



**DRAINAGE REPORT FOR  
ELLISON DRIVE IMPROVEMENTS**  
(COORS BOULEVARD BYPASS TO GOLF COURSE ROAD)  
Prepared for:

**BROWN/NZD DEVELOPMENT JOINT  
VENTURE  
C/O BROWN & ASSOCIATES  
3411 CANDELARIA NE  
ALBUQUERQUE, NEW MEXICO 87107**

Prepared by:

Job No. 94306.40



**BOHANNAN-HUSTON INC.**

ENGINEERS ARCHITECTS PHOTOGRAMMETRISTS SURVEYORS

COURTYARD I, 7500 JEFFERSON NE ALBUQUERQUE, NM 87109 TEL (505) 823-1000 FAX (505) 321-0892

This eastern portion of the site has slopes ranging from 0.5% to 2% in a generally eastern direction. Soils are highly absorptive sandy soils with occasional clay lenses. Vegetation is light outside of the road and shoulder, consisting of grasses and small sagebrush.

### **Offsite Drainage Basins**

The only offsite basins that impact the site are those of Tracts A-2A and A-2B to the south of Ellison Drive from Seven Bar Loop Road (South) to the Black Diversion Channel. This basin is shown on Plate 6 (Existing Conditions Map inset on the Conceptual Drainage Plan for the platting of Tracts A-1A, A-2A and A-2B Seven Bar Ranch dated September, 1994 by Bohannon Huston, Inc. (CoA Hydrology File # A13/D8)). The basin generates an undeveloped flow of 11.29 cfs during the 100-year storm.

## **IV. PROPOSED DEVELOPED CONDITIONS**

The proposed project has been divided into two phases on both of the portions east and west of the Black Diversion Channel. Ellison Drive will ultimately consist of six traffic lanes and a median from Golf Course Road to the Coors Boulevard Bypass. Phase I will construct the outer 4 traffic lanes and Phase II will complete the inner 2 lanes, median and bridge widening at the Black Diversion Channel. Currently, the SAD 223 is under construction and is anticipated to be complete by the Fall of 1996. Phase I of this project will be complete by the end of 1995. The start of Phase II construction will depend on the development of the tracts to the north of Ellison Drive and east of the Black Diversion Channel, it is not anticipated that Phase II will be required prior to the completion of the SAD 223.

## **Construction east of the Black Diversion Channel**

Phase II construction of Ellison Drive east of the Black Diversion Channel includes two inside traffic lanes and a median from the Black Diversion Channel to the Coors Boulevard Bypass, and an extension of the Phase I storm drain from the intersection of Ellison Drive and Cibola Loop East to the intersection of Ellison Drive and Cibola Loop West. This storm drain extension will convey the off-site flows from Tract B-9G, a portion of Tract B-9H and the Cibola Loop West right-of-way, and will be built either with the Phase II pavement or with the development of Tracts B-9G and B-9H, whichever occurs first. The Phase I storm drain is designed for the flows at the full build-out (Phase II) of Ellison and the tracts to the north (see Offsite Basins below). The Phase I median is wide enough to accommodate the construction of this storm drain extension prior to the inner two traffic lanes being built, if this is necessary. Please refer to Plate 8.

## **Offsite Basins west of Black Diversion Channel**

Most of the residential lots planned for Tract A-2A and located adjacent to Ellison Drive require either backyard ponds or curb drains to Ellison Drive due to elevation differences between pads and Ellison Drive. The street section and the storm drain in Ellison Drive west of the Diversion Channel has been design to accommodate these flows should a curb drain option be approved for this subdivision.

Tract A-2B, the site planned for a school by APS, is currently under design by Wilson and Company. The Conceptual Drainage Plan for the platting of Tracts A-1A, A-2A and A-2B Seven Bar Ranch (dated September, 1994 by Bohannon Huston, Inc. (CoA Hydrology File # A13/D8)), allows for free discharge from the northern portion of this tract. The street section and the storm drain in Ellison Drive west of the Diversion Channel has been design to accommodate the free discharge of these flows up to 21.67 cfs without ponding onsite. Please refer to Plate 6.

As discussed in the existing conditions section above, the tracts to the south of Ellison Drive generate 11.29 cfs in their undeveloped conditions. Prior to development of these site, a swale on the south side of the proposed Ellison Drive and in the right-of-way will convey existing flows east to the maintenance road adjacent to the Black Diversion Channel. This swale will discharge less flow onto the maintenance road than currently because the curb and gutter being built with Ellison Drive will intercept all impervious flow.

#### **Offsite Basins east of Black Diversion Channel**

For all the Tracts that eventually discharge into the Ellison Drive storm drain system as designed herein, the flows were taken directly from the SAD No. 223 Drainage Management Plan dated May, 1991 by Easterling and Associates, Inc. (CoA Hydrology File # A01/D223). That report describes detailed requirements for onsite ponding and allowable release rates, no attempt was made here to justify or modify these. Please refer to Plate 7.

#### **V. PHASING/BUILDING PERMIT/FINAL PLAT APPROVALS**

This report requests CoA/Hydrology approval for the phased infrastructure improvement plans for Ellison Drive between the Coors Boulevard Bypass and Golf Course Road. These improvements include the construction of 4 traffic lanes, a masterplan sanitary sewer line and the phased construction of two storm drain systems.

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CONNECTION  
TO EXISTING  
STORM DRAIN

3+00  
4+00  
5+00  
6+00  
7+00  
8+00

STA 3+63.27 21.60' LT  
INV=82.00

STA 4+18.05 10' RT  
BUILD 1-4' SD MH

STA 6+18.37 10' RT  
BUILD 1-6' SD MH

STA 6+47.13 18' LT  
BUILD 1-DOUBLE "C"  
CATCH BASIN

CHANDLER DRIVE  
SEE CITY PROJECT  
#5010.90

STA 6+47.13 18' RT  
BUILD 1-DOUBLE "C"  
CATCH BASIN

STA 6+72.83-18' LT  
BUILD 1-TYPE "A"  
CATCH BASIN

STA 6+72.15  
BUILD 1-TYPE  
CATCH BAS

BLACK'S-DIVERSION-CHANNEL

ANNE & SEVEN BAR LOOP ROAD  
NEL STA 61+42.80

FOR STORM PIPE CONNECTION  
DETAIL SEE SHEET 11

SEVEN BAR LOOP ROAD

Proposed  
Entrance  
Road

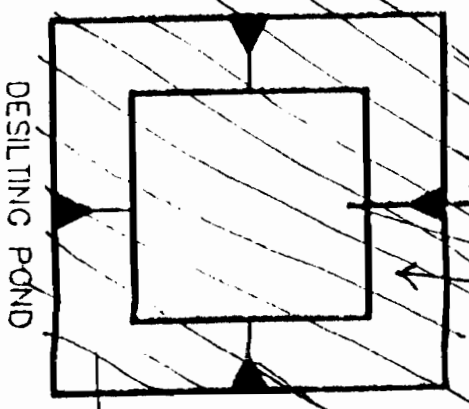
Proposed  
SD Catch  
36" Ø 1.0%  
+30.53

STA 6+31.29 140.55' RT  
INV=5101.91

NOT CONSTRUCTED

Tract A-2A

N  
↑



DESILTING POND

NOT TO EXCEED  
3:1 SLOPE  
95% COMPACTION

7 Bar Loop Road As Built 7-95

STORM PIPING CONNECTION  
TO EXISTING

63.25 LF @ 14.751%  
200.32 LF @ 4.403%  
281.63 LF @ 3.00%  
329.46 LF @ 3.00%

TRACT A-2A  
CONNECTION  
TO MH#3

EXISTING GRADE AT CL

EXISTING GRADE AT CL

TOP OF PAVI

ING AT CL

H.G.L.

IDENTICAL

POINTS

EX. 4" PR. RELIEF PIPE

NEW WATER LINE

NEW SAS

NEW SAS

+72.50 NEW SAS MH

+63.27  
INV=5082.00

+18.05 MH#3A  
BUILD 1-4' SD MH  
RIM=5107.79  
INV IN=5091.43  
INV OUT=5091.33

+48.05 CB8B-18'-LT  
+48.05 CB7B-18'-RT  
BUILD 1-DBL'C' CB LT  
AND 1-DBL'C' CB RT  
CB7B-GRADE=5107.54  
INV=103.01  
CB8B-GRADE=107.56  
INV=104.32

+18.37 MH#3  
BUILD 1-6' SD MH  
RIM=5110.49 5110.46  
INV IN=5100.35-FROM MH#4  
INV IN=5103.72-FROM CB8-5101.26  
INV OUT=5100.25 5101.16

+47.13 CB8 18' LT  
+47.13 CB7 18' RT

BUILD 1-DBL'C' CB LT  
AND 1-DBL'C' CB RT --  
GRADE=5111.30 5110.84  
CB7 INV=5105.46 5108.73  
CB8 INV IN=5104.50 5110.88  
CB8 INV OUT=5104.40 5107.75  
CB8 GRADE=5110.95

+62.83 CB8A 18' LT  
+62.15 CB7A 18' RT  
BUILD TYPE "A" CB LT & RT  
CB8A GRADE=5111.56 5111.41  
INV IN=5105.10  
INV OUT=5105.00 5110.41  
CB7A GRADE=5111.54 5111.30  
INV IN=5106.10  
INV OUT=5106.00 5109.75

+00 MH#4  
BUILD 1-4' SD MH  
RIM=5116.76  
INV IN=5108.90  
INV OUT=5108.80

3+00  
4+00  
5+00  
6+00  
7+00  
8+00  
9+00  
10+00  
11+00

Bar Locat Road As-Built 7-28-95

F.22

**7-Bar Loop Road Drainage Calculations  
Worksheet for Irregular Channel**

*Sta 13+95?*

*36' F-F*

Project Description	
Project File	c:\haestad\fmw\7-barlp.fm2
Worksheet	7-barlp
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data	
Channel Slope	0.080000 ft/ft ✓
Elevation range: 99.64 ft to 100.64 ft.	
Station (ft)	Elevation (ft)
100.00	100.64
116.00	100.31
116.05 <i>118</i>	<del>99.64</del> <i>99.86</i>
134.00	100.00
151.95 <i>150</i>	<del>99.64</del> <i>99.86</i>
152.00	100.31
168.00	100.64
Discharge	14.30 cfs ✓

Start Station  
100.00

End Station  
168.00

Roughness  
0.014

*n = 0.017*

*Gutter Lip*  
*100.18*

*EXISTING DOWNSTREAM*

Results	
Wtd. Mannings Coefficient	0.014
Water Surface Elevation	99.85 ft
Flow Area	2.18 ft <sup>2</sup>
Wetted Perimeter	21.24 ft
Top Width	20.85 ft
Height	0.21 ft
Critical Depth	99.99 ft
Critical Slope	0.005244 ft/ft
Velocity	6.57 ft/s
Velocity Head	0.67 ft
Specific Energy	100.52 ft ✓
Froude Number	3.59
Flow is supercritical.	
Flow is divided.	

*Attachment*



**7-Bar Loop Road Drainage Calculations  
Worksheet for Irregular Channel**

Project Description	
Project File	c:\haestad\fmw\7-barlp.fm2
Worksheet	7-barlp
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Sta 10+00?  
36' F-F

Input Data				
Channel Slope	0.017930 ft/ft ✓			
Elevation range: 99.64 ft to 100.64 ft.				
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness
100.00	100.64	100.00	168.00	0.014
116.00	100.31			
116.05	99.64			
134.00	100.00			
151.95	99.64			
152.00	100.31			
168.00	100.64			
Discharge	7.50	cfs	✓ EXISTING UPSTREAM	

Results		
Wtd. Mannings Coefficient	0.014	
Water Surface Elevation	99.86	ft
Flow Area	2.35	ft <sup>2</sup>
Wetted Perimeter	22.07	ft
Top Width	21.66	ft
Height	0.22	ft
Critical Depth	99.91	ft
Critical Slope	0.005717	ft/ft
Velocity	3.19	ft/s
Velocity Head	0.16	ft
Specific Energy	100.02	ft ✓
Froude Number	1.71	
Flow is supercritical.		
Flow is divided.		

# 7-Bar Loop Road Drainage Calculations Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\7-barlp.fm2
Worksheet	7-barlp
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Sta 13+95

Input Data	
Channel Slope	0.080000 ft/ft
Elevation range: 99.64 ft to 100.64 ft.	
Station (ft)	Elevation (ft)
100.00	100.64
116.00	100.31
116.05	99.64
134.00	100.00
151.95	99.64
152.00	100.31
168.00	100.64
Discharge	28.90 cfs

CRT AL 0.014

$n = 0.017$   
100.18 Gutter Lip

Proposed

Results	
Wtd. Mannings Coefficient	0.014
Water Surface Elevation	99.91 ft
Flow Area	3.69 ft <sup>2</sup>
Wetted Perimeter	27.65 ft
Top Width	27.14 ft
Height	0.27 ft
Critical Depth	100.09 ft
Critical Slope	0.004549 ft/ft
Velocity	7.84 ft/s
Velocity Head	0.95 ft
Specific Energy	100.87 ft
Froude Number	3.75
Flow is supercritical.	
Flow is divided.	

$$d = 0.37'$$

$$V = 6.9 \text{ fps}$$

$$E = 0.37 + \frac{(6.9)^2}{2g} = 1.11'$$

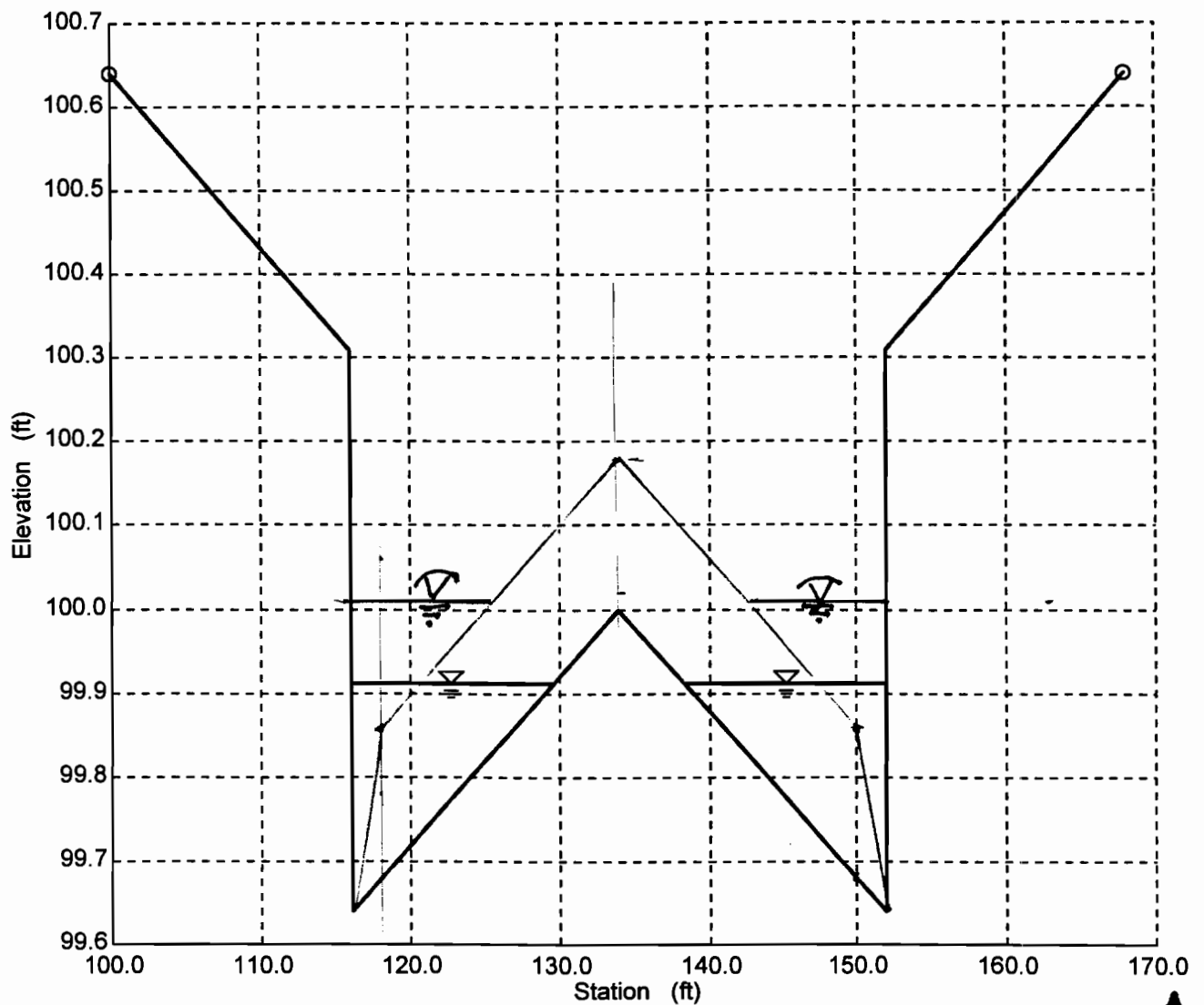
$$= 100.75'$$

A

# Cross Section Cross Section for Irregular Channel

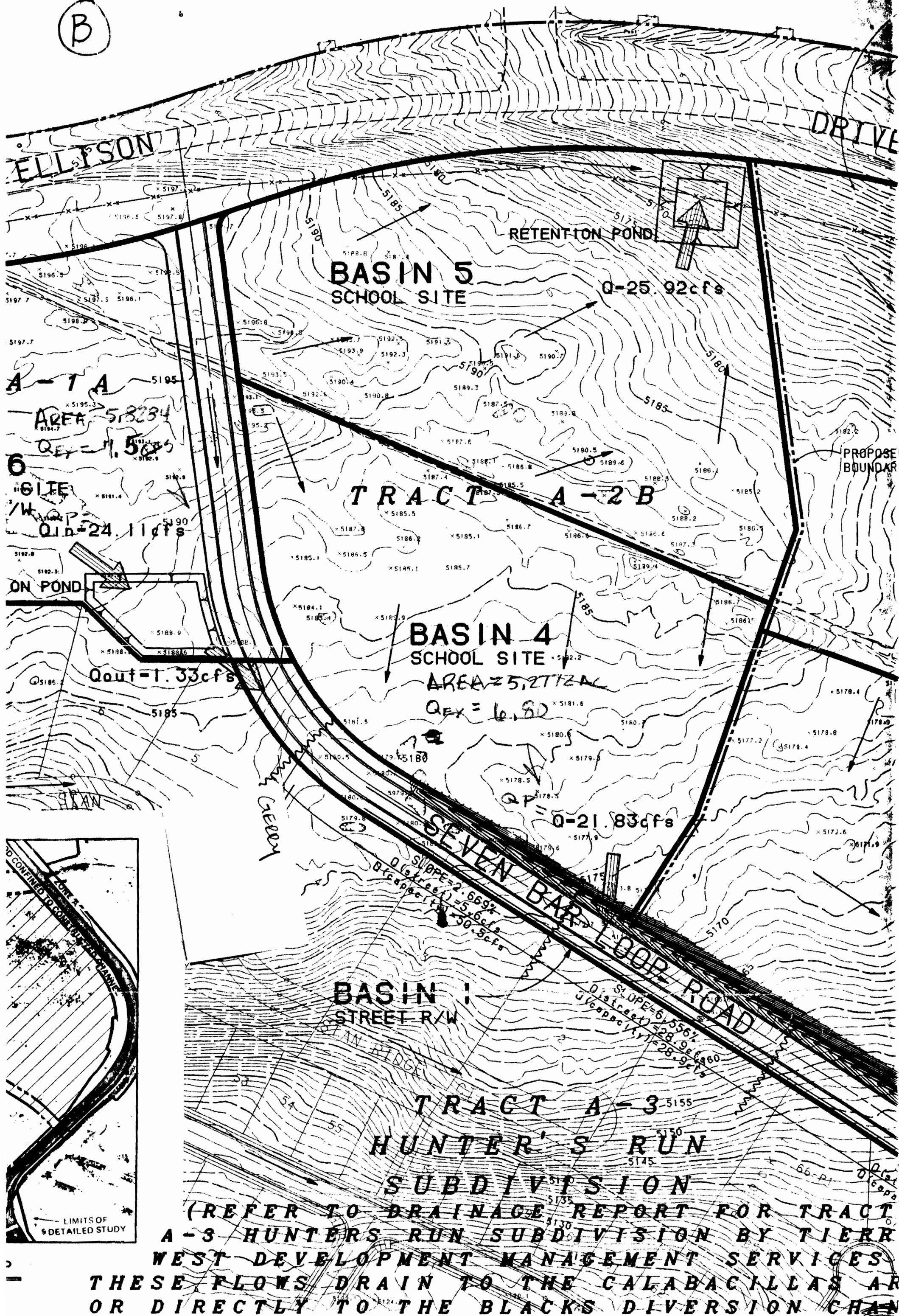
Project Description	
Project File	c:\haestad\fmw\7-barlp.fm2
Worksheet	7-barlp
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Section Data	
Wtd. Mannings Coefficient	0.014
Channel Slope	0.080000 ft/ft
Water Surface Elevation	99.91 ft
Discharge	28.90 cfs



A

③



BASIN ID	AREA (ACRES)	COMPOSITE % LAND TREATMENT			RATIONAL METHOD PEAK DISCHARGE C(cfs/ac)	RATIONAL METHOD RUNOFF Q-100(cfs)	RATIONAL METHOD RUNOFF Q-10(cfs)	COMPOSITE EXCESS PRECIP. E	RATIONAL METHOD 24-HR VOLUME V-100(ac-ft)
		A	B	C					
	3.2872	0	28	0	3.71	12.21	7.54	1.61	0.44
2	23.4938	0	29	29	3.26	76.51	43.85	1.31	2.56
3	19.2441	0	29	29	3.26	62.67	35.92	1.31	2.10
4	5.1407	0	10	0	4.14	21.26	13.76	1.84	0.79
5	6.3596	0	10	0	4.14	26.30	17.02	1.84	0.98
6	5.7821	0	10	0	4.14	23.91	15.48	1.84	0.89
	63.3075					222.8630			7.7512

NOTE:

**RAINFALL DATA FOR 100-YEAR, 24-HOUR STORM**

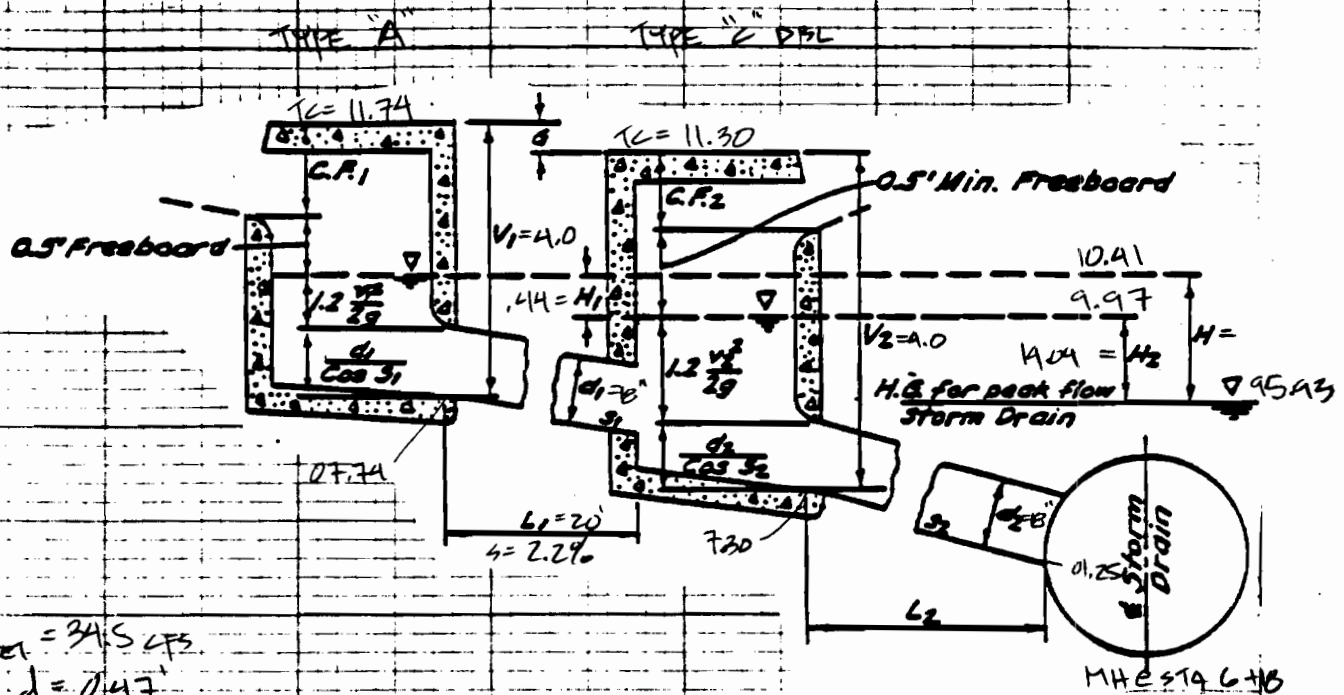
**PEAK DISCHARGE (C\*I) IN cfs/ac BY LAND TREATMENTS**

	100yr	10yr
C*I(a)=	1.29	0.24
C*I(b)=	2.03	0.76
C*I(c)=	2.87	1.49
C*I(d)=	4.37	2.89

**EXCESS PRECIPITATION (E) IN inches BY LAND TREATMENTS**

E(a)=	0.44
E(b)=	0.67
E(c)=	0.99
E(d)=	1.97

MEYEN BARK LOD ROAD - STA 5+88.91 TO 6+47



$$Q_{STREET} = 34.5 \text{ LFS}$$

$$d = 0.47$$

$$Q_{\text{GRATE}} = 784 \text{ ps} \times 2$$

$$Q_{\text{STREET}} = 18.9 \text{ cfs.}$$

$$Q_1 = 7.13 \text{ LFS}$$

$$V_1 = 4.41 \text{ FPS}$$

$$H_1 = \frac{1.2 V_1^2}{2\eta} = 0.36$$

$$V_1 = 0.83 + 0.50 + 0.36 + .5 = 3.19' \text{ USE } 4'$$

$$INV = 11.74 - 4.00 = 7.74$$

$$H_{1, \text{AVGIL}} = 0.44" > 0.36" \text{ P.E.D.}$$

$$Q_{\text{DIRECT}} = 18.9 \text{ cps}$$

$$d = 0.40 \text{ cm}$$

$$Q_{GATE} = 6.4 \text{ CPS} \times 2$$

$$Q_{STEEL} = 6.1 \text{ C/s}$$

$$Q_2 = 6.4 + 7.8 = 14.2 \text{ cfs}$$

$$V_2 = 15.04 \text{ m/s}$$

$$H_2 = \frac{1.2 \sqrt{2}}{2} = 1.2$$

$$V_2 = 0.83 + 0.50 + 1.2 + 1.5 = 4.0$$

$$114V = 11.30 - 4.0 = 7.30'$$

$$H_{2, \text{AVAIL}} = 14.04 \gg 1.2' \text{ req'd}$$



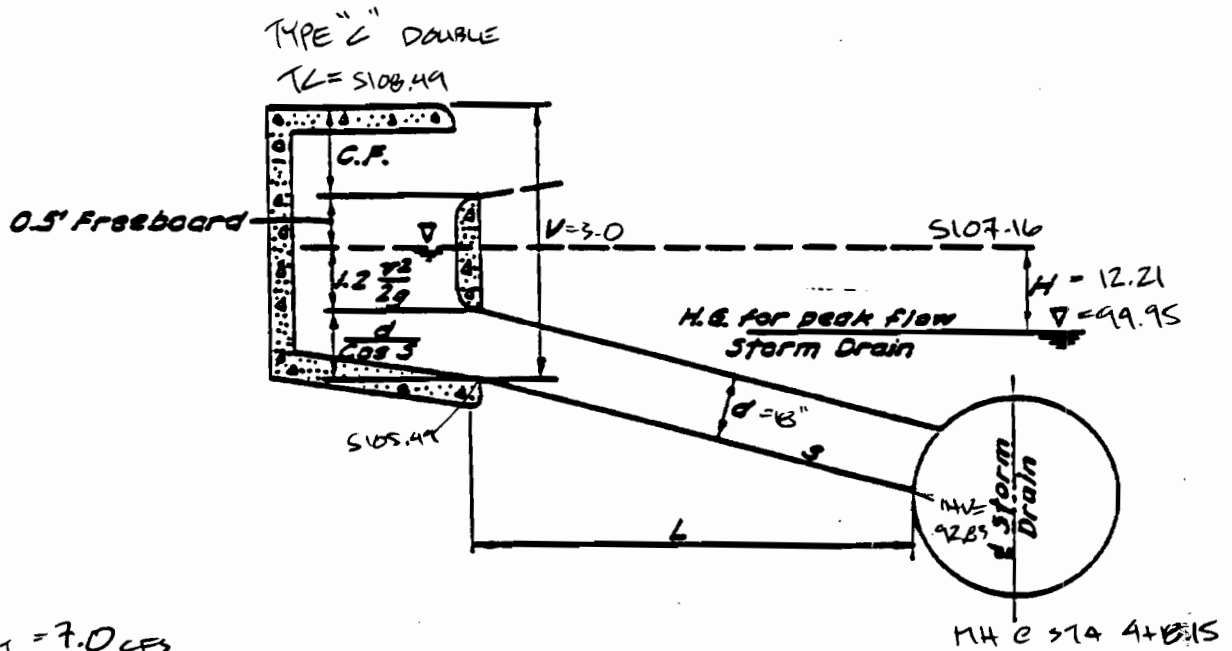
BOHANNAN-HUSTON INC.

PROJECT NAME SEVEN BAY - TRUSS A-ZA, A-ZB SHEET 1 OF 2

PROJECT NO. 94165.40 BY \_\_\_\_\_ DATE \_\_\_\_\_

PROJECT NO. \_\_\_\_\_ DT \_\_\_\_\_ DATE \_\_\_\_\_  
SUBJECT HEVEN BAR LAP ROAD INLETS CH'D \_\_\_\_\_ DATE \_\_\_\_\_

# SEVEN BAR LOOP RD - STA 4+28



$$Q_{\text{STREET}} = 7.0 \text{ cfs}$$

$$d = 0.33'$$

$$Q_{\text{GRADE}} = 3.0 \text{ cfs} \times 2$$

$$\therefore Q_{\text{STREET}} = 1.0 \text{ cfs RESIDUAL}$$

$$Q = 3.0 \text{ cfs}$$

$$V_i = 1.70 \text{ fps}$$

$$H = \frac{1.2 V^2}{2g} = 0.05'$$

$$V = 0.83 + 0.50 + 0.05 + 1.5 = 2.88, \text{ USE } 3'$$

$$\text{H.W.} = 5108.49 - 3 = 5105.49$$

$$H_{\text{AVAIL}} = 12.21 \gg 0.05 = H_{\text{REQ'D.}}$$



BOHANNAN-HUSTON INC.

PROJECT NAME SEVEN BAR - TRAIL A-2A, A-2B SHEET 2 OF 2  
PROJECT NO 94165.40 BY \_\_\_\_\_ DATE \_\_\_\_\_  
SUBJECT SEVEN BAR LOOP ROAD INLETS CH'D \_\_\_\_\_ DATE \_\_\_\_\_

TRACTS A-1 & A-1 SEVEN BAR RANCH  
 \*\*\*\*\* HYDRAULIC GRADE LINE CALCULATIONS \*\*\*\*\*

Station	Structure	Diem.	Q	Area	Vel.	K	St	Length	MH Dia.	JNCT Angle	Ht	Hb	Hj	Hm	Ht	Total Losses	HGL(dn)	HGL(up)	Low Point	HV	EGL(dn)	EGL(up)
3+63.27	OUTLET	36	110.41	7.07	15.62	667	0.0274	63.25	0.00	0.00	1.73	0.00	0.00	0.00	0.00	0.00	5065.51	5065.51	5216.02	3.79	5069.30	5069.30
4+16.15	MH	30	28.40	4.91	5.79	410	0.0046	200.32	6.00	30.00	0.98	0.21	1.37	0.00	0.98	1.96	5067.24	5062.46	5107.79	0.52	5091.03	5062.98
6+18.37	MH	18	14.20	1.77	6.04	105	0.0163	261.63	4.00	0.00	5.15	0.00	0.46	0.00	0.02	0.50	5063.42	5063.44	5110.49	1.00	5069.94	5064.44

Manning's n = 0.013  
 for pipe



SEVEN BAR TRACTS A-2A & A-2B SEDIMENT YIELD ANALYSIS  
UNIVERSAL SOIL LOSS EQUATION

DESCRIPTION	VARIABLE	UNIT
Drainage Area	DA	Sq. Mi.
Slope	S	Ft/Ft
Slope Angle	THETA	Radians
	L	Feet
		400.000
Rainfall	R	
Soil Erodability*	K	25.000
Slope Length Factor	LS	0.280
Cover*	C	0.902
Support Practice Factor	P	0.170
Sediment Yield	A	1.000
		1.073
		Tons/Acre
		30.738
		Tons
		Cy
		22.769
		Total Annual Sediment Yield
Estimated Soil Unit Weight	100.000	Lbs/Cf
		Adjustment Factor
		22.769 Cy
		4.000
		-----
		Adjusted Sediment Yield
		91.076 Cy

NOTE: The Universal Soil Loss Equation typically underestimates the actual sediment yield by 4 times so a factor of 4 is applied to the total annual sediment yield.

# West Boundary Swales

tmp#1.txt

- adjacent to site,  
on APS land

## Channel Calculator

### Given Input Data:

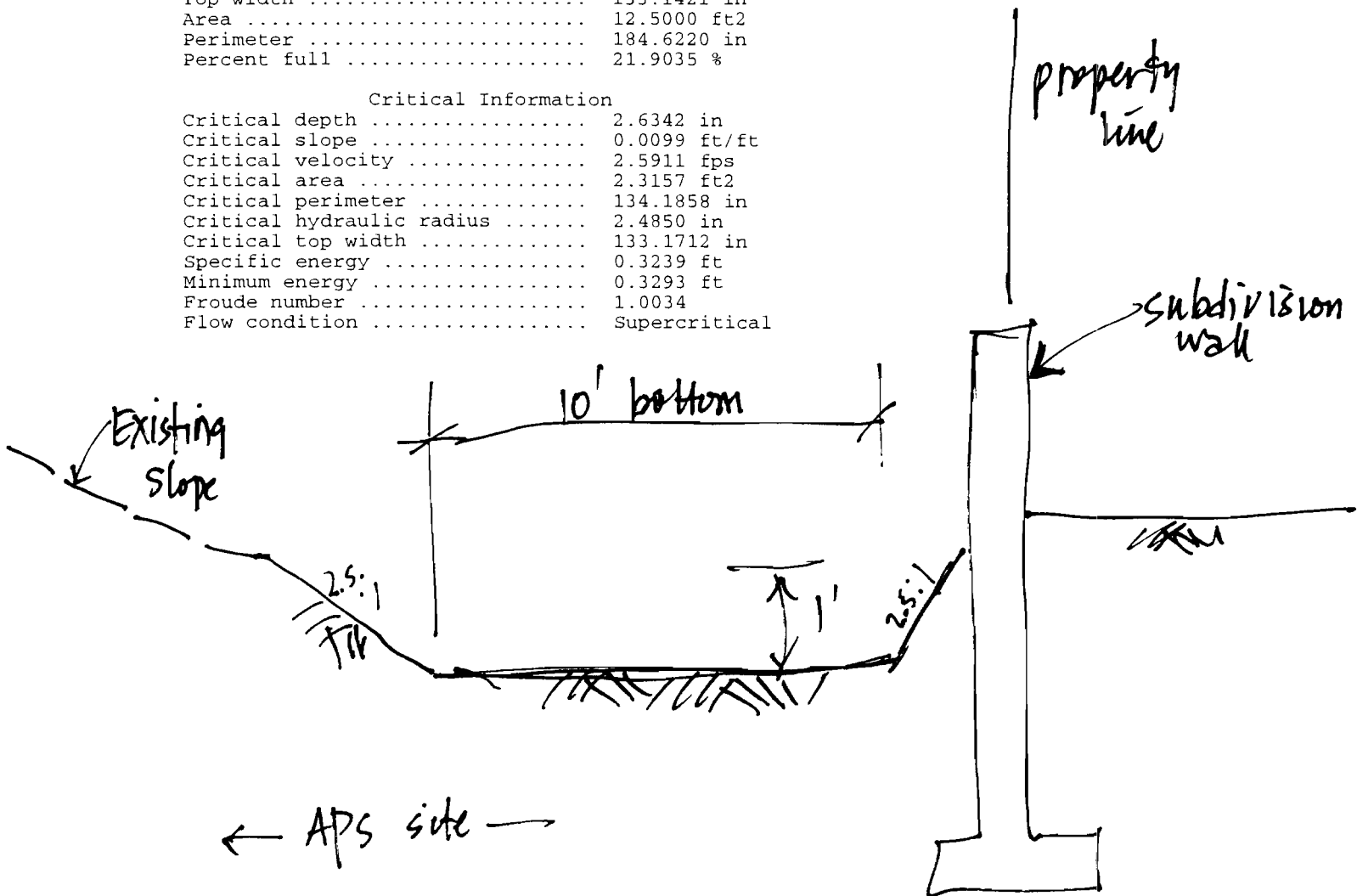
Shape .....	Trapezoidal
Solving for .....	Depth of Flow
Flowrate .....	6.0000 cfs
Slope .....	0.0100 ft/ft
Manning's n .....	0.0200
Height .....	12.0000 in
Bottom width .....	120.0000 in
Left slope .....	0.4000 ft/ft
Right slope .....	0.4000 ft/ft

### Computed Results:

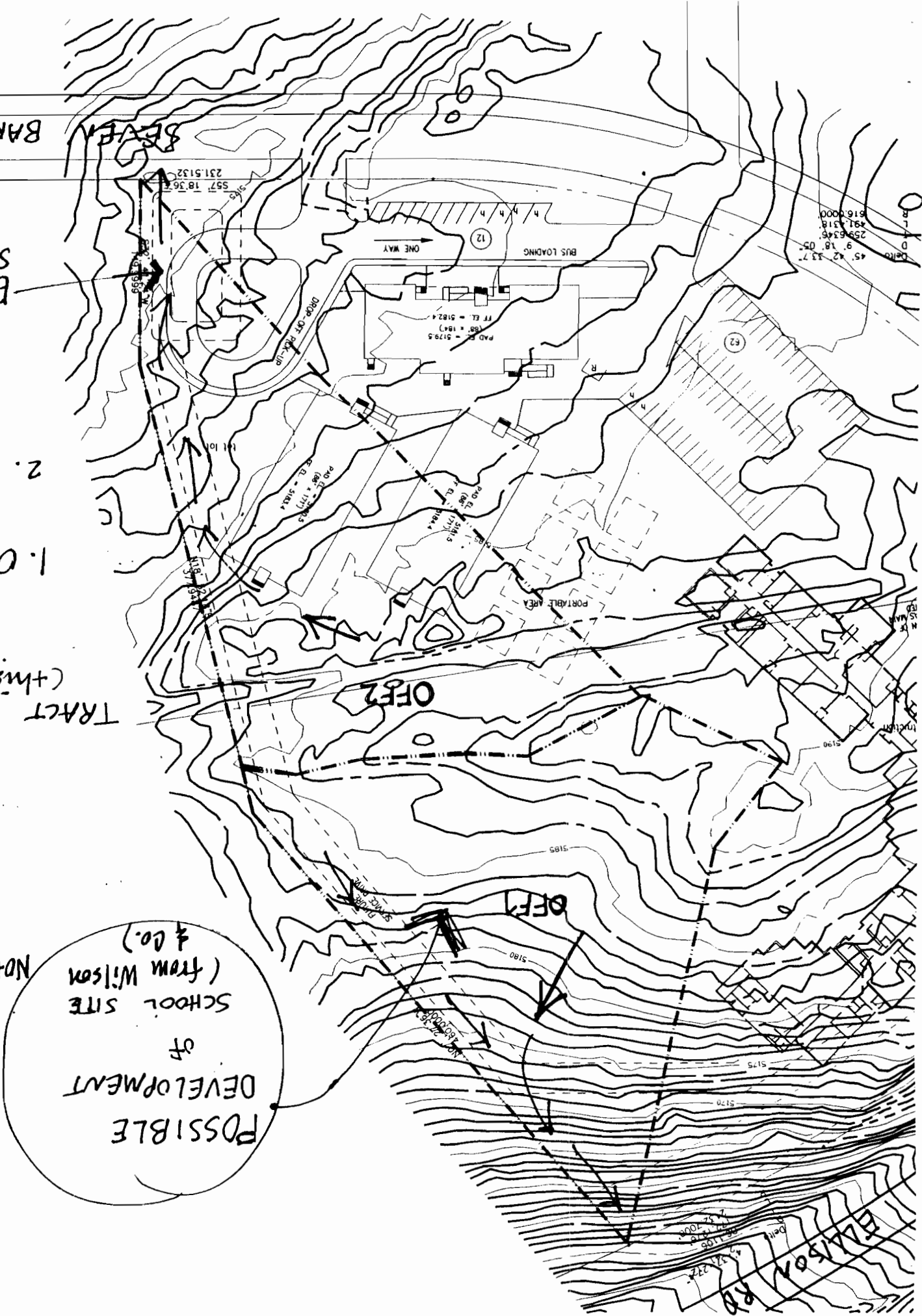
Depth .....	2.6284 in
Velocity .....	2.5971 fps
Flow area .....	2.3103 ft <sup>2</sup>
Flow perimeter .....	134.1545 in
Hydraulic radius .....	2.4798 in
Top width .....	133.1421 in
Area .....	12.5000 ft <sup>2</sup>
Perimeter .....	184.6220 in
Percent full .....	21.9035 %

### Critical Information

Critical depth .....	2.6342 in
Critical slope .....	0.0099 ft/ft
Critical velocity .....	2.5911 fps
Critical area .....	2.3157 ft <sup>2</sup>
Critical perimeter .....	134.1858 in
Critical hydraulic radius .....	2.4850 in
Critical top width .....	133.1712 in
Specific energy .....	0.3239 ft
Minimum energy .....	0.3293 ft
Froude number .....	1.0034
Flow condition .....	Supercritical



# OFFSITE MAP





**DRAINAGE REPORT FOR  
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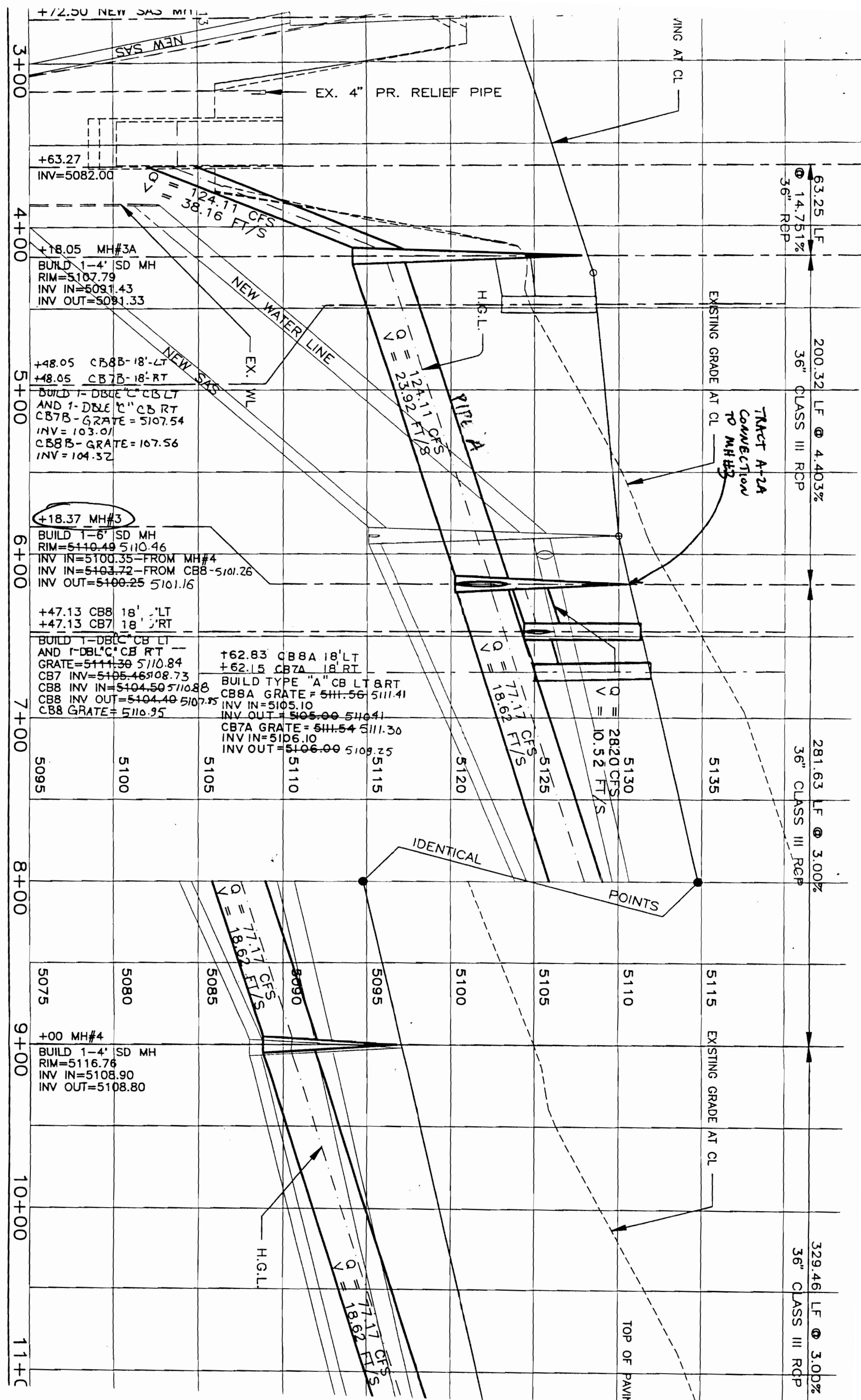
**Job No. 94306.40**



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1+00  
2+00  
3+00  
4+00  
5+00  
6+00  
7+00  
8+00

STA 3+63.27 21.60' LT  
INV=82.00

STA 6+18.37 10' RT  
BUILD 1-6' SD MH

STA 6+47.13 18' LT  
BUILD 1-DOUBLE "C"  
CATCH BASIN

STA 4+18.05 10' RT  
BUILD 1-4' SD MH

CHANDLER DRIVE  
SEE CITY PROJECT  
#5010.90

STA 6+47.13 18' RT  
BUILD 1-DOUBLE "C"  
CATCH BASIN

STA 6+72.83-18' LT  
BUILD 1-TYPE "A"  
CATCH BASIN

STA 6+72.15  
BUILD 1-TYPE  
CATCH BAS

BLACK'S DIVERSION CHANNEL

ANNE & SEVEN BAR LOOP ROAD  
NEL STA 61+42.80

FOR STORM PIPE CONNECTION  
DETAIL SEE SHEET 11

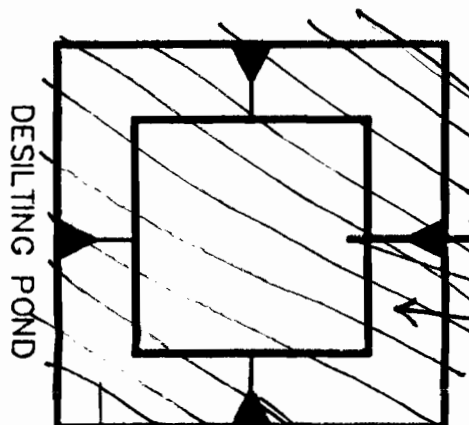
Proposed  
Entrance  
Road

Proposed  
SD Catch  
36" @ 1.0%  
130.53

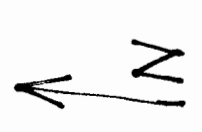
STA 6+31.29 140.55' RT  
INV=5101.91

NOT CONSTRUCTED

Tract A-2A



NOT TO EXCEED  
3:1 SLOPE  
95% COMPACTION







SCALE: 1" = 100'

GOLF COURSE ROAD

ELLISON DRIVE

BASIN 5  
SCHOOL SITE  
0-26.30 cfs

TRACT A-1A

BASIN 6  
CONCRETE  
& STREET T/Y  
0.25.01 cfs

BASIN 4  
SCHOOL SITE

BASIN 3  
SINGLE FAMILY RESIDENTIAL  
2.57 DU/AC

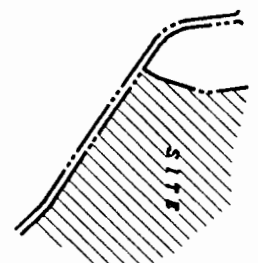
TRACT A-2B

BASIN 2  
SINGLE FAMILY RESIDENTIAL  
2.52 DU/AC

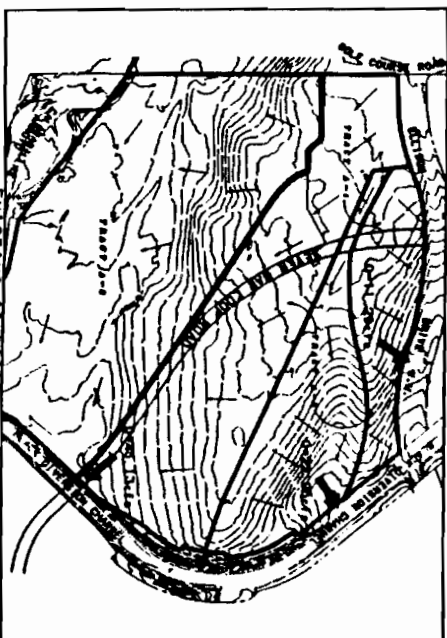
TRACT A-1A

HUNTER'S RUN  
SUBDIVISION  
A-3 HUNTER'S RUN SUBDIVISION BY TIERA  
WEST DEVELOPMENT MANAGEMENT SERVICES  
THESE DRAINS TO THE CATABOLUS ARROYO  
OR DIRECTED TO THE BLACK'S DIVERSION CHANNEL

FLOOD HAZARD MAP  
SCALE 1"=400'



LOCATION MAP  
ZONE FILES AND NO. A-13 & B-13  
NO SCALE



EXISTING CONDITIONS MAP  
EXISTING DRAINAGE, TIERA A-1 & A-2  
SCALE 1"=400'

NOTE:

1. DRAINAGE FLOWS ON BASIN 6 AND USING THE STREET OF THE STORM DRAIN SYSTEM IN SEVEN BAR LOOP ROAD AS SHOWN IN THE PREVIOUS DRAINAGE REPORT HAS BEEN REDUCED. THE SIZE AND LOCATION OF THE CONNECTION TO THE BLACK'S DIVERSION CHANNEL WILL REMAIN AS ORIGINALLY DESIGNED. THE SEVEN BAR LOOP ROAD STREET CAPACITY, 0.25.01 cfs, IS BASED ON A 36" VERTICAL CURVE AND A 36" DRAINAGE DITCH. THE 100-YEAR STORM EVENT BEING CONTAINED IN THE RIGHT-OF-WAY DURING THE 100-YEAR STORM EVENT.

HYDROLOGIC BASIN SUMMARY DATA  
PROPOSED CONDITIONS - TRACTS A-1A, A-2A & A-2B

BASIN ID	AREA (ACRES)	COMPOSITE				RATIONAL PEAK DISCHARGE (CFS)	RATIONAL PEAK DISCHARGE (CFS)	COMPOSITE PEAK DISCHARGE (CFS)	RATIONAL PEAK DISCHARGE (CFS)
		A	B	C	D	0-100 cfs	0-100 cfs	0-100 cfs	0-100 cfs
1	3.2872	0	28	0	72	3.71	12.21	7.54	1.51
2	23.4938	0	29	29	42	3.26	76.51	43.48	1.31
3	19.2441	0	29	29	42	3.26	62.67	35.92	1.31
4	5.1407	0	10	0	90	4.14	21.25	17.05	1.84
5	5.7821	0	10	0	90	4.14	23.91	15.48	1.84
6	0.0101	0	10	0	90	4.14	23.91	15.48	1.84
7	63.3075	0	10	0	90	4.14	222.8630	15.48	1.84

RAINFALL DATA FOR 100-YEAR, 24-HOUR STORM

PEAK DISCHARGE (CFS) IN cfs/AC BY LAND TREATMENTS	0-100 cfs	0-100 cfs	0-100 cfs	0-100 cfs
C(1) 1.29	0.24	0.24	0.24	0.24
C(1) 2.03	0.76	0.76	0.76	0.76
C(1) 2.87	1.49	1.49	1.49	1.49
C(1) 4.37	2.89	2.89	2.89	2.89
E(1) 0.44	0.44	0.44	0.44	0.44
E(1) 0.67	0.67	0.67	0.67	0.67
E(1) 0.99	0.99	0.99	0.99	0.99
E(1) 1.97	1.97	1.97	1.97	1.97

DRAINAGE MANAGEMENT PLAN  
DEVELOPED CONDITIONS

1. THE DEVELOPED FLOWS IN BASIN 1, THE SEVEN BAR LOOP RIGHT-OF-WAY, ARE COLLECTED IN A STORM DRAIN SYSTEM AND DISCHARGED TO THE BLACK'S DIVERSION CHANNEL.
2. THE DEVELOPED FLOWS FROM BASIN 2, THE SOUTHERN PORTION OF TRACT A-2A, A PROPOSED SINGLE FAMILY RESIDENTIAL SUBDIVISION, ARE CONVEYED INTERNALLY AS STREET FLOWS TO A LOW POINT AT THE SOUTHEAST CORNER OF BASIN 2. THE FLOWS ARE THEN COLLECTED IN A STORM DRAIN SYSTEM INSIDE THE SUBDIVISION WHICH CONNECTS TO THE STORM DRAIN BUILT IN SEVEN BAR LOOP ROAD AND DISCHARGE INTO THE BLACK'S DIVERSION CHANNEL.
3. THE DEVELOPED FLOWS FROM BASIN 3, THE NORTHERN PORTION OF TRACT A-2A, A PROPOSED SINGLE FAMILY RESIDENTIAL SUBDIVISION, ARE CONVEYED INTERNALLY AS STREET FLOWS TO A LOW POINT AT THE SOUTHEAST CORNER OF BASIN 3. THE FLOWS ARE THEN COLLECTED IN A STORM DRAIN SYSTEM INSIDE THE SUBDIVISION AND DISCHARGE INTO THE BLACK'S DIVERSION CHANNEL VIA A NEW CHANNEL, CONVECTION WITH THE APPROVAL OF MAFAC/ACC.
4. THE DEVELOPED FLOWS FROM BASIN 4, THE PROPOSED SCHOOL SITE, ARE CONVEYED SOUTH TO SEVEN BAR LOOP ROAD WHERE THEY DISCHARGE INTO SEVEN BAR LOOP ROAD AS STREET FLOW.
5. THE DEVELOPED FLOWS FROM BASIN 5, THE PROPOSED SCHOOL SITE, TRACT A-2B, ARE RETAINED ON SITE DUE TO GRADE CONSTRAINTS AND THE INABILITY TO DISCHARGE IN THE 100-YEAR, 10-DAY DEVELOPED VOLUME IS 1.43 AC-FT. WITH THE CONSTRUCTION OF ELLISON DRIVE, ANOTHER SECTION OF ELLISON DRIVE AND SEVEN BAR LOOP ROAD COULD BE CONVEYED TO A RETENTION POND WITH A CONTROLLED DISCHARGE TO THE BLACK'S DIVERSION CHANNEL. IF THE CAPACITY IN ELLISON IS PROVED TO EXIST AT THE TIME OF DEVELOPMENT OF THE SCHOOL SITE.
6. THE DEVELOPED FLOWS FROM BASIN 6, TRACT A-1A, A PROPOSED COMMERCIAL SITE, ARE CONVEYED TO THE SOUTHEAST CORNER OF BASIN 6 INTO A DETENTION POND WITH A CONTROLLED DISCHARGE OF 2.00 CFS INTO SEVEN BAR LOOP ROAD AS STREET FLOW.

LEGEND

- DRAINAGE FLOW
- DRAINAGE BASIN BOUNDARY
- TRACT BOUNDARY
- EXISTING CONTOUR
- SEVEN BAR LOOP ROAD R/W
- BASIN DRAINAGE OUTFALL (DEVELOPED FLOWS)

CONCEPTUAL DRAINAGE PLAN  
PROPOSED PLATTING:  
TRACTS A-1A, A-2B AND A-2A  
SEVEN BAR RANCH  
NOVEMBER, 1994







Descollado & Ridgrunner

$$Q = 47.5 \times 2 = 95.0 \text{ cfs}$$

Q. Upstream inlets

17.2	Ridgrunner
26.4	Descollado
<hr/>	
43.6	

$$\therefore 95.0 - 43.6 = 51.4 \text{ cfs in sump grate}$$

$$A_{\text{req}} = \frac{51.4}{.6 \sqrt{2(32.2)(.8)}} = 11.94 \text{ ft}^2$$

$$1 \text{ grate} = 3.79 \text{ ft}^2 \text{ use 4 grate}$$



Ridingcircle @ Packway

$$Q = 55.9$$

$$Q_{\text{upstream}} = 11 + 7.6 = 18.6$$

$$Q_{\text{sump}} = 55.9 - 18.6 = 37.6$$

$$\frac{37.6}{3.79} = 10 \text{ grates}$$

PROJECT NAME  
PROJECT NO.  
SHEET NO.

SHEET  
NO.  
OF

OF  
DATE  
DATE

**Bohannon & Huston**

