

City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

March 5, 1999

James Topmiller, P.E. Bohannan-Huston, Inc. 7500 Jefferson NE Albuquerque, NM 87109

Attn: John C.Alexander, P.E.

RE: TRACT A-2A, SEVEN BAR NORTH, COTTONWOOD HILLS SUBDIVISION, MIRADOR SANDIA SUBDIVISION (A13-D8). Revised DRAINAGE REPORT AND FINAL GRADING & DRAINAGE PLAN FOR Amended PRELIMINARY PLAT AND Amended ROUGH GRADING PERMIT APPROVALS. ENGINEER'S STAMP DATED FEBRUARY 2, 1999.

Dear Mr. Alexander:

Based on the information provided on your February 9,1999 resubmittal, the above referenced project is apprroved for Preliminary Plat and Rough Grading Permit. See also City Consultant's letter dated February 25, 1999 (copy enclosed).

Please attach a copy of this approved plan to the construction sets prior to sign-off by Hydrology.

Prior to Certificate of Occupancy approval, an Engineer's Certification per the DPM will be required.

If I can be of further assistance, please feel free to contact me at 924-3984.

Sincerely,

John P. Mueray, P.

Hydrology

c: Andrew Garcia

REVISED DRAINAGE STUDY FOR TRACT A-2A, SEVEN BAR NORTH **COTTONWOOD HILLS SUBDIVISION MIRADOR SANDIA SUBDIVISION**

FEBRUARY 2, 1999

PREPARED BY:

BOHANNAN-HUSTON INC. COURTYARD I, 7500 JEFFERSON STREET NE ALBUQUERQUE, NM 87109

PREPARED FOR:

BROWN/NZ DEVELOPMENT JOINT VENTURE 3411 CANDELARIA NE ALBUQUERQUE, NM 87107



PREPARED BY:

UNDER THE SUPERVISION OF:

Colleen Garcia

TRACTERIAL PLANTERS PROTOGRAMMETRISTS SURVIVORS SOCIONAR DEVILOPER

John Alexander, P.E.

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I, INTRODUCTION

The original drainage study dated July 30, 1998 was approved by the City of Albuquerque Hydrology Department on September 23, 1998. However, the developer and engineer re-evaluated the grading scheme and deemed it necessary to raise a majority of the site to reduce the earthwork export. Thus, we are submitting the revised grading plans and drainage report to identify these changes.

Since the entire site could not be raised the same amount, we have a couple of streets with slopes that differ from the original report. We have attached all street capacity and drainage calculations in the Appendix. We have also expanded the original appendix to incorporate backyard pond calculations. In addition, we have included the Off-Site Conditions, per your comments dated August 20, 1998, in Appendix F. For your convenience, a copy of your letter has also been attached to Appendix F.

This Drainage Study addresses the storm runoff for the development of the property legally described as Tract A-2A of Seven Bar Ranch (described as Tract F in the Seven Bar Ranch Sector Plan). Tract A-2A is approximately 45 acres of vacant land bounded by Ellison Dr. on the north, Seven Bar Loop Rd. on the south, the Black Diversion Channel on the east and Tract A-2B on the west. This property is in the process of being subdivided into two minor subdivisions, Tract A-2A-1 and Tract A-2A-2, but this study addresses the entire Tract and thus refer to it as Tract A-2A. See **Figure 1** for the vicinity map. It is zoned R-1 and it is proposed to develop 203 total lots of detached, single family, residential housing, as well as related streets and infrastructure, in the two subdivisions.

This study was revised in order to obtain agency approval for the revised preliminary platting and revised rough grading of Tract A-2A. Prior to final plat and building permit approvals, final grading plans and work order construction plans must be approved by the City of Albuquerque (CoA) and the Albuquerque Metropolitan Arroyo Flood Control Authority (AMAFCA).

II. METHODOLOGY

Existing and proposed site hydrological conditions were analyzed for the 100-year, 6-hour storm in accordance with the revised Section 22.2, Hydrology, of the Development Process Manual (DPM) for the City of Albuquerque, dated January 1993. Street capacities were analyzed using Manning's equation,

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consistent with the revised DPM Section 22.2. All data and calculations supporting this report are located in **Appendix B** of this report. The new rational method hydrologic procedures identified within the revised DPM Section 22.2 are utilized to determine peak flow rates for design of the storm drainage improvements within the projects. The 100-year, 6-hour storm is used as the design event.

The storm sewer system internal to the subdivision is analyzed using current DPM methods for pressure flow conditions. Inlet capacity computations along with all hydraulic computations are included in **Appendix B**.

III. LAND TREATMENTS

The minimum lot is 50' x 110' (see **Figure 2** and **Plate 1**). Since there are numerous lots deeper than the 110' minimum (to account for slopes), the percent impervious will be determined using the following formula from Table A-5 of the DPM, Section 22.2.

percent "D" =
$$7 * \sqrt{((N*N) + (5*N))}$$

where N = units/acre. Substituting 4.44 for N, % D = 45. Approximately 10% of the area will have slopes at 20% or greater (type "C"), with the remaining 45% being a type "B", irrigated lawns with 0-10% slopes.

IV. EXISTING CONDITIONS

A. Topography and Existing Drainage Patterns

Tract A-2A is undeveloped land with slopes approximately ranging from 5% to 33%. Soils are highly absorptive sandy soils with occasional clay lenses. Vegetation is light, consisting of grasses and small sagebrush. The site is not located within a FEMA floodplain, as shown on the FEMA Flood Insurance Rate Map shown on Plate 2 and Plate 3. The existing drainage conditions are shown graphically on the Existing Conditions, Onsite Basins Map, on Plate 2.

An east-west ridge divides Tract A-2A into three main drainage basins, Basin EX-1 on the northern portion, Basin EX-2 on the southern portion, and Basin EX-3 on the eastern portion. Basin EX-3

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approximately, 31.1 acres, currently drains to the east side of the tract, where it collects in a natural depression and discharges into the Black Diversion Channel. The 100-year storm currently generates approximately 14.40 cfs of peak flow from undeveloped conditions of Basin EX-3.

Basin EX-1, approximately 5.0 acres, currently drains to the northwest corner of the tract, where it collects in a swale and discharges into the Black Diversion Channel. The 100-year storm currently generates approximately 7.11 cfs of peak flow from undeveloped conditions of Basin EX-1.

Basin EX-2, approximately 10.1 acres, currently drains to the south and enters the right-of-way of Seven Bar Loop Rd. and ultimately into the Black Diversion Channel via the existing storm drain system. The 100-year storm generates approximately 14.4 cfs. See **Plate 2** for a summary of the historic basins and flows.

B. Offsite Drainage

A small portion of adjoining land currently drains onto the northwest portion of Tract A-2A. With coordination with the land owner (Albuquerque Public Schools) and their engineer, a small amount of offsite grading can be accomplished to keep the runoff onsite until it enters the Seven Bar Loop or Ellison rights-of-way. See **Plate 7**. For further off-site information, please refer to Appendix F.

On the eastern boundary lies the Black Diversion Channel, which is a concrete-lined, rectangular open channel structure, currently managed by AMAFCA, but owned and originally constructed by the Soil Conservation Service (SCS).

V. PROPOSED DEVELOPED CONDITIONS

The proposed development is two single-family, detached-unit residential subdivisions with 203 lots on 44.7 acres, producing a density of 4.44 D.U. per acre. Proposed street configurations are shown on the Preliminary Plat.

The two subdivisions are divided into six basins for analysis purposes. See **Plate 3**. Basins 1, 2 and 3, which will drain only a portion of the backyards of lots adjoining Ellison Dr., the Black Diversion

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Channel-and Seven Bar Loop Rd., respectively. These backyards will be graded to a 3:1 slope with retaining walls where necessary. Runoff will be released through a grout joint opening or a turned block in the property wall. Basin A drains developed flows of 47.5 cfs to the southeast corner of the basin where it is picked up by storm inlets and conveyed thru a 30' wide utility easement to connect to the storm drain system in Basin C. Basin B drains developed flows of 55.9 cfs to the northeast where the it will be picked up by storm inlets and conveyed to the AMAFCA channel via a 25' wide drainage and access easement. This connection must be approved by AMAFCA and the SCS. Basin C drains developed flows of 22.5 cfs to the southeast and is collected in storm inlets and then enters the Seven Bar Loop system and eventually into the Black Diversion Channel. All of these collection points in a sump condition and the storm drain system will be designed for twice the 100-year event. Total combined flows from Basins A + C = 69.9 cfs. This is the amount entering the storm drain system in Seven Bar Loop Rd.

The peak developed flows from Basin 1 are approximately 4.8 cfs. This flow will drain to the existing swale at Ellison and enter the Black Diversion Channel near the Ellison Dr. crossing. Basin 2 will drain to a small swale at the property boundary and cross the Channel access road through small culverts at critical locations. The developed flows from this basin will approximate 8.3 cfs. Basin 3 will drain into the Seven Bar Loop R/W and then enter the existing storm drain system. The peak developed flows equal 4.2 cfs.

SUMMARY

	Historic	Developed
Runoff Entering Ellison Dr.	7.1 cfs	4.8 cfs
Runoff Entering AMAFCA R/W	44.4 cfs	8.3 cfs
Runoff Entering Seven Bar Loop	14.4 cfs	4.3 cfs
Channel Connection Seven Bar Connection		55.9 cfs 69.9 cfs

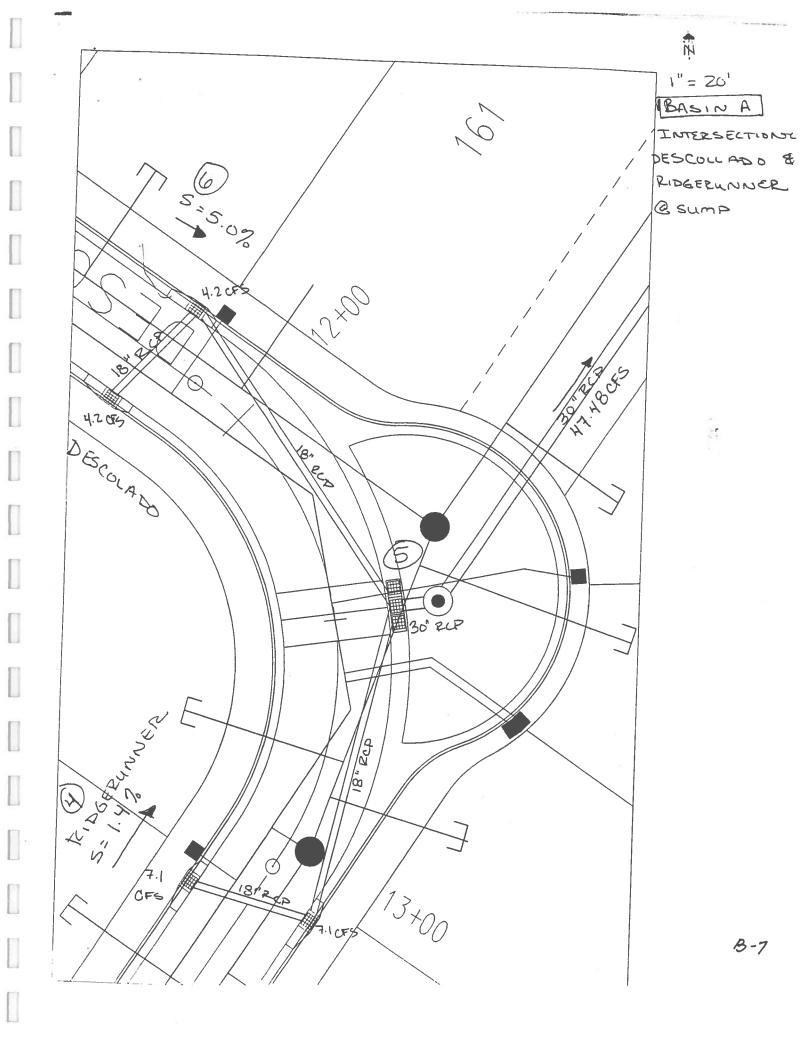
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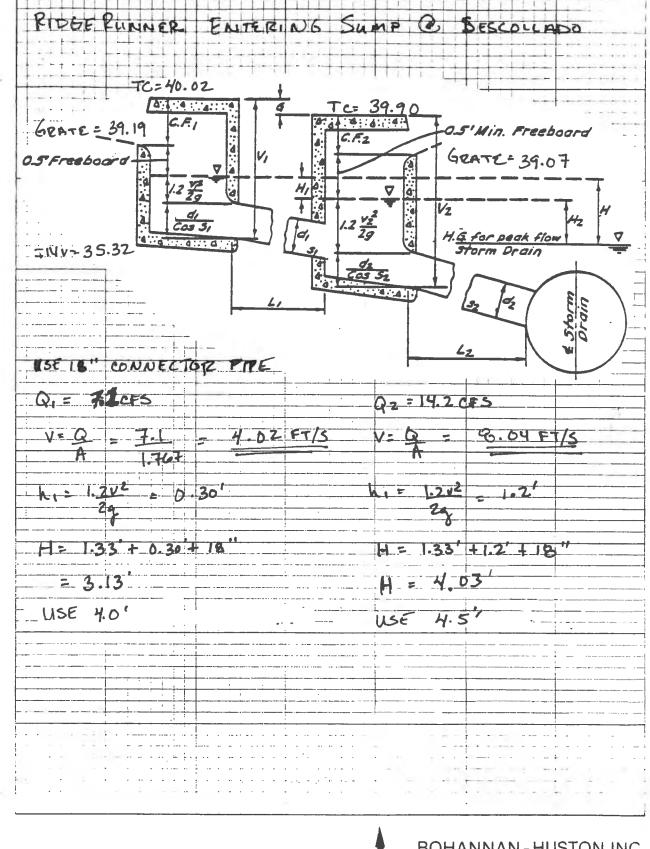
VI. BACKYARD PONDS

Seven lots will require backyard ponds due to elevation differences between street and backyards. The ponds will only retain backyard flows, all impervious flows, with the exception of a 100-square-foot patio, which will be routed to the front of the lots and onto their respective streets. The ponds are designed to contain the 100-year, 10-day volume. Pond locations are shown on the grading plans enclosed in the Plates section of this report. Pond calculations are enclosed in Appendix E.

VII. CONCLUSION

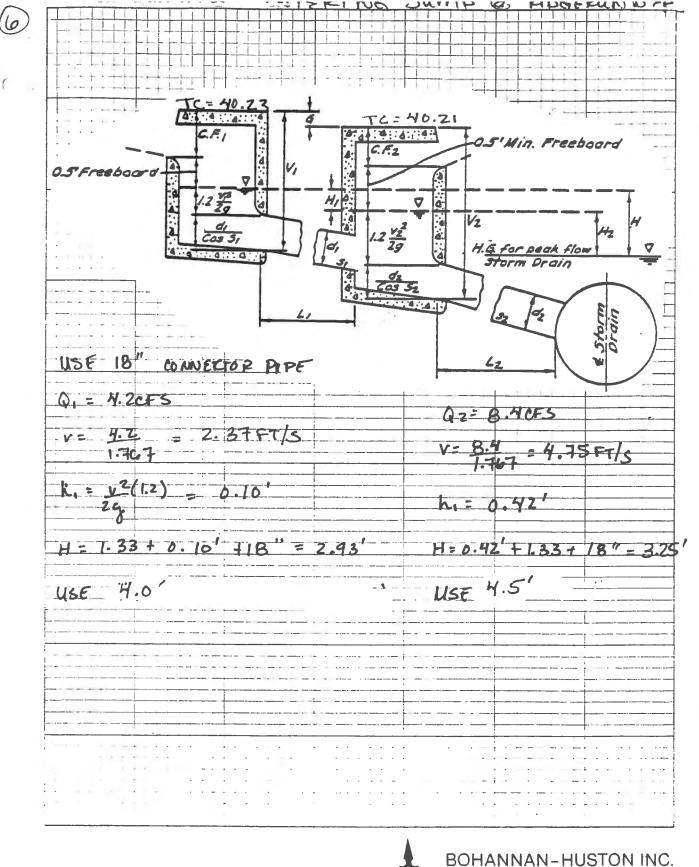
The runoff from the site will enter the Black Diversion Channel from 2 different points along its course. Good drainage management dictates that it is best to get the developed flows into the Black as quickly as possible so as not to add to the peak from upstream basins. Dividing the flows into 2 major access points minimizes the hydraulic changes in the channel and allows runoff to enter it faster. The development of this property substantially decreases the surface runoff to the Channel thus reducing erosion.





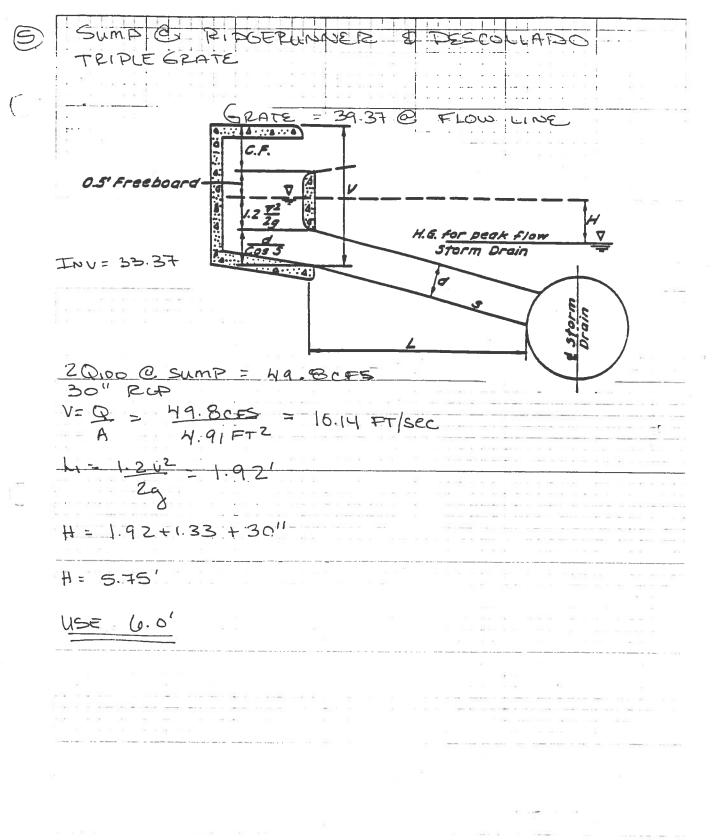
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PROJECT NAME	SHEET-	OF	B-9
PROJECT NO.	BY	DATE	
SUBJECT	CH'D	DATE	



BOHANNAN-HUSTON	INC

PROJECT NAME	_SHEET	_OF
PROJECT NO.	_BY	<i>B-11</i>
SUBJECT	_CH'D	_DATE



A
1

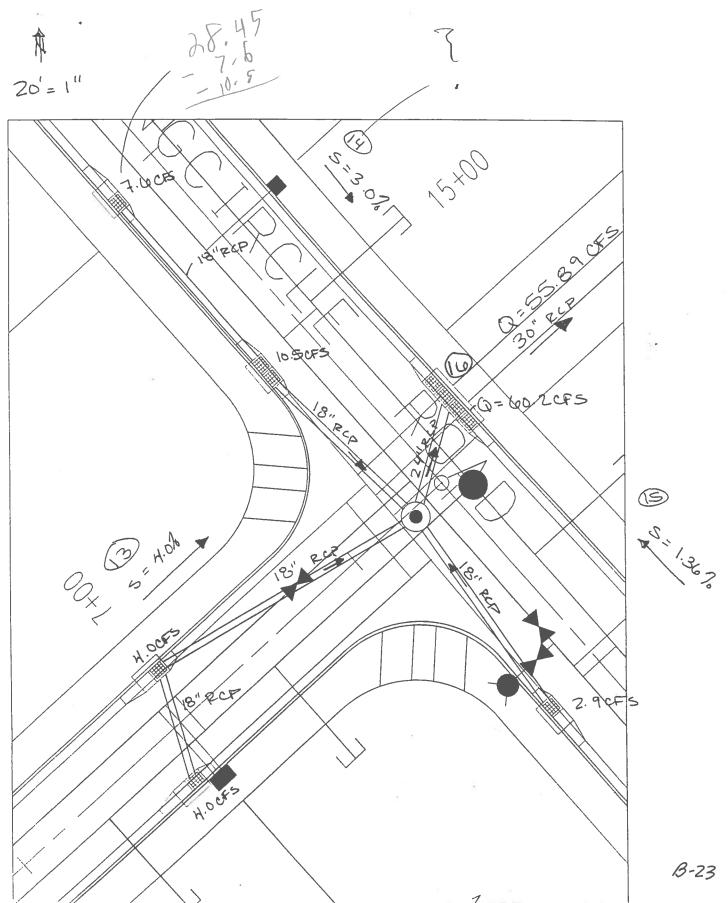
BOHANNAN-HUSTON INC.

PROJECT NAIME	SHEET	OF
PROJECT NO.	BY	DATE
SUBJECT	_CH'D	DATE

BASIN A: PIPE SIZING
RIDGERUNNER AND DESCOLLADO INTERSECTION
ANALYSIS POINT 5

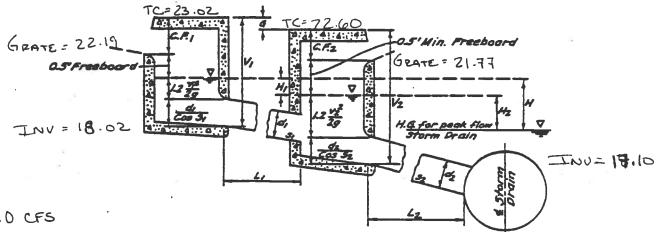
Entrance Street	Q (CFS)	H (FT)	A = Q 0.6 (2Gh) 1/2	$d=12*(4A/\pi)^{1/2}$ (IN)	PIPE SIZE
RIDGERUNNER	7.1	4.0	0.74	11.65	18"
RIDGERUNNER	14.2	4.5	1.39	15.96	18"
DESCOLLADO	4.2	4.0	0.44	8.98	18"
DESCOLLADO	8.4	4.5	0.82	12.26	18"
GRATE TO MH	47.5	6.0	4.03	27.18	30"
MH TO BASIN C	47.5	6.0	4.03	27.18	30"

SUMP @ INTERSECTION OF RIDING CIRCLE, CHANDLER, & PACKAUM



(15) FACKAWAY ENTERING SUMP @ PIDING CIRCLE Chapter 22 - Drainage, Flood Control and Erosion Control

d. Catch Basins in Series



USE 18" CONNECTOR PIPE

$$k_1 = \frac{1.2 \, \text{V}^2}{29} = 0.10^{\circ}$$

$$Q_2 = 8.0 \text{ CFS}$$

USE 18" CONNECTOR PIPE

 $V = \frac{8.0 \text{ CFS}}{1.767} = 4.52 \text{ FT/S}$

$$h_1 = \frac{1.2(4.52)^2}{29} = 0.38'$$

RIDING CIRCLE EXNTERNO SUMP @ PACKAWAY

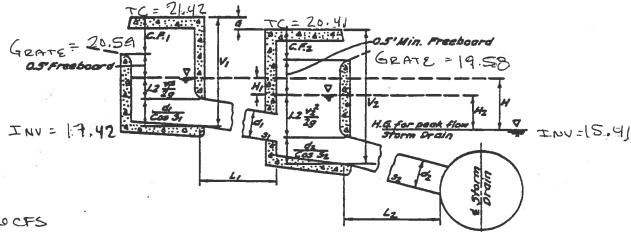
Chapter 22 - Drainage, Flood Control and Erosion Control

SINGLE

d. Catch Basins in Series

DOUBLE





Q = 7.6 CFS

USE 18" CONNECTOR PIPE

V= Q = 7.60cfs = 4.30 FT/S A 1.70 FTZ

 $h = \frac{1.2 \, \text{V}^2}{29} = \frac{1.2 \, (4.30)^2}{29} = 0.34'$

H= 1.33' +0.34' +1.5'

H= 3.17'

USE H = M. D'

Q2 = 7.6+10.5 = 18.1 CFS USE AN 18" CONNECTOR

V= Q = 18.1 = 10.24 FT/S

 $h = \frac{1.2v^2}{2g} = 1.96$

H= 1.33' + 1.96' +15'

H= 4.78'

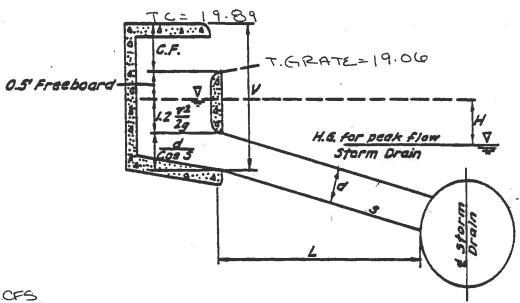
45E H = 5.0'

(15)

CATCH BASIN ON CHANDLER ENTERING SUMD @ HIVER Chapter 22 - Drainage, Flood Control and Erosion Control OF PACLAWAYS

CHANDLER

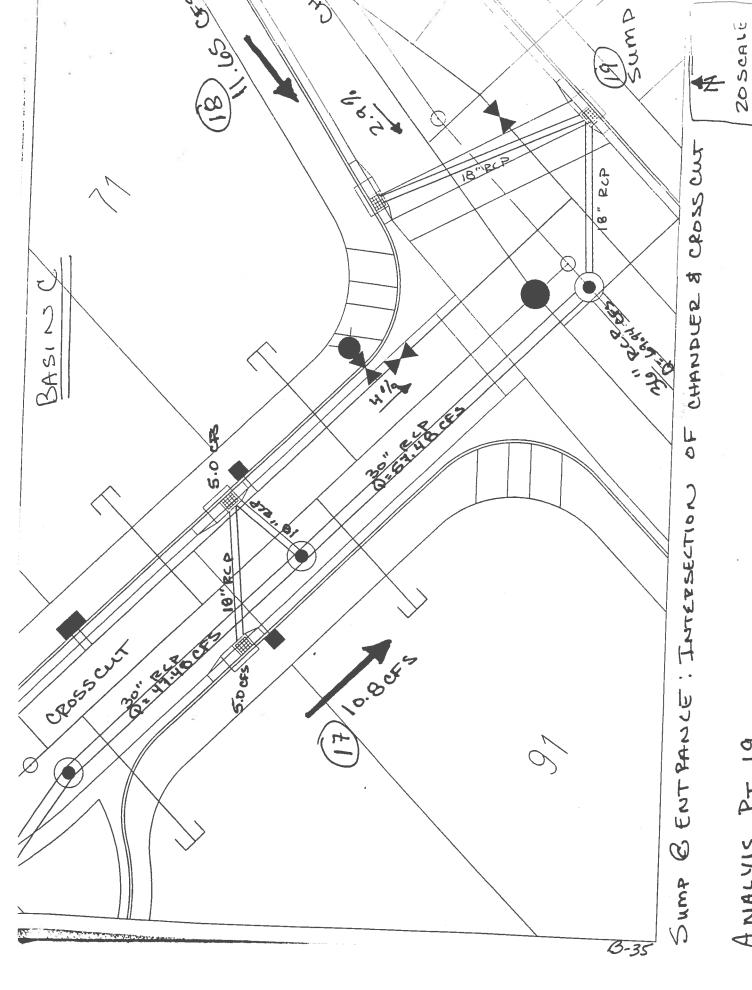
- c. Connector Pipe and "V" Depth Calculation
- (1) Single Catch Basins



USE 18" CONNECTOR PIPE

BASIN B:PIPE SIZING
RIDING CIRCLE, CHANDLER, AND PACKAWAY INTERSECTION
ANALYSIS POINT 16

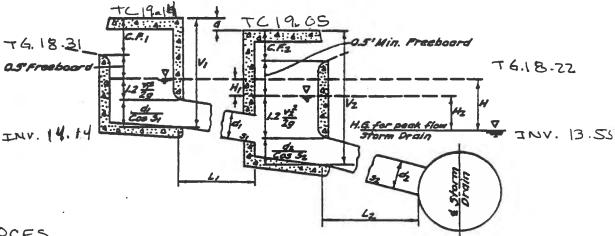
Entrance Street	Q (CFS)	H (FT)	A= 0 0.6(2Gh) ^{1/2}	$d=12*(4A/\pi)^{1/2}$ (IN)	PIPE SIZE
RIDING CIRCLE	7.6	4.0	0.79	12.04	18"
RIDING CIRCLE	18.1	5.0	1.68	17.56	18"
CHANDLER	2.9	4.0	0.30	4.60	18"
PACKAWAY	4.0	4.0	0.42	8.73	18"
PACKAWAY	8.0	4.5	0.78	11.98	18"
MH TO GRATE	29.0	6	2.46	21.23	24"
GRATE TO CHAN.	55.9	6	4.73	29.45	30"



ANALVIS PT 19

Chapter 22 - Drainage, Flood Control and Erosion Control

d. Catch Basins in Series



Q, = 5.0CFS

USE 18" CONNECTOR

$$h_1 = \frac{1.2v^2}{2q} = 0.15'$$

H= 1.33'+18"+0.15'

USE 18' CONNECTOR

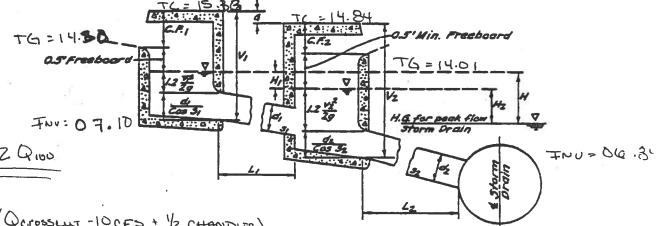
$$h_1 = 1.2v^2 = 0.41^7$$

Hmin = 133+18"+0.41"

Hmin = 3.24'

USE H= 5.5'
(AVOIDS WE CROSSING)

d. Catch Basins in Series



Q = 2 (QCrosslut-10CFS + 1/2 CHANDLER)

USE 18" CONNECTOR FIFE:

$$h_1 = 1.2 v^2 = 1.05'$$

$$h = \frac{1.2 \sqrt{2}}{2g} = 1.17$$

BASIN C PIPE SIZING
CHANDLER-CROSSCUT INTERSECTION
ANALYSIS POINT 19

Entrance Street	Q (CFS)	H (FT)	A = Q 0.6 (2Gh) ^{1/2}	$d=12*(4A/\pi)^{1/2}$ (IN)	PIPE SIZE
CROSSCUT	5.00	5.0	0.46	9.23	18"
CROSSCUT	10.00	5.5	0.88	12.74	18"
MH ON CROSSCUT	57.50	7.19	4.45	28.58	30"
CHANDLER	6.62	7.2	0.51	9.70	18"
CHANDLER	12.44	7.17	0.96	13.30	24"*
CHAND./CROSS.	69.94	8.46	4.99	30.26	36"

^{* 24&}quot; RCP DECREASED THE REQUIRED H FOR THE INLET.

TRACT A-2A **BACKYARD POND DESIGN** FEBRUARY, 1999

BACKYARD PONDS

ASSUMING: (50% treatment "B" and 50% treatment "C") X (Backyard Area) + (100 sf X Treatment "D") for 10 day, 100 year volumes

V(10) =

 $V(360) + Ad^*(P(10) - P(360)$

Wher E is the weighted excess percipitation

eq. a-7 DPM

12 in/ft

A is the area in each treatment type

E for treatment "B" and "C" portions:

E = EaAa + EbAb + EcAc + EdAdAa+Ab+Ac+Ad

eq. a-5 DPM

Given:

Ea = n/a

P10 = 3.67

Eb = 0.67

P360 = 2.20

Ec = 0.99

Ed = 1.97

E = [.67 + .99] = 0.069 ft

2*(12)

(converts inches to feet)

 $V(10) = [(X BACKYARD AREA - Ad) \times E] + Ad*(3.67-2.20)/12 eq. a-9 DPM$

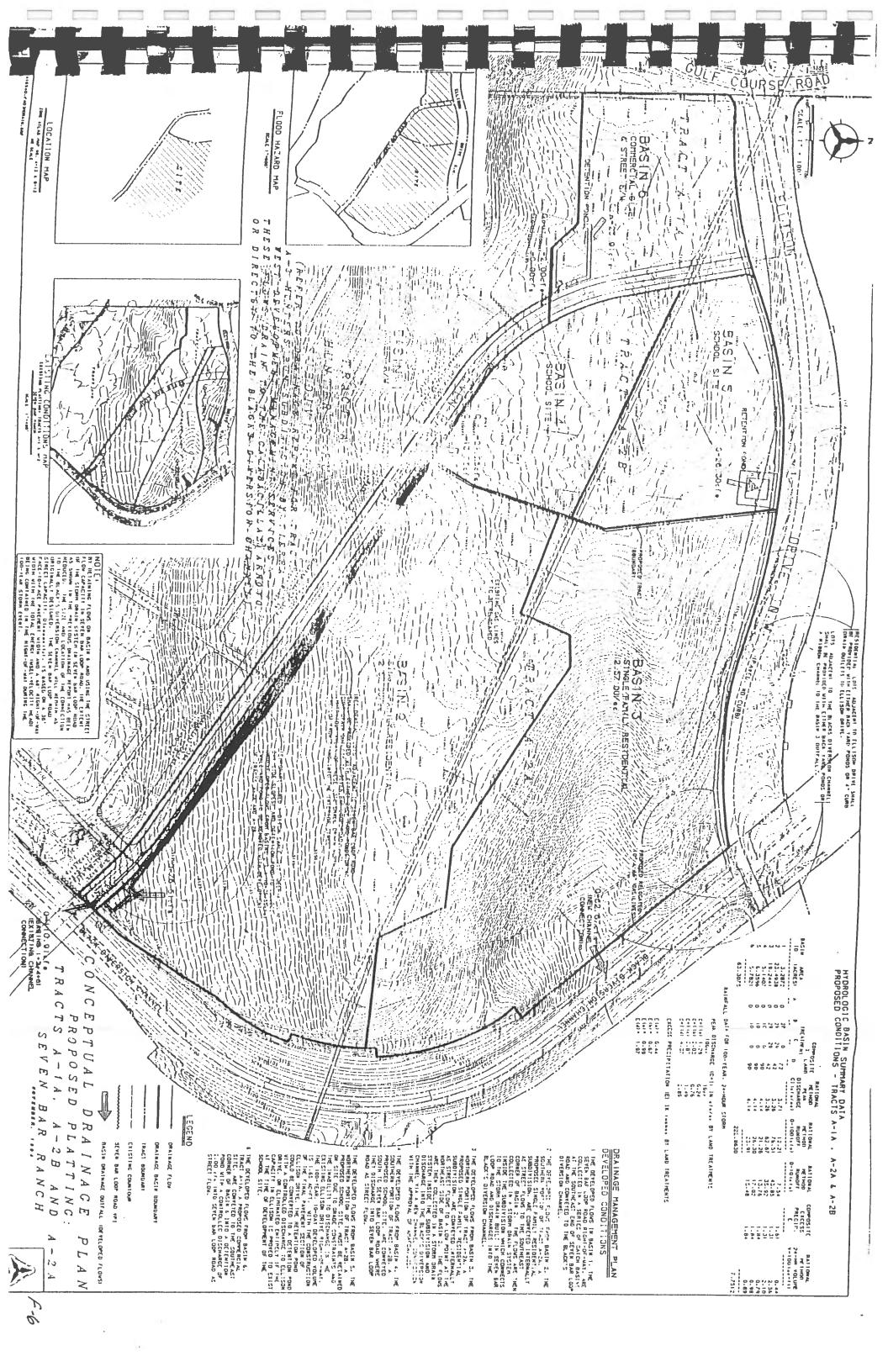
TRACT A-2A

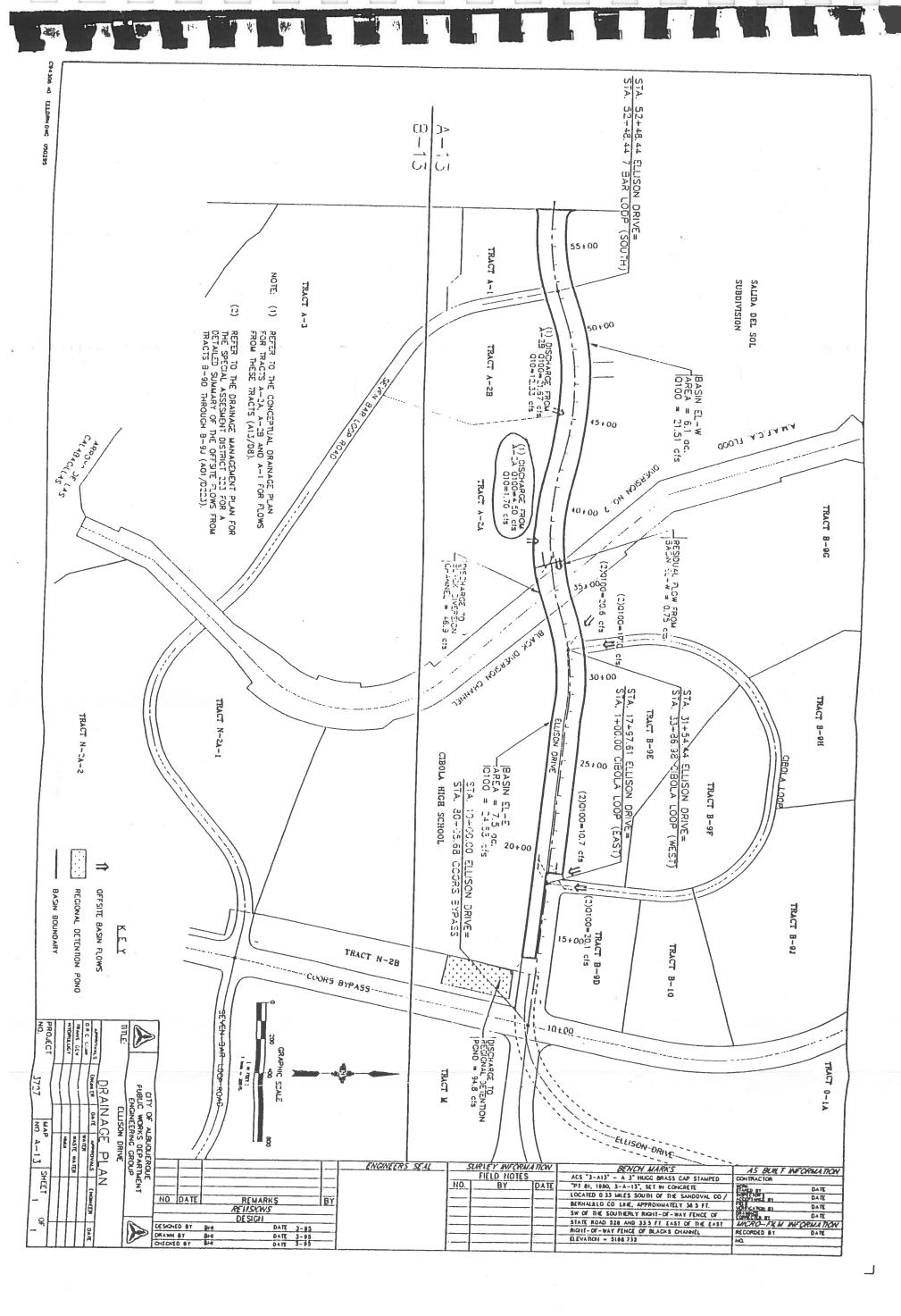
LOT#	BACKYARD AREA	REQUIRED V (100)	-		SION .) DTHS)		POND VOLUME			Q(100)
UNIT B-9	(SQ. FT.)	(CU. FT.)	L	W1	W2	D	(CU. FT.)	С	ı	cfs
74	1755	126	21	5.8	9.4	0.8	128	0.52	4.7	0.10
153	1558.8	113	22	6.1	6.7	0.8	113	0.52	4.7	0.09
154	1710	123	26	7.6	4.2	0.8	123	0.52	4.7	0.10
155	3660	258	23	14.1	13.9	0.8	258	0.52	4.7	0.21
156	7610.9	531	35	19.8	23.7	0.7	536	0.52	4.7	0.43
174	1585.3	115	23	7.3	7.5	0.7	117	0.52	4.7	0.09
175	1585.3	115	21	7.6	8.2	0.7	115	0.52	4.7	0.09

TOTAL =

1.09

100 ys - 10 day volume





OFFSITE MAP

