

# CITY OF ALBUQUERQUE

Planning Department  
Brennon Williams, Director



Mayor Timothy M. Keller

August 28, 2020

Ronald Bohannon, P.E.  
Tierra West, LLC  
5571 Midway Park Place NE  
Albuquerque, NM 87109

**RE: Paradise North - Unser/McMahon  
Grading and Drainage Plan & Master Drainage Plan  
Engineer's Stamp Date: 08/04/20  
Hydrology File: A11D017**

Dear Mr. Bohannon:

Based upon the information provided in your submittal received 08/05/20, the Grading & Drainage Plan & Master Drainage Plan are approved for Grading Permit, Paving Permit, and for action by the DRB on Platting. Once the grading and paving of the project is complete, an engineering certification will be required.

As a reminder, if the project total area of disturbance (including the staging area and any work within the adjacent Right-of-Way) is 1 acre or more, then an Erosion and Sediment Control (ESC) Plan and Owner's certified Notice of Intent (NOI) is required to be submitted to the Stormwater Quality Engineer (Doug Hughes, PE, [jhughes@cabq.gov](mailto:jhughes@cabq.gov), 924-3420) 14 days prior to any earth disturbance.

If you have any questions, please contact me at 924-3995 or [rbrissette@cabq.gov](mailto:rbrissette@cabq.gov).

Sincerely,

Renée C. Brissette, P.E. CFM  
Senior Engineer, Hydrology  
Planning Department





# City of Albuquerque

Planning Department

Development & Building Services Division

## DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 11/2018)

**Project Title:** \_\_\_\_\_ **Building Permit #:** \_\_\_\_\_ **Hydrology File #:** \_\_\_\_\_

**DRB#:** \_\_\_\_\_ **EPC#:** \_\_\_\_\_ **Work Order#:** \_\_\_\_\_

**Legal Description:** \_\_\_\_\_

**City Address:** \_\_\_\_\_

**Applicant:** \_\_\_\_\_ **Contact:** \_\_\_\_\_

**Address:** \_\_\_\_\_

**Phone#:** \_\_\_\_\_ **Fax#:** \_\_\_\_\_ **E-mail:** \_\_\_\_\_

**Owner:** \_\_\_\_\_ **Contact:** \_\_\_\_\_

**Address:** \_\_\_\_\_

**Phone#:** \_\_\_\_\_ **Fax#:** \_\_\_\_\_ **E-mail:** \_\_\_\_\_

**TYPE OF SUBMITTAL:** \_\_\_\_\_ PLAT ( 9 # OF LOTS) \_\_\_\_\_ RESIDENCE \_\_\_\_\_ DRB SITE \_\_\_\_\_ ADMIN SITE

IS THIS A RESUBMITTAL?: \_\_\_\_\_ Yes \_\_\_\_\_ No

**DEPARTMENT:** \_\_\_\_\_ TRAFFIC/ TRANSPORTATION \_\_\_\_\_ HYDROLOGY/ DRAINAGE

Check all that Apply:

### TYPE OF SUBMITTAL:

- \_\_\_\_\_ ENGINEER/ARCHITECT CERTIFICATION
- \_\_\_\_\_ PAD CERTIFICATION
- \_\_\_\_\_ CONCEPTUAL G & D PLAN
- \_\_\_\_\_ GRADING PLAN
- \_\_\_\_\_ DRAINAGE MASTER PLAN
- \_\_\_\_\_ DRAINAGE REPORT
- \_\_\_\_\_ FLOODPLAIN DEVELOPMENT PERMIT APPLIC
- \_\_\_\_\_ ELEVATION CERTIFICATE
- \_\_\_\_\_ CLOMR/LOMR
- \_\_\_\_\_ TRAFFIC CIRCULATION LAYOUT (TCL)
- \_\_\_\_\_ TRAFFIC IMPACT STUDY (TIS)
- \_\_\_\_\_ OTHER (SPECIFY) \_\_\_\_\_
- \_\_\_\_\_ PRE-DESIGN MEETING?

### TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

- \_\_\_\_\_ BUILDING PERMIT APPROVAL
- \_\_\_\_\_ CERTIFICATE OF OCCUPANCY
- \_\_\_\_\_ PRELIMINARY PLAT APPROVAL
- \_\_\_\_\_ SITE PLAN FOR SUB'D APPROVAL
- \_\_\_\_\_ SITE PLAN FOR BLDG. PERMIT APPROVAL
- \_\_\_\_\_ FINAL PLAT APPROVAL
- \_\_\_\_\_ SIA/ RELEASE OF FINANCIAL GUARANTEE
- \_\_\_\_\_ FOUNDATION PERMIT APPROVAL
- \_\_\_\_\_ GRADING PERMIT APPROVAL
- \_\_\_\_\_ SO-19 APPROVAL
- \_\_\_\_\_ PAVING PERMIT APPROVAL
- \_\_\_\_\_ GRADING/ PAD CERTIFICATION
- \_\_\_\_\_ WORK ORDER APPROVAL
- \_\_\_\_\_ CLOMR/LOMR
- \_\_\_\_\_ FLOODPLAIN DEVELOPMENT PERMIT
- \_\_\_\_\_ OTHER (SPECIFY) \_\_\_\_\_

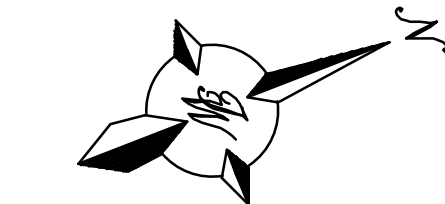
**DATE SUBMITTED:** \_\_\_\_\_ **By:** \_\_\_\_\_

COA STAFF:

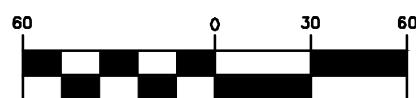
ELECTRONIC SUBMITTAL RECEIVED: \_\_\_\_\_

FEE PAID: \_\_\_\_\_



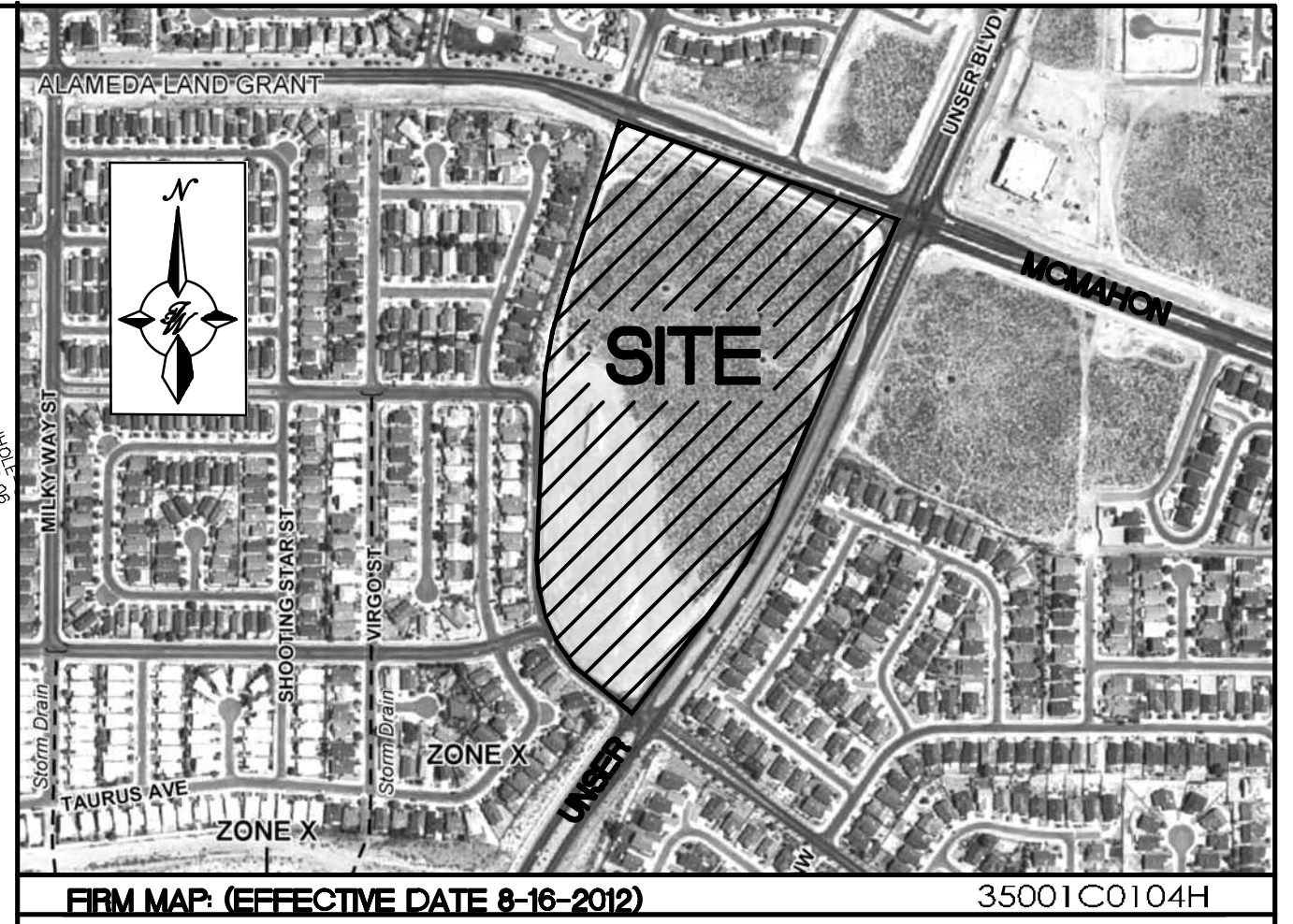


GRAPHIC SCALE



( IN FEET )  
1 inch = 60 ft.

PARADISE SKIES UNIT 1  
FD 4/02/1996  
BK 96C, PG. 145



FRM MAP (EFFECTIVE DATE 8-16-2012)

35001C0104H

#### LEGEND

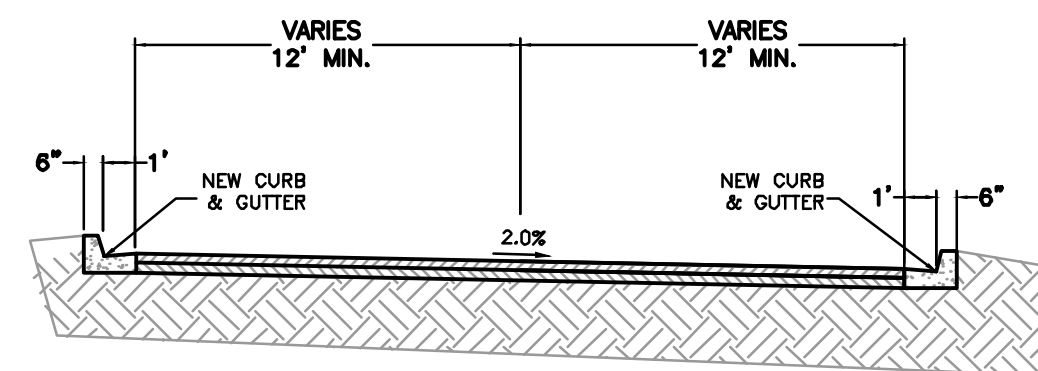
	CURB & GUTTER
	BOUNDARY LINE
	EASEMENT
	CENTERLINE
	RIGHT-OF-WAY
	BUILDING
	SIDEWALK
	ASPHALT PAVING
	CONTOUR MAJOR
	CONTOUR MINOR
	SPOT ELEVATION (FLOWLINE)
	FLOW ARROW
	EXISTING CURB & GUTTER
	EXISTING BOUNDARY LINE
	EXISTING CONTOUR MAJOR
	EXISTING CONTOUR MINOR
	EXISTING SPOT ELEVATION

#### KEYED NOTES:

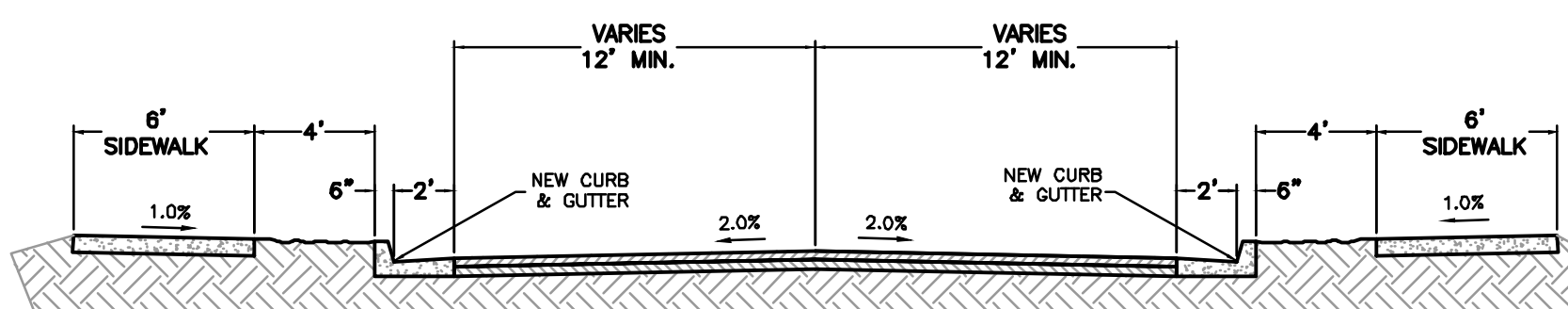
- (A) 18" RCP @ 2.0%
- (B) 18" RCP @ 1.0%
- (C) 18" RCP @ 1.0%
- (D) 18" RCP @ 2.0%
- (E) 18" RCP @ 2.0%
- (F) 18" RCP @ 2.0%
- (G) 24" RCP @ 1.0%
- (H) 24" RCP @ 1.0%
- (I) 18" RCP @ 2.0%
- (J) 24" RCP @ 2.0%
- (K) 18" RCP @ 2.0%
- (L) 36" RCP @ 2.0%
- (M) 18" RCP @ 2.0%
- (N) 36" RCP @ 2.0%
- (O) 18" RCP @ 2.0%
- (P) 30" RCP @ 2.0%, STUBBED 5' PAST EDGE OF PAVEMENT  
STUB INV=5299.53

#### NOTICE TO CONTRACTORS

- AN EXCAVATION/CONSTRUCTION PERMIT WILL BE REQUIRED BEFORE BEGINNING ANY WORK WITHIN CITY RIGHT-OF-WAY. AN APPROVED COPY OF THESE PLANS MUST BE SUBMITTED AT THE TIME OF APPLICATION FOR THIS PERMIT.
- ALL WORK DETAILED ON THESE PLANS TO BE PERFORMED, EXCEPT AS OTHERWISE STATED OR PROVIDED HEREON, SHALL BE CONSTRUCTED IN ACCORDANCE WITH CITY OF ALBUQUERQUE INTERIM STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION, 1985.
- TWO WORKING DAYS PRIOR TO ANY EXCAVATION, CONTRACTOR MUST CONTACT LINE LOCATING SERVICE, 260-1990 (OR DIAL 811 LOCALLY), FOR LOCATION OF EXISTING UTILITIES.
- PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL EXCAVATE AND VERIFY THE HORIZONTAL AND VERTICAL LOCATIONS OF ALL CONSTRUCTIONS. SHOULD A CONFLICT EXIST, THE CONTRACTOR SHALL NOTIFY THE ENGINEER SO THAT THE CONFLICT CAN BE RESOLVED WITH A MINIMUM AMOUNT OF DELAY.
- BACK FILL COMPACTION SHALL BE ACCORDING TO RESIDENTIAL STREET USE.
- MAINTENANCE OF THESE FACILITIES SHALL BE THE RESPONSIBILITY OF THE OWNER OF THE PROPERTY SERVED.
- WORK ON ARTERIAL STREETS SHALL BE PERFORMED ON A 24-HOUR BASIS.



CORRIDOR SECTION A-A  
NTS



BOULEVARD CORRIDOR SECTION B-B  
NTS

#### CAUTION:

ALL EXISTING UTILITIES SHOWN WERE OBTAINED FROM RESEARCH, AS-BUILTS, SURVEYS OR INFORMATION PROVIDED BY OTHERS. IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO AND INCLUDING ANY EXCAVATION, TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND OTHER IMPROVEMENTS. PRIOR TO STARTING THE WORK, ANY CHANGES FROM THIS PLAN SHALL BE COORDINATED WITH AND APPROVED BY THE ENGINEER.

	UNSER & MCMAHON		DRAWN BY RMG
	GRADING AND DRAINAGE PLAN		DATE 08/03/2020
	 5571 MIDWAY PARK PLACE NE ALBUQUERQUE, NM 87109 (505) 858-3100 www.tierravestllc.com		2020015-GR
	SHEET # <b>C1</b>		JOB # 2020015



# MASTER DRAINAGE PLAN

For

## Paradise North SW Corner of Unser/McMahon

Prepared by:

Tierra West, LLC  
5571 Midway Park Place NE  
Albuquerque, New Mexico 87109

August 3, 2020

I certify that this report was prepared under my supervision, and I am a registered professional engineer in the State of New Mexico in good standing.



08-04-20

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Ronald R. Bohannon  
PE # 7868

Job No. 2020015



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## **Purpose**

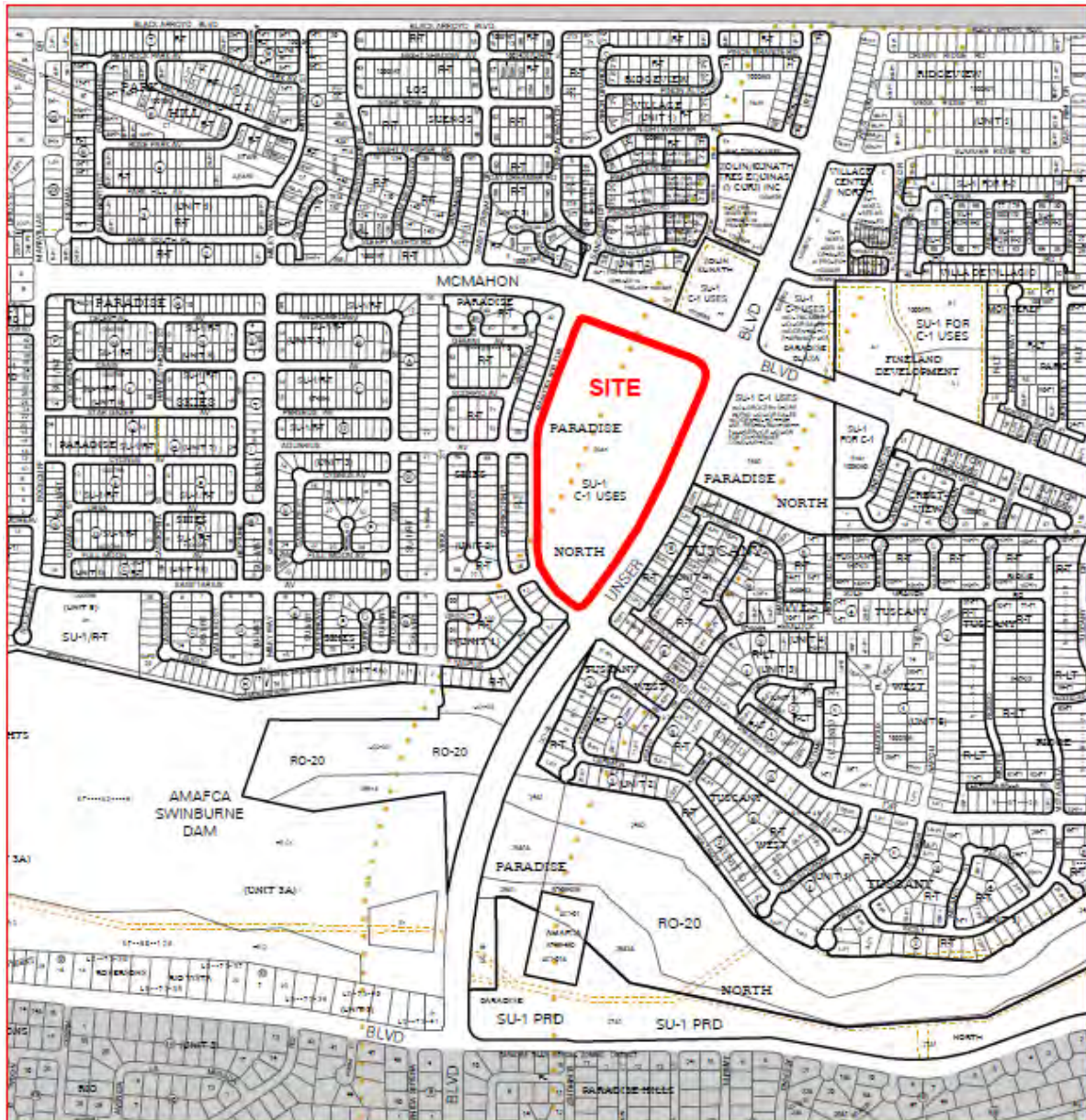
The purpose of this report is to develop a Master Drainage Management Plan for a mixed-use development with commercial/retail and multi-family residential living uses on a 19-acre vacant tract of land. The land is currently going through a replatting process to subdivide the property from 1 lot into 9 lots, private main internal roads will provide access to each of the 9 proposed lots. The current legal description of the lot is “Tract 20A-1 Vacation Amended Plat & Replat of Paradise North”. The legal description for the site once the plat is finalized and recorded will be “Tracts 20A-1A thru 20A-1I Paradise North”. The project construction will be phased, with the initial work being to rough grade the site, pave the internal access roads, and install main utility service lines (storm drain, sanitary sewer, water, dry utility conduits); so this report is also to seek approval for rough grading the site, installing storm drain/manholes/inlets, and paving the internal main drive aisles to have the site “pad-ready” for the proposed 9 lots for potential users.

## **Location**

The site is located at the southwest corner of the Unser Blvd/McMahon Blvd intersection. The property is currently vacant with no development in place. The site is bounded by McMahon Blvd to the north, Unser Blvd to the east, and Bandelier Drive to the west. A portion of Bandelier Drive at the northwest corner of the property has not yet been constructed; this road will be extended to McMahon Blvd along with the construction of this development, however is not taken into consideration for this drainage master plan as it is assumed that the drainage for that roadway extension will be handled within the public Right-of-Way. A vicinity map and aerial image of the site can be seen in Exhibits A and B, respectively.



## Exhibit A – Vicinity Map



For more current information and more details visit: <http://www.cabq.gov/gis>



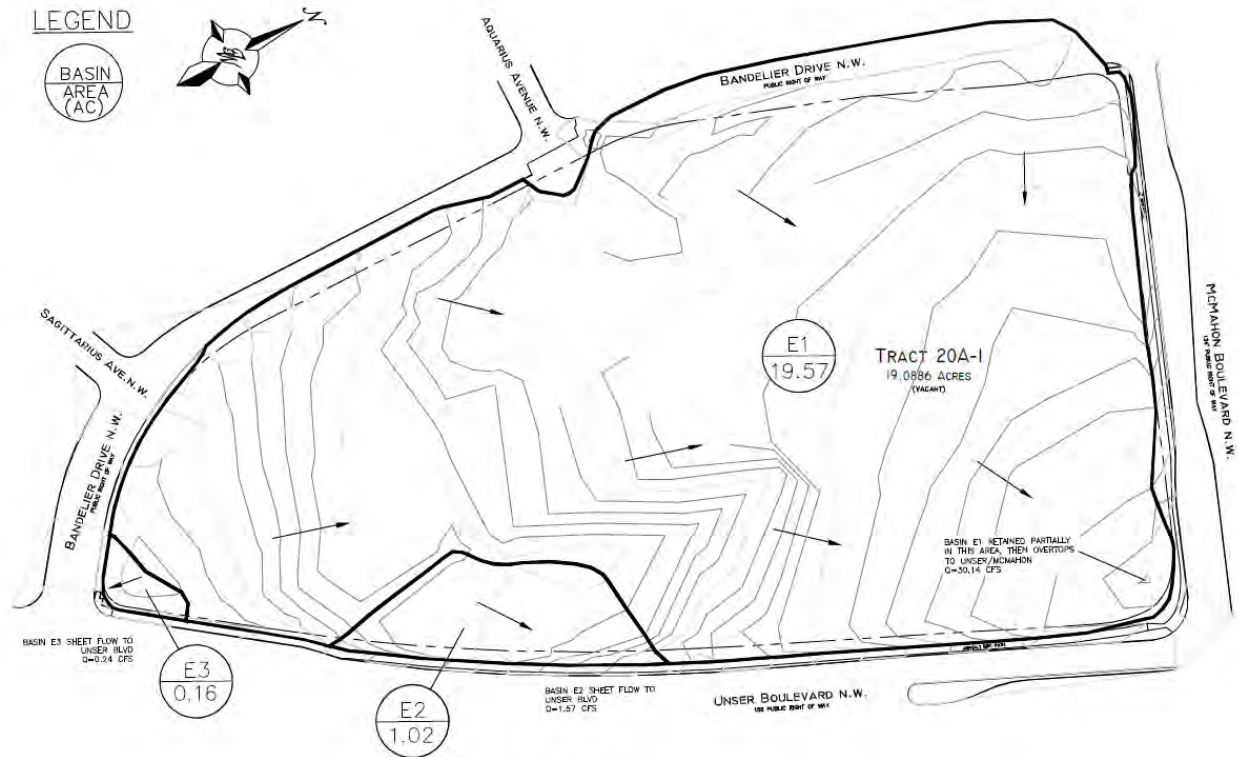


## **Exhibit B – Site Aerial Image**





## Exhibit C – Existing Basin Map



### Existing Conditions

The site is currently vacant and undeveloped. Drainage of the site predominantly flows from southwest to northeast with three primary basins, E1, E2, and E3. The two smaller drainage basins, E2 and E3, sheet flow runoff to the Unser Blvd right-of-way, basin E1 directs runoff towards the Unser/McMahon intersection.

Basin E1 consists of the majority of the site, plus the unbuilt portion of Bandelier Drive near the northwest corner of the site. Runoff from this basin flows from southwest to northeast and is directed towards a small low point onsite near the Unser/McMahon intersection. The runoff from this basin retains a small volume in this low point area and then overtops to the McMahon and Unser right-of-way.

Basin E2 consists of just over one acre of land adjacent to Unser Blvd. Runoff from this basin flows from west to east and sheet flows into the Unser right-of-way.



Basin E3 consists of a small portion of the site located at the northwest corner of the Bandelier Dr/Unser Blvd intersection. This is the highpoint of the site where drainage sheet flows from northwest to southwest and into the Bandelier/Unser intersection.

The total 100-year peak flow of these existing basins is 31.95 cfs, hydrology tables and an enlarged existing drainage basin map can be found in Appendix A. This site lies within the *Master Drainage Study for the Unser/McMahon Area* by Bohannon-Huston, Inc. with an amended date of 11/13/2001 (COA Drainage File #A11/D5A). Per this study, the site lies within Basin DB6 and is allowed a maximum developed flow rate discharge of 78.2 cfs into the existing storm drain in McMahon. Excerpts from this report and developed drainage basin map can be found in Appendix F.

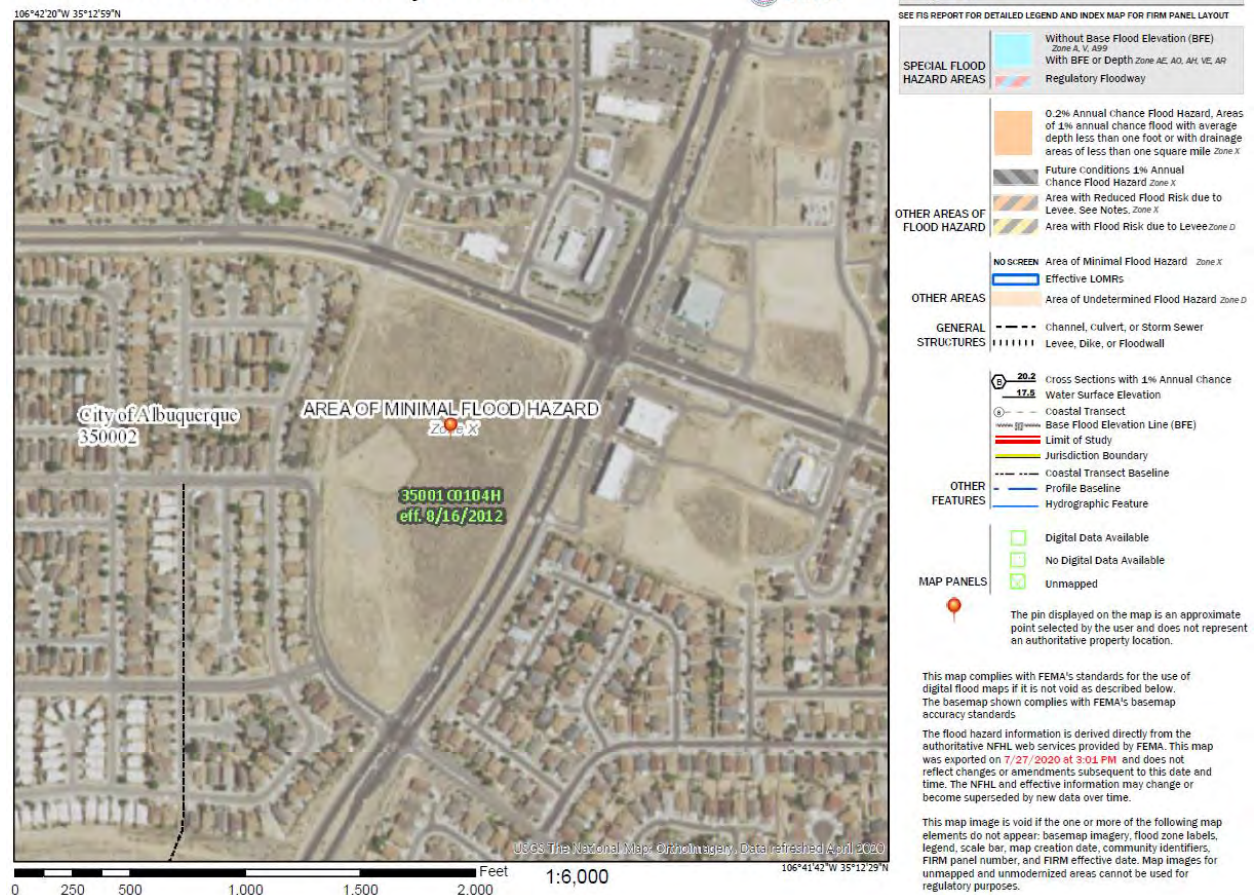


## Flood Plain

The site is located on FIRM Map 35001C0104H. The map indicates that the site does not lie within any flood hazard areas.

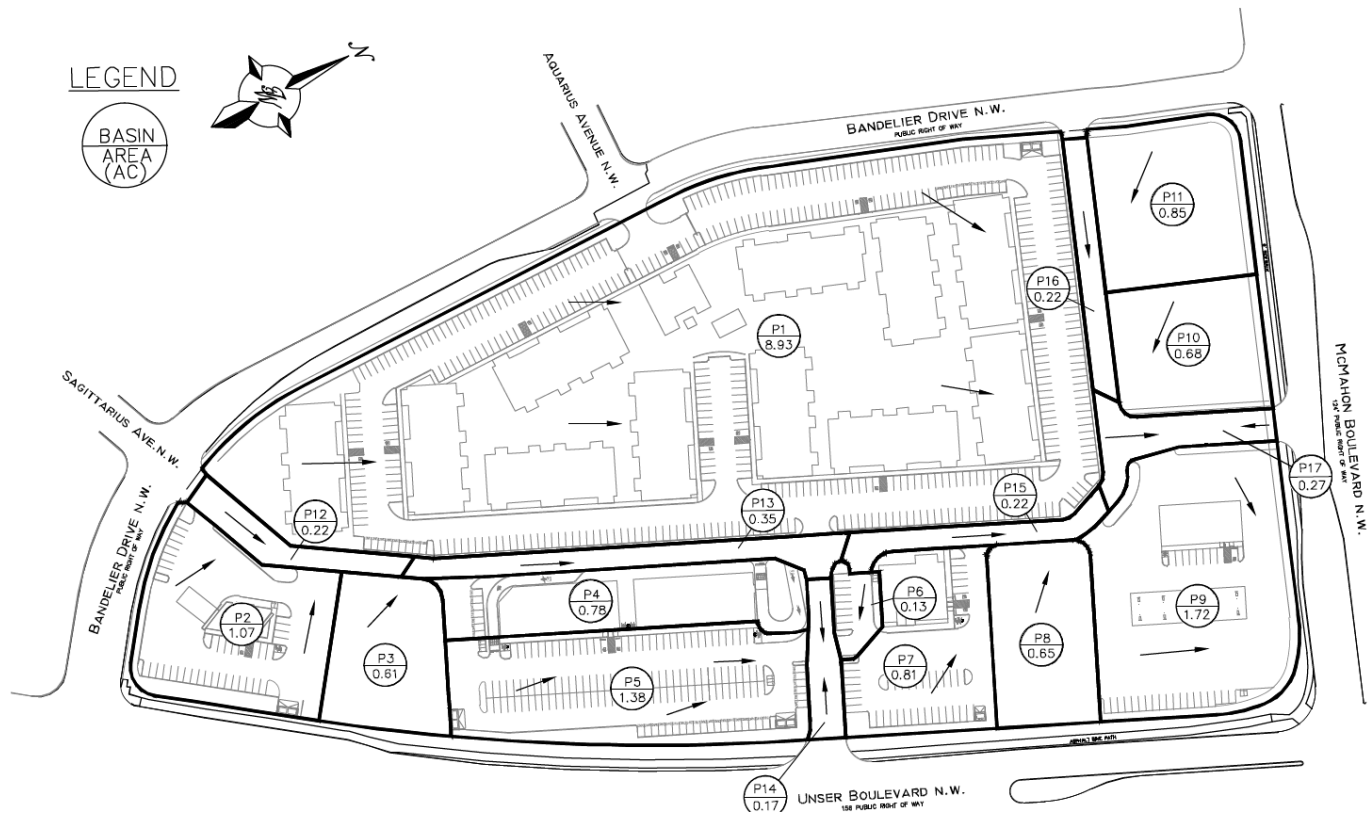
### Exhibit D – FIRM Map

#### National Flood Hazard Layer FIRMette





## **Exhibit E – Proposed Basin Map**



### **Proposed Conditions**

All improvements of the site will be built in phases, depending on when each of the 9 proposed lots gain a user for development. The first phase of construction will be to rough grade the entire site, install the main utilities internal to the site (main storm drain/manholes/inlets, sanitary sewer, water, and dry utility conduits). The intent is to have the entire site “pad-ready” for full development. Subsequent phases will then consist of site development plans of each lot as users come in for development. This overall drainage plan assumes full development, with each lot (Basins P1 thru P11) having 10% Type ‘C’ and 90% Type ‘D’ Land Treatment. The internal roads (Basins P12 thru P17) are assumed as 100% Type ‘D’ Land Treatment. As previously stated in the “Purpose” section of this report, our intent is to first rough grade the site, pave the main



internal roads (Basins P12 thru P17) and install the main storm drain line and associated manholes and curb inlets within these internal roads.

The overall drainage concept will be to discharge the site from south to north via storm drain connection to the public storm drain in McMahon Blvd. The site will be limited to a maximum discharge of 78.2 cfs to the McMahon storm drain per the BHI 2001 *Master Drainage Study for the Unser/McMahon Area*. As each lot goes through the development and entitlement process, they will each have to have their own grading and drainage plan that conforms to the discharge and water quality criteria identified in this drainage study.

Basin P1 consists of the largest proposed lot onsite, predominantly fronted along Bandelier Drive. The lot is intended to be a multi-family residential apartment complex and is zoned as such. This basin will be required to drain from Southeast to northwest towards Basin P17 via storm drain connection. A 30" storm drain will be stubbed from the main storm drain line near the northwest corner of the basin. The peak discharge from this basin will be limited to 35.69 cfs.

Basin P2 consists of the commercial lot at the southeast corner of the site. This lot will drain via surface flow from southeast to northwest into the internal road, Basin P12. Discharge from this site will be limited to 4.28 cfs. Basin P12 will drain from south to north into an at-grade Double Type 'A' Inlet at a rate of 5.08 cfs and with a bypass of 2.8 cfs to Basin P13.

Basin P3 consists of the next northern commercial lot that fronts Unser Blvd, drainage will surface flow from southeast to northwest into the internal road, Basin P13. This lot/basin will be limited to a discharge rate of 2.44 cfs into Basin P13. Basin P4 consists of the western half of the next northern lot that fronts Unser Blvd. Like P3, Basin P4 will drain from southeast to northwest into P13 at a maximum discharge rate of 3.13 cfs. The internal road Basin P13 outfall will consist of a Double Type 'A' Inlet and a Double Type 'C' Inlet that will pick up 7.8 cfs of the basins and have 1.3 cfs bypass to Basin P15.



Basins P5 and P6 will surface flow towards Basin P14, which is the internal road connection to Unser Blvd. Basin P14 will have a Double Type 'C' Inlet in a sump that will connect via storm drain to the inlets of the internal road storm drain in P12, P13 and P15. The sump inlet has taken into account a 50% clogging factor and doesn't consider the throat of the inlet as part of the capacity, but should the inlet fully clog, then drainage flows can overtop into the Unser Blvd right-of-way. The sump inlet will pick up 6.73 cfs of drainage from these basins with no bypass flows.

Basin P7 and P8 will convey drainage via surface flow from southeast to northwest towards the internal road, Basin P15. Basin P7 will be limited to a discharge to this road of 3.25 cfs and Basin P8 will be limited to a discharge rate of 2.59 cfs. The internal road Basin P15 outfall will consist of a Double Type 'A' inlet and a Double Type 'C' inlet at-grade that will pick up 7.0 cfs from the upland basins and will have 1.05 cfs bypass to Basin P17.

Basins P10 and P11 will surface flow from northwest to southeast towards the internal road Basin P16. Basin P16 will have a Double Type 'A' Inlet at-grade near the easternmost side of the basin. The inlet will pick up 3.0 cfs from the upland basins and will have 4.0 cfs bypass to Basin P17. Basin P10 will be limited to a discharge rate of 2.72 cfs and Basin P11 will be limited to 3.38 cfs.

Basin P17 is the furthest downstream basin within this development. This basin will pick up the bypass flows from P15 and P16 and discharge into a Double Type 'C' inlet in sump condition. Similar to P14, the inlet in Basin P17 capacity has taken into account a 50% clogging factor and excludes the capacity of the inlet throat, but should the inlet clog then drainage flows will overtop towards the McMahon Blvd right-of-way. The inlet in this basin will connect to the existing storm drain in McMahon Blvd.

Basin P9 is the only lot that will not surface flow towards the internal road due to the grades of the development. Instead, this basin will flow from southwest to northeast and will be required to discharge via storm drain connection to the back of the existing storm drain inlet in McMahon Blvd, near the McMahon/Unser intersection. This ultimately



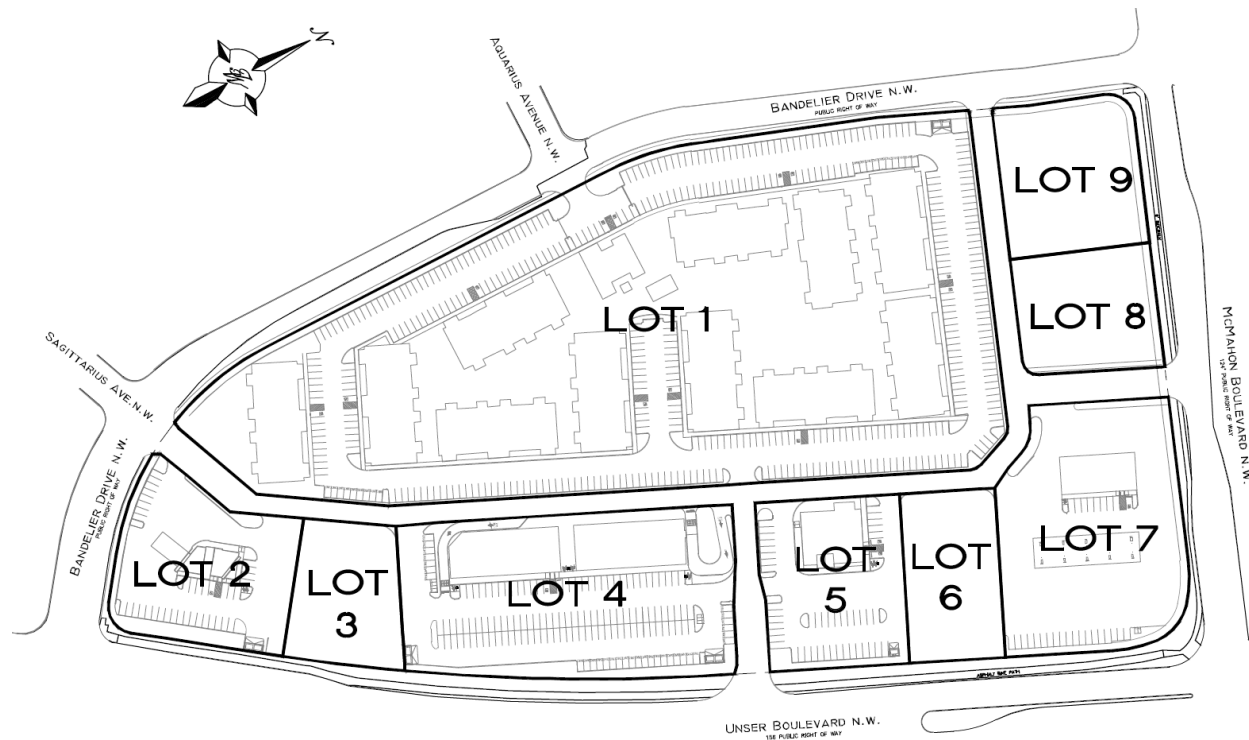
leads P9 developed drainage into the same McMahon storm drain that captures all of the developed onsite drainage.

The total 100-year 6-hour peak discharge of the entire site at the assumed land treatments and full development is 76.37 cfs. The maximum discharge rate allowed from this site from the 2001 BHI *Master Drainage Study for the Unser/McMahon Area* is 78.2 cfs, so the fully developed conditions will be allowable for this site. The developed conditions hydrology table and enlarged proposed basin map can be found in Appendix A. *Table 1* below also gives the drainage criteria needed to be followed for each proposed lot as they become ready for specific site development. A more detailed Drainage Criteria Map, providing this table plus the lots and storm drain layout, can be found in Appendix G.

**Table 1 - Paradise North Developed Drainage Criteria**

Lot No.	Designated Basin(s)	Drains to Basin...	Discharge Conveyance Method	Max Allowable Discharge Rate (cfs)
1	P1	P17	Storm Drain Connection Only	35.69
2	P2	P12	Surface Flow	4.28
3	P3	P13	Surface Flow	2.44
4	P4	P13	Surface Flow	3.13
	P5	P14	Surface Flow	5.52
5	P6	P14	Surface Flow	0.52
	P7	P15	Surface Flow	3.25
6	P8	P15	Surface Flow	2.59
7	P9	McMahon Curb Inlet	Storm Drain Connection Only	6.88
8	P10	P16	Surface Flow	2.72
9	P11	P16	Surface Flow	3.38





## Stormwater Quality Management

As each lot becomes ready to be developed, each lot will need to capture their own onsite water quality volume prior to discharging any runoff to the main internal roads and to any public right-of-way. The onsite stormwater quality volume required to be captured shall follow Article 6-12 of the COA Development Process Manual dated June 15, 2020 for new development, which can be calculated as 0.42 inches multiplied by the impervious area of each developed lot.

## Calculations

The *Weighted E Method* and *Peak Discharge Rate for Small Watersheds* Under Article 6-2 of the COA Development Process Manual dated June 15, 2020 was used to calculate the runoff and volume for the site, the hydrology tables can be found in Appendix A. Drainage capacities for the gutter depths and storm drains were



determined through Bentley FlowMaster and results can be found in Appendix C and D, respectively. Drop inlet capacity calculations can be found in Appendix D as well, which follow Figure 6.9.10 of the COA DPM. Lastly, Appendix E gives calculations for runoff bypass flow for internal roads curb inlets.

## **Summary**

The entire site will consist of 9 lots and internal roads for access to each lot. The entire site will be phased for development, with the first phase being rough grading the entire site, installing the main storm drain line/inlets, and paving the internal roads to be “pad-ready” for development of each lot. The enclosed grading plan shows the proposed rough grades for each lot, the finished grades of the internal roads, and the grate and invert elevations of the drainage inlets and storm drain.

The proposed full development will consist of 1 residential multi-family lot while the remaining 8 will be for commercial/retail uses. As each lot goes through the site development plan process for building permit approval, the developer will need to follow the drainage criteria set for in this master drainage plan. The intent of this master plan is also for approval of rough grading, storm drain installation, paving internal roads, and plat approval.



## **APPENDIX A**

### **EXISTING/PROPOSED HYDROLOGY TABLE AND DRAINAGE BASIN MAPS**



## DPM Weighted E Method

Precipitation Zone 1

SW Corner Unser Blvd/McMahon Blvd

Tracts 20A-1A thru 20A-1I Paradise North (Formerly Tract 20A-1 Paradise North)

TWLLC VP Date 7/22/2020

### Existing Conditions

Basin Descriptions												100-Year, 6-Hr			10-Year, 6-Hr		
Basin ID	Area (sf)	Area (acres)	Area (sq miles)	Treatment A		Treatment B		Treatment C		Treatment D		Weighted E (in)	Volume (ac-ft)	Flow cfs	Weighted E (in)	Volume (ac-ft)	Flow cfs
				%	(acres)	%	(acres)	%	(acres)	%	(acres)						
E1	852,497.83	19.571	0.03058	100%	19.571	0%	0.000	0%	0.000	0%	0.000	0.550	0.897	30.14	0.110	0.179	5.87
E2	44,474.92	1.021	0.00160	100%	1.021	0%	0.000	0%	0.000	0%	0.000	0.550	0.047	1.57	0.110	0.009	0.31
E3	6,826.56	0.157	0.00024	100%	0.157	0%	0.000	0%	0.000	0%	0.000	0.550	0.007	0.24	0.110	0.001	0.05
<b>Total</b>	<b>903,799.31</b>	<b>20.748</b>	<b>0.03242</b>		<b>0.000</b>		<b>0.000</b>		<b>0.000</b>		<b>0.000</b>		<b>0.951</b>	<b>31.95</b>		<b>0.190</b>	<b>6.22</b>

### Proposed Conditions

Basin Descriptions												100-Year, 6-Hr			10-Year, 6-Hr		
Basin ID	Area (sf)	Area (acres)	Area (sq miles)	Treatment A		Treatment B		Treatment C		Treatment D		Weighted E (in)	Volume (ac-ft)	Flow cfs	Weighted E (in)	Volume (ac-ft)	Flow cfs
				%	(acres)	%	(acres)	%	(acres)	%	(acres)						
P1	389,121.54	8.933	0.01396	0%	0.000	0%	0.000	10%	0.893	90%	0.040	2.111	1.571	35.69	1.330	0.990	21.97
P2	46,633.06	1.071	0.00167	0%	0.000	0%	0.000	10%	0.107	90%	0.963	2.111	0.188	4.28	1.330	0.119	2.63
P3	26,588.77	0.610	0.00095	0%	0.000	0%	0.000	10%	0.061	90%	0.549	2.111	0.107	2.44	1.330	0.068	1.50
P4	34,092.59	0.783	0.00122	0%	0.000	0%	0.000	10%	0.078	90%	0.704	2.111	0.138	3.13	1.330	0.087	1.92
P5	60,232.39	1.383	0.00216	0%	0.000	0%	0.000	10%	0.138	90%	1.244	2.111	0.243	5.52	1.330	0.153	3.40
P6	5,706.02	0.131	0.00020	0%	0.000	0%	0.000	10%	0.013	90%	0.118	2.111	0.023	0.52	1.330	0.015	0.32
P7	35,443.02	0.814	0.00127	0%	0.000	0%	0.000	10%	0.081	90%	0.732	2.111	0.143	3.25	1.330	0.090	2.00
P8	28,224.99	0.648	0.00101	0%	0.000	0%	0.000	10%	0.065	90%	0.583	2.111	0.114	2.59	1.330	0.072	1.59
P9	75,044.37	1.723	0.00269	0%	0.000	0%	0.000	10%	0.172	90%	1.551	2.111	0.303	6.88	1.330	0.191	4.24
P10	29,615.39	0.680	0.00106	0%	0.000	0%	0.000	10%	0.068	90%	0.612	2.111	0.120	2.72	1.330	0.075	1.67
P11	36,890.30	0.847	0.00132	0%	0.000	0%	0.000	10%	0.085	90%	0.762	2.111	0.149	3.38	1.330	0.094	2.08
P12	9,404.71	0.216	0.00034	0%	0.000	0%	0.000	0%	0.000	100%	0.216	2.240	0.040	0.89	1.430	0.026	0.55
P13	15,328.54	0.352	0.00055	0%	0.000	0%	0.000	0%	0.000	100%	0.352	2.240	0.066	1.45	1.430	0.042	0.90
P14	7,315.89	0.168	0.00026	0%	0.000	0%	0.000	0%	0.000	100%	0.168	2.240	0.031	0.69	1.430	0.020	0.43
P15	9,646.85	0.221	0.00035	0%	0.000	0%	0.000	0%	0.000	100%	0.221	2.240	0.041	0.91	1.430	0.026	0.57
P16	9,520.30	0.219	0.00034	0%	0.000	0%	0.000	0%	0.000	100%	0.219	2.240	0.041	0.90	1.430	0.026	0.56
P17	11,897.56	0.273	0.00043	0%	0.000	0%	0.000	0%	0.000	100%	0.273	2.240	0.051	1.13	1.430	0.033	0.70
<b>Total</b>	<b>830,706.29</b>	<b>19.070</b>	<b>0.02980</b>		<b>0.000</b>		<b>0.000</b>		<b>1.762</b>		<b>17.308</b>		<b>3.370</b>	<b>76.37</b>		<b>2.126</b>	<b>47.05</b>

### Equations:

Weighted E =  $E_a \cdot A_a + E_b \cdot A_b + E_c \cdot A_c + E_d \cdot A_d$  / (Total Area)

Volume = Weighted E \* Total Area

Flow =  $Q_a \cdot A_a + Q_b \cdot A_b + Q_c \cdot A_c + Q_d \cdot A_d$

Excess Precipitation, E (in.)		
Zone 1	100-Year	10-Year
Ea	0.55	0.11
Eb	0.73	0.26
Ec	0.95	0.43
Ed	2.24	1.43

Peak Discharge (cfs/acre)		
Zone 1	100-Year	10-Year
Qa	1.54	0.3
Qb	2.16	0.81
Qc	2.87	1.46
Qd	4.12	2.57

### Water Quality Volume (Onsite)

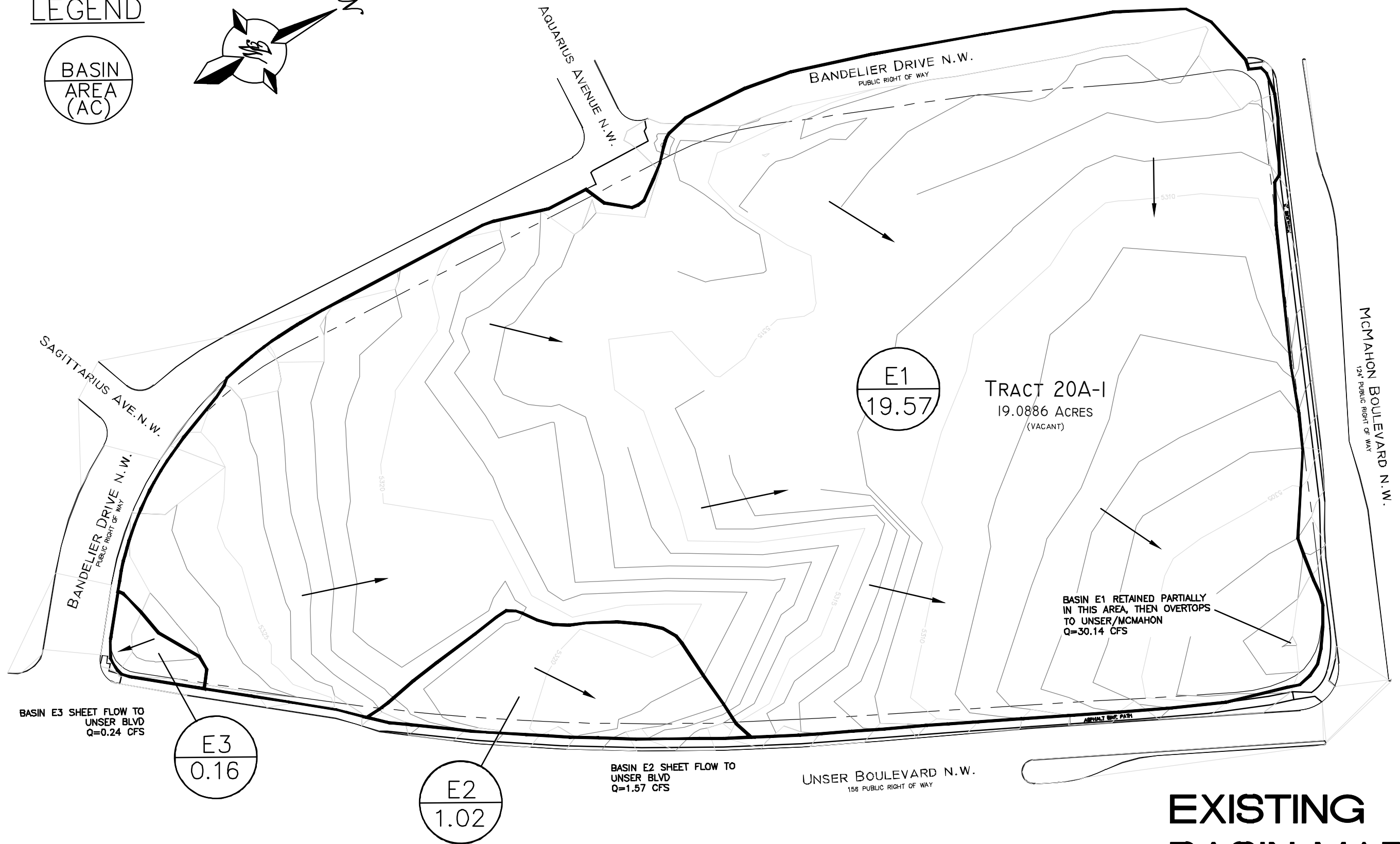
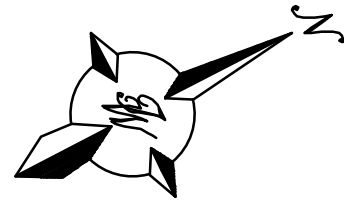
Total Impervious Area = 17.307 Acres = 753,892.92 SF

Retainage depth = 0.42" = 0.035' (COA DPM Article 6-12)

Retention Volume =  $0.035 \cdot 753,892.92 = 26,386.25$  CF = **0.606 Ac-Ft**



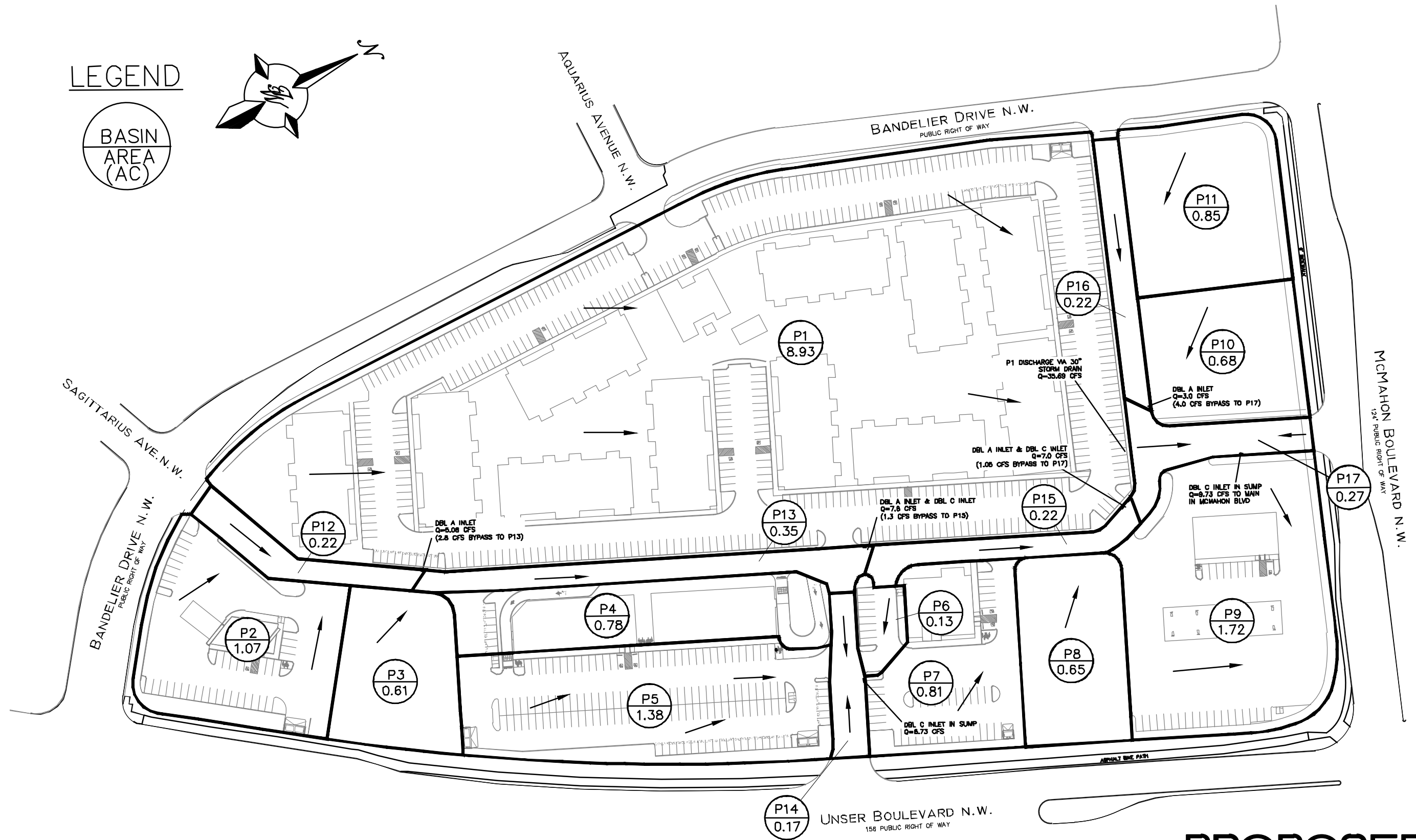
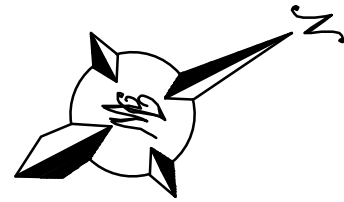
# LEGEND



## EXISTING BASIN MAP



# LEGEND



## PROPOSED BASIN MAP



## **APPENDIX B**

### **STORM DRAIN AND INLET SCHEMATIC MAP**



## **APPENDIX C**

### **GUTTER DEPTH MODELING RESULTS**



## Worksheet for Gutter Depth - Inlet Area 1

### Project Description

Solve For Spread

### Input Data

Channel Slope	0.03000	ft/ft
Discharge	5.08	ft <sup>3</sup> /s
Gutter Width	2.00	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	

### Results

Spread	9.25	ft	
Flow Area	0.94	ft <sup>2</sup>	
Depth	0.27	ft	← Used for Inlet Grate Capacity Determination
Gutter Depression	0.09	ft	
Velocity	5.40	ft/s	



## Worksheet for Gutter Depth - Inlet Area 2

### Project Description

Solve For Spread

### Input Data

Channel Slope	0.01000	ft/ft
Discharge	9.10	ft <sup>3</sup> /s
Gutter Width	2.00	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	

### Results

Spread	14.83	ft
Flow Area	2.28	ft <sup>2</sup>
Depth	0.38	ft
Gutter Depression	0.08	ft
Velocity	3.99	ft/s

← Used for Inlet Grate  
Capacity Determination



## Worksheet for Gutter Depth - Inlet Area 4

### Project Description

Solve For Spread

### Input Data

Channel Slope	0.01100	ft/ft
Discharge	8.05	ft <sup>3</sup> /s
Gutter Width	2.00	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	

### Results

Spread	13.86	ft
Flow Area	2.00	ft <sup>2</sup>
Depth	0.36	ft
Gutter Depression	0.08	ft
Velocity	4.02	ft/s

← Used for Inlet Grate  
Capacity Determination



## Worksheet for Gutter Depth - Inlet Area 5

### Project Description

Solve For Spread

### Input Data

Channel Slope	0.01700	ft/ft
Discharge	7.00	ft <sup>3</sup> /s
Gutter Width	2.00	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	

### Results

Spread	11.99	ft
Flow Area	1.52	ft <sup>2</sup>
Depth	0.32	ft
Gutter Depression	0.08	ft
Velocity	4.61	ft/s

← Used for Inlet Grate  
Capacity Determination



## **APPENDIX D**

### **DRAINAGE INLET AND STORM DRAIN CAPACITIES**



FIGURE 6.9.10 Grate Capacities for Types "Double A," "Double C," and "Double D"

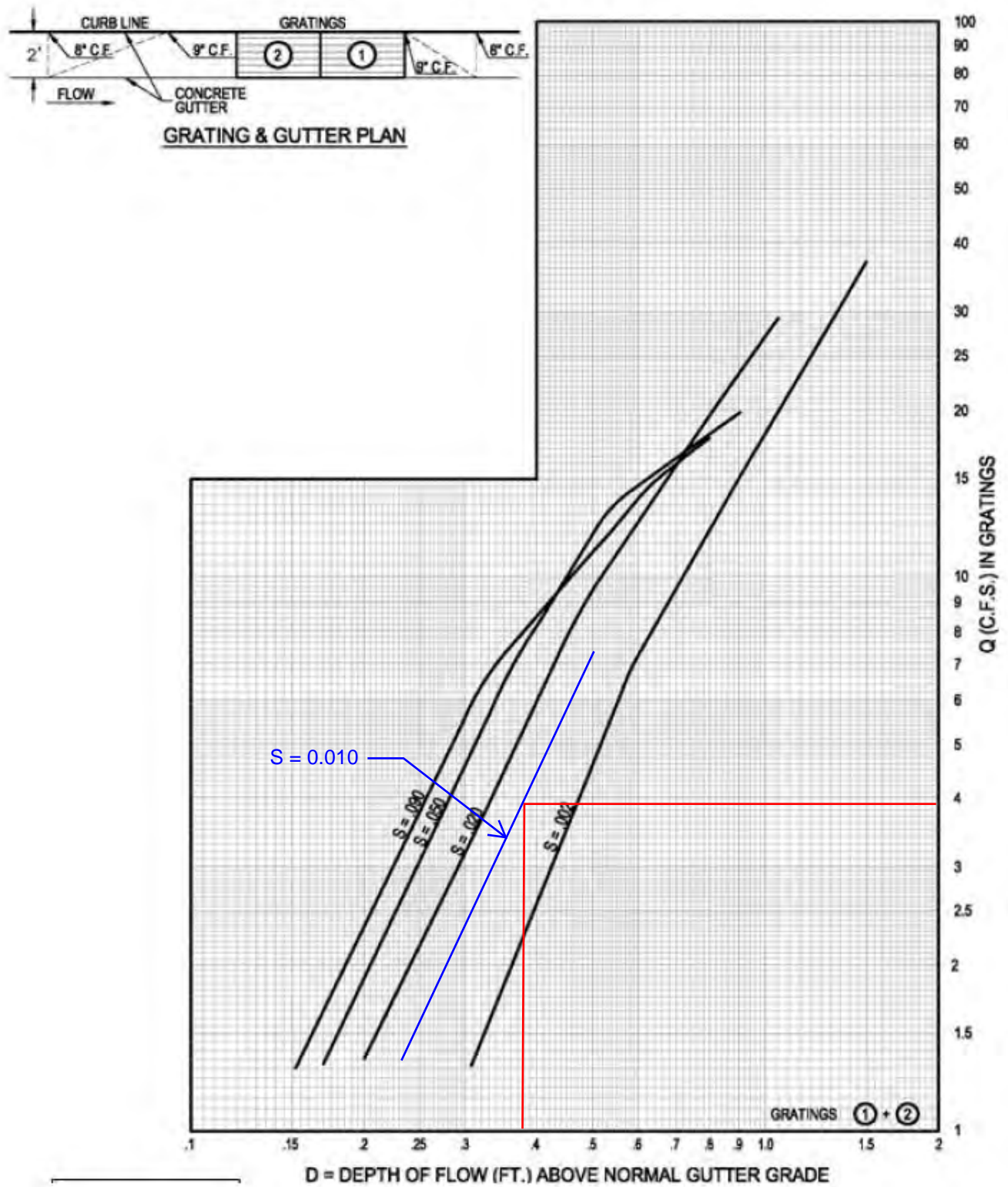




FIGURE 6.9.10 Grate Capacities for Types "Double A," "Double C," and "Double D"

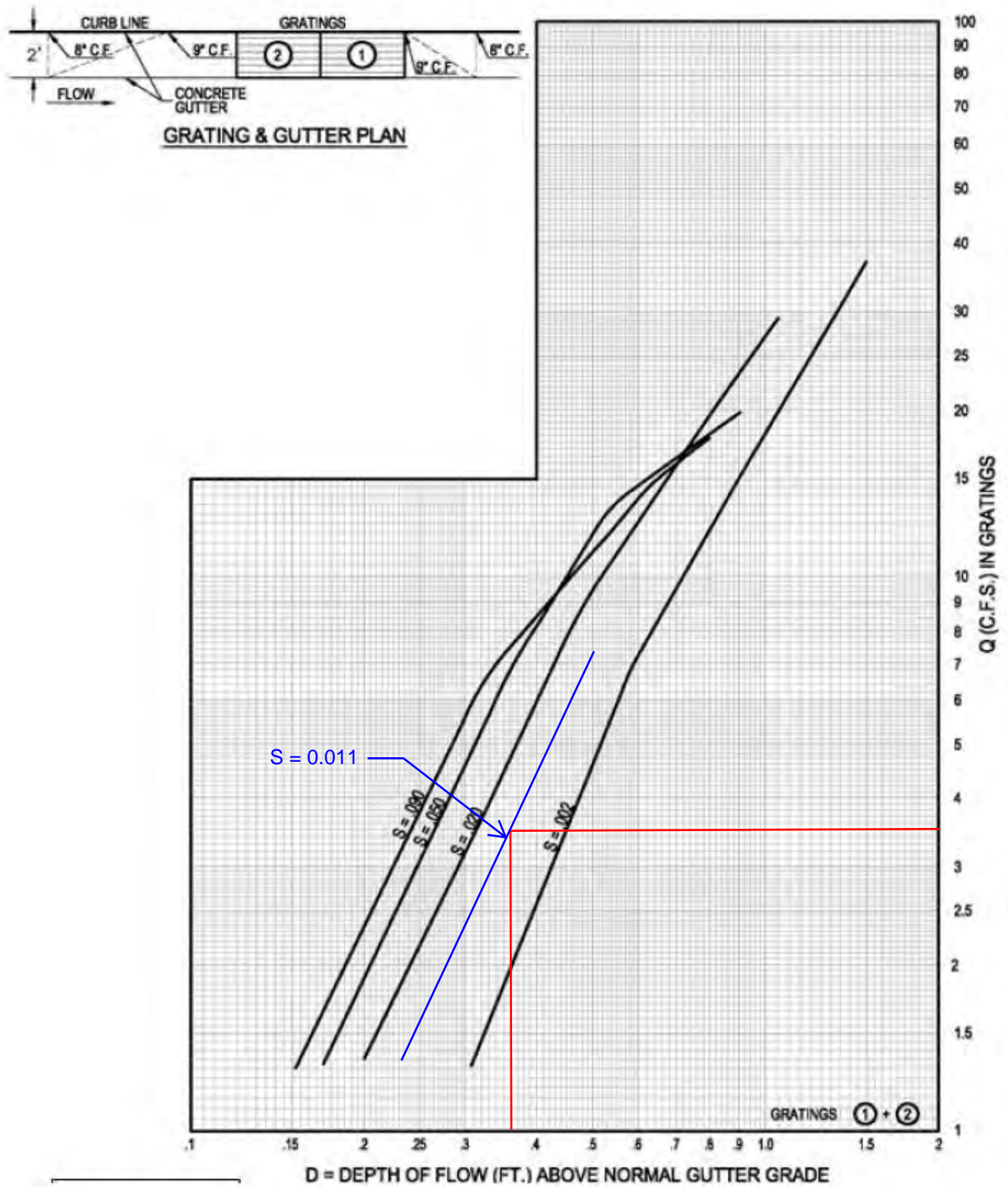




FIGURE 6.9.10 Grate Capacities for Types "Double A," "Double C," and "Double D"

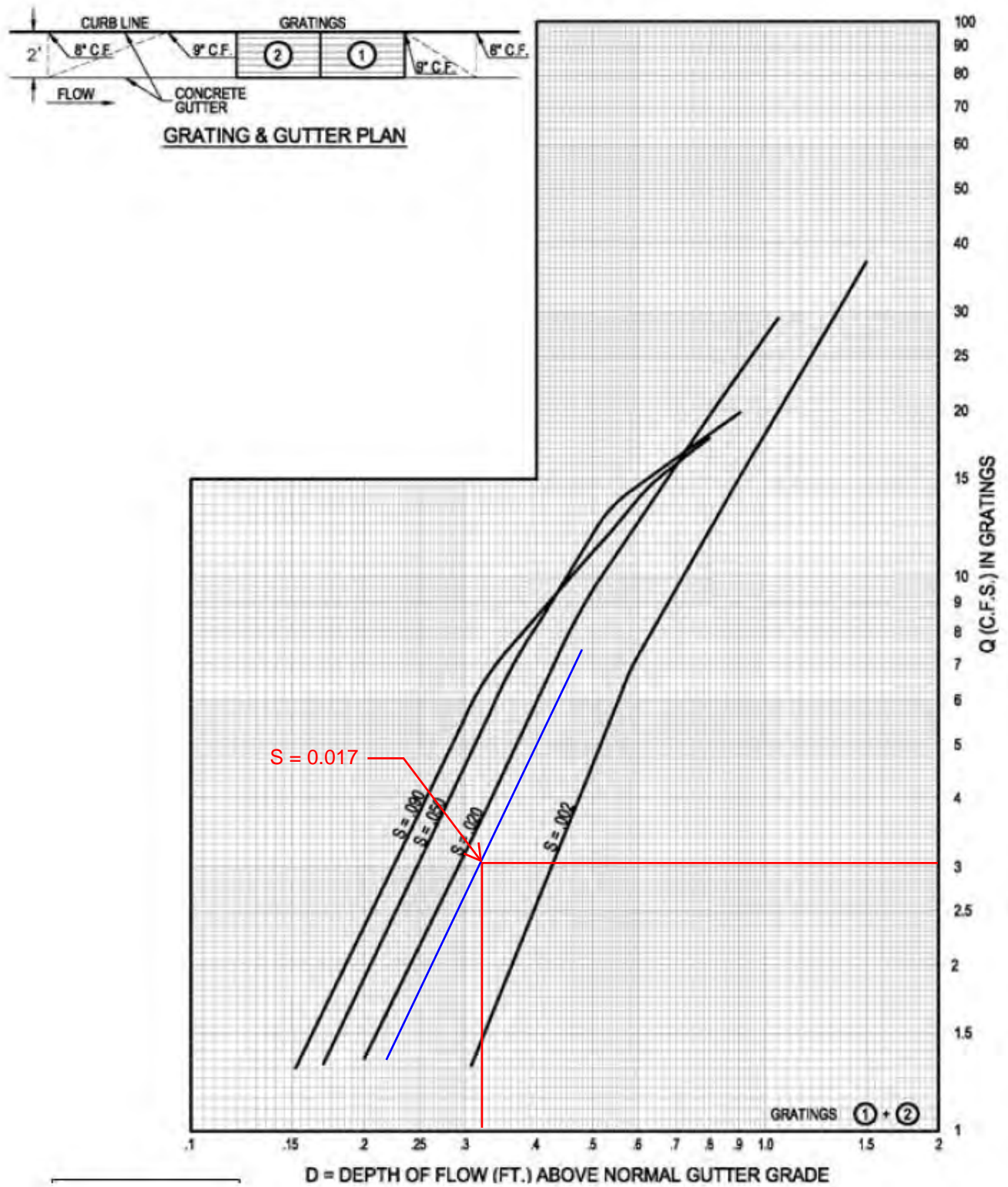
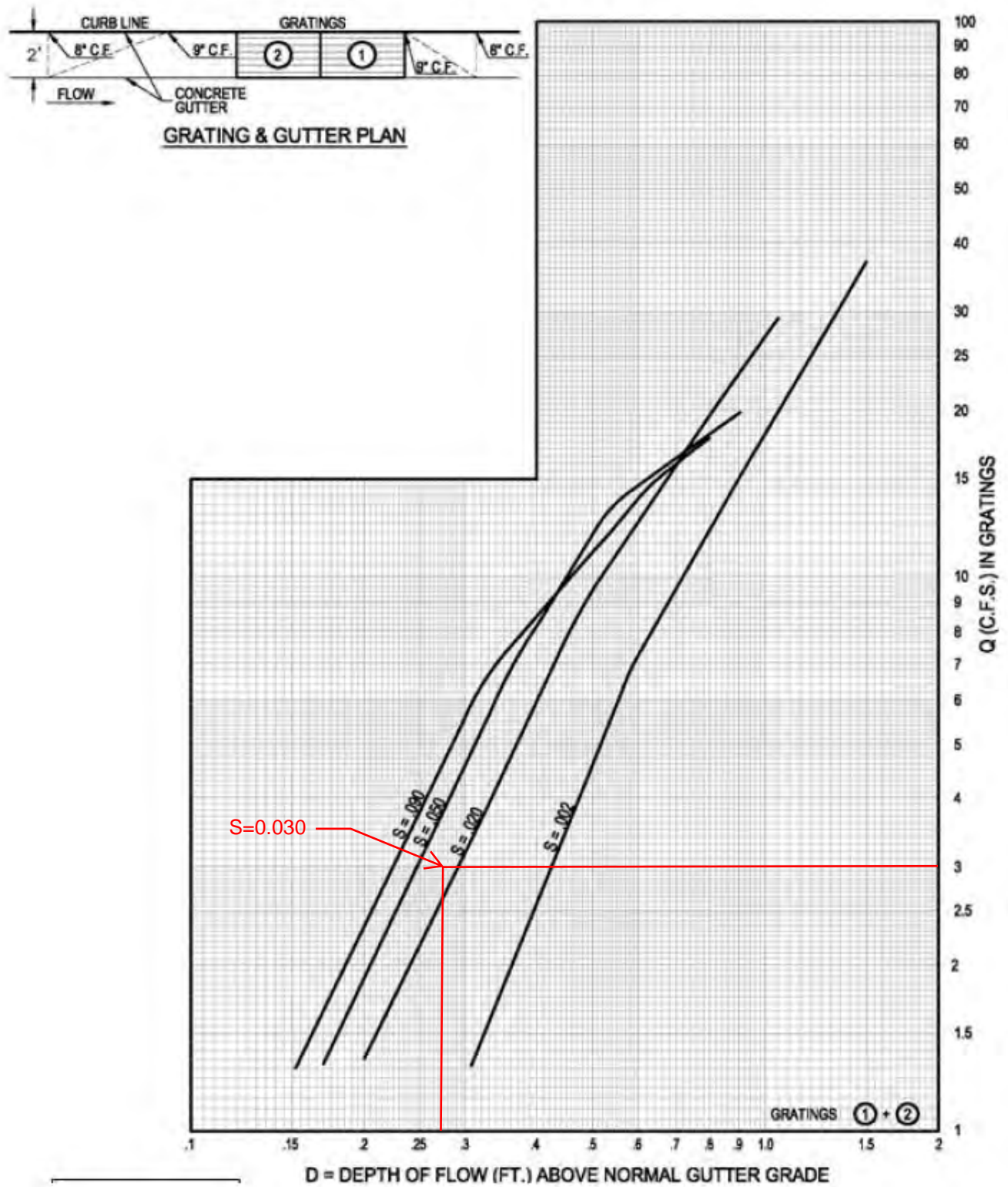




FIGURE 6.9.10 Grate Capacities for Types "Double A," "Double C," and "Double D"





## Worksheet for Storm Drain A/B Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	1.50	ft
Discharge	3.00	ft <sup>3</sup> /s

### Results

Normal Depth	0.55	ft
Flow Area	0.59	ft <sup>2</sup>
Wetted Perimeter	1.95	ft
Hydraulic Radius	0.30	ft
Top Width	1.44	ft
Critical Depth	0.66	ft
Percent Full	36.6	%
Critical Slope	0.00513	ft/ft
Velocity	5.13	ft/s
Velocity Head	0.41	ft
Specific Energy	0.96	ft
Froude Number	1.42	
Maximum Discharge	11.30	ft <sup>3</sup> /s
Discharge Full	10.50	ft <sup>3</sup> /s
Slope Full	0.00082	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	36.58	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain C Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	1.50	ft
Discharge	6.73	ft <sup>3</sup> /s

### Results

Normal Depth	0.87	ft
Flow Area	1.07	ft <sup>2</sup>
Wetted Perimeter	2.60	ft
Hydraulic Radius	0.41	ft
Top Width	1.48	ft
Critical Depth	1.00	ft
Percent Full	58.2	%
Critical Slope	0.00661	ft/ft
Velocity	6.31	ft/s
Velocity Head	0.62	ft
Specific Energy	1.49	ft
Froude Number	1.31	
Maximum Discharge	11.30	ft <sup>3</sup> /s
Discharge Full	10.50	ft <sup>3</sup> /s
Slope Full	0.00411	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	58.20	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain D Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	1.50	ft
Discharge	9.73	ft <sup>3</sup> /s

### Results

Normal Depth	0.89	ft
Flow Area	1.09	ft <sup>2</sup>
Wetted Perimeter	2.63	ft
Hydraulic Radius	0.41	ft
Top Width	1.48	ft
Critical Depth	1.20	ft
Percent Full	59.0	%
Critical Slope	0.00892	ft/ft
Velocity	8.96	ft/s
Velocity Head	1.25	ft
Specific Energy	2.13	ft
Froude Number	1.84	
Maximum Discharge	15.98	ft <sup>3</sup> /s
Discharge Full	14.85	ft <sup>3</sup> /s
Slope Full	0.00858	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	59.03	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain E/F Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	1.50	ft
Discharge	7.80	ft <sup>3</sup> /s

### Results

Normal Depth	0.77	ft
Flow Area	0.92	ft <sup>2</sup>
Wetted Perimeter	2.40	ft
Hydraulic Radius	0.38	ft
Top Width	1.50	ft
Critical Depth	1.08	ft
Percent Full	51.5	%
Critical Slope	0.00728	ft/ft
Velocity	8.51	ft/s
Velocity Head	1.13	ft
Specific Energy	1.90	ft
Froude Number	1.92	
Maximum Discharge	15.98	ft <sup>3</sup> /s
Discharge Full	14.85	ft <sup>3</sup> /s
Slope Full	0.00551	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	51.47	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain G/H Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	2.00	ft
Discharge	17.53	ft <sup>3</sup> /s

### Results

Normal Depth	1.32	ft
Flow Area	2.20	ft <sup>2</sup>
Wetted Perimeter	3.80	ft
Hydraulic Radius	0.58	ft
Top Width	1.89	ft
Critical Depth	1.51	ft
Percent Full	66.1	%
Critical Slope	0.00712	ft/ft
Velocity	7.95	ft/s
Velocity Head	0.98	ft
Specific Energy	2.31	ft
Froude Number	1.30	
Maximum Discharge	24.33	ft <sup>3</sup> /s
Discharge Full	22.62	ft <sup>3</sup> /s
Slope Full	0.00601	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	66.13	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain I/O Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	1.50	ft
Discharge	7.00	ft <sup>3</sup> /s

### Results

Normal Depth	0.72	ft
Flow Area	0.84	ft <sup>2</sup>
Wetted Perimeter	2.30	ft
Hydraulic Radius	0.37	ft
Top Width	1.50	ft
Critical Depth	1.02	ft
Percent Full	48.3	%
Critical Slope	0.00676	ft/ft
Velocity	8.28	ft/s
Velocity Head	1.07	ft
Specific Energy	1.79	ft
Froude Number	1.95	
Maximum Discharge	15.98	ft <sup>3</sup> /s
Discharge Full	14.85	ft <sup>3</sup> /s
Slope Full	0.00444	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	48.28	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain J Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	2.00	ft
Discharge	24.53	ft <sup>3</sup> /s

### Results

Normal Depth	1.31	ft
Flow Area	2.19	ft <sup>2</sup>
Wetted Perimeter	3.78	ft
Hydraulic Radius	0.58	ft
Top Width	1.90	ft
Critical Depth	1.75	ft
Percent Full	65.6	%
Critical Slope	0.01065	ft/ft
Velocity	11.22	ft/s
Velocity Head	1.96	ft
Specific Energy	3.27	ft
Froude Number	1.84	
Maximum Discharge	34.41	ft <sup>3</sup> /s
Discharge Full	31.99	ft <sup>3</sup> /s
Slope Full	0.01176	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	65.63	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain K Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	1.50	ft
Discharge	3.00	ft <sup>3</sup> /s

### Results

Normal Depth	0.46	ft
Flow Area	0.46	ft <sup>2</sup>
Wetted Perimeter	1.75	ft
Hydraulic Radius	0.26	ft
Top Width	1.38	ft
Critical Depth	0.66	ft
Percent Full	30.5	%
Critical Slope	0.00513	ft/ft
Velocity	6.58	ft/s
Velocity Head	0.67	ft
Specific Energy	1.13	ft
Froude Number	2.02	
Maximum Discharge	15.98	ft <sup>3</sup> /s
Discharge Full	14.85	ft <sup>3</sup> /s
Slope Full	0.00082	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	30.48	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain L Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	3.00	ft
Discharge	63.22	ft <sup>3</sup> /s

### Results

Normal Depth	1.80	ft
Flow Area	4.42	ft <sup>2</sup>
Wetted Perimeter	5.31	ft
Hydraulic Radius	0.83	ft
Top Width	2.94	ft
Critical Depth	2.56	ft
Percent Full	59.9	%
Critical Slope	0.00843	ft/ft
Velocity	14.30	ft/s
Velocity Head	3.18	ft
Specific Energy	4.98	ft
Froude Number	2.06	
Maximum Discharge	101.46	ft <sup>3</sup> /s
Discharge Full	94.32	ft <sup>3</sup> /s
Slope Full	0.00899	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	59.91	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain M Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	1.50	ft
Discharge	6.18	ft <sup>3</sup> /s

### Results

Normal Depth	0.67	ft
Flow Area	0.77	ft <sup>2</sup>
Wetted Perimeter	2.21	ft
Hydraulic Radius	0.35	ft
Top Width	1.49	ft
Critical Depth	0.96	ft
Percent Full	45.0	%
Critical Slope	0.00631	ft/ft
Velocity	8.02	ft/s
Velocity Head	1.00	ft
Specific Energy	1.67	ft
Froude Number	1.97	
Maximum Discharge	15.98	ft <sup>3</sup> /s
Discharge Full	14.85	ft <sup>3</sup> /s
Slope Full	0.00346	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	44.98	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain N Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	3.00	ft
Discharge	69.48	ft <sup>3</sup> /s

### Results

Normal Depth	1.91	ft
Flow Area	4.76	ft <sup>2</sup>
Wetted Perimeter	5.55	ft
Hydraulic Radius	0.86	ft
Top Width	2.88	ft
Critical Depth	2.65	ft
Percent Full	63.8	%
Critical Slope	0.00972	ft/ft
Velocity	14.59	ft/s
Velocity Head	3.31	ft
Specific Energy	5.22	ft
Froude Number	2.00	
Maximum Discharge	101.46	ft <sup>3</sup> /s
Discharge Full	94.32	ft <sup>3</sup> /s
Slope Full	0.01085	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	63.82	%
Downstream Velocity	Infinity	ft/s



## Worksheet for Storm Drain P Capacity

### Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.02000	ft/ft
Diameter	2.50	ft
Discharge	35.69	ft <sup>3</sup> /s

### Results

Normal Depth	1.42	ft
Flow Area	2.87	ft <sup>2</sup>
Wetted Perimeter	4.26	ft
Hydraulic Radius	0.67	ft
Top Width	2.48	ft
Critical Depth	2.03	ft
Percent Full	56.7	%
Critical Slope	0.00772	ft/ft
Velocity	12.42	ft/s
Velocity Head	2.40	ft
Specific Energy	3.82	ft
Froude Number	2.03	
Maximum Discharge	62.40	ft <sup>3</sup> /s
Discharge Full	58.00	ft <sup>3</sup> /s
Slope Full	0.00757	ft/ft
Flow Type	SuperCritical	

### GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

### GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	56.72	%
Downstream Velocity	Infinity	ft/s



## **APPENDIX E**

### **DRAINAGE INLET BYPASS CALCULATIONS**





TIERRA WEST, LLC

Project \_\_\_\_\_ Date \_\_\_\_\_

Project No. \_\_\_\_\_

Meeting Purpose \_\_\_\_\_ Sheet No. \_\_\_\_\_ of \_\_\_\_\_

Attendees \_\_\_\_\_

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

### Inlet Area 1:

Basins :  $P2 + P12 = 4.28 + 0.8 = 5.08$  cfs , Depth = 0.27 ft (Flowmaster)

Grate Capacity = 3 cfs (Double A, COA DPM Figure 6.9.10 for  $S=3\%$ )

\* Use Double A Inlet  $\Rightarrow$  2.08 cfs bypass

### Inlet Area 2:

Basins :  $P12(\text{bypass}) + P3 + P4 + P13 = 2.08 + 2.44 + 3.13 + 1.45 = 9.1$  cfs

Depth = 0.38 ft (Flowmaster)

Grate Capacity = 3.9 cfs (Double A/C, COA DPM Figure 6.9.10 for  $S=1\%$ )

\* Use Double A and Double C Inlet = 7.8 cfs capacity  $\Rightarrow$  1.3 cfs bypass

Inlet Spacing = 20.5 ft (COA DPM Figure 6.9.12 w/  $Fr=1.14$ )

### Inlet Area 3:

Basins :  $P5 + P6 + P14 = 5.52 + 0.52 + 0.69 = 6.73$  cfs , Depth = 0.25 ft

Grate Capacity = 9.73 cfs (See Double C Sump Orifice Egn. Calcs this appendix)

\* Use Double C in sump  $\Rightarrow$  No bypass

### Inlet Area 4:

Basins :  $P13(\text{bypass}) + P7 + P8 + P15 = 1.3 + 3.25 + 2.59 + 0.91 = 8.05$  cfs

Depth = 0.36 ft (Flowmaster)

Grate Capacity = 3.5 cfs (Double A/C, COA DPM Figure 6.9.10 for  $S=1.1\%$ )

\* Use Double A and Double C Inlet = 7.0 cfs capacity  $\Rightarrow$  1.05 cfs bypass

Inlet Spacing = 20.9 ft (COA DPM Figure 6.9.12 w/  $Fr=1.18$ )







TIERRA WEST, LLC

Project \_\_\_\_\_ Date \_\_\_\_\_

Project No. \_\_\_\_\_

Meeting Purpose \_\_\_\_\_ Sheet No. \_\_\_\_\_ of \_\_\_\_\_

Attendees \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

### Inlet Area 5:

Basins :  $P10 + P11 + P16 = 2.72 + 3.38 + 0.90 = 7.0 \text{ cfs}$

Depth = 0.32 ft (Flowmaster)

Grate Capacity = 3 cfs (Double A/C, COA DPM Figure 6.9.10 for  $S = 1.7\%$ )

\* Use Double A = 3 cfs  $\Rightarrow$  4 cfs bypass

### Inlet Area 6:

Basins :  $P15(\text{bypass}) + P16(\text{bypass}) + P17 = 1.05 + 4.0 + 1.13 = 6.18 \text{ cfs}$  , Depth = 0.25 ft

Grate Capacity = 9.73 cfs (See Double C Sump Orifice Eqn. calcs this appendix)

\* Use Double C  $\Rightarrow$  No bypass





## **APPENDIX F**

### **EXCERPTS FROM *MASTER DRAINAGE STUDY FOR THE UNSER/MCMAHON AREA***



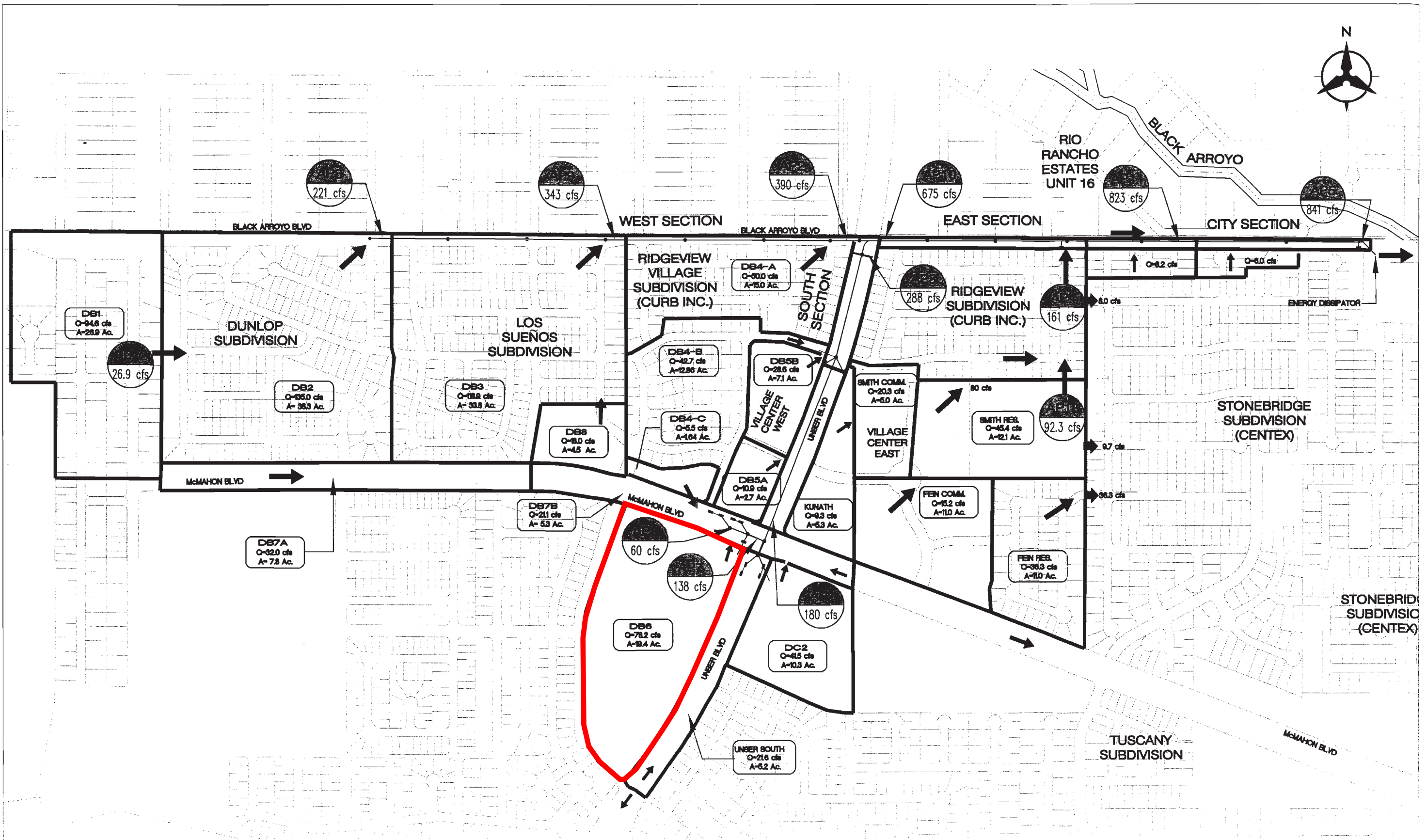
using 25% type 'B', 25% type 'C', and 50% type 'D'. The commercial tracts were restricted to historic discharge of 95% type 'A' and 5% type 'B'. The only commercial tracts allowed developed discharge in the Ridgeview report were the Village Center North Tracts because Mr. Smith paid to upsize the Ridgeview storm drain. One amendment was made to the drainage plan proposed by the Ridgeview Subdivision. The runoff from the Fein Residential property that was originally conveyed through the Ridgeview Subdivision and discharged into Black Arroyo Boulevard is now directed through the Stonebridge Subdivision. This change was made due to a subsequent analysis of the Fein property performed by Community Sciences. This analysis determined that there is sufficient capacity in the Stonebridge storm drain to accommodate the 36.3 cfs from the Fein Residential property. Therefore, the contribution from this basin was removed from the Ridgeview storm drain.

The tracts of land west of Unser or south of McMahon do not drain through the Ridgeview Subdivision. The commercial tracts in this area are permitted developed discharge and were analyzed using 90% type 'D' and 10% type 'B'. The residential tracts were analyzed using 20% type 'B', 20% type 'C', and 60% type 'D'. See **Figure 3**, the Developed Conditions Land Treatment Exhibit for an illustration of land treatment values.

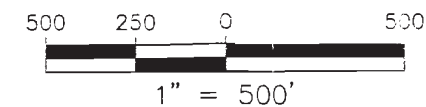
## V. PROPOSED DEVELOPED CONDITIONS

There are four major storm drain reaches included in this analysis. First, the southern reach of the analysis consists of basins that contribute flow to McMahon Boulevard and Unser Boulevard south of Black Arroyo Boulevard. Secondly, the West section of the analysis consists of the basins that contribute flow to Black Arroyo Boulevard west of Unser. Thirdly, the east portion of the analysis consists of basins that contribute flow to Black Arroyo Boulevard adjacent to the Ridgeview Subdivision. Finally, the ~~the~~ **Lower Reach** of the analysis includes the section of storm drain that conveys the flow from the other reaches east to the Lands of A.M.A.F.C.A. **At the top of the southern reach, the runoff from basins DB6 and DC2 south of McMahon combine with the street flow from McMahon Boulevard and the commercial tract DB4-C and is conveyed to the intersection of McMahon and Unser Boulevards.** The flow then combines with the Unser street flow and 180 cfs is diverted north in Unser Boulevard. Basin DB5A discharges into the Unser storm drain and is conveyed to the south boundary of the Ridgeview Subdivision. At this point, basin DB5B





**FIGURE 2**  
**DEVELOPED CONDITIONS**  
**BASIN MAP**



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 ENGINEERS PLANNERS PHOTOGRAMMETRISTS SURVEYORS SOFTWARE DEVELOPERS



## **APPENDIX G**

### **DRAINAGE CRITERIA MAP FOR FULL DEVELOPMENT**



Table 1 - Paradise North Developed Drainage Criteria

Lot No.	Designated Basin(s)	Drains to Basin...	Discharge Conveyance Method	Max Allowable Discharge Rate (cfs)
1	P1	P17	Storm Drain Connection Only	35.69
2	P2	P12	Surface Flow	4.28
3	P3	P13	Surface Flow	2.44
4	P4	P13	Surface Flow	3.13
5	P5	P14	Surface Flow	5.52
	P6	P14	Surface Flow	0.52
6	P7	P15	Surface Flow	3.25
	P8	P15	Surface Flow	2.59
7	P9	McMahon Curb Inlet	Storm Drain Connection Only	6.88
8	P10	P16	Surface Flow	2.72
9	P11	P16	Surface Flow	3.38

**LEGEND:**

- - - - - = Basin Delineation
- = Storm Drain
- = Drainage Inlet
- = Direction of Flow

Basin ID  
Area  
(Ac)

SAGITTARIUS AVE. N.W.

BANDELIER DRIVE N.W.  
PUBLIC RIGHT OF WAY

AQUARIUS AVENUE N.W.

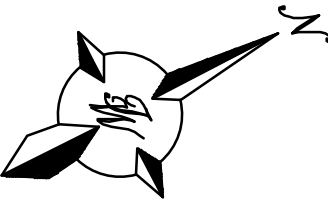
BANDELIER DRIVE N.W.  
PUBLIC RIGHT OF WAY

Ultimate Outfall from Site  
SD Connection to McMahon Main

MCMAHON BOULEVARD N.W.  
12' PUBLIC RIGHT OF WAY

Outfall from Lot 7/P9  
SD Connection to Ex. McMahon Curb Inlet

UNSER BOULEVARD N.W.  
156' PUBLIC RIGHT OF WAY



# DEVELOPED DRAINAGE CRITERA

