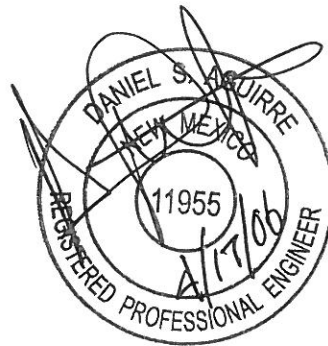


DR63: 5

**GOLF COURSE ROAD
DRAINAGE SYSTEM ANALYSIS**



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INTRODUCTION

This report is an amendment to the final drainage report for the Golf Course Road Widening Project from Southern Boulevard to Westside Boulevard. It outlines the hydrologic and hydraulic analysis performed to provide the City of Rio Rancho with a capacity analysis and recommendations for adequately conveying runoff within the corridor using the assumptions of free discharge from the full depth commercial properties along the west side of the roadway as identified in the Black Arroyo Watershed Management Plan (BLWMP) prepared for Southern Sandoval County Arroyo Flood Control Authority. The analysis provides adjusted hydrology for modified drainage basins as shown in the BLWMP and the hydraulic analysis of the storm drain system to handle the ultimate developed conditions. A basin boundary map showing the limits of the analysis is included on Plate 1.

The purpose of the analysis is to model the existing storm drain system as-built with the Golf Course Road widening project and identify the capacity for conveyance of the ultimate conditions model as defined in the BLWMP.

DRAINAGE CRITERIA

Drainage requirements of the City of Rio Rancho were the basis of analysis for this drainage report. The following is a section taken from the City's drainage criteria stated in the City Health, Safety and Sanitation Ordinance, Article 8-7-7.

8.7.7

- B. *The 100-year design storm runoff shall not exceed a depth of 0.87 feet at any point within the street right-of-way, or 0.2 feet above top of curb, in any street or enter private property, built in compliance with appropriate regulations, from a street, except in recorded drainage or flood control easements or rights-of-way (or historic channels and watercourses where easements of rights-of-way can be obtained).*
- C. *The 10-year design storm runoff shall not exceed a depth of 0.5 feet in any arterial street and shall flow such that one (1) twelve-foot (12-foot) driving lane in each direction is free of flowing or standing water. The 10-year design storm runoff shall not exceed a depth of 0.5 feet in any collector street. Arterial and collector streets that are in the State Highway system may require more stringent drainage criteria.*
- D. *The product of depth times velocity shall not exceed 6.5 at any location in any street in the event of a 10-year design storm (with velocity calculated as the average velocity measured in feet per second and depth measured at the gutter flow line in feet).*

The storm drain design is based on the criteria that the hydraulic grade line be kept below the grate and manhole cover elevations.

Based on the final drainage report for the Golf Course Road Widening Project a 6-percent bulking factor is used in the hydrologic analysis. This allows for a conservative system to convey full runoff with possible sediment loading within the system

EXISTING CONDITIONS

Golf Course road was recently widened to a 4/5 lane section with eight-inch standard curb and gutter. The normal crown in the existing roadway ranges between 1.5% and 2.0%. Plate 2 is a detail of the existing typical roadway section.

A storm drain system was installed with pipe size varying from 30" to 48" RCP pipe. The captured runoff then drains through the 23rd Street ponds, along an earth channel, and finally into the east branch of the Blacks Arroyo which conveys flow to the Black Detention Dam Facility. Plate 3 shows the existing system.

The majority of the lots along the west side of Golf Course are still undeveloped. The parcels that have been developed are commercially owned. The businesses consist of a large storage facility, various churches and other small business including a daycare and doctor's clinic. According to the City's zoning map, these adjacent (west) lots are zoned either commercial or residential/special use. The basins affecting the runoff in the roadway are moderately sloped and no evidence of concentrated flow is present. The residential lots along the east side of the roadway are fully developed and provide a small percentage of the runoff in Golf Course Road.

Drainage Basins

Delineation of the drainage basins was completed in accord with the analysis of the BLWMP. The drainage basin map is provided in Plate 1 in the back of this report.

In order to meet future requirements of the ultimate developed conditions we assume that the lots adjacent to the west side of Golf Course Road would be entirely commercial. For the basins east of golf course we have assumed 6 du's per acre to be conservative. For the purposes of this report we have also assumed that all lots within the basin boundaries delineated for this report will have free discharge. Table 1A is a summary of the land treatment types used in the analysis for each of the contributing basins. The Ahymo summary and input files can be found in Appendix A.

Table 1A
Basin Land Treatment Types
Ultimate Developed Conditions

Basin	Area (sq. mi.)	Land Treatment Percentages			
		A	B	C	D
1W	0.00794	0.0	10	0	90.0
1E	0.00300	0.0	25.0	15.0	60.0
2WU	0.00803	0.0	10	0	90.0
2EU	0.00225	0.0	25.0	15.0	60.0
2WL	0.00580	0.0	10	0	90.0
2EL	0.00180	0.0	25.0	15.0	60.0
3WU	0.01230	0.0	10	0	90.0
3EU	0.00375	0.0	25.0	15.0	60.0
3WL	0.00803	0.0	10	0	90.0
3EL	0.00268	0.0	25.0	15.0	60.0
4W	0.00546	0.0	10	0	90.0
4E	0.00140	0.0	25.0	15.0	60.0

5W	0.00470	0.0	10	0	90.0
5E	0.00190	0.0	25.0	15.0	60.0
6W	0.00290	0.0	10	0	90.0
6E	0.00170	0.0	25.0	15.0	60.0
7W	0.00940	0.0	15	5	80.0
7E	0.00107	0.0	25.0	15.0	60.0
8W	0.00296	0.0	10	0	90.0
8E	0.00960	0.0	25.0	15.0	60.0
9W	0.00323	0.0	10	0	90.0
9E	0.01300	0.0	25.0	15.0	60.0
10W	0.00320	0.0	10	0	90.0
10E	0.01950	0.0	25.0	15.0	60.0

Description of the land treatment allocations taken from the City of Albuquerque DPM, Section 22.2 (1997):

Land Treatment A: Soil uncompacted by human activity with 0 to 10 percent slopes. Native grasses, weeds and shrubs in typical densities with minimal disturbance to grading, groundcover and infiltration capacity. Croplands. Unlined arroyos.

Land Treatment B: Irrigated lawns, parks and golf courses with 0 to 10 percent slopes. Native grasses, weeds and shrubs, and soil uncompacted by human activity with slopes greater than 10 percent and less than 20 percent.

Land Treatment C: Soil compacted by human activity. Minimal vegetation. Unpaved parking, roads, trails. Most vacant lots. Gravel or rock on plastic (desert landscaping). Irrigated lawns and parks with slopes greater than 10 percent. Native grasses, weeds and shrubs, and soil uncompacted by human activity with slopes at 20 percent or greater. Native grass, weed and shrub areas with clay or clay loam soils and other soils of very low permeability as classified by SCS Hydrologic Soil Group D.

Land Treatment D: Impervious areas, pavement and roofs.

The drainage basins shown on Plate 1 were confirmed using available mapping and field visits. No other offsite basins are contributing to the flow in Golf Course Road. Flows from the north are intercepted by Southern Boulevard and conveyed east toward NMSR 528.

Structures

Analysis of all inlets installed with the Golf Course Road widening project is included in the analysis to add the maximum flow at each inlet and convey the by-pass flow in the roadway.

The existing pond on 20th Street outflows into the Golf Course Road system. We assume that neither the existing flow rates nor the outflow pipe size would change in the future. Therefore, in both analyses, the flow rate added to the system at 22nd Street was approximately 60-cfs. The hydrograph used in the AHYMO analysis was taken directly from the model used in the BLWMP.

Methodology

The method of analysis was the AHYMO Computer Program (Anderson, 1997). The Type II rainfall distribution specified in the model assumes a "24-hour rainfall distribution based on NOAA Atlas 2 with peak intensity at 1.4 hours." A minimum time of concentration (t_c) of 10 minutes was used to calculate the time to peak (T_p) for each basin ($T_p = 2/3 t_c$). A sediment bulk factor of 1.06 was used to simulate the effects of increased flow rates caused by the movement of sediment with the runoff. A copy of the input and summary files for each case are included in Appendix A.

The following table is a summary of the peak discharge and volume rates for each sub-basin.

Table 2A
100-Year Values
Ultimate Conditions Discharge

Basin	Area (sq. mi.)	100-Year Event	
		Peak Discharge (cfs)	Runoff Volume (ac-ft)
1W	0.00794	21.9	1.022
1E	0.00300	7.4	0.306
2WU	0.00803	22.1	1.034
2EU	0.00225	5.6	0.230
2WL	0.00580	16.0	0.747
2EL	0.00180	4.5	0.184
3WU	0.01230	33.8	1.583
3EU	0.00375	9.3	0.383
3WL	0.00803	22.1	1.034
3EL	0.00268	6.6	0.273
4W	0.00546	15.0	0.703
4E	0.00140	3.5	0.143
5W	0.00470	12.9	0.605
5E	0.00190	4.7	0.194
6W	0.00290	8.0	0.373
6E	0.00170	4.2	0.173
7W	0.00940	24.8	1.121
7E	0.00107	2.7	0.109
8W	0.00296	8.2	0.381
8E	0.00960	23.7	0.980
9W	0.00323	8.9	0.416
9E	0.01300	32.0	0.385
20 th St. Pond	0.13340	59.1	9.968
10W	0.00320	8.8	0.412
10E	0.01950	48.1	1.990

Table 2B
100-Year
Ultimate Conditions Discharge

Analysis Point		100-Year Event	
			Peak Discharge (cfs)
AP1	Chianti Road Diversion		58
AP9	To Storm Drain in Westside		243

The storm drain analysis was prepared using the Hydraflow Storm Sewers 2000 computer program. With this program, the runoff values obtained from the AHYMO output have been input to evaluate the hydraulic grade line for the pipe system. The 100-year models were run with the constraint that the hydraulic grade elevations stay below the manhole cover and inlet grate elevations. The inlet capacity files and hydraulic grade line models can be found in Appendix B.

DISCUSSION

The existing storm water conveyance system in Golf Course Road was designed to handle the runoff for the 100 year event. The design assumed fully developed roadway flow and historic flow from the adjacent offsite basins. This system works as designed with these assumptions. The report states that to allow for discharge rates above these assumptions diversion pipes would be required to convey flows west to the East Branch Channel. See Plate 3 for the existing system.

Significant development west of Golf Course Road is currently in design and construction requiring a detailed look at what diversion structures are necessary to allow for the free discharge of future developments. WCI has prepared a detailed analysis of the ultimate conditions allowing free discharge from the adjacent properties to evaluate the requirements for the future system to be installed with the current development.

CONCLUSION

The analysis of the existing Golf Course Road system for the ultimate conditions looked at the capacity of the existing pipe and inlet system. During this analysis it was noted that the inlets have a greater capacity than the conveyance pipes from the inlets to the main line. Based on this information, we modeled the system with two options. Option 1 (GC100ULT) assumed that improvements would be made to the conveyance system to match the capacity of the inlets. The second option (GC100ULTmod) assumed that the system would remain as constructed today.

In both options the system failed with the full flow being carried by the Golf Course Road system alone. Each of the systems were then modified with a full diversion of pipe flow at Chianti Road. With this modification both systems operate with the HGL below the top of inlet and with the street flow contained within the curb and gutter.

We recommend that the system improvements for the ultimate developed condition include the diversion of the pipe flows at Chianti Road. The design for the diversion at Chianti Road should be a storm drain

pipe from Golf Course Road to the East Branch Channel sized for the possible discharge of 58 cfs. In addition the original model allowed for a by pass flow of 8 cfs to the City of Albuquerque portion of the roadway. To meet this requirement, using the data from option 2, additional inlets located upstream of Westside Boulevard to capture approximately 35 cfs are required.

A system is currently being proposed to convey the discharge from the existing pipe outlets at 23rd Street to the east branch channel. The proposed storm drain parallels Golf Course road to Westside Boulevard. The line then turns west in Westside Boulevard and terminates at the East Branch Channel. We recommend this Westside Boulevard storm drain system be designed to carry the total pipe flow from the Golf Course Road systems, the additional 35 cfs and the Westside Boulevard flows. The system would include a 60 - 66 inch mainline with the installation of 2 type "A" inlets and 3 type "C" inlets in Golf Course Road upstream of Westside Boulevard. If the system is designed per these recommendations it is not required to divert the flows from the Golf Course Road system at 18th Street to meet the current City requirements as described above.

Appendix A
Alymo Files

Ultimate
Conditions

*S GOLF COURSE ROAD HYDROLOGY
 *S AHYMO MODEL TO CALCULATE RUNOFF BASED ON PROPOSED CONDITIONS (MODIFIED TO
 *S REPRESENT ULTIMATE CONDITIONS AS SHOWN IN THE blwmp BY dsa 3/07/06)
 *S ON GOLF COURSE ROAD FROM SOUTHERN BLVD SOUTH TO 23RD STREET DETENTION PONDS
 *S THIS MODEL ASSUMES THAT ALL LOTS ADJACENT TO THE WEST SIDE OF GOLF COURSE
 *S WILL BE DEVELOPED AS COMMERCIAL LOTS AND THAT ON-SITE DETENTION WILL BE
 *S REQUIRED TO CONTROL RUNOFF ABOVE HISTORICAL VALUES.

*S DRAINAGE BASIN DELINEATIONS WERE MADE IN ACCORDANCE WITH THE BLACKS ARROYO
 *S DRAINAGE MASTER PLAN TO BE COMPLETED FOR SSCAFCA. BULKING FACTOR ADDED IN
 *S ACCORDANCE WITH SSCAFCA REQUIREMENTS FOR THE BLACKS ARROYO ANALYSIS.

*S*****
 *S***** 100-YEAR STORM *****
 *S*****
 *

START TIME=0.0 HR PUNCH CODE=0

*EACH STORM INPUT DATA FOLLOWS

RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 RAIN ONE=1.80 IN RAIN SIX=2.21 IN
 RAIN DAY=2.7 IN DT=0.05 HRS

*TWO YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=0.739 IN RAIN SIX=0.925 IN
 * RAIN DAY=1.075 IN DT=0.05 HRS

*FIVE YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.001 IN RAIN SIX=1.250 IN
 * RAIN DAY=1.475 IN DT=0.05 HRS

*TEN YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.184 IN RAIN SIX=1.450 IN
 * RAIN DAY=1.700 IN DT=0.05 HRS

*TWENTY FIVE YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.394 IN RAIN SIX=1.825 IN
 * RAIN DAY=2.100 IN DT=0.05 HRS

*FIFTY YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.604 IN RAIN SIX=2.000 IN
 * RAIN DAY=2.350 IN DT=0.05 HRS

*HUNDRED YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.878 IN RAIN SIX=2.225 IN
 * RAIN DAY=2.700 IN DT=0.05 HRS

*S*****BEGIN AP 1*****

*S1
 SEDIMENT BULK CODE=1 BULK FACTOR=1.06

*S1A
 COMPUTE NM HYD ID=1 HYD NO=1W AREA=0.00794 SQ MI
 PER A=0 PER B=10 PER C=0 PER D=90
 TP=0.111 HR MASS RAIN=-1

*S2
 COMPUTE NM HYD ID=2 HYD NO=1E AREA=0.003 SQ MI
 PER A=0 PER B=15 PER C=25 PER D=60
 TP=0.111 HR MASS RAIN=-1

*FOR THIS MODEL, SPLIT BASIN 2W INTO UPPER (U) AND LOWER (L) BASINS

*S3
 COMPUTE NM HYD ID=3 HYD NO=2WU AREA=0.00803 SQ MI
 PER A=0 PER B=10 PER C=0 PER D=90
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 2WU BASIN AND 1W BASIN

*S4
 ADD HYD ID=4 HYD NO=1W2WU IDS=1 AND 3

*S5 PLOT
 PLOT HYD ID=1 ID=3 Q SCALE=0 T SCALE=0

*S6
 COMPUTE NM HYD ID=5 HYD NO=2EU AREA=0.00225 SQ MI
 PER A=0 PER B=15 PER C=25.0 PER D=60.0
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 2EU BASIN AND 1E BASIN


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*S7
ADD HYD          ID=6          HYD NO=1E2EU      IDS=2 AND 5

*S8 PLOT
PLOT HYD          ID=2    ID=5    Q SCALE=0    T SCALE=0

*S9
COMPUTE NM HYD    ID=7          HYD NO=2WL      AREA=0.0058 SQ MI
                  PER A=0        PER B=10        PER C=0          PER D=90
                  TP=0.111 HR  MASS RAIN=-1

*COMBINE FLOW FROM 2WU BASIN AND 2WL BASIN
*S10
ADD HYD          ID=8          HYD NO=AP1W      IDS=4 AND 7

*S11 PLOT
PLOT HYD          ID=4    ID=7    Q SCALE=0    T SCALE=0

*S12
COMPUTE NM HYD    ID=9          HYD NO=2EL      AREA=0.0018 SQ MI
                  PER A=0        PER B=15        PER C=25          PER D=60
                  TP=0.111 HR  MASS RAIN=-1

*COMBINE FLOW FROM 2EU BASIN AND 2EL BASIN
*S13
ADD HYD          ID=10         HYD NO=AP1E      IDS=6 AND 9

*S14 PLOT
PLOT HYD          ID=6    ID=9    Q SCALE=0    T SCALE=0

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S15
DIVIDE HYD        ID=8          Q=49            ID I=11      HYD NO=AP1WSD
                  ID II=12     HYD NO=AP1WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET
*S16
DIVIDE HYD        ID=10         Q=9             ID I=13      HYD NO=AP1ESD
                  ID II=14     HYD NO=AP1EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN
*S17
ADD HYD          ID=15         HYD NO=AP1SD     IDS=11 AND 13

*S18 PLOT
PLOT HYD          ID=11    ID=13    Q SCALE=0    T SCALE=0

*ROUTE INTERCEPTED FLOW THROUGH AP2 IN 30" PIPE TO AP2
COMPUTE RATING CURVE CID=1      VS NO=1 CODE=-1 SLP=0.015
                        DIA=2.5 FT N=0.013

*S19
ROUTE MCUNGE      ID=16    HYD NO=AP1R    INFLOW ID=15
                  DT=0.0 HR  LENGTH=1170 FT
                  NS=0    SLOPE=0.0150    MATCODE=0
                  REGCODE=0    CCODE=0

*S*****Note Flow Routed to East Branch Channel Down Chianti*****
*S*****END AP 1*****
*S*****BEGIN AP 2*****

*FOR THIS MODEL, SPLIT BASIN 3W INTO UPPER (U) AND LOWER (L) BASINS
*S20
COMPUTE NM HYD    ID=17         HYD NO=3WU      AREA=0.0123 SQ MI
                  PER A=0        PER B=10        PER C=0          PER D=90
                  TP=0.111 HR  MASS RAIN=-1

*TOTAL SURFACE FLOW AT AP2
ADD HYD          ID=7          HYD NO=AP2W      IDS=12 AND 17

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S15
DIVIDE HYD        ID=7          Q=19.9          ID I=50      HYD NO=AP2WSD
                  ID II=51     HYD NO=AP2WST

*ROUTE INTERCEPTED FLOW THROUGH AP2 IN 30" PIPE TO AP3
COMPUTE RATING CURVE CID=1      VS NO=1 CODE=-1 SLP=0.04
                        DIA=2.5 FT N=0.013

*S19
ROUTE MCUNGE      ID=53    HYD NO=AP2R    INFLOW ID=50
                  DT=0.0 HR  LENGTH=770 FT
                  NS=0    SLOPE=0.040    MATCODE=0
                  REGCODE=0    CCODE=0

*S*****END AP 2*****
*S*****BEGIN AP 3*****

*S21
COMPUTE NM HYD    ID=18         HYD NO=3EU      AREA=0.00375 SQ MI

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GC100ULT.txt

PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*S22
COMPUTE NM HYD ID=19 HYD NO=3WL AREA=0.00803 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 3WU BASIN AND 3WL BASIN
*S23
ADD HYD ID=20 HYD NO=3WU3WL IDS=51 AND 19

*S25
COMPUTE NM HYD ID=21 HYD NO=3EL AREA=0.00268 SQ MI
PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 3EL BASIN AND 3EU BASIN
*S26
ADD HYD ID=22 HYD NO=3EU3EL IDS=18 AND 21

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S15
DIVIDE HYD ID=20 Q=20 ID I=50 HYD NO=AP3WSD
ID II=55 HYD NO=AP3WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET
*S16
DIVIDE HYD ID=22 Q=11 ID I=56 HYD NO=AP3ESD
ID II=57 HYD NO=AP3EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN
*S17
ADD HYD ID=58 HYD NO=AP3CSD IDS=50 AND 56

*COMBINE INTERCEPTED FLOW WITH ROUTED FLOW FROM AP2
*S17
ADD HYD ID=56 HYD NO=AP3SD IDS=53 AND 58

*ROUTE INTERCEPTED FLOW THROUGH AP3 IN 36" PIPE TO AP4
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.018
DIA=3.0 FT N=0.013

*S19
ROUTE MCUNGE ID=59 HYD NO=AP3R INFLOW ID=56
DT=0.0 HR LENGTH=514 FT
NS=0 SLOPE=0.018 MATCODE=0
REGCODE=0 CCODE=0

*****END AP 3*****
*****BEGIN AP 4*****

*S28
COMPUTE NM HYD ID=23 HYD NO=4W AREA=0.00546 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 4W BASIN AND 3WL BASIN
*S29
ADD HYD ID=24 HYD NO=3WL4W IDS=55 AND 23

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S15
DIVIDE HYD ID=24 Q=12.5 ID I=60 HYD NO=AP4WSD
ID II=61 HYD NO=AP4WST

*COMBINE INTERCEPTED FLOW FROM WEST SIDE OF ROADWAY IN STORM DRAIN
*S17
ADD HYD ID=62 HYD NO=AP4SD IDS=59 AND 60

*ROUTE INTERCEPTED FLOW THROUGH AP2 IN 36" PIPE TO AP3
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.0525
DIA=3.0 FT N=0.013

*S19
ROUTE MCUNGE ID=53 HYD NO=AP2R INFLOW ID=62
DT=0.0 HR LENGTH=600 FT
NS=0 SLOPE=0.0525 MATCODE=0
REGCODE=0 CCODE=0

*****END AP 4*****
*****BEGIN AP 5*****

*S31
COMPUTE NM HYD ID=25 HYD NO=4E AREA=0.0014 SQ MI
PER A=0.0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 4E BASIN AND STREET FLOW

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*S32
ADD HYD          ID=26      HYD NO=3EL4E    IDS=57 AND 25

*S34
COMPUTE NM HYD   ID=27      HYD NO=5W      AREA=0.0047 SQ MI
                  PER A=0    PER B=10      PER C=0      PER D=90
                  TP=0.111 HR MASS RAIN=-1

*COMBINE STREET FLOW FROM 4W BASIN AND 5W BASIN
*S35
ADD HYD          ID=28      HYD NO=AP5W     IDS=61 AND 27

*S37
COMPUTE NM HYD   ID=29      HYD NO=5E      AREA=0.0019 SQ MI
                  PER A=0    PER B=15      PER C=25      PER D=60
                  TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 4E BASIN AND 5E BASIN
*S38
ADD HYD          ID=30      HYD NO=AP5E     IDS=26 AND 29

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S40
DIVIDE HYD       ID=28      Q=14.0        ID I=31     HYD NO=AP5WSD
                  ID II=32    HYD NO=AP5WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET
*S41
DIVIDE HYD       ID=30      Q=13.2        ID I=33     HYD NO=AP5ESD
                  ID II=34    HYD NO=AP5EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN
*S42
ADD HYD          ID=35      HYD NO=AP5EAP2W IDS=31 AND 33

*COMBINE INTERCEPTED FLOW FROM AP 5 AND ROUTED FLOW FROM AP 4 IN STORM DRAIN
*S44
ADD HYD          ID=36      HYD NO=AP5SD    IDS=53 AND 35

*ROUTE INTERCEPTED FLOW THROUGH AP6 IN 42" PIPE TO 19TH STREET
COMPUTE RATING CURVE CID=1    VS NO=1 CODE=-1 SLP=0.0400
                        DIA=3.5 FT N=0.013

*S46
ROUTE MCUNGE     ID=37      HYD NO=AP619    INFLOW ID=36
                  DT=0.0 HR  LENGTH=550 FT
                  NS=0    SLOPE=0.0400    MATCODE=0
                  REGCODE=0    CCODE=0

*****END AP 5*****
*****BEGIN AP 6*****

*S47
COMPUTE NM HYD   ID=1       HYD NO=6W      AREA=0.0029 SQ MI
                  PER A=0    PER B=10      PER C=0      PER D=90
                  TP=0.111 HR MASS RAIN=-1

*S48
COMPUTE NM HYD   ID=2       HYD NO=6E      AREA=0.0017 SQ MI
                  PER A=0    PER B=15      PER C=25      PER D=60
                  TP=0.111 HR MASS RAIN=-1

*COMBINE STREET FLOW FROM 5W BASIN AND 6W BASIN
*S35
ADD HYD          ID=63      HYD NO=AP6W     IDS=32 AND 1

*COMBINE FLOW FROM 5E BASIN AND 6E BASIN
*S38
ADD HYD          ID=30      HYD NO=AP6E     IDS=34 AND 2

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S40
DIVIDE HYD       ID=63      Q=11.0        ID I=65     HYD NO=AP6WSD
                  ID II=66    HYD NO=AP6WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET
*S41
DIVIDE HYD       ID=30      Q=3.75        ID I=67     HYD NO=AP6ESD
                  ID II=68    HYD NO=AP6EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN
*S42
ADD HYD          ID=64      HYD NO=AP6CSD    IDS=65 AND 67

*COMBINE INTERCEPTED FLOW FROM AP 6 AND ROUTED FLOW FROM AP 5 IN STORM DRAIN
*S44
ADD HYD          ID=36      HYD NO=AP6SD    IDS=37 AND 64

*ROUTE INTERCEPTED FLOW THROUGH AP7 IN 48" PIPE TO 21ST STREET

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COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.0060
DIA=4.0 FT N=0.013

*S46
ROUTE MCUNGE ID=37 HYD NO=AP721 INFLOW ID=36
DT=0.0 HR LENGTH=1200 FT
NS=0 SLOPE=0.006 MATCODE=0
REGCODE=0 CCODE=0

*****END AP 6*****
*****BEGIN AP 7*****

*S49
COMPUTE NM HYD ID=3 HYD NO=7W AREA=0.0094 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*COMBINE STREET FLOW FROM 6W BASIN AND 7W BASIN
*S50
ADD HYD ID=4 HYD NO=7W6W IDS=66 AND 3

*S52
COMPUTE NM HYD ID=5 HYD NO=7E AREA=0.00107 SQ MI
PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 7E BASIN AND 6E BASIN
*S53
ADD HYD ID=6 HYD NO=6E7E IDS=68 AND 5

*S55
COMPUTE NM HYD ID=7 HYD NO=8W AREA=0.00296 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 7W BASIN AND 8W BASIN
*S56
ADD HYD ID=8 HYD NO=7W8W IDS=4 AND 7

*S58
COMPUTE NM HYD ID=9 HYD NO=8E AREA=0.0096 SQ MI
PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 8E BASIN AND 7E BASIN
*S59
ADD HYD ID=10 HYD NO=7E8E IDS=6 AND 9

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S40
DIVIDE HYD ID=8 Q=34 ID I=65 HYD NO=AP7WSD
ID II=66 HYD NO=AP7WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET
*S41
DIVIDE HYD ID=10 Q=12.5 ID I=67 HYD NO=AP7ESD
ID II=68 HYD NO=AP7EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN
*S42
ADD HYD ID=64 HYD NO=AP7CSD IDS=65 AND 67

*COMBINE INTERCEPTED FLOW FROM AP 7 AND ROUTED FLOW FROM AP 6 IN STORM DRAIN
*S44
ADD HYD ID=36 HYD NO=AP7SD IDS=37 AND 64

*ROUTE INTERCEPTED FLOW THROUGH AP8 IN 48" PIPE TO 21ST STREET
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.0060
DIA=4.0 FT N=0.013

*S46
ROUTE MCUNGE ID=37 HYD NO=AP822 INFLOW ID=36
DT=0.0 HR LENGTH=550 FT
NS=0 SLOPE=0.006 MATCODE=0
REGCODE=0 CCODE=0

*****END AP 7*****
*****BEGIN AP 8*****

*S64
COMPUTE NM HYD ID=13 HYD NO=9E AREA=0.013 SQ MI
PER A=0.0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

DIVIDE HYD ID=13 Q=21 ID I=80 HYD NO=AP822SD
ID II=81 HYD NO=AP822ST

*****20TH STREET POND MODEL*****

*S INSERT PUNCH HYDROGRAPH FROM BLACKS ARROYO DMP FOR 20TH STREET POND AND
 *S DISCHARGE INTO EXISTING 48" PIPE. ASSUME THAT IMPROVEMENTS WILL BE MADE
 *S TO CONTROL FLOW RATE IN PIPE WITH FUTURE DEVELOPMENTS.

*S70

RECALL HYD

ID=17	HYD=530.92	DT=.050000	HRS DA=	.1334	SQ MI
PEAK=	59.067CFS	RO= 1.4014	INCHES	NO	PTS=521
FLOW RATES					
.000	.000	.000	.000	.000	.000
.000	.000	.000	.000	.000	.000
.000	.000	.000	.000	.000	.000
.000	.000	.000	.000	.000	.002
.024	.115	.336	.715	1.336	1.336
2.663	5.861	13.602	27.907	41.771	41.771
49.812	54.633	56.785	57.779	58.336	58.336
58.671	58.878	58.996	59.053	59.067	59.067
59.051	59.013	58.955	58.878	58.780	58.780
58.665	58.537	58.399	58.254	58.104	58.104
57.950	57.792	57.632	57.468	57.301	57.301
56.948	56.041	54.691	53.253	51.799	51.799
50.251	48.349	46.167	39.633	28.145	28.145
17.708	10.958	7.134	4.975	3.754	3.754
2.991	2.461	2.101	1.856	1.684	1.684
1.545	1.428	1.339	1.274	1.224	1.224
1.183	1.148	1.120	1.095	1.073	1.073
1.054	1.037	1.023	1.010	.999	.999
.989	.980	.972	.966	.961	.961
.958	.956	.955	.955	.956	.956
.955	.956	.956	.956	.957	.957
.960	.963	.968	.974	.979	.979
.984	.989	.996	1.003	1.011	1.011
1.019	1.028	1.036	1.042	1.050	1.050
1.058	1.068	1.076	1.085	1.094	1.094
1.104	1.113	1.121	1.127	1.129	1.129
1.129	1.128	1.128	1.127	1.126	1.126
1.125	1.122	1.118	1.114	1.110	1.110
1.108	1.105	1.103	1.101	1.097	1.097
1.093	1.088	1.085	1.082	1.079	1.079
1.076	1.072	1.067	1.062	1.059	1.059
1.055	1.052	1.050	1.048	1.046	1.046
1.043	1.039	1.036	1.034	1.031	1.031
1.027	1.023	1.020	1.017	1.013	1.013
1.009	1.005	1.002	.999	.997	.997
.995	.993	.991	.988	.985	.985
.982	.979	.976	.973	.971	.971
.968	.965	.962	.960	.957	.957
.953	.950	.947	.944	.941	.941
.940	.938	.936	.933	.930	.930
.927	.924	.922	.921	.918	.918
.915	.912	.910	.908	.907	.907
.904	.900	.896	.893	.891	.891
.890	.888	.885	.883	.881	.881
.880	.879	.878	.876	.872	.872
.869	.866	.864	.863	.862	.862
.859	.856	.853	.851	.849	.849
.847	.846	.844	.842	.839	.839
.836	.833	.831	.829	.828	.828
.827	.826	.825	.822	.819	.819
.818	.816	.815	.812	.810	.810
.807	.805	.803	.802	.800	.800
.799	.797	.795	.793	.792	.792
.791	.790	.788	.786	.783	.783
.780	.778	.776	.775	.773	.773
.772	.771	.770	.767	.765	.765
.763	.762	.760	.758	.757	.757
.756	.754	.753	.753	.751	.751
.749	.746	.744	.742	.741	.741
.740	.738	.736	.734	.733	.733
.732	.730	.728	.727	.727	.727
.727	.726	.724	.722	.721	.721
.719	.717	.715	.712	.710	.710
.709	.708	.707	.705	.703	.703
.702	.700	.700	.698	.697	.697
.695	.694	.694	.693	.691	.691
.689	.688	.687	.686	.684	.684
.683	.682	.681	.680	.679	.679
.678	.676	.673	.672	.671	.671
.671	.671	.670	.668	.667	.667
.665	.664	.663	.661	.659	.659
.656	.654	.653	.653	.653	.653
.652	.651	.649	.647	.646	.646
.645	.644	.643	.642	.642	.642
.641	.639	.638	.637	.636	.636
.635	.634	.633	.633	.632	.632
.630	.629	.628	.627	.626	.626
.625	.624	.621	.620	.619	.619
.618	.618	.617	.615	.613	.613

.612	.610	.609	.610	.611
.611	.609	.607	.604	.603
.602	.602	.602	.602	.601
.600	.598	.597	.596	.595
.593	.593	.592	.592	.590
.588	.587	.586	.586	.585
.584	.583	.581	.580	.580
.579	.578	.578	.577	.577
.576	.575	.574	.572	.571
.571	.570	.569	.569	.568
.567	.565	.564	.563	.563
.563	.562	.560	.558	.557
.556	.556	.557	.557	.557
.556	.555	.554	.553	.550
.547	.546	.545	.544	.545
.545	.545	.544	.542	.541
.541	.541	.540	.539	.538
.538	.537	.530	.509	.473
.427	.377	.328	.283	.243
.207	.176	.149	.127	.107
.090	.076	.064	.054	.045
.038	.032	.026	.022	.018
.015	.013	.011	.009	.007
.006	.005	.004	.004	.003
.003	.002	.002	.002	.001
.001				

*COMBINE STORM DRAIN FLOW FROM 20 ST POND TO SD AT 22ND STREET

*S71

ADD HYD ID=18 HYD NO=AP8POND IDS=37 AND 17
ADD HYD ID=82 HYD NO=AP822ND IDS=80 AND 18

*ROUTE COMBINED STORM DRAIN FLOW THROUGH AP9 IN 54" PIPE TO 23RD STREET

COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.05

DIA=4.5 FT N=0.013

*S72

ROUTE MCUNGE ID=19 HYD NO=AP9SD INFLOW ID=82
DT=0.0 HR LENGTH=600 FT
NS=0 SLOPE=0.05 MATCODE=0
REGCODE=0 CCODE=0

*****END AP 8*****

*****BEGIN AP 9*****

*S61

COMPUTE NM HYD ID=11 HYD NO=9W AREA=0.00323 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 9W BASIN AND 8W BASIN

*S62

ADD HYD ID=12 HYD NO=8W9W IDS=66 AND 11

*S67

COMPUTE NM HYD ID=15 HYD NO=10E AREA=0.0195 SQ MI
PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*S73

COMPUTE NM HYD ID=20 HYD NO=10W AREA=0.0032 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 10W BASIN AND 9W BASIN

*S74

ADD HYD ID=21 HYD NO=9W10W IDS=12 AND 20

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET

*S79

DIVIDE HYD ID=21 Q=38 ID I=24 HYD NO=AP9WSD
ID II=25 HYD NO=AP9WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET

*S80

DIVIDE HYD ID=68 Q=40 ID I=26 HYD NO=AP9ESD
ID II=27 HYD NO=AP9EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN

*S81

ADD HYD ID=28 HYD NO=AP9EAP3W IDS=24 AND 26

*COMBINE INTERCEPTED FLOW FROM AP 3 AND ROUTED FLOW FROM AP 2 IN STORM DRAIN

*S83

ADD HYD ID=29 HYD NO=AP9SD IDS=19 AND 28

*****END AP 9*****

FINISH

[illegible]


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GC100ULT.SUM
*****END AP 1*****
*****BEGIN AP 2*****
*520
  COMPUTE NM HYD      3WU      - 17      .01230      33.84      1.583
  ADD HYD              AP2W 12&17 7      .01298      44.76      1.670
*515
  DIVIDE HYD          AP2WSD 7 50      .01106      19.90      1.423
                      AP2WST and 51      .00192      24.86      .247
*519
  ROUTE MCUNGE        AP2R 50 53      .01106      19.90      1.423
*****END AP 2*****
*****BEGIN AP 3*****
*521
  COMPUTE NM HYD      3EU      - 18      .00375      9.25      .383
*522
  COMPUTE NM HYD      3WL      - 19      .00803      22.10      1.034
*523
  ADD HYD              3WU3WL 51&19 20      .00995      46.96      1.281
*525
  COMPUTE NM HYD      3EL      - 21      .00268      6.62      .273
*526
  ADD HYD              3EU3EL 18&21 22      .00643      15.87      .656
*515
  DIVIDE HYD          AP3WSD 20 50      .00812      20.00      1.045
                      AP3WST and 55      .00183      26.96      .236
*516
  DIVIDE HYD          AP3ESD 22 56      .00598      11.00      .611
                      AP3EST and 57      .00045      4.87      .046
*517
  ADD HYD              AP3CSD 50&56 58      .01410      31.00      1.656
*517
  ADD HYD              AP3SD 53&58 56      .02516      50.90      3.078
*519
  ROUTE MCUNGE        AP3R 56 59      .02516      50.90      3.072
*****END AP 3*****
*****BEGIN AP 4*****
*528
  COMPUTE NM HYD      4W      - 23      .00546      15.03      .703
*529
  ADD HYD              3WL4W 55&23 24      .00729      41.99      .939
*515
  DIVIDE HYD          AP4WSD 24 60      .00537      12.50      .691
                      AP4WST and 61      .00192      29.49      .248
*517
  ADD HYD              AP4SD 59&60 62      .03053      63.40      3.764
*519
  ROUTE MCUNGE        AP2R 62 53      .03053      63.40      3.764
*****END AP 4*****

COMMAND      HYDROGRAPH IDENTIFICATION NO. FROM TO ID NO. AREA (SQ MI) PEAK DISCHARGE (CFS) RUNOFF VOLUME (AC-FT) TIME TO PEAK (HOURS) RUNOFF (INCHES) CFS PER ACRE PAGE = 3
NOTATION

*****BEGIN AP 5*****
*531
  COMPUTE NM HYD      4E      - 25      .00140      3.46      .143
*532
  ADD HYD              3EL4E 57&25 26      .00185      8.34      .188
*534
  COMPUTE NM HYD      5W      - 27      .00470      12.94      .605
*535
  ADD HYD              AP5W 61&27 28      .00662      42.43      .853
*537
  COMPUTE NM HYD      5E      - 29      .00190      4.70      .194
*538
  ADD HYD              AP5E 26&29 30      .00375      13.03      .382

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GC100ULT.SUM										
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 4
*S40	DIVIDE HYD	AP5WSD 28	31	.00486	14.00	.625	2.41361	1.450	4.506	
		AP5WST and 32		.00177	28.43	.228	2.41361	1.500	25.125	
*S41	DIVIDE HYD	AP5ESD 30	33	.00375	13.03	.382	1.91313	1.500	5.436	
		AP5EST and 34		.00000	.00	.000	.00000	.050	.000	
*S42	ADD HYD	AP5EAP2W 31&33	35	.00860	27.03	1.007	2.19564	1.500	4.911	
*S44	ADD HYD	AP5SD 53&35	36	.03913	90.43	4.771	2.28616	1.500	3.611	
*S46	ROUTE MCUNGE	AP619 36	37	.03913	90.43	4.771	2.28616	1.500	3.611	CCODE = .0
*****END AP 5*****										
*****BEGIN AP 6*****										
*S47	COMPUTE NM HYD	6W -	1	.00290	7.99	.373	2.41367	1.500	4.305	PER IMP= 90.00
*S48	COMPUTE NM HYD	6E -	2	.00170	4.20	.173	1.91328	1.500	3.863	PER IMP= 60.00
*S35	ADD HYD	AP6W 32& 1	63	.00467	36.42	.601	2.41360	1.500	12.191	
*S38	ADD HYD	AP6E 34& 2	30	.00170	4.20	.173	1.91312	1.500	3.863	
*S40	DIVIDE HYD	AP6WSD 63	65	.00310	11.00	.399	2.41360	1.450	5.551	
		AP6WST and 66		.00157	25.42	.202	2.41360	1.500	25.273	
*S41	DIVIDE HYD	AP6ESD 30	67	.00167	3.75	.170	1.91312	1.450	3.515	
		AP6EST and 68		.00003	.45	.003	1.91312	1.500	21.429	
*S42	ADD HYD	AP6CSD 65&67	64	.00476	14.75	.569	2.23845	1.450	4.838	
*S44	ADD HYD	AP6SD 37&64	36	.04389	105.18	5.340	2.28098	1.500	3.744	
*S46	ROUTE MCUNGE	AP721 36	37	.04389	103.58	5.332	2.27754	1.500	3.687	CCODE = .2
*****END AP 6*****										
*****BEGIN AP 7*****										
*S49	COMPUTE NM HYD	7W -	3	.00940	25.87	1.210	2.41367	1.500	4.300	PER IMP= 90.00
*S50										
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 4
ADD HYD		7W6W 66& 3	4	.01097	51.29	1.412	2.41364	1.500	7.304	
*S52	COMPUTE NM HYD	7E -	5	.00107	2.65	.109	1.91328	1.500	3.869	PER IMP= 60.00
*S53	ADD HYD	6E7E 68& 5	6	.00110	3.10	.113	1.91308	1.500	4.395	
*S55	COMPUTE NM HYD	8W -	7	.00296	8.16	.381	2.41367	1.500	4.305	PER IMP= 90.00
*S56	ADD HYD	7W8W 4& 7	8	.01393	59.44	1.793	2.41363	1.500	6.667	
*S58	COMPUTE NM HYD	8E -	9	.00960	23.67	.980	1.91328	1.500	3.853	PER IMP= 60.00
*S59	ADD HYD	7E8E 6& 9	10	.01070	26.77	1.092	1.91323	1.500	3.909	
*S40	DIVIDE HYD	AP7WSD 8	65	.01237	34.00	1.593	2.41363	1.450	4.294	
		AP7WST and 66		.00156	25.44	.201	2.41363	1.500	25.492	
*S41	DIVIDE HYD	AP7ESD 10	67	.00889	12.50	.907	1.91323	1.400	2.198	
		AP7EST and 68		.00182	14.27	.185	1.91323	1.500	12.271	
*S42	ADD HYD	AP7CSD 65&67	64	.02126	46.50	2.499	2.20447	1.450	3.418	
*S44										

ADD HYD	AP7SD 37&64	36	.06515	150.08	GC100ULT.SUM	2.25369	1.500	3.600	
*S46	ROUTE MCUNGE	AP822 36 37	.06515	132.32	7.831				
*S*****	*****END AP 7*****				7.686				.2
*S*****	*****BEGIN AP 8*****								
*S64	COMPUTE NM HYD	9E - 13	.01300	32.05	1.327				
DIVIDE HYD	AP822SD 13 80		.01190	21.00	1.215				
	AP822ST and 81		.00110	11.05	.112				
*S*****	*****20TH STREET POND MODEL*****								
*S	INSERT PUNCH HYDROGRAPH FROM BLACKS ARROYO DMP FOR 20TH STREET POND AND								
*S	DISCHARGE INTO EXISTING 48" PIPE. ASSUME THAT IMPROVEMENTS WILL BE MADE								
*S	TO CONTROL FLOW RATE IN PIPE WITH FUTURE DEVELOPMENTS.								
*S70	RECALL HYD	530.92 - 17	.13340	59.07	9.968				
*S71	ADD HYD	AP8POND 37&17 18	.19855	185.91	17.654				
ADD HYD	AP822ND 80&18 82		.21045	206.91	18.869				
*S72	ROUTE MCUNGE	AP9SD 82 19	.21045	206.91	18.869				.0
*S*****	*****END AP 8*****								
*S*****	*****BEGIN AP 9*****								
*S61	COMPUTE NM HYD	9W - 11	.00323	8.90	.416				
*S62	ADD HYD	8W9W 66&11 12	.00479	34.34	.617				
*S67	COMPUTE NM HYD	10E - 15	.01950	48.07	1.990				
*S73									
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 5 NOTATION
COMPUTE NM HYD	10W - 20			8.81	.412	2.41367	1.500	4.303	PER IMP= 90.00
*S74	ADD HYD	9W10W 12&20 21	.00799	43.15	1.028	2.41360	1.500	8.439	
*S79	DIVIDE HYD	AP9WSD 21 24	.00774	38.00	.996	2.41360	1.450	7.671	
	AP9WST and 25		.00025	5.15	.032	2.41359	1.500	32.231	
*S80	DIVIDE HYD	AP9ESD 68 26	.00182	14.27	.185	1.91323	1.500	12.271	
	AP9EST and 27		.00000	.00	.000	.00000	-.050	.000	
*S81	ADD HYD	AP9EAP3W 24&26 28	.00956	52.27	1.182	2.31844	1.500	8.546	
*S83	ADD HYD	AP9SD 19&28 29	.22001	255.41	20.051	1.70879	1.500	1.814	
*S*****	*****END AP 9*****								
FINISH									

Modified Ultimate
Conditions

*S GOLF COURSE ROAD HYDROLOGY
 *S AHYMO MODEL TO CALCULATE RUNOFF BASED ON PROPOSED CONDITIONS (MODIFIED TO
 *S REPRESENT ULTIMATE CONDITIONS AS SHOWN IN THE b1wmp BY dsa 3/07/06)
 *S ON GOLF COURSE ROAD FROM SOUTHERN BLVD SOUTH TO 23RD STREET DETENTION PONDS
 *S THIS MODEL ASSUMES THAT ALL LOTS ADJACENT TO THE WEST SIDE OF GOLF COURSE
 *S WILL BE DEVELOPED AS COMMERCIAL LOTS AND THAT ON-SITE DETENTION WILL BE
 *S REQUIRED TO CONTROL RUNOFF ABOVE HISTORICAL VALUES.

*S DRAINAGE BASIN DELINEATIONS WERE MADE IN ACCORDANCE WITH THE BLACKS ARROYO
 *S DRAINAGE MASTER PLAN TO BE COMPLETED FOR SSCAFCA. BULKING FACTOR ADDED IN
 *S ACCORDANCE WITH SSCAFCA REQUIREMENTS FOR THE BLACKS ARROYO ANALYSIS.

*S*****
 *S***** 100-YEAR STORM *****
 *S*****
 *

START TIME=0.0 HR PUNCH CODE=0

*EACH STORM INPUT DATA FOLLOWS

RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 RAIN ONE=1.80 IN RAIN SIX=2.21 IN
 RAIN DAY=2.7 IN DT=0.05 HRS

*TWO YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=0.739 IN RAIN SIX=0.925 IN
 * RAIN DAY=1.075 IN DT=0.05 HRS

*FIVE YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.001 IN RAIN SIX=1.250 IN
 * RAIN DAY=1.475 IN DT=0.05 HRS

*TEN YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.184 IN RAIN SIX=1.450 IN
 * RAIN DAY=1.700 IN DT=0.05 HRS

*TWENTY FIVE YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.394 IN RAIN SIX=1.825 IN
 * RAIN DAY=2.100 IN DT=0.05 HRS

*FIFTY YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.604 IN RAIN SIX=2.000 IN
 * RAIN DAY=2.350 IN DT=0.05 HRS

*HUNDRED YEAR STORM DATA
 *RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
 * RAIN ONE=1.878 IN RAIN SIX=2.225 IN
 * RAIN DAY=2.700 IN DT=0.05 HRS

*S*****BEGIN AP 1*****

*S1
 SEDIMENT BULK CODE=1 BULK FACTOR=1.06

*S1A
 COMPUTE NM HYD ID=1 HYD NO=1W AREA=0.00794 SQ MI
 PER A=0 PER B=10 PER C=0 PER D=90
 TP=0.111 HR MASS RAIN=-1

*S2
 COMPUTE NM HYD ID=2 HYD NO=1E AREA=0.003 SQ MI
 PER A=0 PER B=15 PER C=25 PER D=60
 TP=0.111 HR MASS RAIN=-1

*FOR THIS MODEL, SPLIT BASIN 2W INTO UPPER (U) AND LOWER (L) BASINS

*S3
 COMPUTE NM HYD ID=3 HYD NO=2WU AREA=0.00803 SQ MI
 PER A=0 PER B=10 PER C=0 PER D=90
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 2WU BASIN AND 1W BASIN

*S4
 ADD HYD ID=4 HYD NO=1W2WU IDS=1 AND 3

*S5 PLOT
 PLOT HYD ID=1 ID=3 Q SCALE=0 T SCALE=0

*S6
 COMPUTE NM HYD ID=5 HYD NO=2EU AREA=0.00225 SQ MI
 PER A=0 PER B=15 PER C=25.0 PER D=60.0
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 2EU BASIN AND 1E BASIN

```

*S7
ADD HYD          ID=6          HYD NO=1E2EU      IDS=2 AND 5

*S8 PLOT
PLOT HYD          ID=2    ID=5    Q SCALE=0    T SCALE=0

*S9
COMPUTE NM HYD    ID=7          HYD NO=2WL        AREA=0.0058 SQ MI
                  PER A=0        PER B=10          PER C=0          PER D=90
                  TP=0.111 HR  MASS RAIN=-1

*COMBINE FLOW FROM 2WU BASIN AND 2WL BASIN
*S10
ADD HYD          ID=8          HYD NO=AP1W        IDS=4 AND 7

*S11 PLOT
PLOT HYD          ID=4    ID=7    Q SCALE=0    T SCALE=0

*S12
COMPUTE NM HYD    ID=9          HYD NO=2EL        AREA=0.0018 SQ MI
                  PER A=0        PER B=15          PER C=25          PER D=60
                  TP=0.111 HR  MASS RAIN=-1

*COMBINE FLOW FROM 2EU BASIN AND 2EL BASIN
*S13
ADD HYD          ID=10         HYD NO=AP1E        IDS=6 AND 9

*S14 PLOT
PLOT HYD          ID=6    ID=9    Q SCALE=0    T SCALE=0

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S15
DIVIDE HYD        ID=8          Q=32              ID I=11    HYD NO=AP1WSD
                  ID II=12     HYD NO=AP1WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET
*S16
DIVIDE HYD        ID=10         Q=11              ID I=13    HYD NO=AP1ESD
                  ID II=14     HYD NO=AP1EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN
*S17
ADD HYD          ID=15         HYD NO=AP1SD        IDS=11 AND 13

*S18 PLOT
PLOT HYD          ID=11    ID=13    Q SCALE=0    T SCALE=0

*S*****
*S*****ROUTE INTERCEPTED FLOW THROUGH DOWN CHIANTI (13TH STREET) IN 30" PIPE
COMPUTE RATING CURVE CID=1    VS NO=1 CODE=-1 SLP=0.015
                        DIA=2.5 FT N=0.013

*S19
ROUTE MCUNGE      ID=16    HYD NO=AP1R    INFLOW ID=15
                  DT=0.0 HR    LENGTH=1170 FT
                  NS=0    SLOPE=0.0150    MATCODE=0
                  REGCODE=0    CCODE=0

*S*****
*S*****END AP 1*****
*S*****BEGIN AP 2*****

*FOR THIS MODEL, SPLIT BASIN 3W INTO UPPER (U) AND LOWER (L) BASINS
*S20
COMPUTE NM HYD    ID=17         HYD NO=3WU        AREA=0.0123 SQ MI
                  PER A=0        PER B=10          PER C=0          PER D=90
                  TP=0.111 HR  MASS RAIN=-1

*TOTAL SURFACE FLOW AT AP2
ADD HYD          ID=7          HYD NO=AP2W        IDS=12 AND 17

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
*S15
DIVIDE HYD        ID=7          Q=20              ID I=50    HYD NO=AP2WSD
                  ID II=51     HYD NO=AP2WST

*ROUTE INTERCEPTED FLOW THROUGH AP2 IN 30" PIPE TO AP3
COMPUTE RATING CURVE CID=1    VS NO=1 CODE=-1 SLP=0.04
                        DIA=2.5 FT N=0.013

*S19
ROUTE MCUNGE      ID=53    HYD NO=AP2R    INFLOW ID=50
                  DT=0.0 HR    LENGTH=770 FT
                  NS=0    SLOPE=0.040    MATCODE=0
                  REGCODE=0    CCODE=0

*S*****
*S*****END AP 2*****
*S*****BEGIN AP 3*****

*S21

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 COMPUTE NM HYD ID=18 HYD NO=3EU AREA=0.00375 SQ MI
 PER A=0 PER B=15 PER C=25 PER D=60
 TP=0.111 HR MASS RAIN=-1

*S22
 COMPUTE NM HYD ID=19 HYD NO=3WL AREA=0.00803 SQ MI
 PER A=0 PER B=10 PER C=0 PER D=90
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 3WU BASIN AND 3WL BASIN
 *S23
 ADD HYD ID=20 HYD NO=AP3W IDS=51 AND 19

*S25
 COMPUTE NM HYD ID=21 HYD NO=3EL AREA=0.00268 SQ MI
 PER A=0 PER B=15 PER C=25 PER D=60
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM AP1E BASIN AND 3EU BASIN
 *S26
 ADD HYD ID=81 HYD NO=AP1E3EU IDS=18 AND 14

*COMBINE FLOW FROM 3EL BASIN AND 3EU BASIN
 *S26
 ADD HYD ID=22 HYD NO=AP3E IDS=81 AND 21

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
 *S15
 DIVIDE HYD ID=20 Q=20 ID I=50 HYD NO=AP3WSD
 ID II=55 HYD NO=AP3WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET
 *S16
 DIVIDE HYD ID=22 Q=12 ID I=56 HYD NO=AP3ESD
 ID II=57 HYD NO=AP3EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN
 *S17
 ADD HYD ID=58 HYD NO=AP3CSD IDS=50 AND 56

*COMBINE INTERCEPTED FLOW WITH ROUTED FLOW FROM AP2
 *S17
 ADD HYD ID=56 HYD NO=AP3SD IDS=53 AND 58

*ROUTE INTERCEPTED FLOW THROUGH AP3 IN 36" PIPE TO AP4
 COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.018
 DIA=3.0 FT N=0.013

*S19
 ROUTE MCUNGE ID=59 HYD NO=AP3R INFLOW ID=56
 DT=0.0 HR LENGTH=514 FT
 NS=0 SLOPE=0.018 MATCODE=0
 REGCODE=0 CCODE=0

*****END AP 3*****
 *****BEGIN AP 4*****

*S28
 COMPUTE NM HYD ID=23 HYD NO=4W AREA=0.00546 SQ MI
 PER A=0 PER B=10 PER C=0 PER D=90
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 4W BASIN AND 3WL BASIN
 *S29
 ADD HYD ID=24 HYD NO=3WL4W IDS=55 AND 23

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET
 *S15
 DIVIDE HYD ID=24 Q=12.5 ID I=60 HYD NO=AP4WSD
 ID II=61 HYD NO=AP4WST

*COMBINE INTERCEPTED FLOW FROM WEST SIDE OF ROADWAY IN STORM DRAIN
 *S17
 ADD HYD ID=62 HYD NO=AP4SD IDS=59 AND 60

*ROUTE INTERCEPTED FLOW THROUGH AP2 IN 36" PIPE TO AP3
 COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.0525
 DIA=3.0 FT N=0.013

*S19
 ROUTE MCUNGE ID=53 HYD NO=AP2R INFLOW ID=62
 DT=0.0 HR LENGTH=600 FT
 NS=0 SLOPE=0.0525 MATCODE=0
 REGCODE=0 CCODE=0

*****END AP 4*****
 *****BEGIN AP 5*****

*S31
 COMPUTE NM HYD ID=25 HYD NO=4E AREA=0.0014 SQ MI

PER A=0.0 PER B=15
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 4E BASIN AND STREET FLOW

*S32
ADD HYD ID=26 HYD NO=3EL4E IDS=57 AND 25

*S34
COMPUTE NM HYD ID=27 HYD NO=5W AREA=0.0047 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*COMBINE STREET FLOW FROM 4W BASIN AND 5W BASIN

*S35
ADD HYD ID=28 HYD NO=AP5W IDS=61 AND 27

*S37
COMPUTE NM HYD ID=29 HYD NO=5E AREA=0.0019 SQ MI
PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 4E BASIN AND 5E BASIN

*S38
ADD HYD ID=30 HYD NO=AP5E IDS=26 AND 29

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET

*S40
DIVIDE HYD ID=28 Q=14 ID I=31 HYD NO=AP5WSD
ID II=32 HYD NO=AP5WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET

*S41
DIVIDE HYD ID=30 Q=12 ID I=33 HYD NO=AP5ESD
ID II=34 HYD NO=AP5EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN

*S42
ADD HYD ID=35 HYD NO=AP5EAP2W IDS=31 AND 33

*COMBINE INTERCEPTED FLOW FROM AP 5 AND ROUTED FLOW FROM AP 4 IN STORM DRAIN

*S44
ADD HYD ID=36 HYD NO=AP5SD IDS=53 AND 35

*ROUTE INTERCEPTED FLOW THROUGH AP6 IN 42" PIPE TO 19TH STREET

COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.0400
DIA=3.5 FT N=0.013

*S46
ROUTE MCUNGE ID=37 HYD NO=AP619 INFLOW ID=36
DT=0.0 HR LENGTH=550 FT
NS=0 SLOPE=0.0400 MATCODE=0
REGCODE=0 CCODE=0

*S*****END AP 5*****
*****BEGIN AP 6*****

*S47
COMPUTE NM HYD ID=1 HYD NO=6W AREA=0.0029 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*S48
COMPUTE NM HYD ID=2 HYD NO=6E AREA=0.0017 SQ MI
PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*COMBINE STREET FLOW FROM 5W BASIN AND 6W BASIN

*S35
ADD HYD ID=63 HYD NO=AP6W IDS=32 AND 1

*COMBINE FLOW FROM 5E BASIN AND 6E BASIN

*S38
ADD HYD ID=30 HYD NO=AP6E IDS=34 AND 2

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET

*S40
DIVIDE HYD ID=63 Q=11 ID I=65 HYD NO=AP6WSD
ID II=66 HYD NO=AP6WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET

*S41
DIVIDE HYD ID=30 Q=4 ID I=67 HYD NO=AP6ESD
ID II=68 HYD NO=AP6EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN

*S42
ADD HYD ID=64 HYD NO=AP6CSD IDS=65 AND 67

*COMBINE INTERCEPTED FLOW FROM AP 6 AND ROUTED FLOW FROM AP 5 IN STORM DRAIN

*S44
ADD HYD ID=36 HYD NO=AP6SD IDS=37 AND 64

*ROUTE INTERCEPTED FLOW THROUGH AP7 IN 48" PIPE TO 21ST STREET
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.0060
DIA=4.0 FT N=0.013

*S46
ROUTE MCUNGE ID=37 HYD NO=AP721 INFLOW ID=36
DT=0.0 HR LENGTH=1200 FT
NS=0 SLOPE=0.006 MATCODE=0
REGCODE=0 CCODE=0

*S*****END AP 6*****
*S*****BEGIN AP 7*****

*S49
COMPUTE NM HYD ID=3 HYD NO=7W AREA=0.0094 SQ MI
PER A=0 PER B=15 PER C=5 PER D=80
TP=0.111 HR MASS RAIN=-1

*COMBINE STREET FLOW FROM 6W BASIN AND 7W BASIN

*S50
ADD HYD ID=4 HYD NO=7W6W IDS=66 AND 3

*S52
COMPUTE NM HYD ID=5 HYD NO=7E AREA=0.00107 SQ MI
PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 7E BASIN AND 6E BASIN

*S53
ADD HYD ID=6 HYD NO=6E7E IDS=68 AND 5

*S55
COMPUTE NM HYD ID=7 HYD NO=8W AREA=0.00296 SQ MI
PER A=0 PER B=10 PER C=0 PER D=90
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 7W BASIN AND 8W BASIN

*S56
ADD HYD ID=8 HYD NO=AP7W IDS=4 AND 7

*S58
COMPUTE NM HYD ID=9 HYD NO=8E AREA=0.0096 SQ MI
PER A=0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 8E BASIN AND 7E BASIN

*S59
ADD HYD ID=10 HYD NO=AP7E IDS=6 AND 9

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET

*S40
DIVIDE HYD ID=8 Q=20 ID I=65 HYD NO=AP7WSD
ID II=66 HYD NO=AP7WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET

*S41
DIVIDE HYD ID=10 Q=11 ID I=67 HYD NO=AP7ESD
ID II=68 HYD NO=AP7EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN

*S42
ADD HYD ID=64 HYD NO=AP7CSD IDS=65 AND 67

*COMBINE INTERCEPTED FLOW FROM AP 7 AND ROUTED FLOW FROM AP 6 IN STORM DRAIN

*S44
ADD HYD ID=36 HYD NO=AP7SD IDS=37 AND 64

*ROUTE INTERCEPTED FLOW THROUGH AP8 IN 48" PIPE TO 21ST STREET
COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.0060
DIA=4.0 FT N=0.013

*S46
ROUTE MCUNGE ID=37 HYD NO=AP822 INFLOW ID=36
DT=0.0 HR LENGTH=550 FT
NS=0 SLOPE=0.006 MATCODE=0
REGCODE=0 CCODE=0

*S*****END AP 7*****
*S*****BEGIN AP 8*****

*S64
COMPUTE NM HYD ID=13 HYD NO=9E AREA=0.013 SQ MI
PER A=0.0 PER B=15 PER C=25 PER D=60
TP=0.111 HR MASS RAIN=-1

DIVIDE HYD ID=13 Q=16 ID I=80 HYD NO=AP822SD

*S*****20TH STREET POND MODEL*****

*S INSERT PUNCH HYDROGRAPH FROM BLACKS ARROYO DMP FOR 20TH STREET POND AND
*S DISCHARGE INTO EXISTING 48" PIPE. ASSUME THAT IMPROVEMENTS WILL BE MADE
*S TO CONTROL FLOW RATE IN PIPE WITH FUTURE DEVELOPMENTS.

*S70

RECALL HYD

ID=17 HYD=530.92 DT=.050000 HRS DA=.1334 SQ MI
PEAK= 59.067CFS RO= 1.4014 INCHES NO PTS=521
FLOW RATES

.000	.000	.000	.000	.000
.000	.000	.000	.000	.000
.000	.000	.000	.000	.000
.000	.000	.000	.000	.002
.024	.115	.336	.715	1.336
2.663	5.861	13.602	27.907	41.771
49.812	54.633	56.785	57.779	58.336
58.671	58.878	58.996	59.053	59.067
59.051	59.013	58.955	58.878	58.780
58.665	58.537	58.399	58.254	58.104
57.950	57.792	57.632	57.468	57.301
56.948	56.041	54.691	53.253	51.799
50.251	48.349	46.167	39.633	28.145
17.708	10.958	7.134	4.975	3.754
2.991	2.461	2.101	1.856	1.684
1.545	1.428	1.339	1.274	1.224
1.183	1.148	1.120	1.095	1.073
1.054	1.037	1.023	1.010	.999
.989	.980	.972	.966	.961
.958	.956	.955	.955	.956
.955	.956	.956	.956	.957
.960	.963	.968	.974	.979
.984	.989	.996	1.003	1.011
1.019	1.028	1.036	1.042	1.050
1.058	1.068	1.076	1.085	1.094
1.104	1.113	1.121	1.127	1.129
1.129	1.128	1.128	1.127	1.126
1.125	1.122	1.118	1.114	1.110
1.108	1.105	1.103	1.101	1.097
1.093	1.088	1.085	1.082	1.079
1.076	1.072	1.067	1.062	1.059
1.055	1.052	1.050	1.048	1.046
1.043	1.039	1.036	1.034	1.031
1.027	1.023	1.020	1.017	1.013
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.995	.993	.991	.988	.985
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.953	.950	.947	.944	.941
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.927	.924	.922	.921	.918
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.780	.778	.776	.775	.773
.772	.771	.770	.767	.765
.763	.762	.760	.758	.757
.756	.754	.753	.753	.751
.749	.746	.744	.742	.741
.740	.738	.736	.734	.733
.732	.730	.728	.727	.727
.727	.726	.724	.722	.721
.719	.717	.715	.712	.710
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.588	.587	.586	.586	.585
.584	.583	.581	.580	.580
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.547	.546	.545	.544	.545
.545	.545	.544	.542	.541
.541	.541	.540	.539	.538
.538	.537	.530	.509	.473
.427	.377	.328	.283	.243
.207	.176	.149	.127	.107
.090	.076	.064	.054	.045
.038	.032	.026	.022	.018
.015	.013	.011	.009	.007
.006	.005	.004	.004	.003
.003	.002	.002	.002	.001
.001				

*COMBINE STORM DRAIN FLOW FROM 20 ST POND TO SD AT 22ND STREET

*S71
 ADD HYD ID=18 HYD NO=AP8POND IDS=37 AND 17
 ADD HYD ID=82 HYD NO=AP822ND IDS=80 AND 18

*ROUTE COMBINED STORM DRAIN FLOW THROUGH AP9 IN 54" PIPE TO 23RD STREET
 COMPUTE RATING CURVE CID=1 VS NO=1 CODE=-1 SLP=0.05
 DIA=4.5 FT N=0.013

*S72
 ROUTE MCUNGE ID=19 HYD NO=AP9SD INFLOW ID=82
 DT=0.0 HR LENGTH=600 FT
 NS=0 SLOPE=0.05 MATCODE=0
 REGCODE=0 CCODE=0

S***END AP 8*****
 *S*****BEGIN AP 9*****

*S61
 COMPUTE NM HYD ID=11 HYD NO=9W AREA=0.00323 SQ MI
 PER A=0 PER B=10 PER C=0 PER D=90
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 9W BASIN AND 8W BASIN

*S62
 ADD HYD ID=12 HYD NO=8W9W IDS=66 AND 11

*S67
 COMPUTE NM HYD ID=15 HYD NO=10E AREA=0.0195 SQ MI
 PER A=0 PER B=15 PER C=25 PER D=60
 TP=0.111 HR MASS RAIN=-1

*COMBINE BYPASS FLOW FROM 9E BASIN AND 10E BASIN

*S68
 ADD HYD ID=16 HYD NO=AP9E IDS=68 AND 81

*S73
 COMPUTE NM HYD ID=20 HYD NO=10W AREA=0.0032 SQ MI
 PER A=0 PER B=10 PER C=0 PER D=90
 TP=0.111 HR MASS RAIN=-1

*COMBINE FLOW FROM 10W BASIN AND 9W BASIN

*S74
 ADD HYD ID=21 HYD NO=AP9W IDS=12 AND 20

*DIVIDE WEST FLOW BETWEEN STORM DRAIN AND STREET

*S79
 DIVIDE HYD ID=21 Q=28 ID I=24 HYD NO=AP9WSD
 ID II=25 HYD NO=AP9WST

*DIVIDE EAST FLOW BETWEEN STORM DRAIN AND STREET

*S80
 DIVIDE HYD ID=16 Q=20 ID I=26 HYD NO=AP9ESD
 ID II=27 HYD NO=AP9EST

*COMBINE INTERCEPTED FLOW FROM EAST AND WEST SIDES OF ROADWAY IN STORM DRAIN

*S81

GC100ULTmod.txt
ADD HYD ID=28 HYD NO=AP9EAP9W IDS=24 AND 26
*COMBINE INTERCEPTED FLOW FROM AP 9 AND ROUTED FLOW FROM AP 8 IN STORM DRAIN
*S83
ADD HYD ID=29 HYD NO=AP9SD IDS=19 AND 28

*S*****END AP 9*****
FINISH

ROUTE	MCUNGE	AP1R	15	16	GC100ULmod.SUM	2.28628	1.450	2.639	CCODE =	.1
*S20	COMPUTE NM HYD	3WU	-	17	.01230	33.84	1.583	4.299	PER IMP=	90.00
*S21	ADD HYD	AP2W	12&17	7	.01500	61.76	1.931	6.432		
*S15	DIVIDE HYD	AP2WSD	7	50	.01108	20.00	1.427	2.820		
*S19		AP2WST	and	51	.00392	41.76	.505	16.648		
*S21	ROUTE MCUNGE	AP2R	50	53	.01108	20.00	1.426	2.820	CCODE =	.1
*S22	COMPUTE NM HYD	3EU	-	18	.00375	9.25	.383	3.856	PER IMP=	60.00
*S23	COMPUTE NM HYD	3WL	-	19	.00803	22.10	1.034	4.300	PER IMP=	90.00
*S25	ADD HYD	AP3W	51&19	20	.01195	63.86	1.538	8.350		
*S26	COMPUTE NM HYD	3EL	-	21	.00268	6.62	.273	3.859	PER IMP=	60.00
*S27	ADD HYD	AP1E3EU	18&14	81	.00441	15.67	.450	5.548		
*S28	ADD HYD	AP3E	81&21	22	.00709	22.28	.724	4.910		
*S15	DIVIDE HYD	AP3WSD	20	50	.00819	20.00	1.054	3.816		
*S16	DIVIDE HYD	AP3WST	and	55	.00376	43.86	.484	18.221		
*S17	COMPUTE NM HYD	AP3ESD	22	56	.00615	12.00	.627	3.051		
*S18	ADD HYD	AP3EST	and	57	.00095	10.28	.097	16.985		
*S19	ADD HYD	AP3CSD	50&56	58	.01433	32.00	1.681	3.488		
*S20	ADD HYD	AP3SD	53&58	56	.02542	52.00	3.107	3.197		
*S21	ROUTE MCUNGE	AP3R	56	59	.02542	52.00	3.101	3.197	CCODE =	.1
*S22	COMPUTE NM HYD	4W	-	23	.00546	15.03	.703	4.302	PER IMP=	90.00
*S23	ADD HYD	3WL4W	55&23	24	.00922	58.89	1.187	9.979		
*S15	DIVIDE HYD	AP4WSD	24	60	.00538	12.50	.692	3.632		
*S17		AP4WST	and	61	.00384	46.39	.495	18.860		
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID	TO ID	NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 3
ADD HYD		AP4SD	59&60	62	.03079	64.50	3.793	2.30975	3.273	NOTATION
*S19	ROUTE MCUNGE	AP2R	62	53	.03079	64.50	3.793	2.30975	3.273	CCODE = .0
*S31	COMPUTE NM HYD	4E	-	25	.00140	3.46	.143	1.91328	3.866	PER IMP= 60.00
*S32	ADD HYD	3EL4E	57&25	26	.00235	13.75	.239	1.91312	9.156	
*S34	COMPUTE NM HYD	5W	-	27	.00470	12.94	.605	2.41367	4.302	PER IMP= 90.00
*S35	ADD HYD	AP5W	61&27	28	.00854	59.33	1.100	2.41362	10.851	

GC100ULTmod.SUM

*S37	COMPUTE NM HYD	5E	-	29	.00190	4.70	.194	1.91328	1.500	3.862	PER IMP=	60.00
*S38	ADD HYD	AP5E 26&29	30		.00425	18.44	.433	1.91314	1.500	6.787		
*S40	DIVIDE HYD	AP5WSD 28	31		.00504	14.00	.649	2.41362	1.400	4.336		
		AP5WST and 32	32		.00350	45.33	.450	2.41362	1.500	20.247		
*S41	DIVIDE HYD	AP5ESD 30	33		.00376	12.00	.384	1.91314	1.450	4.986		
		AP5EST and 34	34		.00049	6.44	.050	1.91314	1.500	20.722		
*S42	ADD HYD	AP5EAP2W 31&33	35		.00881	26.00	1.033	2.19989	1.450	4.614		
*S44	ADD HYD	AP5SD 53&35	36		.03960	90.50	4.827	2.28532	1.500	3.571		
*S46	ROUTE MCUNGE	AP619 36	37		.03960	90.50	4.827	2.28532	1.500	3.571	CCODE =	.0
*****END AP 5*****												
*S47	*****BEGIN AP 6*****	6W	-	1	.00290	7.99	.373	2.41367	1.500	4.305	PER IMP=	90.00
*S48	COMPUTE NM HYD	6E	-	2	.00170	4.20	.173	1.91328	1.500	3.863	PER IMP=	60.00
*S35	ADD HYD	AP6W 32& 1	63		.00640	53.32	.824	2.41361	1.500	13.021		
*S38	ADD HYD	AP6E 34& 2	30		.00219	10.65	.223	1.91312	1.500	7.610		
*S40	DIVIDE HYD	AP6WSD 63	65		.00342	11.00	.440	2.41361	1.400	5.032		
		AP6WST and 66	66		.00298	42.32	.384	2.41361	1.500	22.170		
*S41	DIVIDE HYD	AP6ESD 30	67		.00169	4.00	.172	1.91313	1.450	3.704		
		AP6EST and 68	68		.00050	6.65	.051	1.91312	1.500	20.827		
*S42	ADD HYD	AP6CSD 65&67	64		.00510	15.00	.612	2.24812	1.450	4.593		
*S44	ADD HYD	AP6SD 37&64	36		.04470	105.50	5.438	2.28108	1.500	3.688		
*S46	ROUTE MCUNGE	AP721 36	37		.04470	104.83	5.430	2.27765	1.500	3.664	CCODE =	.2
*****END AP 6*****												
COMMAND	HYDROGRAPH IDENTIFICATION	FROM NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	NOTATION	
*****BEGIN AP 7*****												
*S49	COMPUTE NM HYD	7W	-	3	.00940	24.82	1.121	2.23579	1.500	4.126	PER IMP=	80.00
*S50	ADD HYD	7W6W 66& 3	4		.01238	67.14	1.505	2.27860	1.500	8.472		
*S52	COMPUTE NM HYD	7E	-	5	.00107	2.65	.109	1.91328	1.500	3.869	PER IMP=	60.00
*S53	ADD HYD	6E7E 68& 5	6		.00157	9.30	.160	1.91309	1.500	9.260		
*S55	COMPUTE NM HYD	8W	-	7	.00296	8.16	.381	2.41367	1.500	4.305	PER IMP=	90.00
*S56	ADD HYD	AP7W 4& 7	8		.01534	75.29	1.886	2.30464	1.500	7.668		
*S58	COMPUTE NM HYD	8E	-	9	.00960	23.67	.980	1.91328	1.500	3.853	PER IMP=	60.00
*S59	ADD HYD	AP7E 6& 9	10		.01117	32.97	1.140	1.91323	1.500	4.612		
*S40	DIVIDE HYD	AP7WSD 8	65		.01104	20.00	1.357	2.30464	1.400	2.830		
		AP7WST and 66	66		.00430	55.29	.529	2.30464	1.500	20.085		
*S41	DIVIDE HYD	AP7ESD 10	67		.00854	11.00	.871	1.91323	1.350	2.014		

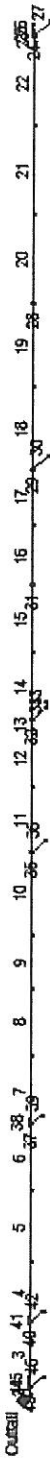
GC100ULTmod.SUM									
*S42	AP7EST and 68	.00263	21.97	1.91323	1.500	13.038			
ADD HYD	AP7CSD 65&67 64	.01958	31.00	2.13398	1.400	2.474			
*S44	ADD HYD								
ADD HYD	AP7SD 37&64 36	.06428	135.83	2.23388	1.500	3.302			
*S46									
ROUTE MCUNGE	AP822 36 37	.06428	125.78	2.19960	1.550	3.057	CCODE =	.2	
*S*****	*****END AP 7*****								
*S*****	*****BEGIN AP 8*****								
*S64									
COMPUTE NM HYD	9E - 13	.01300	32.05	1.91328	1.500	3.852	PER IMP=	60.00	
DIVIDE HYD	AP822SD 13 80	.01098	16.00	1.91326	1.400	2.276			
	AP822ST and 81	.00202	16.05	1.91326	1.500	12.445			
*S*****	*****20TH STREET POND MODEL*****								
*S*****	*****PUNCH HYDROGRAPH FROM BLACKS ARROYO DMP FOR 20TH STREET POND AND								
*S*****	*****DISCHARGE INTO EXISTING 48" PIPE. ASSUME THAT IMPROVEMENTS WILL BE MADE								
*S*****	*****S TO CONTROL FLOW RATE IN PIPE WITH FUTURE DEVELOPMENTS.								
*S70									
RECALL HYD	530.92 - 17	.13340	59.07	1.40108	1.950	.692			
*S71									
ADD HYD	AP8POND 37&17 18	.19768	180.41	1.66073	1.550	1.426			
ADD HYD	AP822ND 80&18 82	.20866	196.41	1.67403	1.550	1.471			
*S72									
ROUTE MCUNGE	AP9SD 82 19	.20866	196.41	1.67403	1.550	1.471	CCODE =	.0	
*S*****	*****END AP 8*****								
*S*****	*****BEGIN AP 9*****								
*S61									
COMPUTE NM HYD	9W - 11	.00323	8.90	2.41367	1.500	4.303	PER IMP=	90.00	
*S62									
COMMAND	HYDROGRAPH ID NO. FROM TO	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	5	
ADD HYD	8W9W 66&11 12	.00753	64.19	.945	2.35137	13.317	NOTATION		
*S67									
COMPUTE NM HYD	10E - 15	.01950	48.07	1.990	1.91328	3.852	PER IMP=	60.00	
*S68									
ADD HYD	AP9E 68&81 16	.00465	38.02	.474	1.91324	12.781			
*S73									
COMPUTE NM HYD	10W - 20	.00320	8.81	.412	2.41367	4.303	PER IMP=	90.00	
*S74									
ADD HYD	AP9W 12&20 21	.01073	73.00	1.356	2.36992	10.629			
*S79									
DIVIDE HYD	AP9WSD 21 24	.00787	28.00	.995	2.36992	5.557			
	AP9WST and 25	.00286	45.00	.361	2.36992	24.605			
*S80									
DIVIDE HYD	AP9ESD 16 26	.00328	20.00	.335	1.91324	9.530			
	AP9EST and 27	.00137	18.02	.140	1.91324	20.567			
*S81									
ADD HYD	AP9EAP9W 24&26 28	.01115	48.00	1.330	2.23565	6.725			
*S83									
ADD HYD	AP9SD 19&28 29	.21982	242.50	19.960	1.70252	1.724			
*S*****	*****END AP 9*****								
FINISH									

Appendix B
Hydraulic Calculations

All Report

Label	Worksheet Type	Discharge (cfs)	Depth (ft)	Slope (ft/ft)	Mannings Coefficient	Diameter (in)	Velocity (ft/s)	Flow Type	Headwater Elevation (ft)	Crest Elevation (ft)	Centroid Elevation (ft)	Tailwater Elevation (ft)	Intercepted Flow (cfs)	Spread (ft)	Gutter Width (ft)	Gutter Cross Slope (ft/ft)	Road Cross Slope (ft/ft)
AP1E - Type A	Combinatic	17.40	0.32	0.013900	0.013		4.66						10.15	21.88	2.00	0.020000	0.015000
AP1W - Type A	Combinatic	59.92	0.56	0.013900	0.013		6.92						22.87	29.09	2.00	0.020000	0.020000
AP1W - Type C	Combinatic	36.60	0.48	0.013900	0.013		6.19						15.59	24.18	2.00	0.020000	0.020000
AP1W - Type C	Combinatic	20.90	0.38	0.013900	0.013		5.36						11.28	19.60	2.00	0.020000	0.020000
AP2W - Type A	Combinatic	43.30	0.53	0.009700	0.013		5.54						20.06	27.55	2.00	0.020000	0.020000
AP3E - Type A	Combinatic	22.30	0.38	0.009700	0.013		4.33						11.86	25.70	2.00	0.020000	0.015000
AP3W - Type A	Combinatic	45.30	0.54	0.009700	0.013		5.60						20.59	28.02	2.00	0.020000	0.020000
AP4W - Type A	Combinatic	39.00	0.37	0.055000	0.013		10.45						12.63	19.14	2.00	0.020000	0.020000
AP5E - Type A	Combinatic	17.04	0.27	0.040000	0.013		6.95						9.16	17.79	2.00	0.020000	0.015000
AP5E - Type C	Combinatic	7.20	0.20	0.040000	0.013		5.67						5.06	12.85	2.00	0.020000	0.015000
AP5W - Type A	Combinatic	39.33	0.39	0.040000	0.013		9.27						14.44	20.38	2.00	0.020000	0.020000
AP6E - Type A	Combinatic	6.25	0.20	0.022000	0.013		4.21						4.12	13.64	2.00	0.020000	0.015000
AP6W - Type A	Combinatic	32.32	0.41	0.022000	0.013		7.02						11.33	21.18	2.00	0.020000	0.020000
AP7E - Type A	Combinatic	28.07	0.45	0.005700	0.013		3.76						11.08	30.97	2.00	0.020000	0.015000
AP7W - Type A	Combinatic	54.64	0.63	0.005700	0.013		4.80						24.13	33.22	2.00	0.020000	0.020000
AP7W - Type C	Combinatic	30.10	0.36	0.040000	0.013		8.77						11.45	18.43	2.00	0.020000	0.020000
AP8E - Type C	Combinatic	15.00	0.33	0.010000	0.013		4.04						8.12	22.02	2.00	0.020000	0.015000
AP923RD - Type A	Combinatic	24.00	0.41	0.010000	0.013		4.78						13.88	21.96	2.00	0.020000	0.020000
AP9E - Type A	Combinatic	29.00	0.31	0.050000	0.013		8.69						11.39	20.84	2.00	0.020000	0.015000
AP9E - Type A	Combinatic	17.00	0.26	0.050000	0.013		7.56						8.79	17.04	2.00	0.020000	0.015000
AP9W - Type A	Combinatic	36.35	0.37	0.050000	0.013		9.89						12.86	18.97	2.00	0.020000	0.020000
AP9W - Type A	Combinatic	13.60	0.25	0.050000	0.013		7.63						8.07	13.12	2.00	0.020000	0.020000
AP9W - Type C	Combinatic	23.20	0.32	0.050000	0.013		8.93						9.52	16.03	2.00	0.020000	0.020000
AP9W - Type C	Combinatic	5.35	0.18	0.050000	0.013		6.12						4.17	9.25	2.00	0.020000	0.020000
AP9W - Type C	Combinatic	1.50	0.11	0.050000	0.013		4.36						1.49	5.74	2.00	0.020000	0.020000

Hydraflow Plan View



Project File: GCULT100mod.stm

No. Lines: 46

03-20-2006

Page 1

Line No.	Line ID	Flow rate (cfs)	Line size (in)	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line slope (%)	HGL down (ft)	HGL up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns line No.
1	Inserted Line	242.6	60 c	40.0	5193.00	5193.18	0.450	5198.00*	5198.35*	1.42	5199.77	End
2	Inserted Line	242.6	60 c	29.0	5193.28	5194.42	3.932	5199.77*	5200.02*	1.42	5201.45	1
3	Inserted Line	226.1	54 c	291.0	5194.92	5210.36	5.306	5201.45	5214.55	n/a	5214.55	2
4	Inserted Line	197.1	54 c	267.0	5210.46	5224.59	5.292	5215.50	5228.62	1.07	5228.62	3
5	Inserted Line	138.1	48 c	320.0	5225.09	5230.75	1.769	5229.42	5234.25	n/a	5234.25	4
6	Inserted Line	138.1	48 c	296.0	5230.85	5233.78	0.990	5234.85	5237.28	n/a	5237.28	5
7	Inserted Line	110.1	48 c	304.0	5233.88	5235.51	0.536	5238.27*	5240.05*	0.48	5240.53	6
8	Inserted Line	110.1	48 c	304.0	5235.61	5237.76	0.707	5240.53*	5242.32*	0.48	5242.80	7
9	Inserted Line	110.1	42 c	238.0	5238.26	5239.53	0.534	5242.80*	5245.65*	0.81	5246.46	8
10	Inserted Line	110.1	42 c	367.0	5239.63	5241.79	0.589	5246.46*	5250.86*	0.81	5251.67	9
11	Inserted Line	93.90	42 c	295.0	5241.89	5256.24	4.864	5252.23	5259.21	n/a	5259.21	10
12	Inserted Line	93.90	36 c	256.0	5256.74	5264.77	3.137	5259.74	5267.64	n/a	5267.64	11
13	Inserted Line	93.90	36 c	39.0	5264.87	5266.16	3.308	5267.87	5269.03	n/a	5269.03	12
14	Inserted Line	67.80	36 c	303.0	5266.26	5279.76	4.455	5270.43	5282.39	n/a	5282.39	13
15	Inserted Line	67.80	36 c	300.0	5279.86	5295.61	5.250	5282.86	5298.24	n/a	5298.24	14
16	Inserted Line	54.80	36 c	264.0	5295.71	5301.37	2.144	5298.96	5303.73	n/a	5303.73	15
17	Inserted Line	54.80	36 c	250.0	5301.47	5303.99	1.008	5304.47	5306.35	n/a	5306.35	16
18	Inserted Line	20.40	30 c	367.0	5304.49	5318.92	3.932	5307.39	5320.43	n/a	5320.43	17
19	Inserted Line	20.40	30 c	370.0	5319.02	5323.06	1.092	5321.52	5324.57	n/a	5324.57	18
20	Inserted Line	0.40	30 c	400.0	5323.16	5327.46	1.075	5325.66	5327.67	n/a	5327.67	19
21	Inserted Line	0.40	30 c	400.0	5327.56	5335.75	2.047	5330.06	5335.96	n/a	5335.96	20
22	Inserted Line	0.40	30 c	367.0	5335.85	5343.02	1.954	5338.35	5343.23	n/a	5343.23	21
23	Inserted Line	0.40	30 c	32.0	5343.12	5343.63	1.593	5345.62	5345.62	0.00	5345.62	22
24	Inserted Line	32.00	24 c	11.0	5343.68	5343.90	1.998	5345.68	5345.90	1.13	5347.03	23
25	Inserted Line	24.00	24 c	25.0	5344.00	5344.50	2.000	5347.74*	5348.02*	0.64	5348.65	24
26	Inserted Line	12.00	18 c	25.0	5344.60	5345.10	2.000	5348.84*	5349.17*	0.43	5349.60	25
27	Inserted Line	11.40	18 c	94.0	5343.72	5345.60	2.000	5345.62	5346.89	n/a	5346.89	23
28	Inserted Line	20.00	18 c	11.0	5326.12	5326.34	1.998	5327.62*	5328.02*	1.39	5329.41	19
29	Inserted Line	21.00	18 c	11.0	5307.05	5307.27	2.002	5308.55*	5308.99*	1.54	5310.53	17
30	Inserted Line	13.40	18 c	84.0	5306.20	5307.88	2.000	5307.70	5309.25	n/a	5309.25	17
31	Inserted Line	13.00	18 c	11.0	5297.17	5297.39	2.002	5299.05*	5299.22*	0.59	5299.81	15
32	Inserted Line	14.80	18 c	11.0	5267.72	5267.94	1.998	5270.77*	5270.99*	0.76	5271.75	13
Project File: GCULT100mod.stm							Number of lines: 46			Run Date: 03-20-2006		
NOTES: c = cir; e = ellip; b = box; Return period = 100 Yrs. ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump.												

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[illegible]

Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream								Len (ft)	Upstream								Check		JL coeff (K)	Minor loss (ft)
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Energy loss (ft)		
1	60	245.6	5193.00	5198.00	5.00	19.63	12.51	2.43	5200.43	0.889	40.0	5193.18	5198.36	5.00	19.63	12.51	2.43	5200.79	0.889	0.889	0.356	0.60	1.46
2	60	245.6	5193.28	5199.82	5.00	19.63	12.51	2.43	5202.25	0.889	29.0	5194.42	5200.08	5.00	19.63	12.51	2.43	5202.51	0.889	0.889	0.258	0.60	1.46
3	54	227.1	5194.92	5201.53	4.50	15.44	14.28	3.17	5204.71	1.334	291	5210.36	5214.56	4.20**	15.44	14.71	3.36	5217.92	1.153	1.244	n/a	0.40	1.35
4	54	197.1	5210.46	5215.53	4.50	15.01	12.40	2.39	5217.92	1.005	267	5224.59	5228.62	4.03**	15.01	13.13	2.68	5231.30	0.889	0.947	n/a	0.40	1.07
5	48	138.1	5225.09	5229.42	4.00	11.66	10.99	1.88	5231.30	0.925	320	5230.75	5234.25	3.50**	11.66	11.84	2.18	5236.43	0.837	0.881	n/a	0.40	n/a
6	48	138.1	5230.85	5234.85	4.00*	11.66	10.99	1.88	5236.73	0.925	296	5233.78	5237.28	3.50**	11.66	11.84	2.18	5239.46	0.837	0.881	n/a	0.40	n/a
7	48	110.1	5233.88	5238.27	4.00	12.56	8.76	1.19	5239.46	0.588	304	5235.51	5240.05	4.00	12.57	8.76	1.19	5241.25	0.587	0.588	1.786	0.40	0.48
8	48	110.1	5235.61	5240.53	4.00	12.56	8.76	1.19	5241.73	0.588	304	5237.76	5242.32	4.00	12.57	8.76	1.19	5243.51	0.587	0.588	1.786	0.40	0.48
9	42	110.1	5238.26	5242.80	3.50	9.62	11.45	2.04	5244.83	1.198	238	5239.53	5245.65	3.50	9.62	11.44	2.04	5247.68	1.198	1.198	2.851	0.40	0.81
10	42	110.1	5239.63	5246.46	3.50	9.62	11.45	2.04	5248.50	1.198	367	5241.79	5250.86	3.50	9.62	11.44	2.04	5252.90	1.198	1.198	4.396	0.40	0.81
11	42	93.90	5241.89	5252.23	3.50	9.62	9.76	1.48	5253.71	0.871	295	5256.24	5259.21	2.97**	8.70	10.80	1.81	5261.02	0.824	0.847	n/a	0.40	n/a
12	36	93.90	5256.74	5259.74	3.00*	6.96	13.29	2.74	5262.49	1.983	256	5264.77	5267.64	2.87**	6.96	13.48	2.83	5270.47	1.723	1.853	n/a	0.40	n/a
13	36	93.90	5264.87	5267.87	3.00*	6.96	13.29	2.74	5270.62	1.983	39.0	5266.16	5269.03	2.87**	6.96	13.48	2.83	5271.86	1.723	1.853	n/a	0.40	n/a
14	36	67.80	5266.26	5270.43	3.00	6.57	9.59	1.43	5271.86	1.034	303	5279.76	5282.39	2.63**	6.57	10.32	1.66	5284.05	0.933	0.984	n/a	0.40	n/a
15	36	67.80	5279.86	5282.86	3.00*	6.57	9.59	1.43	5284.29	1.034	300	5295.61	5298.24	2.63**	6.57	10.32	1.66	5299.90	0.933	0.984	n/a	0.40	n/a
16	36	54.80	5295.71	5298.96	3.00	7.07	7.75	0.93	5299.90	0.675	264	5301.37	5303.73	2.36**	5.96	9.19	1.31	5305.04	0.731	0.703	n/a	0.40	n/a
17	36	54.80	5301.47	5304.47	3.00*	7.07	7.75	0.93	5305.41	0.675	250	5303.99	5306.35	2.36**	5.96	9.19	1.31	5307.66	0.731	0.703	n/a	0.40	n/a
18	30	20.40	5304.49	5307.39	2.50	4.91	4.16	0.27	5307.66	0.248	367	5318.92	5320.43	1.51**	3.10	6.58	0.67	5321.10	0.538	0.393	n/a	0.40	0.27
19	30	20.40	5319.02	5321.52	2.50*	4.91	4.16	0.27	5321.79	0.248	370	5323.06	5324.57	1.51**	3.10	6.58	0.67	5325.24	0.538	0.393	n/a	0.40	0.27
20	30	0.40	5323.16	5325.66	2.50*	4.91	0.08	0.00	5325.66	0.000	400	5327.46	5327.67	0.21**	0.20	2.00	0.06	5327.73	0.443	0.222	n/a	0.40	0.02
21	30	0.40	5327.56	5330.06	2.50*	4.91	0.08	0.00	5330.06	0.000	400	5335.75	5335.96	0.21**	0.20	2.00	0.06	5336.02	0.443	0.222	n/a	0.40	0.02

Project File: GCMODULT100.stm

Number of lines: 23

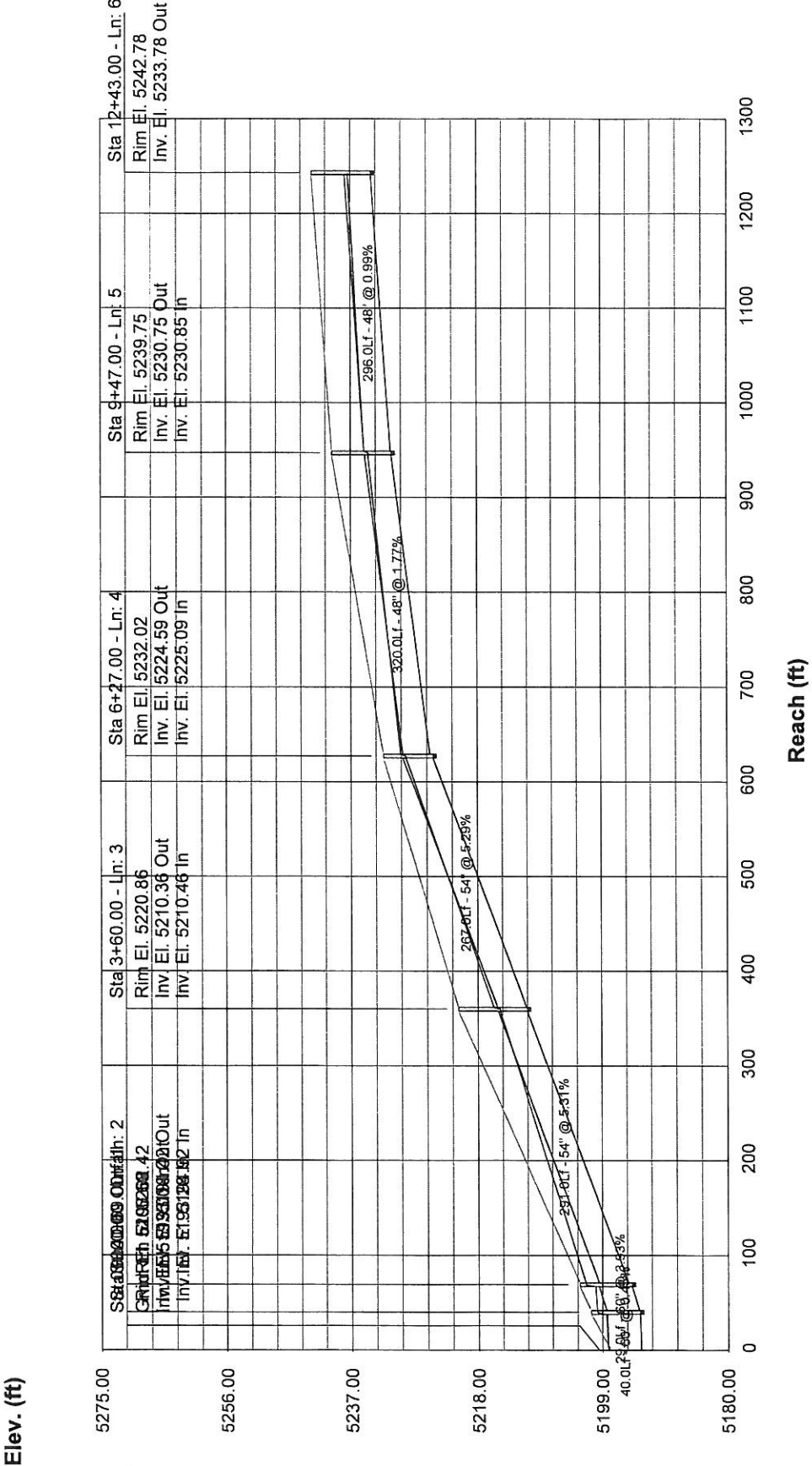
Run Date: 03-20-2006

Notes: * Crown depth assumed.; ** Critical depth.; j-Line contains hyd. jump.

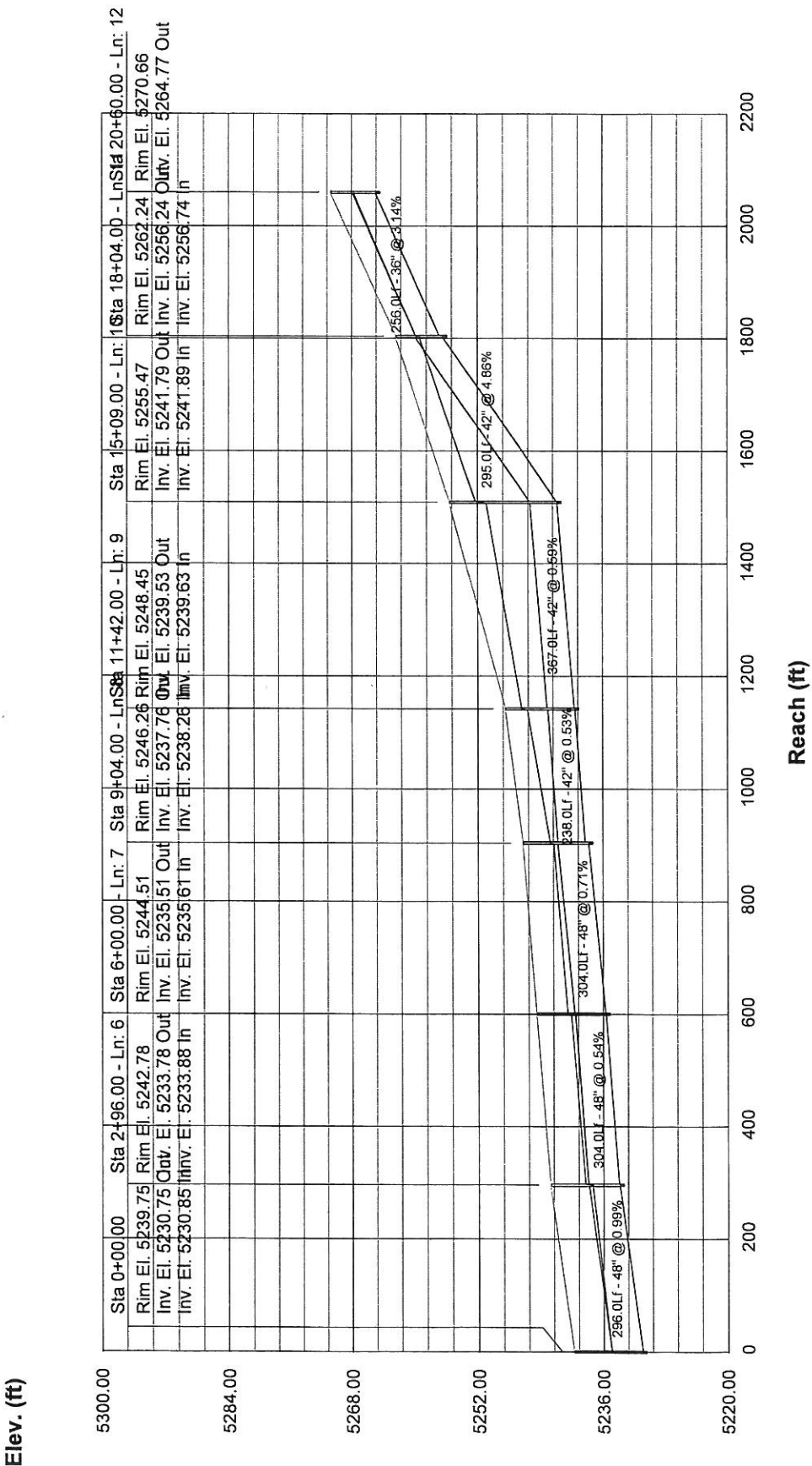
Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream								Len (ft)	Upstream								Check		JL coeff (K)	Minor loss (ft)	
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy loss (ft)			
22	30	0.40	5335.85	5338.35	2.50*	4.91	0.08	0.00	5338.35	0.000	367	5343.02	5343.23	0.21**	0.20	2.00	0.06	5343.29	0.443	0.222	n/a	0.40	0.02	
23	30	0.40	5343.12	5345.62	2.50*	4.91	0.08	0.00	5345.62	0.000	32.0	5343.63	5345.62	1.99	4.19	0.10	0.00	5345.62	0.000	0.000	0.000	0.40	0.00	
Project File: GCMODULT100.stm												Number of lines: 23								Run Date: 03-20-2006				
Notes: * Crown depth assumed.; ** Critical depth.; j-Line contains hyd. jump.																								

Storm Sewer Profile

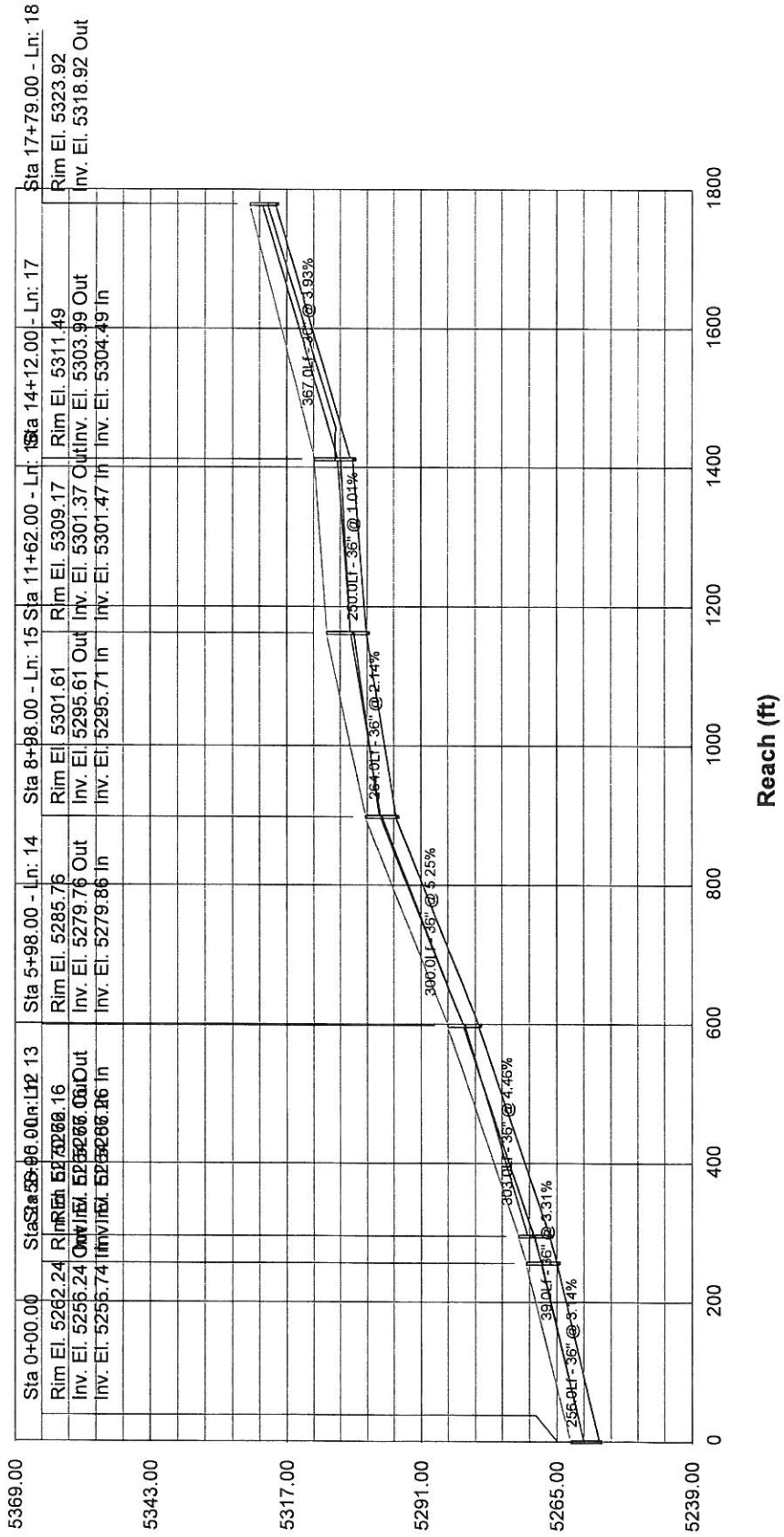


Storm Sewer Profile



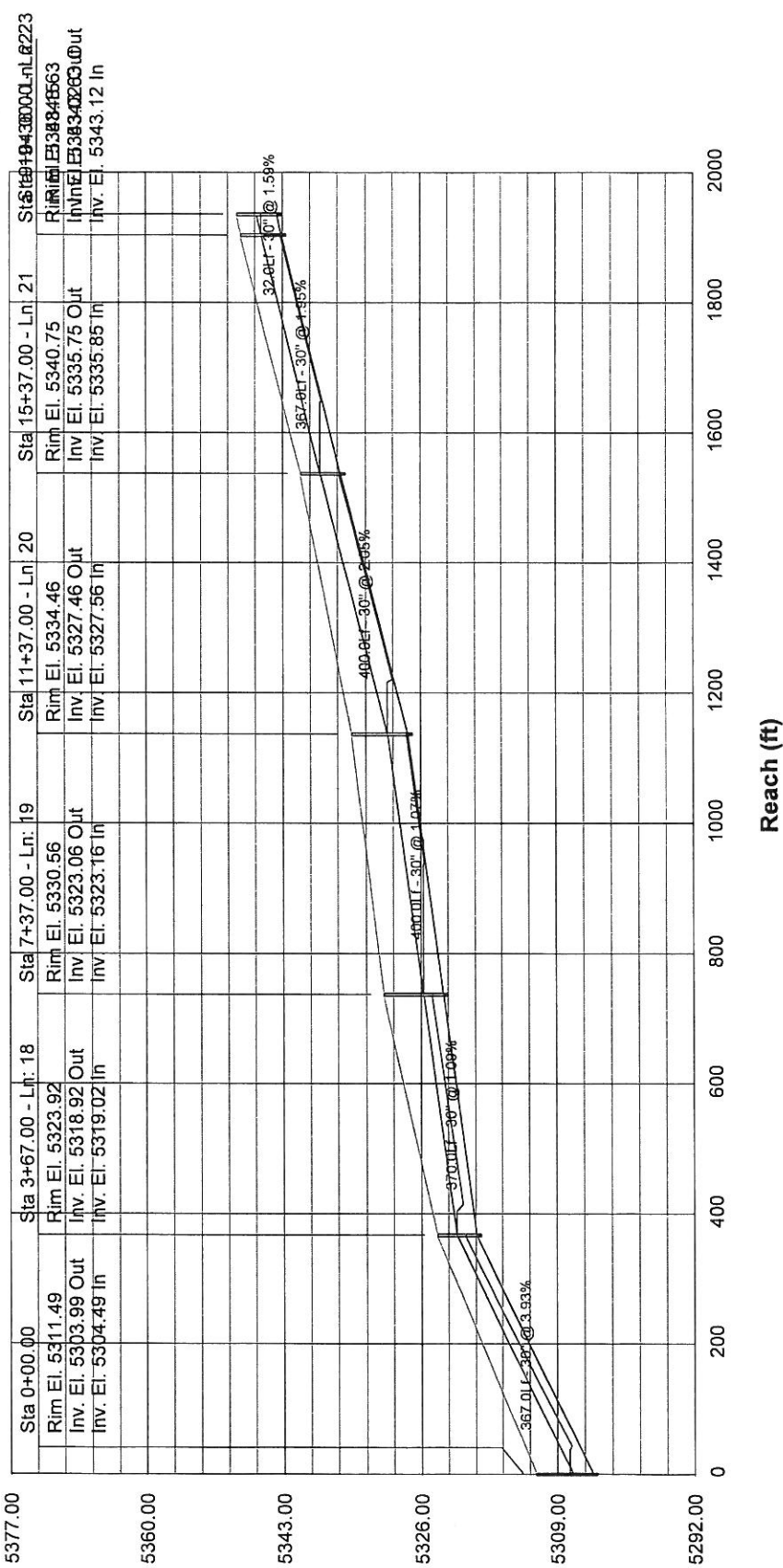
Storm Sewer Profile

Elev. (ft)

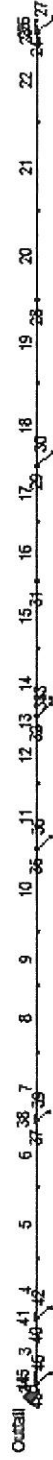


Storm Sewer Profile

Elev. (ft)



Hydraflow Plan View



Project File: GC100ULT.stm

No. Lines: 46

03-20-2006

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Line No.	Line ID	Flow rate (cfs)	Line size (in)	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line slope (%)	HGL down (ft)	HGL up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns line No.
1	Inserted Line	262.0	60 c	40.0	5193.00	5193.18	0.450	5198.00*	5198.41*	1.66	5200.07	End
2	Inserted Line	262.0	60 c	29.0	5193.28	5194.42	3.932	5200.07*	5200.36*	1.66	5202.02	1
3	Inserted Line	241.5	54 c	291.0	5194.92	5210.36	5.306	5202.02	5214.61	n/a	5214.61	2
4	Inserted Line	211.5	54 c	267.0	5210.46	5224.59	5.292	5215.61	5228.70	1.20	5228.70	3
5	Inserted Line	152.5	48 c	320.0	5225.09	5230.75	1.769	5229.41	5234.37	1.01	5234.37	4
6	Inserted Line	152.5	48 c	296.0	5230.85	5233.78	0.990	5234.85*	5238.19*	0.92	5239.10	5
7	Inserted Line	106.5	48 c	304.0	5233.88	5235.51	0.536	5240.28*	5241.95*	0.45	5242.40	6
8	Inserted Line	106.5	48 c	304.0	5235.61	5237.76	0.707	5242.40*	5244.07*	0.45	5244.51	7
9	Inserted Line	106.5	42 c	238.0	5238.26	5239.53	0.534	5244.51*	5247.18*	0.76	5247.94	8
10	Inserted Line	106.5	42 c	367.0	5239.63	5241.79	0.589	5247.94*	5252.06*	0.76	5252.82	9
11	Inserted Line	91.50	42 c	295.0	5241.89	5256.24	4.864	5253.32	5259.17	0.70	5259.17	10
12	Inserted Line	91.50	36 c	256.0	5256.74	5264.77	3.137	5259.74	5267.63	1.08	5267.63	11
13	Inserted Line	91.50	36 c	39.0	5264.87	5266.16	3.308	5267.87	5269.02	1.08	5269.02	12
14	Inserted Line	63.50	36 c	303.0	5266.26	5279.76	4.455	5270.46	5282.30	0.62	5282.30	13
15	Inserted Line	63.50	36 c	300.0	5279.86	5295.61	5.250	5282.86	5298.15	0.62	5298.15	14
16	Inserted Line	51.50	36 c	264.0	5295.71	5301.37	2.144	5298.86	5303.66	0.49	5303.66	15
17	Inserted Line	51.50	36 c	250.0	5301.47	5303.99	1.008	5304.47	5306.28	0.49	5306.28	16
18	Inserted Line	20.50	30 c	367.0	5304.49	5318.92	3.932	5307.24	5320.43	n/a	5320.43	17
19	Inserted Line	20.50	30 c	370.0	5319.02	5323.06	1.092	5321.52	5324.57	n/a	5324.57	18
20	Inserted Line	0.50	30 c	400.0	5323.16	5327.46	1.075	5325.66	5327.70	n/a	5327.70	19
21	Inserted Line	0.50	30 c	400.0	5327.56	5335.75	2.047	5330.06	5335.99	n/a	5335.99	20
22	Inserted Line	0.50	30 c	367.0	5335.85	5343.02	1.954	5338.35	5343.26	n/a	5343.26	21
23	Inserted Line	0.50	30 c	32.0	5343.12	5343.63	1.593	5345.62	5345.62	0.00	5345.62	22
24	Inserted Line	48.00	24 c	11.0	5343.68	5343.90	1.998	5345.68*	5346.18*	2.54	5348.72	23
25	Inserted Line	37.00	24 c	25.0	5344.00	5344.50	2.000	5350.19*	5350.86*	1.51	5352.37	24
26	Inserted Line	22.00	18 c	25.0	5344.60	5345.10	2.000	5352.37*	5353.47*	1.45	5354.91	25
27	Inserted Line	10.00	18 c	94.0	5343.72	5345.60	2.000	5345.62	5346.81	n/a	5346.81	23
28	Inserted Line	20.00	18 c	11.0	5326.12	5326.34	1.998	5327.62*	5328.02*	1.39	5329.41	19
29	Inserted Line	20.00	18 c	11.0	5307.05	5307.27	2.002	5308.55*	5308.95*	1.39	5310.34	17
30	Inserted Line	11.00	18 c	84.0	5306.20	5307.88	2.000	5307.70	5309.15	n/a	5309.15	17
31	Inserted Line	12.00	18 c	11.0	5297.17	5297.39	2.002	5298.97*	5299.12*	0.50	5299.62	15
32	Inserted Line	14.00	18 c	11.0	5267.72	5267.94	1.998	5270.74*	5270.94*	0.68	5271.62	13
Project File: GC100ULT.stm							Number of lines: 46			Run Date: 03-20-2006		
NOTES: c = cir; e = ellip; b = box; Return period = 100 Yrs. ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump.												

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NOTES: c = cir; e = ellip; b = box; Return period = 100 Yrs. ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump.

Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream								Len (ft)	Upstream								Check		JL coeff (K)	Minor loss (ft)
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Energy loss (ft)		
1	60	262.0	5193.00	5198.00	5.00	19.63	13.35	2.77	5200.77	1.012	40.0	5193.18	5198.41	5.00	19.63	13.34	2.77	5201.17	1.012	1.012	0.405	0.60	1.66
2	60	262.0	5193.28	5200.07	5.00	19.63	13.35	2.77	5202.84	1.012	29.0	5194.42	5200.36	5.00	19.63	13.34	2.77	5203.13	1.012	1.012	0.293	0.60	1.66
3	54	241.5	5194.92	5202.02	4.50	15.57	15.19	3.59	5205.61	1.509	291	5210.36	5214.61	4.25**	15.57	15.51	3.74	5218.36	1.304	1.406	n/a	0.40	n/a
4	54	211.5	5210.46	5215.61	4.50	15.24	13.30	2.75	5218.36	1.157	267	5224.59	5228.70	4.11**	15.24	13.88	3.00	5231.70	1.008	1.082	n/a	0.40	1.20
5	48	152.5	5225.09	5229.41	4.00	11.96	12.14	2.29	5231.70	1.128	320	5230.75	5234.37	3.62**	11.96	12.75	2.53	5236.90	0.988	1.058	n/a	0.40	1.01
6	48	152.5	5230.85	5234.85	4.00*	12.56	12.14	2.29	5237.14	1.128	296	5233.78	5238.19	4.00	12.57	12.14	2.29	5240.48	1.127	1.127	3.337	0.40	0.92
7	48	106.5	5233.88	5240.28	4.00	12.56	8.48	1.12	5241.39	0.550	304	5235.51	5241.95	4.00	12.57	8.48	1.12	5243.07	0.550	0.550	1.671	0.40	0.45
8	48	106.5	5235.61	5242.40	4.00	12.56	8.48	1.12	5243.51	0.550	304	5237.76	5244.07	4.00	12.57	8.48	1.12	5245.18	0.550	0.550	1.671	0.40	0.45
9	42	106.5	5238.26	5244.51	3.50	9.62	11.07	1.91	5246.42	1.121	238	5239.53	5247.18	3.50	9.62	11.07	1.91	5249.09	1.121	1.121	2.668	0.40	0.76
10	42	106.5	5239.63	5247.94	3.50	9.62	11.07	1.91	5249.85	1.121	367	5241.79	5252.06	3.50	9.62	11.07	1.91	5253.96	1.121	1.121	4.113	0.40	0.76
11	42	91.50	5241.89	5253.32	3.50	9.62	9.51	1.41	5254.73	0.827	295	5256.24	5259.17	2.93**	8.60	10.64	1.76	5260.93	0.798	0.813	n/a	0.40	0.70
12	36	91.50	5256.74	5259.74	3.00*	6.95	12.95	2.61	5262.35	1.883	256	5264.77	5267.63	2.86**	6.95	13.17	2.70	5270.33	1.632	1.758	n/a	0.40	1.08
13	36	91.50	5264.87	5267.87	3.00*	6.95	12.95	2.61	5270.48	1.883	39.0	5266.16	5269.02	2.86**	6.95	13.17	2.70	5271.72	1.632	1.758	n/a	0.40	1.08
14	36	63.50	5266.26	5270.46	3.00	7.07	8.99	1.26	5271.72	0.907	303	5279.76	5282.30	2.54**	6.38	9.95	1.54	5283.84	0.859	0.883	n/a	0.40	0.62
15	36	63.50	5279.86	5282.86	3.00*	7.07	8.99	1.26	5284.12	0.907	300	5295.61	5298.15	2.54**	6.38	9.95	1.54	5299.69	0.859	0.883	n/a	0.40	0.62
16	36	51.50	5295.71	5298.86	3.00	7.07	7.29	0.83	5299.69	0.597	264	5301.37	5303.66	2.29**	5.78	8.91	1.23	5304.89	0.691	0.644	n/a	0.40	0.49
17	36	51.50	5301.47	5304.47	3.00*	7.07	7.29	0.83	5305.30	0.597	250	5303.99	5306.28	2.29**	5.78	8.91	1.23	5307.51	0.691	0.644	n/a	0.40	0.49
18	30	20.50	5304.49	5307.24	2.50	4.91	4.18	0.27	5307.51	0.250	367	5318.92	5320.43	1.51**	3.11	6.60	0.68	5321.11	0.539	0.394	n/a	0.40	n/a
19	30	20.50	5319.02	5321.52	2.50*	4.91	4.18	0.27	5321.79	0.250	370	5323.06	5324.57	1.51**	3.11	6.60	0.68	5325.25	0.539	0.394	n/a	0.40	n/a
20	30	0.50	5323.16	5325.66	2.50*	4.91	0.10	0.00	5325.66	0.000	400	5327.46	5327.70	0.24**	0.24	2.13	0.07	5327.77	0.432	0.216	n/a	0.40	0.03
21	30	0.50	5327.56	5330.06	2.50*	4.91	0.10	0.00	5330.06	0.000	400	5335.75	5335.99	0.24**	0.24	2.13	0.07	5336.06	0.432	0.216	n/a	0.40	0.03

Project File: GC100ULT.stm

Number of lines: 46

Run Date: 03-20-2006

Notes: * Crown depth assumed.; ** Critical depth.; j-Line contains hyd. jump.

Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream								Len (ft)	Upstream								Check		JL coeff (K)	Minor loss (ft)
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Energy loss (ft)		
22	30	0.50	5335.85	5338.35	2.50*	4.91	0.10	0.00	5338.35	0.000	367	5343.02	5343.26	0.24**	0.24	2.13	0.07	5343.33	0.432	0.216	n/a	0.40	0.03
23	30	0.50	5343.12	5345.62	2.50*	4.91	0.10	0.00	5345.62	0.000	32.0	5343.63	5345.62	1.99	4.19	0.12	0.00	5345.62	0.000	0.000	0.000	0.40	0.00
24	24	48.00	5343.68	5345.68	2.00*	3.14	15.28	3.63	5349.31	4.506	11.0	5343.90	5346.18	2.00	3.14	15.28	3.63	5349.81	4.504	4.505	0.496	0.70	2.54
25	24	37.00	5344.00	5350.19	2.00	3.14	11.78	2.16	5352.35	2.677	25.0	5344.50	5350.86	2.00	3.14	11.78	2.16	5353.02	2.676	2.677	0.669	0.70	1.51
26	18	22.00	5344.60	5352.37	1.50	1.77	12.45	2.41	5354.78	4.391	25.0	5345.10	5353.47	1.50	1.77	12.45	2.41	5355.88	4.389	4.390	1.098	0.60	1.45
27	18	10.00	5343.72	5345.62	1.50	1.77	5.66	0.50	5346.12	0.907	94.0	5345.60	5346.81	1.21**	1.52	6.56	0.67	5347.48	0.938	0.923	n/a	0.60	0.40
28	18	20.00	5326.12	5327.62	1.50*	1.77	11.32	1.99	5329.61	3.629	11.0	5326.34	5328.02	1.50	1.77	11.32	1.99	5330.01	3.627	3.628	0.399	0.70	1.39
29	18	20.00	5307.05	5308.55	1.50*	1.77	11.32	1.99	5310.54	3.629	11.0	5307.27	5308.95	1.50	1.77	11.32	1.99	5310.94	3.627	3.628	0.399	0.70	1.39
30	18	11.00	5306.20	5307.70	1.50*	1.77	6.23	0.60	5308.30	1.098	84.0	5307.88	5309.15	1.27**	1.59	6.91	0.74	5309.89	1.045	1.071	n/a	0.60	0.45
31	18	12.00	5297.17	5298.97	1.50	1.77	6.79	0.72	5299.69	1.306	11.0	5297.39	5299.12	1.50	1.77	6.79	0.72	5299.83	1.306	1.306	0.144	0.70	0.50
32	18	14.00	5267.72	5270.74	1.50	1.77	7.92	0.98	5271.72	1.778	11.0	5267.94	5270.94	1.50	1.77	7.92	0.98	5271.91	1.777	1.778	0.196	0.70	0.68
33	18	14.00	5267.84	5270.74	1.50	1.77	7.92	0.98	5271.72	1.778	82.0	5269.48	5272.20	1.50	1.77	7.92	0.98	5273.17	1.777	1.778	1.458	0.60	0.59
34	18	5.00	5269.58	5273.63	1.50	1.77	2.83	0.12	5273.76	0.227	25.0	5270.97	5273.69	1.50	1.77	2.83	0.12	5273.82	0.227	0.227	0.057	0.60	0.07
35	18	11.00	5251.03	5254.12	1.50	1.77	6.23	0.60	5254.73	1.098	11.0	5251.25	5254.24	1.50	1.77	6.22	0.60	5254.85	1.097	1.098	0.121	0.70	0.42
36	18	4.00	5250.20	5254.65	1.50	1.77	2.26	0.08	5254.73	0.145	75.0	5251.70	5254.76	1.50	1.77	2.26	0.08	5254.83	0.145	0.145	0.109	0.60	0.05
37	18	35.00	5237.88	5239.38	1.50*	1.77	19.81	6.10	5245.48	11.113	11.0	5238.10	5240.60	1.50**	1.77	19.81	6.10	5246.70	11.109	11.111	1.222	0.70	4.27
38	18	24.00	5238.20	5248.10	1.50	1.77	13.58	2.87	5250.97	5.226	25.0	5238.70	5249.41	1.50	1.77	13.58	2.87	5252.28	5.224	5.225	1.306	0.70	2.01
39	18	11.00	5237.61	5240.79	1.50	1.77	6.23	0.60	5241.39	1.098	61.0	5238.83	5241.46	1.50	1.77	6.22	0.60	5242.06	1.097	1.098	0.669	0.60	0.36
40	18	20.00	5216.32	5217.82	1.50*	1.77	11.32	1.99	5219.81	3.629	11.0	5216.54	5218.22	1.50	1.77	11.32	1.99	5220.21	3.627	3.628	0.399	0.70	1.39
41	18	12.00	5216.64	5220.89	1.50	1.77	6.79	0.72	5221.61	1.306	25.0	5217.24	5221.21	1.50	1.77	6.79	0.72	5221.93	1.306	1.306	0.327	0.70	0.50
42	18	11.00	5216.61	5218.11	1.50*	1.77	6.23	0.60	5218.71	1.098	70.0	5218.01	5219.28	1.27**	1.59	6.91	0.74	5220.02	1.045	1.071	n/a	0.60	0.45

Project File: GC100ULT.stm

Number of lines: 46

Run Date: 03-20-2006

Notes: * Crown depth assumed.; ** Critical depth.; j-Line contains hyd. jump.

Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream								Len (ft)	Upstream								Check		JL coeff (K)	Minor loss (ft)
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy loss (ft)		
43	24	14.50	5197.88	5204.46	2.00	3.14	4.62	0.33	5204.79	0.411	11.0	5198.00	5204.50	2.00	3.14	4.62	0.33	5204.84	0.411	0.411	0.045	0.70	0.23
44	24	13.00	5198.10	5204.80	2.00	3.14	4.14	0.27	5205.07	0.331	25.0	5199.79	5204.88	2.00	3.14	4.14	0.27	5205.15	0.330	0.330	0.083	0.70	0.19
45	18	9.00	5199.89	5205.07	1.50	1.77	5.09	0.40	5205.47	0.735	25.0	5201.38	5205.25	1.50	1.77	5.09	0.40	5205.66	0.735	0.735	0.184	0.60	0.24
46	18	8.00	5197.44	5204.47	1.50	1.77	4.53	0.32	5204.79	0.581	73.0	5199.84	5204.90	1.50	1.77	4.53	0.32	5205.21	0.580	0.581	0.424	0.60	0.19

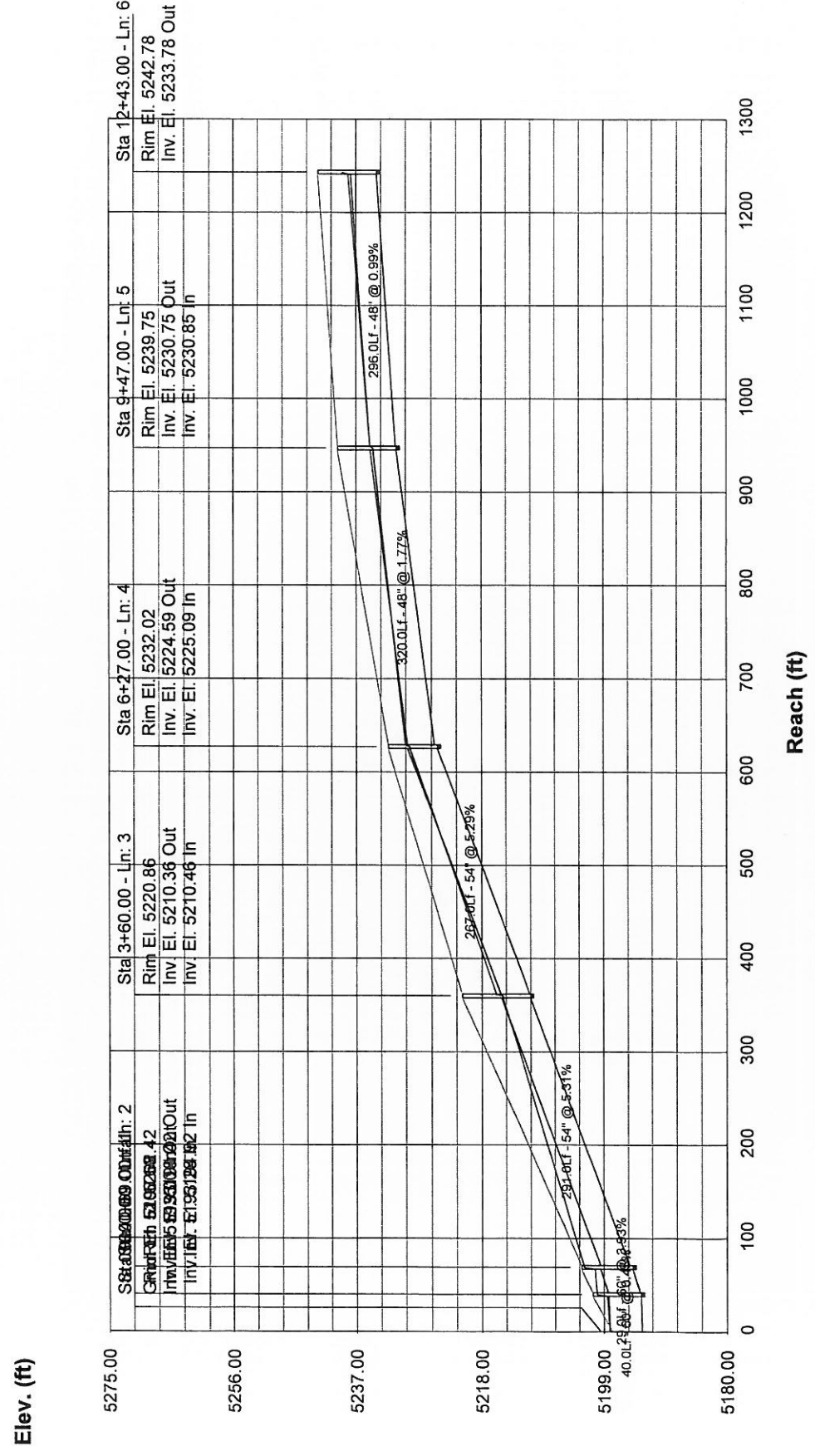
Project File: GC100ULT.stm

Number of lines: 46

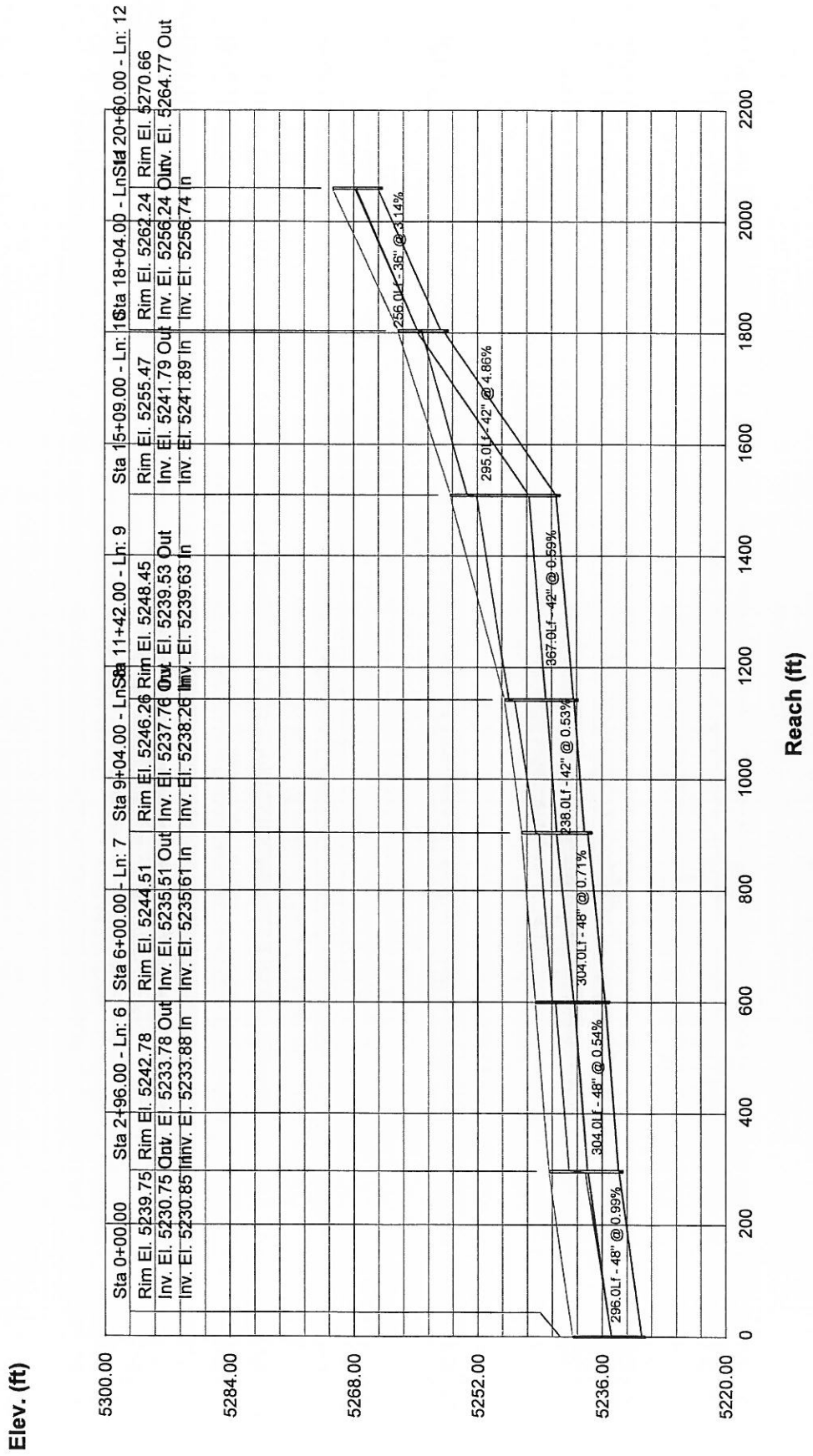
Run Date: 03-20-2006

Notes: * Crown depth assumed.; ** Critical depth.; j-Line contains hyd. jump.

Storm Sewer Profile

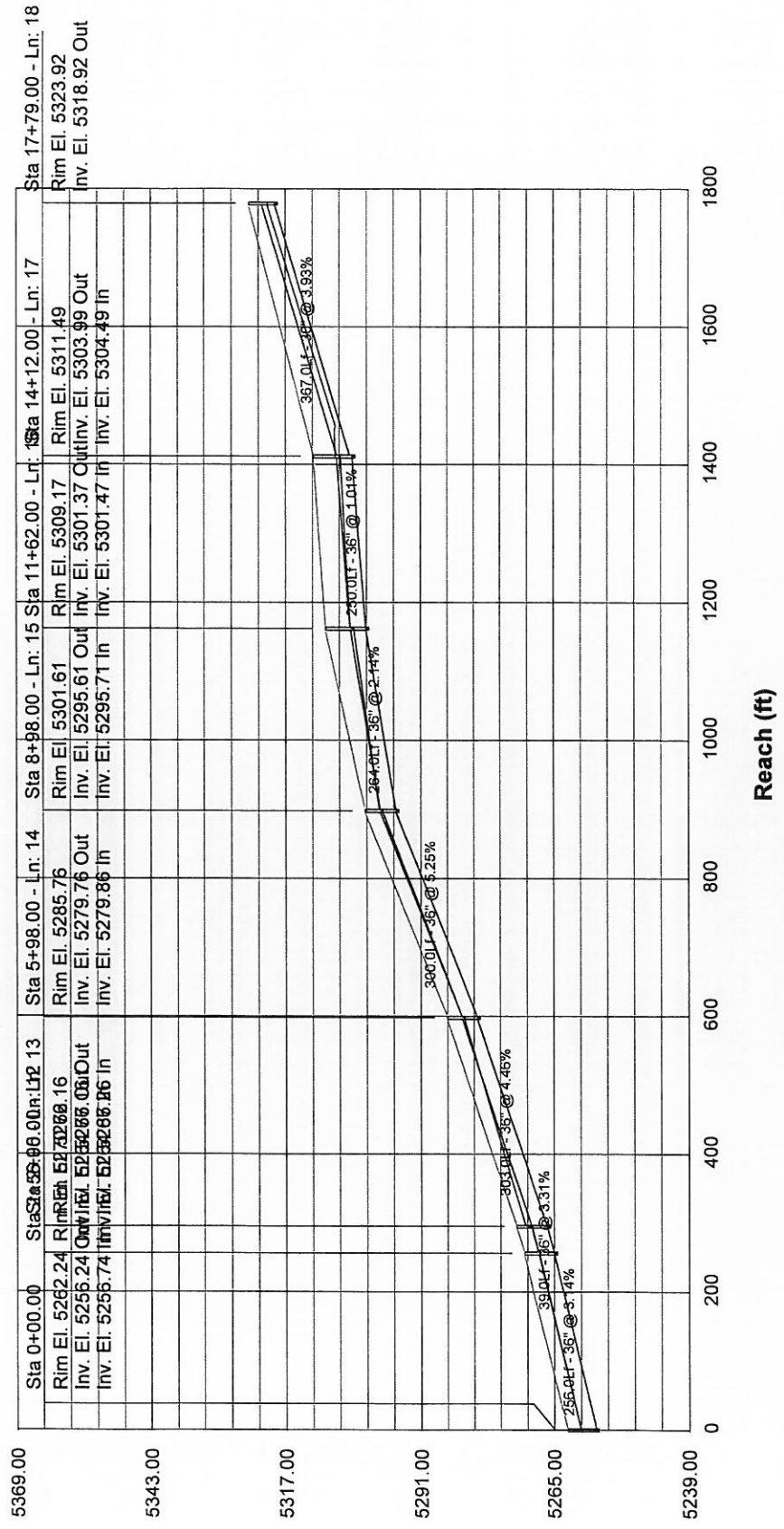


Storm Sewer Profile



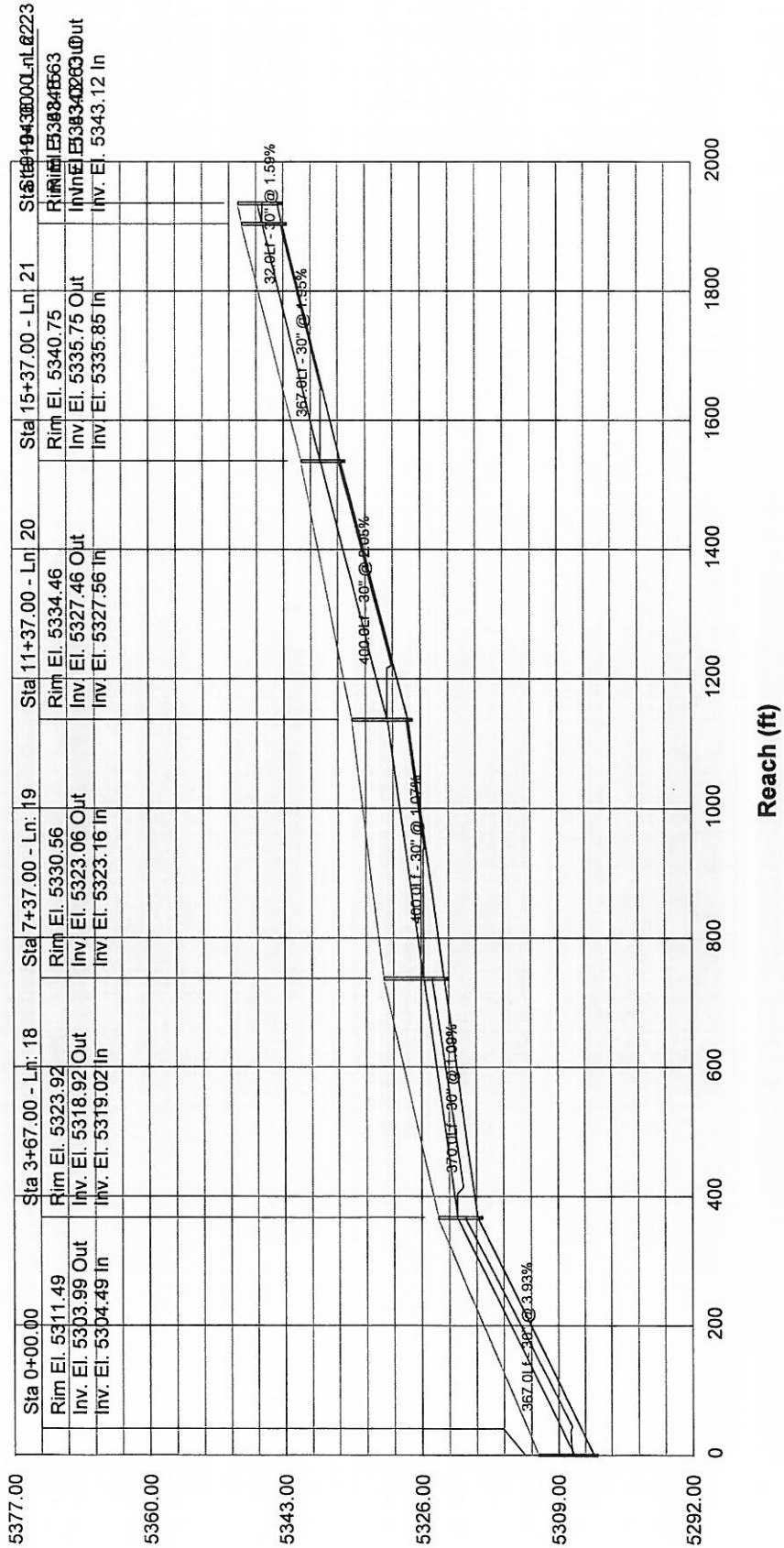
Storm Sewer Profile

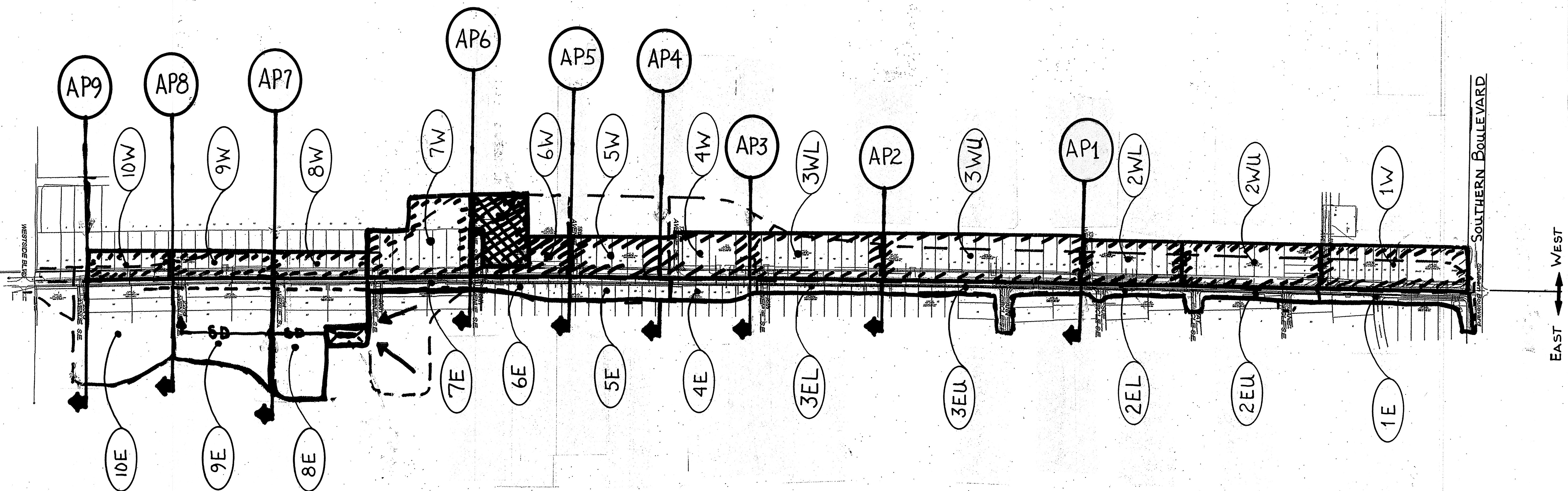
Elev. (ft)



Storm Sewer Profile

Elev. (ft)





Analysis Point	Pipe Flow Ultimate	Street Flow East	Street Flow West	Pipe Flow Modified	Street Flow East	Street Flow West
AP1	43	6.4	28	58	8.4	10.9
AP2	20	15.6	41.8	24.9	17.6	25
AP3	52	10.3	43.9	50.9	4.9	27
AP4	64.5	13.6	46.4	63.4	8.4	29.5
AP5	90.5	6.44	45.3	90.4	0	28.4
AP6	105.5	6.7	42.3	105.2	1	24.4
AP7	135.8	22	55.3	150.08	14.3	25.4
AP8	196.4	54	64.3	206.91	46.6	34.4
AP9	242.5	18	45	255.41	0	5.2

1" = 300'

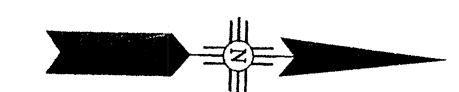
CITY OF RIO RANCHO
PUBLIC WORKS DEPARTMENT

GOLF COURSE RD.
DRAINAGE REPORT
BASIN MAP

N.M. Project No.

Sheet

PLATE 1



GOLF COURSE ROAD
Scale: 1"=300'

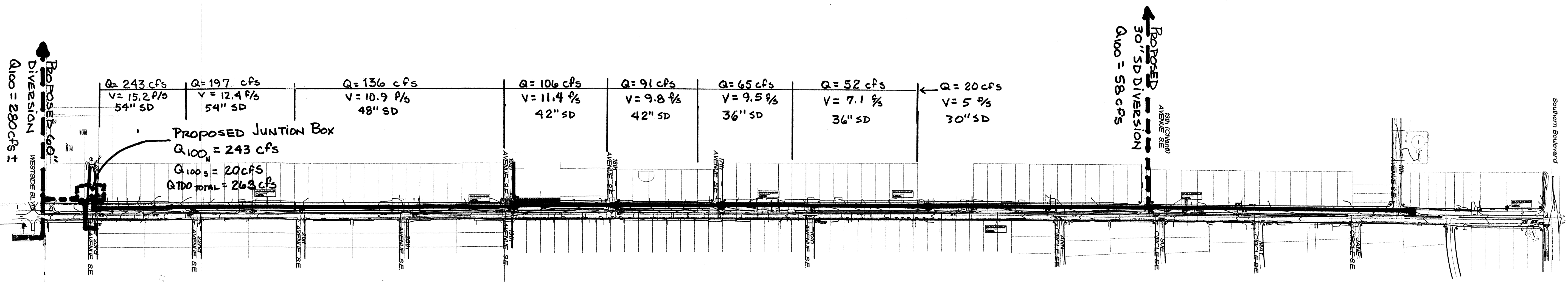


PLATE 3

CITY OF RIO RANCHO
PUBLIC WORKS DEPARTMENT

GOLF COURSE RD.
DRAINAGE REPORT
SYSTEM MAP
Plate 3

N.M. Project No.

Sheet

PLATE 3