

**WESTSIDE BLVD./NM528
INTERSECTION IMPROVEMENTS
DRAINAGE REPORT**

MARCH 1995

**WESTSIDE BLVD./NM528
INTERSECTION IMPROVEMENTS
DRAINAGE REPORT**

Prepared for:

**INTEL CORPORATION
BROWN/Z & ASSOCIATES
AMREP CORPORATION
DON CHALMERS FORD**

TABLE OF CONTENTS

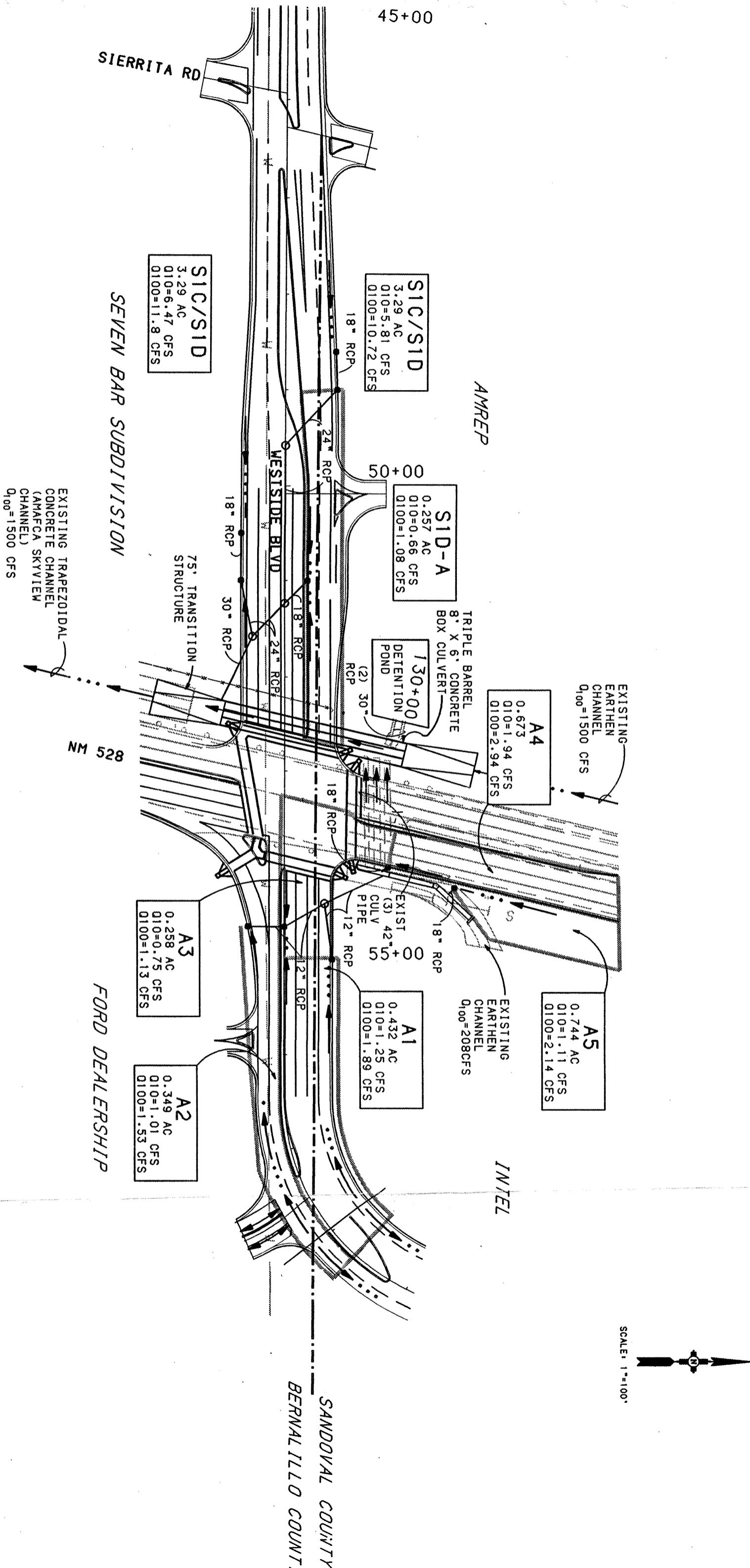
	PAGE
I. INTRODUCTION	1
II. EXISTING CONDITIONS	1
III. PROPOSED CONDITIONS	3
IV. BOX CULVERTS	4
A. NM 528 West Right-of-Way Structure	4
B. NM 528 East Right-of-Way/Intel Outlet Structure	5
V. CONCLUSION	6

FIGURES

FIGURE 1 - DRAINAGE MAP	2
-------------------------------	---

TABLES

TABLE 1 - SUMMARY	5
-------------------------	---



- **Northwest:** existing and proposed runoff discharges south and intercepted by a detention basin located south of the property and discharge into the AMAFCA channel by 2-30" R.C.P.s.
- **Southwest:** existing and proposed runoff will continue to flow in a southerly direction as outlined in the Drainage Master Plan Seven Bar North Subdivision. This drainage plan was submitted for review by the City of Albuquerque in June 1994.

Runoff within the 200' right-of-way of NM 528 flows east and west of the roadway. The flow on the west is intercepted by the AMAFCA channel. The flow on the east is intercepted by the roadway ditch east of NM 528 and eventually discharges to the Cabezon Channel.

III. PROPOSED CONDITIONS

Offsite flows will not enter the proposed Westside Blvd. The only runoff conveyed by Westside Blvd. will be what is generated within the street. Flowrates east of the intersection were calculated using the City of Albuquerque Design Process Manual (DPM) criteria. The area generating runoff to the roadway consists of the roadway section and adjacent sidewalk areas. Flowrates west of the intersection were taken from the DRAINAGE Master Plan Seven Bar North Subdivision study. Basins S1C and S1D are the basins that flow toward the intersection. Figure 2 shows the typical street section and maximum street capacity of $Q=18.2$ cfs. Figures 3 and 4 show the street section with depths of flow, flowrates, water widths, and open lanes for the 10 year and 100 year storm (see back of report for figures). The street hydraulics was determined by using manning's equation. Inlets were placed at the low points of the proposed vertical alignment and before intersections. The City of Albuquerque grate capacity charts was used to determine the flow intercepted by each inlet that were on a continuous grade. Inlets that are in a sump condition were analyzed using the Drainage of Highway Pavements Manual Section 8. Weir and orifice equations were used to calculate the depth of water for both conditions. The condition requiring the higher depth of water over each inlet to pass the design flow was selected. The width of the water and the number of lanes opened were

determined (see the appendix for calculations and nomographs). All inlets were designed to intercept the 100-year storm. A minimum of one lane open, both directions, is provided for the 10-year storm. Table 1, page 5, is a summary of the inlet locations and other data. The proposed storm drain will be 18" to 30" R.C.P. pipes. The storm drain is designed for the 100-year storm and will discharge into the Skyview Channel crossing structure.

IV. BOX CULVERTS

A. NM 528 West Right-of-Way Structure - The existing AMAFCA Skyview Channel is located west and within the NM 528 right-of-way and is concrete lined south of the county line. This facility is an earthen channel north of the Sandoval county line. The channels cross section consists of a 10' foot bottom with 2:1 side slopes. Meetings with Albuquerque Metropolitan Arroyo Flood Control Authority (AMAFCA) to discuss the crossing structure design resulted in an agreement to construct either a trapezoidal structure with a slab on top or a concrete box culvert crossing structure. Due to physical constraints and economical reasons a box culvert was chosen to be the best alternative. During this coordination with AMAFCA, the City of Albuquerque, and New Mexico Highway and Transportation Department (NMSH&TD) were also asked to review the design with subsequent verbal approvals. AMAFCA issued a design flowrate requirement of 1500 cfs for ultimate design of the drainage structure. A 8'X6' triple concrete box culvert with 75' transition structures on both ends was selected. The end transitions tie the box culvert section to a trapezoidal section. See the appendix at the end of the report for the structure profile, flow data, and HEC-2 hydraulic run for this structure.

TABLE 1 - SUMMARY

East Leg

Sta	Q100	Q10	Intercepted Q100	PassBy Q100	Inlet Size	Intersection Condition
55+00 LT	1.89	1.25	1.89	0	Single A	Passby
54+65 @ CL	1.13+.54	0.75	---	---	Modified Single D	Passby
54+65 RT	1.53	1.01	1.53	0	Single A	Sump

NM528

130+03 Rt	2.94	1.94	2.4	0.54 to 54+65 @ CL	Single A	Passby
130+88 Rt	2.14	1.11	---	---	Double D	Sump

West Leg

51+00 Lt	1.08	0.66	---	---	Modified Double D	Sump
50+50 Rt	5.9	3.24	---	---	Single A	Sump
51+00 Rt	5.9	3.24	---	---	Single C	Sump
48+60 Lt	10.72	5.81	6.2	4.52	Single A	Passby
49+00 Lt	4.52	---	4.52	0	Double C	Passby

B. NM 528 East Right-of-Way/Intel Outlet Structure - The existing structure consists of a concrete trapezoidal channel with a 10' bottom and 2:1 side slopes. This channel is located on the northeast corner of the proposed intersection. This structure carries Intel's runoff (Q100=208 cfs) and discharges west to Skyview Channel via 3-42" CMPs. The existing guardrail will be removed with the proposed improvements to the intersection. To safely

isolate the channel, new installation of a guardrail, or a concrete wall barrier will be needed. In considering the type of end treatment required for either the guardrail or the wall barrier, it was decided it would be more economical to enclose the existing drainage system underground and eliminate the hazard and the need for guardrail. The discharge portion of the channel will be replaced with a 7' X 5' concrete box culvert to connect the existing 42" pipes that route flows west under NM 528. The proposed storm drain system will drain the east leg of the intersection. The design will also compliment the design of wheelchair ramps and traffic signals needed at this location. An 87" Span X 63" Rise corrugated metal pipe culvert arch will connect to the 7' X 5' concrete box culvert and a proposed head wall at the end of the existing concrete lined channel and beginning of the earthen channel that conveys Intel's site discharge to NM 528. See the appendix at the end of the report for the structure profile, flowrate, and hydraulic run for this structure.

V. CONCLUSION

Since existing runoff flow is generally in a southerly direction, the two areas that will discharge runoff into Westside Blvd. are AMREP development and the Intel site. AMREP is utilizing detention ponds and discharging into the Skyview Channel via 2-30" RCP pipes at the NW corner of the intersection and Intel is discharging into an existing channel located at the NE corner of the intersection. Drainage reports for these areas indicate that future runoff will be discharged in the same manner that it exists today. Therefore, no offsite flows will be discharged to Westside Blvd. and it will carry only the runoff generated within the roadway. Storm drain inlets and pipe will be utilized to convey onsite runoff and discharged into the Skyview Channel or the proposed 7'X5' concrete box culvert at the NE corner. The proposed improvements will provide adequate drainage for the roadway and adjacent drainage facilities.

I. INTRODUCTION

Westside Blvd. is a new at-grade signalized intersection with NM 528 at the Bernalillo/Sandoval county line. The new intersection will consist of curb & gutter, paving, traffic signals & lighting, drainage, and waterline improvements. These improvements will extend approximately 700 feet from NM 528 to the west and 500 feet to the east (see Figure 1, page 2). The proposed improvements on NM 528 consist of an additional northbound lane with curb and gutter. This lane will tie the improvements of the SAD 223 project on the south; to the right turn lane drop at the Intel entrance at the NM 528, and 21st street intersection on the north. Median improvements include curb and gutter to create the left turn bays and some new striping. A 18" waterline on Westside will connect to an existing 12" waterline east of NM 528 and terminate immediately west of Sierrita Road.

II. EXISTING CONDITIONS

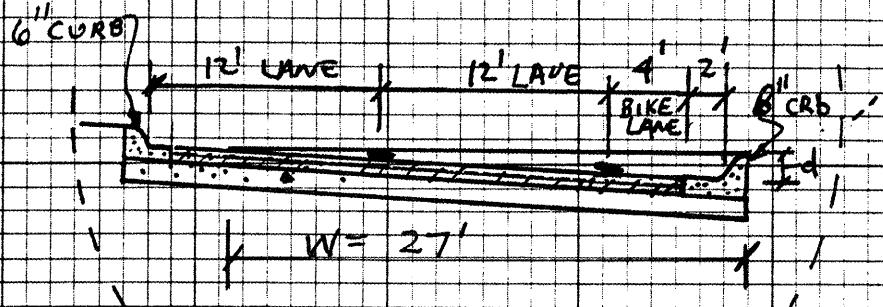
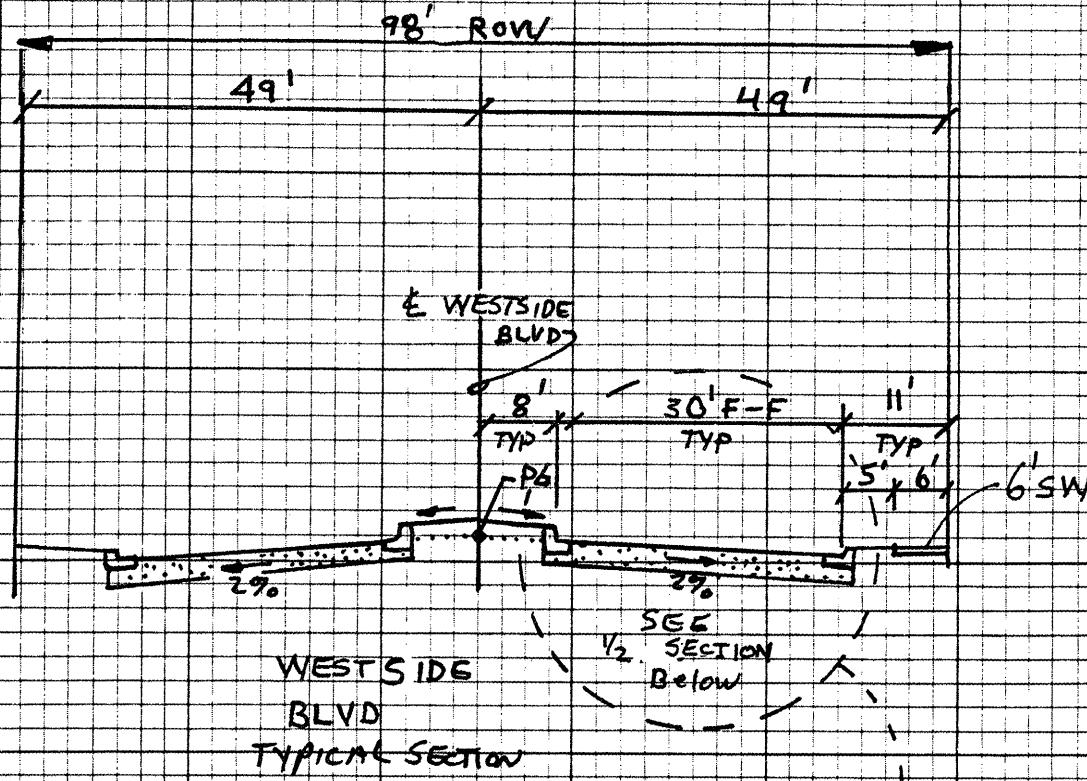
Three private developments and the Intel site bound the intersection. East of the intersection it is bounded by Intel on the north and a new Ford dealership on the south, both of which lie within the City of Rio Rancho. The west leg of the intersection consists of the AMREP Corporation development on the north and the Brown-Z development, Seven Bar North Subdivision on the south. The AMREP development lies within Sandoval County and the Seven Bar North Subdivision development is within Bernalillo County and the City of Albuquerque. The following is a summary on how each quadrant of the roadway currently handles its runoff:

- **Northeast:** Intel detains its runoff and discharges into an existing channel at a rate of $Q_{100}=208$ cfs. The channel is located NE of the intersection which discharges through (3) 42" CMPs to the Albuquerque Metropolitan Arroyo Flood Control Authority (AMAFCA) channel west of NM 528. The flowrate is based from the Drainage Restudy for Intel Plant prepared by Bohannan-Huston, Inc. in August 1995.
- **Southeast:** existing runoff discharges south into the existing ditch located east of NM 528.

FIGURE 1 - DRAINAGE MAP

APPENDIX

FIGURE 2
STREET CAPACITY



STREET GRADE = 0.5%

CROSS SLOPE = 2.0% \downarrow $\frac{1}{2}$ SECTION \downarrow

DESIGN STORM : CAPACITY

FLOW RATE $Q = 18.2 \text{ CFS}$

VELOCITY $V = 2.5 \text{ FPS}$

MOMENTUM FACTOR = $MF = V \times d = \frac{1.7}{12}$

LANES OPEN = 0.25 EA

DEPTH; $d = 8" \text{ inch}$

WATER WIDTH $W = 27 \text{ FT}$

SP/SEC < 6.5 OK

N/R = NOT
REQ'D.



BOHANNAN-HUSTON INC.

PROJECT NAME WEST SIDE BLVD.

SHEET _____ OF _____

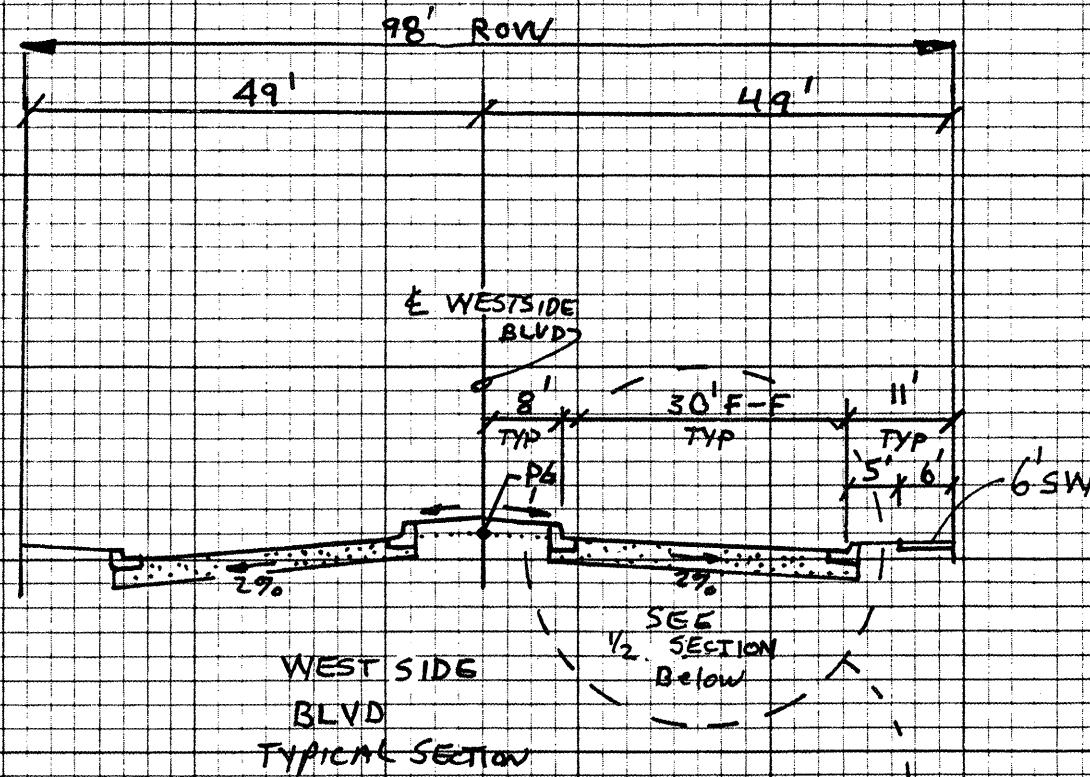
PROJECT NO. 95343A1 2222

BY TG DATE 2/7/96

SUBJECT STREET CAPACITY

CH'D _____ DATE _____

FIGURE 3
10 YEAR



STREET GRADE = 0.5%

CROSS SLOPE = 2.0%

DESIGN STORM : 10 YR

FLOW RATE $Q = 3.9 \text{ CFS}$

VELOCITY $V = 1.7 \text{ FPS}$

MOMENTUM FACTOR = $MF = V \times d = 0.72 \text{ SF/SEC} < 6.5 \text{ OK}$

* INCLUDES 1 1/2" GUTTER PAN DROPS

R = REQ'D.



BOHANNAN-HUSTON INC.

PROJECT NAME WEST SIDE BLVD.

SHEET OF

PROJECT NO. 95343A1 2222

BY TG DATE 2/7/96

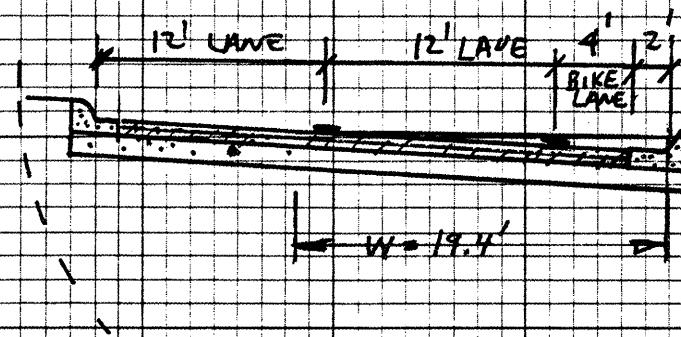
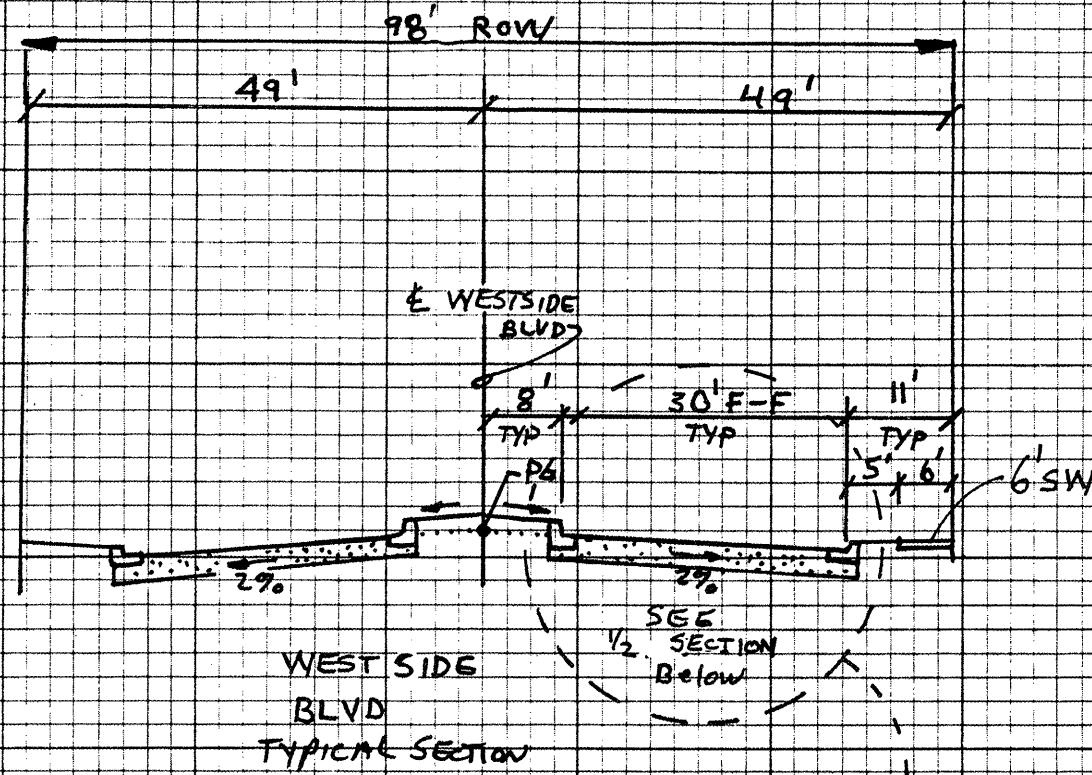
SUBJECT STREET CAPACITY

CH'D DATE

COMMENT

R

FIGURE 4 100 YEAR



LIN = 20.75'

STREET GRADE = 0.5%

CROSS SLOPE = 2.0%

DESIGN STORM : 100 YR

FLOW RATE Q = 7.6 CFS

VELOCITY V = 2.0 FPS

MOMENTUM FACTOR = MF = $V \times \frac{1}{12}$ = 1.0

LANES OPEN 0.88 EA

DEPTH, d = 6.18 inch *

WATER WIDTH W = 19.4 FT

N/R = NOT REQUIRED

* Includes 1 1/2" GUTTER PAN DROP



BOHANNAN-HUSTON INC.

PROJECT NAME WEST SIDE BLVD.

SHEET _____ OF _____

PROJECT NO. 95343A1 2222

BY TG DATE 2/7/96

SUBJECT STREET CAPACITY

CH'D _____ DATE _____

HEC2 S/N: 1363001424

HMVersion: 6.52 Data File: west.hec

```
*****  
* HEC-2 WATER SURFACE PROFILES *  
* Version 4.6.2; May 1991 *  
* RUN DATE 28FEB96 TIME 7:42:16 *  
*****
```

```
*****  
* U.S. ARMY CORPS OF ENGINEERS *  
* HYDROLOGIC ENGINEERING CENTER *  
* 609 SECOND STREET, SUITE D *  
* DAVIS, CALIFORNIA 95616-4687 *  
* (916) 756-1104 *  
*****
```

X	X	XXXXXX	XXXXX	X	XXXXXX	X
X	X	X	X	X	X	X
X	X	X	X	X	X	X
XXXXXX	XXXXX	X	XXXXXX	X	XXXXXX	X
X	X	X	X	X	X	X
X	X	X	X	X	X	X
X	X	XXXXXX	XXXXX	X	XXXXXX	X

```
:::::::::::  
:::::::::::  
::: :::  
::: : FULL MICRO-COMPUTER IMPLEMENTATION :::  
::: :::  
:::::::::::  
:::::::::::
```

HAESTAD METHODS

37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

Run Date: 28FEB96 Run Time: 7:42:17 HVersion: 6.52 Data File: west.hec

Page 1

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

THIS RUN EXECUTED 28FEB96 7:42:17

T1 528 Channel and Box Under Westside Blvd.

Second Label

T3 SUPERCRITICAL RUN

J1 ICHECK INQ MNW IDIR SIRT METRIC HVINS Q WSEL FQ

2. 1. 0 5211.55

J2 NPROF IPLOT PREVS XSECV XSECN ALLOC IBM CHNM TTRACE

-1. 0 -1. -1.

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38. 42. 4. 26. 1. 2. 8. 14. 33.

J5 LFRNT NMSEC ***** REQUESTED SECTION NUMBERS*****

-10 -10

QT	1.0	1500	.025	.1	.3	0.0	0.0	5212.55	536.0
NC	.025	.025	500.00	536.0	0.00	0.0	0.0		
XI	0.0	4.0	5205.55	510.5	5205.55	525.5			
GR	5212.5	500.0							
XI	10.0	4.0	500.00	536.4	10.00	10.0	10.0		
GR	5212.5	500.0	5205.51	511.2	5205.51	525.2	5212.51	536.4	
XI	20.0	4.0	500.00	536.8	10.00	10.0	10.0		
GR	5212.5	500.0	5205.46	511.9	5205.46	524.9	5212.46	536.8	
XI	30.0	4.0	500.00	537.2	10.00	10.0	10.0		
GR	5212.4	500.0	5205.42	512.6	5205.42	524.6	5212.42	537.2	
XI	40.0	4.0	500.00	537.6	10.00	10.0	10.0		
GR	5212.4	500.0	5205.37	513.3	5205.37	524.3	5212.37	537.6	
NC	.015	.015	.015	.1	.3				
XI	50.0	4.0	500.00	538.0	10.00	10.0	10.0		
GR	5212.3	500.0	5205.33	514.0	5205.33	524.0	5212.33	538.0	

Run Date:	Run Time:	HMVersion: 6.52	Data File:	west.hec	Page
	28FEB96				2
XI CR CR	60.0 5212.1 5212.1	6.0 500.0 536.4	500.00 5211.17	536.4 500.0	10.00 5205.10
XI CR CR	70.0 5211.9 5211.9	6.0 500.0 534.8	500.00 5210.01	534.8 500.0	10.00 5204.88
XI CR CR	80.0 5211.6 5211.6	6.0 500.0 533.2	500.00 5208.85	533.2 500.0	10.00 5204.65
XI CR CR	90.0 5211.4 5211.4	6.0 500.0 531.6	500.00 5207.69	531.6 500.0	10.00 5204.42
XI CR CR	100.0 5211.2 5211.2	6.0 500.0 530.0	500.00 5206.53	530.0 500.0	10.00 5204.20
XI CR CR	110.0 5211.0 5211.0	6.0 500.0 528.4	500.00 5205.37	528.4 500.0	10.00 5203.97
XI CR CR	120.0 5210.7 5210.7	6.0 500.0 526.8	500.00 5204.21	526.8 500.0	10.00 5203.74
XI CR CR CR	125.0 5210.6 5203.6 5203.6	12.0 500.0 509.0 526.0	500.00 5203.63 5203.63 5210.63	526.0 500.0 517.0 526.0	5.00 5203.63 508.0 517.00
XI CR CR CR	316.0 5210.6 5203.6 5202.6	12.0 500.0 509.0 526.0	500.00 5202.55 5202.55 5209.55	526.0 500.0 517.0 526.0	191.00 5202.55 508.0 517.00
XI CR CR	320.0 5209.5 5209.5	6.0 500.0 526.6	500.00 5202.89	526.6 500.0	4.00 5202.51
XI CR CR	330.0 5209.4 5209.4	6.0 500.0 528.2	500.00 5203.73	528.2 500.0	10.00 5202.42
XI CR CR	340.0 5209.3 5209.3	6.0 500.0 529.8	500.00 5204.57	529.8 500.0	10.00 5202.33

Run Date:	28FEB96	Run Time:	7:42:17	HMSVersion:	6.52	Data File:	west.hec	Page	3
-----------	---------	-----------	---------	-------------	------	------------	----------	------	---

XI	350.0	6.0	500.00	531.4	10.00	10.0	525.1	5205.41	531.4
GR	5209.2	500.0	5205.41	500.0	5202.23	506.3	5202.23		
GR	5209.2	531.4							
XI	360.0	6.0	500.00	533.0	10.00	10.0	5202.14	524.8	5206.25
GR	5209.1	500.0	5206.25	500.0	5202.14	508.2	5202.14		
GR	5209.1	533.0							
XI	370.0	6.0	500.00	534.6	10.00	10.0	5202.05	524.6	5207.09
GR	5209.0	500.0	5207.09	500.0	5202.05	510.1	5202.05		
GR	5209.0	534.6							
XI	380.0	6.0	500.00	536.2	10.00	10.0	5201.95	524.3	5207.93
GR	5209.0	500.0	5207.93	500.0	5201.95	511.9	5201.95		
GR	5209.0	536.2							
XI	390.0	6.0	500.00	537.8	10.00	10.0	5201.86	524.0	5208.77
GR	5208.9	500.0	5208.77	500.0	5201.86	513.8	5201.86		
GR	5208.9	537.8							
XI	391.0	4.0	500.00	538.0	1.00	1.0	5201.85	5208.85	538.0
GR	5208.9	500.0	5201.85	514.0	5201.85	524.0	5201.85		

Run Date: 28FEB96 Run Time: 7:42:17 HMVersion: 6.52 Data File: west.hec

Page 4

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

THIS RUN EXECUTED 28FEB96 7:42:19

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

SUPERCRITICAL RUN

SUMMARY PRINTOUT

SECNO	ELMIN	TOFWID	VCH	CWSEL	CRWS	DEPTH	QCH	K*CHSL
*	0.000	5205.55	31.73	11.56	5211.10	5.56	1500.00	0.00
*	10.000	5205.51	32.17	11.45	5211.19	5.68	1500.00	-40.04
*	20.000	5205.46	32.56	11.41	5211.23	5.77	1500.00	-4.98
*	30.000	5205.42	33.13	11.35	5211.28	5.86	1500.00	-4.00
*	40.000	5205.37	33.60	11.29	5211.33	5.96	1500.00	-4.98
*	50.000	5205.33	34.23	11.22	5211.37	6.04	1500.00	-4.00
*	60.000	5205.10	31.08	14.64	5209.83	4.73	1500.00	-23.00
*	70.000	5204.88	30.84	16.08	5209.02	4.14	1500.00	-22.02
*	80.000	5204.65	31.10	17.18	5208.32	3.67	1500.00	-23.00
*	90.000	5204.42	31.60	18.02	5207.73	5209.68	3.31	1500.00
*	100.000	5204.20	30.00	18.63	5207.25	5208.82	3.05	1500.00
*	110.000	5203.97	28.40	19.02	5206.88	5208.53	2.91	1500.00
*	120.000	5203.74	26.80	19.17	5206.68	5208.34	2.94	1500.00
*	125.000	5203.60	24.00	17.66	5207.16	5208.55	3.56	1500.00
*	316.000	5202.55	24.00	19.45	5205.95	5207.68	3.40	1500.00
*	320.000	5202.51	26.60	13.45	5206.72	5207.12	4.21	1500.00
*	330.000	5202.42	28.20	14.48	5206.21	5206.97	3.79	1500.00

Trans. +
Err. of Box

-22.46 -23.00 -23.00 -23.00 -23.00 -23.00 -23.00 -23.00 -23.00

Run Date: 28FEB96 Run Time: 7:42:17 HMVersion: 6.52 Data File: west.hec
 SECNO ELMIN TOEWID VCH CMSEL CRIMS DEPTH QCH K*CHSL
 340.000 5202.33 29.80 14.56 5205.12 5206.93 3.79 1500.00 -8.98
 350.000 5202.23 31.40 13.50 5206.40 5206.98 4.17 1500.00 -10.01
 * 360.000 5202.14 33.00 12.74 5206.73 5207.14 4.59 1500.00 -8.98
 * 370.000 5202.05 34.60 11.20 5207.39 5207.39 5.34 1500.00 -9.03
 * 380.000 5201.95 34.97 11.17 5207.62 5207.62 5.67 1500.00 -9.96
 * 390.000 5201.86 34.14 11.29 5207.85 5207.85 5.99 1500.00 -9.03
 * 391.000 5201.85 34.09 11.26 5207.89 5207.89 6.04 1500.00 -0.98 -

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION SECNO= 0.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 10.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 10.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 10.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

CAUTION SECNO= 20.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 20.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 20.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

CAUTION SECNO= 30.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 30.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 30.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

CAUTION SECNO= 40.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 40.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 40.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

CAUTION SECNO= 50.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 50.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 50.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

WARNING SECNO= 60.000 PROFILE= 1 CONVEYANCE CHANGE OUTSIDE ACCEPTABLE RANGE
CAUTION SECNO= 320.000 PROFILE= 1 CONVEYANCE CHANGE OUTSIDE ACCEPTABLE RANGE

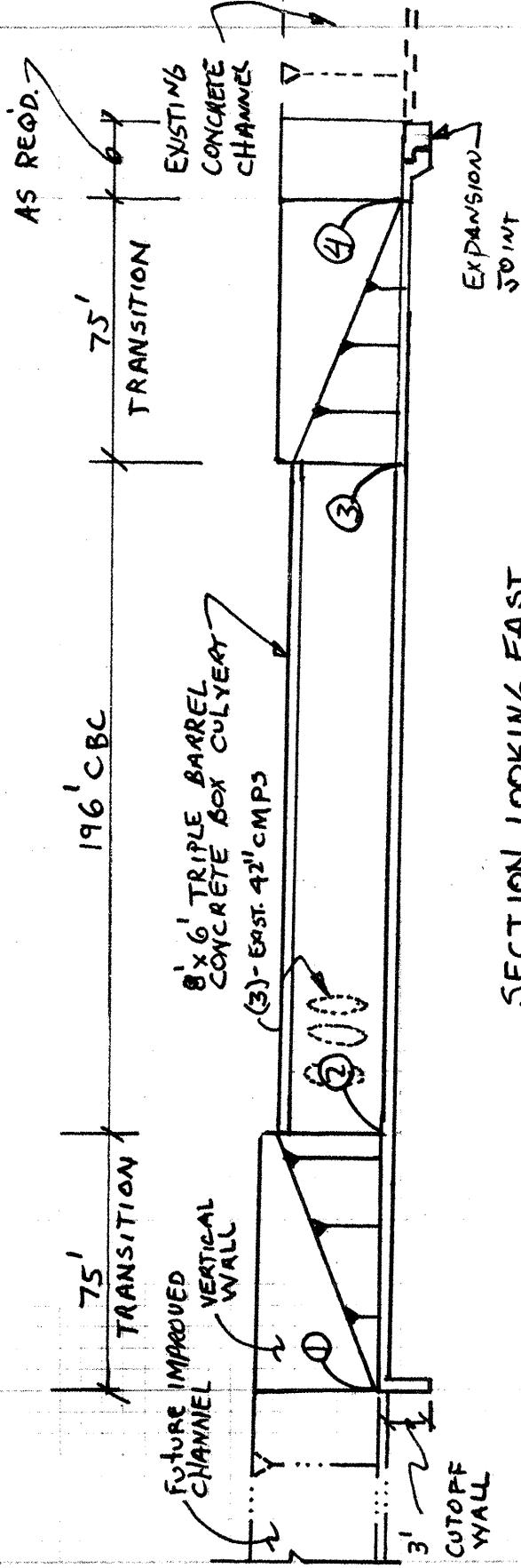
CAUTION SECNO= 360.000 PROFILE= 1 WSEL ASSUMED BASED ON MIN DIFF
CAUTION SECNO= 360.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

CAUTION SECNO= 370.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 370.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 370.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

CAUTION SECNO= 380.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 380.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 380.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

CAUTION SECNO= 390.000 PROFILE= 1 CRITICAL DEPTH ASSUMED
CAUTION SECNO= 390.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 390.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL

CAUTION SECNO= 391.000 PROFILE= 1 CRITICAL DEPH ASSUMED
CAUTION SECNO= 391.000 PROFILE= 1 PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION SECNO= 391.000 PROFILE= 1 20 TRIALS ATTEMPTED TO BALANCE WSEL



SECTION LOOKING EAST

N.T.S.

$$\begin{aligned}
 Q_{100} &= 1500 \text{ cfs} \\
 D &= 6.04' \\
 V &= 11.22 \text{ ft/s} \\
 Y &= 17.466 \\
 HGL \textcircled{2} &= 5207.16 \\
 HGL \textcircled{3} &= 5205.95 \\
 Q_{100} &= 1500 \text{ cfs} \\
 D &= 6.04' \\
 V &= 11.24 \text{ ft/s} \\
 Y &= 17.466 \\
 HGL \textcircled{1} &= 5207.89
 \end{aligned}$$

Point	Inv.	of WS
①	5205.33	6.04 5211.37
②	5203.63	3.56 5207.16
③	5202.55	3.4 5205.95
④	5201.82	6.04 5207.89



BOHANNAN-HUSTON INC.

CONCRETE BOX CULVERT
 AT STA 52+53.23 WESTSIDE BLVD.
 13° SKEW LEFT FORWARD

WESTSIDE/NM 528 INTERSECTION

***** HYDRAULIC GRADE LINE CALCULATIONS *****

CMP Manning's n = 0.024
Concrete Manning's n = 0.013
for pipe

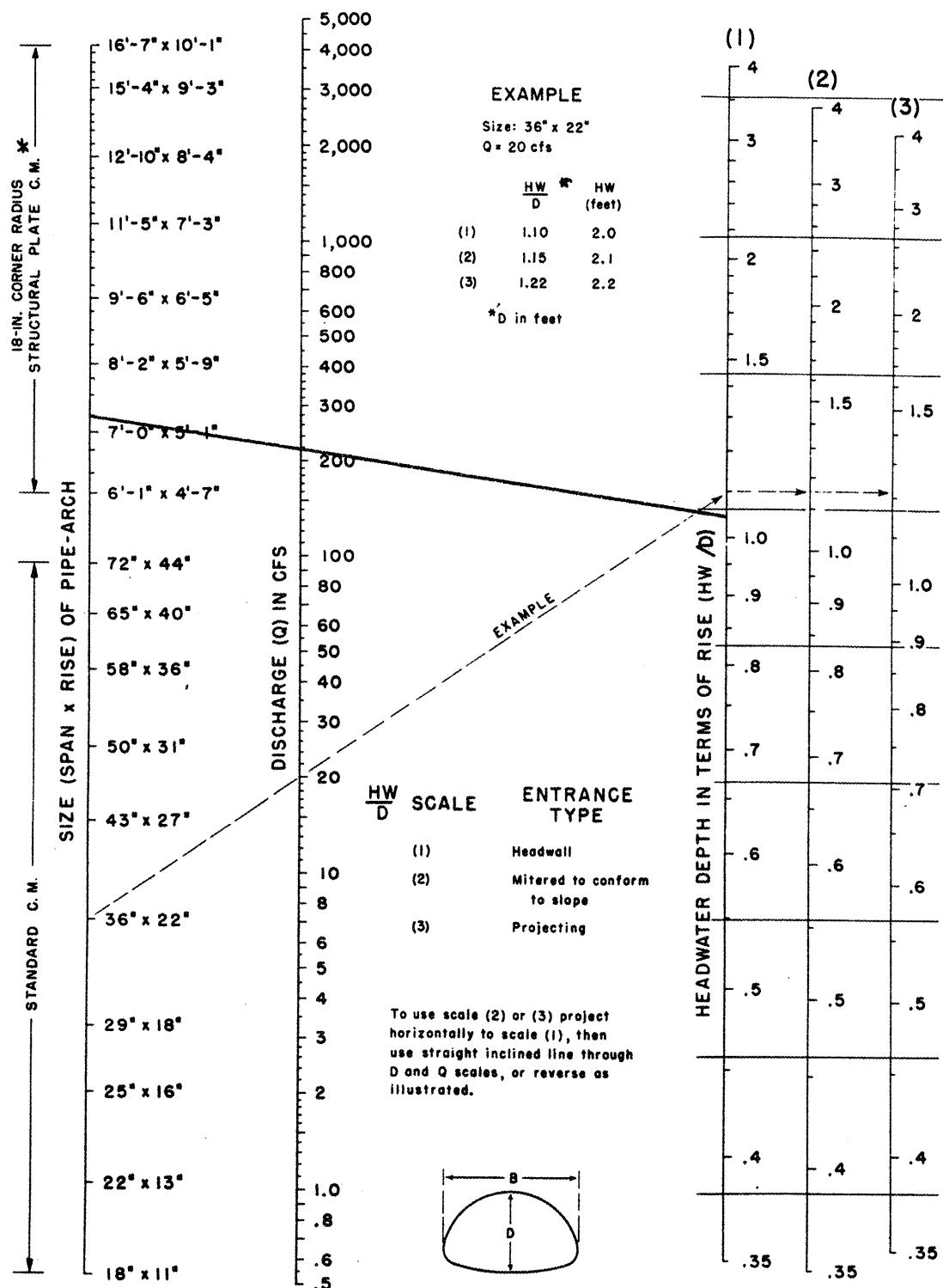
Equivalents:

5x7' CBC - 80" RCP

87"x65" CM Arch Pipe - 78" CMP

Station	Structure	Diam.	Q	Area	Vel.	K	Sf	Length	MH	JNCT Dia.	Angle	Hf	Hb	Hj	Hmh	Ht	Total Losses	HGL(dn)	HGL(up)	HV	EGL(dn)	EGL(up)
0+00	OUTFALL	42	70.0	9.62	7.28	545	0.0165	114.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	5208.87	0.82	5209.69	5209.69	
1+14	EX. INLET	80	208.0	34.91	5.96	5609	0.0014	33.60	0.00	75.00	0.05	0.12	0.00	0.00	0.00	0.13	0.05	5210.75	5211.15	0.55	5211.57	5211.70
1+74	TRANSITION	78	208.0	33.18	6.27	2840	0.0054	48.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	5211.19	5211.14	0.61	5211.75	5211.75
2+34	BEND	78	208.0	33.18	6.27	2840	0.0054	60.00	0.00	30.00	0.26	0.07	0.00	0.03	0.00	0.10	0.26	5211.39	5211.49	0.61	5212.00	5212.10
2+54	INLET								0.00	0.00	0.32	0.07	0.00	0.03	0.00	0.32	0.32	5211.82	5211.82	5212.43		
1+14	7x5' Box	18	5.2	1.77	2.94	57	0.0084	68.00	0.00	0.00	0.57	0.00	0.00	0.00	0.00	0.00	0.57	5211.15	0.13	5211.28	5211.28	
1+82	MH	18	2.1	1.77	1.19	57	0.0014	56.00	4.00	80.00	0.08	0.01	0.00	0.00	0.00	0.01	0.08	5211.72	5211.84	0.02	5211.85	5211.86
2+38	Drop Inlet																0.08	5211.92	5211.94	5211.94		
1+82	MH	18	3.1	1.77	1.75	57	0.0030	46.00	0.00	0.00	0.14	0.00	0.00	0.00	0.00	0.00	0.14	5211.84	0.05	5211.89	5211.89	
2+28	Drop Inlet	12	1.9	0.79	2.42	19	0.0097	36.00	0.00	30.00	0.35	0.01	0.00	0.00	0.00	0.01	0.35	5211.98	5211.94	0.09	5212.02	5212.03
2+64	Drop Inlet																0.35	5212.29	5212.38	5212.38		

CHART 34

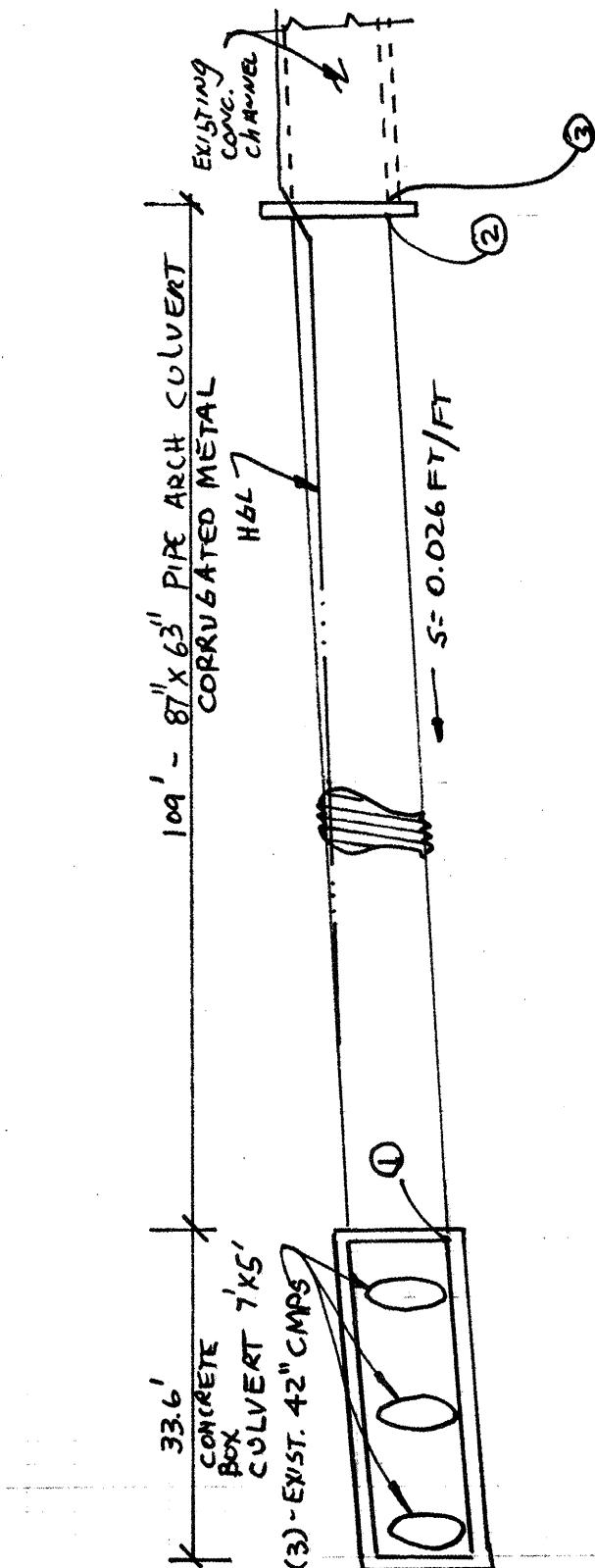


*ADDITIONAL SIZES NOT DIMENSIONED ARE
LISTED IN FABRICATOR'S CATALOG

BUREAU OF PUBLIC ROADS JAN. 1963

**HEADWATER DEPTH FOR
C. M. PIPE-ARCH CULVERTS
WITH INLET CONTROL**

$$63 \times 1.05 = 66''$$



SECTION LOOKING WEST

N.T.S.

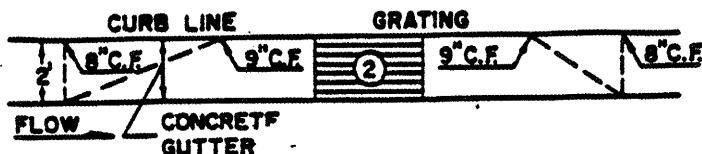
$$\begin{aligned}
 Q_{100} &= 208 \text{ CFS} & P_1 = Q_1 \text{ VARIES} & D_2 = 2.93' \\
 D &= \text{Full} & P_2 = Q_2 \text{ Full TO} & \\
 V &= 6.27 \text{ FPS} & H_{L1} &= 2.93' \\
 H_{L1} &= Q_1 = 5211.82 & &
 \end{aligned}$$

- POINT INV d HGL
- ① 5205.17 6.02 5211.19
 - ② 5208.89 2.93 5211.82
 - ③ 5208.89 5.5 5214.39

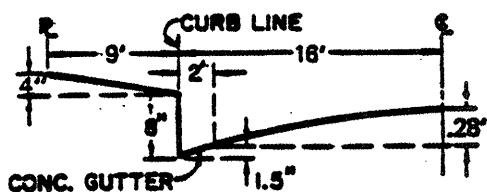
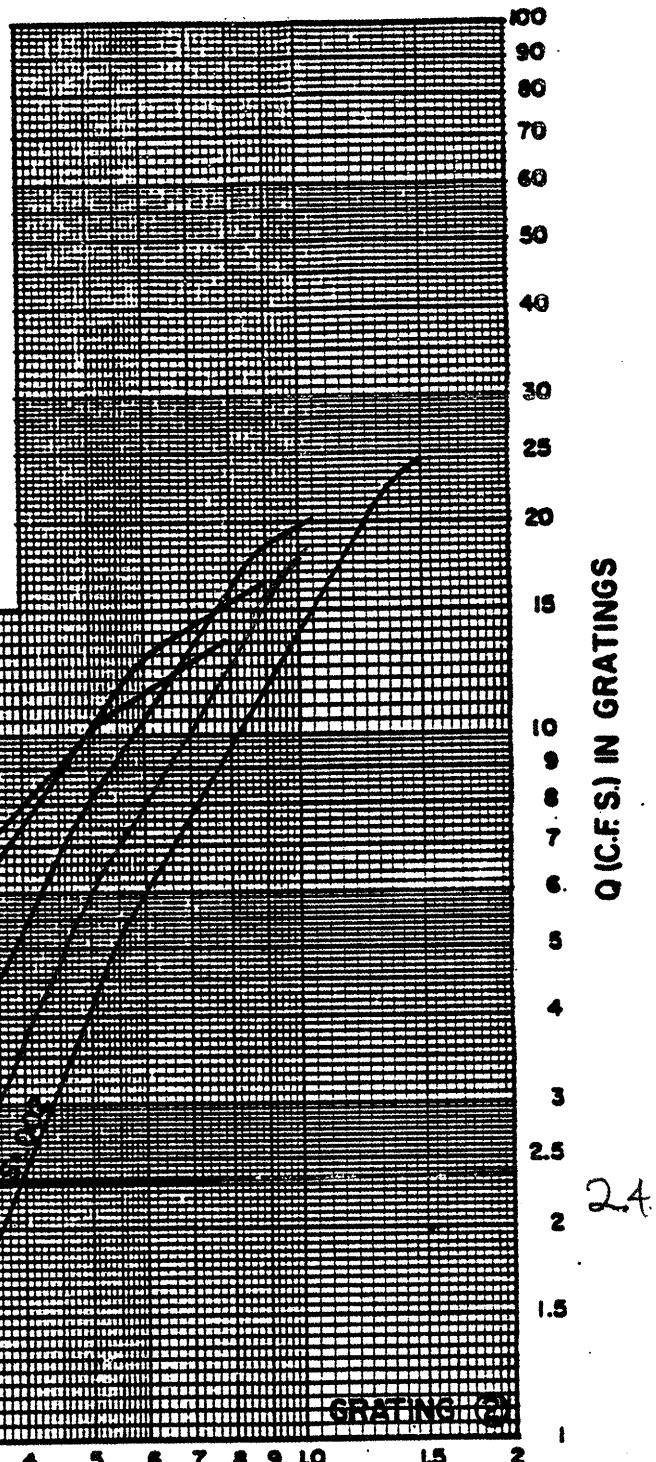
BOHANNAN-HUSTON INC.

CONCRETE BOX CULVERT & PIPE ARCH CULVERT
 STORM DRAIN @ STA 129+72.15 TO STA 131+06.83 NM528
 56.76' RT 86.37' RT

GRATING CAPACITIES FOR TYPE "A", "C" and "D"



GRATING & GUTTER PLAN

TYPICAL HALF STREET SECTION
(ABOVE BASIN)Exact loc.Inlet @ STA

55+00 ~ 50' IT

$$Q_{100} = 1.09 \text{ cfs}$$

$$Q_{10} = 1.25 \text{ cfs}$$

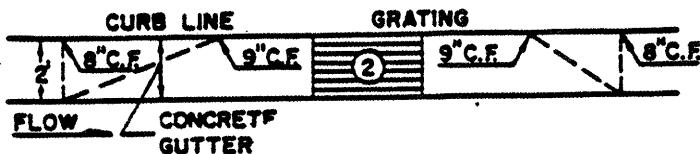
$$\times \text{slope} = 2\%$$

$$\text{Longitudinal} = 0.8\%$$

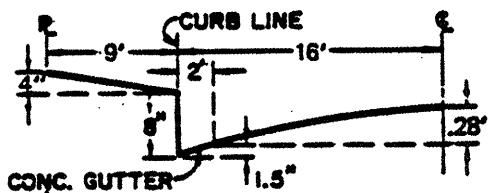
$$d = .34'$$

∴ Inlet intercepts
the whole runoff

GRATING CAPACITIES FOR TYPE "A", "C" and "D"



GRATING & GUTTER PLAN

TYPICAL HALF STREET SECTION
(ABOVE BASIN)

East leg

Inlet @

54+65 38.30' RT

$$Q_{100} = 1.53 \text{ cfs}$$

$$Q_{10} = 1.01 \text{ cfs}$$

$$\times \text{slope} = 1.62\%$$

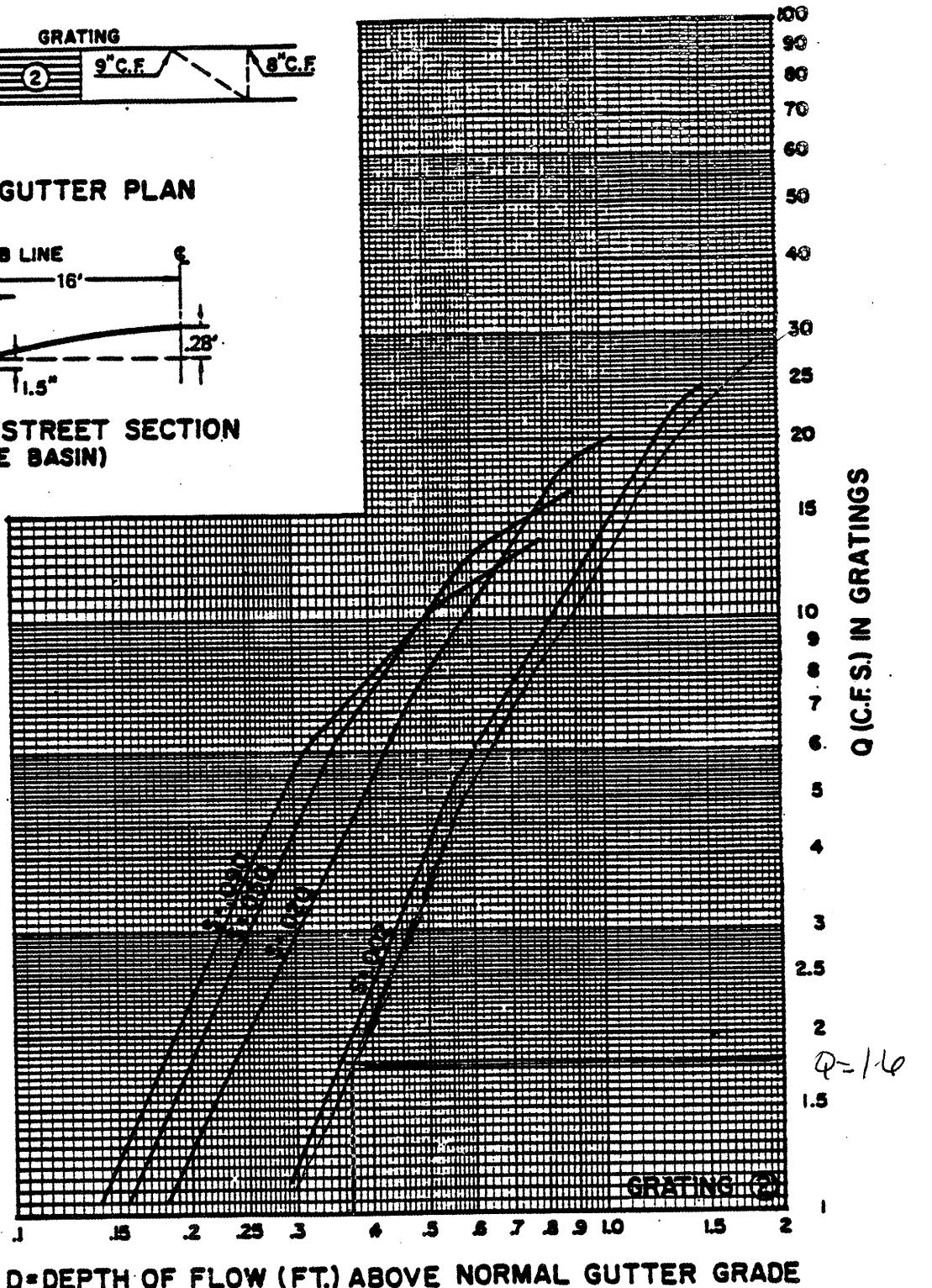
$$\text{Long} = 0.175\%$$

$$d = .37 \text{ (100yr)}$$

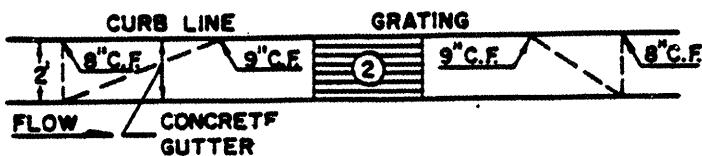
Single "A"

$$Q = 1.6 > 1.53 \text{ cfs}$$

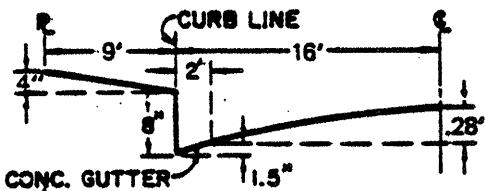
Intercept the 100 yrs



GRATING CAPACITIES FOR TYPE "A", "C" and "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)

NMS28

Inlet @
130+03 - 4619' RT

© NM 528

Type A

$$Q_{100} = 2.94 \text{ cfs}$$

$$Q_{10} = 1.94 \text{ cfs}$$

$$\times \text{Slope} = 1\%$$

$$-L_{\text{org}} = 1.2\%$$

33

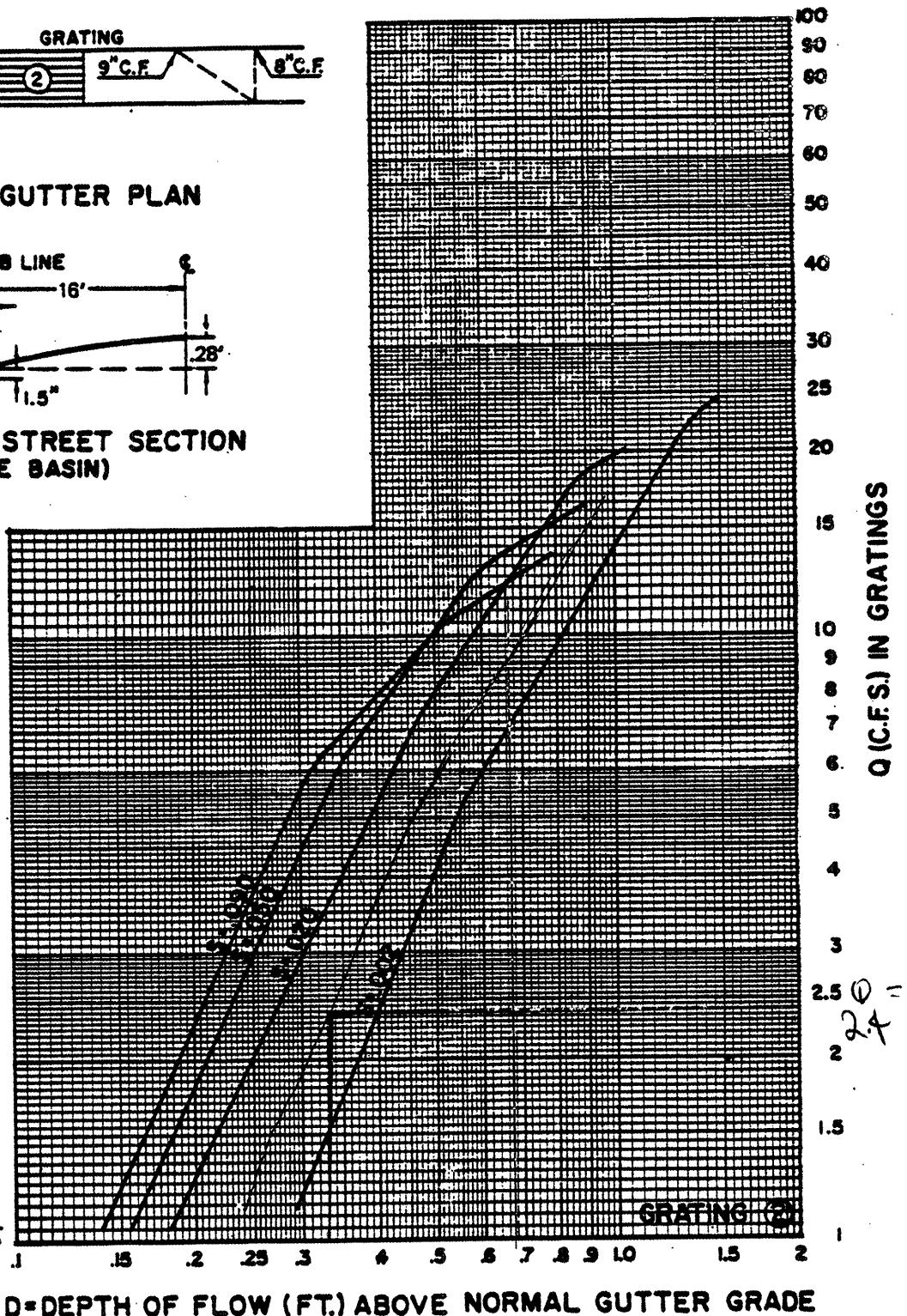
, pick all of

10.4.65

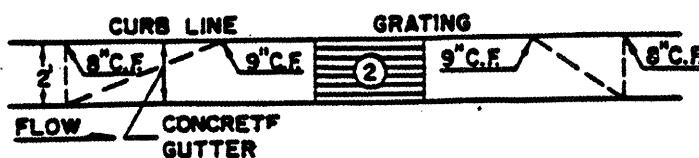
$$+ B_{\text{y}}/c = 0.54 \text{ cfs}$$

$D \in 100\text{ yr.}$

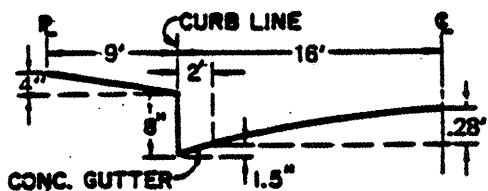
50es to Inlet
54+es @ E



GRATING CAPACITIES FOR TYPE "A", "C" and "D"



GRATING & GUTTER PLAN

TYPICAL HALF STREET SECTION
(ABOVE BASIN)Neatleg

Inlet @ 49+60 - LT
 $Q_{100} = 10.72 \text{ cfs}$

$$Q_{10} = 5.81 \text{ cfs}$$

$$\times \text{slope} = 2\%$$

$$\text{Long} = 1.7\%$$

$$d = .48$$

Single 'A' @ 49+60

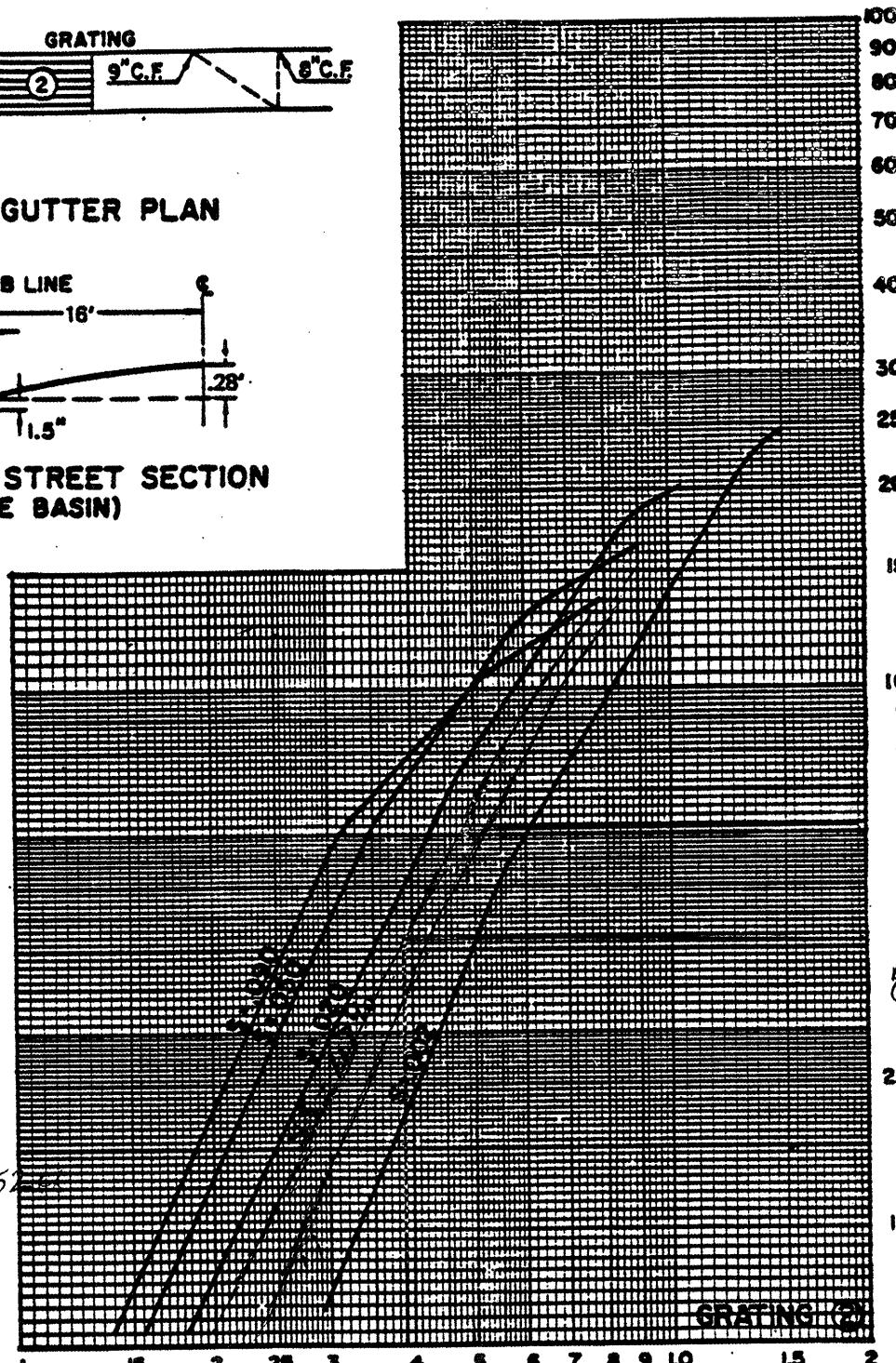
Inlet 49+00

$$Q_{100} = 10.72 - 6.2 = 4.52 \text{ cfs}$$

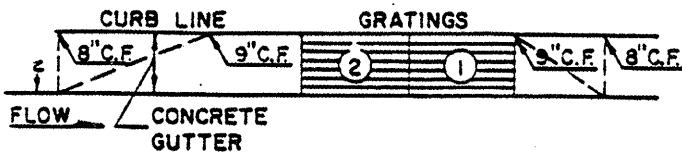
$$\times \text{slope} = 2\%$$

$$\text{Long} = 1.7\%$$

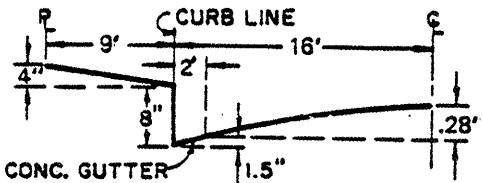
$$d = .39$$



GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



**TYPICAL HALF STREET SECTION
(ABOVE BASIN)**

Inlet @ 49±0

$$Q_{100} = 4.52$$

$$x_{slope} = 2\%$$

$$\text{Lung} = 1.7\%$$

cl- , 39

- 4B-452

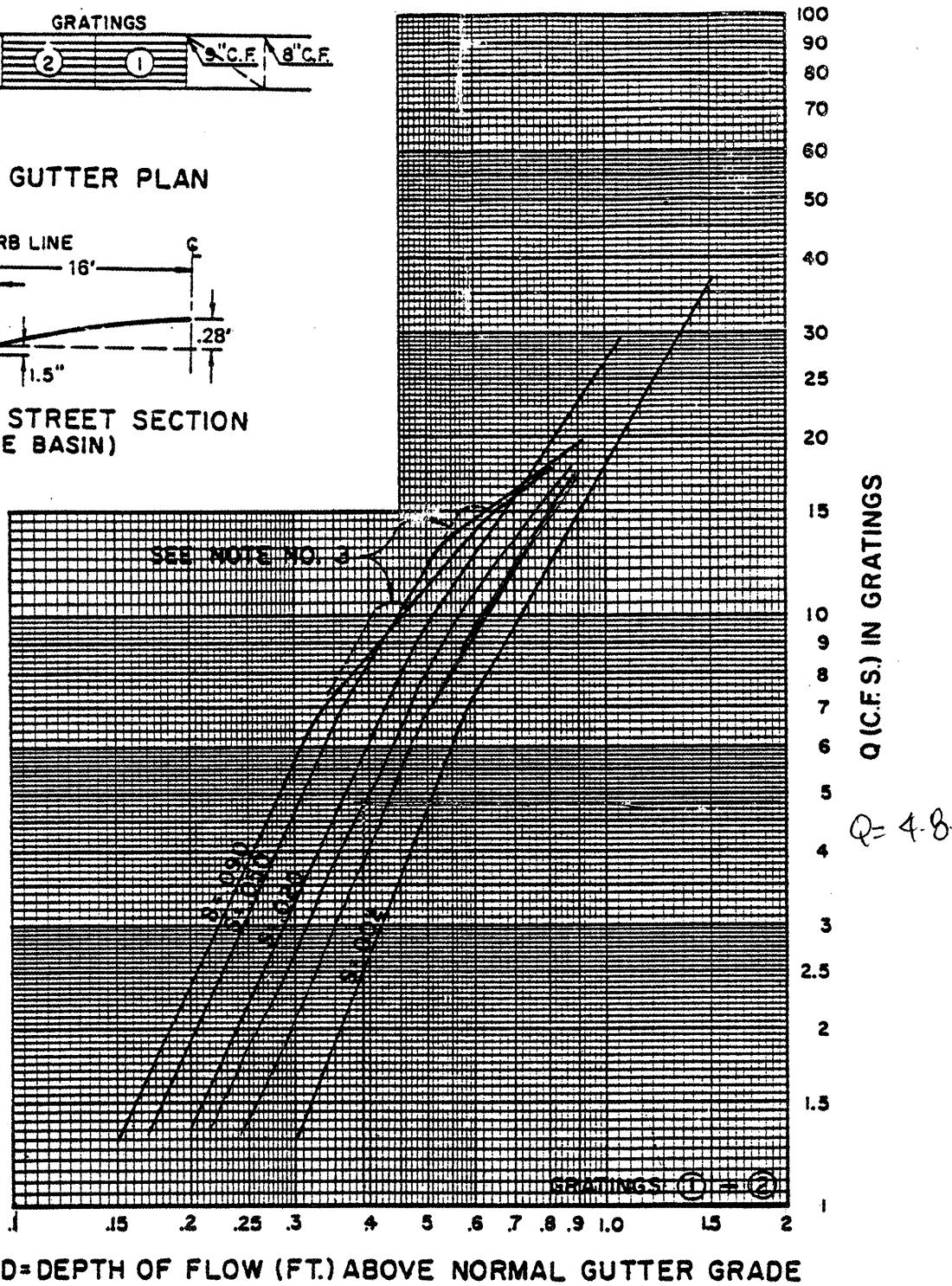
· double 'c'

Tatreefts

persecuting

flow

Inlet 49100



VM520

Inlet@ STA 130+88 ~58' RT
Area Double "D" Inlet

$$Q_{100} = 2.14 \text{ cfs}$$

$$Q_{10} = 1.11 \text{ cfs}$$

no curb opening

$$P = 2(w+l) = 2(\frac{76+25}{12}) = 16.83'$$

$$Q = (3)(16.83)d^{3/2}$$

$$2.14 = 50.49 d^{3/2}$$

$$d = .12' (100)$$

$$d = 0.08' (10)$$

Area is not in street + by dirt area.



BOHANNAN-HUSTON INC.

PROJECT NAME

Westside Blvd

SHEET _____ OF _____

PROJECT NO.

BY MT DATE

2/92

SUBJECT

Drainage

CH'D DATE

Westlog

Inlet 54H05 ~ @ ④

$$Q_{100} = 1.13 \text{ cfs}$$

$$Q_{10} = 0.15 \text{ cfs}$$

$$+ Q = 0.54 \text{ from Bypass from Inlet 130 to 3}$$

$$= 1.13 + .54 = 1.67 \text{ cfs}$$

Weir

$$Q = (3)(7.5) d^{3/2}$$

$$1.67 = (22.5)(d)^{3/2}$$

$$d = 1.8' (100\text{yr})$$

$$d = 0.10' (10\text{yr})$$

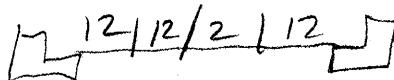
$$Q = (0.67)(4.43)(8.02)d^{1/2}$$

$$1.13 = 23.30 d^{1/2}$$

$$d = 0.002'$$

Weir controls

$$\therefore X_{slope} = 1.213\%$$



$$\frac{.18}{0.01213} = 14.8$$

$$d = 14.8' (100\text{yr})$$

$$d = 8.24' (10\text{yr})$$

$$\frac{.10}{.01213} = 8.24$$

\therefore OK will only flood 1 lane



BOHANNAN-HUSTON INC.

PROJECT NAME

Westside Blvd

SHEET

OF

PROJECT NO.

BY

DATE

SUBJECT

CH'D

DATE

2/94

P.69 Design of Highway Pavements

Weirs:

$$Q = 3.0 P d^{1.5}$$

on file

$$Q = \sqrt{67} A (644 d)^{1/2}$$

$$\text{Perimeter} = 2w + l = \frac{2(25) + 40}{12''/l} = 7.5' \quad (\text{single gully})$$

$$\therefore 3.0(7.5) d^{1.5}$$

Westleg Inlet @ 50% + 5% Sump condition
Assume 1/2 flow goes to each inlet

$$Q_{100} = 11.0 \text{ cfs} \quad Q_{10} = 6.47 \text{ cfs}$$

$$Q =$$

$$5.9 = 3(7.5) d^{3/2}$$

$$d = 0.41' (100)$$

$$d = 0.27' (10)$$

$$5.9 \cdot 67(443)(8.02) d^{1/2}$$

$$= 23.82 d^{1/2}$$

$$d = 0.26' (100)$$

$$d = 0.02' (10)$$

\therefore Weir equation controls

$$\begin{array}{r} 4 \\ \hline 14 \ 12 \ 12 \ 12 \ 14 \\ \hline \end{array} \quad \begin{array}{r} 0.41 \\ - .13 \\ \hline .28 \end{array} \quad .28 / .0168 = 16.7$$

Width of inlet 100yr.

$w = 16.7'$ \therefore covers only one lane + leaves the remaining open

$$= 8.33' \frac{10 \text{ year}}{\text{Cover Bike Lane}} \cdot \frac{.27}{.14} = .14 / .0168 = 8.33'$$

Single "A" +
Single "C"



BOHANNAN-HUSTON INC.

PROJECT NAME _____ SHEET _____ OF _____

PROJECT NO. _____ BY _____ DATE _____

SUBJECT _____ CH'D _____ DATE _____

Intlet 51+00 LT = 25' Li westleg

Area = 510-A Inlet @ 51+00 25' LT.

Q₁₀₀ = 1.08 cfs Q₁₀ = 0.06 cfs Single 'D' orifice

Weir

$$Q = 3.0 \times 7.5 d^{1/2}$$
$$1.08 = (3.0) 7.5 d^{3/2}$$

$$d = 0.13' (100\text{yr})$$

$$d = 0.10' (10\text{yr})$$

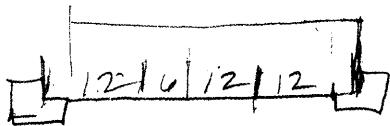
∴ Weir controls

$$1.08 = (0.67) 443 (8.02) d^{1/2}$$

$$d = 0.05' (100\text{yr})$$

$$d = 0.03' (10\text{yr})$$

DS



$$\frac{13}{.007} = 18.6'$$

$$w = 18.6' (100\text{yr})$$

$$\cdot 10/.007 = 14.3'$$

$$w = 14.3' (10\text{yr})$$

∴ not good try a Double

$$P = 2w + L = \\ = \frac{(2 \times 25) + 74}{12} = 10.50'$$

$$1.08 = (3) 10.5 d^{3/2}$$

$$d = 0.10' (100\text{yr})$$

$$\cdot 10/.007 = 14.3'$$

$$d = 0.08' (10\text{yr})$$

$$\cdot 108/.007 = 11.43'$$

$$w = 14.3' (100\text{yr})$$

$$w = 11.4' (10\text{yr})$$

Modified

∴ Double 'D' w/ 1 knee open @ 10yr



BOHANNAN-HUSTON INC.

PROJECT NAME

Westside Blvd

SHEET

OF

PROJECT NO.

BY

DATE

2/96

SUBJECT

Drainage

CH'D

DATE

KEY NOTES

- ① STA 48+00.00, 56.00' RT
BUILD 1-SINGLE A CATCH BASIN
TC-5214.39 INV=5209.39
COA SD 2201
- ② STA 48+00.00, 56.00' RT TO
STA 48+40.00, 56.00' RT
BUILD 33.65'-18" RCP CL III
 $S = 0.0350 \text{ FT/FT}$
- ③ STA 48+40.00, 56.00' RT
BUILD 1-DOUBLE C CATCH BASIN
TC-5213.57 INV=5208.21
COA SD 2205
- ④ STA 48+40.00, 56.00' RT TO
STA 48+79.00, 20.00' RT
BUILD 51.65'-24" RCP CL III
 $S = 0.0256 \text{ FT/FT}$
- ⑤ STA 48+79.00, 20.00' RT
BUILD 1-4" DIA MH TYPE "C"
W/ VENTED COVER.
PROVIDE 2" CURB OPENING IN
CURB AT COVER. ROTATE COVER
TOWARD CURB OPENING.
RIM=5213.04 TC=5213.54
SHAPE MEDIAN PAVEMENT AROUND
VENTED COVER. COVER IS 6"
BELOW MEDIAN PAVEMENT.
COA SD 2102 & 2110
- ⑥ SEE SHEET 7 FOR BUILD NOTES
- ⑦ RELOCATED 4" MP GAS LINE
(NEW LOCATION)

AS-BUILT INFORMATION		BENCH MARKS	
NO.	FIELD NOTES	A.C.S. I 3/4" ALUMINUM DISK, STAMPED	DATE
		CONCRETE BASE OF GALV STL POLE #1C-28 AT ANGLE PT. IN THE ELECTRIC TRANSMISSION FIELD BY 248 +/- NORTHERLY OF THE BERNALILLO/ SANDOVAL COUNTY LINE, 78.5' EASTERLY OF E OF RIO RANCHO BLVD (SR 528) ON SW	
		CORNERS OF SAID CONC BASE. FIELD ELEV = 5215.872 - SEE SH 5 FOR LOCATION	

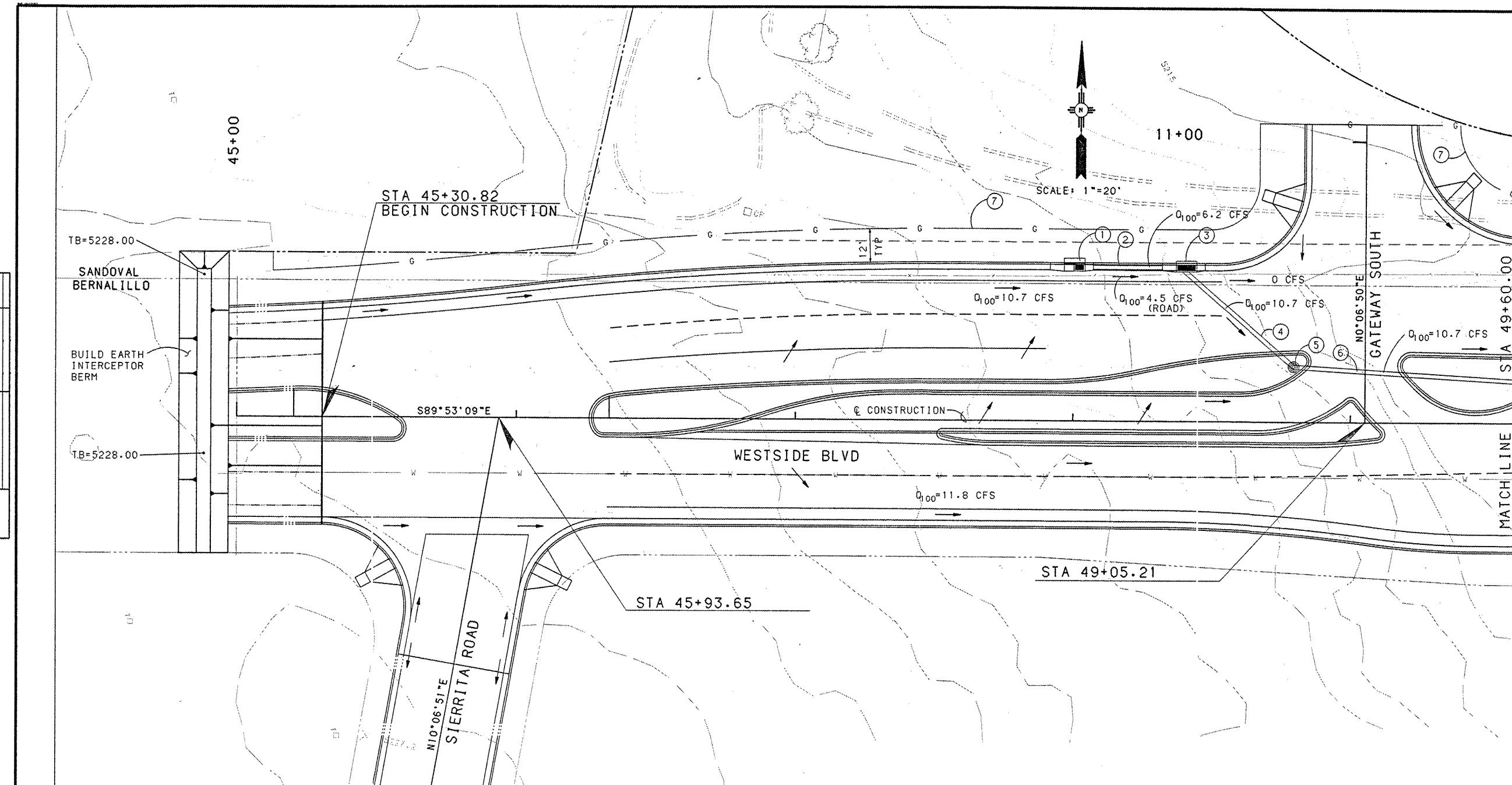


ENGINEER'S SEAL		SURVEY INFORMATION		BENCH MARKS	
NO.	FIELD NOTES	A.C.S. I 3/4" ALUMINUM DISK, STAMPED	DATE	NO.	FIELD NOTES
		CONCRETE BASE OF GALV STL POLE #1C-28 AT ANGLE PT. IN THE ELECTRIC TRANSMISSION FIELD BY 248 +/- NORTHERLY OF THE BERNALILLO/ SANDOVAL COUNTY LINE, 78.5' EASTERLY OF E OF RIO RANCHO BLVD (SR 528) ON SW			
		CORNERS OF SAID CONC BASE. FIELD ELEV = 5215.872 - SEE SH 5 FOR LOCATION			

BOHANNAN-HUSTON INC.
ENGINEERS • PLANNERS • PHOTOGRAHMETRISTS • SURVEYORS • LANDSCAPE ARCHITECTS
ALBUQUERQUE LAS CRUCES SANTA FE

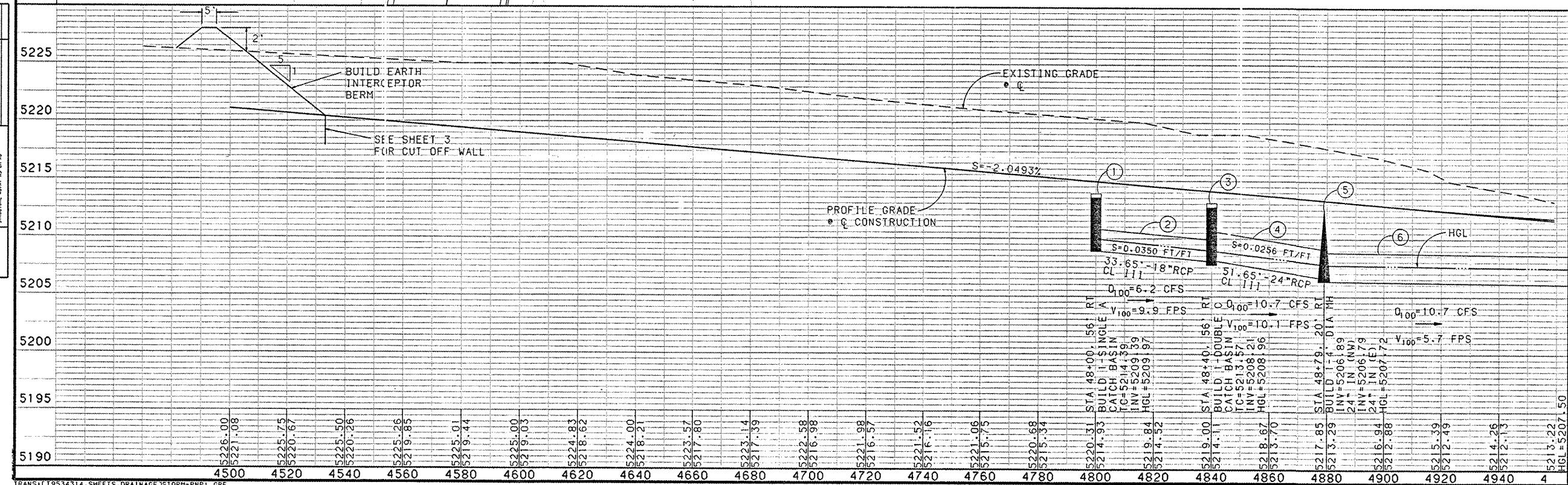
CITY OF ALBUQUERQUE
PUBLIC WORKS DEPARTMENT
ENGINEERING GROUP

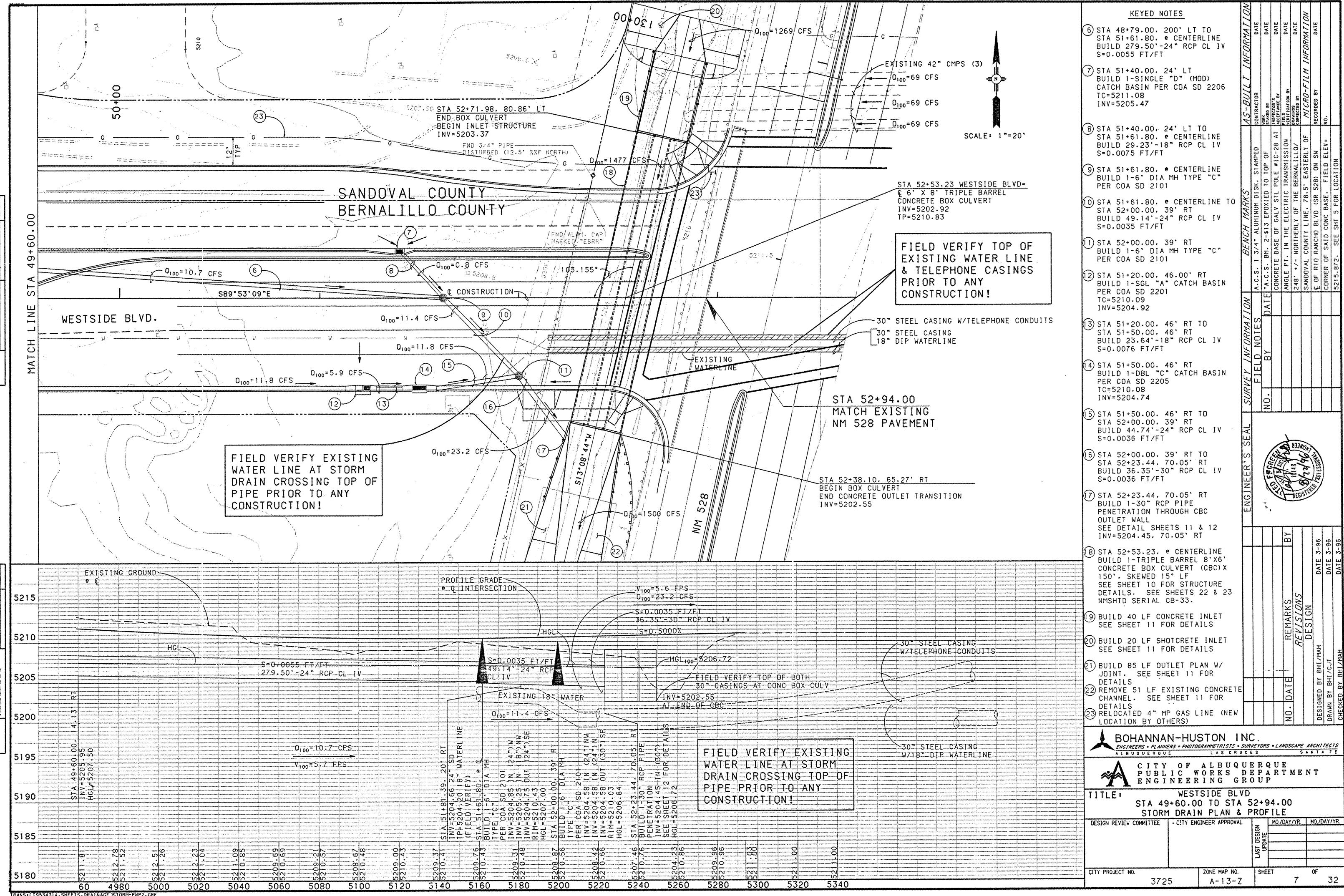
TITLE: WESTSIDE BLVD
STA 45+30.00 TO STA 49+60.00
STORM DRAIN PLAN & PROFILE

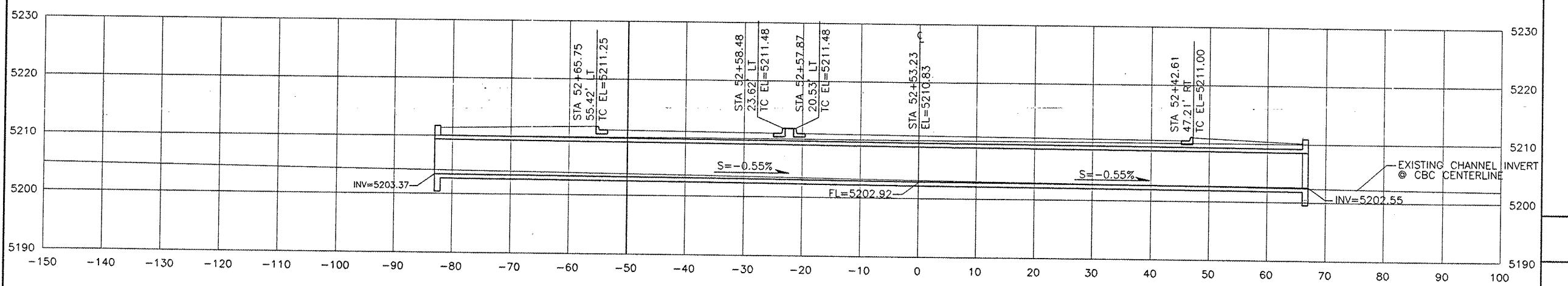
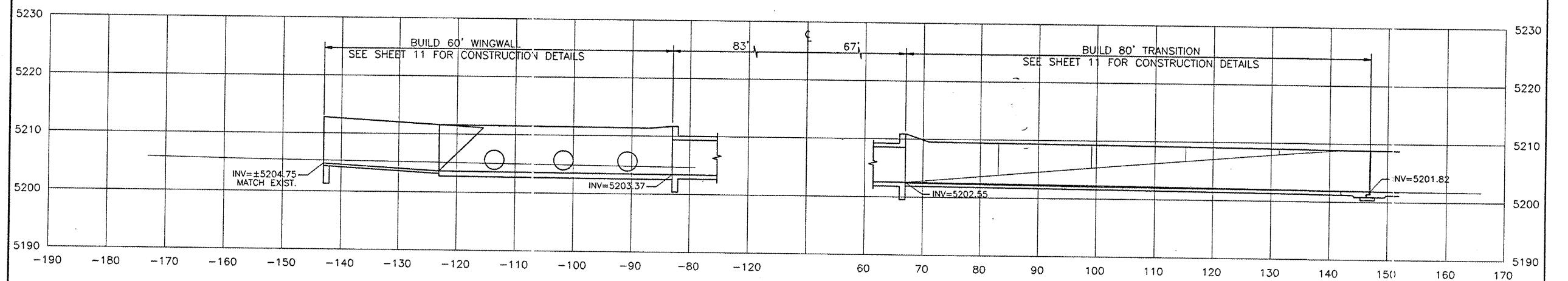
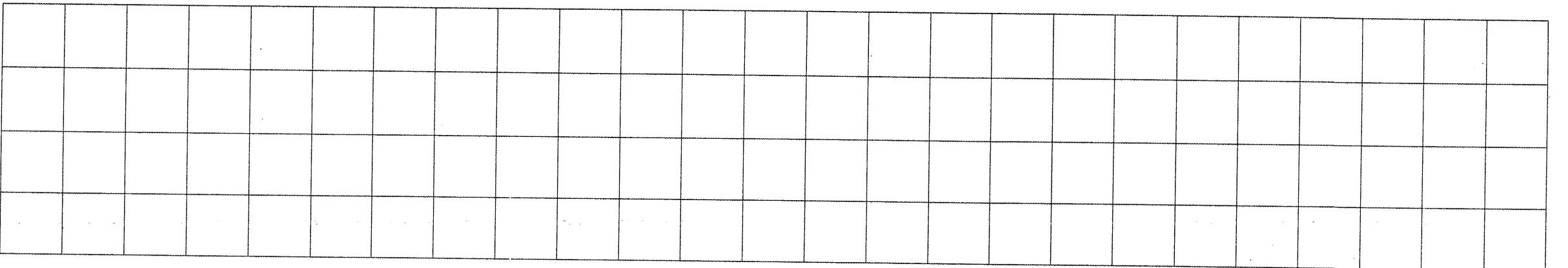


PLAN	BY	DATE
NOTE BOOK	BY	DATE
REVISIONS	BY	DATE
REMOVED	BY	DATE
CHANGES CHECKED	BY	DATE
REMOVED	BY	DATE
REMOVED	BY	DATE

PROFILE	BY	DATE
NOTE BOOK	BY	DATE
REMOVED	BY	DATE
CHANGES CHECKED	BY	DATE
REMOVED	BY	DATE
REMOVED	BY	DATE







STA 52+53.23

BUILD 3 ~ 8'x6'x150' CBC'S ~ 13° SK LF
W/WINGWALLS LT & RT, DESIGN I
SERIALS: CB-33

AS-BUILT INFORMATION	
CONTRACTOR	DATE
WORKS BY	DATE
INSPECTOR'S	DATE
ACCEPTANCE BY	DATE
ENGINEER'S	DATE
DRAWINGS BY	DATE
CORRECTED BY	DATE
MICRO-FILM INFORMATION	DATE
RECORDED BY	DATE
NO.	NO.
REMARKS	BY
REVISIONS	
DESIGN	
DESIGNED BY BH	DATE 1-95
DRAWN BY BH	DATE 1-95
CHECKED BY BH	DATE 1-95

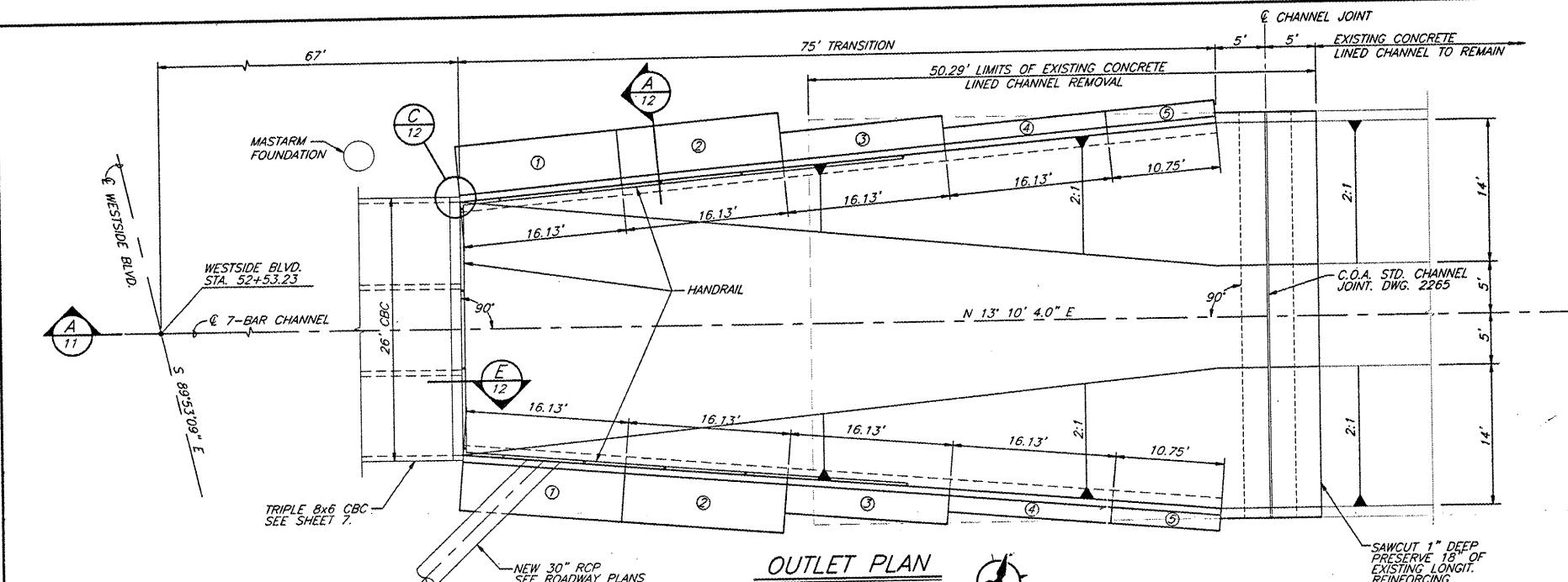
BOHANNAN-HUSTON INC.
ENGINEERS • PLANNERS • PHOTOGRAMMETRISTS • SURVEYORS • LANDSCAPE ARCHITECTS
ALBUQUERQUE LAB CRUCES SANTA FE

CITY OF ALBUQUERQUE
PUBLIC WORKS DEPARTMENT
ENGINEERING DEVELOPMENT GROUP

TITLE: WESTSIDE BLVD
CBC STRUCTURE SECTION

DESIGN REVIEW COMMITTEE	CITY ENGINEER APPROVAL	LAST DESIGN UPDATE DATE	MO./DAY/YR.	MO./DAY/YR.

CITY PROJECT NO. 3725 ZONE MAP NO. A-13-Z SHEET 10 OF 32



DESIGN DATA

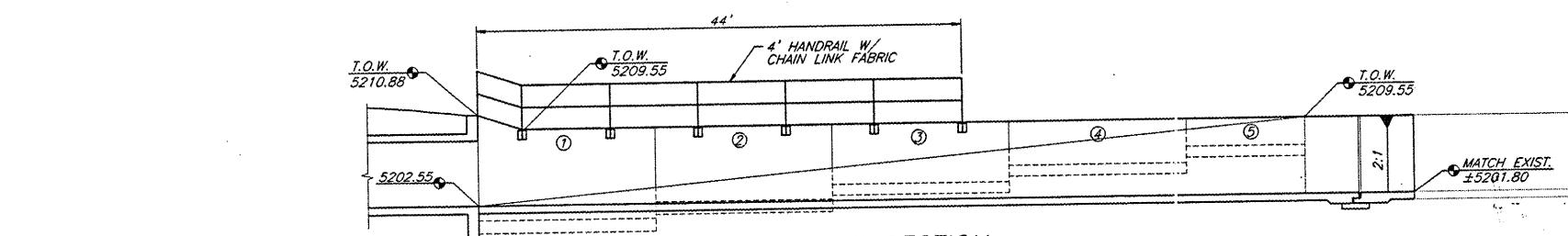
Live Load: 2' surcharge
Equivalent Fluid Earth Pressure:
Active = 35 pcf; Passive = 320 pcf.
Soil Weight: 110 pcf
Allowable soil pressure = 2000 psf
Sliding coefficient of friction = 0.40

GENERAL NOTES

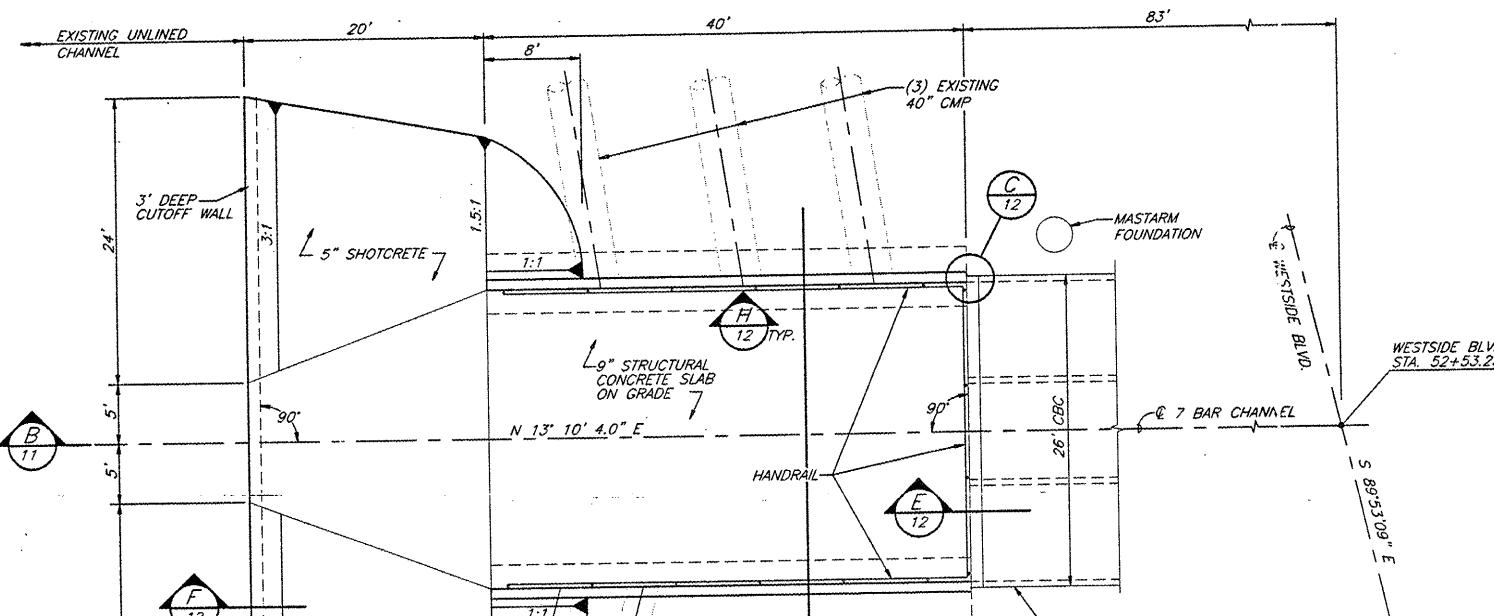
- 1 This work shall be in accordance with the New Mexico Standard Specifications for Highway and Bridge Construction, 1994 Edition and applicable supplemental special provisions.
 - 2 Concrete for retaining walls shall be Structural Concrete Class A, 4000 psi, with type F fly ash. Type F fly ash will be used at a rate of 4:1 (cement:FA). All concrete shall receive a Class 1, Ordinary Surface Finish.
 - 3 Reinforcing bars shall be grade 60 unless noted otherwise. Dimensions refer to the centerline of the bar.
 - 4 The contractor shall be responsible to locate in the field all existing utilities prior to beginning work. The contractor shall provide safe and adequate shoring of all utilities and structure during construction.
 - 5 The quantity for reinforcing bars is estimated based on the volume of concrete. Final payment will be made on the pounds of reinforcement in place.
 - 6 Anchor bolts, nuts and washers shall be ASTM A307, galvanized.
 - 7 Removal of portions of the existing concrete channel lining is required. Removal and disposal of all necessary items are paid for under item 601000. Removals include approx. 40 l.f. of 5' deep concrete cutoff wall, approx. 15 l.f. of riprap, type L, 3" thick in bottom, 18" thick on slopes (\pm 43 cy.) and approx. 230 sq. yd. of 8" conc. slope paving.

QUANTITIES

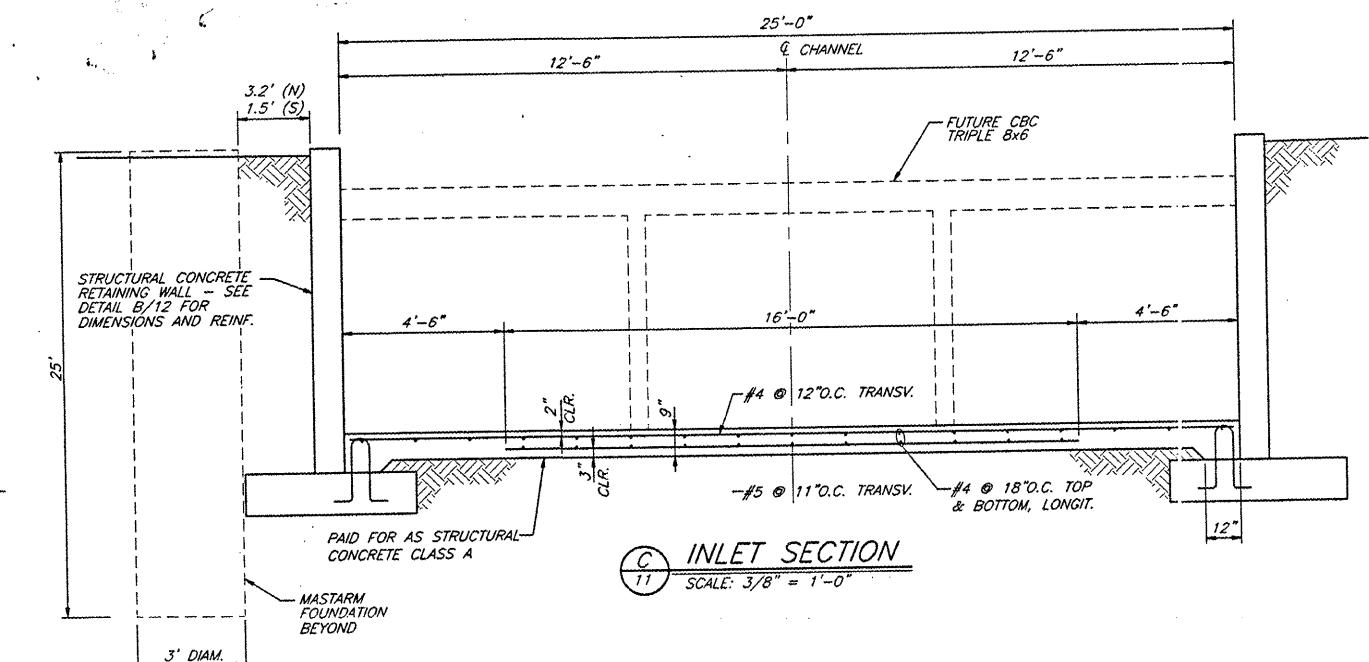
Item No.	Description	Unit	Quantity
203000	Unclassified Excavation	CY	1,425
203100	Borrow	CY	-
511000	Structural Concrete Class A	CY	128.5
540060	Reinforcing Bars Grade 60	LBS	22,975
601000	Removal of Structures and Obstr	LS	1
XXXXXX	8' Concrete Channel Lining	SY	325.0
XXXXXX	Channel Joint	LF	37.25
XXXXXX	5' Shotcrete	SY	143.6
XXXXXX	4' Chain Link Fence	LF	228.0



OUTLET SECTION



INLET PLAN



INLET SECTION

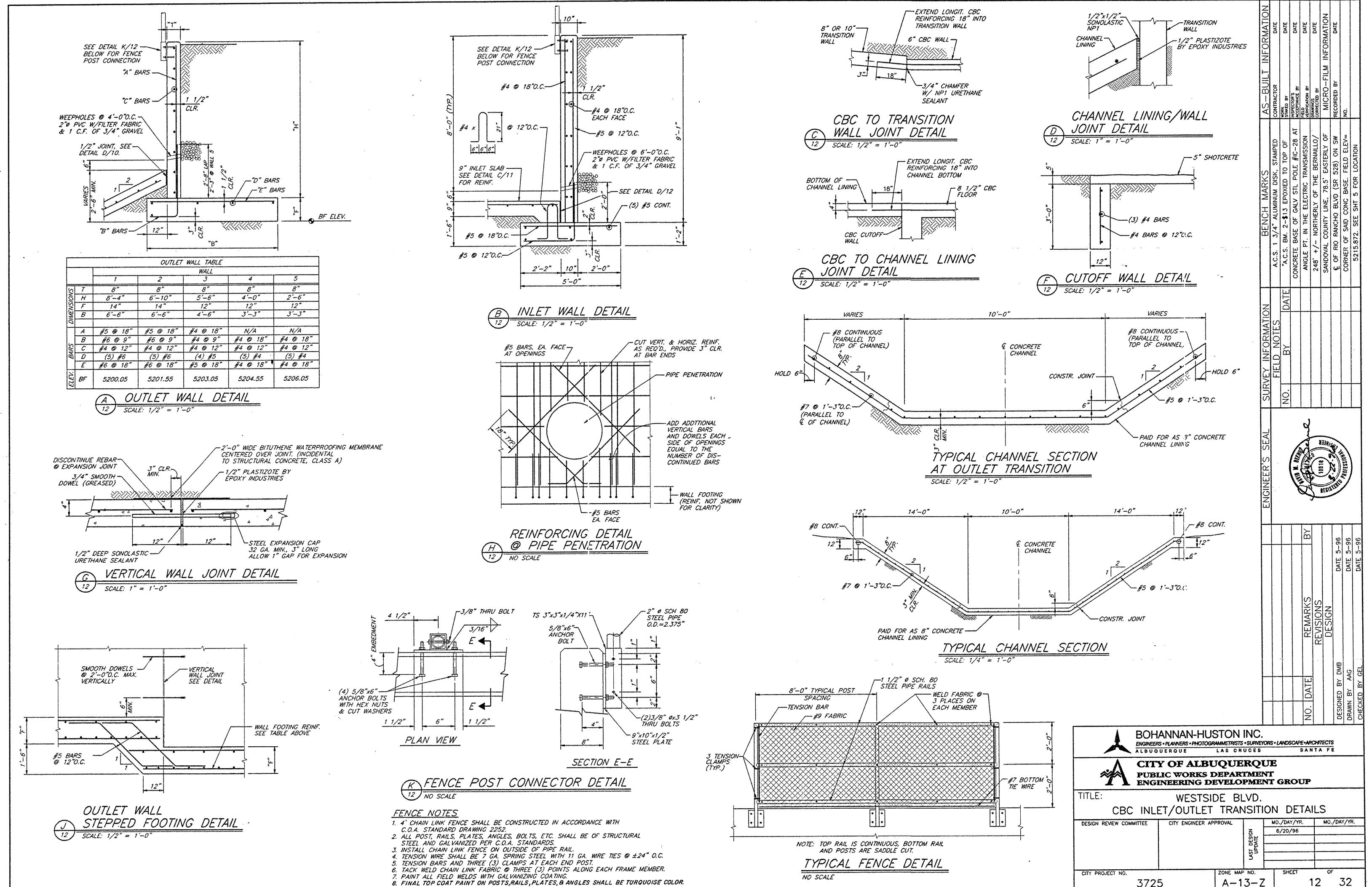


BOHANNAN-HUSTON INC.
ENGINEERS • PLANNERS • PHOTOGRAmmETRISTS • SURVEYORS • LANDSCAPE • ARCHITECTS
SANTA FE

**CITY OF ALBUQUERQUE
PUBLIC WORKS DEPARTMENT
ENGINEERING DEVELOPMENT GROUP**

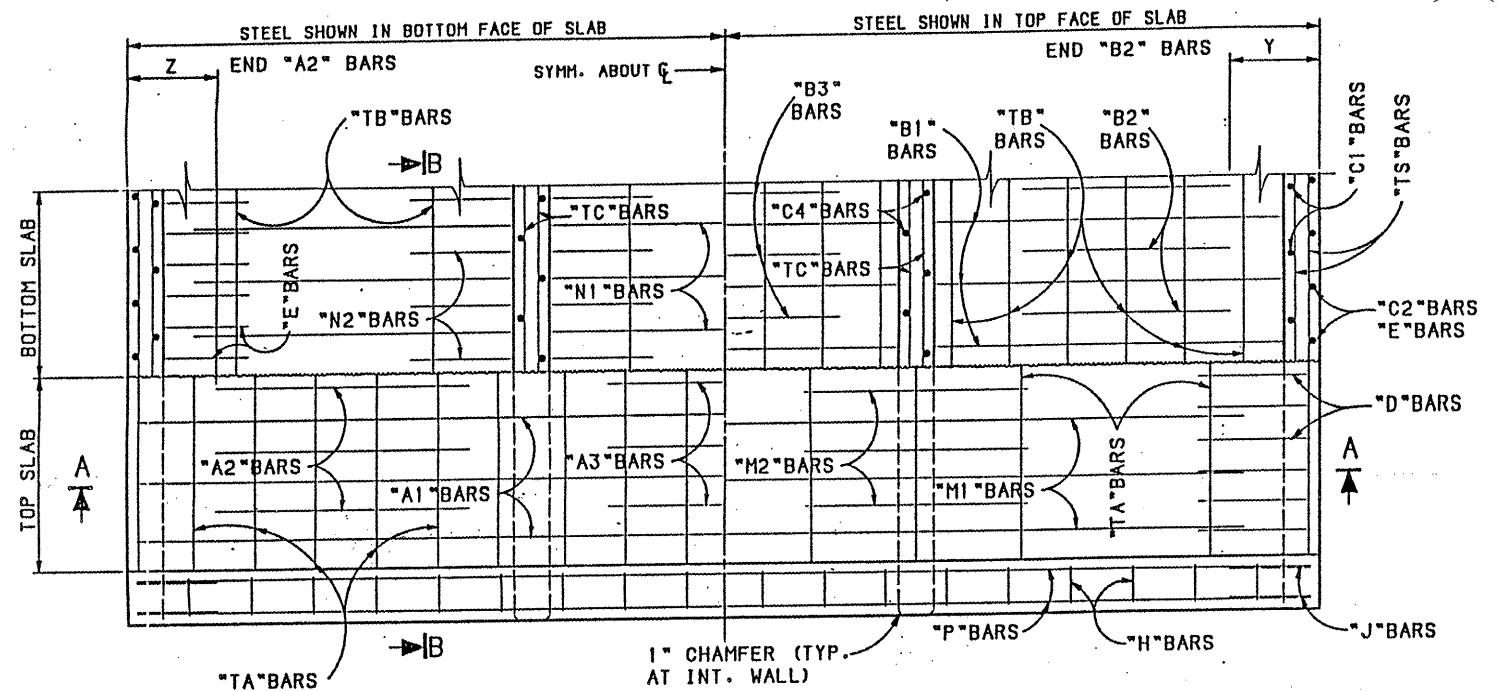
TITLE: WESTSIDE BLVD.
CBC INLET/OUTLET TRANSITION PLANS & SECTIONS

DESIGN REVIEW COMMITTEE	CITY ENGINEER APPROVAL	LAST DESIGN UPDATE	MO./DAY/YR.	MO./DAY/YR.
			6/20/96	
CITY PROJECT NO.		ZONE MAP NO.	SHEET	OF
3725		A-13-Z	11	32

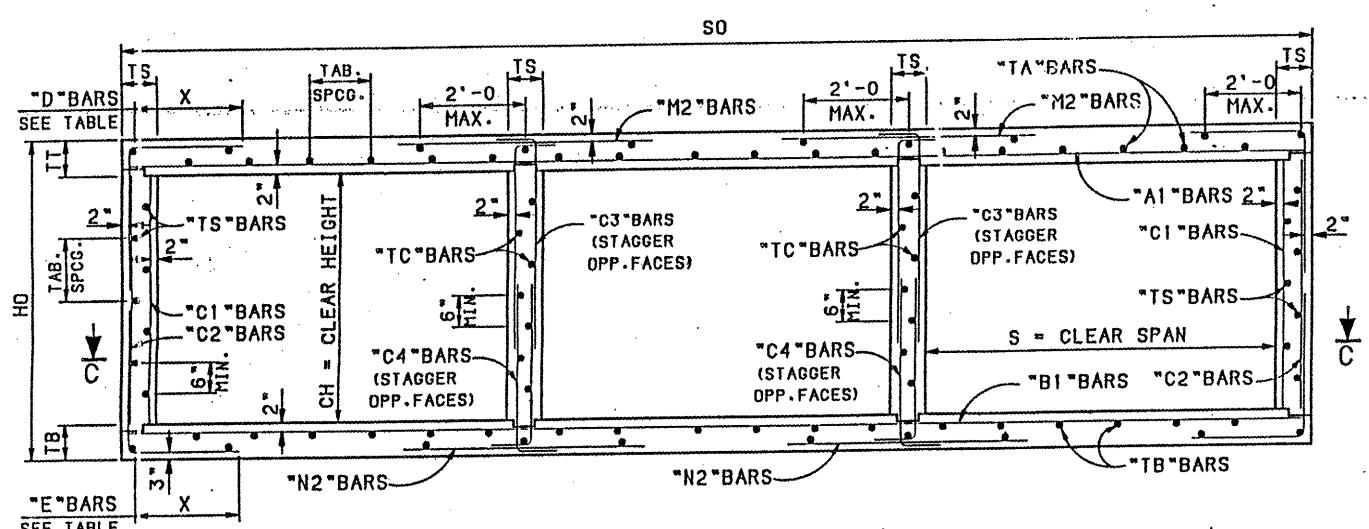


DESIGNED BY: H.T. 10/60 CHECKED BY: S.J.M. 10/93
DETAILED BY: J.A.K. 10/93 CHECKED BY: R.A. 10/93

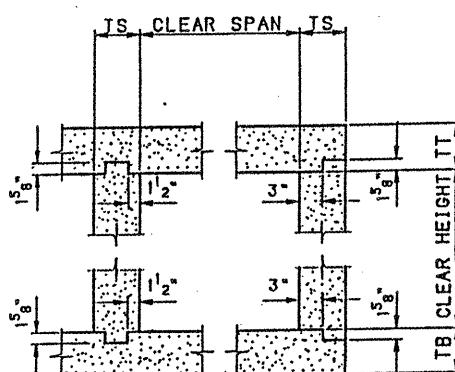
PLOT DATE: 10/28/93



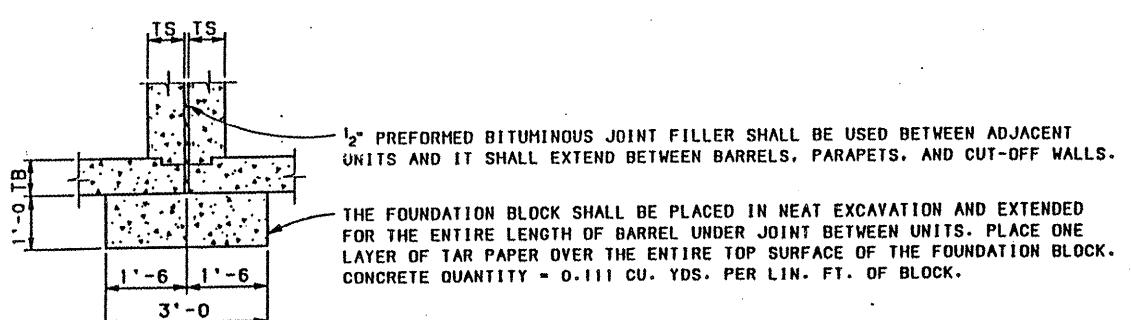
PART PLAN AND PART SECTION C-C



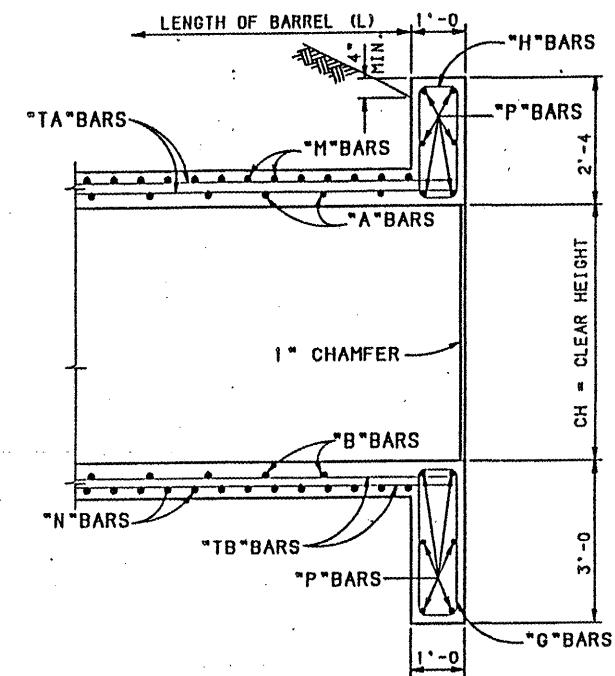
SECTION A-A



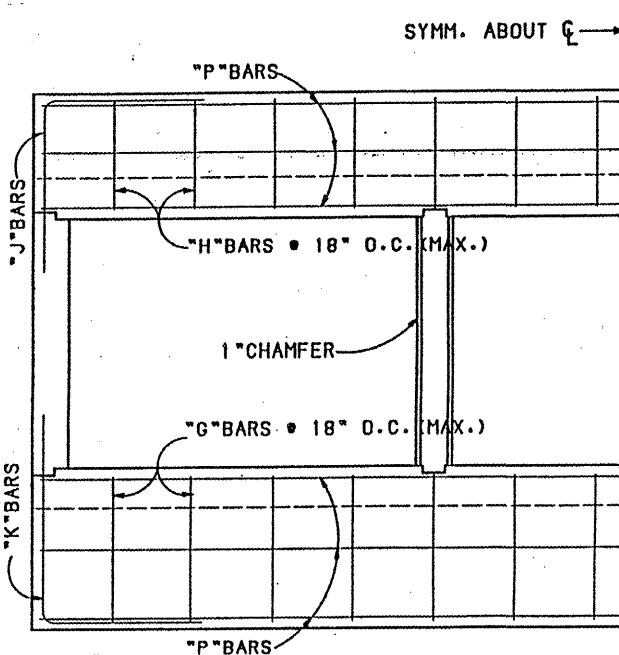
CONSTRUCTION JOINT DETAIL



JOINT DETAIL FOR MULTIPLE UNIT BOXES



ART. SECTION B-B



PART END ELEVATION

- ## GENERAL NOTES
1. ALL CONCRETE SHALL BE CLASS "A". CHAMFER ALL THE EXPOSED EDGES 3/4".
 2. ALL REINFORCING STEEL TO BE DEFORMED BARS, CONFORMING TO AASHTO M-31, GRADE 60. ALL DIMENSIONS REFER TO THE CENTERLINE OF BAR.
 3. WHEN NECESSARY, "T" BARS MAY BE SPLICED BY LAPPING AT LEAST 20 BAR DIAMETERS. PAY WEIGHT FOR REINFORCING STEEL DOES NOT INCLUDE SPLICES. THE COST OF THE SPLICE MATERIAL IS TO BE INCLUDED IN THE UNIT PRICE BID FOR REINFORCING STEEL.
 4. VOLUME OF CONCRETE = $(L) \times (\text{CONCRETE QUANTITY/LIN. FT.})$
PLUS CONCRETE AT ENDS.
 5. WEIGHT OF REINFORCING STEEL = $(L) \times (\text{WEIGHT OF REINF./LIN.FT.})$
PLUS WEIGHT AT ENDS.
 6. PLACE "TA" BARS ON "A" BARS AND "TB" BARS UNDER "E" BARS, SPACED AS SHOWN IN THE TABLE. THE REMAINING "TA" BARS, AND "TB" BARS ARE TO BE PLACED ADJACENT TO THE "D", "E", "M", AND "N" BARS AS INDICATED IN "SECTION A-A", AT 2'-0 MAX.
 7. PLACE "TS" BARS NEXT TO "C1" BARS, SPACED AS SHOWN IN THE TABLE; THE REMAINING "TS" BARS SHALL BE PLACED IN SIDEWALL NEXT TO "C2", "D", AND "E" BARS. WHEN "C1" BARS ARE NOT REQUIRED, PLACE ALL "TS" BARS NEXT TO "C2", "D", AND "E" BARS.
 8. PLACE "A1", "A3", "B1", "B3", "M1", AND "N1" BARS SYMMETRICAL TO THE CENTERLINE OF THE BOX. PLACE "M2" AND "N2" BARS SYMMETRICAL TO THE CENTERLINE OF THE WALLS.
 9. "COVER" IS HEIGHT OF FILL FROM TOP OF THE BOX TO THE FINISHED GRADE.

DESIGN DATA

DESIGN ACCORDING TO A.A.S.H.O. SPECIFICATIONS, 1957.
LIVE LOAD: H20-S16-44 & INTERSTATE ALTERNATE LOADING
WEIGHT OF FILL ON TOP OF BOX: 84#/CU.FT.
HORIZONTAL EARTH PRESSURE: 30#/CU.FT., 2' SURCHARGE
DESIGN STRESSES: $f'_c = 3000$ psi, $f_b = 1200$ psi,
 $f_a = 20,000$ psi, $f_s = 10$.

6			
5			
4			
3			
2			
1	REVISED NOTE #2	6-8-94	PH
NO.	DESCRIPTION	DATE	BY
REVISIONS (OR CHANGE NOTICES)			
<p style="text-align: center;">NEW MEXICO STATE HIGHWAY AND TRANSPORTATION DEPARTMENT</p>			
<p style="text-align: center;">CONCRETE BOX CULVERT BARRELS TRIPLE OPENING - NORMAL ALL DESIGNS</p>			
<p style="text-align: center;">GENERAL DATA</p>			
<p style="text-align: center;">CITY PROJECT# 3725</p>			
APPROVAL BY MAINT BY CHECKED BY	APPROVAL RECOMMENDED BY ENGINEER	APPROVED BY DESIGN BUREAU CHIEF	APPROVAL DATE 2-27-94 DATE
<p style="text-align: center;">SERIAL CB-33</p>		<p style="text-align: right;">SHEET 13 OF 32</p>	

DESIGNED BY: H.T. 1/61
CHECKED BY: S.J.M. 10/93
DETAILED BY: J.A.K. 10/93

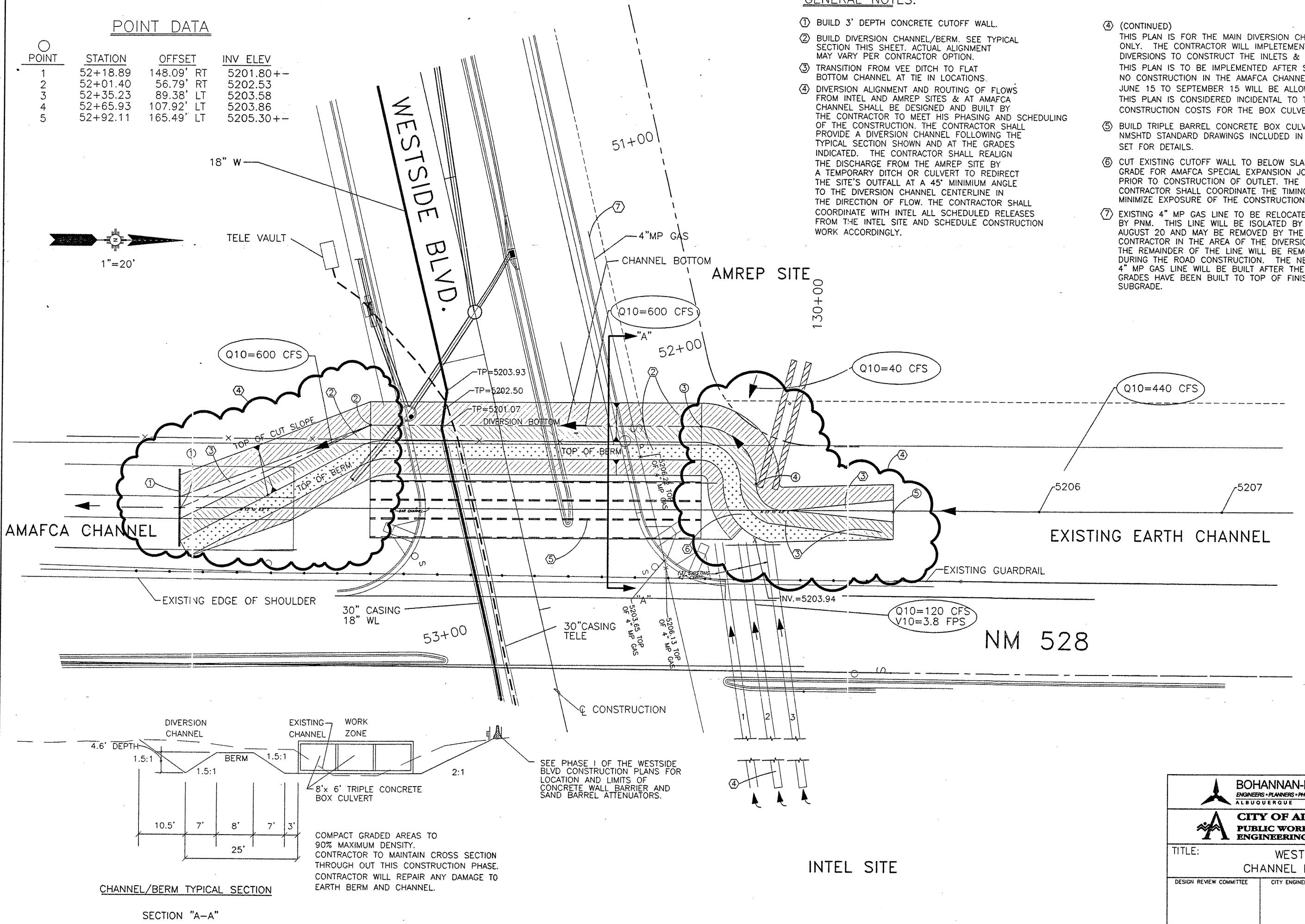
PLOT DATE: 10/28/93

REINFORCING STEEL DIAGRAM

DIMENSIONS							QUANTITIES							REINFORCING BARS																																															
CLEAR SPAN	CLEAR HEIGHT	TT	TS	TB	SO	HO	Y	Z	PER L.F. OF BARREL		AT ONE END *		"A" BARS						"B" BARS						"C" BARS						"M" BARS			"N" BARS			"D"			"E"			"TA"		"TB"		"TC"		"TS"		G.H.										
									STEEL POUNDS PER L.F.	CONCRETE CU. YDS.	STEEL POUNDS PER L.F.	CONCRETE CU. YDS.	"A1"	"A2"	"A3"	SIZE	LENGTH	"B1"	"B2"	"B3"	SIZE	LENGTH	"C1"	"C2"	C3	C4	SIZE	LENGTH	"X"	SIZE	LENGTH	"X"	SIZE	LENGTH	"X"	SIZE	LENGTH	"X"	NO.	SIZE	SPACING	NO.	SIZE	SPACING	NO.	SIZE	SPACING	NO. OF EA.													
4	2	7"	6"	6'2"	14'-0	3'-1'2	---	---	115.8	0.731	337	2.91	#5	13'-9"	--	NONE	--	NONE	6"	#4	13'-9"	--	NONE	--	NONE	12"	NONE	NONE	#4	2'-3"	2'-3"	12"	#4	12'-6"	#4	3'-9"	18"	#5	3'-6"	1'-6	12"	19	#4	16"	6	#4	18"	9													
	3	7"	6"	6'2"	14'-0	4'-1'2	---	---	122.8	0.806	347	2.99	#5	13'-9"	--	NONE	--	NONE	6"	#4	13'-9"	--	NONE	--	NONE	12"	NONE	NONE	#4	2'-9"	2'-9"	12"	#4	12'-6"	#4	3'-9"	18"	#5	4'-0"	1'-6	12"	19	#4	16"	8	#4	18"	9													
	4	7"	6"	6'2"	14'-0	5'-1'2	---	---	124.3	0.880	355	3.06	#5	13'-9"	--	NONE	--	NONE	6"	#4	13'-9"	--	NONE	--	NONE	13"	NONE	NONE	#4	3'-3"	3'-3"	13"	#4	12'-6"	#4	3'-9"	18"	#5	4'-6"	1'-6	13"	19	#4	16"	10	#4	18"	9													
6	2	7'2"	6"	7"	20'-0	3'-2'2	1'-0	2"	185.4	1.043	472	4.10	#5	18'-6"	#6	5'-9"	#5	5'-0"	12"	#4	19'-9"	#4	5'-0"	--	NONE	14"	NONE	NONE	#4	2'-3"	2'-3"	9"	#4	18'-6"	#6	5'-0"	18"	#4	18'-6"	12"	31	#4	16"	25	#4	18"	12														
	3	7'2"	6"	7"	20'-0	4'-2'2	1'-0	2"	191.0	1.117	460	4.17	#5	18'-6"	#6	5'-9"	#5	5'-0"	12"	#4	19'-9"	#4	5'-0"	--	NONE	14"	NONE	NONE	#4	2'-9"	2'-9"	9"	#4	18'-6"	#6	5'-0"	18"	#4	18'-6"	12"	31	#4	16"	25	#4	18"	12														
	4	7'2"	6"	7"	20'-0	5'-2'2	1'-0	2"	197.6	1.191	493	4.25	#5	18'-6"	#6	5'-9"	#5	5'-0"	12"	#4	19'-9"	#4	5'-0"	--	NONE	14"	NONE	NONE	#4	3'-3"	3'-3"	9"	#4	18'-6"	#6	5'-0"	18"	#4	18'-6"	12"	31	#4	16"	25	#4	18"	12														
8	5	7'2"	6"	7"	20'-0	6'-2'2	1'-0	2"	210.4	1.285	505	4.32	#5	18'-6"	#6	5'-9"	#5	5'-6"	12"	#4	19'-9"	#4	5'-6"	--	NONE	13"	NONE	NONE	#4	4'-3"	3'-3"	9"	#4	18'-6"	#6	5'-3"	18"	#4	18'-6"	13"	31	#4	16"	25	#4	18"	12														
	6	7'2"	6"	7"	20'-0	7'-2'2	1'-0	2"	227.9	1.339	550	4.40	#5	18'-6"	#6	5'-9"	#5	5'-9"	11"	#4	19'-9"	#4	5'-9"	--	NONE	12"	NONE	NONE	#4	5'-3"	3'-3"	9"	#4	18'-6"	#6	5'-6"	18"	#4	18'-6"	14"	31	#4	16"	25	#4	18"	12														
	7	8"	6"	8'	26'-0	7'-2'2	1'-0	2"	292.4	1.620	790	5.43	#5	25'-9"	#7	7'-9"	#6	6'-3"	12"	#4	25'-9"	#4	6'-6"	--	NONE	11"	NONE	NONE	#5	4'-3"	3'-0"	10"	#4	24'-0"	#6	6'-0"	11"	#6	4'-3"	1'-6	11"	#5	5'-3"	1'-6	11"	#4	14"	34	#4	16"	10	#4	18"	18							
10	8	8"	6"	8'	26'-0	5'-4'2	1'-0	2"	314.7	1.694	804	5.51	#5	25'-9"	#7	7'-9"	#6	6'-3"	12"	#4	25'-9"	#4	6'-6"	--	NONE	10"	NONE	NONE	#5	5'-3"	3'-0"	10"	#4	25'-6"	#6	6'-9"	12"	#4	25'-6"	#6	6'-9"	10"	#6	4'-8"	1'-6	10"	#5	6'-0"	1'-6	10"	#4	14"	34	#4	16"	14	#4	18"	18		
	9	8"	6"	8'	26'-0	7'-4'2	1'-0	2"	333.4	1.769	816	5.59	#5	25'-9"	#7	7'-9"	#6	6'-3"	11"	#4	25'-9"	#4	6'-6"	--	NONE	10"	NONE	NONE	#5	6'-3"	3'-0"	10"	#4	25'-6"	#6	7'-9"	12"	#4	25'-6"	#6	7'-9"	11"	#6	5'-6"	1'-6	10"	#5	5'-6"	1'-6	10"	#4	14"	34	#4	16"	16	#4	18"	18		
	10	9"	8"	8'	26'-0	8'-4'2	1'-0	2"	347.3	1.946	882	5.82	#5	26'-0"	#7	8'-0"	#6	6'-6"	12"	#4	26'-0"	#4	6'-6"	--	NONE	14"	NONE	NONE	#5	7'-3"	3'-0"	12"	#4	25'-6"	#6	8'-6"	12"	#4	25'-6"	#7	8'-6"	14"	#7	6'-9"	1'-6	14"	#6	5'-6"	1'-6	14"	#4	16"	40	#4	17"	34	#4	16"	18	#4	18"
12	11	9"	9"	9'	32'-0	32'-4	8'-6'2	1'-3	411.6	2.451	1223	7.00	#6	30'-0"	#6	9'-6"	#5	8'-0"	12"	#5	32'-0"	#5	7'-0"	--	NONE	14"	NONE	NONE	#5	7'-3"	3'-0"	12"	#5	30'-0"	#7	9'-6"	13"	#4	25'-6"	#7	9'-6"	13"	#7	4'-6"	1'-6	13"	#6	4'-3"	1'-6	13"	#3	16"	34	#4	16"	22	#4	18"	18		
	12	9"	9"	9'	32'-0	32'-4	8'-6'2	1'-3	430.0	2.655	1262	7.26	#6	30'-3"	#6	9'-6"	#5	8'-0"	12"	#5	32'-3"	#4	7'-0"	--	NONE	12"	NONE	NONE	#5	13"-3"	5"-3"	12"	#5	29'-6"	#7	7'-3"	12"	#5	29'-3"	#7	6'-3"	12"	#7	6'-0"	2'-3"	12"	#7	6'-0"	2'-3"	15"	#9	4	16"	43	#4	18"	12	#4	17"	21	

POINT DATA

POINT	STATION	OFFSET	INV ELEV
1	52+18.89	148.09' RT	5201.80+-
2	52+01.40	56.79' RT	5202.53
3	52+35.23	89.38' LT	5203.58
4	52+65.93	107.92' LT	5203.86
5	52+92.11	165.49' LT	5205.30+-



BOHANNAN-HUSTON INC. ENGINEERS • PLANNERS • PHOTOGRAHMETRISTS • SURVEYORS • LANDSCAPE ARCHITECTS ALBUQUERQUE LAS CRUCES SANTA FE	
CITY OF ALBUQUERQUE PUBLIC WORKS DEPARTMENT ENGINEERING DEVELOPMENT GROUP	
TITLE: WESTSIDE BLVD. CHANNEL DIVERSION PLAN	
DESIGN REVIEW COMMITTEE	CITY ENGINEER APPROVAL
LAST DESIGN UPDATE	
MO./DAY/YR.	
MO./DAY/YR.	
CITY PROJECT NO. 3725 ZONE MAP NO. A-13-Z SHEET 15 OF 32	