LE

JULY 3, 2014

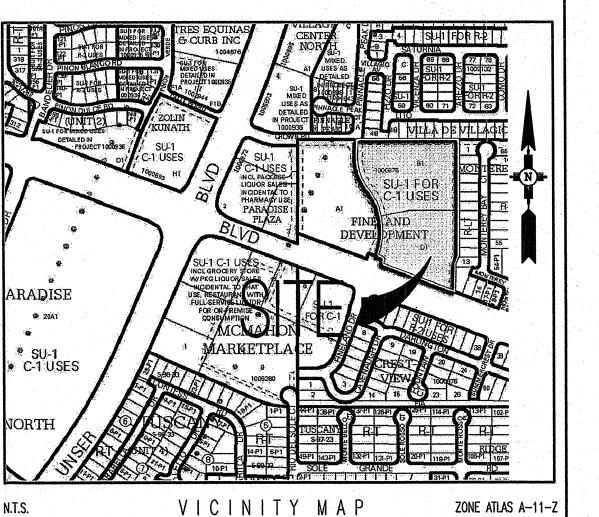
AWN

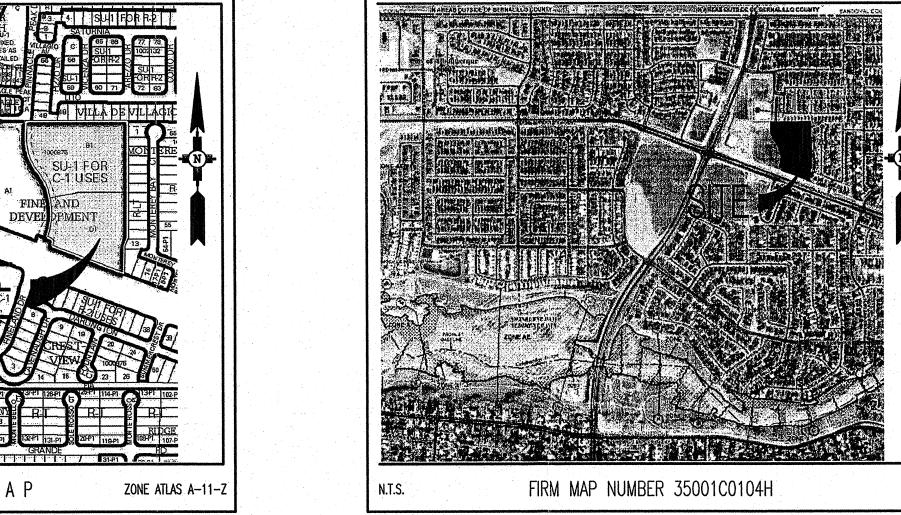
EVICIONS

REVISIONS

NEVIOIONO

C-100
DRAINAGE MANAGEMENT





				AFFIN	NITY AT	ALBUC	QUERQL	IE			
			E	xisting	Condition	ons Bas	in Data 1	able			
This table	is based on	the DPM S	Section 22.	2, Zone:	1	Service States					
Basin	Area	Area	Land	Treatme	ent Percer	ntages	Q(100yr)	Q(100yr-6hr)	WTE	<b>V</b> (100yr-6hr)	<b>V</b> (100yr-10day
ID	(SQ. FT)	(AC.)	Α	В	С	D	(cfs/ac.)	(CFS)	(inches)	(CF)	CF
Existing		a de la companya de La companya de la co			** 						
1	288227	6.62	95.0%	0.0%	5.0%	0.0%	1.37	9.06	0.47	11229	11229
TOTAL	288227	6.62									11228.844
					The second second						2

#### POND DATA

#### POND #1:

Lot 41

Lot 40

POND BOTTOM: 5283.0 FEET
POND VOLUME PROVIDED: 0.131 ACRE—FEET
POND VOLUME REQUIRED: 0.106 ACRE—FEET (PER AHYMO ANALYSIS)
MAX WATER SURFACE ELEVATION: 5287.0 FEET (PER AHYMO

## POND #2:

POND BOTTOM: 5277.0 FEET

ANALYSIS) SPILL ELEVATION: 5287.5 FEET

POND VOLUME PROVIDED: 0.342 ACRE—FEET
POND VOLUME REQUIRED: 0.308 ACRE—FEET (PER AHYMO ANALYSIS)
MAX WATER SURFACE ELEVATION: 5283.1 FEET (PER AHYMO ANALYSIS)
SPILL ELEVATION: 5283.5 FEET

### POND #3:

POND BOTTOM: 5281.00 FEET
POND VOLUME PROVIDED: 0.0257 ACRE—FEET
POND VOLUME REQUIRED: 0.0239 ACRE—FEET (PER CHAPTER 22 DPM)
MAX WATER SURFACE ELEVATION: 5281.45 FEET (PER CHAPTER 22 DPM)
SPILL ELEVATION: 5281.50 FEET

#### NTRODUCTION:

THE PROJECT IS LOCATED NORTHWEST OF THE INTERSECTION OF MCMAHON BLVD AND UNSER BLVD. THIS SITE IS NOT WITHIN A DEFINED FLOOD ZONE AS SHOWN ON FIRM MAP NUMBER 35001C0104H (THIS SHEET). THE PURPOSE OF THIS SUBMITTAL IS TO PROVIDE A DRAINAGE MANAGEMENT PLAN FOR THE DEVELOPMENT OF AFFINITY AT ALBUQUERQUE SENIOR HOUSING AND REQUEST GRADING PERMIT AND BUILDING PERMIT APPROVAL.

#### EXISTING CONDITIONS:

THE 6.62 ACRE SITE IS CURRENTLY UNDEVELOPED. EXISTING FLOW IS APPROXIMATELY EQUAL TO 9.0 CFS. THE SITE SLOPES TO THE NORTH / NORTHWEST WHERE THE RUNOFF FLOWS INTO AN EXISTING 24"STORM DRAIN IN PINNACLE PEAK DRIVE.

BASED ON A DRAINAGE STUDY FOR VILLA DE VILLAGIO SUBDIVISION DATED FEBRUARY 10, 2003 (COA HYDRO FILE #A11/D9), ALLOWABLE PEAK DISCHARGE FROM THE SITE IS APPROXIMATELY 9.0 CFS.

### METHODOLOGY:

THE HYDROLOGIC ANALYSIS PROVIDED WITH THIS DRAINAGE MANAGEMENT PLAN HAS BEEN PREPARED IN ACCORDANCE WITH SECTION 22.2 OF THE DPM. THE SITE IS LOCATED WEST OF THE RIO GRANDE WITHIN PRECIPITATION ZONE 1. ALTHOUGH THE SITE IS SMALL ENOUGH TO USE THE "SMALL WATERSHEDS" PROCEDURE GIVEN IN SECTION A.6, WE ELECTED TO USE AHYMO IN ORDER TO MODEL THE STORMWATER FLOWS THROUGH THE TWO PROPOSED PONDS ON THE SITE. LAND TREATMENT PERCENTAGES WERE CALCULATED BASED ON THE ACTUAL CONDITIONS IN EACH ONSITE BASIN AND ARE SUMMARIZED IN THE "DEVELOPED CONDITIONS BASIN DATA TABLE" ON SHEET C-101.

ALL ONSITE STORM DRAIN PIPES ARE BE SIZED BASED ON GRAVITY FLOW USING THE MANNING'S EQUATION. DETAILED CALCULATIONS FOR PIPES AND INLETS ARE PROVIDED ON SHEET C-101.

### PROPOSED CONDITIONS:

ALLOWABLE DISCHARGE (PER COA HYDRO FILE #A11/D9): 9.0 CFS ALLOWABLE DISCHARGE WITH FINELAND DRIVE (BASIN 4): 7.1 CFS PROPOSED DISCHARGE: 6.5 CFS DIFFERENCE BETWEEN ALLOWABLE AND PROPOSED: .6 CFS

THE ALLOWABLE DISCHARGE FROM THE SITE WAS FOUND TO BE APPROXIMATELY 7.1 CFS WHEN CONSIDERING THE RUNOFF FROM FINELAND DRIVE (BASIN 4). WITH THE DEVELOPMENT OF THE SITE, THE PROPOSED FLOW IS APPROXIMATELY 6.5 CFS WHICH IS LESS THAN THE ALLOWABLE DISCHARGE.

TO MITIGATE PEAK FLOWS GENERATED WITH PROPOSED CONDITIONS, TWO PONDS HAVE BEEN DESIGNED ONSITE. BOTH PONDS WERE ANALYZED USING AHYMO. DISCHARGE FROM THE PONDS WAS CALCULATED USING THE ORIFICE EQUATION. SEE TABLE 2, SHEET C-101 FOR DETAILED CALCULATIONS.

POND 2 IS LOCATED AT THE NORTHWEST CORNER OF THE SITE. THE PRIMARY DISCHARGE POINT FOR POND 2 IS A NEW STORM DRAIN TO BE CONNECTED TO AN EXISTING PUBLIC STORM DRAIN MANHOLE AT THE INTERSECTION OF PINNACLE PEAK AND CROWN ROAD. IN THE EVENT THAT THE DISCHARGE PIPE IS PLUGGED, OR IN THE EVENT OF A STORM LARGER THAN THE 100 YEAR STORM, THE POND WILL OVERFLOW TO THE RIGHT—OF—WAY OF FINELAND DRIVE (AKA PINNACLE PEAK). UNDER EXISTING CONDITIONS, THE TOP OF CURB ELEVATION OF PINNACLE PEAK AT THE INTERSECTION WITH CROWN ROAD IS APPROXIMATELY 5283.78. THE EXISTING GRADE ALONG THE NORTH PROPERTY LINE OF THE SITE (DELINEATED WITH AN EXISTING CMU WALL) WHICH ADJOINS EXISTING RESIDENTIAL LOTS, VARIES BETWEEN 5281 AND 5282. THEREFORE, THE EXISTING GRADE ALONG MOST OF THE NORTH PROPERTY LINE IS ABOUT 2' LOWER THAN THE TOP OF CURB OF PINNACLE PEAK. IN ORDER TO ENSURE THAT ANY OVERFLOW FROM POND 2 DOES NOT IMPACT THE RESIDENTIAL LOTS TO THE NORTH, WE ARE PROVIDING A CAST—IN—PLACE CONCRETE WALL ALONG THE NORTH SIDE OF POND 2. THE WALL WILL BE APPROXIMATELY 3' TALL, WITH A TOP—OF—WALL ELEVATION OF 5285.0.

BASIN 5 CONSISTS OF SMALL LANDSCAPED AREAS BEHIND THE GARAGES ON THE NORTH SIDE OF THE SITE AND A SMALL PORTION OF THE EAST SIDE OF THE SITE. THERE IS NO IMPERVIOUS AREA WITHIN BASIN 5. ALL OF THE GARAGE ROOFS DRAIN TO THE PARKING LOTS AND DRIVEWAYS. FLOWS FROM BASIN 5 (PEAK DISCHARGE IS LESS THAN 1.0 CFS) WILL BE RETAINED IN A SHALLOW WATER HARVESTING AREA WITHIN THE LANDSCAPED AREA NEAR THE NORTH PROPERTY LINE. THE TOTAL VOLUME FOR THE 100 YR — 10 DAY STORM WAS CALCULATED TO BE APPROXIMATELY 1010 CF BASED ON THE CALCULATION METHOD GIVEN IN CHAPTER 22 SECTION A5 OF THE

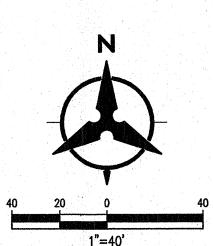
 $V_{360} = (.29 \text{ ACRES X } .99 \text{ INCHES}) / 12 = .0239 \text{ AC-FT (APPROX 1042 CF)}$ 

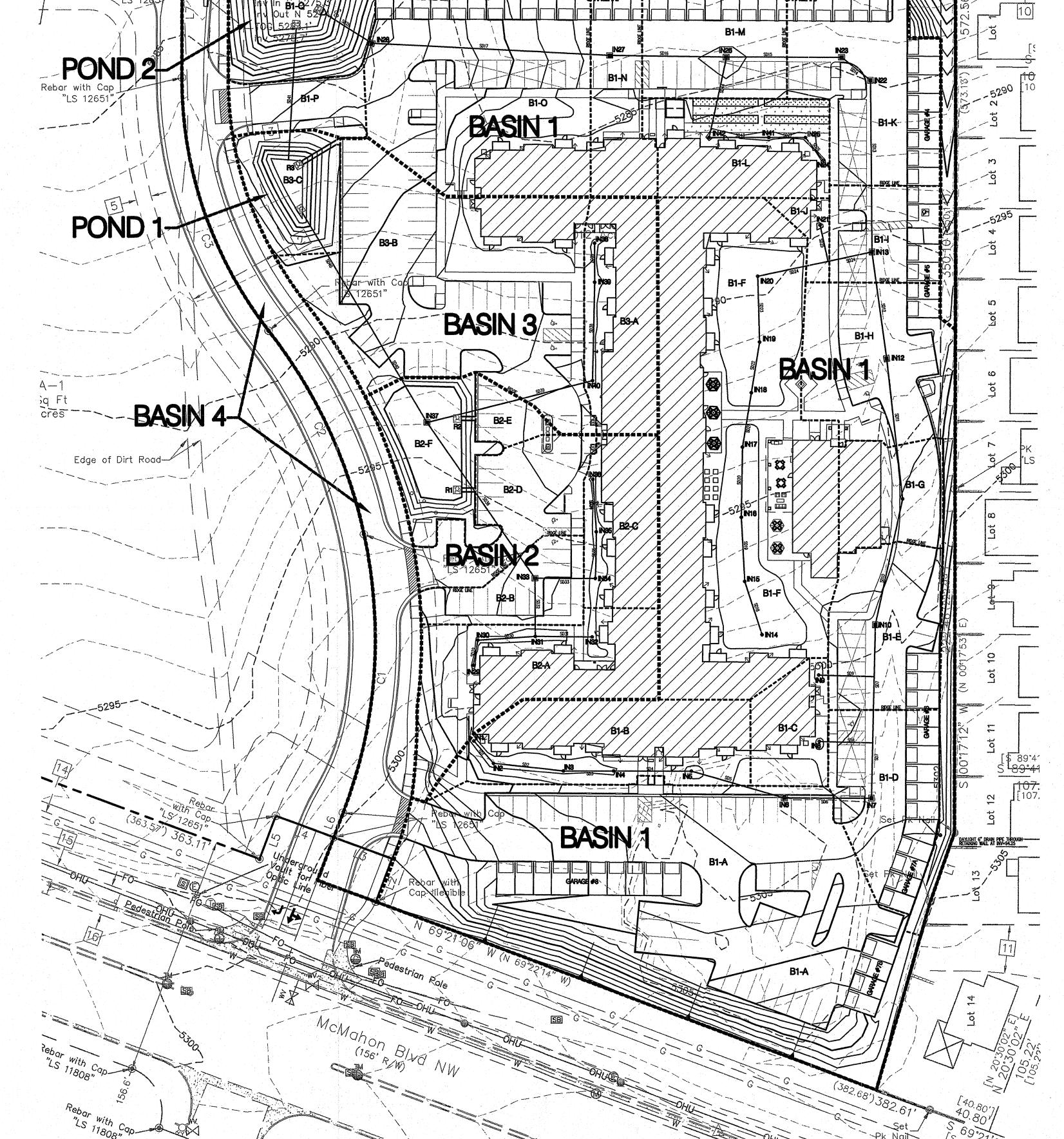
 $A_D = 0$ THEREFORE:  $V_{10DAY} = .0239$  AC-FT (APPROX 1042 CF)

THE WATER HARVESTING AREA WAS SIZED TO BE APPROXIMATELY 1120CF, APPROXIMATELY 10% LARGER THAN THE TOTAL VOLUME REQUIRED.

### CONCLUSION:

THE PEAK DISCHARGE FROM THE SITE IS 6.5 CFS WHICH IS LESS THAN THE ALLOWABLE PEAK DISCHARGE RATE, THEREFORE WE ARE IN CONFORMANCE WITH CITY OF ALBUQUERQUE HYDROLOGY REQUIREMENTS AND REQUEST BUILDING PERMIT APPROVAL.





DRAINAGE MANAGEMENT PLAN

SEAL						
		THE REAL PROPERTY.	J. STID	www.		
	<u>م</u>	STOCK	J. MAE	WO'S	Day of the second	11
		2. 3	N me		The	Un
	RE		14523	377		ر"
	G.S.		\\\	<i>}</i>		
	WANT		7/3/	14:		

FILE DATE JULY 3, 2014

> .wn S

REVISIONS

DRAINAGE MANAGEMENT PLAN

AFFINITY AT ALBUQUERQUE SENIOR HOUSING **Developed Conditions Basin Data Table** This table is based on the DPM Section 22.2, Zone: 1 Q(100yr) Q(100yr) V(100yr) V(100yr-6hr) V(100yr-24hr) (cfs/ac.) (CFS) (inches) (CF) (CF) PROPOSED BASINS 43701 1.00 0.0% 0.0% 35.0% 65.0% 1.63 5925 6872 1301 1498 B1-B 9890 0.23 0.0% 0.0% 40.0% 60.0% 1.58 0.25 B1-C 3047 | 0.07 | 0.0% | 0.0% | 50.0% | 50.0% 1.48 376 427 7288 | 0.17 | 0.0% | 0.0% | 5.0% | 95.0% B1-D 0.72 1.92 1397 1167 8618 0.20 0.0% 0.0% 35.0% 65.0% 1355 B1-E 0.76 1.63 1168 32806 | 0.75 | 0.0% | 0.0% | 45.0% | 55.0% 4781 B1-F 2.78 1.53 4180 4563 0.10 0.0% 0.0% 20.0% 80.0% 796 B1-G 0.43 1.77 4.07 675 B1-H 1.06 1.53 1590 12479 0.29 0.0% 0.0% | 45.0% | 55.0% 1819 4542 0.10 0.0% 0.0% 30.0% 70.0% 0.41 1.68 634 740 3.92 B1-J 1157 | 0.03 | 0.0% | 0.0% | 67.0% | 33.0% 0.09 1.31 127 139 10518 0.24 0.0% 0.0% 10.0% 90.0% B1-K 1.87 1641 1956 7423 | 0.17 | 0.0% | 0.0% | 50.0% | 50.0% B1-L 1.48 0.62 916 1039 B1-M 6715 0.15 0.0% 0.0% 0.0% 100.0% 0.67 1.97 1102 1326 **B1-N** 4930 | 0.11 | 0.0% | 0.0% | 15.0% | 85.0% 0.47 1.82 749 889 4.15 3337 B1-0 <u> 18750 | 0.43 | 0.0% | 0.0% | 17.0% | 83.0% </u> 1.77 1.80 2818 3095 | 0.07 | 0.0% | 0.0% | 0.0% | 100.0% 4.37 0.31 1.97 508 611 B1-Q 7219 | 0.17 | 0.0% | 0.0% | 100.0% | 0.0% 0.48 0.99 596 596 **BASIN 1 TOTAL:** 186741 4.29 16.55 10156 | 0.23 | 0.0% | 0.0% | 50.0% | 50.0% 0.84 1.48 1253 1422 B2-B 4084 | 0.09 | 0.0% | 0.0% | 5.0% | 95.0% 0.40 1.92 4.30 654 783 5273 | 0.12 | 0.0% | 0.0% | 33.0% | 67.0% 0.47 841 1.65 724 B2-D 6326 0.15 0.0% 0.0% 5.0% 95.0% 0.62 1213 1.92 1013 **B2-E** 1474 | 0.03 | 0.0% | 0.0% | 0.0% | 100.0% | 0.15 1.97 242 291 5979 0.14 0.0% 0.0% 100.0% 0.0% B2-F 2.87 0.39 0.99 493 493 **BASIN 2 TOTAL:** 33292 0.76 2.88 7187 0.16 0.0% 0.0% 25.0% 75.0% **B3-A** 0.66 1.73 1033 1213 23277 0.53 0.0% 0.0% 10.0% 90.0% 2.26 1.87 3631 4330 B3-C 4694 0.11 0.0% 0.0% 100.0% 0.0% 387 0.31 0.99 387 **BASIN 3 TOTAL:** 35158 0.81 3.22 20305 | 0.47 | 0.0% | 0.0% | 25.0% | 75.0% 1.86 3426 1.73 2919 20305 0.47 **BASIN 4 TOTAL:** 1.86 12659 | 0.29 | 0.0% | 0.0% | 100.0% | 0.0% 0.83 2.87 0.99 1044 1044 12659 0.29 **BASIN 5 TOTAL:** 0.83 TOTAL 288155 6.62 25.35 38864 45024

# TABLE 1: BASIN & SUB-BASIN DATA

					ACTUAL
PIPE#	INLET/SD/BASIN	Size	Slope	Capacity*	FLOW
manta anto mere eponente el trateste la está en sen umadas. Estándos entesas		in.	The state of the s	cfs	cfs
SD1	IN1	8	0.60%	0.94	0.17
SD2	IN2, SD1	8	0.60%	0.94	0.34
SD3	IN3, SD2	8	0.60%	0.94	0.51
SD4	IN4, SD3	8	0.60%	0.94	0.68
SD5	IN5, SD4	8	0.60%	0.94	0.86
SD6	IN6, SD5	18	0.60%	8.14	4.71
SD7	IN7, SD8, SD9, SD6	18	0.60%	8.14	5.69
SD8	IN8	6	7.00%	1.48	0.13
SD9	IN9	6	7.45%	1.53	0.13
SD10	IN10, SD7	18	0.60%	8.14	6.45
SD11	SD10	18	0.60%	8.14	6.45
SD12	IN12, SD11	18	0.60%	8.14	7.50
SD13	IN13, SD12, SD24	24	0.60%	17.52	10.59
SD14	IN22, SD13	24	0.60%	17.52	11.10
SD15	IN23, SD14	24	0.60%	17.52	11.61
SD16	IN26, SD15, SD44	24	0.60%	17.52	12.90
SD17	IN27, SD16	24	0.60%	17.52	13.37
SD18	IN14	<u></u> 8	0.60%	0.94	0.31
SD19	IN15, SD18	8	0.60%	0.94	0.62
SD20	IN16, SD19	8	0.60%	0.94	0.93
SD21	IN17, SD20	8	0.60%	0.94	1.24
SD22	IN18, SD21	8	0.60%	0.94	1.55
SD23	IN19, SD22	8	0.60%	0.94	1.86
SD24	IN20, SD23, SD25	8	0.60%	0.94	2.67
SD25	IN21	6	9.75%	1.75	0.51
SD26	IN24	6	0.60%	0.43	0.15
SD27	IN25, SD26	6	0.60%	0.43	0.10
SD28	IN28, SD17	24	12.35%	79.52	15.14
SD29	IN29	6	1.00%	0.56	0.21
SD30	IN30, SD29	6	1.00%	0.56	0.42
SD31	IN32	6	1.00%	0.56	0.42
SD32	IN31, SD30, SD31	8	1.00%	1.21	0.84
SD33	IN34, SD35	8	1.00%	1.21	0.47
SD34	IN36	6	1.00%	0.56	0.16
SD35	IN35, SD34	6	1.00%	0.56	0.10
SD36	IN33, SD32, SD33	10	1.50%	2.68	1.72
SD37	IN38	6	1.00%	0.56	0.22
SD37	IN39, SD37	6	1.00%	0.56	0.22
SD39	IN40, SD38	10	1.00%	2.19	0.44
SD40	IN37, SD36, SD39	10	2.20%	3.25	3.54
SD40	B3 B2	10	6.60%	SEE AHYMO	
SD42	B9 B2		8/00%	SEE AHYM	
SD42	IN41, SD27	6	0.60%	0.43	0.46
SD43 SD44	IN42, SD43	6	0.60%	0.43	0.46
3044	IIV42, 3D43		Capacity Based		

**TABLE 3: STORM DRAIN SIZING** 

Inlet	Inlet	NLET TABLE	Actual	A	T 0
#		Basin	Actual	Avail	Capacity
# IN1	Type 8" NYLOPLAST DOME	D4 D (4/C)	Flow	Head ft	CFS
		B1-B (1/5)	0.17	0.50	0.71
IN2	8" NYLOPLAST DOME	B1-B (1/5)	0.17	0.50	0.71
IN3	8" NYLOPLAST DOME	B1-B (1/5)	0.17	0.50	0.71
IN4	8" NYLOPLAST DOME	B1-B (1/5)	0.17	0.50	0.71
IN5	8" NYLOPLAST DOME	B1-B (1/5)	0.17	0.50	0.71
IN6	18" NYLOPAST	B1-A	3.86	0.70	2.37
IN7	18" NYLOPAST	B1-D	0.72	0.70	2.37
IN8	8" NYLOPLAST DOME	B1-C (1/2)	0.13	0.50	0.71
IN9	8" NYLOPLAST DOME	B1-C (1/2)	0.13	0.50	0.71
IN10	18" NYLOPAST	B1-E	0.76	0.50	2.00
IN12	18" NYLOPAST	B1-H	1.06	0.50	2.00
IN13	18" NYLOPAST	B1-I	0.41	0.50	2.00
IN14	8" NYLOPLAST CIRCULAR	B1-F (1/7)	0.31	0.50	0.44
IN15	8" NYLOPLAST CIRCULAR	B1-F (1/7)	0.31	0.50	0.44
IN16	8" NYLOPLAST CIRCULAR	B1-F (1/7)	0.31	0.50	0.44
IN17	8" NYLOPLAST CIRCULAR	B1-F (1/7)	0.31	0.50	0.44
IN18	8" NYLOPLAST CIRCULAR	B1-F (1/7)	0.31	0.50	0.44
IN19	8" NYLOPLAST CIRCULAR	B1-F (1/7)	0.31	0.50	0.44
IN20	8" NYLOPLAST CIRCULAR	B1-F (1/7)	0.31	0.50	0.44
IN21	8" NYLOPLAST DOME	B1-J	0.09	0.50	0.71
IN22	18" NYLOPAST	B1-K (1/2)	0.51	0.50	2.00
IN23	18" NYLOPAST	B1-K (1/2)	0.51	0.50	2.00
IN24	8" NYLOPLAST DOME	B1-L (1/4)	0.15	0.50	0.71
IN25	8" NYLOPLAST DOME	B1-L (1/4)	0.15	0.50	0.71
IN26	18" NYLOPAST	B1-M	0.67	0.50	2.00
IN27	18" NYLOPAST	B1-N	0.47	0.50	2.00
IN28	18" NYLOPAST	B1-O	1.77	0.50	2.00
IN29	8" NYLOPLAST DOME	B2-A (1/4)	0.21	0.50	0.71
IN30	8" NYLOPLAST DOME	B2-A (1/4)	0.21	0.50	0.71
IN31	8" NYLOPLAST DOME	B2-A (1/4)	0.21	0.50	0.71
IN32	8" NYLOPLAST DOME	B2-A (1/4)	0.21	0.50	0.71
IN33	18" NYLOPAST	B2-B	0.40	0.50	2.00
IN34	8" NYLOPLAST DOME	B2-C (1/3)	0.16	0.50	0.71
IN35	8" NYLOPLAST DOME	B2-C (1/3)	0.16	0.50	0.71
IN36	8" NYLOPLAST DOME	B2-C (1/3)	0.16	0.50	0.71
IN37	18" NYLOPAST	B2-D,E,F	1.17	0.50	2.00
IN38	8" NYLOPLAST DOME	B3-A (1/3)	0.22	0.50	0.71
IN39	8" NYLOPLAST DOME	B3-A (1/3)	0.22	0.50	0.71
IN40	8" NYLOPLAST DOME	B3-A (1/3)	0.22	0.50	0.71
IN41	8" NYLOPLAST DOME	B1-L (1/4)	0.22		
IN42	8" NYLOPLAST DOME	B1-L (1/4)	0.15	0.50 0.50	0.71

**TABLE 4: INLET SIZING** 

		FROM		ТО			RUNOFF		TIME TO	CFS		PAGE	=	1	
	HYDROGRAPH	ID		ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER					
COMMAND	IDENTIFICATION	NO.		NO.	(SQ MI)	es (CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE			NOTATIO	N	
*C ALIVAAO EU E E	OD A FEINITY AT ALDU	OUEDOLIE	ALDUOLI	DOLLE NA	4 0110001	# 204 40202					···				
*S 100 YEAR - 6 H	OR AFFINITY AT ALBU	QUERQUE -	ALBUQUE	RQUE, NIV	I, BH PRUJ	# 20140292									
*S	OOKOTOKIII						•				·				***************************************
	P:\20140292\CDP\HYD	ORO\AHYMO	0\100YR 6-	10-2014.H	IYM						***************************************			***************************************	***************************************
	- P:\20140292\CDP\H	·····													
START	TIME= 0														
OCATION	ALBUQUERQUE														
RAINFALL TYPE= 1	NOAA 14														
S*********	******	*****	******	*****	******	*									
<b>*</b> \$		n vite with stad other lang case date case case case case after star to	pr was that then have seen then two two laws have not		12 40 40 40 40 40										
S* COMPUTE BAS	IN DEVELOPED COND	ITIONS													
'S		* data (alle sipe der sans hap den som som den den den den som	· · · · · · · · · · · · · · · · · · ·		~ ~ ~ ~ ~ ~										
S BASIN 1									100 H 44						
COMPUTE NM HYD		B1	<del>.</del>	2	0.00669	1723	0.592	1.66018	1.5			4.023 PER	IMP= 66.0	0	
S BASIN 2															
COMPUTE NM HYD		B2	-	3	0.0012	3.04	0.103	1.60797	1.5			3.962 PER	IMP= 60.0	00	
S BASIN 3													gan after i e Transport e e		
COMPUTE NM HYD		B3	<u>.</u>	4	0.00126	3.35	0.117	1.73849	1.5			4.159 PER	IMP= 75.0	00	
S BASIN 4								_							
COMPUTE NM HYD		B4	_	5	0.00073	1.95	0.068	1.73849	1.5			4.175 PER	IMP= 75.0	00	
S BASIN 5		·						<u> </u>				-			
COMPUTE NM HYD		B5	_	6	0.00045	0.91	0.026	1.08591	1.5			3.168 PER	R IMP= 0.0	0	
S************	********	*****	******	*****	*****	*				·					
S ADDITION OF BA	SIN 2 TO BASIN 3	,													
ADD HYD		B2B3	-	20	0.00246	6.4	0.220	1.67459	1.5		******************				
	& B3 TO POND 1. OU		ED ON 6" (	ORIFICE =	<del></del>										
ROUTE RESERVOIR	<del></del>	POND1	-	11	0.00246	1,9	0.220	1.67459	1.8		MA	X VOLUM	E = 0.106 A	C-FT	
S ADDITION OF PO	ND1 TO BASIN 1					- Particular substantial de la constantia									
ADD HYD		P1B1	-	21		48.73	0.812	1.66401	1.5						
	TO POND 2. OUTFLO	·	N 10" ORIF												
ROUTE RESERVOIR		POND2	-	12	0.00915	6.49	0.812	1.66401	1.8		MA	X VOLUM	E = 0.308 A	C-FT	

THE HYDROLOGIC ANALYSIS PROVIDED WITH THIS DRAINAGE MANAGEMENT PLAN HAS BEEN PREPARED IN ACCORDANCE WITH SECTION 22.2 OF THE DPM. BASIN AND SUB-BASIN BOUNDARIES DELINEATED PER SHEET C-100. BASIN AND SUB-BASINS WERE DEFINED FOR ANALYSIS OF SECONDARY OR UPSTREAM REACHES OF STORM DRAINS AND INLETS. AREAS, LAND TREATMENTS, AND FLOWS CAN BE SEEN IN TABLE 1, THIS SHEET.

### AHYMO ANALYSIS (TABLE 2):

SEE NARRATIVE SHEET C-100.

### STORM DRAIN SIZING (TABLE 3):

STORM DRAINS WERE SIZED BASED ON MANNING'S EQUATION AND GRAVITY FLOW. SIZE OF STORM DRAINS RANGE FROM 6" (FOR SMALL AREA DRAINS) TO 24" (FOR DOWNSTREAM END OF COLLECTION SYSTEM). SEE TABLE 3 (THIS SHEET) FOR STORM DRAIN REACH ANALYSIS. BASIN AND SUB-BASIN FLOWS CAN BE SEEN ON TABLE 1 (THIS SHEET)

### INLET SIZING (TABLE 4):

STORM DRAIN INLETS HAVE BEEN DESIGNED IN SUMP CONDITION. TRAFFIC RATED NYLOPLAST INLETS ARE PROVIDED IN DRIVEWAYS. NON-TRAFFIC RATED NYLOPLAST DOME INLETS ARE PROVIDED IN LANDSCAPED AREAS. INLET CAPACITIES ARE BASED ON NOMOGRAPHS PROVIDED BY THE MANUFACTURER. TABLE 4 SHOWS INLET CAPACITIES AND ACTUAL FLOW TO THE INLET.

INLET 6 IS UNDERSIZED FOR THE SUB-BASIN IT IS INTENDED TO CONTAIN. ONCE CAPACITY IS REACHED, EXCESS FLOW WILL CONTINUE NORTH TO INLET 7 WHICH HAS ENOUGH CAPACITY TO ACCEPT THE ADDITIONAL FLOWS.

### RUNDOWN SIZING (TABLE 5):

CONCRETE RUNDOWNS HAVE BEEN DESIGNED USING MANNING'S EQUATION AND THE WEIR EQUATION (PROVIDED IN TABLE 5). RUNDOWNS R1 & R2 OUTFALL INTO A WATER HARVESTING AREA ON THE WEST PORTION OF THE PROPERTY. RUNDOWN R3 OUTFALLS INTO POND #1.

CONCR	ETE RUNDOWN TABLE			Applications of the second of				
Rundown		Rundown	Actual	Min Weir**	Channel	Channel	Minimum	Capacity*
#	Basin ID	Type	Flow	Length ft	Width ft	Height ft	Slope	CFS
Pond Ru	ndowns							
R1	B2-D	Rectang	0.62	1.00	2.00	0.50	30.00%	30.10
R2	B2-E	Rectang	0.15	1.00	2.00	0.50	30.00%	30.10
R3	B3-B	Rectang	2.26	2.00	2.00	0.50	30.00%	30.10
			Weir Eq: Q=3	3.3L(h^1.5) - **	Ca	pacity Based	on Manning's Eq	w/ n=0.013 -

# **TABLE 5: RUNDOWN SIZING**