



DRAINAGE REPORT FOR TRACTS B-1 & B-2 SEVEN BAR NORTH SUBDIVISION

Prepared for:

**BROWN/NZD DEVELOPMENT JOINT VENTURE
C/O BROWN & ASSOCIATES
3411 CANDELARIA NE
ALBUQUERQUE, NEW MEXICO 87107**

JUN - 7 1994

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Job No. 93217.43

Drainage Report
for
Tracts B-1 & B-2
Seven Bar North Subdivision

May 1994
(Revised June 1994)

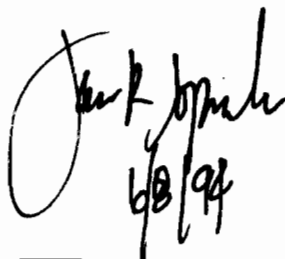
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C/O BROWN & ASSOCIATES
3411 CANDELARIA NE
ALBUQUERQUE, NEW MEXICO 87107

Prepared by:

Under the Supervision of:


Pierce Runnels


6/8/94



James Topmiller, P.E.

i:\cdp\9321743\drainage.rpt - June 6, 1994

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I. INTRODUCTION/PURPOSE OF REPORT

This report presents the Drainage Management Plan for Preliminary Plat and rough grading approval for the development of Tracts B-1 and B-2 of the Seven Bar North Subdivision. The property is currently zoned R-LT and the proposed development is for 162 lots of detached, single family residential housing and the related streets and infrastructure. As shown on the location map on the Drainage Basin Map, the property is bounded by Seven Bar Loop Road on the west, Sierrita Road and undeveloped, vacant land (Tract B-3) on the north, and Seven Bar/Skyview Channel on the south and east.

The report outlines the study methodologies used and summarizes the existing and proposed drainage conditions. Calculations and supporting data are presented in the appendices. A drainage basin map, a preliminary grading plan and a copy of the Preliminary Plat are included in the Plates at the end of the report. The purpose of this report is to obtain drainage report approval for the Preliminary Plat for Tracts B-1 and B-2, and rough grading approval.

II. STUDY METHODOLOGIES

Undeveloped, existing conditions and proposed, developed conditions were analyzed for the 100-year, 6-hour storm event consistent with the City of Albuquerque Design Process Manual (DPM), including the January, 1993 revision of Section 22.2, Hydrology. The analysis also references the previously submitted Drainage Master Plan for the Seven Bar North Subdivision, dated April, 1994 and is consistent with that report.

Street hydraulics and channel capacities were analyzed using Manning's equation with the Manning's "n" values suggested in the DPM. Rating curves for streets and channels are provided in the Appendices, along with all hydrologic and

hydraulic calculations. Streets are designed to convey the energy grade line of the design storm event within the right-of-way. Normal flow depth is confined to the top of curb.

III. EXISTING CONDITIONS

Site Characteristics

This site is currently undeveloped vacant land with slopes ranging from 2% to 8% in a generally southwestern direction. Soils are highly absorptive sandy soils with occasional clay lenses. Vegetation is light, consisting of grasses and small sagebrush.

The site is not located within a FEMA floodplain, as shown on the Floodplain Map provided on the Drainage Master Plan (enclosed in the rear of this report).

The existing drainage conditions are shown graphically on the "Existing Drainage Conditions" map (from the Drainage Master Plan submittal, see Appendix) and are summarized as follows:

Onsite Drainage Basins

Tract B-2, approximately 19.9 acres, currently drains in primarily sheet flow, to the southwest corner of the tract, where it discharges over a concrete rundown into the Seven Bar/Skyview Channel. The 100-year storm event currently generates 26.2 cfs of peak flow.

Tract B-1, approximately 15.2 acres, also drains in sheet flow into the Seven Bar/Skyview Channel. The 100-year storm event generates a peak flow rate of 20.0 cfs from Tract B-1.

Offsite Drainage Basins

The area to the north of Tracts B-1 and B-2 and south of Westside Boulevard currently drains across these tracts and into the Seven Bar/Skyview Channel. This area is shown on the Existing Drainage Conditions map as Basin E-3 and consists of approximately 56.6 acres which generate a peak flow of 74.5 cfs during the 100-year storm.

IV. PROPOSED DEVELOPED CONDITIONS

The proposed development is a single-family, detached-unit residential subdivision with 162 lots on 35.1 acres, producing a density of 4.62 du/acre. Proposed street configurations are shown on the Preliminary Plat, the Drainage Basin Map and on the Preliminary Grading Plan. As shown on the Preliminary Plat, the project is proposed to be divided into two phases.

Phase I Development

Phase 1 includes the development of all of Tract B-1 and the construction of Seven Bar Loop Road and associated storm drain from Black's Arroyo to Sierrita Road, and the construction of Sierrita Road and associated storm drain from Seven Bar Loop Road to the eastern boundary of Tract B-1. The storm drain to be constructed in Seven Bar Loop Road and Sierrita Road is designed to accommodate flows for the fully developed condition of Basins B-1 through B-9 as shown in the Drainage Master Plan for Seven Bar North Subdivision. The detention pond at the northeast intersection of Seven Bar Loop Road and Sierrita Road and the swale along the north edge of the project will also be constructed during Phase 1.

For purposes of analysis, Tract B-1 is subdivided into six smaller sub-basins, Basins 1A through 1F, as shown on the Drainage Basin Map. Basin 1A discharges

8.0 cfs into the Seven Bar Loop Road storm drain. This storm drain then discharges via existing storm drain pipe stub out into the Black's Channel. The remaining five basins (1B through 1F) together generate a fully developed runoff of 44.7 cfs ($9.7 + 5.4 + 11.2 + 5.2 + 13.2$). This runoff is conveyed by street flow to a proposed storm drain inlet and storm drain which lies in a 25' public drainage easement between Lots 15 and 16. This storm drain then discharges through a pipe penetration directly into Seven Bar/Skyview Channel as preliminarily shown on a plan and profile sheet in the appendix.

As stated in the Methodology Section of this report, street flows were calculated and energy grade lines confined to the right-of-way. A Summary Table of the street calculations is provided at the front of Appendix 2 for review and reference. The allowable locations for the use of roll curb have been identified on the Curb Type Identification Map in the rear of this report.

Calculations are found in Appendix 3 for the public drainage channel sizing and preliminary designs of this channel are located in the rear of this report (see Plates).

Phase II Development

Phase II consists of the development of all of Tract B-2 and the construction of Sierrita Road and storm drain from the west boundary of Tract B-2 to the northeast boundary of Tract B-2. Tract B-2 is subdivided into six smaller basins, 2A through 2F. These basins combine to generate a fully developed runoff of 68.1 cfs. This flow is conveyed by street flow to a public concrete channel which discharges, through a drainage and public utility easement, into Seven Bar/Skyview Channel. All connections, in both phases, to the Seven Bar/Skyview Channel will be coordinated through AMAFCA.

As stated in the Methodology Section of this report, street flows were calculated and energy grade lines confined to the right-of-way. A Summary Table of the street calculations is provided at the front of Appendix 2 for review and reference. The allowable locations for the use of roll curb have been identified on the Drainage Plan.

Calculations are found in Appendix 3 for the public drainage channel sizing and preliminary design are also shown in the rear plates of this report.

Backyard Ponding

Most of the lots located against the Skyview Channel require backyard ponds due to elevation differences between pads and the channel right-of-way. Pond locations are shown on the preliminary grading plans enclosed in the rear of this report.

Offsite Basins

This offsite basin that impacts Tracts B-1 and B-2 is Basin E-3. Basin E-3 consists of approximately 56.6 acres and generates a peak flow of 74.5 cfs and a peak volume of 2.13 acre-feet during the 100-year storm. These flows will be captured in a temporary swale beginning on the northern boundary of Tract B-2 and flowing adjacent to, and north of, Sierrita Road. Calculations for the swale are found in the Appendix.

A detention/sedimentation pond will be provided at the terminus of the swale at the northeast corner of the intersection of Seven Bar Loop Road and Sierrita Road. The pond is designed to remove the sediment from the 10-year storm and have an orifice-controlled discharge into a connector pipe that runs to a storm drain manhole that is being built in Sierrita Road as part of the Phase I improvements.

With the development of upstream basins, the pond will be filled, the asphalt-lined swale will be removed and disposed of, and the connector pipe will be removed from the pond to the property line and the remainder abandoned in place. Design details of the pond are to be found in Appendix at the end of this report.

V. PHASING/BUILDING PERMIT/FINAL PLAT APPROVALS

This report requests only Preliminary Plat and rough grading approvals. Prior to final plat and building permit approvals, final grading plans and work order construction plans, by phase, must be submitted and approved by the City and AMAFCA.

VI. CONCLUSION

The drainage management plan presented in this report for Tracts B-1 and B-2 provides a workable solution to the drainage issues created by the development of this property and should be approved as satisfying the requirements for Preliminary Plat drainage report and rough grading approval.

HYDROLOGY - FORMULAS USED

FROM SECTION 22.2 OF DPM - JANUARY 93 UPDATE

EXISTING CONDITIONS:

$$\text{TIME OF CONCENTRATION, } t_c = \left(\frac{L_1}{V_1} + \frac{L_2}{V_2} + \dots + \frac{L_x}{V_x} \right) / 3600 \text{ sec/hr}$$

$$\text{WHERE } V = K \sqrt{S}$$

K FROM TABLE B-1

S IS SLOPE IN PERCENT

$L_1 + L_2 + \dots + L_x \leq 4000 \text{ FT}$

$$\text{INTENSITY, } I = 0.726 (\log(24.6 \times t_c)) P_{60}$$

$$\text{RATIONAL METHOD "C"} = \%A(.27) + \%B(.43) + \%C(.61) + \%D(.93) \\ \text{(ZONE 1, 100 YR, 6 HR STORM)}$$

$$Q_p = CIA$$

DEVELOPED CONDITIONS

FOR SMALL WATERSHEDS $t_p = 8 \text{ MINUTES}$

$t_c = 12 \text{ MINUTES}$

$$\text{RATIONAL METHOD "C"} = \%A(.27) + \%B(.43) + \%C(.61) + \%D(.93) \\ \text{(ZONE 1, 100 YR, 6 HR STORM)}$$

$$\text{"C"} = \%A(.08) + \%B(.24) + \%C(.47) + \%D(.92) \\ \text{(ZONE 1, 10 YR, 6 HR STORM)}$$

$$\text{EXCESS PRECIPITATION, } E_c = \%A(.44) + \%B(.67) + \%C(.99) + \%D(1.97)$$

$$\text{VOLUME} = \text{AREA}(E_c)$$



BOHANNAN-HUSTON INC.

PROJECT NAME TRACTS A&D

SHEET _____ OF _____

PROJECT NO. C9221740

BY PP DATE 3/31/04

SUBJECT HYDROLOGY

CH'D _____ DATE _____

FULLY DEVELOPED CONDITIONS

SUMMARY OF HYDROLOGIC DATA												
BASIN ID	AREA AC	AREA SQ.ML	% LAND TREATMENT			TIME TO PEAK	10-YR DISCHARGE		RATIONAL METHOD (100YR)		I (IN/HR)	Q(100YR) (CFS)
			A	B	C		CFS/AC	CFS	Q	Q		
1-A	2.455	0.0038	3.7	25.8	25.8	44.6	1.88	4.6	0.69	4.70	4.70	8.0
1-B	2.878	0.0045	3.2	23.4	23.4	49.9	1.98	5.7	0.72	4.70	4.70	9.7
1-C	1.532	0.0024	4.8	17.3	17.3	60.5	2.15	3.3	0.76	4.70	4.70	5.4
1-D	3.214	0.0050	4.9	19.0	19.0	57.2	2.09	6.7	0.74	4.70	4.70	11.2
1-E	1.502	0.0023	4.3	19.9	19.9	55.9	2.07	3.1	0.74	4.70	4.70	5.2
1-F	3.727	0.0058	4.9	17.7	17.7	59.6	2.13	8.0	0.75	4.70	4.70	13.2
2-A	3.555	0.0056	4.1	19.8	19.8	56.3	2.08	7.4	0.74	4.70	4.70	12.4
2-B	2.662	0.0042	3.8	20.4	20.4	55.4	2.07	5.5	0.74	4.70	4.70	9.2
2-C	3.382	0.0053	4.3	21.0	21.0	53.7	2.03	6.9	0.73	4.70	4.70	11.6
2-D	3.645	0.0057	4.3	20.7	20.7	54.2	2.04	7.5	0.73	4.70	4.70	12.5
2-E	2.522	0.0039	4.0	18.5	18.5	59.1	2.13	5.4	0.75	4.70	4.70	8.9
2-F	3.945	0.0062	4.4	20.8	20.8	54.0	2.04	8.0	0.73	4.70	4.70	13.5

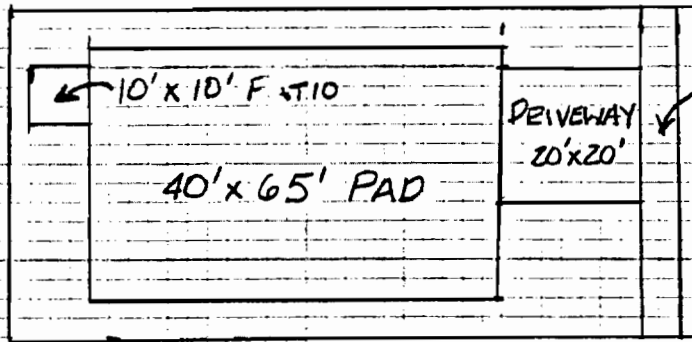
EXISTING CONDITIONS

100-YEAR STORM							RATIONAL			
<u>BASIN</u> <u>ID</u>	<u>AREA</u> <u>AC</u>	<u>AREA</u> <u>SQ.MI.</u>	<u>A</u>	<u>% LAND TREATMENT</u>		<u>D</u>	<u>TIME OF</u> <u>CONCENT</u>	<u>COMPOSITE</u> <u>C</u>	<u>I</u> <u>(IN/HR)</u>	<u>Q</u> <u>(CFS)</u>
E-1	73.0	0.1141	100.0	0.0	0.0	0.0	0.20	0.27	3.68	72.5
E-3	56.6	0.0884	100.0	0.0	0.0	0.0	0.20	0.28	4.70	74.5

IMPERVIOUS AREA CALCULATIONS

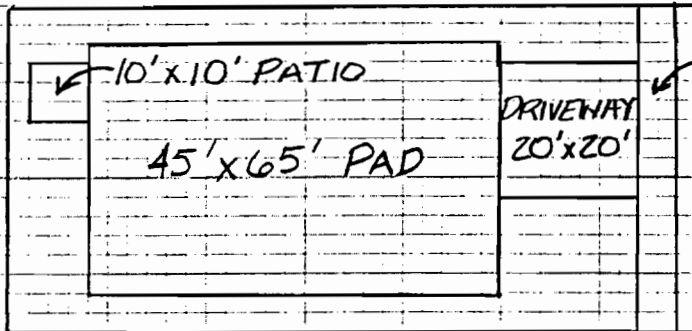
BASIN ID	AREA TYPED AC	PERCENT TYPE D	LOT WIDTH (IN FEET)						50' sq.ft/lot	55'	60'	TOTAL NUMBER OF LOTS PER BASIN				80'	ROADWAY	TYPE 1 sq.ft/ft	TOTAL LENGTH OF ROADWAY PER BASIN			TYPE 4 sq.ft/ft	CUL 1
			50'	55'	60'	TOTAL NUMBER OF LOTS PER BASIN		80'				TYPE 2	TYPE 3	TYPE 4									
						65'	70'																
1-A	1.09	44.6	5	5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	220	1	
1-B	1.44	49.9	7	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	124	450	1	
1-C	0.93	60.5	4	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	350	0	
1-D	1.84	57.2	5	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	550	0	
1-E	0.84	55.9	5	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	320	0.25	
1-F	2.22	59.6	14	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	762	0.25	
2-A	2.00	56.3	0	9	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	700	0.25	
2-B	1.48	55.4	0	2	9	0	0	0	0	0	0	0	0	0	0	0	0	0	113	400	0		
2-C	1.81	53.7	0	7	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	350	1	
2-D	1.98	54.2	0	6	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	530	0.25	
2-E	1.49	59.1	0	9	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	530	1	
2-F	2.13	54.0	0	11	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	440	1	
			44	46	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			

50' LOT



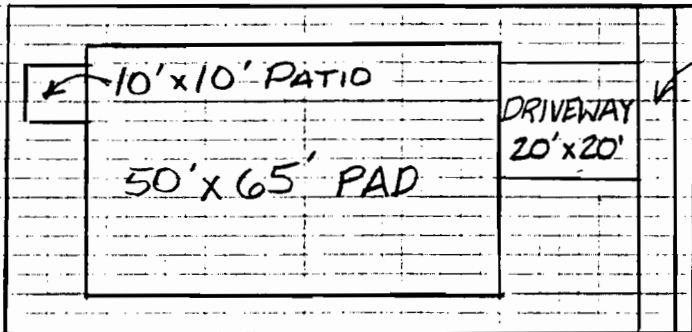
50' LOT TOTAL
IMPERVIOUS AREA = 3300 ^{sq ft}

55' LOT



55' LOT TOTAL
IMPERVIOUS AREA = 3645 ^{sq ft}

60' LOT



60' LOT TOTAL
IMPERVIOUS AREA = 3990 ^{sq ft}



BOHANNAN-HUSTON INC.

PROJECT NAME TRACTS A & D

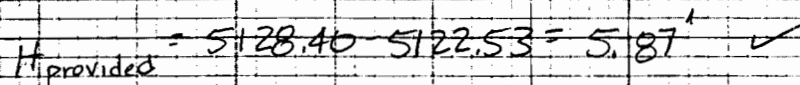
SHEET 1 OF 2

PROJECT NO. 9321740

BY PR DATE

SUBJECT HYDROLOGY

CH'D DATE

$$TC = 5129.73$$


DATE

GRATE 1A

CAPACITY OF SINGLE "A" CATCH BASIN IN SUMP

ORIFICE EQUATION

$$Q = 0.6 A_{\text{NET}} \sqrt{2gH}$$
$$A_{\text{NET}} = \frac{31 \times 18.5}{144} = 3.98 \text{ FT}^2$$

$$H = 0.83^{1.44} (10")$$

$$Q = 17.5 \text{ CFS}$$

WEIR EQUATION

$$Q = 2.68 P_{\text{NET}} H^{1.5}$$

$$P_{\text{NET}} = \frac{2(18.5) + 31}{12} = 5.67$$

$$H = 0.83^{1.2} (10" \text{ CURB})$$

$$Q = 11.5 \text{ CFS}$$

$$\text{NEED } Q_{\text{CAP}} = 8.0 (1.15) = 9.2 \text{ CFS}$$

↳ clogging
factor



BOHANNAN-HUSTON INC.

PROJECT NAME _____ SHEET _____ OF _____

PROJECT NO. _____ BY _____ DATE _____

SUBJECT _____ CH'D _____ DATE _____

OUTLET IC: PIPE TO CHANNEL CONNECTION

STORM INLETS:

$$Q_{100} = 44.7 \text{ CFS}$$

DESIGN FOR 200% IN SUMP = 89.4 CFS

USE QUADRUPLE TYPE "A" WITH 4 GRATES & WINGS AT EACH END:



CAPACITY OF ORIFICE: $Q = 0.6 A \sqrt{2gh}$

GRATES: $A_{NET} = 4 [31 \times 18.5 / 144] = 15.9 \text{ SF}$

$$H = 0.83 + 0.18 = 1.0' \text{ @ RIGHT OF WAY}$$

$$Q = 0.6 (15.9) \sqrt{2(32.2)(1)} = 76.6 \text{ CFS}$$

WINGS: $A_{NET} = 2(3.5)(6 \text{ in}) / 12 = 3.5 \text{ SF}$

$$H = 0.74'$$

$$Q = 0.6 (3.5) \sqrt{2(32.2)(0.74)} = 14.5 \text{ CFS}$$

$$\text{TOTAL CAPACITY} = 76.6 + 14.5 = \underline{91.1 \text{ CFS}} > 89.4 \checkmark$$

PIPE TO CHANNEL:

USE 42" RCP - RATING CURVE ATTACHED

NORMAL DEPTH = 6.03'

CHECK ORIFICE OF PIPE: $A = \pi (1.75)^2 = 9.62 \text{ SF}$

$$h = 1 + 6.78 - 3.5/2 = 6.03' \quad Q = 0.6 (9.62) \sqrt{2g(6.03)} = 113 \text{ CFS} > 89.4 \checkmark$$



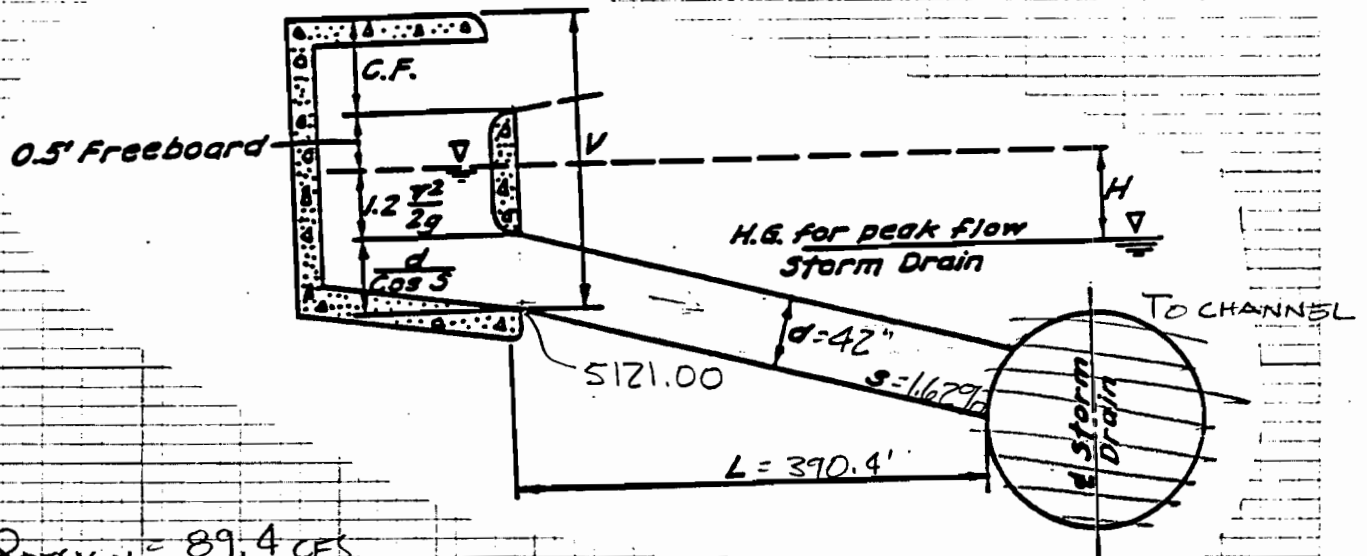
BOHANNAN-HUSTON INC.

PROJECT NAME SEVEN BAR NORTH SHEET _____ OF _____
PROJECT NO. C9321740 BY PR DATE _____
SUBJECT _____ CH'D _____ DATE _____

CATCH BASIN DEPTH:

STA 5+49.15
TC=5127.78

QUAD TYPE "A" IN SUMP



$$Q_{\text{DESIGN}} = 89.4 \text{ CFS}$$

$$A_{42"} = \pi (1.75)^2 = 9.62 \text{ SF}$$

$$V = Q/A = 9.29 \text{ FPS} \Rightarrow 1.2 \frac{V^2}{2g} = 1.61'$$

$$V_{\text{DEPTH, MIN}} = 1.33 + 1.61 + 3.5 = 6.44'$$

$$\text{DEPTH PROVIDED} = 5127.78 - 5121.00 = 6.78' > 6.44' \checkmark$$



BOHANNAN-HUSTON INC.

PROJECT NAME SEVEN BAR NORTH

SHEET _____ OF _____

PROJECT NO. 19321740

BY PZ DATE _____

SUBJECT DRAINAGE

CH'D _____ DATE _____

BACKWATER CHECK, CHANNEL AT PEAK

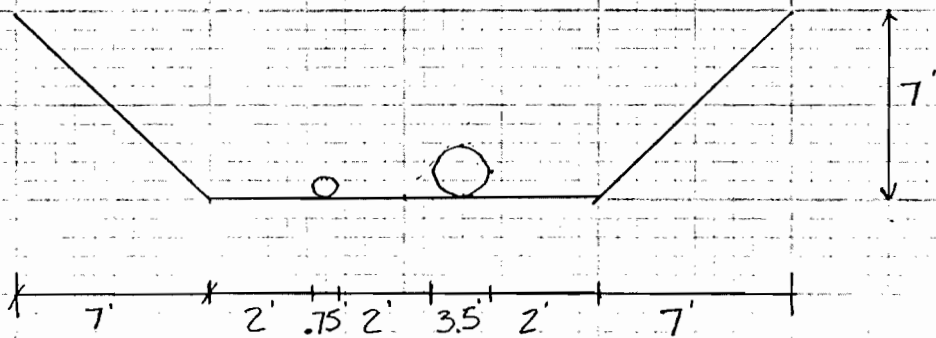
MAX DEPTH IN CHANNEL ($\pm$ STA 7+20) = 5.75'

CHANNEL INVERT = 5113.68

WATER SURFACE @ 5119.43 < 5121 ✓

AT THE PEAK FLOW IN SEVEN BAR CHANNEL, THE MINOR FLOWS FROM THE DEVELOPMENT WILL ENTER THROUGH CATCH BASIN.

CHECK TRENCH:



TOTAL WIDTH REQ'D = 24.25 < 25 ✓



BOHANNAN-HUSTON INC.

PROJECT NAME SEVEN BAR NORTH SHEET _____ OF _____
PROJECT NO. C9321746 BY PR DATE _____
SUBJECT _____ CH'D _____ DATE _____

OUTLET PIPE AT BASIN 1C

CULVERT RATING TABLE

42. INCH DIAMETER PIPE

N = 0.01300 INCREMENT = 1.00 SLOPE = 0.01620

FLOW DEPTH (IN)	FLOW AREA (SQ FT)	DISCHARGE (CFS)	VELOCITY (FPS)
1.00000	0.05957	0.12525	2.10244
2.00000	0.16728	0.55406	3.31225
3.00000	0.30503	1.31374	4.30691
4.00000	0.46609	2.41279	5.17663
5.00000	0.64640	3.85195	5.95910
6.00000	0.84309	5.62740	6.67470
7.00000	1.05400	7.73216	7.33602
8.00000	1.27735	10.15689	7.95153
9.00000	1.51167	12.89037	8.52726
10.00000	1.75567	15.91981	9.06768
11.00000	2.00821	19.23116	9.57625
12.00000	2.26829	22.80913	10.05565
13.00000	2.53496	26.63742	10.50802
14.00000	2.80736	30.69880	10.93512
15.00000	3.08467	34.97512	11.33837
16.00000	3.36612	39.44738	11.71893
17.00000	3.65099	44.09579	12.07777
18.00000	3.93855	48.89979	12.41570
19.00000	4.22811	53.83798	12.73335
20.00000	4.51900	58.88823	13.03124
21.00000	4.81056	64.02759	13.30980
22.00000	5.10212	69.23224	13.56932
23.00000	5.39301	74.47753	13.81001
24.00000	5.68258	79.73788	14.03200
25.00000	5.97013	84.98666	14.23530
26.00000	6.25500	90.19618	14.41986
27.00000	6.53645	95.33746	14.58551
28.00000	6.81376	100.38007	14.73196
29.00000	7.08616	105.29201	14.85883
30.00000	7.35283	110.03918	14.96556
31.00000	7.61291	114.58525	15.05145
32.00000	7.86545	118.89076	15.11556
33.00000	8.10945	122.91258	15.15671
34.00000	8.34377	126.60252	15.17331
35.00000	8.56712	129.90555	15.16327
36.00000	8.77802	132.75681	15.12377
37.00000	8.97472	135.07658	15.05079
38.00000	9.15503	136.76060	14.93831
39.00000	9.31609	137.65956	14.77654
40.00000	9.45384	137.52634	14.54714
41.00000	9.56155	135.82037	14.20485
42.00000	9.62112	128.05524	13.30980

Q = 89.4 CFS

OUTLET 2A

$$Q = 68.1 \text{ CFS}$$

WEIR IS @ STA 3+61.93, 57.65' LT

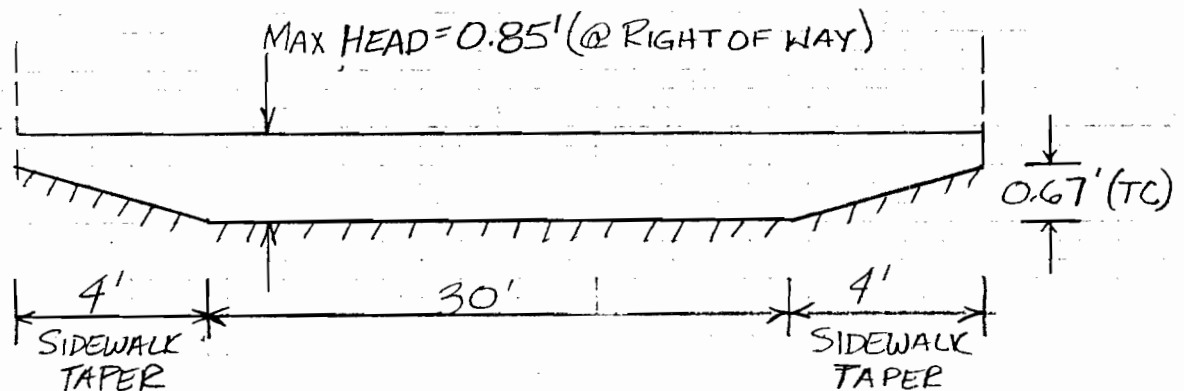
$$H = 44.17 - (57.65 - 13) 0.02 = \underline{5143.28}$$

7 BAR CHANNEL INVERT @ STA 15+73.24 (7.92' LT)

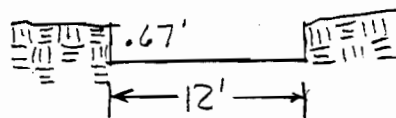
$$= 5132.21$$

$$\text{TOP OF CHANNEL} = 5132.21 + 6 = 5138.21$$

WEIR X-SECTION: DEPTH = 0.83' FOR $Q = 68.1 \text{ CFS}$



CHANNEL X-SECTION:



BOHANNAN-HUSTON INC.

PROJECT NAME _____ SHEET _____ OF _____
PROJECT NO. _____ BY _____ DATE _____
SUBJECT _____ CH'D _____ DATE _____

TREATMENT OF EXISTING FLOWS

THE UPSTREAM, UNDEVELOPED BASIN E-3 HAS THE FOLLOWING CHARACTERISTICS:

AREA = 56.6 ACRES

%A = 95

%B = 5

$t_c = 0.20$ HRS

$I = 4.44$ $\frac{1}{4}$ IN/HR

$E = 0.452$

$Q_{100} = 74.5$ CFS

$V_{100} = 2.13$ AC-FT

① CONVEY FLOWS IN AN EARTHEN SWALE ADJACENT TO THE NORTHERN BOUNDARY OF TRACT B-2 AND SIERRITA RD.

MANHATTAN "n" = 0.030

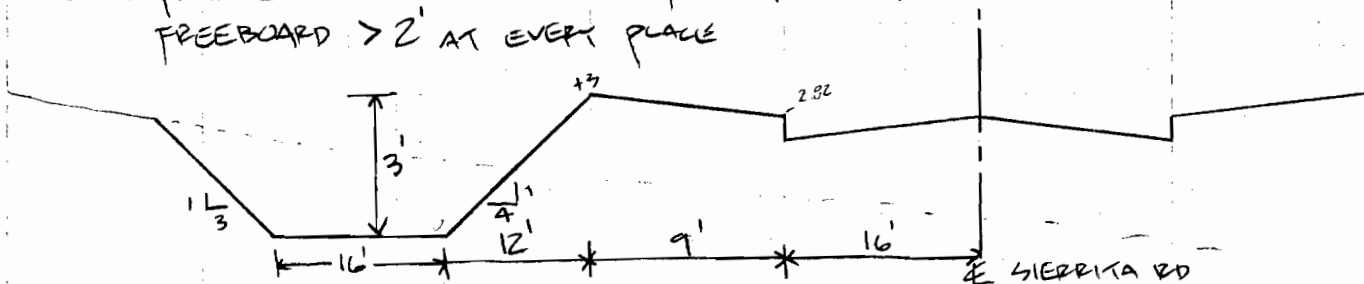
MAX. STREET SLOPE IN SIERRITA = MAX SWALE SLOPE = 6.163%

TO KEEP VELOCITY IN SWALE < 8 FPS, USE A BOTTOM WIDTH = 16' AND SIDE SLOPES @ 4:1 & 3:1 - SEE ATTACHED STREAM OUTPUTS FOR $s = 6.163\% \times 3.70\%$

FOR $s = 6.163\%$ VEL = 7.7 FPS, $d = 0.55'$

FOR $s = 3.7\%$ VEL = 6.6 FPS, $d = 0.64'$

PROVIDE A LINED HEIGHT OF 3', GIVING A FREEBOARD > 2' AT EVERY PLACE



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PROJECT NAME KEYEN BAR NORTH

SHEET 1 OF

PROJECT NO. 93217.43

BY DATE

SUBJECT TRACTS B-1 & B-2

CH'D DATE

② SEDIMENT POND

PROVIDE A SEDIMENTATION, DETENTION POND AT THE CORNER OF SEVEN BAR LOOP ROAD AND SIERRITA ROAD TO ACCEPT FLOWS FROM THE SWALE IN ① AND DISCHARGE INTO THE STORM DRAIN IN SIERRITA ROAD

$$\begin{aligned}\text{FLOW INTO POND} &= 74.5 \text{ cfs} \\ \text{VOLUME} &= 2.13 \text{ AC-Ft} = 92,867 \text{ Ft}^3\end{aligned}$$

ASSUME FLOWS ENTER AN ORIFICE CONTROLLED 18" OUTLET THAT ENTERS INTO THE SD MANHOLE @ STA. 10+32.91 (SIERRITA ROAD)

2A - POND SIZE BASED ON SETTLING VELOCITY (V_s)

- ASSUME:
- DESIGN PARTICLE: VERY FINE SAND ($D = 0.06 \text{ mm}$)
 - 100% REMOVAL OF DESIGN PARTICLE FOR 10-YEAR STORMS
 - $V_s = 0.009 \text{ FPS}$ FOR VERY FINE SAND

$$\text{SURFACE AREA} = SA = (1.2)(Q_0)/V_s$$

$$\begin{aligned}\text{WHERE } Q_0 &= 10\text{-YEAR PEAK FLOW RATE} \\ &= 14.8 \text{ cfs}\end{aligned}$$

$$SA = (1.2)(14.8)/(0.009) = 1,970 \text{ SF}$$

$$\text{ASSUME POND LENGTH} = 3 \times \text{POND WIDTH} = 3W$$

$$\text{OR } (3W)(W) = 1970 \text{ SF}$$

$$\begin{aligned}W &= 26' \\ L &= 77'\end{aligned}$$



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PROJECT NAME	SEVEN BAR NORTH	SHEET	2	OF	
PROJECT NO.	93217.43	BY		DATE	
SUBJECT	TRACTS B-1 & B-2	CH'D		DATE	

ZP3 - Pond SIZED BASED ON SEDIMENT STORAGE

- FROM LKLE SPREADSHEET (ATTACHED), THE AVERAGE ANNUAL SEDIMENT YIELD FOR BASIN E-3 IS 286CY OR 7732CF

ASSUME: MAXIMUM SEDIMENT STORAGE DEPTH = 3'
MINIMUM SETTLING DEPTH = 2'

USING SA = 1,970SF FROM ABOVE WHERE THE VOLUME IS A FUNCTION OF THE DEPTH Z

$$\text{BOTTOM AREA} = (77')(26') = 2002 \text{ FT}^2$$

$$\text{TOP AREA} = (2002 + 618Z + 36Z^2) \text{ FT}^2$$

$$\text{Volume} = \frac{(\text{BOTTOM AREA}) + (\text{TOP AREA})}{2} Z$$

$$\text{Volume} = 2002Z + 309Z^2 + 18Z^3$$

FOR SEDIMENT VOLUME = 7,732CF * SOLVING FOR Z:

$$Z = 2.63' < 3'$$

SEDIMENT STORAGE DEPTH = 2.63'

POND VOLUMETRICS

- ASSUMING THAT THE POND OUTFLOW IS ORIFICE CONTROLLED AND THE OUTFLOW PIPE $\phi = 18"$

- FROM SITE GEOMETRY: POND INVERT = 5148

POND TOP = 5153

POND DEPTH = 5'

POND VOLUME = 19,985 FT^3 = 0.459 AC-FT

VOLUME IN = 92,783 FT^3 = 2.13 AC-FT

$Q_{in} = 74.5 \text{ cfs}$



BOHANNAN-HUSTON INC.

PROJECT NAME SEVEN PACE NORTH SHEET 3 OF
PROJECT NO. 93217.43 BY DATE
SUBJECT TRAILS B-1 & B-2 CH'D DATE

POND VOLUMETRICS (CONT'D)

FOR A POND: $V_{\text{PONDED}} = \left(\frac{V_{\text{TOTAL}}}{Q_{\text{IN}}^2} \right) Q_{\text{OUT}}^2 - (D_{\text{URATION}}) Q_{\text{OUT}} + V_{\text{TOTAL}}$

WHERE $D_{\text{URATION}} = \frac{2V_{\text{TOTAL}}}{Q_{\text{IN}}} = \frac{2(92,783 \text{ FT}^3)}{74.5 \text{ cfs}} = 2491 \text{ sec.}$

SO $19,985 = \left(\frac{92,783}{(74.5)^2} \right) Q_{\text{OUT}}^2 - (2491) Q_{\text{OUT}} + 92,783$

OR $16.72 Q_{\text{OUT}}^2 - 2491 Q_{\text{OUT}} + 72,798 = 0$

OR $Q_{\text{OUT}} = 39.9 \text{ cfs}$ TO MAINTAIN POND VOLUMETRICS

ORIFICE CONTROL:

1) ASSUME OUTLET = 18"

IF $Q = 0.6 A \sqrt{2gh}$

$$h = \frac{Q^2}{(0.72) A^2 g} = \frac{(39.9)^2}{(0.72)(1.767)^2 32.2} = 22' \text{ HEAD}$$

18" ϕ PIPE INSUFFICIENT

2) ORIFICE REQUIRED FOR HEAD = $S' - \text{SEDIMENT STORAGE DEPTH}$
 $= S' - 2.3' = 2.37'$

$$\begin{aligned} A &= \frac{Q}{0.6 \sqrt{2gh}} = \frac{39.9}{0.6 \sqrt{2(32.2)(2.37)}} \\ &= 5.38 \text{ FT}^2 \\ &= 31.4" \phi \end{aligned}$$

$\therefore$ USE A 36" CMP STANDPIPE WITH AN ORIFICE PLATE INSTALLED WITH A 31.4" ϕ HOLE IN IT.



BOHANNAN-HUSTON INC.

PROJECT NAME SEVEN BAR NORTH SHEET 4 OF
PROJECT NO. 93217.43 BY DATE
SUBJECT TRACTS B-1 & B-2 CH'D DATE

CONNECTOR PIPE

- DISCHARGE INTO MANHOLE ON SIERRITA ROAD: (STA 10+32.91)

MH #SD2441: INV = 5142.52

ASSUME CMP PROJECTS 3' BELOW POND OR INV = 5145.00

L CONNECTOR = 97'

∴ SLOPE = 2.56%

MIN ϕ = 25" < 36"

- USE 36" RCP TO MINIMIZE TRANSITION

- AFTER CMP STAND PIPE, TRANSITION TO 36" RCP



BOHANNAN-HUSTON INC.

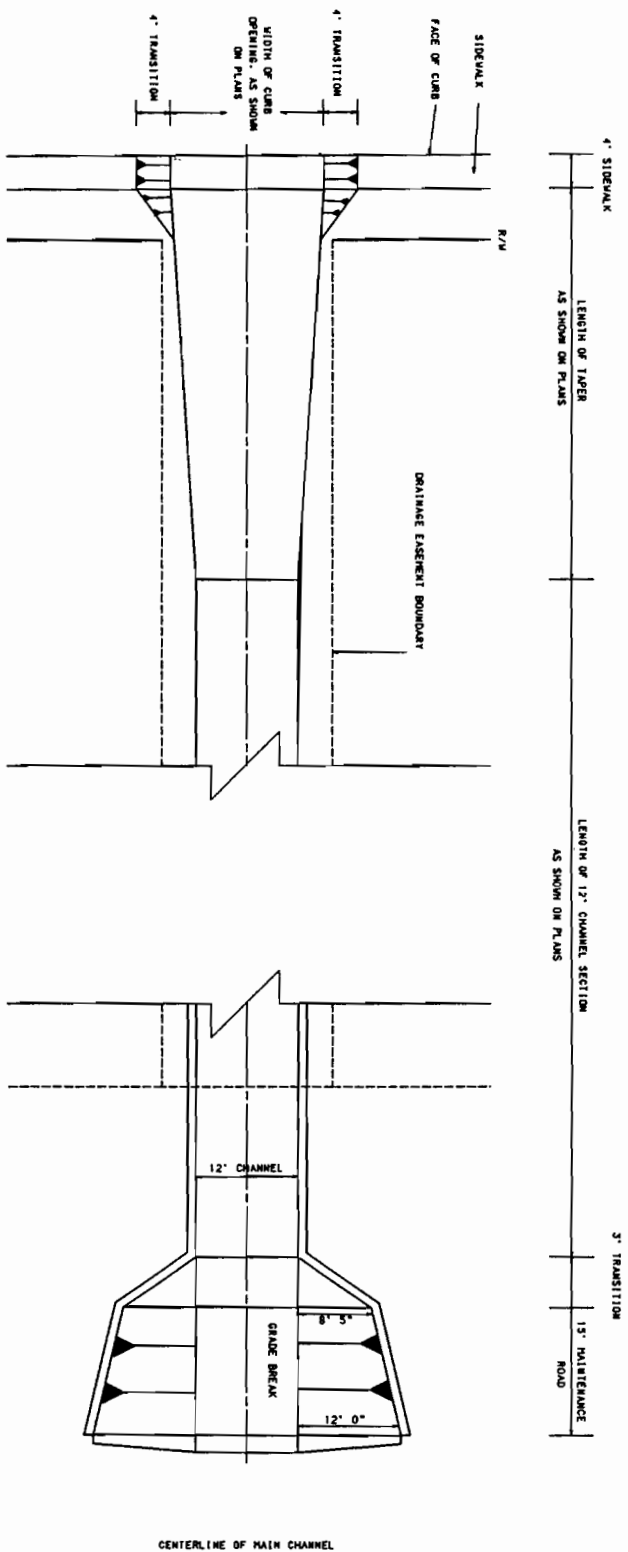
PROJECT NAME KEVEN BAR RANCH SHEET 5 OF
PROJECT NO. 9321743 BY DATE
SUBJECT TRAILS B-1 & B-2 CH'D DATE

SEVEN BAR RANCH NORTH SEDIMENT YIELD ANALYSIS
UNIVERSAL SOIL LOSS EQUATION

DESCRIPTION	VARIABLE	UNIT	
BASIN			E-3
Drainage Area	DA	Sq. Mi.	0.088
Slope	S	Ft/Ft	0.050
Slope Angle	THETA	Radians	0.050
	L	Feet	1900.000
Rainfall	R		25.000
Soil Erodability*	K		0.240
Slope Length Factor	LS		1.682
Cover*	C		0.170
Support Practice Factor	P		1.000
Sediment Yield	A	Tons/Acre	1.716
		Tons	96.649
		Cy	71.591
Estimated Soil Unit Weight	100.000	Lbs/Cf	Total Annual Sediment Yield
			71.591 Cy
			4.000

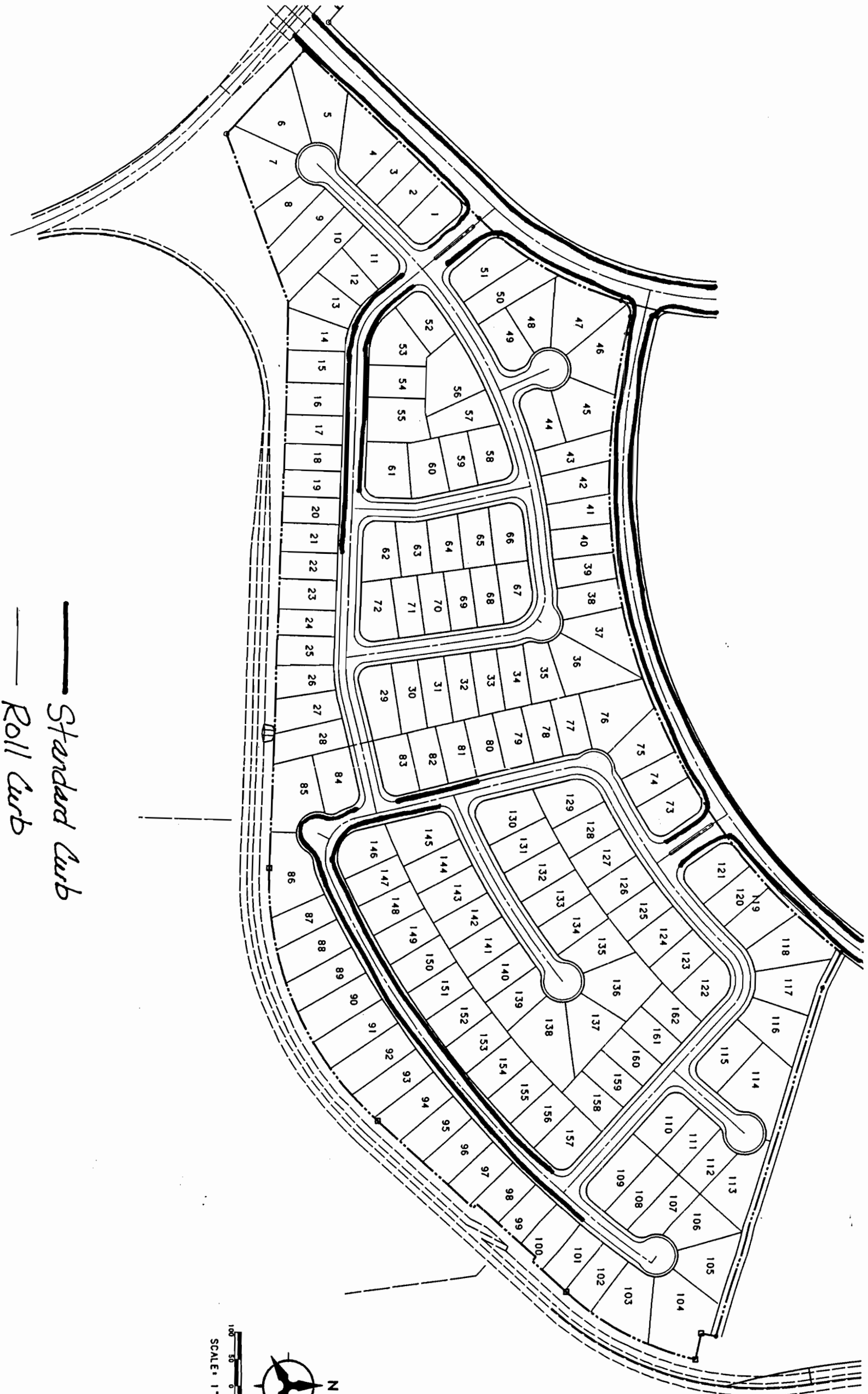
			Adjusted Sediment Yield
			286.366 Cy
			7731.880 Cf

NOTE: The Universal Soil Loss Equation typically underestimates the actual sediment yield by 4 times so a factor of 4 is applied to the total annual sediment yield.



OUTFLOW CHANNEL PLAN VIEW

CITY OF ALBUQUERQUE PUBLIC WORKS DEPARTMENT ENGINEERING GROUP		SEVEN BAR RANCH NORTH OUTFLOW STRUCTURE DETAILS	
APPROVALS	ENGINEER	DATE	APPROVALS
ONE CHAIRMAN			WATER
TRANSFORMATION			WASTE WATER
HYDROLOGY			
DRAWING NO.	XXXX	MAP NO.	A-13
		SHEET	X OF X
DESIGNED BY PR. OF DATE 5/94 DRAWN BY TSG DATE 5/94 CHECKED BY JRT DATE 5/94		ENGINEER'S SEAL SURVEY INFORMATION FIELD NOTES NO. BY DATE TBM NO. 205 CHISLED "X" LOCATED APPROXIMATELY 459 FEET SOUTH OF THE BLACK'S DIVERSION INLET STRUCTURE ON THE EAST WALL. ELEV. 5110.55	
NO. DATE REMARKS BY REVISIONS DESIGN		BENCH MARKS AS-BUILT INFORMATION CONTRACTOR STARTED BY INSPECTOR'S ACCEPTANCE BY DATE FIELD VERIFICATION BY DATE DRAWING CORRECTED BY DATE MICRO-FILM INFORMATION RECORDED BY DATE NO.	



SCALE: 1" = 100'



CITY OF ALBUQUERQUE

PUBLIC WORKS DEPARTMENT

ENGINEERING GROUP



SEVEN BAR RANCH
CURB TYPE IDENTIFICATION MAP

APPROVALS	ENGINEER	DATE	APPROVALS	ENGINEER	DATE
DEC CHAIRMAN			WATER		
TRANSPORTATION			WASTE WATER		
HYDRA. DEPT					
DRAWING NO.	XXXX	MAP NO.	A-13	SHEET	1 OF 1

ENGINEER'S SEAL			SURVEY INFORMATION			BENCH MARKS			AS-BUILT INFORMATION		
			FIELD NOTES			TBM NO. 205			CONTRACTOR		
			NO.	BY	DATE	CHISELED "X" LOCATED APPROXIMATELY 459 FEET SOUTH OF THE BLACK'S DIVERSION INLET			WORK STAKED BY		
						STRUCTURE ON THE EAST WALL.			INSPECTOR'S ACCEPTANCE BY		
						ELEV. 5110.55			FIELD LOCATION BY		
									DRAWINGS CORRECTED BY		
									MICRO-FILM INFORMATION		
									RECORDED BY		
									NO.		

NO.	DATE	REMARKS	BY
REVISIONS			
DESIGN			
DESIGNED BY	PR. OF	DATE 5/94	
DRAWN BY	TSG. OF	DATE 5/94	

