

# **DRAINAGE REPORT FOR TRACTS B-4, B-5 & B-6 SEVEN BAR NORTH SUBDIVISION**

Prepared for:

**BROWN/NZD DEVELOPMENT JOINT  
VENTURE  
C/O BROWN & ASSOCIATES  
3411 CANDELARIA NE  
ALBUQUERQUE, NEW MEXICO 87107**

Prepared by:



**BOHANNAN-HUSTON INC.**

ENGINEERS ARCHITECTS PHOTOGRAHAMETRISTS SURVEYORS

COURTYARD I, 7500 JEFFERSON NE ALBUQUERQUE, NM 87109 TEL (505) 823-1000 FAX (505) 821-0892

**Job No. 93217.43**

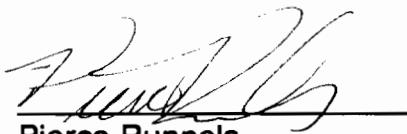
Drainage Report  
for  
Tracts B-4, B-5 & B-6  
Seven Bar North Subdivision

October 1994

Prepared for:

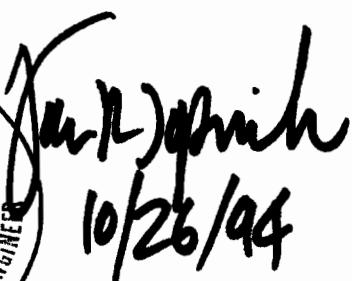
BROWN/NZD DEVELOPMENT JOINT VENTURE  
C/O BROWN & ASSOCIATES  
3411 CANDELARIA NE  
ALBUQUERQUE, NEW MEXICO 87107

Prepared by:



Pierce Runnels

Under the Supervision of:



Jar-L) Smith  
10/26/94

James Topmiller, P.E.

## TABLE OF CONTENTS

	Page
I. INTRODUCTION/PURPOSE OF REPORT .....	1
II. STUDY METHODOLOGIES .....	1
III. EXISTING CONDITIONS .....	2
Site Characteristics .....	2
Onsite Drainage Basins .....	2
Offsite Drainage Basins .....	3
IV. PROPOSED DEVELOPED CONDITIONS .....	3
Unit 4 Development .....	4
Unit 5 & 6 Development .....	5
Backyard Ponding .....	6
Offsite Basins .....	6
V. PHASING/BUILDING PERMIT/FINAL PLAT APPROVALS .....	6
VI. CONCLUSION .....	7

## APPENDICES

### APPENDIX 1 HYDROLOGY/FLOWRATE CALCULATIONS

#### EXISTING DRAINAGE CONDITIONS

#### PROPOSED DRAINAGE CONDITIONS

### APPENDIX 2 STREET FLOW CAPACITY CALCULATIONS

### APPENDIX 3 HYDRAULIC DESIGN CALCULATIONS

#### UNIT 4 OUTFLOW

#### STORM DRAIN

#### UNIT 5 OUTFLOW

### APPENDIX 4 OFFSITE FLOW/DETENTION POND CALCULATIONS

## PLATES

- 1 EXISTING DRAINAGE CONDITIONS MAP
- 2 DRAINAGE MASTER PLAN(FROM REPORT, JUNE 6, 1994)
- 3 DRAINAGE PLAN & ONSITE BASIN MAP (Proposed Developed Conditions)
- 4 SUBDIVISION SITE GRADING AND DRAINAGE PLAN - SHEET 1 OF 3
- 5 SUBDIVISION SITE GRADING AND DRAINAGE PLAN - SHEET 2 OF 3
- 6 SUBDIVISION SITE GRADING AND DRAINAGE PLAN - SHEET 3 OF 3
- 7 PRELIMINARY PLAT (For Tracts B-4, B-5 and B-6)
- 8-16 STORM DRAIN PLAN & PROFILE SHEETS
- 17 CURB TYPE IDENTIFICATION MAP

## **I. INTRODUCTION/PURPOSE OF REPORT**

This report presents the Drainage Management Plan for Preliminary Plat and rough grading approval for the development of Tracts B-4, B-5 and B-6 of the Seven Bar North Subdivision. The property is 45.5 acres, currently zoned R-1 and the proposed development is for 182 lots of detached, single family residential housing and the related streets and infrastructure. As shown on the location map on the Drainage Basin Map, the property is bounded by Seven Bar Loop Road on the east, Westside Boulevard on the north, undeveloped, vacant land on the west, and Black's Arroyo on the south.

The report outlines the study methodologies used and summarizes the existing and proposed drainage conditions. Calculations and supporting data are presented in the appendices. A drainage basin map, a preliminary grading plan and a copy of the Preliminary Plat are included in the Plates at the end of the report. The purpose of this report is to obtain drainage report approval for the Preliminary Plat for Tracts B-4, B-5 and B-6, and rough grading approval.

## **II. STUDY METHODOLOGIES**

Undeveloped, existing conditions and proposed, developed conditions were analyzed for the 100-year, 6-hour storm event consistent with the City of Albuquerque Design Process Manual (DPM), including the January, 1993 revision of Section 22.2, Hydrology. The hydrology was also analyzed with the AHYMO Computer Program (AMAFCA Hydrologic Model). The analysis also references the previously submitted Drainage Master Plan for the Seven Bar North Subdivision, dated April, 1994 and revised June 6, 1994, and is consistent with that report.

Street hydraulics and channel capacities were analyzed using Manning's equation with the Manning's "n" values suggested in the DPM. Rating curves for

streets and channels are provided in the Appendices, along with all hydrologic and hydraulic calculations. Streets are designed to convey the energy grade line of the design storm event within the right-of-way. Normal flow depth is confined to the top of curb. Pipe hydraulics provided are for pressure flow conditions and are analyzed by computer methods.

### **III. EXISTING CONDITIONS**

#### **Site Characteristics**

This site is currently undeveloped vacant land with slopes ranging from 2% to 8% in a generally southern direction. Soils are highly absorptive sandy soils with occasional clay lenses. Vegetation is light, consisting of grasses and small sagebrush.

The site is not located within a FEMA floodplain, as shown on the Floodplain Map provided on the Drainage Master Plan (enclosed in the rear of this report).

The existing drainage conditions are shown graphically on the "Existing Drainage Conditions" map and are summarized as follows:

#### **Onsite Drainage Basin**

Tracts B-4, B-5 and B-6, a total drainage basin of approximately 45.5 acres, currently drains to the south in primarily sheet flow, where it discharges in a concrete rundown into the Black's Arroyo Channel. The 100-year storm event currently generates 45.9 cfs of runoff from this basin.

## **Offsite Drainage Basins**

Two off-site basins drain directly into the proposed development. The first basin(OFF1) lies north of Westside Boulevard in the City of Rio Rancho and generates a total of 24.9 cfs under the developed conditions. The flow is conveyed by CMP to Westside Boulevard, where it will be intercepted by the storm drain system in Seven Bar Loop Road. The appendix to the Drainage Master Plan provides the text and basin information excerpted from the Rio Rancho Special Assessment District Drainage Report prepared by Wilson & Company. Basin E-1 is approximately 23.8 acres and generates approximately 28.5 cfs which drains in sheet flow to the Seven Bar Loop Road right-of-way, where it continues south to the Black's Arroyo channel.

*CHECK ON  
METHOD USE  
TD CALC. 24.*

Basins E-2 and E-3 do not drain onto Tracts B-4, B-5 & B6, but they are part of the Seven Bar North Subdivision and affect the pond calculations presented in Appendix 4. Both basins flow into the existing temporary drainage pond in the northeast corner of the Seven Bar Loop Road/Sierrita Road intersection.

Basin E-2 is approximately 36.0 acres, has 29.9 cfs of runoff in the 100-year storm and flows into the existing temporary drainage pond in the northeast corner of the Seven Bar Loop Road/Sierrita Road intersection. Basin E-2 drains in sheet flow to the channel on the north side of Sierrita Road, where it collects and is conveyed to the pond. Basin E-3, which is 19.0 acres and generates 23.9 cfs of runoff, runs in sheet flow to the northern boundary of the developed area of Units 1 and 2, and is conveyed by the V-ditch to the channel on the north side of Sierrita Road.

## **IV. PROPOSED DEVELOPED CONDITIONS**

The proposed development is a single-family, detached-unit residential subdivision with 182 lots on 45.5 acres, producing a density of 4.00 D.U. per acre.

Proposed street configurations are shown on the Preliminary Plat, the Drainage Basin Map and on the Preliminary Grading Plan. For drainage, the development can be broken into two major areas. The first area is Unit 4 and the second is the combined areas of Units 5 and 6.

## **Unit 4 Development**

Unit 4 includes the development of all of Tract B-4 and the construction of Seven Bar Loop Road and associated storm drain from Sierrita Road to the north boundary of Tract B-4. A swale along the north boundary of Tract B-4 will also be constructed during Unit 4 construction. The storm drain in Seven Bar Loop Road is designed to accommodate flows from Tract B-8 as shown in the Drainage Master Plan for the Seven Bar North Subdivision.

For purpose of analysis, Unit 4 is subdivided into four smaller sub-basins, Basins A-1 through A-4, as shown on the Drainage Basin Map. These basins together generate a fully developed runoff of 39.4 cfs ( $11.8+6.3+11.2+10.1$ ). This flow is conveyed by street flow to the southern end of Unit 4 where it is picked up in catch basins and discharged into the Seven Bar Loop Road storm drain at an existing stub-out.

As stated in the Methodology Section of this report, street flows were calculated and energy grade lines confined to the right-of-way. A Summary Table of the street calculations is provided at the front of Appendix 2 for review and reference. The allowable locations for the use of roll curb have been identified on the Curb Type Identification Map in the rear of this report.

## **Units 5 & 6 Development**

Units 5 & 6 development consist of the development of all of Tracts B-5 and B-6, the construction of Seven Bar Loop Road and the associated storm drain and the construction of Westside Boulevard from Seven Bar Loop Road to the existing pavement at the west boundary of Tract B-6. Units 5 & 6 are subdivided into 14 smaller sub-basins, Basins B-1 through B-14. These basins combine to generate a fully developed runoff of 154.7 cfs. This runoff is conveyed partially by street flow and partially in storm drain to the Unit 5 outflow.

The storm drain system consists of two "legs," which meet at the southeast end of Units 5 & 6 and combine flows into an existing 42" pipe-to-channel connection (Unit 5 outflow). The eastern leg begins at the intersection of Seven Bar Loop Road and Westside Boulevard where it picks up the flows from the offsite basin OFF1 (24.9 cfs) and Westside Boulevard basin S-1B (17.4 cfs). This leg turns into the subdivision at the Seven Bar Loop Road entrance and continues to the outflow. The storm drain is shown on plan and profile sheets in the appendix. The outflow connection will be coordinated with AMAFCA. The Drainage Master Plan analysis used 142.4 cfs peak flow into Black's Arroyo from this development, and the outflow calculated herein is actually 154.7cfs.

As stated in the Methodology Section of this report, street flows were calculated and energy grade lines confined to the right-of-way. A Summary Table of the street calculations is provided at the front of Appendix 2 for review and reference. The allowable locations for the use of roll curb have been identified on the Curb Type Identification Map.

Calculations are found in Appendix 3 for the two outflow configurations and all storm drain components.

## **Backyard Ponding**

Several lots will require backyard ponds due to extreme elevation differences between streets. Pond locations are shown on the preliminary grading plans enclosed in the rear of this report.

## **Offsite Basins**

The offsite basins that impact Tracts B-4, B-5 and B-6 are Basin OFF1, Basin S-1B and Basin E-1. As mentioned above, Basins OFF1 and Basin S-1B will be introduced into the Seven Bar Loop Road storm drain and conveyed ultimately to the Unit 5 outflow. These basins contribute a total of 38.8 cfs, which is consistent with the Master Drainage Plan. Basin E-1 consists of approximately 23.8 acres which generate a peak flow of 28.5 cfs. This flow will be captured in a temporary swale flowing adjacent to, and east of, Seven Bar Loop Road, and will be added to the existing pond at Sierrita Road. Calculations for the swale and pond are found in Appendix 4. The pond is designed to remove the sediment from the 10-year storm and have an orifice-controlled discharge into a connector pipe that runs to a storm drain manhole in Sierrita Road.

## **V. PHASING/BUILDING PERMIT/FINAL PLAT APPROVALS**

This report requests only Preliminary Plat and rough grading approvals. Prior to final plat and building permit approvals, final grading plans and work order construction plans, by phase, must be submitted and approved by the City, AMAFCA and NMUI.

## **VI. CONCLUSION**

The drainage management plan presented in this report for Tracts B-4, B-5 and B-6 provides a workable solution to the drainage issues created by the development of this property and should be approved as satisfying the requirements for Preliminary Plat drainage report and rough grading approval.

## HYDROLOGY - FORMULAS USED

FROM SECTION 22.2 OF DPM - JANUARY 95 UPDATE

### EXISTING CONDITIONS:

$$\text{TIME OF CONCENTRATION, } t_c = \frac{(L_1 + L_2 + \dots + L_x)}{V} / 3600 \text{ sec/hr}$$

WHERE  $V = K \sqrt{S}$

\* FROM TABLE B-1

S IS SLOPE IN PERCENT

$L_1 + L_2 + \dots + L_x \leq 4000 \text{ FT}$

$$\text{INTENSITY, } I = 0.726 (\log(24.6 \times t_c)) P_{60}$$

$$\text{RATIONAL METHOD "C" } = \%A(.27) + \%B(.43) + \%C(.61) + \%D(.93)$$

(ZONE 1, 100 YR, 6 HR STORM)

$$Q_p = C I A$$

### DEVELOPED CONDITIONS

FOR SMALL WATERSHEDS  $t_p = 8 \text{ MINUTES}$

$t_c = 12 \text{ MINUTES}$

$$\text{RATIONAL METHOD "C" } = \%A(.27) + \%B(.43) + \%C(.61) + \%D(.93)$$

(ZONE 1, 100 YR, 6 HR STORM)

$$\text{"C" } = \%A(.08) + \%B(.24) + \%C(.47) + \%D(.92)$$

(ZONE 1, 10 YR, 6 HR STORM)

$$\text{EXCESS PRECIPITATION, } E_c = \%A(.44) + \%B(.67) + \%C(.99) + \%D(1.97)$$

$$\text{VOLUME} = \text{AREA}(E_c)$$



BOHANNAN-HUSTON INC.

PROJECT NAME TRACTS A&D SHEET        OF       

PROJECT NO. C9721740 BY DR DATE 3-3-95

SUBJECT TRACTS A&D CH'D        DATE

## EXISTING DRAINAGE:

<u>BASIN</u>	<u>%A</u>	(SL 10%, UNDEVELOPED, PRIMARILY SHEET FLOW)
TRACTS 4,5,6	100	
E1	100	
E2	95	
E3	95	

## CALCULATION OF $t_c$ :

$t_c$  (TRACTS 4,5,6):  $L = 2100'$  (PRIMARILY SHEET FLOW)

$$t_c = \frac{2000}{0.716} + \frac{100}{316} \quad (6\% \text{ ANG})$$

$$\frac{2000}{3600} \quad P_{60} = 1.87''$$

$$= 0.33 \text{ HRS}$$

$$I = 0.726 \left( \log((24.6)(0.33)) \right) \frac{1}{0.33} (1.87) = 3.74 \text{ IN/HR}$$

$t_c$  (BASIN E-1):  $L = 1400'$  (PRIMARILY SHEET FLOW)

$$t_c = \frac{1400}{0.716} / 3600 = 0.23 \text{ HR} \quad I = 4.44 \text{ IN/HR}$$

$t_c$  (BASIN E-2):  $L = 2200'$  (SHEET & CHANNEL)

$$t_c = \frac{1200}{0.716} + \frac{1000}{417} = 0.24 \text{ HR}$$

$$I = 4.33 \text{ IN/HR}$$

$t_c$  (BASIN E-3):  $L = 1800'$  (SHEET & CHANNEL)

$$t_c = \frac{1200}{0.716} + \frac{1000}{413} = 0.22 \text{ HR}$$

$$3600$$

$$I = 4.53 \text{ IN/HR}$$

<u>BASIN</u>	<u>C</u>	<u>I</u>	<u>A (AC)</u>	<u>Q<sub>p</sub></u>
TRACTS 456	0.27	3.74	45.5	45.9
E1	0.27	4.44	23.8	28.5
E2	0.28	4.33	29.9	36.0
E3	0.28	4.53	19.0	23.9



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PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

## FULLY DEVELOPED CONDITIONS

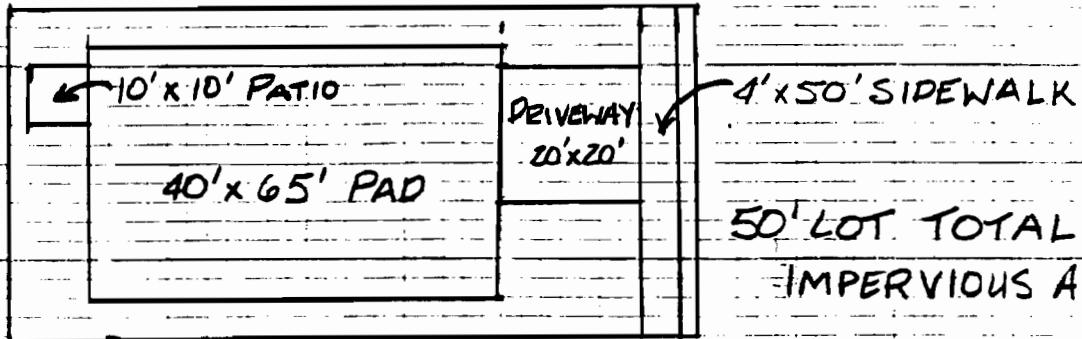
BASIN ID	AREA AC	AREA SQ.MI.	A	% LAND TREATMENT				TIME TO PEAK	DISCHARGE CFS/AC	Q(10YR) CFS	COMPOSITE C	I (IN/HR)	Q(100YR) (CFS)
				B	C	D							
A1	3.315	0.0052	3.9	18.3	18.3	59.5	0.1333	2.14	7.1	0.75	4.70	11.8	
A2	1.912	0.0030	3.4	24.7	24.7	47.2	0.1333	1.93	3.7	0.71	4.70	6.3	
A3	3.065	0.0048	3.9	15.4	15.4	65.3	0.1333	2.24	6.9	0.78	4.70	11.2	
A4	3.015	0.0047	3.4	23.4	23.4	49.8	0.1333	1.97	5.9	0.72	4.70	10.1	
B1	1.747	0.0027	3.7	22.5	22.5	51.3	0.1333	2.00	3.5	0.72	4.70	5.9	
B2	1.286	0.0020	3.6	18.1	18.1	60.2	0.1333	2.16	2.8	0.76	4.70	4.6	
B3	1.401	0.0022	3.9	16.5	16.5	63.0	0.1333	2.20	3.1	0.77	4.70	5.1	
B4	3.489	0.0055	3.7	20.6	20.6	55.2	0.1333	2.07	7.2	0.74	4.70	12.1	
B5	2.892	0.0045	3.8	22.3	22.3	51.5	0.1333	2.00	5.8	0.72	4.70	9.8	
B6	3.548	0.0055	3.9	21.7	21.7	52.8	0.1333	2.02	7.2	0.73	4.70	12.1	
B7	2.799	0.0044	4.3	19.4	19.4	56.9	0.1333	2.09	5.9	0.74	4.70	9.8	
B8	2.349	0.0037	3.5	21.9	21.9	52.6	0.1333	2.02	4.8	0.73	4.70	8.0	
B9	2.038	0.0032	3.6	20.1	20.1	56.2	0.1333	2.08	4.2	0.74	4.70	7.1	
B10	1.586	0.0025	4.1	20.1	20.1	55.8	0.1333	2.07	3.3	0.74	4.70	5.5	
B11	1.589	0.0025	3.5	14.5	14.5	67.5	0.1333	2.29	3.6	0.79	4.70	5.9	
B12	3.766	0.0059	3.2	26.3	26.3	44.2	0.1333	1.88	7.1	0.69	4.70	12.3	
B13	2.861	0.0045	3.9	22.0	22.0	52.1	0.1333	2.01	5.7	0.72	4.70	9.7	
B14	2.366	0.0037	3.9	22.2	22.2	51.7	0.1333	2.00	4.7	0.72	4.70	8.0	

## SUMMARY OF HYDROLOGIC DATA

## RATIONAL METHOD (100YR)



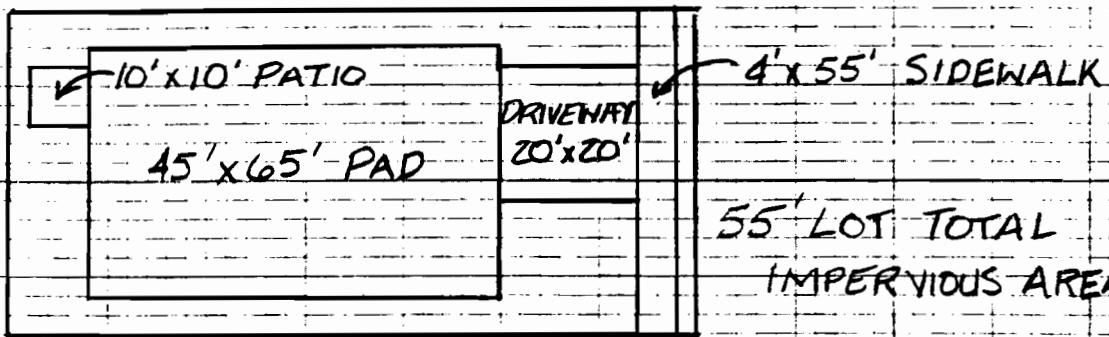
50' LOT



50' LOT TOTAL

IMPERVIOUS AREA = 3300 sf

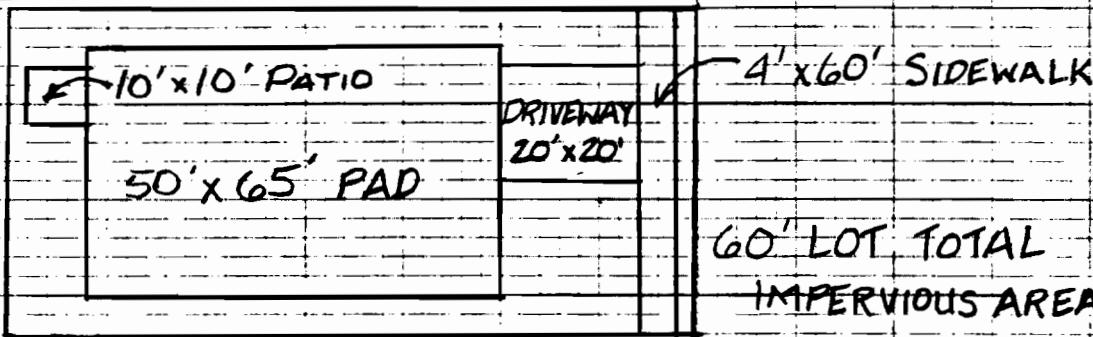
55' LOT



55' LOT TOTAL

IMPERVIOUS AREA = 3645 sf

60' LOT



60' LOT TOTAL

IMPERVIOUS AREA = 3990 sf



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PROJECT NAME TRACTS A & D

SHEET 1 OF 2

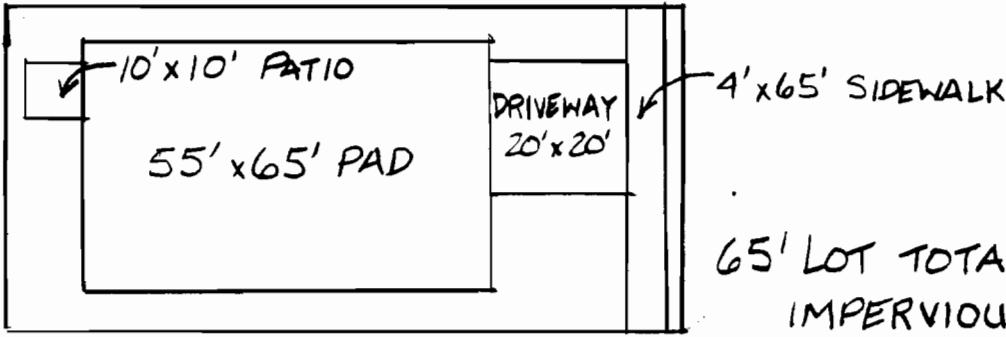
PROJECT NO. 9321740

BY FB DATE \_\_\_\_\_

SUBJECT HYDROLOGY

CH'D \_\_\_\_\_ DATE \_\_\_\_\_

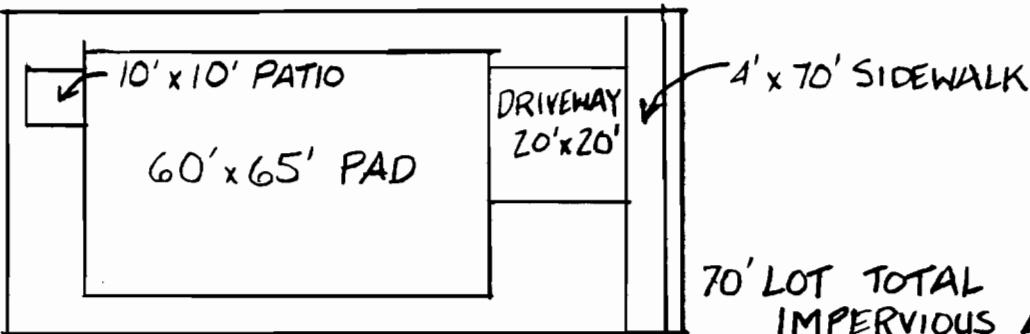
65' LOT



65' LOT TOTAL

IMPERVIOUS AREA = 4335 □

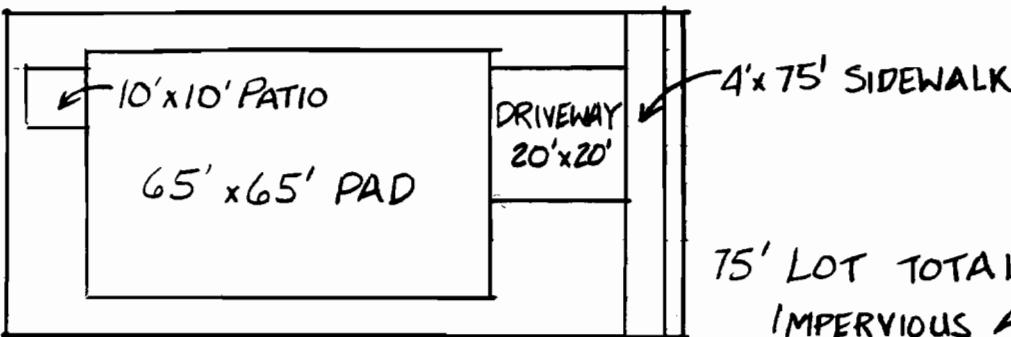
70' LOT



70' LOT TOTAL

IMPERVIOUS AREA = 4680 □

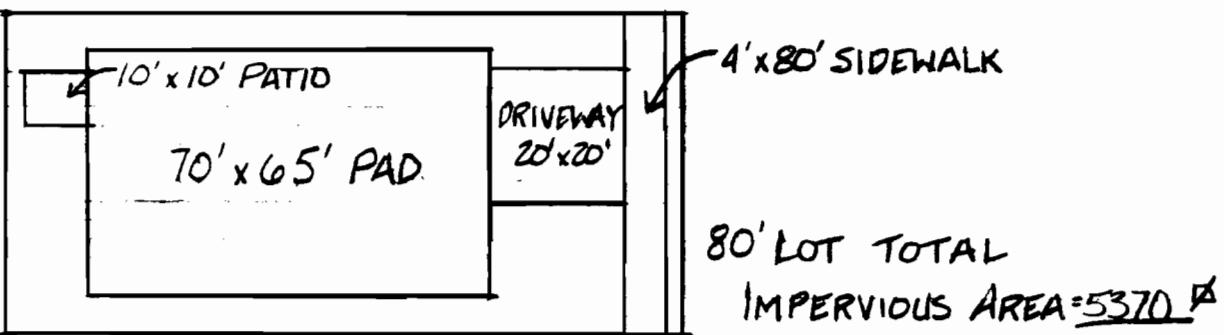
75' LOT



75' LOT TOTAL

IMPERVIOUS AREA = 5025 □

80' LOT



80' LOT TOTAL

IMPERVIOUS AREA = 5370 □



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PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

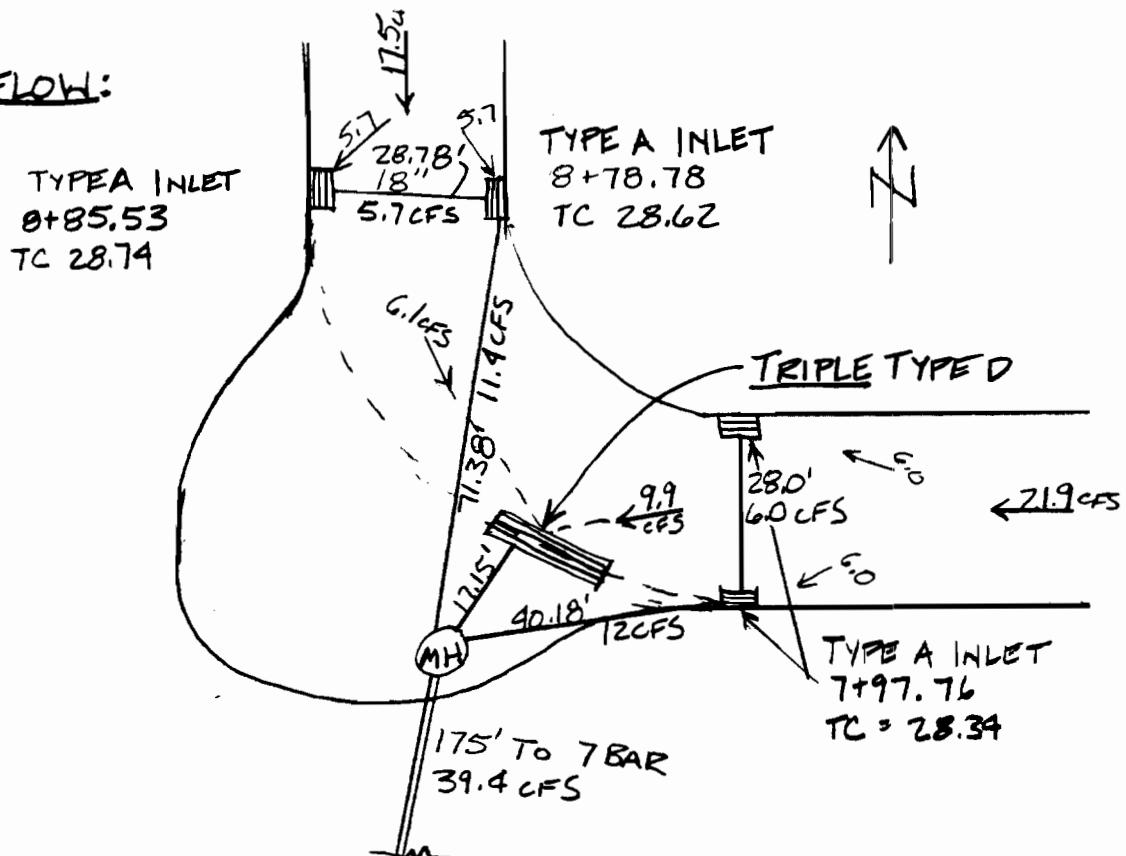
SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

**STREET CAPACITY ANALYSIS**  
**SUMMARY TABLE**  
 SEVEN BAR NORTH  
 UNITS 4, 5 AND 6

<u>ANALYSIS POINT</u>	<u>SLOPE %</u>	<u>TYPE OF CURB</u>	<u>Q-100YR (CFS)</u>	<u>DEPTH (FT)</u>	<u>V-100YR (FPS)</u>	<u>E-100YR (FT)</u>	<u>E&lt;0.87? &lt;.51 ROLL</u>	<u>NOTES</u>
A	2.50	STD	17.5	0.38	4.0	0.63	YES	USE STD
B	2.50	ROLL	11.2	0.28	3.4	0.46	YES	USE ROLL
C	6.21	STD	10.1	0.24	4.8	0.60	YES	USE STD TO CULDESAC
D	3.00	STD	21.9	0.39	4.5	0.70	YES	USE STD
2	1.35	STD	32.0	0.50	4.2	0.77	YES	USE STD
3	1.35	STD	26.1	0.47	3.8	0.69	YES	USE STD
4	1.00	STD	19.2	0.44	3.1	0.59	YES	USE STD
5	3.82	STD	26.9	0.40	5.3	0.84	YES	USE STD
6	1.00	ROLL	9.8	0.31	2.4	0.40	YES	USE ROLL
7	5.25	STD	7.2	0.26	4.1	0.52	YES	USE STD
7A	5.25	STD	20.8	0.36	5.4	0.81	YES	USE STD
8	1.00	ROLL	13.5	0.35	2.7	0.46	YES	USE ROLL
9	4.57	ROLL	8.0	0.23	4.0	0.48	YES	USE ROLL
10	4.57	STD	22.3	0.38	5.4	0.83	YES	USE STD
11	4.57	STD	12.5	0.32	4.6	0.65	YES	USE STD
12	3.25	STD	27.9	0.42	5.2	0.84	YES	USE STD
13	4.00	STD	12.3	0.32	4.3	0.61	YES	USE STD, TRANS 100'
14	4.00	ROLL	9.7	0.25	4.0	0.50	YES	USE ROLL

SUMMARY: Use roll curb only in Basins A3, B7, B10, B13, B14 and a portion of Basins A4 and B12.

## UNIT 4 OUTFLOW:



## CATCH BASINS:

### TYPE A WEST:

$$Q = 17.5 \text{ CFS}$$

$$S = 2.50 \%$$

$$\text{NORMAL } D = 0.38'$$

$$\text{VELOCITY} = 4.0 \text{ FPS}$$

CAPACITY OF SINGLE TYPE A = 5.7 CFS  
(FROM COA NOMOGRAPH)

$$\text{FLOW REMAINING} = [17.5 - 2(5.7)] + [21.9 - 2(6.0)] = 16.0 \text{ CFS}$$

→ USING TYPE D IN SUMP, NO OVERFLOW PROVIDED, DESIGN FOR 200%:

$$Q_{DES} = 2(Q_{100}) = 2(16) = 32.0 \text{ CFS}$$

ORIFICE EQN: TRIPLE GRATE

$$Q = 0.6 A_{NET} \sqrt{2gh}; h = 0.83'$$

$$A_{NET} = 3(31)(185)/144 = 11.9 \text{ SF}$$

$$Q = 0.6 (11.9) (2(32.2)(.83))^{1/2} \\ = 52.2 \text{ CFS} > 32.0 \checkmark$$

### TYPE A EAST:

$$Q = 21.9 \text{ CFS}$$

$$S = 3.00 \%$$

$$\text{NORMAL } D = 0.39'$$

$$\text{VELOCITY} = 4.5 \text{ FPS}$$

CAPACITY OF SINGLE TYPE A  
= 6.0 CFS

WEIR EQUATION: TRIPLE GRATE

$$Q = 2.68 P_{NET} H^{1.5}$$

$$P_{NET} = \frac{2(18.5) + 6(31)}{12} = 18.6 \text{ FT}$$

$$Q = 39.1 \text{ CFS} > 32.0 \checkmark$$



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## UNIT 4 CATCH BASINS (WEST LEG)

STA 8+85.53, 4' RT

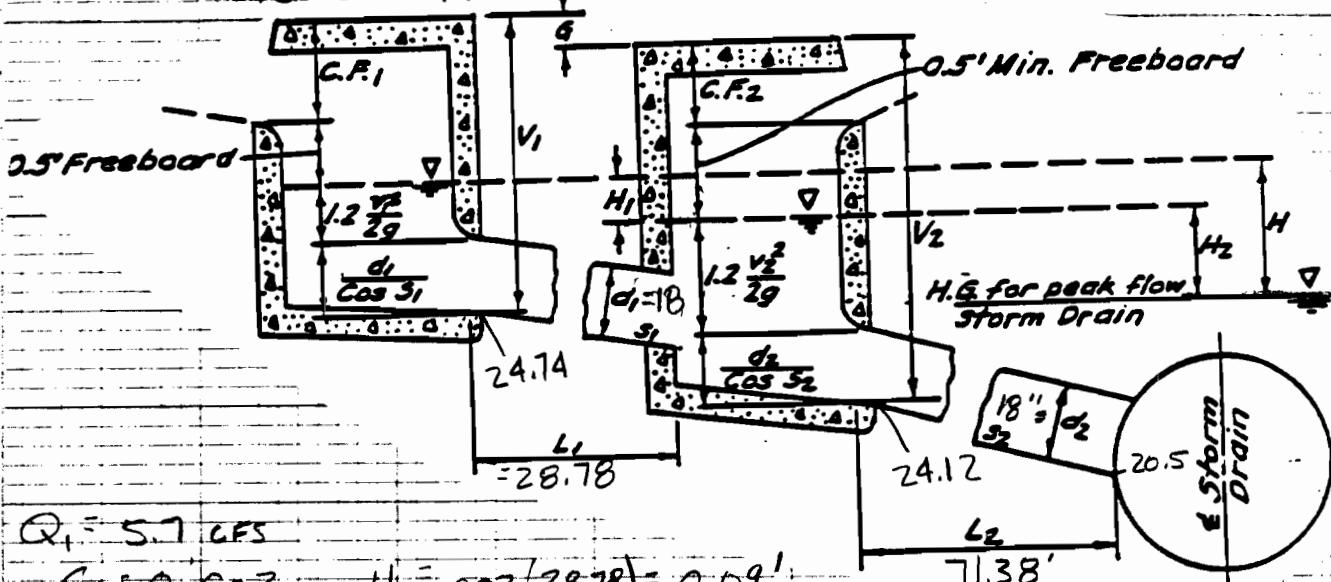
**TYPE "A"**

TC: 5128.74

STA B+78.78, 19' IT

**TYPE "A"**

$$TC = 5128.62$$



$$Q_1 = 5.1 \text{ cfs}$$

$$S_f = 0.003 \quad H_i = .003(28.78) = 0.09'$$

$$V = 8.23 \text{ EPS}$$

$$\underline{1.7 v^2 = 0.19}$$

$$V_{min} = 1.33 + .19 + 1.5 = 3.02$$

## USE 4 (MINIMUM)

$$Q_2 = 11.4 \text{ cfs}$$

$$V_2 = 6.45 \quad S_f = 0.0118$$

$$\frac{1.2 \times 2}{29} = 0.78$$

$$V_2 = 1.33 + 0.09 + 0.78 + 1.5 - 0.12 \\ = 3.58$$

USE 4.5 (ALLOW SAME SLOPE  
ON PIPE 1)

CHECK HEAD LOSSES TO SEVEN BAR LOOP ROAD

Losses:  $H_{f1} = 0.09'$

$$H_{F2} \rightarrow S_{FL} = .0118(71.38) = 0.89$$

$$H_j = \frac{39.4(803) - 11.4(1.45) - 28(\cos 45) + 8(0.051 + 0.22)(1.77 + 4.91)}{32.2} + h_{r_1}$$

$$\frac{1}{2} (1.77 + 4.91) \\ 3.34$$

$$= 2.37' + 0.65 - 1.00 = 2.02$$

$$H_{E3} = 0.0092(175) = 1.61$$



## BOHANNAN-HUSTON INC.

**PROJECT NAME** \_\_\_\_\_ **SHEET** \_\_\_\_\_ **OF** \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

HGL @ 7 BAR LOOP ROAD = 5120.6

$$H_{\text{AVAILABLE}} = 28.74 - 1.33 - 20.6 \\ = 6.81$$

$$H_{f1} + H_{f2} + H_3 + H_{f3} = 0.09 + 0.84 + 2.02 + 1.61 = 4.56 < 6.81 \quad \boxed{\text{OK.}}$$



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

# UNIT 4 CATCH BASINS (EAST LEG)

STA 7+97.76, 14' RT

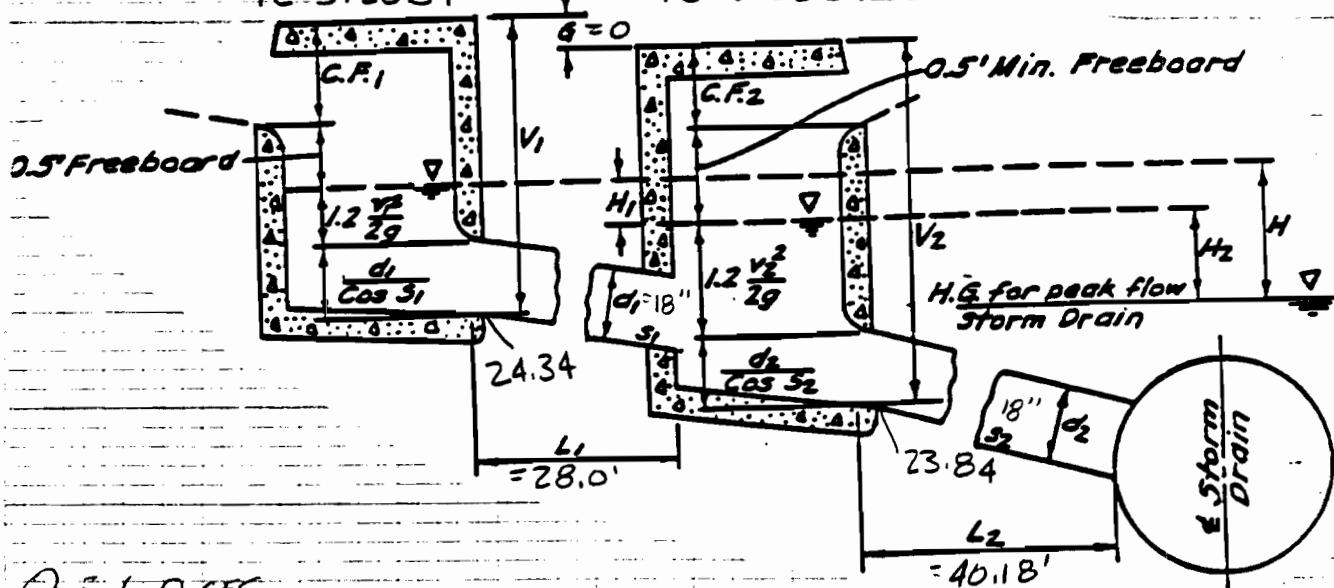
TYPE A

TC ST2834

STA 7+97.76, 14' LT

TYPE A

TC 5128.34



$$Q_1 = 6.0 \text{ cfs}$$

$$S_f = 0.0033 \quad H_f = .0033(28) = 0.09'$$

$$V = 3.4 \text{ FPS} \quad 1.2 \frac{V^2}{2g} = 0.21' \quad \frac{d_1}{2g} = 18''$$

$$V_{1\text{MIN}} = 1.33 + 0.21 + 1.5 = 3.04'$$

USE 4' (MIN.)

$$Q_2 = 12.0 \text{ cfs}$$

$$V_2 = 6.79 \text{ FPS; } 1.2 \frac{V^2}{2g} = 0.86' \quad \frac{d_2}{2g} = 18''$$

$$V_{2\text{MIN}} = 1.33 + 0.09 + 0.86 + 1.5 = 3.78$$

USE 4.5' (PROVIDE SLOPE ON CONNECTOR PIPE)

CHECK HEAD LOSSES TO SEVEN BAR LOOP ROAD:

LOSSES:  $H_{f1} = 0.09$

$$H_{f2} = S_f L = 0.013(40.18) = 0.52' \text{ loss}$$

$$H_j = \frac{39.4(8.03)}{32.2} - 12(6.79) - 27.4(\cos 45^\circ) + 8(0.083 + 0.022)(1.77 + 4.91)$$

$$\frac{1}{2}(1.77 + 4.91)$$

$$= 2.42' + 0.72 - 1.00 = 2.14$$

$$H_{f3} = 1.61$$

$$HGL @ 7 BAR LOOP ROAD = 5120.6$$

$$H_{\text{AVAILABLE}} = 28.34 - 1.33 - 20.6 = 6.41$$

$$H_{f1} + H_{f2} + H_j + H_{f3} = 4.36 < 6.41 \quad \boxed{\text{OK}}$$



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

CATCH BASIN CALCULATION SHEET

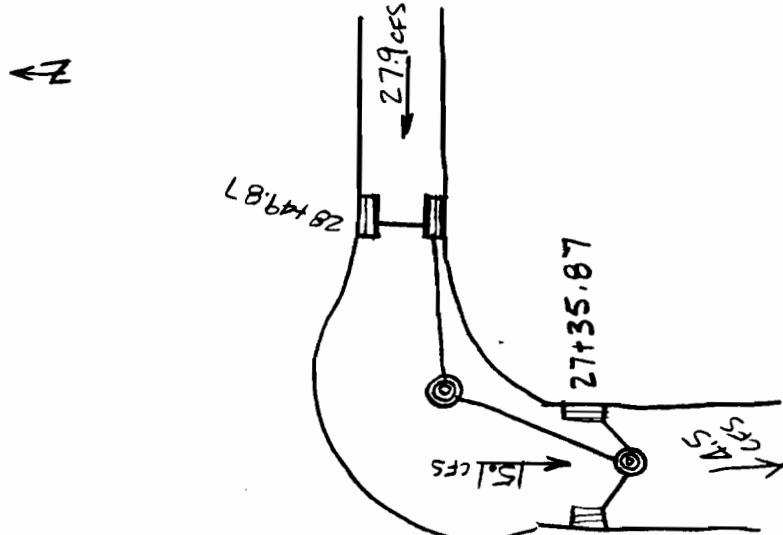
Sht \_\_\_\_\_ of \_\_\_\_\_

PROJECT \_\_\_\_\_  
DESIGN FREQUENCY  
(Indicate street slopes)

CALCULATED BY \_\_\_\_\_

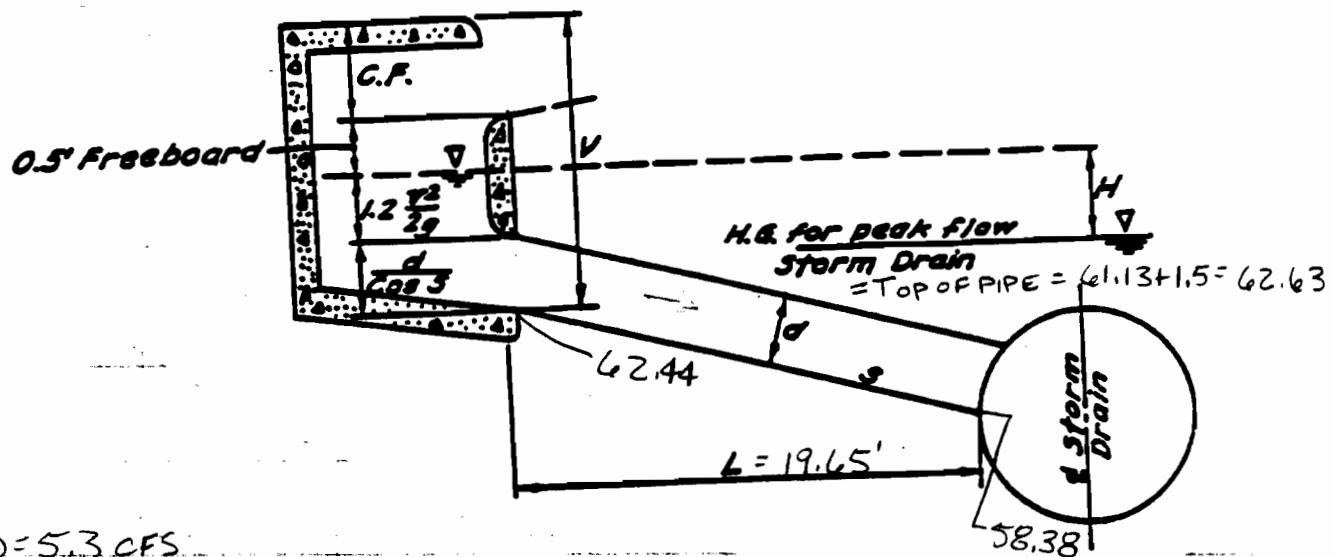
DATE

FLOW DIAGRAM	Sym.	Drain. Area	Total Inter.	Q	Cap. of Street "d"	Gutter "d"	C.B. No.	Size	Head	Connector Pipe L	Dia.	V Depth
28+	49.87		2x6.4									
27+		27.9	12.8		0.41	2	"A"					
35.87		2x5.3										
		15.1	10.6		0.34	2	"C"					
				4.5								



CATCH BASINS - UNITS 5 / 6

STA 27+35.87, 14' RT&LT  
SINGLE TYPE C  
TC 66.44



$$Q = 5.3 \text{ CFS}$$

$$V_{EL} = 3.0 \text{ FPS}$$

$$\frac{1}{2} \frac{V_{EL}^2}{Zg} = 0.17'$$

$$V_{MIN} = 1.33 + 0.17 + 1.5 = 3.00$$

Use 4' (min)



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

# CATCH BASINS

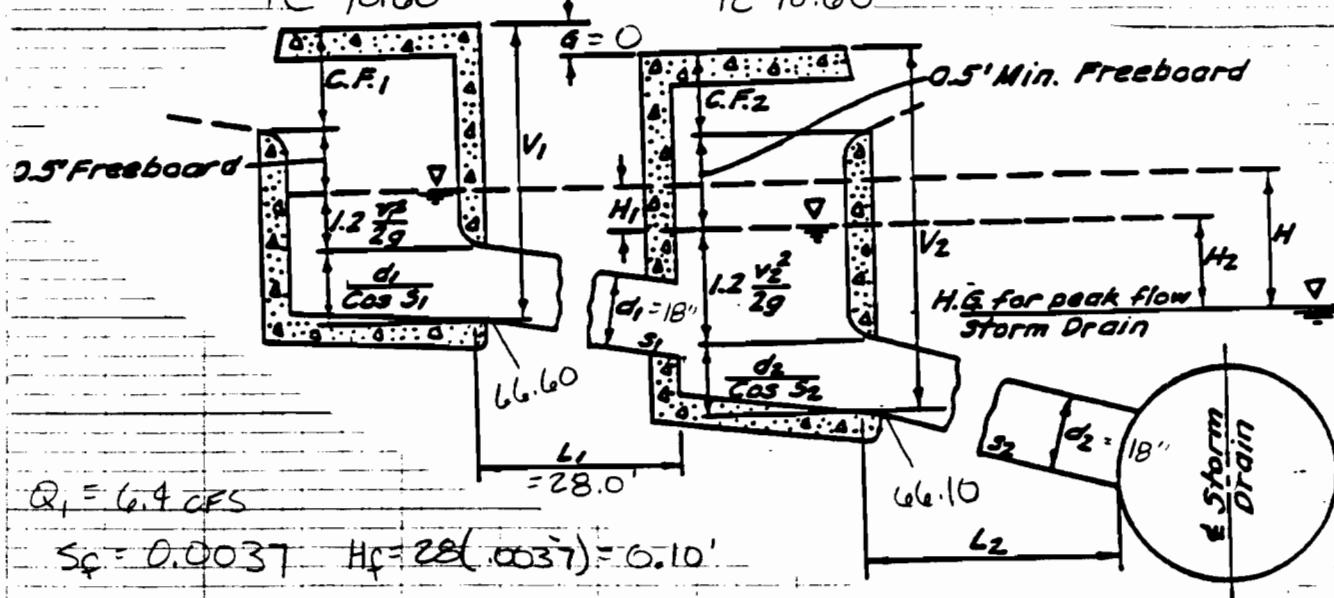
STA 28+49.87, 14' LT 14' RT

SINGLE TYPE "A"

TC 70.60

SINGLE TYPE A

TC 70.60



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

Sheet of

PROJECT \_\_\_\_\_ DESIGN FREQUENCY

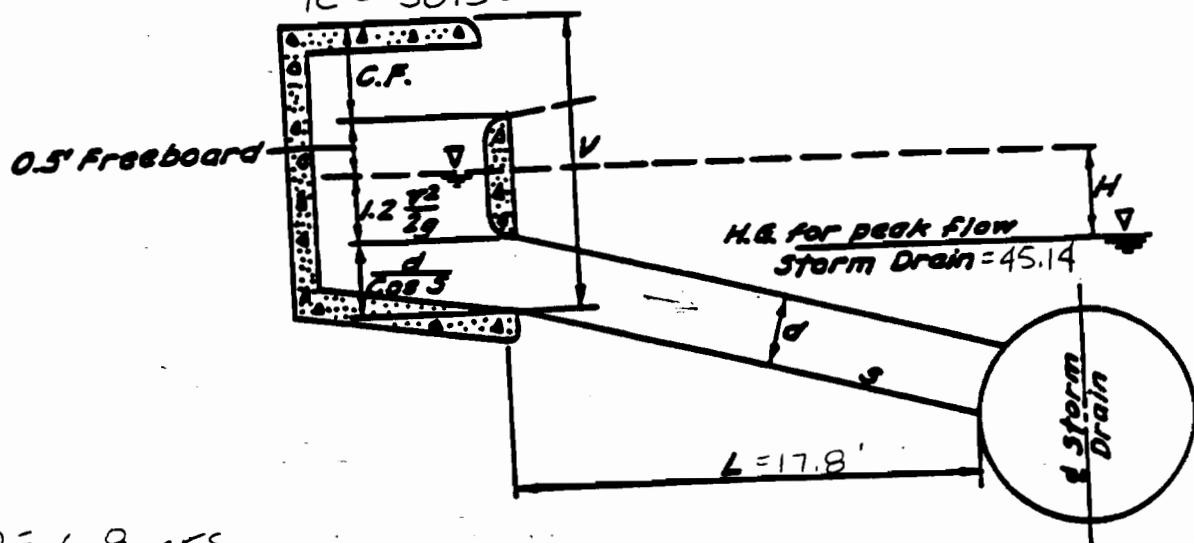
CALCULATED BY \_\_\_\_\_

DATE

STA 14+56, 14' RT, LT

SINGLE TYPE "A"

TC = 50.5 ±



$$Q = 6.8 \text{ CFS}$$

$$V_{EL} = 3.85 \text{ FPS}$$

$$1.2 V_{EL}^2 = 0.28'$$

$$2g$$

$$V_{MIN} = 1.33 + 0.28 + 1.5 = 3.11'$$

$$S_f = 0.0042$$

USE 9' (MIN)

$$HGL + H = 45.14 + .0042(17.8) < 50.5 - 1.33$$

$$45.21 < 49.17$$



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

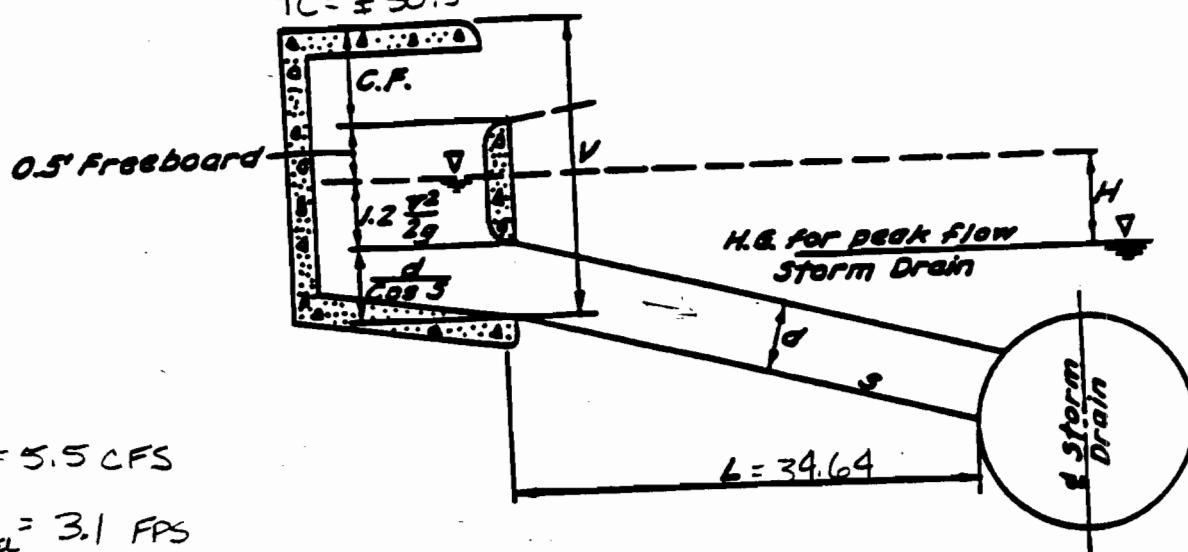
CATCH BASINS - UNIT 5/6

(CONNECTING FROM SIDE STREET TO MH # SD4 - FROM BASINS B9 & B6)

STA 6+61.60

SINGLE TYPE A

TC = ± 50.5



$$Q = 5.5 \text{ CFS}$$

$$V_{EL} = 3.1 \text{ FPS}$$

$$\frac{1.2 V_{EL}^2}{2g} = 0.18'$$

$$V_{MIN} = 1.33 + 0.18 + 1.5 = 3.01'$$

USE 4' (MIN)



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

CATCH BASIN CALCULATION SHEET

Shl \_\_\_\_\_ of \_\_\_\_\_

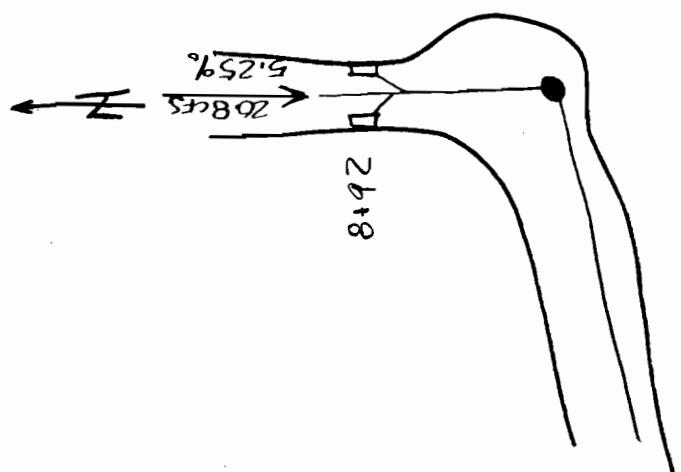
PROJECT \_\_\_\_\_

DESIGN FREQUENCY

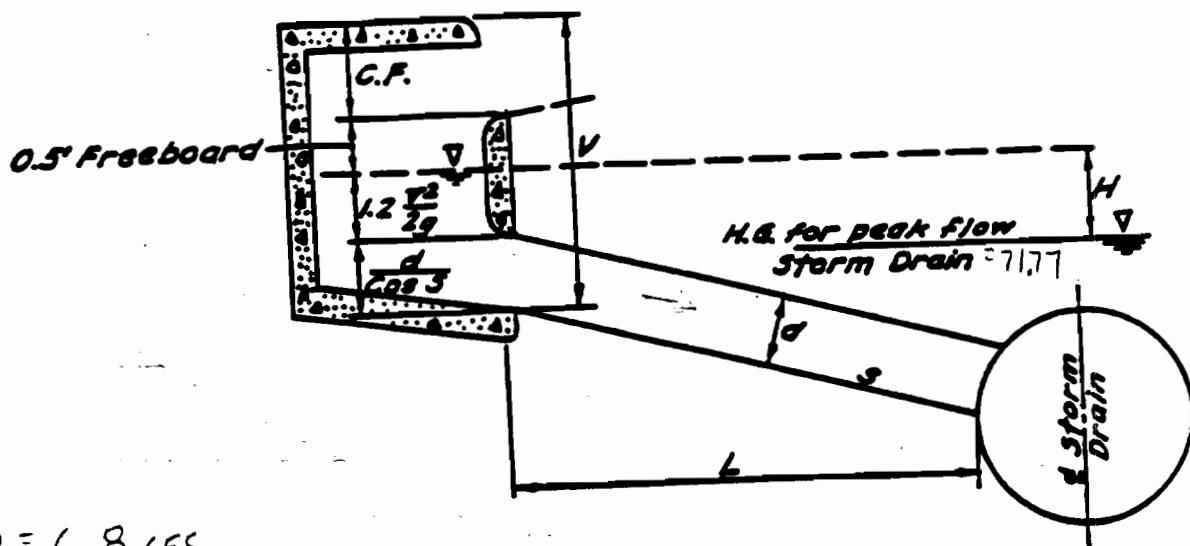
CALCULATED BY \_\_\_\_\_

DATE \_\_\_\_\_

FLOW DIAGRAM (Indicate street slopes)	Sym.	Drain. Area	Q Total	Q Inter. Street	Cap. of Gutter "d"	C.B. No.	Connector Pipe			V Depth
							Size	Head	L	
B+86			20.8	13.6	.36	2	"A"			



STA 8+92  
TC ± 75.7  
TYPE "A"



$$Q = 6.8 \text{ CFS}$$

$$S_f = 0.0042$$

$$V_{EL} = 3.85 \text{ FPS}$$

$$1.2 V_{EL}^2 / 2g = 0.28'$$

$$V_{MIN} = 1.33 + 0.28 + 1.5 = 3.11$$

Use 4' (MIN)

$$HGL + H =$$

$$71.77 + 17.9(0.0042) < 75.7 - 1.33$$

$$71.69 < 74.37$$



BOHANNAN-HUSTON INC.

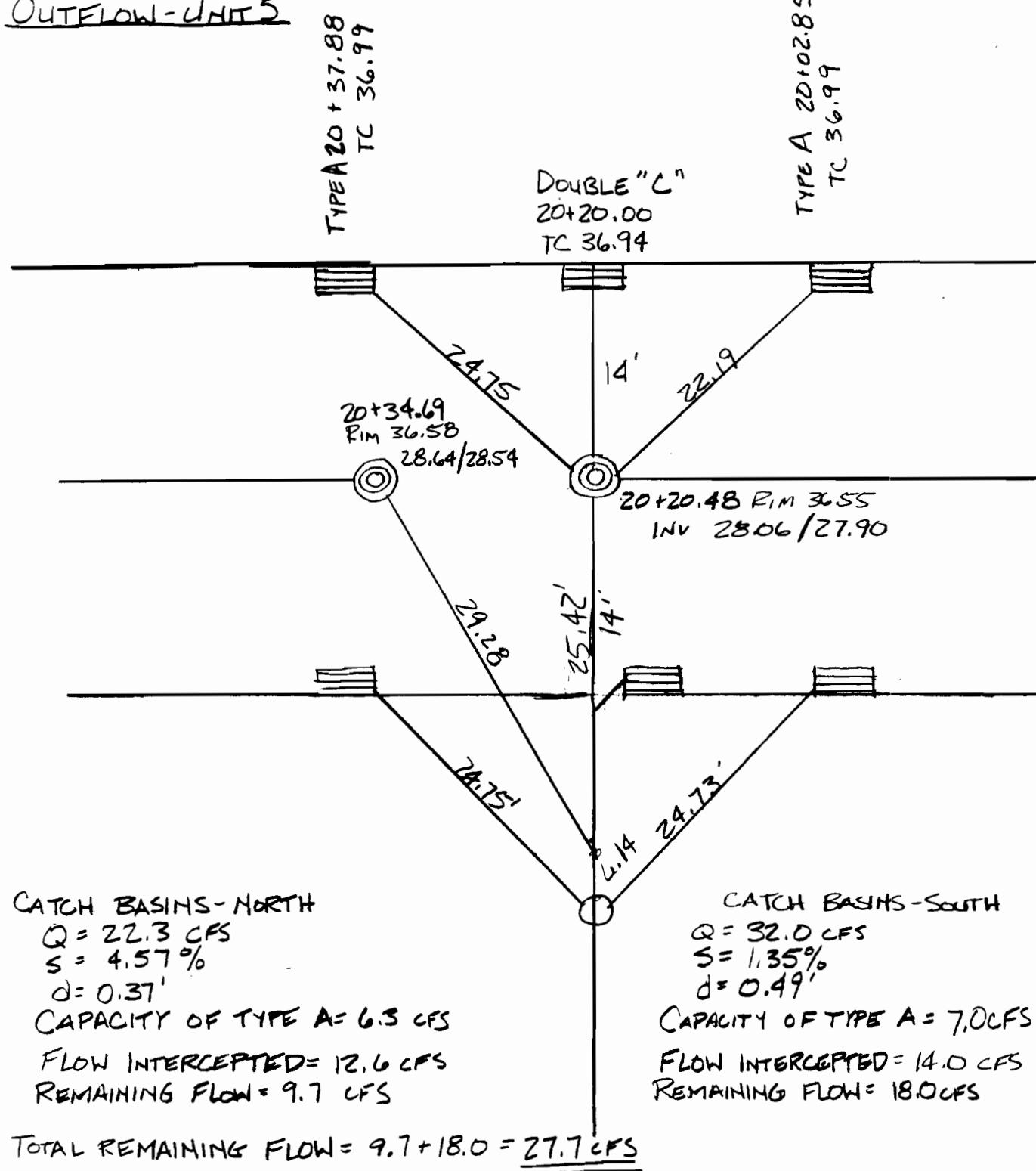
PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

STORM DRAIN

## OUTFLOW-UNIT 5



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_  
SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

USE TYPE "DOUBLE C" IN SUMP @ LOW POINT: WILL OVERFLOW TO OTHER INLETS

$$Q_{DES} = Q_{100} = 27.7 \text{ cfs}$$

ORIFICE EQN

$$Q = 0.6 A_{NET} \sqrt{2gh}; h = 0.83$$

$$A_{NET} = 2(31)(18.5) / 144 = 7.97 \text{ SF}$$

$$Q = 0.6(7.97) \sqrt{2(32.2)(.85)} = 35.38$$

USING 2-Double C's,  $Q = 2(35.38) = 70.8 > 27.7$  OK

WEIR EQN

$$Q = 2.68 P_{NET} H^{1.5} \quad P_{NET} = \frac{2(18.5) + 2(31)}{12} = 8.25'$$

$$Q = 2.68(8.25)(.85)^{1.5} = 17.3$$

USING 2- Double C's,  $Q = 2(17.3) = 34.6 > 27.7$  ✓



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

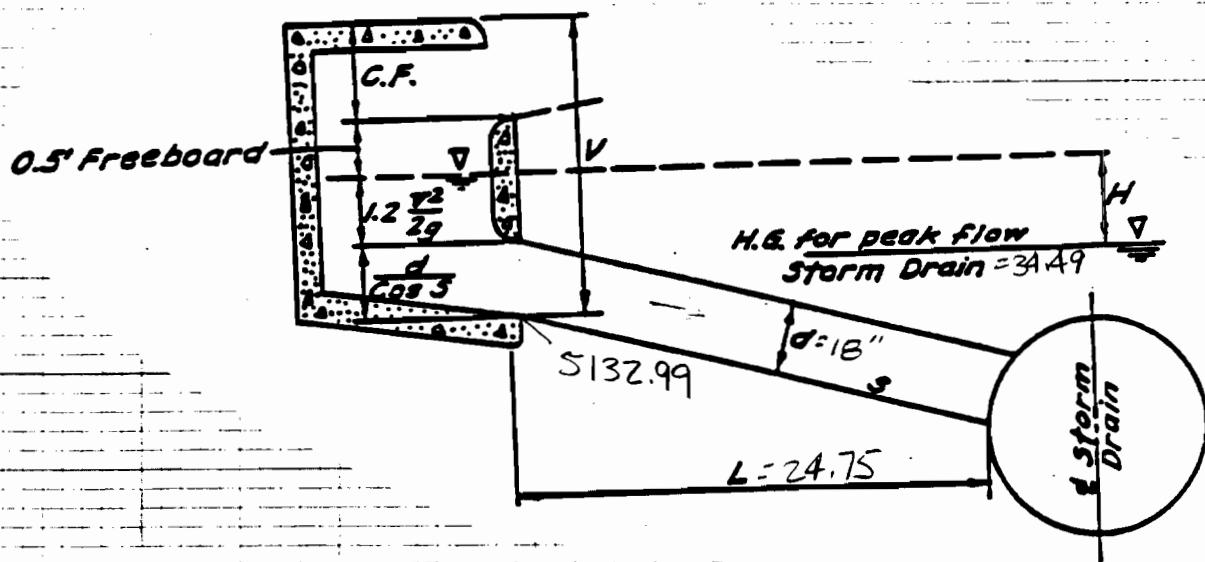
PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

STA 20 + 37.88, 14' RT

TC 5136.99

TYPE "A"



$$Q = 6.3 \text{ CFS}$$

$$S_f = 0.0036$$

$$V = 3.57 \text{ FPS}$$

$$1.2 V^2 = 0.237$$

2g

$$V_{min} = 1.33 + 0.24 + 1.5 = 3.07'$$

USE 4' (MIN)

$$HGL + H = 34.49 + 0.0036(24.75) = 34.58 < 36.99 - 1.33 = 35.66 \checkmark$$



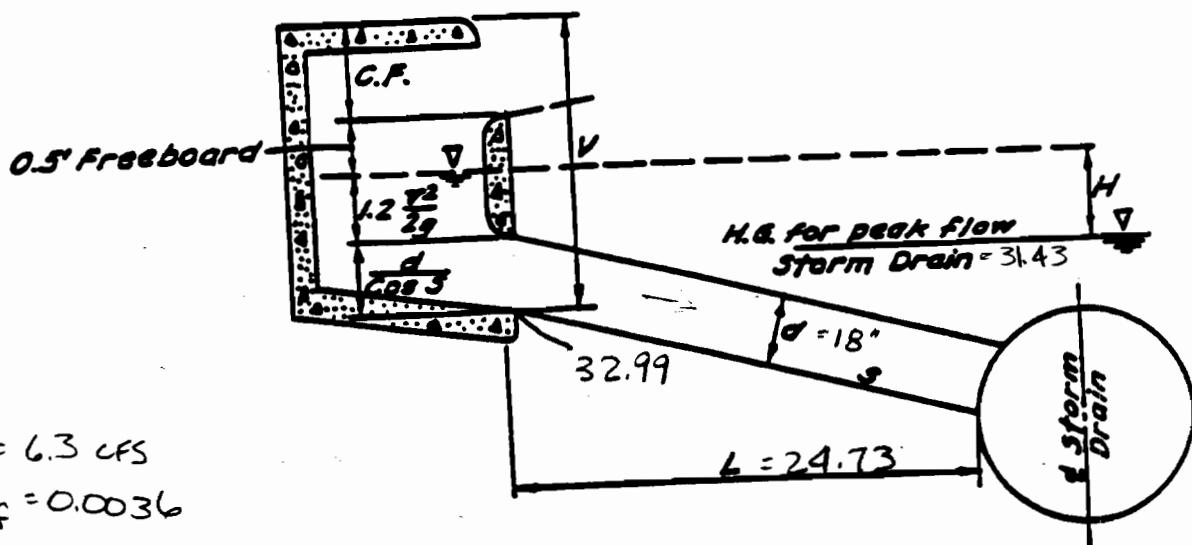
BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

STA 20+37.88, 14' LT  
TL 5136.99  
TYPE "A"



$$Q = 6.3 \text{ cfs}$$

$$S_f = 0.0036$$

$$V_{EL} = 3.57 \text{ fps}$$

$$\frac{1.2 V^2}{2g} = 0.24'$$

$$V_{MIN} = 1.33 + 0.24 + 1.5 = 3.07'$$

USE 4' (MIN)

$$HGL + H = 31.43 + 0.0036(24.73) = 31.52 < 36.99 - 1.33 = 35.66$$



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

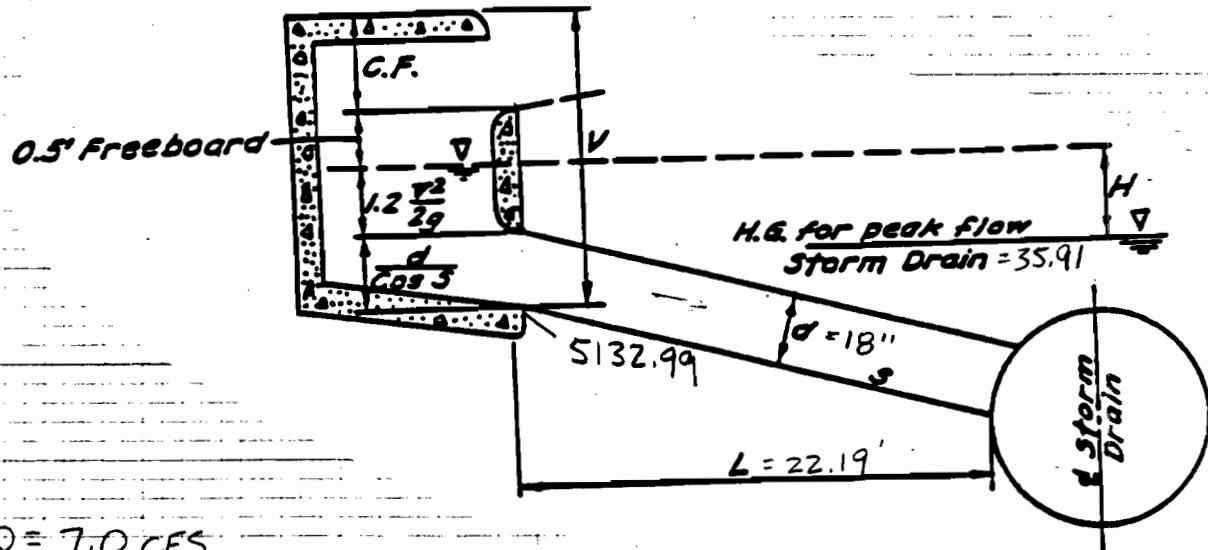
PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

STA 20102.85, 14' RT

TC 5136.99

TYPE A



$$Q = 7.0 \text{ cfs}$$

$$S_f = 0.0044$$

$$VEL = 4.0 \text{ fpm}$$

$$\frac{1.2(VEL)^2}{2g} = 0.29'$$

$$V_{MIN} = 1.33 + 0.29 + 1.5 = 3.12$$

USE 4' (MIN)

$$HGL + H = 34.49 + 0.0044(22.19) = 34.59 \quad 34.99 - 1.33 = 33.66$$



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

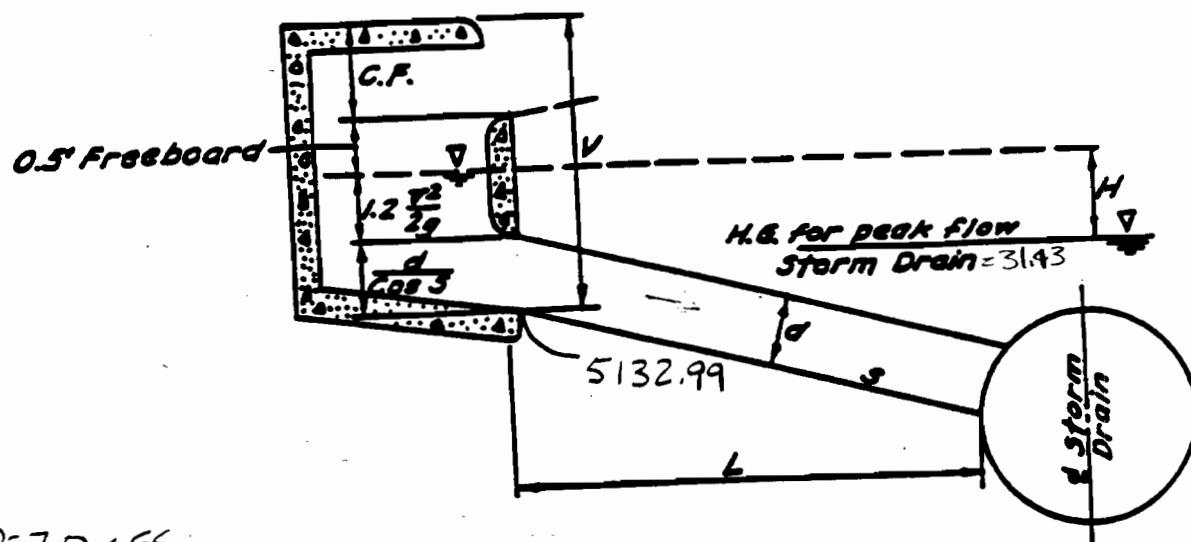
PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

STA 20+02.85, 14' LT

TC 5136.99

TYPE "A"



$$Q = 7.0 \text{ CFS}$$

$$S_f = 0.0044$$

$$VEL = 4.0 \text{ CFS}$$

$$\frac{1.2 V^2}{2g} = 0.29'$$

$$V_{MIN} = 1.33 + 0.29 + 1.5 = 3.12$$

USE 4' (MIN)

$$HGL + H = 5131.43 + 0.0044(24.73) = 31.53 \text{ L } 36.99 - 1.33 = 35.66 \text{ L }$$



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

## SWALE CALCULATIONS

SWALE ADJACENT TO SEVEN BAR LOOP TO CONVEY FLOWS FROM BASIN E-1:

$$\text{AREA} = 23.8 \text{ ACRE}$$

$$\% A = 100$$

$$t_c = 0.23 \text{ HRS}$$

$$I = 4.44 \text{ IN/HR} \quad E = 0.44''$$

$$Q_{100} = 28.5 \text{ CFS}$$

$$V = 0.87 \text{ AC-FT}$$

4.85%

① CONVEY FLOWS IN AN EARTHEN SWALE ADJACENT TO SEVEN BAR LOOP ROAD.

$$\text{MANNINGS "n" } = 0.030$$

$$\text{MAX SLOPE} = 4.85\%$$

TO KEEP VELOCITY IN SWALE < 8 FPS, USE A V-DITCH WITH SIDE SLOPES = 3:1. MAX DEPTH = 1.05', USE 2' DEPTH.

$$S = 4.85\%, V_{EL} = 6.9 \text{ FPS}, d = 1.05'$$

$$4.66 \quad V_{EL} = 7.0 \text{ FPS}, d = 1.10$$

$$1.50 \quad V_{EL} = 4.5 \text{ FPS}, d = 1.35'$$

PROVIDE A LINED HEIGHT OF 2.5', GIVING A FREEBOARD > 1' IN ALL LOCATIONS.

② CHECK POND SIZE:

$$\text{TOTAL FLOW INTO POND} = 28.5 + 36.0 + 23.9 = 88.4 \text{ CFS}$$

$$V_{100} = (23.8 + 29.9 + 19.0)(.44) / 12 = 2.67 \text{ ac-ft.} = 116,300 \text{ CF}$$

ZA - POND SIZE BASED ON SETTLING VELOCITY: ( $V_s$ )

ASSUME - DESIGN PARTICLE: VERY FINE SAND ( $D = 0.06 \text{ mm}$ )

- 100% REMOVAL FOR 10 YR STORM

-  $V_s = 0.009 \text{ FPS}$  FOR VERY FINE SAND

$$P_{60-10} = 1.87 \times 0.667 = 1.25''$$

$$I = 0.726 \left( \log((24.6)(.23)) \frac{1}{.23} \right) (1.25) = 2.97 \text{ IN/HR}$$

$$C = 0.08$$

$$A = 23.8 + 29.9 + 19.0 = 72.7 \text{ ACRE}$$

$$Q = CIA = 0.08(2.97)(72.7) = 17.3 \text{ CFS}$$



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_ OF \_\_\_\_

PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_

SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

$$\text{SURFACE AREA} = SA = 1.2(Q_{in}) / V_s$$

$$SA = 1.2(17.3) / .009 = 2307 \text{ SF}$$

$$\text{KEEP LENGTH} = 77' \quad W = \underline{2307} = 30'$$

77

POND IS NOW $77 \times 26$
INCREASED TO $77' \times 30'$

ZB FROM USLE SPREADSHEET (ATTACHED), THE AVERAGE ANNUAL SEDIMENT YIELD IS  $371 \text{ CY} = 10016 \text{ FT}^3$

ASSUME: MAXIMUM SEDIMENT STORAGE DEPTH = 3'  
MINIMUM SETTLING DEPTH = 2'

USING  $SA = 2307$  (FROM ZA) ( $z$  = POND DEPTH)

$$\text{BOTTOM AREA} = (77)(30) = 2310 \text{ FT}^2$$

$$\text{TOP AREA} = 2310 + 64Zz + 36z^2$$

$$\text{VOLUME} = \frac{(\text{BOTTOM AREA}) + (\text{TOP AREA})}{z}$$

$$= 2310z + 321z^2 + 18z^3$$

$$V = 10016 \text{ FT}^3 = 2310z + 321z^2 + 18z^3$$

$$z = 2.94' < 3'$$

SEDIMENT STORAGE DEPTH = 2.94'

### POND VOLUMETRICS

POND DEPTH = 5'

POND VOLUME =  $21,825 \text{ FT}^3 = 0.501 \text{ AC-FT}$

VOLUME IN =  $116,300 \text{ CF} = 2.67 \text{ AC-FT}$

$Q_{in} = 88.4 \text{ CFS}$

$$V_{PONDED} = \left( \frac{V_{TOTAL}}{Q_{in}^2} \right) Q_{out}^2 - (\text{DURATION})Q_{out} + V_{TOTAL}$$

$$\text{DURATION} = \frac{2 V_{TOTAL}}{Q_{in}} = \frac{2 (116,300)}{88.4} = 2631 \text{ SEC}$$

$$21,825 \text{ FT}^3 = \left( \frac{116,300}{88.4^2} \right) Q_{out}^2 - (2631)Q_{out} + 116,300$$



BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
 PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_  
 SUBJECT \_\_\_\_\_ CH'D \_\_\_\_\_ DATE \_\_\_\_\_

$$14.88 Q_{out}^2 - 2631 Q_{out} + 94,475 = 0$$

$Q_{out} = 50.1 \text{ CFS}$  TO MAINTAIN VOLUMETRICS

ORIFICE CONTROL:

HEAD = 5' - SEDIMENT STORAGE DEPTH:

$$A = \frac{Q}{\cdot 612gh} = \frac{50.1}{\cdot 612(32.2)(2.06)} = 7.25 \text{ FT}^2 = \frac{\pi D^2}{4}$$

$$D = 3.04'$$

USE EXISTING 36" CMP STANDPIPE. REMOVE ORIFICE PLATE.

CONNECTOR PIPE SLOPE = 2.56%

36" RCP, 97',  $Q = 50.1 \text{ CFS}$

- SUMMARY:
- ① BUILD 2.5' DEEP LINED DITCH ON THE EAST SIDE OF 7BAR LOOP ROAD, 3:1 SIDES
  - ② "WIDEN" POND TO 30' X 77' FROM 26' X 77'.
  - ③ REMOVE ORIFICE PLATE ON POND OUTFLOW.



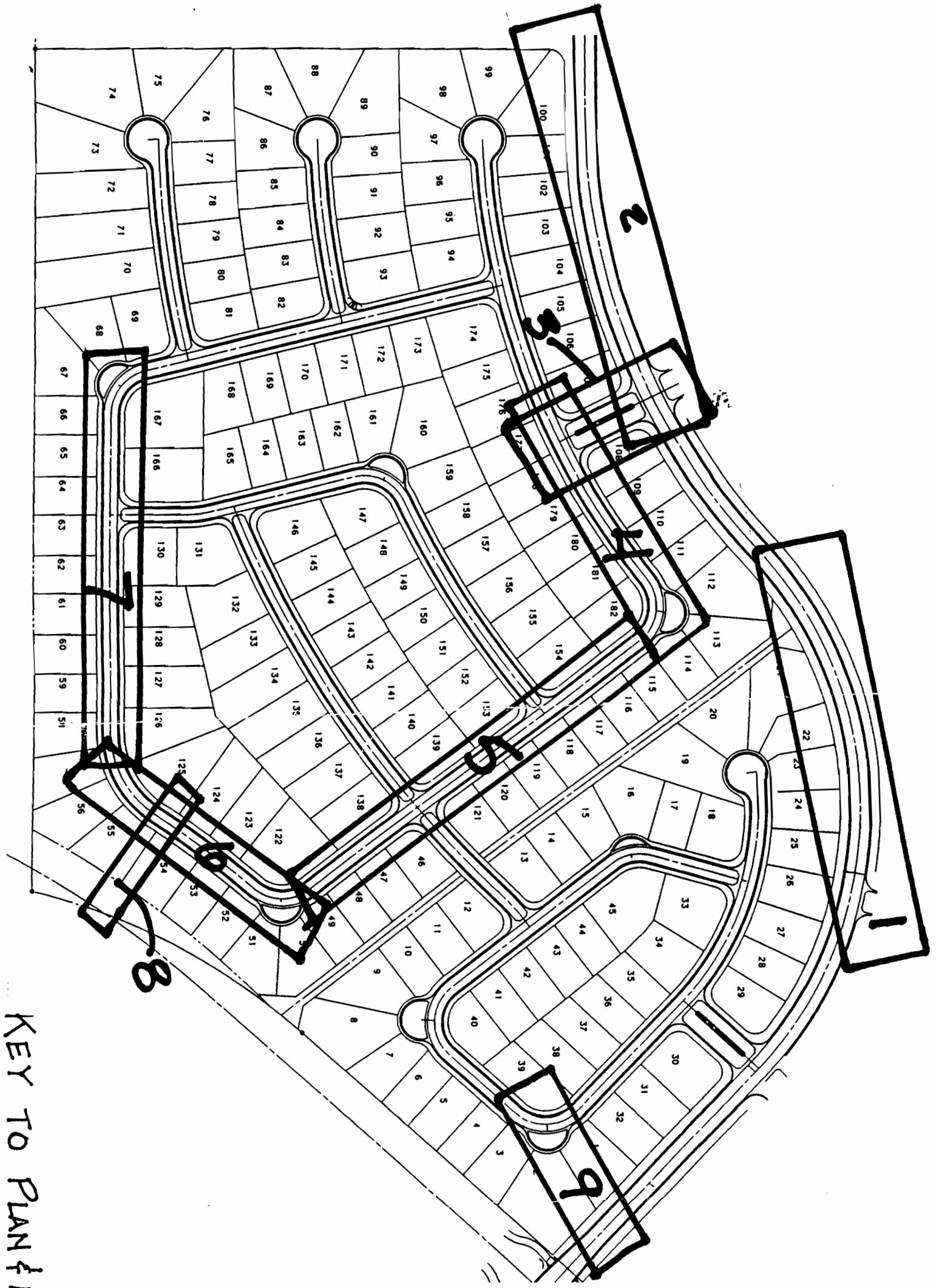
BOHANNAN-HUSTON INC.

PROJECT NAME \_\_\_\_\_ SHEET \_\_\_\_\_ OF \_\_\_\_\_  
PROJECT NO. \_\_\_\_\_ BY \_\_\_\_\_ DATE \_\_\_\_\_  
SUBJECT \_\_\_\_\_ CH'D. \_\_\_\_\_ DATE \_\_\_\_\_

**SEVEN BAR RANCH NORTH SEDIMENT YIELD ANALYSIS**  
**UNIVERSAL SOIL LOSS EQUATION**

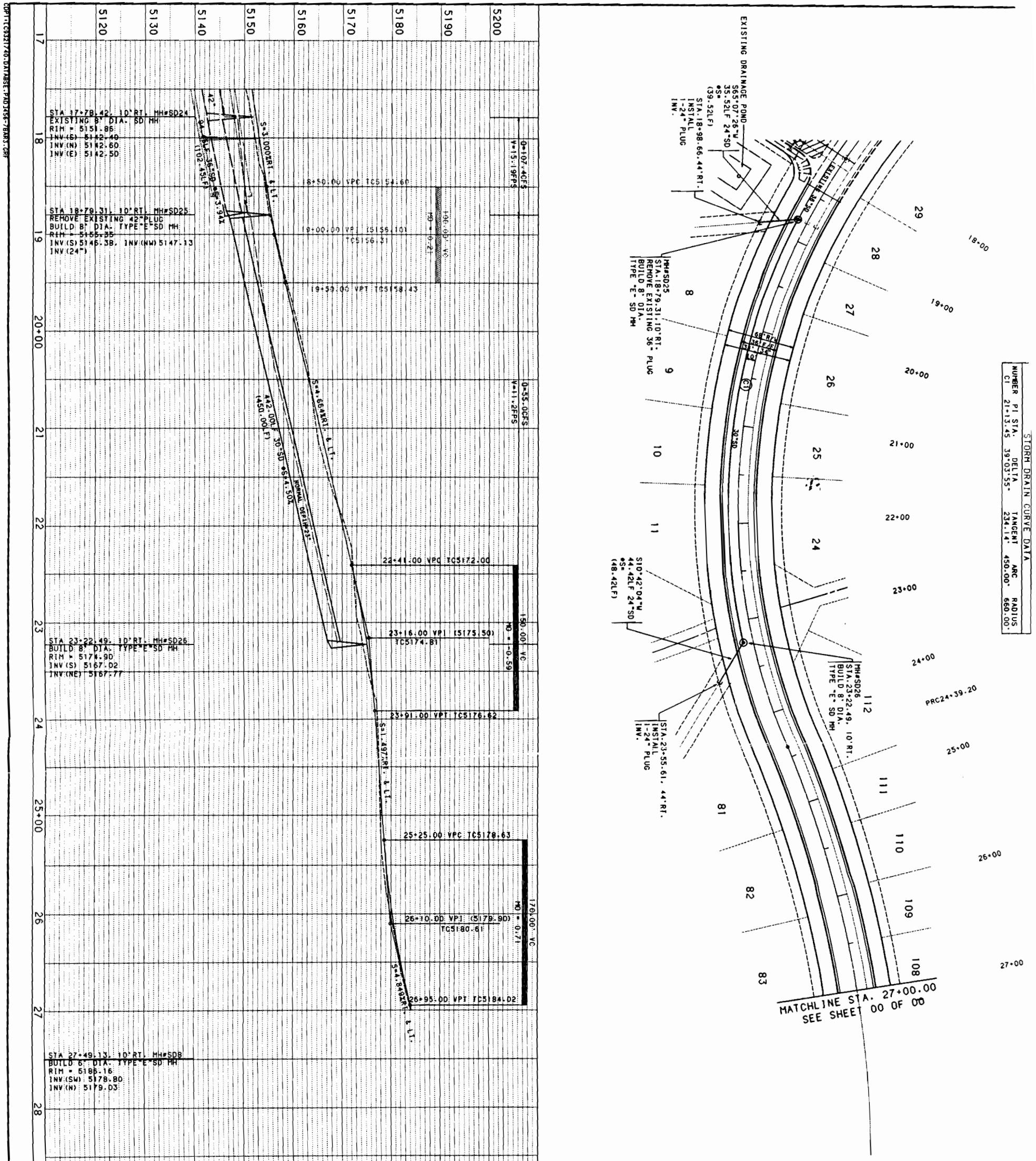
DESCRIPTION	VARIABLE	UNIT
BASIN		
Drainage Area	DA	Sq. Mi.
	S	Ft/Ft
Slope	THETA	Radians
Slope Angle	L	Feet
Rainfall	R	25.000
Soil Erodability*	K	0.240
Slope Length Factor	LS	1.682
Cover*	C	0.170
Support Practice Factor	P	1.000
Sediment Yield	A	Tons/Acre
		Tons
		Cy
Estimated Soil Unit Weight	100.000	Lbs/Cf
		Total Annual Sediment Yield
		92.744 Cy
		Adjustment Factor
		4.000
		-----
		Adjusted Sediment Yield
		370.974 Cy
		-----
		10016.299 Cf

NOTE: The Universal Soil Loss Equation typically underestimates the actual sediment yield by 4 times so a factor of 4 is applied to the total annual sediment yield.



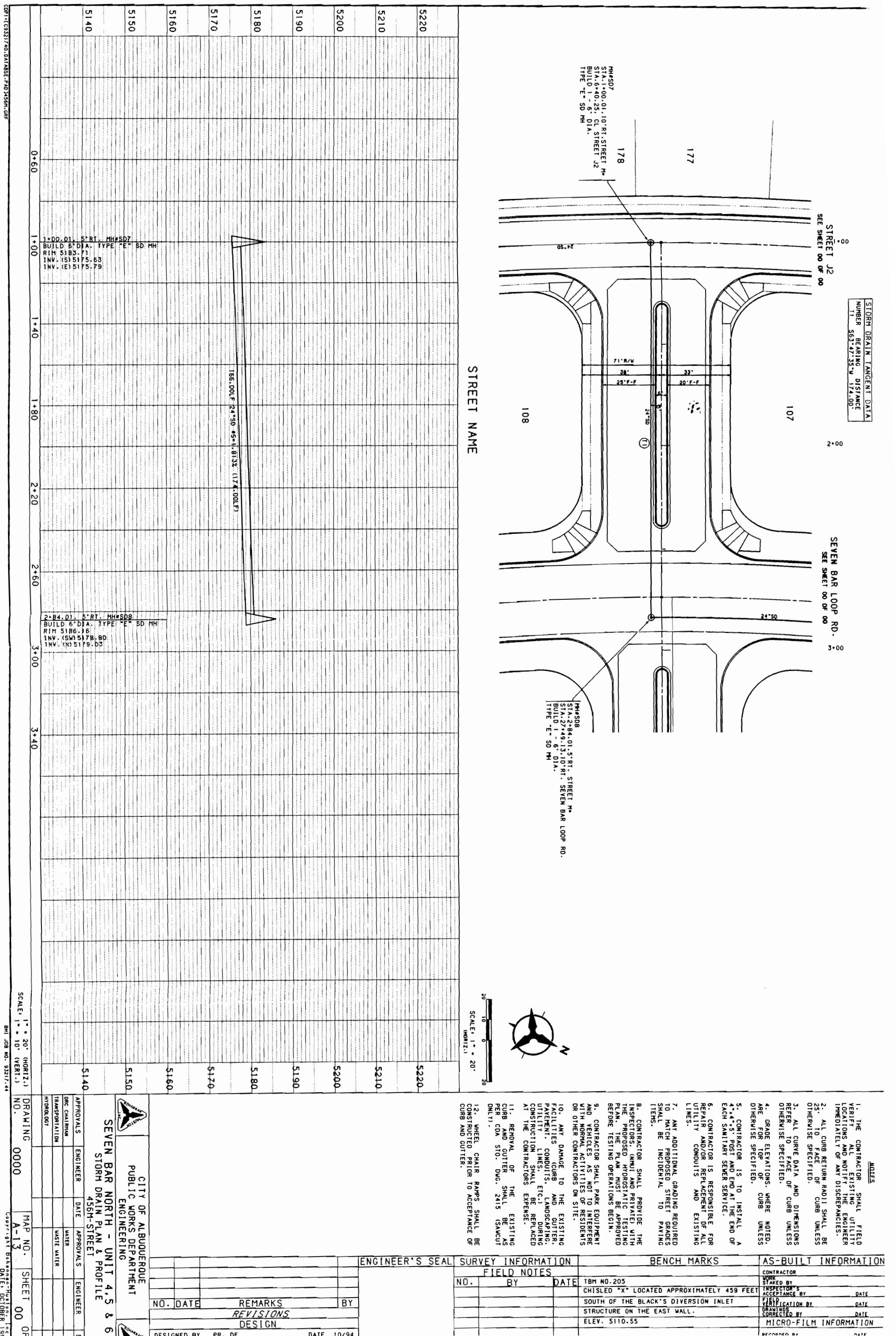
KEY TO PLAN & PROFILE SHEETS

H 1 4 , S 1 4 ( M A I N H 1 )



NOTES											
<p>1. THE CONTRACTOR SHALL FIELD VERIFY ALL EXISTING UTILITY LOCATIONS AND NOTIFY THE ENGINEER IMMEDIATELY OF ANY DISCREPANCIES.</p> <p>2. ALL CURB RETURN RADII SHALL BE 25' TO FACE OF CURB UNLESS OTHERWISE SPECIFIED.</p> <p>3. ALL CURVE DATA AND DIMENSIONS REFER TO FACE OF CURB UNLESS OTHERWISE SPECIFIED.</p> <p>4. GRADE ELEVATIONS WHERE NOTED ARE FOR TOP OF CURB UNLESS OTHERWISE SPECIFIED.</p> <p>5. CONTRACTOR IS TO INSTALL A 4"-4 1/2" POST AND END AT THE END OF EACH SANITARY SEWER SERVICE.</p> <p>6. CONTRACTOR IS RESPONSIBLE FOR REPAIR AND/OR REPLACEMENT OF ALL UTILITY CONDUITS AND EXISTING LINES.</p> <p>7. ANY ADDITIONAL GRADING REQUIRED TO MATCH PROPOSED STREET GRADES SHALL BE INCIDENTAL TO PAYING ITEMS.</p> <p>8. CONTRACTOR SHALL PROVIDE THE INSPECTORS (MUNI AND PRIVATE) WITH THE PROPOSED HYDROSTATIC TESTING PLAN. THE PLAN MUST BE APPROVED BEFORE TESTING OPERATIONS BEGIN.</p> <p>9. CONTRACTOR SHALL PARK EQUIPMENT AND VEHICLES AS NOT TO INTERFERE WITH NORMAL ACTIVITIES OF RESIDENTS OR OTHER CONTRACTORS ON SITE.</p> <p>10. ANY DAMAGE TO THE EXISTING PAVEMENT, CONDUITS, LANDSCAPING, UTILITY LINES, ETC., DURING CONSTRUCTION SHALL BE REPAID AT THE CONTRACTOR'S EXPENSE.</p> <p>11. REMOVAL OF THE EXISTING CURB AND GUTTER SHALL BE AS PER COA STD. DUG. 2415 (SAMCUT ONLY).</p> <p>12. WHEEL CHAIR RAMPS SHALL BE CONSTRUCTED PRIOR TO ACCEPTANCE OF CURB AND GUTTER.</p>											
<p><b>SEVEN BAR NORTH - UNIT 4, 5 &amp; 6 STORM DRAIN PLAN &amp; PROFILE SEVEN BAR LOOP ROAD</b></p>											
<p><b>5120</b></p>											
<p><b>CITY OF ALBUQUERQUE PUBLIC WORKS DEPARTMENT ENGINEERING</b></p>											
<p><b>REVISIONS DESIGN</b></p>											
<p>DESIGNED BY: RR DE DATE: 10/94</p>											
<p>APPROVALS      APPROVALS      APPROVALS      APPROVALS</p>											
ENG. CHAIRMAN	WATER	WATER	WATER	WATER	WATER	WATER	WATER	WATER	WATER	WATER	WATER
TRANSPORTATION	WASTE WATER	WASTE WATER	WASTE WATER	WASTE WATER	WASTE WATER	WASTE WATER	WASTE WATER	WASTE WATER	WASTE WATER	WASTE WATER	WASTE WATER
HDR/LGT											
0' (HORIZ.) NO. (VERT.)	DRAWING NO. 0000	MAP NO. A-13	SHEET 00	00	00	00	00	00	00	00	00
<p>Copyright Behannon-Houston, Inc. Drawing No. 93217-44</p>											

H 1 6 S 1 6 (MAIN H 1 0)



**STORM DRAIN CURVE DATA**

NUMBER PI STA. DELTA TANGENT ARC RADIUS  
C1 7+5.36 12'06"26" 135.11 269.21 1274.00.

**STORM DRAIN TANGENT DATA**

NUMBER BEARING DISTANCE  
T1 S37°08'41"E 76.95'  
T2 S52°51'19"W 320.88'

6+00

7+00

8+00

9+00

10+00

11+00

12+00

13+00

14+00

15+00

16+00

17+00

18+00

19+00

20+00

21+00

22+00

23+00

24+00

25+00

26+00

27+00

28+00

29+00

30+00

31+00

32+00

33+00

34+00

35+00

36+00

37+00

38+00

39+00

40+00

41+00

42+00

43+00

6+00

7+00

8+00

9+00

10+00

11+00

12+00

13+00

14+00

15+00

16+00

17+00

18+00

19+00

20+00

21+00

22+00

23+00

24+00

25+00

26+00

27+00

28+00

29+00

30+00

31+00

32+00

33+00

34+00

35+00

36+00

37+00

38+00

39+00

40+00

41+00

6+00

7+00

8+00

9+00

10+00

11+00

12+00

13+00

14+00

15+00

16+00

17+00

18+00

19+00

20+00

21+00

22+00

23+00

24+00

25+00

26+00

27+00

28+00

29+00

30+00

31+00

32+00

33+00

34+00

35+00

36+00

37+00

38+00

39+00

40+00

41+00

6+00

7+00

8+00

9+00

10+00

11+00

12+00

13+00

14+00

15+00

16+00

17+00

18+00

19+00

20+00

21+00

22+00

23+00

24+00

25+00

26+00

27+00

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29+00

30+00

31+00

32+00

33+00

34+00

35+00

36+00

37+00

38+00

39+00

40+00

41+00

6+00

7+00

8+00

9+00

10+00

11+00

12+00

13+00

14+00

15+00

16+00

17+00

18+00

19+00

20+00

21+00

22+00

23+00

24+00

25+00

26+00

27+00

28+00

29+00

30+00

31+00

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34+00

35+00

36+00

37+00

38+00

39+00

40+00

41+00

6+00

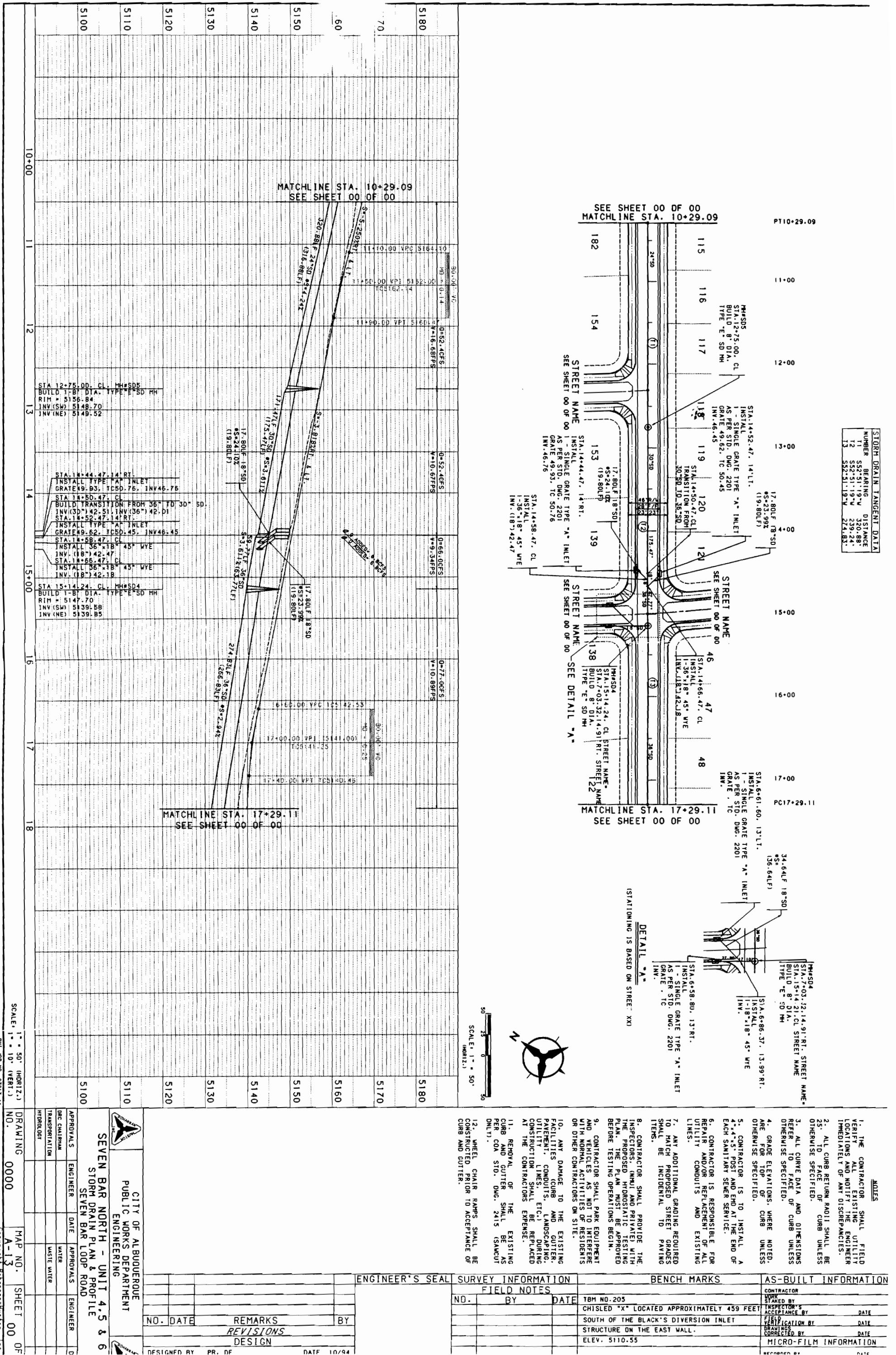
7+00

8+00

9+00

10+00

H 1 9 4 6 1 S 1 9 (M A T I N H 6)



H20 ▷ H21 ▷ S20 (MAIN H7)

