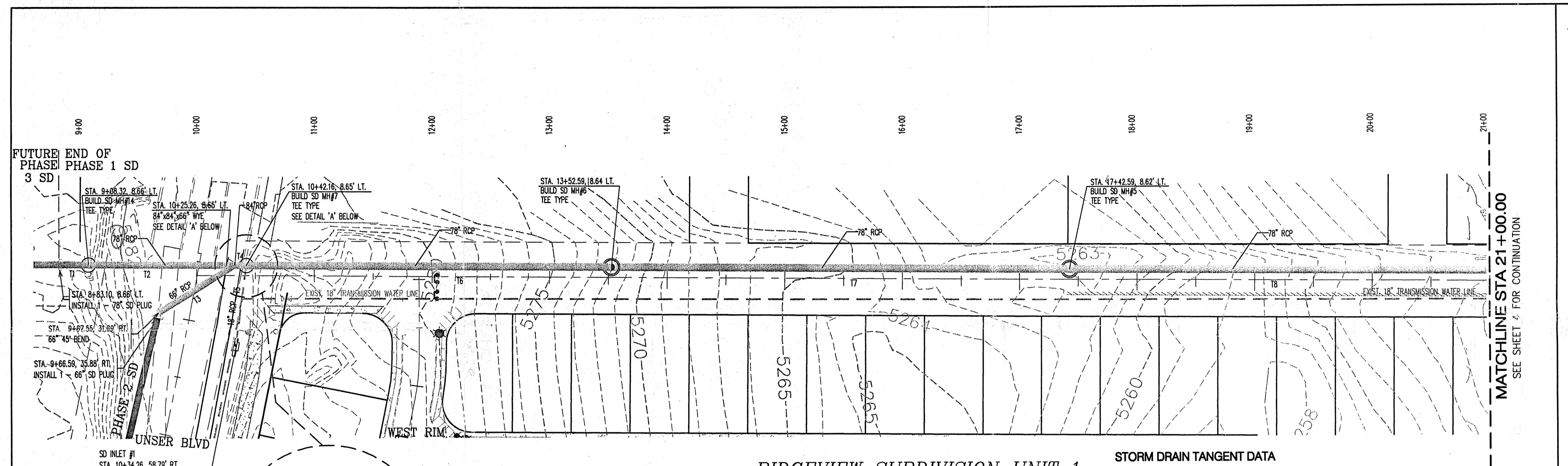
10. SAS STATIONING FOLLOWS CL OF ROAD UNLESS OTHERWISE NOTED.

11. STATIONING OF DROP INLET IS TO MIDDLE OF DOWN HILL GRATE AT FACE OF CURB.

12. FOR STORM DRAIN CONSTRUCTION: ALL RCP JOINTS SHALL NOT BE GROUTED PRIOR TO FINAL INSPECTION. FINAL INSPECTION SHALL DETERMINE WHICH JOINTS ARE TO BE GROUTED FOR FINAL ACCEPTANCE OF THE CONSTRUCTION.





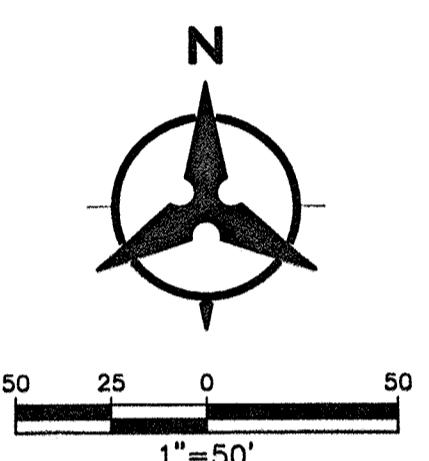


RIDGEVIEW SUBDIVISION UNIT 1

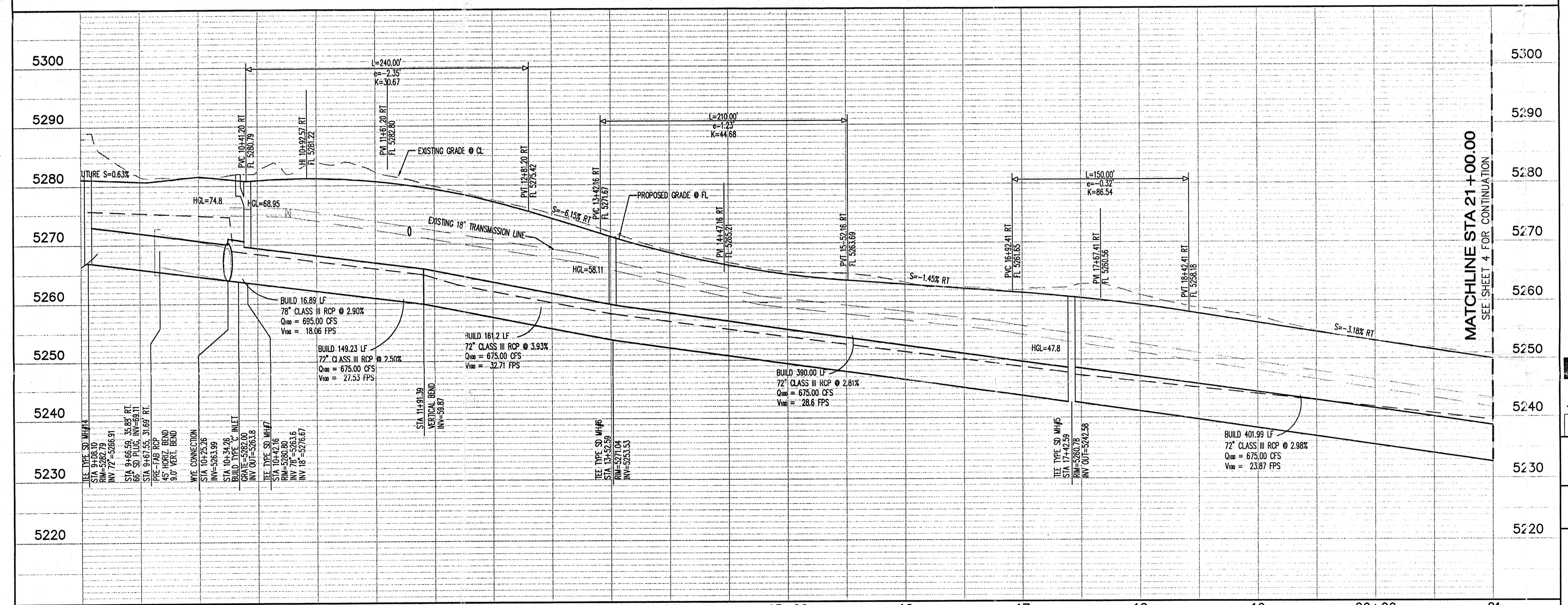
COA #657981

STORM DRAIN TANGENT DATA

NUMBER	BEARING	DISTANCE
T1	N89°37'07"W	25.00'
T2	N89°37'07"W	134.06'
T3	S58°17'24"W	75.94'
T4	N89°37'07"W	10.27'
T5	N073°57'4"E	68.09'
T6	N89°37'07"W	310.43'
T7	N89°37'07"W	390.00'
T8	S89°37'48"E	401.99'



BLACK ARROYO BLVD



SCALE: 1"=50'
(HORIZ.)
1"=10'
(VERT.)

GENERAL NOTES					
1. THE CONTRACTOR SHALL FIELD VERIFY ALL EXISTING UTILITY LOCATIONS AND NOTIFY THE ENGINEER IMMEDIATELY OF ANY DISCREPANCIES.					
2. ALL CURVE DATA AND DIMENSIONS ARE CALCULATED FROM CENTERLINE OF PIPE OR MANHOLE. ALL SAS & SD SLOPES ARE CALCULATED TO TRUE PIPE DIMENSIONS FROM INVERT TO INVERT. (PAY ITEMS ARE SHOWN IN PARENTHESES)					
3. GRADE ELEVATIONS, WHERE NOTED, ARE FOR FLOWLINE OF CURB UNLESS OTHERWISE SPECIFIED.					
4. CONTRACTOR IS TO INSTALL A 4" X 4" X 5' POST AND END AT THE END OF EACH SANITARY SEWER LINE.					
5. CONTRACTOR IS RESPONSIBLE FOR REPAIR AND/OR REPLACEMENT OF ALL UTILITY CONDUITS AND EXISTING LINES.					
6. CONTRACTOR SHALL PROVIDE THE INSPECTORS WITH THE PROPOSED TESTING PLAN. THE PLAN MUST BE APPROVED BEFORE TESTING OPERATIONS BEGIN.					
7. CONTRACTOR SHALL PARK EQUIPMENT AND VEHICLES AS NOT TO INTERFERE WITH NORMAL ACTIVITIES OF RESIDENTS OR OTHER CONTRACTORS ON SITE.					
8. ANY DAMAGE TO THE EXISTING FACILITIES (CURB & GUTTER, PAVEMENT, CONDUITS, LANDSCAPING, UTILITY LINES, ETC.) DURING CONSTRUCTION SHALL BE REPLACED AT THE CONTRACTORS' EXPENSE.					
9. MH RIMS & CATCH BASIN INLET ELEVATIONS, VALVE BOXES, ARV, FIRE HYDRANT & FLANGE ELEVATIONS ARE APPROXIMATE. CONTRACTOR SHALL FIELD VERIFY AND ADJUST TO FINAL PAVEMENT GRADES.					
10. SAS STATIONING FOLLOWS CL OF ROAD UNLESS OTHERWISE NOTED.					
11. STATIONING OF DROP INLET IS TO MIDDLE OF DOWN HILL GRATE AT FACE OF CURB.					
12. FOR STORM DRAIN CONSTRUCTION: ALL RCP JOINTS SHALL NOT BE GROUTED PRIOR TO FINAL INSPECTION. FINAL INSPECTION SHALL DETERMINE WHICH JOINTS ARE TO BE GROUTED FOR FINAL ACCEPTANCE OF THE CONSTRUCTION.					

AS-BUILT INFORMATION					
CONTRACTOR	DATE	WORK BY	DATE	INSPECTOR	DATE
PERFORMANCE BY	DATE	VERIFICATION BY	DATE	RECORDS BY	DATE
MANUFACTURER	DATE	MANUFACTURER	DATE	NO.	NO.

MICRO-FILE INFORMATION					
RECORDED BY	DATE	NO.	NO.		

<i>RICHARD LYNN BELTRANO FRED PACHECO</i>	
REVISIONS	DESIGN
No. Date	Remarks
Design E.S.	Date: 07/01
Drawn By: LSM	Date: 12/2000
Checked By: RLB	Date: 07/01

Bohannan + Huston
Courtyard One 7500 JEFFERSON NE Albuquerque NEW MEXICO 87109

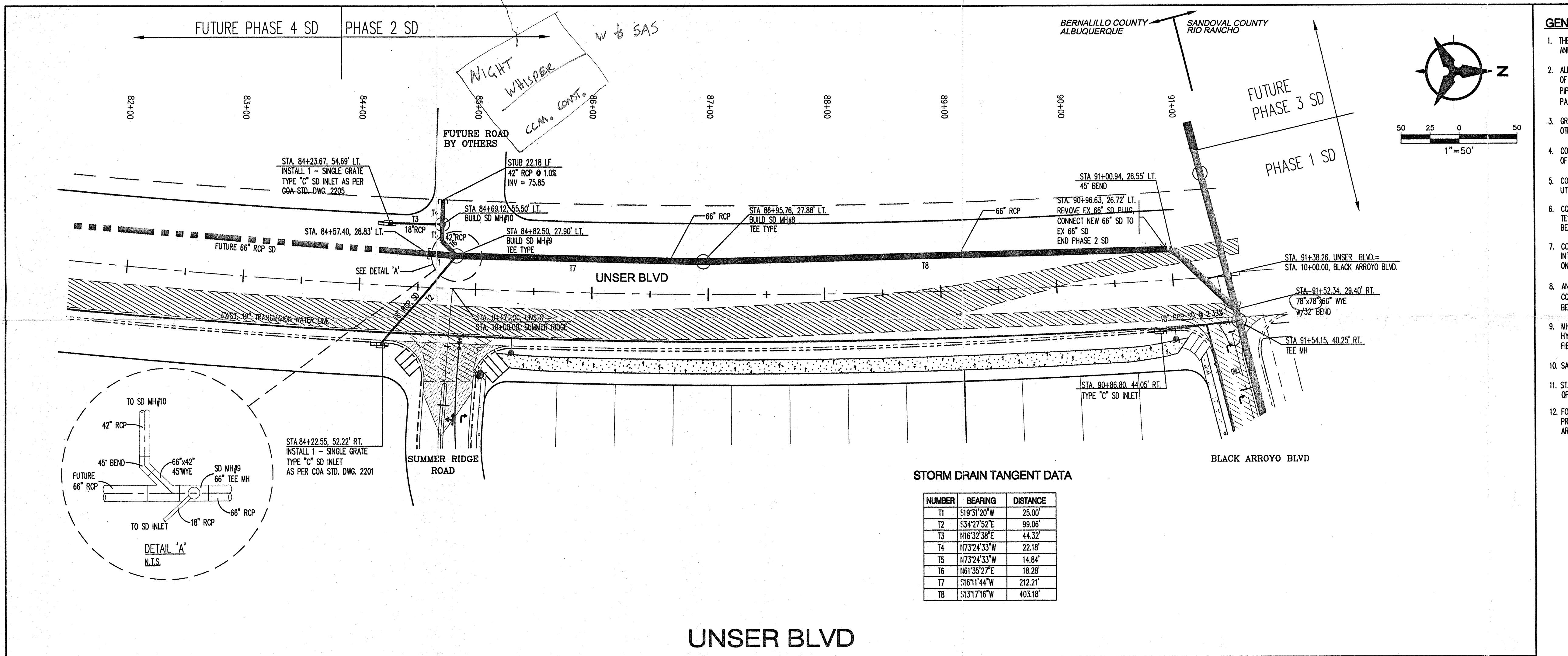
ENGINEERS PLANNERS PHOTOGRAMMETRISTS SURVEYORS SOFTWARE DEVELOPERS

CITY OF ALBUQUERQUE
PUBLIC WORKS DEPARTMENT

BLACK ARROYO BOULEVARD
MASTER STORM DRAIN PHASE IA
BLACK ARROYO BLVD 10+00.00 TO 21+00.00

Design Review Committee	City Engineer Approval	Mo./Day/Yr.	Mo./Day/Yr.
Last Design Update			

City Project No. Zone Map No. Sheet
A-12-Z 3 of 8



- BENCH MARKS

CONTRACTOR SHALL FIELD VERIFY ALL EXISTING UTILITY LOCATIONS
NOTIFY THE ENGINEER IMMEDIATELY OF ANY DISCREPANCIES.

CURVE DATA AND DIMENSIONS ARE CALCULATED FROM CENTERLINE
PIPE OR MANHOLE. ALL SAS & SD SLOPES ARE CALCULATED TO TRUE
DIMENSIONS FROM INVERT TO INVERT. (PAY ITEMS ARE SHOWN IN
THESES)

ELEVATIONS, WHERE NOTED, ARE FOR FLOWLINE OF CURB UNLESS
WISE SPECIFIED.

TRACTOR IS TO INSTALL A 4" X 4" X 5' POST AND EMD AT THE END
OF SANITARY SEWER SERVICE.

TRACTOR IS RESPONSIBLE FOR REPAIR AND/OR REPLACEMENT OF ALL
CONDUITS AND EXISTING LINES.

TRACTOR SHALL PROVIDE THE INSPECTORS WITH THE PROPOSED
TESTING PLAN. THE PLAN MUST BE APPROVED BEFORE TESTING OPERATIONS

TRACTOR SHALL PARK EQUIPMENT AND VEHICLES AS NOT TO
INTERFERE WITH NORMAL ACTIVITIES OF RESIDENTS OR OTHER CONTRACTORS
ON SITE.

DAMAGE TO THE EXISTING FACILITIES (CURB & GUTTER, PAVEMENT,
CURB JOINTS, LANDSCAPING, UTILITY LINES, ETC.) DURING CONSTRUCTION SHALL
BE PLACED AT THE CONTRACTORS' EXPENSE.

ALL CATCH BASIN INLET ELEVATIONS, VALVE BOXES, ARV, FIRE
HYDRANT & FLANGE ELEVATIONS ARE APPROXIMATE. CONTRACTOR SHALL
VERIFY AND ADJUST TO FINAL PAVEMENT GRADES.

STATIONING FOLLOWS CL OF ROAD UNLESS OTHERWISE NOTED.

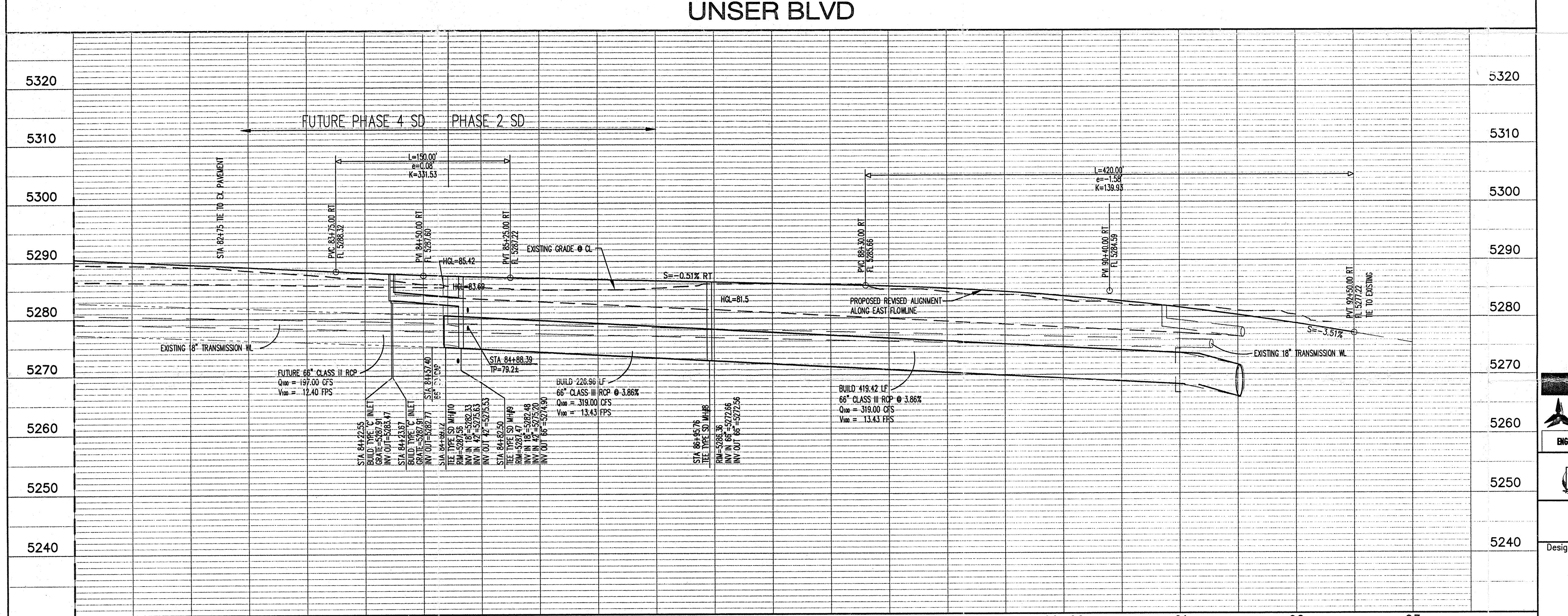
STATIONING OF DROP INLET IS TO MIDDLE OF DOWN HILL GRATE AT FACE
OF CURB.

STORM DRAIN CONSTRUCTION: ALL RCP JOINTS SHALL NOT BE GROUTED
UNTIL FINAL INSPECTION. FINAL INSPECTION SHALL DETERMINE WHICH JOINTS
TO BE GROUTED FOR FINAL ACCEPTANCE OF THE CONSTRUCTION.



LEGEND

DOUBLE WATER METER
SINGLE WATER METER
WL AIR RELEASE VALVE
WATER LINE SHUTOFF VALVE
WATER LINE TEE
SAS LATERAL
SAS MANHOLE
STORM DRAIN MANHOLE
STORM DRAIN INLET
PROPOSED FIRE HYDRANT
EXISTING WATER VALVE
PROPOSED STREET LIGHT



Author - Host Site

10 JEFFERSON NE ALBUQUERQUE NEW MEXICO 87109

SCORING MANTRAS | SUMMERS | SOFTWARE DEVELOPERS

CITY OF ALBUQUERQUE PUBLIC WORKS DEPARTMENT

**UNSER BOULEVARD
MASTER STORM DRAIN PHASE II
UNSER BLVD STA 81+50.00 TO 91+50.00**