

FINAL DRAINAGE STUDY

YUCATAN DEL ESTE AT CABEZON TRACT 6A

*Rio Rancho Estates Unit 16
Rio Rancho, New Mexico*

for

**CURB NORTH, INC
5160 SAN FRANCISCO NE
ALBUQUERQUE, NEW MEXICO 87109**

February 7, 2006



Prepared By:

**HUITT-ZOLLARS, Inc.
333 RIO RANCHO DRIVE NE, SUITE 101, RIO RANCHO, NEW MEXICO
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**FINAL
DRAINAGE STUDY**

**YUCATAN DEL ESTE
AT CABEZON TRACT 6A**



I, Jarrod D. Likar being first duly sworn, upon my oath state that I am a registered professional engineer, qualified in Civil engineering, and that the accompanying report was prepared by me or under my supervision and is true and correct to the best of my knowledge and belief.

Jarrod D. Likar 2/7/06

Registered Professional Engineer

**DRAINAGE STUDY
FOR
YUCATAN DEL ESTE TRACT 6A SUBDIVISION**

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DRAINAGE STUDY FOR YUCATAN DEL ESTE AT CABEZON TRACT 6A

PURPOSE

This drainage report addresses the storm water runoff and proposed infrastructure needed to convey the runoff from the Yucatan Del Este at Cabezon Tract 6A Subdivision of the Cabezon Redevelopment. This report will also demonstrate that the development of this project complies with the approved **Cabezon Communities Phase II Drainage Management Plan** and the **Cabezon Communities Drainage Implementation Plan**.

PROJECT LOCATION AND DESCRIPTION



Exhibit 1 – Vicinity Map

The project is located at the northwest corner of the intersection of Chianti Road (13th Avenue) and Golf Course Road within Unit 16 of Rio Rancho Estates, City of Rio Rancho; see **Exhibit 1**. The site is currently undeveloped and in its natural condition. The east branch of the Blacks Arroyo is currently being hard lined to the west of the development. Southern Boulevard is paved to the north of the development. The development is bound by; Chianti Road to the south and Golf Course Road to the east, where it is separated by existing ½ acre lots.

ZONING AND PLATTING STATUS

The zoning for this project is R-4, Single Family Residential, of approximately 57.3 acres. The project is located in Tract 6A within Rio Rancho Estates Unit 16. This report is an attachment to the Final Plat Submittal for this project.

FLOOD HAZARD ZONES

Per FEMA's Flood Insurance Rate Map (FIRM) 35043C0894 C, dated July 16, 1996, a portion of the project site is located within a FEMA 100-year Flood Hazard Zone. See **Appendix A-1**. Wilson & Co. is under contract with the developer for the corresponding CLOMR and LOMR needed to reconfigure the existing flood zone. The CLOMR has been submitted to FEMA by Wilson & Co. per discussions with the City of Rio Rancho, the developer has agreed to restrict building permit requests for the lots that are located within the current FEMA Floodplain. Once the CLOMR/LOMR process has revised the Floodplain, the developer can proceed with building permits for the affected lots. Refer to **Appendix A-2** for an exhibit indicating the affected lots.

JURISDICTIONS OF PUBLIC AGENCIES

Local

This project is located entirely within the City of Rio Rancho (CoRR) Municipal Limits and is therefore within their jurisdiction and must comply with the City's development requirements.

Regional

This project is located within the jurisdiction of the Southern Sandoval County Arroyo Flood Control Authority (SSCAFCA) and is therefore subject to their review.

RELATED REPORTS

The ***Cabazon Communities Phase II Drainage Management Plan (CCDMP)*** prepared by Wilson & Company, Engineers & Architects and dated August 2004, provides an overall master plan for this area. This report has been approved by the City and SSSCAFCA. It determined the pre-developed drainage patterns of this development and the design parameters for the buildout of the subdivision. However, that study only gave a conceptual design for the Tract 6A Subdivision.

The ***Cabazon Communities Drainage Implementation Plan (CCDIP)*** prepared by Wilson & Company, Engineers & Architects and dated February 19, 2004, provides permissible discharge rates for individual tracts as well as offsite flow rates entering individual tracts.

METHODOLOGY

This drainage study is based on the procedures outlined in the CoRR's "Grading and Drainage Design Requirements and Policies for Land Development in Rio Rancho (Revised 3-18-93)." That policy states, "The minimum criteria for hydrology and hydraulic calculations and design shall be as described in the Development Process Manual Section 22.2, City of Albuquerque (CoA DPM), latest revision, or the AHYMO version of the ARS HYMO Computer Program." This drainage study follows the procedures outlined in both the CoA DPM Section 22.2 and the AHYMO Computer Program.

PRECIPITATION

This project will not utilize an on-site detention pond. Storm water will be conveyed through underground pipe systems that will discharge into the East Branch of the Blacks Arroyo at three separate locations. The 100-yr 24-hr design storm was used for this analysis. The AHYMO Computer Program requires the 1, 6 and 24-hour precipitation values. These values were obtained from the **CCDMP** and are shown on **Table 1**.

Table 1
Precipitation Values

Return Period (yrs)	24 hr Rainfall (in)	6 hr Rainfall (in)	1 hr Rainfall (in)
100	2.7	2.2	1.8

LAND TREATMENTS

The land treatments used in the AHYMO Computer model are as described by Table A-4 of the CoA DPM Section 22.2, 1993 revision, and are summarized in **Table 2**.

Table 2
Land Treatment Classifications

Treatment	Land Condition
A	Soil uncompacted by human activity with 0 to 10 percent slopes. Native grasses, weeds and shrubs in typical densities with minimal disturbance to grading, groundcover and infiltration capacity. Croplands. Unlined Arroyos.
B	Irrigated lawns, parks and golf courses with 0 to 10 percent slopes. Soil uncompacted by human activity with slopes greater than 10 percent and less than 20 percent.
C	Soil compacted by human activity. Unpaved parking, roads and trail. Most vacant lots. Gravel or rock on plastic (desert landscaping)
D	Impervious areas, pavement and roofs.

Table A-5 of the CoA DPM Section 22.2, 1993 revision summarizes the Percent of Treatment D with a corresponding land use. Since this project site is a Single Family Residential Subdivision, the corresponding Percent of Treatment D is determined by the equation: $7*((N*N)+(5*N))^{0.5}$ where, N=units/acre (N=284units/57.77=4.92). The remaining was split between Treatment B and C. Therefore the Land Treatments for this site are as follows: %A = 0, %B = 25.6, %C = 25.6, and %D = 48.8.

The Land Treatments for the Off-Site **Basins 601, 602, 605 and 606** were taken directly from **CCDMP** and are as follows: **Basins 601 and 605; %A = 0, %B = 0, %C = 15, and %D = 85. Basins 602 and 606; %A = 10, %B = 33, %C = 30, %D = 27.**

STREET AND INLET CAPACITY CALCULATIONS

Both street and inlet capacities were calculated using the plates in the **City of Albuquerque DPM**. Tract 6A Subdivision incorporated flow splits into the creation of each actual drainage basin. See **Appendix C** for additional information.

STORM DRAIN HYDRAULICS

Storm Drains were modeled using Haestad Method's "StormCad" software (see Appendix C). Headlosses were calculated using the procedures outlined in the *City of Albuquerque DPM*. The main line of the storm drain was designed based on the routed peak discharges as indicated in the AHYMO model and the storm drain design is included in **Appendix D**. The lateral lines into the main system were designed for the peak flow for each particular line without reference to any routing in the main line.

PRE-DEVELOPMENT CONDITIONS

This project site is in its pre-development condition with existing natural vegetation throughout the site. The project site naturally slopes from northeast to the southwest across the site. The East Branch of the Blacks Arroyo to the west and ½ Acre Lots and Southern Boulevard to the north bound the property. Southern Blvd is paved with curb and gutter while the East Branch of the Blacks Arroyo is concrete lined. On-site runoff sheet flows across the site and concentrates into the East Branch of the Black Arroyo. The runoff discharges through Unit 16 of Rio Rancho Estates, crosses into Bernalillo County and into the Blacks Arroyo Dam.

There are four small off-site basins (**Basins 601, 602, 605, 606**) between the Tract 6A Boundary and Southern Boulevard, that discharge onto the subject property. These Basins represent the offsite basin **OFF_4** and a portion of **OFF_5** as shown on Figure 2 of the *CCDMP*. Field investigations and surveys indicate that the remainder of **OFF_5**, at the southwest corner of Southern and Golf Course, will drain east directly to Golf Course Road. **Basins 601** and **605** consist of ½ Acre Commercial Lots. **Basins 602** and **606** consist of ½ Acre Residential Lots. **Basins 601 and 602** discharge onto Tract 6A via Walsh Street. **Basins 605 and 606** discharge onto Tract 6A via 28th Street. The East Branch of the Blacks Arroyo located along the western boundary of Tract 6A, intercepts off-site runoff from the west. Please refer to the *CCDMP* and *CCDIP* for further information and analysis of the pre-developed condition.

ULTIMATE DEVELOPED CONDITIONS

According to the Figure 2 of the *CCDIP*, the site is required to accept 57 cfs from the off-site basins to the north and 50 cfs from the Golf Course Storm Drain System to the east. As indicated in the previous section, the off-site basins to the north have been modified based on field investigation. Based on discussions with Wilson & Company, the 50 cfs from the Golf Course Storm Drain System will be picked up by the construction of Chianti Road, south of the development. Therefore the off-site flow rates have been adjusted accordingly.

Also according to the *CCDIP*, Tract 19 is a park area that will generate 12 cfs and combine with the on-site flows at the southwest corner of the development. This area has been incorporated into the development and is included in the on-site analysis as part of the subdivision.

Drainage Patterns

As indicated in **Exhibit 2**, the developed drainage design consists of six (6) on-site and four (4) off-site drainage basins. **Basins 601, 602, 605, and 606** are the off-site flows that discharge into Tract 6A from the north. The developed conditions modeling, of the off-site basins (**Basins 601, 602, 605 and 606**) was taken directly from the approved **CCDMP** and was not altered.

Basins 601 and 602 combine to create **Analysis Point #1**, which will enter the subdivision along Walsh Street and join **Basin 603**. The combined flow will enter Storm Drain **System 100** at **Analysis Point #2**. **Analysis Point #2** is the start of **System 100**, which is connected to **System 200**. **Basin 604** will sheet flow directly into the concrete lined channel. **Analysis Point #3** combines flows from **Basins 605 and 606**, where they will enter **Basin 607**. This combined flow is collected at **Analysis Point #4**, where it will enter **System 200**. **System 200** enters the concrete lined channel through Parcel D. **Basin 608** will drain into **System 300** at **Analysis Point #5**. **Analysis Point #5** is the start of **System 300**, which is connected to **System 400**. **Basin 609** will drain into **System 400** at **Analysis Point #6**. System 400 enters the concrete lined channel through Parcel B. Lastly **Basin 610** will drain directly to the concrete channel through storm drain **System 500**.

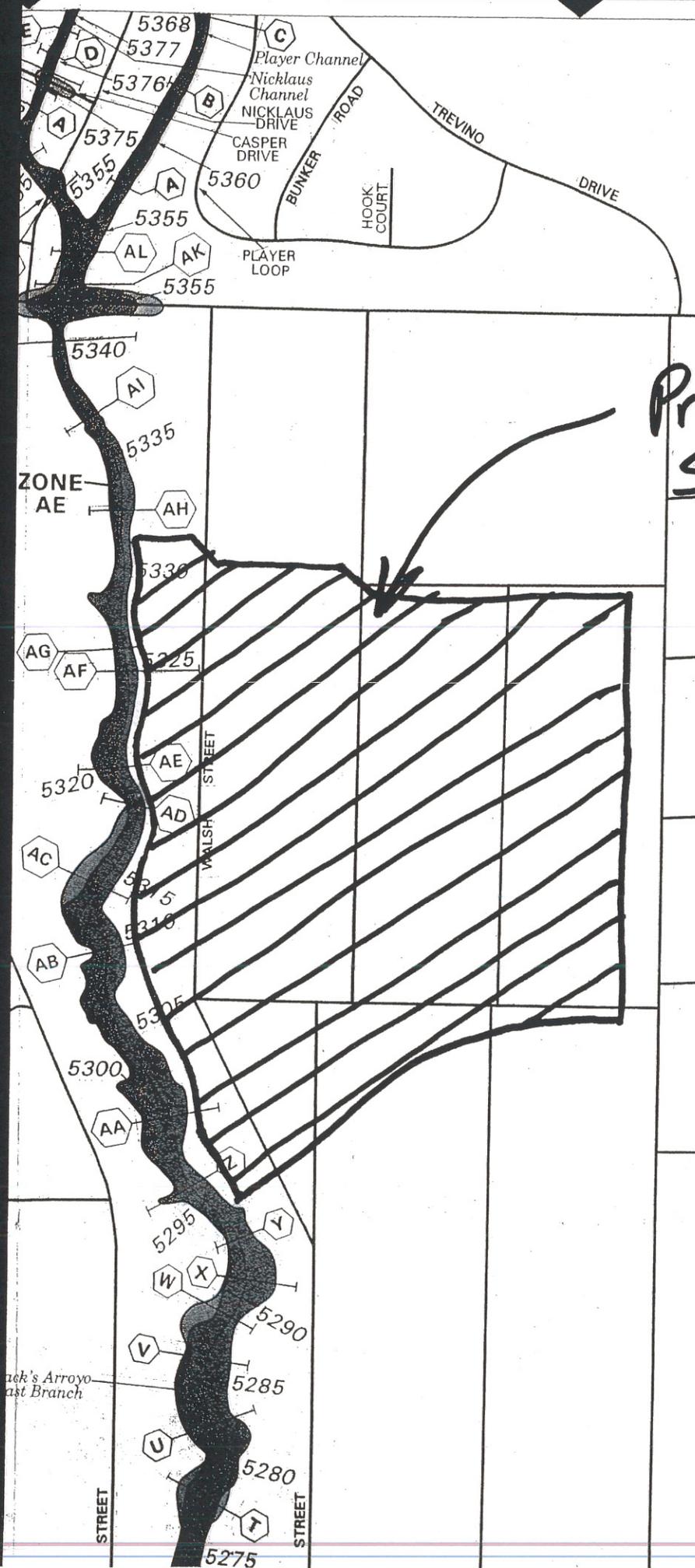
CONCLUSION

Table 3 compares the findings of the analysis of the Tract 6A Subdivision with the results of the approved **Cabazon Communities Drainage Implementation Plan**.

Table 3
Runoff Comparison for Tract 6A

Description	Basin Area (Mi ²)	Time to Peak (hr)	100-Yr Runoff Volume (Ac-ft)	100-Yr Peak Discharge (Ft ³ /s)
CCDIP	0.122	1.50	11.50	276
CCDMP	0.122	1.50	11.50	276
HZI Plan	0.115	1.50	10.27	248.6

The Wilson & Co. DIP allows for 276 cfs to discharge from Tract 6A. This includes offsite flows, which would flow through the site. The total discharge for this project is 248.6 cfs. Therefore this project complies with the **Cabazon Communities Phase II Drainage Management Plan** and the **Cabazon Communities Drainage Implementation Plan**.



Project Site

NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP

SANDOVAL COUNTY;
NEW MEXICO AND
INCORPORATED AREAS

(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:

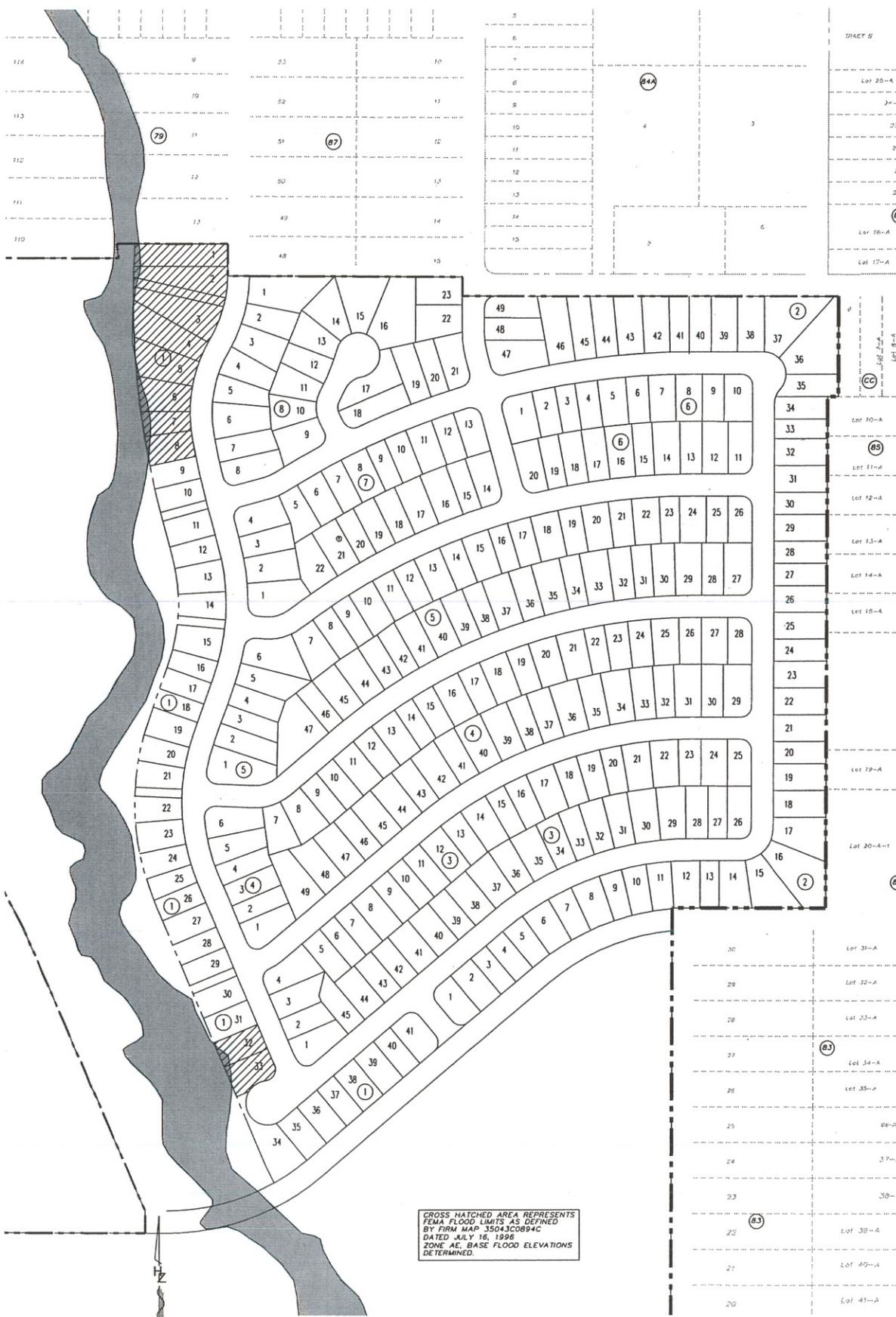
COMMUNITY	NUMBER	PANEL	SUFFIX
RIO RANCHO, CITY OF	350148	0894	C

MAP NUMBER
35043C0894 C

EFFECTIVE DATE:
JULY 16, 1996



Federal Emergency Management Agency



CROSS HATCHED AREA REPRESENTS
 FEMA FLOOD LIMITS AS DEFINED
 BY FIRM MAP 35043C0894C
 DATED JULY 16, 1998
 ZONE AE. BASE FLOOD ELEVATIONS
 DETERMINED.

LEGEND

■ FEMA FLOOD ZONE

▨ AFFECTED LOT

NOT TO SCALE

Designed For:
CURB NORTH, LLC

EXISTING FEMA FLOOD ZONE
YUCATAN DEL ESTE AT CABEZON TRACT 6A
FEBRUARY 2006

Designed By:
HUITT-ZOLLARS
 Huitt-Zollars, Inc. Rio Rancho
 333 Rio Rancho Drive NE, Suite 101
 Rio Rancho, New Mexico 87224
 Phone (505) 892-5141 Fax (505) 892-3259

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Summary File

(s16.67h8.5v0T&l8D

AHYMO PROGRAM SUMMARY TABLE (AHYMO 97) -
INPUT FILE = G:\Proj\170542-1\DRN_ST-1\AHYMO\CAB6A.dat

- VERSION: 1997.02c

RUN DATE (MON/DAY/YR) =02/07/2006
USER NO.= AHYMO-I-9702a01000150-SH

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1	NOTATION
START											TIME= .00
LOCATION			RIO RANCHO								
*S											
*S	CABEZON TRACT 6A										
*S	FN:CAB6A.DAT										
*S											
*S											
*S											
RAINFALL	TYPE= 2										RAIN24= 2.700
*S	*****										
*S	BULK FOR SEDIMENT - DEVELOPED										
SEDIMENT BULK											PK BF = 1.05
*S	-----										
*S	COMPUTE OFFSITE BASIN 601 (COMMERCIAL)										
COMPUTE NM HYD	601.OFF	-	1	.00548	14.52	.686	2.34567	1.500	4.141	PER IMP=	85.00
*S	-----										
*S	COMPUTE OFFSITE BASIN 602 (RESIDENTIAL)										
COMPUTE NM HYD	602.OFF	-	2	.01027	18.68	.682	1.24535	1.500	2.842	PER IMP=	27.00
*S	-----										
*S	ADD 601 TO 602										
ADD HYD	AP.1	1& 2	3	.01575	33.20	1.368	1.62815	1.500	3.294		
*S	-----										
*S	COMPUTE ONSITE BASIN 603										
COMPUTE NM HYD	603.ON	-	4	.01297	28.33	1.177	1.70151	1.500	3.413	PER IMP=	50.00
*S	-----										
*S	ADD AP.1 TO 603										
ADD HYD	AP.2	3& 4	5	.02872	61.53	2.545	1.66127	1.500	3.348		
*S	-----										
*S	DIVIDE AP.2										
*S	ID=6 IS 55.00 CFS INTO INLETS										
*S	ID=7 IS 6.35 CFS BYPASSING INLET TO BASIN103										
DIVIDE HYD	SYSTEM.100	5	6	.02842	55.00	2.518	1.66127	1.500	3.024		
	AP.2.BYPASS	and	7	.00030	6.53	.027	1.66128	1.500	33.502		
*S	-----										
*S	COMPUTE ONSITE BASIN 604										
COMPUTE NM HYD	604.ON	-	8	.00086	1.89	.078	1.70151	1.500	3.440	PER IMP=	50.00
*S	-----										
*S	COMPUTE OFFSITE BASIN 605 (COMMERCIAL)										
COMPUTE NM HYD	605.OFF	-	9	.00166	4.41	.208	2.34567	1.500	4.151	PER IMP=	85.00
*S	-----										
*S	COMPUTE OFFSITE BASIN 606 (RESIDENTIAL)										
COMPUTE NM HYD	606.OFF	-	10	.00747	13.59	.496	1.24535	1.500	2.842	PER IMP=	27.00
*S	-----										
*S	ADD 605.OFF TO 606.OFF										
ADD HYD	AP.3	9&10	11	.00913	18.00	.704	1.44535	1.500	3.080		
*S	-----										
*S	COMPUTE ONSITE BASIN 607										
COMPUTE NM HYD	607.ON	-	12	.02109	46.06	1.914	1.70151	1.500	3.412	PER IMP=	50.00
*S	-----										
*S	ADD AP.2.BYPASS TO 607.ON										
ADD HYD	607.TOTAL	7&12	13	.02139	52.59	1.941	1.70093	1.500	3.841		
*S	-----										
*S	ADD AP.3 TO 607.TOTAL										
ADD HYD	AP.4	11&13	14	.03052	70.59	2.645	1.62448	1.500	3.613		
*S	-----										
*S	DIVIDE AP.4										
*S	ID=15 IS 64.50 CFS INTO INLETS										
*S	ID=16 IS 6.09 CFS BYPASSING INLET TO BASIN103										
DIVIDE HYD	SYSTEM.200	14	15	.03023	64.50	2.619	1.62448	1.500	3.333		
	AP.4.BYPASS	and	16	.00029	6.09	.025	1.62449	1.500	32.760		
*S	-----										
*S	ADD SYSTEM.100 TO SYSTEM.200										
ADD HYD	200.OUTFALL	6&15	17	.05865	119.50	5.137	1.64231	1.500	3.184		
*S	-----										
*S	COMPUTE ONSITE BASIN 608										
COMPUTE NM HYD	608.ON	-	18	.01636	35.73	1.485	1.70151	1.500	3.413	PER IMP=	50.00
*S	-----										
*S	ADD AP.4.BYPASS TO 608.ON										

Cabezon Tract 6A
100-Year 24-Hour Duration Storm-Developed
AHYMO Summary File

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 2	NOTATION
ADD HYD	AP.5 16&18	19		.01665	41.83	1.510	1.70015	1.500	3.925		
*S-----											
*S DIVIDE AP.5											
*S ID=20 IS 34.50 CFS INTO INLETS											
*S ID=21 IS 7.33 CFS BYPASSING INLET TO BASIN103											
DIVIDE HYD	SYSTEM.300	19	20	.01632	34.50	1.480	1.70015	1.500	3.304		
	AP.5.BYPASS	and	21	.00033	7.33	.030	1.70015	1.500	34.286		
*S-----											
*S COMPUTE ONSITE BASIN 609											
COMPUTE NM HYD	609.ON	-	22	.01580	34.51	1.434	1.70151	1.500	3.413	PER IMP=	50.00
*S-----											
*S ADD AP.5.BYPASS TO 609.ON											
ADD HYD	AP.6 21&22	23		.01613	41.84	1.464	1.70147	1.500	4.052		
*S-----											
*S DIVIDE AP.6											
*S ID=24 IS 34.60 CFS INTO INLETS											
*S ID=25 IS 7.24 CFS BYPASSING INLET TO BASIN103											
DIVIDE HYD	SYSTEM.400	23	24	.01580	34.60	1.434	1.70147	1.500	3.421		
	AP.6.BYPASS	and	25	.00033	7.24	.030	1.70147	1.500	34.313		
*S-----											
*S ADD SYSTEM.300 TO SYSTEM.400											
ADD HYD	400.OUTFALL	20&24	26	.03212	69.10	2.914	1.70080	1.500	3.361		
*S-----											
*S COMPUTE ONSITE BASIN 610											
COMPUTE NM HYD	610.ON	-	27	.02331	50.91	2.115	1.70151	1.500	3.412	PER IMP=	50.00
*S-----											
*S ADD AP.6.BYPASS TO 610.ON											
ADD HYD	AP.7 25&27	28		.02364	58.14	2.145	1.70150	1.500	3.843		
*S-----											
*S DIVIDE AP.7											
*S ID=29 IS 36.50 CFS INTO INLETS											
*S ID=30 IS 23.54 CFS BYPASSING INLET TO SUMP											
DIVIDE HYD	SYSTEM.500A	28	29	.02161	34.60	1.961	1.70150	1.450	2.501		
	SUMP	and	30	.00203	23.54	.184	1.70150	1.500	18.165		
*S-----											
*S ADD SYSTEM.500A TO SUMP											
ADD HYD	500.OUTFALL	29&30	31	.02364	58.14	2.145	1.70150	1.500	3.843		
*S-----											
*S ADD 200.OUTFALL TO 400.OUTFALL											
ADD HYD	SUBTOTAL.A	17&26	32	.09077	188.60	8.051	1.66301	1.500	3.247		
*S-----											
*S ADD SUBTOTAL.A TO 500.OUTFALL											
ADD HYD	SUBTOTAL.B	32&31	33	.11441	246.74	10.196	1.67096	1.500	3.370		
*S-----											
*S ADD SUBTOTAL.B TO BASIN 604											
ADD HYD	TOTAL 33& 8	34		.11527	248.64	10.274	1.67118	1.500	3.370		
*S-----											
FINISH											
(s0p10h4099T&l6D_											

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

(s16.67h8.5v0T&l8D

AHYMO PROGRAM (AHYMO_97) - - Version: 1997.02c
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 START TIME (HR:MIN:SEC) = 12:01:07 USER NO.= AHYMO-I-9702a01000150-SH
 INPUT FILE = G:\Proj\170542-1\DRN_ST-1\AHYMO\CAB6A.dat

START TIME=0.0 CODE 0 LINES -6
 LOCATION RIO RANCHO
 City of Rio Rancho soil infiltration values (LAND FACTORS) used for computations.
 Land Treatment Initial Abstr.(in) Unif. Infiltr.(in/hour)
 A 0.65 1.67
 B 0.50 1.25
 C 0.35 0.83
 D 0.10 0.04

*S
 *S CABEZON TRACT 6A
 *S
 *S FN:CAB6A.DAT - HYMO PER JAN 1997 DPM REVISIONS
 *S
 *S
 *S
 *S
 RAINFALL TYPE=2 RAIN QUARTER=0.0 RAIN ONE=1.8
 RAIN SIX=2.2 RAIN DAY=2.7 DT=.05

COMPUTED 24-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.

DT =	.050000 HOURS						END TIME =	24.000000 HOURS					
.0000	.0037	.0075	.0115	.0155	.0197	.0241							
.0286	.0334	.0383	.0434	.0487	.0543	.0602							
.0664	.0730	.0799	.0873	.0953	.1038	.1131							
.1207	.1291	.1534	.2108	.3095	.4622	.6820							
.9826	1.2196	1.3267	1.4161	1.4945	1.5645	1.6279							
1.6858	1.7389	1.7878	1.8329	1.8746	1.9131	1.9225							
1.9311	1.9393	1.9469	1.9542	1.9610	1.9676	1.9739							
1.9799	1.9857	1.9913	1.9966	2.0018	2.0069	2.0118							
2.0166	2.0212	2.0257	2.0301	2.0344	2.0386	2.0426							
2.0466	2.0506	2.0544	2.0582	2.0619	2.0655	2.0690							
2.0725	2.0759	2.0793	2.0826	2.0859	2.0891	2.0923							
2.0954	2.0984	2.1015	2.1044	2.1074	2.1103	2.1132							
2.1160	2.1188	2.1215	2.1242	2.1269	2.1296	2.1322							
2.1348	2.1374	2.1399	2.1424	2.1449	2.1474	2.1498							
2.1522	2.1546	2.1570	2.1593	2.1616	2.1639	2.1662							
2.1684	2.1707	2.1729	2.1751	2.1772	2.1794	2.1815							
2.1837	2.1858	2.1878	2.1899	2.1920	2.1940	2.1960							
2.1980	2.2000	2.2021	2.2042	2.2063	2.2084	2.2105							
2.2126	2.2147	2.2167	2.2188	2.2209	2.2229	2.2250							
2.2270	2.2290	2.2310	2.2330	2.2351	2.2371	2.2390							
2.2410	2.2430	2.2450	2.2470	2.2489	2.2509	2.2528							
2.2548	2.2567	2.2586	2.2605	2.2625	2.2644	2.2663							
2.2682	2.2701	2.2720	2.2738	2.2757	2.2776	2.2795							
2.2813	2.2832	2.2850	2.2869	2.2887	2.2905	2.2923							
2.2942	2.2960	2.2978	2.2996	2.3014	2.3032	2.3050							
2.3068	2.3085	2.3103	2.3121	2.3138	2.3156	2.3174							
2.3191	2.3208	2.3226	2.3243	2.3260	2.3278	2.3295							
2.3312	2.3329	2.3346	2.3363	2.3380	2.3397	2.3414							
2.3431	2.3448	2.3464	2.3481	2.3498	2.3514	2.3531							
2.3547	2.3564	2.3580	2.3596	2.3613	2.3629	2.3645							
2.3662	2.3678	2.3694	2.3710	2.3726	2.3742	2.3758							
2.3774	2.3790	2.3806	2.3821	2.3837	2.3853	2.3869							
2.3884	2.3900	2.3915	2.3931	2.3946	2.3962	2.3977							
2.3993	2.4008	2.4023	2.4038	2.4054	2.4069	2.4084							
2.4099	2.4114	2.4129	2.4144	2.4159	2.4174	2.4189							
2.4204	2.4219	2.4234	2.4248	2.4263	2.4278	2.4293							
2.4307	2.4322	2.4336	2.4351	2.4365	2.4380	2.4394							
2.4409	2.4423	2.4437	2.4452	2.4466	2.4480	2.4494							
2.4509	2.4523	2.4537	2.4551	2.4565	2.4579	2.4593							
2.4607	2.4621	2.4635	2.4649	2.4662	2.4676	2.4690							
2.4704	2.4718	2.4731	2.4745	2.4759	2.4772	2.4786							
2.4799	2.4813	2.4826	2.4840	2.4853	2.4867	2.4880							
2.4893	2.4907	2.4920	2.4933	2.4946	2.4960	2.4973							
2.4986	2.4999	2.5012	2.5025	2.5038	2.5051	2.5064							
2.5077	2.5090	2.5103	2.5116	2.5129	2.5142	2.5155							
2.5168	2.5180	2.5193	2.5206	2.5219	2.5231	2.5244							
2.5257	2.5269	2.5282	2.5294	2.5307	2.5319	2.5332							
2.5344	2.5357	2.5369	2.5382	2.5394	2.5406	2.5419							
2.5431	2.5443	2.5455	2.5468	2.5480	2.5492	2.5504							
2.5516	2.5528	2.5541	2.5553	2.5565	2.5577	2.5589							
2.5601	2.5613	2.5625	2.5636	2.5648	2.5660	2.5672							
2.5684	2.5696	2.5708	2.5719	2.5731	2.5743	2.5754							
2.5766	2.5778	2.5790	2.5801	2.5813	2.5824	2.5836							
2.5847	2.5859	2.5870	2.5882	2.5893	2.5905	2.5916							
2.5928	2.5939	2.5950	2.5962	2.5973	2.5984	2.5996							
2.6007	2.6018	2.6029	2.6041	2.6052	2.6063	2.6074							
2.6085	2.6097	2.6108	2.6119	2.6130	2.6141	2.6152							
2.6163	2.6174	2.6185	2.6196	2.6207	2.6218	2.6229							
2.6239	2.6250	2.6261	2.6272	2.6283	2.6294	2.6304							
2.6315	2.6326	2.6337	2.6347	2.6358	2.6369	2.6379							
2.6390	2.6401	2.6411	2.6422	2.6432	2.6443	2.6454							
2.6464	2.6475	2.6485	2.6496	2.6506	2.6516	2.6527							
2.6537	2.6548	2.6558	2.6569	2.6579	2.6589	2.6600							
2.6610	2.6620	2.6630	2.6641	2.6651	2.6661	2.6671							
2.6682	2.6692	2.6702	2.6712	2.6722	2.6732	2.6742							
2.6752	2.6763	2.6773	2.6783	2.6793	2.6803	2.6813							

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

2.6823 2.6833 2.6843 2.6853 2.6862 2.6872 2.6882
2.6892 2.6902 2.6912 2.6922 2.6932 2.6941 2.6951
2.6961 2.6971 2.6981 2.6990 2.7000

*S-----
*S BULK FOR SEDIMENT - DEVELOPED

SEDIMENT BULK CODE=1 BULK FACTOR=1.05

*S-----
*S COMPUTE OFFSITE BASIN 601 (COMMERCIAL)
COMPUTE NM HYD ID=1 HYD=601.OFF AREA=0.00548 SQ MI
%A=0 %B=0 %C=15 %D=85 TP=0.133 HR
MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 18.432 CFS UNIT VOLUME = .9985 B = 526.28 P60 = 1.8000
AREA = .004658 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .104841HR TP = .133000HR K/TP RATIO = .788276 SHAPE CONSTANT, N = 4.552994
UNIT PEAK = 2.4134 CFS UNIT VOLUME = .9963 B = 390.49 P60 = 1.8000
AREA = .000822 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=1 CODE=10

HYDROGRAPH FROM AREA 601.OFF

TIME HRS	FLOW CFS								
.000	.0	5.000	.1	10.000	.1	15.000	.1	20.000	.1
.500	.0	5.500	.1	10.500	.1	15.500	.1	20.500	.1
1.000	.1	6.000	.1	11.000	.1	16.000	.1	21.000	.1
1.500	14.5	6.500	.1	11.500	.1	16.500	.1	21.500	.1
2.000	3.4	7.000	.1	12.000	.1	17.000	.1	22.000	.1
2.500	.5	7.500	.1	12.500	.1	17.500	.1	22.500	.1
3.000	.2	8.000	.1	13.000	.1	18.000	.1	23.000	.1
3.500	.1	8.500	.1	13.500	.1	18.500	.1	23.500	.1
4.000	.1	9.000	.1	14.000	.1	19.000	.1	24.000	.1
4.500	.1	9.500	.1	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 2.34567 INCHES = .6856 ACRE-FEET
PEAK DISCHARGE RATE = 14.52 CFS AT 1.500 HOURS BASIN AREA = .0055 SQ. MI.

*S-----

*S COMPUTE OFFSITE BASIN 602 (RESIDENTIAL)
COMPUTE NM HYD ID=2 HYD=602.OFF AREA=0.01027 SQ MI
%A=10 %B=33 %C=30 %D=27 TP=0.133 HR
MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
UNIT PEAK = 10.972 CFS UNIT VOLUME = .9981 B = 526.28 P60 = 1.8000
AREA = .002773 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .125336HR TP = .133000HR K/TP RATIO = .942377 SHAPE CONSTANT, N = 3.751846
UNIT PEAK = 19.068 CFS UNIT VOLUME = 1.001 B = 338.27 P60 = 1.8000
AREA = .007497 SQ MI IA = .45890 INCHES INF = 1.13493 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=2 CODE=10

HYDROGRAPH FROM AREA 602.OFF

TIME HRS	FLOW CFS								
.000	.0	5.000	.1	10.000	.1	15.000	.1	20.000	.0
.500	.0	5.500	.1	10.500	.1	15.500	.0	20.500	.0
1.000	.0	6.000	.1	11.000	.1	16.000	.0	21.000	.0
1.500	18.7	6.500	.1	11.500	.1	16.500	.0	21.500	.0
2.000	2.9	7.000	.1	12.000	.1	17.000	.0	22.000	.0
2.500	.5	7.500	.1	12.500	.1	17.500	.0	22.500	.0
3.000	.2	8.000	.1	13.000	.1	18.000	.0	23.000	.0
3.500	.1	8.500	.1	13.500	.1	18.500	.0	23.500	.0
4.000	.1	9.000	.1	14.000	.1	19.000	.0	24.000	.0
4.500	.1	9.500	.1	14.500	.1	19.500	.0	24.500	.0

RUNOFF VOLUME = 1.24535 INCHES = .6821 ACRE-FEET
PEAK DISCHARGE RATE = 18.68 CFS AT 1.500 HOURS BASIN AREA = .0103 SQ. MI.

*S-----
*S ADD 601 TO 602

ADD HYD ID=3 HYD=AP.1 Idi=1 Idii=2
PRINT HYD ID=3 CODE=10

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

HYDROGRAPH FROM AREA AP.1

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1	21.000	.1
1.500	33.2	6.500	.2	11.500	.2	16.500	.1	21.500	.1
2.000	6.3	7.000	.2	12.000	.2	17.000	.1	22.000	.1
2.500	1.0	7.500	.2	12.500	.1	17.500	.1	22.500	.1
3.000	.4	8.000	.2	13.000	.1	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.1	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.62815 INCHES = 1.3676 ACRE-FEET
 PEAK DISCHARGE RATE = 33.20 CFS AT 1.500 HOURS BASIN AREA = .0158 SQ. MI.

*S-----

*S COMPUTE ONSITE BASIN 603

COMPUTE NM HYD ID=4 HYD=603.ON AREA=0.01297 SQ MI
 %A=0 %B=25 %C=25 %D=50 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 25.661 CFS UNIT VOLUME = .9987 B = 526.28 P60 = 1.8000
 AREA = .006485 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 17.268 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .006485 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=4 CODE=10

HYDROGRAPH FROM AREA 603.ON

TIME HRS	FLOW CFS								
.000	.0	5.000	.1	10.000	.1	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.1	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.1	16.000	.1	21.000	.1
1.500	28.3	6.500	.2	11.500	.1	16.500	.1	21.500	.1
2.000	5.4	7.000	.2	12.000	.1	17.000	.1	22.000	.1
2.500	.8	7.500	.2	12.500	.1	17.500	.1	22.500	.1
3.000	.3	8.000	.2	13.000	.1	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.1	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1	24.000	.1
4.500	.1	9.500	.2	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.70151 INCHES = 1.1770 ACRE-FEET
 PEAK DISCHARGE RATE = 28.33 CFS AT 1.500 HOURS BASIN AREA = .0130 SQ. MI.

*S-----

*S ADD AP.1 TO 603

ADD HYD ID=5 HYD=AP.2 Idi=3 Idii=4
 PRINT HYD ID=5 CODE=10

HYDROGRAPH FROM AREA AP.2

TIME HRS	FLOW CFS								
.000	.0	5.000	.3	10.000	.3	15.000	.3	20.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2	20.500	.2
1.000	.2	6.000	.4	11.000	.3	16.000	.2	21.000	.2
1.500	61.5	6.500	.4	11.500	.3	16.500	.2	21.500	.2
2.000	11.7	7.000	.4	12.000	.3	17.000	.2	22.000	.2
2.500	1.8	7.500	.4	12.500	.3	17.500	.2	22.500	.2
3.000	.7	8.000	.4	13.000	.3	18.000	.2	23.000	.2
3.500	.4	8.500	.3	13.500	.3	18.500	.2	23.500	.2
4.000	.3	9.000	.3	14.000	.3	19.000	.2	24.000	.2
4.500	.3	9.500	.3	14.500	.3	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.66127 INCHES = 2.5446 ACRE-FEET
 PEAK DISCHARGE RATE = 61.53 CFS AT 1.500 HOURS BASIN AREA = .0287 SQ. MI.

*S-----

*S DIVIDE AP.2

*S ID=6 IS 55.00 CFS INTO INLETS
 *S ID=7 IS 6.35 CFS BYPASSING INLET TO BASIN103
 DIVIDE HYD ID=5 Q=55.0 IDi=6 HYD=SYSTEM.100
 IDi=7 HYD=AP.2.BYPASS

*S-----

Cabezon Tract 6A

100-Year 24-Hour Duration Storm-Developed

AHYMO Output File

*S COMPUTE ONSITE BASIN 604

COMPUTE NM HYD ID=8 HYD=604.ON AREA=0.00086 SQ MI
 %A=0 %B=25 %C=25 %D=50 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 1.7015 CFS UNIT VOLUME = .9928 B = 526.28 P60 = 1.8000
 AREA = .000430 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 1.1450 CFS UNIT VOLUME = .9896 B = 354.14 P60 = 1.8000
 AREA = .000430 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=8 CODE=10

HYDROGRAPH FROM AREA 604.ON

TIME HRS	FLOW CFS								
.000	.0	5.000	.0	10.000	.0	15.000	.0	20.000	.0
.500	.0	5.500	.0	10.500	.0	15.500	.0	20.500	.0
1.000	.0	6.000	.0	11.000	.0	16.000	.0	21.000	.0
1.500	1.9	6.500	.0	11.500	.0	16.500	.0	21.500	.0
2.000	.4	7.000	.0	12.000	.0	17.000	.0	22.000	.0
2.500	.1	7.500	.0	12.500	.0	17.500	.0	22.500	.0
3.000	.0	8.000	.0	13.000	.0	18.000	.0	23.000	.0
3.500	.0	8.500	.0	13.500	.0	18.500	.0	23.500	.0
4.000	.0	9.000	.0	14.000	.0	19.000	.0	24.000	.0
4.500	.0	9.500	.0	14.500	.0	19.500	.0		

RUNOFF VOLUME = 1.70151 INCHES = .0780 ACRE-FEET
 PEAK DISCHARGE RATE = 1.89 CFS AT 1.500 HOURS BASIN AREA = .0009 SQ. MI.

*S-----

*S COMPUTE OFFSITE BASIN 605 (COMMERCIAL)

COMPUTE NM HYD ID=9 HYD=605.OFF AREA=0.00166 SQ MI
 %A=0 %B=0 %C=15 %D=85 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 5.5833 CFS UNIT VOLUME = .9971 B = 526.28 P60 = 1.8000
 AREA = .001411 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .104841HR TP = .133000HR K/TP RATIO = .788276 SHAPE CONSTANT, N = 4.552994
 UNIT PEAK = .73106 CFS UNIT VOLUME = .9854 B = 390.49 P60 = 1.8000
 AREA = .000249 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=9 CODE=10

HYDROGRAPH FROM AREA 605.OFF

TIME HRS	FLOW CFS								
.000	.0	5.000	.0	10.000	.0	15.000	.0	20.000	.0
.500	.0	5.500	.0	10.500	.0	15.500	.0	20.500	.0
1.000	.0	6.000	.0	11.000	.0	16.000	.0	21.000	.0
1.500	4.4	6.500	.0	11.500	.0	16.500	.0	21.500	.0
2.000	1.0	7.000	.0	12.000	.0	17.000	.0	22.000	.0
2.500	.1	7.500	.0	12.500	.0	17.500	.0	22.500	.0
3.000	.1	8.000	.0	13.000	.0	18.000	.0	23.000	.0
3.500	.0	8.500	.0	13.500	.0	18.500	.0	23.500	.0
4.000	.0	9.000	.0	14.000	.0	19.000	.0	24.000	.0
4.500	.0	9.500	.0	14.500	.0	19.500	.0		

RUNOFF VOLUME = 2.34567 INCHES = .2077 ACRE-FEET
 PEAK DISCHARGE RATE = 4.41 CFS AT 1.500 HOURS BASIN AREA = .0017 SQ. MI.

*S-----

*S COMPUTE OFFSITE BASIN 606 (RESIDENTIAL)

COMPUTE NM HYD ID=10 HYD=606.OFF AREA=0.00747 SQ MI
 %A=10 %B=33 %C=30 %D=27 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 7.9808 CFS UNIT VOLUME = .9979 B = 526.28 P60 = 1.8000
 AREA = .002017 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .125336HR TP = .133000HR K/TP RATIO = .942377 SHAPE CONSTANT, N = 3.751846

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

UNIT PEAK = 13.869 CFS UNIT VOLUME = 1.000 B = 338.27 P60 = 1.8000
 AREA = .005453 SQ MI IA = .45890 INCHES INF = 1.13493 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=10 CODE=10

HYDROGRAPH FROM AREA 606.OFF

TIME HRS	FLOW CFS								
.000	.0	5.000	.0	10.000	.0	15.000	.0	20.000	.0
.500	.0	5.500	.0	10.500	.0	15.500	.0	20.500	.0
1.000	.0	6.000	.1	11.000	.0	16.000	.0	21.000	.0
1.500	13.6	6.500	.1	11.500	.0	16.500	.0	21.500	.0
2.000	2.1	7.000	.1	12.000	.0	17.000	.0	22.000	.0
2.500	.4	7.500	.1	12.500	.0	17.500	.0	22.500	.0
3.000	.1	8.000	.1	13.000	.0	18.000	.0	23.000	.0
3.500	.1	8.500	.1	13.500	.0	18.500	.0	23.500	.0
4.000	.0	9.000	.0	14.000	.0	19.000	.0	24.000	.0
4.500	.0	9.500	.0	14.500	.0	19.500	.0	24.500	.0

RUNOFF VOLUME = 1.24535 INCHES = .4961 ACRE-FEET
 PEAK DISCHARGE RATE = 13.59 CFS AT 1.500 HOURS BASIN AREA = .0075 SQ. MI.

*S-----

*S ADD 605.OFF TO 606.OFF

ADD HYD ID=11 HYD=AP.3 IDi=9 IDii=10
 PRINT HYD ID=11 CODE=10

HYDROGRAPH FROM AREA AP.3

TIME HRS	FLOW CFS								
.000	.0	5.000	.1	10.000	.1	15.000	.1	20.000	.1
.500	.0	5.500	.1	10.500	.1	15.500	.1	20.500	.1
1.000	.0	6.000	.1	11.000	.1	16.000	.1	21.000	.0
1.500	18.0	6.500	.1	11.500	.1	16.500	.1	21.500	.0
2.000	3.1	7.000	.1	12.000	.1	17.000	.1	22.000	.0
2.500	.5	7.500	.1	12.500	.1	17.500	.1	22.500	.0
3.000	.2	8.000	.1	13.000	.1	18.000	.1	23.000	.0
3.500	.1	8.500	.1	13.500	.1	18.500	.1	23.500	.0
4.000	.1	9.000	.1	14.000	.1	19.000	.1	24.000	.0
4.500	.1	9.500	.1	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.44535 INCHES = .7038 ACRE-FEET
 PEAK DISCHARGE RATE = 18.00 CFS AT 1.500 HOURS BASIN AREA = .0091 SQ. MI.

*S-----

*S COMPUTE ONSITE BASIN 607

COMPUTE NM HYD ID=12 HYD=607.ON AREA=0.02109 SQ MI
 %A=0 %B=25 %C=25 %D=50 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 41.726 CFS UNIT VOLUME = .9989 B = 526.28 P60 = 1.8000
 AREA = .010545 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 28.078 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .010545 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=12 CODE=10

HYDROGRAPH FROM AREA 607.ON

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.2	20.000	.2
.500	.0	5.500	.3	10.500	.2	15.500	.2	20.500	.2
1.000	.1	6.000	.3	11.000	.2	16.000	.2	21.000	.2
1.500	46.1	6.500	.3	11.500	.2	16.500	.2	21.500	.2
2.000	8.8	7.000	.3	12.000	.2	17.000	.2	22.000	.1
2.500	1.4	7.500	.3	12.500	.2	17.500	.2	22.500	.1
3.000	.5	8.000	.3	13.000	.2	18.000	.2	23.000	.1
3.500	.3	8.500	.3	13.500	.2	18.500	.2	23.500	.1
4.000	.2	9.000	.3	14.000	.2	19.000	.2	24.000	.1
4.500	.2	9.500	.2	14.500	.2	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.70151 INCHES = 1.9138 ACRE-FEET
 PEAK DISCHARGE RATE = 46.06 CFS AT 1.500 HOURS BASIN AREA = .0211 SQ. MI.

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

*S-----
 *S ADD AP.2.BYPASS TO 607.ON
 ADD HYD ID=13 HYD=607.TOTAL IDi=7 IDii=12
 PRINT HYD ID=13 CODE=10

HYDROGRAPH FROM AREA 607.TOTAL

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.2	20.000	.2
.500	.0	5.500	.3	10.500	.2	15.500	.2	20.500	.2
1.000	.1	6.000	.3	11.000	.2	16.000	.2	21.000	.2
1.500	52.6	6.500	.3	11.500	.2	16.500	.2	21.500	.2
2.000	8.8	7.000	.3	12.000	.2	17.000	.2	22.000	.1
2.500	1.4	7.500	.3	12.500	.2	17.500	.2	22.500	.1
3.000	.5	8.000	.3	13.000	.2	18.000	.2	23.000	.1
3.500	.3	8.500	.3	13.500	.2	18.500	.2	23.500	.1
4.000	.2	9.000	.3	14.000	.2	19.000	.2	24.000	.1
4.500	.2	9.500	.2	14.500	.2	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.70093 INCHES = 1.9408 ACRE-FEET
 PEAK DISCHARGE RATE = 52.59 CFS AT 1.500 HOURS BASIN AREA = .0214 SQ. MI.

*S-----
 *S ADD AP.3 TO 607.TOTAL
 ADD HYD ID=14 HYD=AP.4 IDi=11 IDii=13
 PRINT HYD ID=14 CODE=10

HYDROGRAPH FROM AREA AP.4

TIME HRS	FLOW CFS								
.000	.0	5.000	.3	10.000	.3	15.000	.3	20.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2	20.500	.2
1.000	.2	6.000	.4	11.000	.3	16.000	.2	21.000	.2
1.500	70.6	6.500	.4	11.500	.3	16.500	.2	21.500	.2
2.000	11.9	7.000	.4	12.000	.3	17.000	.2	22.000	.2
2.500	1.9	7.500	.4	12.500	.3	17.500	.2	22.500	.2
3.000	.7	8.000	.4	13.000	.3	18.000	.2	23.000	.2
3.500	.4	8.500	.3	13.500	.3	18.500	.2	23.500	.2
4.000	.3	9.000	.3	14.000	.3	19.000	.2	24.000	.2
4.500	.3	9.500	.3	14.500	.3	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.62448 INCHES = 2.6446 ACRE-FEET
 PEAK DISCHARGE RATE = 70.59 CFS AT 1.500 HOURS BASIN AREA = .0305 SQ. MI.

*S-----
 *S DIVIDE AP.4
 *S ID=15 IS 64.50 CFS INTO INLETS
 *S ID=16 IS 6.09 CFS BYPASSING INLET TO BASIN103
 DIVIDE HYD ID=14 Q=64.5 IDi=15 HYD=SYSTEM.200
 IDii=16 HYD=AP.4.BYPASS

*S-----
 *S ADD SYSTEM.100 TO SYSTEM.200
 ADD HYD ID=17 HYD=200.OUTFALL IDi=6 IDii=15
 PRINT HYD ID=17 CODE=10

HYDROGRAPH FROM AREA 200.OUTFALL

TIME HRS	FLOW CFS								
.000	.0	5.000	.6	10.000	.6	15.000	.5	20.000	.4
.500	.0	5.500	.7	10.500	.6	15.500	.5	20.500	.4
1.000	.4	6.000	.7	11.000	.6	16.000	.5	21.000	.4
1.500	119.5	6.500	.8	11.500	.6	16.500	.5	21.500	.4
2.000	23.5	7.000	.8	12.000	.6	17.000	.5	22.000	.4
2.500	3.7	7.500	.7	12.500	.6	17.500	.5	22.500	.4
3.000	1.3	8.000	.7	13.000	.5	18.000	.5	23.000	.4
3.500	.8	8.500	.7	13.500	.5	18.500	.4	23.500	.4
4.000	.7	9.000	.7	14.000	.5	19.000	.4	24.000	.4
4.500	.6	9.500	.7	14.500	.5	19.500	.4	24.500	.0

RUNOFF VOLUME = 1.64231 INCHES = 5.1371 ACRE-FEET
 PEAK DISCHARGE RATE = 119.50 CFS AT 1.500 HOURS BASIN AREA = .0586 SQ. MI.

*S-----
 *S COMPUTE ONSITE BASIN 608
 COMPUTE NM HYD ID=18 HYD=608.ON AREA=0.01636 SQ MI
 %A=0 %B=25 %C=25 %D=50 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 32.368 CFS UNIT VOLUME = .9988 B = 526.28 P60 = 1.8000
 AREA = .008180 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

UNIT PEAK = 21.781 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .008180 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=18 CODE=10

HYDROGRAPH FROM AREA 608.ON

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1	21.000	.1
1.500	35.7	6.500	.2	11.500	.2	16.500	.1	21.500	.1
2.000	6.8	7.000	.2	12.000	.2	17.000	.1	22.000	.1
2.500	1.1	7.500	.2	12.500	.2	17.500	.1	22.500	.1
3.000	.4	8.000	.2	13.000	.2	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.2	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.2	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.70151 INCHES = 1.4846 ACRE-FEET
 PEAK DISCHARGE RATE = 35.73 CFS AT 1.500 HOURS BASIN AREA = .0164 SQ. MI.

*S-----

*S ADD AP.4.BYPASS TO 608.ON
 ADD HYD ID=19 HYD=AP.5 IDi=16 IDii=18
 PRINT HYD ID=19 CODE=10

HYDROGRAPH FROM AREA AP.5

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1	21.000	.1
1.500	41.8	6.500	.2	11.500	.2	16.500	.1	21.500	.1
2.000	6.8	7.000	.2	12.000	.2	17.000	.1	22.000	.1
2.500	1.1	7.500	.2	12.500	.2	17.500	.1	22.500	.1
3.000	.4	8.000	.2	13.000	.2	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.2	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.2	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.70015 INCHES = 1.5098 ACRE-FEET
 PEAK DISCHARGE RATE = 41.83 CFS AT 1.500 HOURS BASIN AREA = .0167 SQ. MI.

*S-----

*S DIVIDE AP.5
 *S ID=20 IS 34.50 CFS INTO INLETS
 *S ID=21 IS 7.33 CFS BYPASSING INLET TO BASIN103
 DIVIDE HYD ID=19 Q=34.5 IDi=20 HYD=SYSTEM.300
 IDii=21 HYD=AP.5.BYPASS

*S-----

*S COMPUTE ONSITE BASIN 609
 COMPUTE NM HYD ID=22 HYD=609.ON AREA=0.01580 SQ MI
 %A=0 %B=25 %C=25 %D=50 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 31.260 CFS UNIT VOLUME = .9988 B = 526.28 P60 = 1.8000
 AREA = .007900 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 21.035 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .007900 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=22 CODE=10

HYDROGRAPH FROM AREA 609.ON

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1	21.000	.1
1.500	34.5	6.500	.2	11.500	.2	16.500	.1	21.500	.1
2.000	6.6	7.000	.2	12.000	.2	17.000	.1	22.000	.1
2.500	1.0	7.500	.2	12.500	.2	17.500	.1	22.500	.1
3.000	.4	8.000	.2	13.000	.2	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.2	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1	24.500	.0

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

RUNOFF VOLUME = 1.70151 INCHES = 1.4338 ACRE-FEET
 PEAK DISCHARGE RATE = 34.51 CFS AT 1.500 HOURS BASIN AREA = .0158 SQ. MI.

*S-----
 *S ADD AP.5.BYPASS TO 609.ON
 ADD HYD ID=23 HYD=AP.6 IDi=21 IDii=22
 PRINT HYD ID=23 CODE=10

HYDROGRAPH FROM AREA AP.6

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	.2	10.000	.2	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1	21.000	.1
1.500	41.8	6.500	.2	11.500	.2	16.500	.1	21.500	.1
2.000	6.6	7.000	.2	12.000	.2	17.000	.1	22.000	.1
2.500	1.0	7.500	.2	12.500	.2	17.500	.1	22.500	.1
3.000	.4	8.000	.2	13.000	.2	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.2	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.70147 INCHES = 1.4641 ACRE-FEET
 PEAK DISCHARGE RATE = 41.84 CFS AT 1.500 HOURS BASIN AREA = .0161 SQ. MI.

*S-----
 *S DIVIDE AP.6
 *S ID=24 IS 34.60 CFS INTO INLETS
 *S ID=25 IS 7.24 CFS BYPASSING INLET TO BASIN103
 DIVIDE HYD ID=23 Q=34.6 IDi=24 HYD=SYSTEM.400
 IDii=25 HYD=AP.6.BYPASS

*S-----
 *S ADD SYSTEM.300 TO SYSTEM.400
 ADD HYD ID=26 HYD=400.OUTFALL IDi=20 IDii=24
 PRINT HYD ID=26 CODE=10

HYDROGRAPH FROM AREA 400.OUTFALL

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	.4	10.000	.4	15.000	.3	20.000	.2
.500	.0	5.500	.4	10.500	.4	15.500	.3	20.500	.2
1.000	.2	6.000	.4	11.000	.3	16.000	.3	21.000	.2
1.500	69.1	6.500	.4	11.500	.3	16.500	.3	21.500	.2
2.000	13.4	7.000	.4	12.000	.3	17.000	.3	22.000	.2
2.500	2.1	7.500	.4	12.500	.3	17.500	.3	22.500	.2
3.000	.8	8.000	.4	13.000	.3	18.000	.3	23.000	.2
3.500	.5	8.500	.4	13.500	.3	18.500	.3	23.500	.2
4.000	.4	9.000	.4	14.000	.3	19.000	.2	24.000	.2
4.500	.4	9.500	.4	14.500	.3	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.70080 INCHES = 2.9137 ACRE-FEET
 PEAK DISCHARGE RATE = 69.10 CFS AT 1.500 HOURS BASIN AREA = .0321 SQ. MI.

*S-----
 *S COMPUTE ONSITE BASIN 610
 COMPUTE NM HYD ID=27 HYD=610.ON AREA=0.02331 SQ MI
 %A=0 %B=25 %C=25 %D=50 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 46.118 CFS UNIT VOLUME = .9989 B = 526.28 P60 = 1.8000
 AREA = .011655 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 31.034 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .011655 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=27 CODE=10

HYDROGRAPH FROM AREA 610.ON

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	.3	10.000	.3	15.000	.2	20.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2	20.500	.2
1.000	.2	6.000	.3	11.000	.3	16.000	.2	21.000	.2
1.500	50.9	6.500	.3	11.500	.2	16.500	.2	21.500	.2
2.000	9.7	7.000	.3	12.000	.2	17.000	.2	22.000	.2
2.500	1.5	7.500	.3	12.500	.2	17.500	.2	22.500	.2
3.000	.6	8.000	.3	13.000	.2	18.000	.2	23.000	.2

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

3.500	.3	8.500	.3	13.500	.2	18.500	.2	23.500	.2
4.000	.3	9.000	.3	14.000	.2	19.000	.2	24.000	.2
4.500	.3	9.500	.3	14.500	.2	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.70151 INCHES = 2.1153 ACRE-FEET
 PEAK DISCHARGE RATE = 50.91 CFS AT 1.500 HOURS BASIN AREA = .0233 SQ. MI.

*S-----
 *S ADD AP.6.BYPASS TO 610.ON
 ADD HYD ID=28 HYD=AP.7 IDi=25 IDii=27
 PRINT HYD ID=28 CODE=10

HYDROGRAPH FROM AREA AP.7

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	.3	10.000	.3	15.000	.2	20.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2	20.500	.2
1.000	.2	6.000	.3	11.000	.3	16.000	.2	21.000	.2
1.500	58.1	6.500	.3	11.500	.2	16.500	.2	21.500	.2
2.000	9.7	7.000	.3	12.000	.2	17.000	.2	22.000	.2
2.500	1.5	7.500	.3	12.500	.2	17.500	.2	22.500	.2
3.000	.6	8.000	.3	13.000	.2	18.000	.2	23.000	.2
3.500	.3	8.500	.3	13.500	.2	18.500	.2	23.500	.2
4.000	.3	9.000	.3	14.000	.2	19.000	.2	24.000	.2
4.500	.3	9.500	.3	14.500	.2	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.70150 INCHES = 2.1452 ACRE-FEET
 PEAK DISCHARGE RATE = 58.14 CFS AT 1.500 HOURS BASIN AREA = .0236 SQ. MI.

*S-----
 *S DIVIDE AP.7
 *S ID=29 IS 36.50 CFS INTO INLETS
 *S ID=30 IS 23.54 CFS BYPASSING INLET TO SUMP
 DIVIDE HYD ID=28 Q=34.6 IDi=29 HYD=SYSTEM.500A
 IDii=30 HYD=SUMP

*S-----
 *S ADD SYSTEM.500A TO SUMP
 ADD HYD ID=31 HYD=500.OUTFALL IDi=29 IDii=30
 PRINT HYD ID=31 CODE=10

HYDROGRAPH FROM AREA 500.OUTFALL

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	.3	10.000	.3	15.000	.2	20.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2	20.500	.2
1.000	.2	6.000	.3	11.000	.3	16.000	.2	21.000	.2
1.500	58.1	6.500	.3	11.500	.2	16.500	.2	21.500	.2
2.000	9.7	7.000	.3	12.000	.2	17.000	.2	22.000	.2
2.500	1.5	7.500	.3	12.500	.2	17.500	.2	22.500	.2
3.000	.6	8.000	.3	13.000	.2	18.000	.2	23.000	.2
3.500	.3	8.500	.3	13.500	.2	18.500	.2	23.500	.2
4.000	.3	9.000	.3	14.000	.2	19.000	.2	24.000	.2
4.500	.3	9.500	.3	14.500	.2	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.70150 INCHES = 2.1452 ACRE-FEET
 PEAK DISCHARGE RATE = 58.14 CFS AT 1.500 HOURS BASIN AREA = .0236 SQ. MI.

*S-----
 *S ADD 200.OUTFALL TO 400.OUTFALL
 ADD HYD ID=32 HYD=SUBTOTAL.A IDi=17 IDii=26
 PRINT HYD ID=32 CODE=10

HYDROGRAPH FROM AREA SUBTOTAL.A

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	1.0	10.000	1.0	15.000	.8	20.000	.7
.500	.0	5.500	1.1	10.500	1.0	15.500	.8	20.500	.6
1.000	.6	6.000	1.2	11.000	1.0	16.000	.8	21.000	.6
1.500	188.6	6.500	1.2	11.500	.9	16.500	.7	21.500	.6
2.000	36.9	7.000	1.2	12.000	.9	17.000	.7	22.000	.6
2.500	5.8	7.500	1.2	12.500	.9	17.500	.7	22.500	.6
3.000	2.1	8.000	1.1	13.000	.9	18.000	.7	23.000	.6
3.500	1.3	8.500	1.1	13.500	.8	18.500	.7	23.500	.6
4.000	1.0	9.000	1.1	14.000	.8	19.000	.7	24.000	.6
4.500	1.0	9.500	1.0	14.500	.8	19.500	.7	24.500	.0

RUNOFF VOLUME = 1.66301 INCHES = 8.0507 ACRE-FEET
 PEAK DISCHARGE RATE = 188.60 CFS AT 1.500 HOURS BASIN AREA = .0908 SQ. MI.

*S-----
 *S ADD SUBTOTAL.A TO 500.OUTFALL
 ADD HYD ID=33 HYD=SUBTOTAL.B IDi=32 IDii=31
 PRINT HYD ID=33 CODE=10

Cabezon Tract 6A 100-Year 24-Hour Duration Storm-Developed AHYMO Output File

HYDROGRAPH FROM AREA SUBTOTAL.B

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	1.3	10.000	1.3	15.000	1.0	20.000	.8
.500	.0	5.500	1.4	10.500	1.2	15.500	1.0	20.500	.8
1.000	.7	6.000	1.5	11.000	1.2	16.000	1.0	21.000	.8
1.500	246.7	6.500	1.6	11.500	1.2	16.500	.9	21.500	.8
2.000	46.6	7.000	1.5	12.000	1.1	17.000	.9	22.000	.8
2.500	7.3	7.500	1.5	12.500	1.1	17.500	.9	22.500	.8
3.000	2.7	8.000	1.4	13.000	1.1	18.000	.9	23.000	.8
3.500	1.6	8.500	1.4	13.500	1.1	18.500	.9	23.500	.7
4.000	1.3	9.000	1.3	14.000	1.0	19.000	.9	24.000	.7
4.500	1.3	9.500	1.3	14.500	1.0	19.500	.9	24.500	.0

RUNOFF VOLUME = 1.67096 INCHES = 10.1959 ACRE-FEET
 PEAK DISCHARGE RATE = 246.74 CFS AT 1.500 HOURS BASIN AREA = .1144 SQ. MI.

*S-----
 *S ADD SUBTOTAL.B TO BASIN 604
 ADD HYD ID=34 HYD-TOTAL IDi=33 IDii=8
 PRINT HYD ID=34 CODE=10

HYDROGRAPH FROM AREA TOTAL

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	1.3	10.000	1.3	15.000	1.0	20.000	.8
.500	.0	5.500	1.4	10.500	1.2	15.500	1.0	20.500	.8
1.000	.7	6.000	1.5	11.000	1.2	16.000	1.0	21.000	.8
1.500	248.6	6.500	1.6	11.500	1.2	16.500	.9	21.500	.8
2.000	47.0	7.000	1.5	12.000	1.1	17.000	.9	22.000	.8
2.500	7.3	7.500	1.5	12.500	1.1	17.500	.9	22.500	.8
3.000	2.7	8.000	1.4	13.000	1.1	18.000	.9	23.000	.8
3.500	1.6	8.500	1.4	13.500	1.1	18.500	.9	23.500	.8
4.000	1.3	9.000	1.3	14.000	1.1	19.000	.9	24.000	.7
4.500	1.3	9.500	1.3	14.500	1.0	19.500	.9	24.500	.0

RUNOFF VOLUME = 1.67118 INCHES = 10.2739 ACRE-FEET
 PEAK DISCHARGE RATE = 248.64 CFS AT 1.500 HOURS BASIN AREA = .1153 SQ. MI.

*S-----
 FINISH
 NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 12:01:07
 (s0p10h4099T&l6D_)

**Yucatan Del Este at Cabezon Tract 6A
Street Flow and Inlet Calculations Analysis**

Description	Inlet #1				Inlet #2				Notes						
	Q (cfs)	Road Slope	Q Half Street (cfs)	Q	Flow Depth (ft)	Velocity (ft/s)	Depth x Velocity	Inlet Type		Q Inlet (cfs)	Q Bypass (cfs)	Flow Depth (ft)	Inlet Type	Q Inlet (cfs)	Q Bypass (cfs)
Basin 603A	50.65	1.60%	25.33	53.35	0.56	5	2.8	Triple C	15.00	10.33	0.45	Double C	6.8	3.53	Use - 1 Triple + 1 Double C Inlet Battery #1; Bypass to Basin 607B
Basin 603B	10.69	4.04%	5.35	29.14	0.38	4.9	1.9	Single C	3.50	1.85	0.22	Single C	2.2	-0.36	Use - 2 Single C Inlet Battery #2; No Bypass
Basin 607A	58.27	2.97%	29.14	62.8	0.54	7.1	3.8	Triple C	18.75	10.39	0.42	Double C	7.0	3.39	Use - 3 Double C Inlet Battery #3; Bypass to Basin 608B
Basin 607B	12.55	1.60%	6.28	13.30	0.45	3.7	1.7	Double C	6.50	-0.23	0.00	None	0.0	-0.23	Use - 1 Double C Inlet Battery #4; No Bypass
Basin 608A	26.59	1.96%	13.30	7.85	0.39	3.8	1.7	Triple C	12.00	2.60	0.22	None	0.0	0.63	Use - 1 Triple C Inlet Battery #5; Bypass to Basin 609B
Basin 608B	15.69	1.60%	7.85	12.93	0.41	3.1	1.2	Double C	5.25	5.13	0.28	None	0.0	2.60	Use - 1 Double C Inlet Battery #6; Bypass to Basin 610B
Basin 609A	25.85	3.06%	12.93	8.12	0.39	4.5	1.8	Double C	7.80	6.49	0.31	Double C	4.5	0.63	Use - 2 Double C Inlet Battery #7; Bypass to Basin 610B
Basin 609B	16.23	1.60%	8.12	20.74	0.45	3.1	1.2	Double C	5.00	3.12	0.25	None	0.0	3.12	Use - 1 Double C Inlet Battery #8; Bypass to Basin 610B
Basin 610A	41.47	3.99%	20.74	10.67	0.36	6	2.7	Triple C	14.25	6.49	0.32	Double C	4.0	2.49	Use - 1 Triple C + 1 Double C Inlet Battery #9; Bypass to Basin 610 B
Basin 610B	21.34	3.99%	10.67		0.36	4.8	1.7	Sump	9.93	0					Use Sump Inlet Battery #10

Assumptions

1. Street Flow Depths and Velocities taken from City of Albuquerque Plate 22.3 D-1
2. Double C Grate Capacities taken from City of Albuquerque Plate 22.3 D-6
3. Triple C Grate Capacities were extrapolated from the Double C Capacities.
4. All Grate Capacities do not account for curb opening inflow. Therefore, inlet inflows shown are conservative and provide a safety factor for items such as inlet clogging

Yucatan Del Este At Cabezon Tract 6A Subdivision Headloss Calculations

Description	Q1	V1	Q2	V2	X1	X3	Q3	V3	A1	A2	dia1	dia2	Q4	x4	A3	A4	D3	D4
J-101	5.7	14.1	11.4	14.32	90	45	5.7	14.38	1.766	3.140	18	24			1.766	0.000	18	
J-102	21.8	6.94	43.6	20.17	45	45	21.8	6.94	3.140	7.065	24	36			3.140	0.000	24	
J-103	43.6	20.17	55	11.2	90	45	11.4	14.32	7.065	7.065	36	36			3.140	0.000	24	
J-201	25.75	22.72	51.5	17.03	30	45	25.75	22.72	3.140	7.065	24	36			3.140	0.000	24	
J-202	55	11.2	68	9.62	0	45	6.5	3.68	7.065	7.065	36	36	6.5	45	1.766	1.766	18	18
J-203	68	9.62	119.5	16.91	90	15	51.5	17.03	7.065	7.065	36	36			7.065	0.000	36	
J-301	12	6.79	24	6.24	45	45	12	15.69	1.766	4.906	18	30			1.766	0.000	18	
J-302	5.25	2.97	10.5	11.26	30	60	5.25	2.97	1.766	1.766	18	18			1.766	0.000	18	
J-303	24	6.24	34.5	10.87	90	10	10.5	11.26	4.906	4.906	30	30			1.766	0.000	18	
J-401	5	2.83	10	5.66	45	45	5	2.83	1.766	1.766	18	18			1.766	0.000	18	
J-402	12.3	6.96	24.6	10.23	90	0	5	6.96	1.766	3.140	18	24			1.766	0.000	18	
J-403	24.6	10.23	34.6	10.34	40	90	10	5.66	3.140	4.906	24	30			1.766	0.000	18	
J-501	18.25	5.81	36.5	15.76	57	90	18.25	5.81	3.140	7.065	24	36			3.140	0.000	24	

EQUATION FROM MODERN SEWER DESIGN, THIRD EDITION, 1995

Description	Headloss, FT	# PIPES
J-101	0.86	3
J-102	1.33	3
J-103	1.75	3
J-201	1.26	3
J-202	0.92	4
J-203	7.28	3
J-301	1.02	3
J-302	0.72	3
J-303	1.14	3
J-401	0.64	3
J-402	2.76	3
J-403	1.24	3
J-501	1.79	3

CALCULATED K VALUES

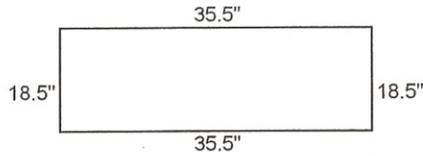
Descr	Angle	coeff	K
I-103	45	0.0033	0.15
I-104	45	0.0033	0.15
I-105	45	0.0033	0.15
I-106	45	0.0033	0.15
I-203	45	0.0033	0.15
I-204	45	0.0033	0.15
J-204	24	0.0033	0.08
J-304	15	0.0033	0.05
J-305	30	0.0033	0.10
I-403	45	0.0033	0.15
I-404	45	0.0033	0.15
J-404	28	0.0033	0.09
I-503	45	0.0033	0.15
I-504	90	0.0033	0.30
I-505	30	0.0033	0.10

Inlet Worksheet (Sump Condition) for Basin 610B

Objective : Design a Double C Inlet in Sump Condition for a 100-year flow of: 23.54 cfs

- 1 Inlet to collect discharge before overtopping curb.
Standard 8" curb and gutter.
Dmax=10.75 in (0.9 ft) - Not 8" because standard inlet has 10.75" depression.

- 2 Grate Dimensions



**Net dimensions of open area of a single grate.
(Total Area less Area of Bars)

Weir Perimeter - Double 'C' = $2 \times 18.5" + 4 \times 35.5" = 14.92$ ft
Area of Orifice - Double 'C' = $18.5" \times (2 \times 35.5") = 9.12$ sq ft

- 3 Calculate Orifice and Weir Flow into Grate at Design Depth (0.9 ft)

Orifice Equation	Weir Equation
$Q = 0.6 \times A \times (2 \times g \times h)^{1/2}$ Where A = 9.120 sq. ft. g = 32.2 ft ^2/sec h = 0.9 ft Therefore Q = 41.65913778 cfs	$Q = 2.65 \times P \times H^{1/2}$ Where P = 14.920 ft H = 0.9 ft Therefore Q = 38 cfs

Weir Equation controls
Double "C" Inlet flow @ TBC = 38 cfs

- 4 Apply 25% Clogging Factor to determine allowable design flow into inlet

$38 \times 0.75 = 28$ cfs

Therefore Capacity of Double C Inlet in Sump Condition = 28 cfs.

Scenario: Base

Combined Pipe/Node Report

Label	Length (ft)	Section Size	Total Flow (cfs)	Full Capacity (cfs)	Average Velocity (ft/s)	Upstream Node	Downstream Node	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Constructed Slope (ft/ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)
P-101	60.00	18 inch	15.00	19.08	11.96	I-101	I-103	5,331.81	5,329.83	0.033000	5,333.22	5,334.64	5,331.86	5,333.66
P-102	60.00	18 inch	15.00	19.08	11.96	I-102	I-104	5,331.81	5,329.83	0.033000	5,333.22	5,334.64	5,331.85	5,333.66
P-103	18.00	24 inch	21.80	55.92	6.94	I-104	J-102	5,329.83	5,328.73	0.061111	5,331.85	5,333.66	5,331.68	5,333.73
P-104	19.00	24 inch	21.80	54.43	6.94	I-103	J-102	5,329.83	5,328.73	0.057895	5,331.86	5,333.66	5,331.68	5,333.73
P-105	53.00	18 inch	3.50	24.27	9.77	I-107	I-106	5,332.83	5,330.00	0.053396	5,333.54	5,335.37	5,330.92	5,333.67
P-106	53.00	18 inch	3.50	24.27	9.77	I-108	I-105	5,332.83	5,330.00	0.053396	5,333.54	5,335.37	5,330.92	5,333.41
P-107	19.00	18 inch	5.70	33.39	14.10	I-106	J-101	5,330.00	5,328.08	0.101053	5,330.92	5,333.67	5,329.60	5,333.08
P-108	18.00	18 inch	5.70	34.31	14.38	I-105	J-101	5,330.00	5,328.08	0.106667	5,330.92	5,333.41	5,329.60	5,333.08
P-109	35.00	24 inch	11.40	57.86	14.32	J-101	J-103	5,328.08	5,325.79	0.065429	5,329.29	5,333.08	5,329.21	5,332.79
P-110	45.00	36 inch	43.60	170.47	20.17	J-102	J-103	5,328.73	5,325.79	0.065333	5,330.88	5,333.73	5,329.21	5,332.79
P-111	168.00	36 inch	55.00	71.85	11.20	J-103	J-202	5,325.79	5,323.84	0.011607	5,328.20	5,332.79	5,327.21	5,330.40
P-201	48.00	24 inch	18.75	37.23	11.87	I-201	I-203	5,328.26	5,326.96	0.027083	5,329.82	5,330.80	5,328.64	5,329.40
P-202	48.00	24 inch	18.75	37.23	11.87	I-202	I-204	5,328.26	5,326.96	0.027083	5,329.82	5,330.80	5,328.64	5,329.40
P-203	22.00	24 inch	25.75	80.12	22.72	I-203	J-201	5,326.86	5,324.10	0.125455	5,328.64	5,329.40	5,326.33	5,329.06
P-204	22.00	24 inch	25.75	80.12	22.72	I-204	J-201	5,326.86	5,324.10	0.125455	5,328.64	5,329.40	5,326.33	5,329.06
P-205	16.00	18 inch	6.50	8.71	3.68	I-205	J-202	5,323.75	5,323.64	0.006875	5,327.27	5,330.19	5,327.21	5,330.40
P-206	17.00	18 inch	6.50	15.29	3.68	I-206	J-202	5,324.00	5,323.64	0.021176	5,327.28	5,330.19	5,327.21	5,330.40
P-207	89.00	36 inch	68.00	67.07	9.62	J-202	J-203	5,323.74	5,322.84	0.010112	5,327.21	5,330.40	5,326.29	5,328.97
P-208	32.00	36 inch	51.50	126.98	17.03	J-201	J-203	5,324.00	5,322.84	0.036250	5,326.33	5,329.06	5,326.29	5,328.97
P-209	132.00	36 inch	119.50	111.06	16.91	J-203	J-204	5,322.74	5,319.08	0.027727	5,326.29	5,328.97	5,322.03	5,327.40
P-210	128.00	36 inch	119.50	144.16	22.80	J-204	O-200	5,318.98	5,313.00	0.046719	5,321.93	5,327.40	5,315.25	5,320.00

D-1

Scenario: Base

Combined Pipe\Node Report

Label	Length (ft)	Section Size	Total Flow (cfs)	Full Capacity (cfs)	Average Velocity (ft/s)	Upstream Node	Downstream Node	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Constructed Slope (ft/ft)	Hydraulic Grade Line In (ft)	Upstream Ground Elevation (ft)	Hydraulic Grade Line Out (ft)	Downstream Ground Elevation (ft)
P-301	17.00	18 inch	12.00	29.05	6.79	I-301	J-301	5,318.14	5,316.84	0.076471	5,319.79	5,322.64	5,319.57	5,322.34
P-302	20.00	18 inch	12.00	29.15	15.69	I-302	J-301	5,318.38	5,316.84	0.077000	5,319.80	5,322.88	5,319.57	5,322.34
P-303	29.00	18 inch	5.25	5.52	2.97	I-303	J-302	5,318.34	5,318.26	0.002759	5,320.20	5,322.84	5,320.13	5,322.97
P-304	16.00	18 inch	5.25	9.83	2.97	I-304	J-302	5,318.40	5,318.26	0.008750	5,320.17	5,322.90	5,320.13	5,322.97
P-305	46.00	18 inch	10.50	19.56	11.26	J-302	J-303	5,318.26	5,316.67	0.034674	5,319.51	5,322.97	5,319.15	5,322.42
P-306	40.00	30 inch	24.00	27.13	6.24	J-301	J-303	5,316.84	5,316.67	0.004375	5,319.27	5,322.34	5,319.15	5,322.42
P-307	64.00	36 inch	34.50	79.75	10.87	J-303	J-304	5,316.67	5,315.75	0.014297	5,318.57	5,322.42	5,318.05	5,321.38
P-308	75.00	36 inch	34.50	111.34	13.89	J-304	J-305	5,315.65	5,313.56	0.027867	5,317.56	5,321.38	5,316.73	5,320.16
P-309	217.00	36 inch	34.50	54.33	8.14	J-305	J-401	5,313.46	5,312.02	0.006636	5,316.23	5,320.16	5,315.68	5,316.60
P-400	50.00	15 inch	7.80	11.70	6.36	I-401	I-403	5,313.51	5,311.87	0.032800	5,316.99	5,317.76	5,316.26	5,316.37
P-401	50.00	15 inch	7.80	12.49	6.36	I-402	I-404	5,313.51	5,311.64	0.037400	5,316.87	5,317.76	5,316.14	5,316.14
P-402	22.00	18 inch	12.30	18.19	6.96	I-403	J-402	5,311.87	5,311.21	0.030000	5,316.26	5,316.37	5,315.96	5,315.96
P-403	23.00	18 inch	12.30	14.36	6.96	I-404	J-402	5,311.64	5,311.21	0.018696	5,316.28	5,316.14	5,315.96	5,315.96
P-405	40.00	21 inch	24.60	25.42	10.23	J-402	J-403	5,311.21	5,310.18	0.025750	5,315.74	5,315.96	5,314.77	5,315.68
P-406	19.00	18 inch	5.00	8.17	2.83	I-405	J-401	5,312.03	5,311.92	0.006053	5,315.73	5,316.53	5,315.68	5,316.60
P-407	17.00	18 inch	5.00	8.64	2.83	I-406	J-401	5,312.03	5,311.92	0.006765	5,315.72	5,316.53	5,315.68	5,316.60
P-408	66.00	36 inch	44.50	108.14	6.30	J-401	J-403	5,311.92	5,310.18	0.026288	5,315.07	5,316.60	5,314.77	5,315.68
P-409	132.00	36 inch	69.10	75.24	9.78	J-403	J-404	5,310.18	5,308.50	0.012727	5,313.58	5,315.68	5,312.17	5,314.00
P-410	77.00	36 inch	69.10	212.14	26.83	J-404	O-400	5,308.50	5,300.71	0.101169	5,311.15	5,314.00	5,302.06	5,310.00
P-501	48.00	18 inch	14.25	26.26	15.16	I-501	I-503	5,310.09	5,307.09	0.062500	5,311.48	5,314.59	5,309.66	5,312.59
P-502	50.00	18 inch	14.25	25.86	14.99	I-502	I-504	5,309.52	5,306.49	0.060600	5,310.91	5,314.02	5,309.58	5,311.99
P-503	30.00	24 inch	18.25	33.93	5.81	I-503	J-501	5,307.09	5,306.42	0.022500	5,309.66	5,312.59	5,309.47	5,312.18
P-504	17.00	24 inch	18.25	15.03	5.81	I-504	J-501	5,306.49	5,306.42	0.004412	5,309.58	5,311.99	5,309.47	5,312.18
P-505	148.00	30 inch	36.50	80.24	15.96	J-501	I-505	5,306.42	5,300.75	0.038277	5,308.46	5,312.18	5,303.11	5,306.15
P-506	160.00	36 inch	57.84	109.46	15.70	I-505	O-500	5,300.65	5,296.34	0.026937	5,303.11	5,306.15	5,297.94	5,305.00

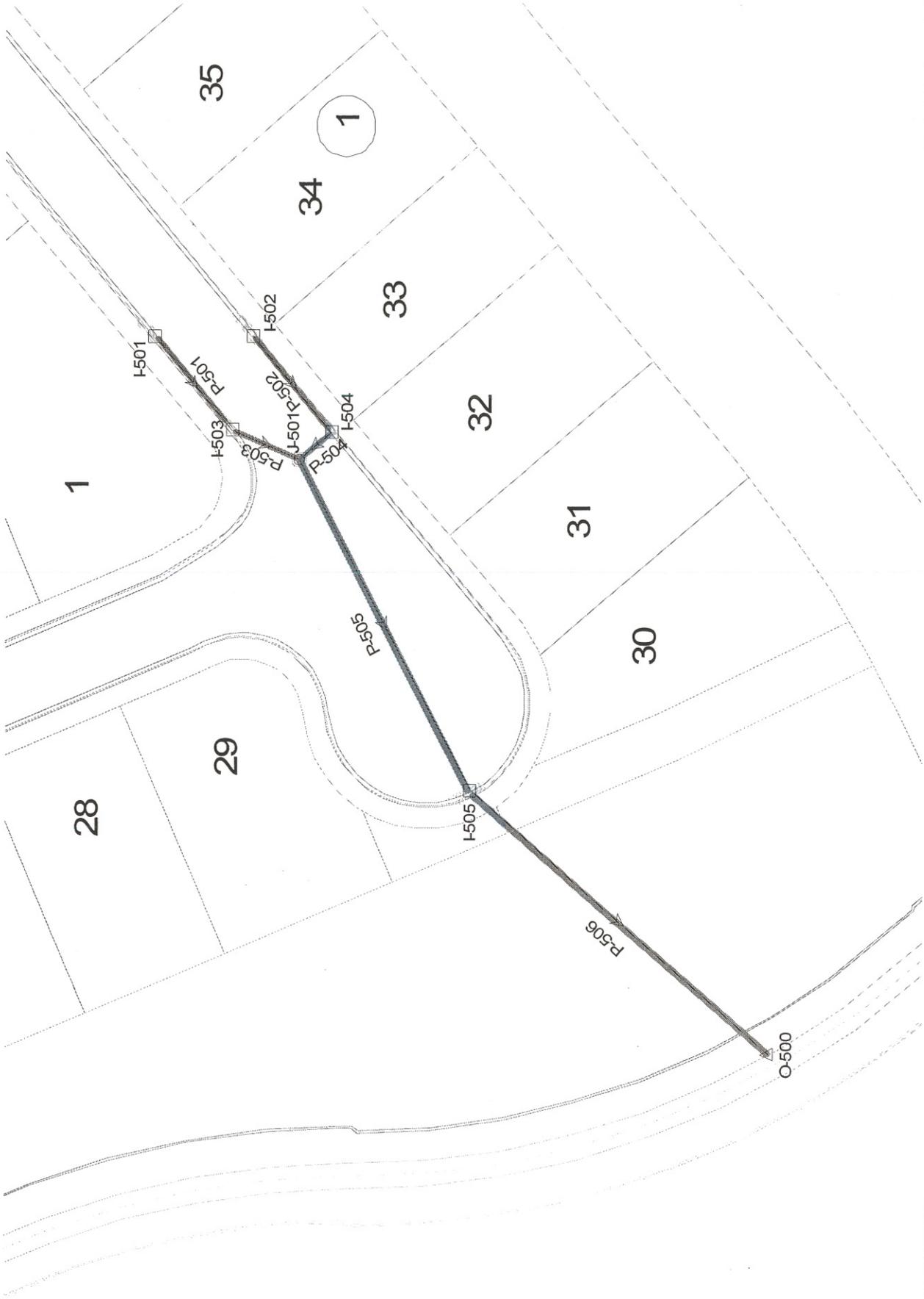
D-3

Scenario: Base



D-4

Scenario: Base



D-5