

**FINAL
DRAINAGE STUDY**

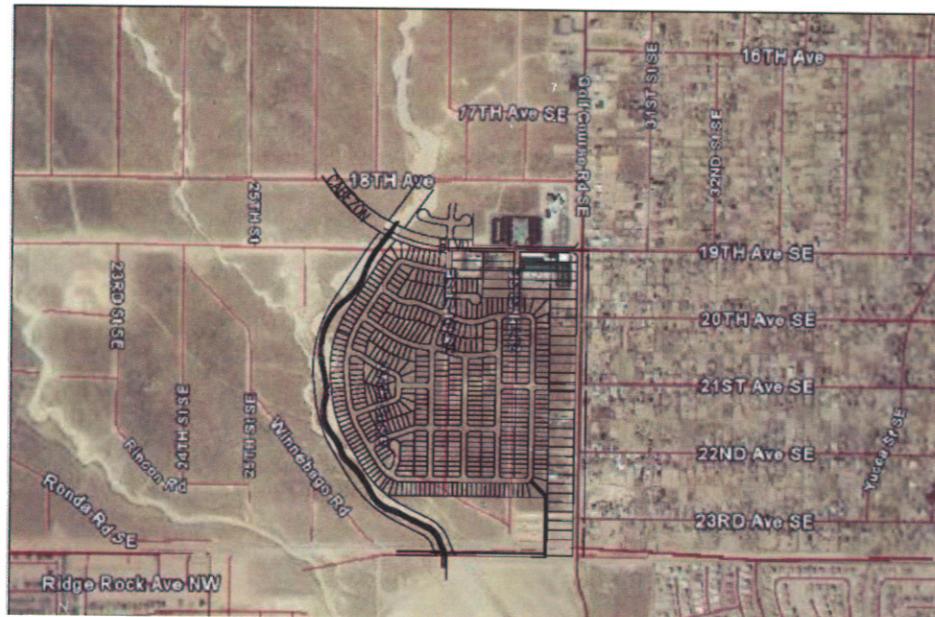
CABEZON TRACT 10A

*Rio Rancho Estates Unit 16
Rio Rancho, New Mexico*

for

**CURB NORTH, INC
5160 SAN FRANCISCO NE
ALBUQUERQUE, NEW MEXICO 87109**

March 3, 2006



Prepared By:

HUITT-ZOLLARS, Inc.
333 RIO RANCHO DRIVE NE, SUITE 101
RIO RANCHO, NEW MEXICO
(505) 892-5141

**CITY OF RIO RANCHO
DEPARTMENT OF
PUBLIC INFRASTRUCTURE
APPROVED: *[Signature]***

DATE: *10-16-04*

**DRAINAGE STUDY
FOR
TRACT 10A SUBDIVISION**

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FINAL DRAINAGE STUDY FOR TRACT 10A SUBDIVISION

PURPOSE

This drainage report addresses the storm water runoff and proposed infrastructure needed to convey the runoff from the Tract 10A Subdivision of the Cabezon Redevelopment. This report will also demonstrate that the development of this project complies with the approved Cabezon Communities Phase II Drainage Management Plan and the Cabezon Communities Drainage Implementation Plan.

PROJECT LOCATION AND DESCRIPTION

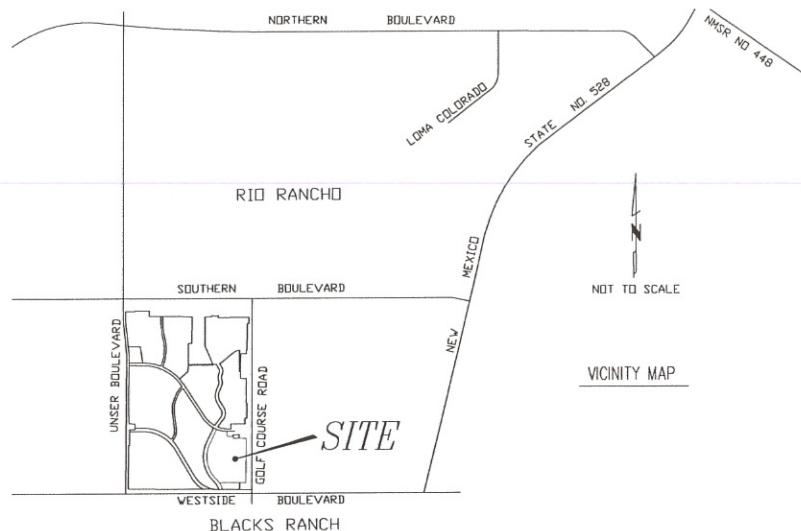


Exhibit 1 – Vicinity Map

The project is located at the southeast corner of the Cabezon Subdivision. The tract is at the northwest corner of the intersection of Westside Boulevard and Golf Course Road within Unit 16 of Rio Rancho Estates, City of Rio Rancho; see **Exhibit 1**. The site is currently undeveloped and in its natural condition. The east branch of the Blacks Arroyo is currently being hard lined to the west of the development. Cabezon Blvd. is being constructed to the north of the development. The development is bound by; Westside Blvd. to the south, Golf Course Road to the east, Cabezon Blvd. to the north and the East Branch Channel of the Blacks Arroyo to the west.

ZONING AND PLATTING STATUS

The zoning for this project is R-4, Single Family Residential, of approximately 78.19 acres. The project is located in Tract 10A within Rio Rancho Estates Unit 16. This report is an attachment to the Final Plat Submittal for this project.

FLOOD HAZARD ZONES

Per FEMA's Flood Insurance Rate Map (FIRM) 35043C0894 C, dated July 16, 1996, a portion of the project site is located within a FEMA 100-year Flood Hazard Zone. See **Appendix A-1**. Wilson & Co. is under contract with the developer for the corresponding CLOMR and LOMR needed to reconfigure the existing flood zone. The CLOMR has been submitted to FEMA by Wilson & Co. per discussions with the City of Rio Rancho, the developer has agreed to restrict building permit requests for the lots that are located within the current FEMA Floodplain. Once the CLOMR/LOMR process has revised the Floodplain, the developer can proceed with building permits for the affected lots. Refer to **Appendix A-2** for an exhibit indicating the affected lots.

JURISDICTIONS OF PUBLIC AGENCIES

Local

This project is located entirely within the City of Rio Rancho (CoRR) Municipal Limits and is therefore within their jurisdiction and must comply with the City's development requirements.

Regional

This project is located within the jurisdiction of the Southern Sandoval County Arroyo Flood Control Authority (SSCAFCA) and is therefore subject to their review.

RELATED REPORTS

The **Cabezon Communities Phase II Drainage Management Plan** prepared by Wilson & Company, Engineers & Architects and dated August 2004, provides an overall master plan for this area. This report has been approved by the City and SSCAFCA. It determined the pre-developed drainage patterns of this development and the design parameters for the buildup of the subdivision. However, this study only gave a conceptual design for the Tract 10A Subdivision.

The **Cabezon Communities Drainage Implementation Plan** prepared by Wilson & Company, Engineers & Architects and dated February 19, 2004, provides permissible discharge rates for individual tracts as well as offsite flow rates entering individual tracts.

METHODOLOGY

This drainage study is based on the procedures outlined in the CoRR's "Grading and Drainage Design Requirements and Policies for Land Development in Rio Rancho (Revised 3-18-93)." That policy states, "The minimum criteria for hydrology and hydraulic calculations and design shall be as described in the Development Process Manual Section 22.2, City of Albuquerque (CoA DPM), latest revision, or the AHYMO version of the ARS HYMO Computer Program." This drainage study follows the

procedures outlined in both the CoA DPM Section 22.2 and the AHYMO Computer Program.

PRECIPITATION

This project will not utilize an on-site detention pond. Storm water will be conveyed through underground pipe systems that will discharge into the East Branch of the Blacks Arroyo at two separate locations. The 100-yr 24-hr design storm was used for this analysis. The AHYMO Computer Program requires the 1, 6 and 24-hour precipitation values. These values were obtained from the **Cabezon Communities Phase II Drainage Management Plan** and are shown on **Table 1**.

Table 1
Precipitation Values

Return Period (yrs)	24 hr Rainfall (in)	6 hr Rainfall (in)	1 hr Rainfall (in)
100	2.7	2.2	1.8

LAND TREATMENTS

The land treatments used in the AHYMO Computer model are as described by Table A-4 of the CoA DPM Section 22.2, 1993 revision, and are summarized in **Table 2**.

Table 2
Land Treatment Classifications

Treatment	Land Condition
A	Soil uncompacted by human activity with 0 to 10 percent slopes. Native grasses, weeds and shrubs in typical densities with minimal disturbance to grading, groundcover and infiltration capacity. Croplands. Unlined Arroyos.
B	Irrigated lawns, parks and golf courses with 0 to 10 percent slopes. Soil uncompacted by human activity with slopes greater than 10 percent and less than 20 percent.
C	Soil compacted by human activity. Unpaved parking, roads and trail. Most vacant lots. Gravel or rock on plastic (desert landscaping)
D	Impervious areas, pavement and roofs.

Table A-5 of the CoA DPM Section 22.2, 1993 revision summarizes the Percent of Treatment D with a corresponding land use. Since this project site is a Single Family Residential Subdivision, the corresponding Percent of Treatment D is determined by the equation: $7*((N^*N)+(5*N))^{0.5}$ where, N=units/acre (N=456units/78.19=5.83). The remaining was split between Treatment B and C. Therefore the Land Treatments for this site are as follows: %A = 0, %B = 22.2, %C = 22.2, and %D = 55.6.

STREET AND INLET CAPACITY CALCULATIONS

Both street and inlet capacities were calculated using the plates in the **City of Albuquerque DPM**. Tract 10A Subdivision incorporated flow splits into the creation of each actual drainage basin. See **Appendix C** for additional information.

STORM DRAIN HYDRAULICS

Storm Drains were modeled using Haestad Method's "StormCad" software (see Appendix C). Headlosses were calculated using the procedures outlined in the **City of Albuquerque DPM**. The storm drain was designed based on peak discharges as indicated in the AHYMO model and the storm drain design is included in **Appendix D**.

PRE-DEVELOPMENT CONDITIONS

This project site is in its pre-development condition with existing natural vegetation throughout the site. The project site naturally slopes from northeast to the southwest across the site. The project is bounded by commercial properties to the east. These lots currently drain into the project site. The project is bounded to the west by the East Branch of the Blacks Arroyo. The Arroyo is concrete lined and on-site runoff sheet flows across the site and concentrates into it. The runoff discharges through Unit 16 of Rio Rancho Estates, crosses into Bernalillo County and into the Blacks Arroyo Dam.

INTERIM DEVELOPED CONDITIONS

The commercial properties to the east make up **Basin 201**. Based on discussions with the City of Rio Rancho, **Basin 201** will drain to a temporary retention pond in **Tract 10B** via a temporary concrete drainage swale. This swale will be contained within parallel easements on both properties. When the storm drain in Westside Blvd. is constructed the runoff from **Basin 201** will be conveyed to that system. See **Exhibit 3** for details of the drainage swale and **Appendix C** for hydraulic calculations.

ULTIMATE DEVELOPED CONDITIONS

The runoff from **Basin 101** will enter **Basin 102** at **Analysis Point #1**. Their runoff will combine to create **Analysis Point #2**. At this point most of the runoff from these basins will drain into the beginning of storm drain **System #200**. The remaining runoff will bypass and combine with **Basin 103** at **Analysis Point #3**. **Basin 103** will enter **Basin 104** and combine to create **Analysis Point #4**. This flow will enter **Basin 109** and drain into the second battery of inlets as part of storm drain **System #200** (**Analysis Point #9**). The remaining flows will bypass to a sump inlet (**Analysis Point #10**).

The runoff from **Basin 105** will enter **Basin 106** at **Analysis Point #5**. Their runoff will combine to create **Analysis Point #6**. At this point most of the runoff from these basins will drain into storm drain **System #100**. The remaining will bypass into **Basin 107**. **Basin 107** will drain into **Basin 108** at **Analysis Point #7**. These flows will combine and

drain into storm drain **System #300** at **Analysis Point #8**. The remaining flows will bypass to the sump inlet at **Analysis Point #10**.

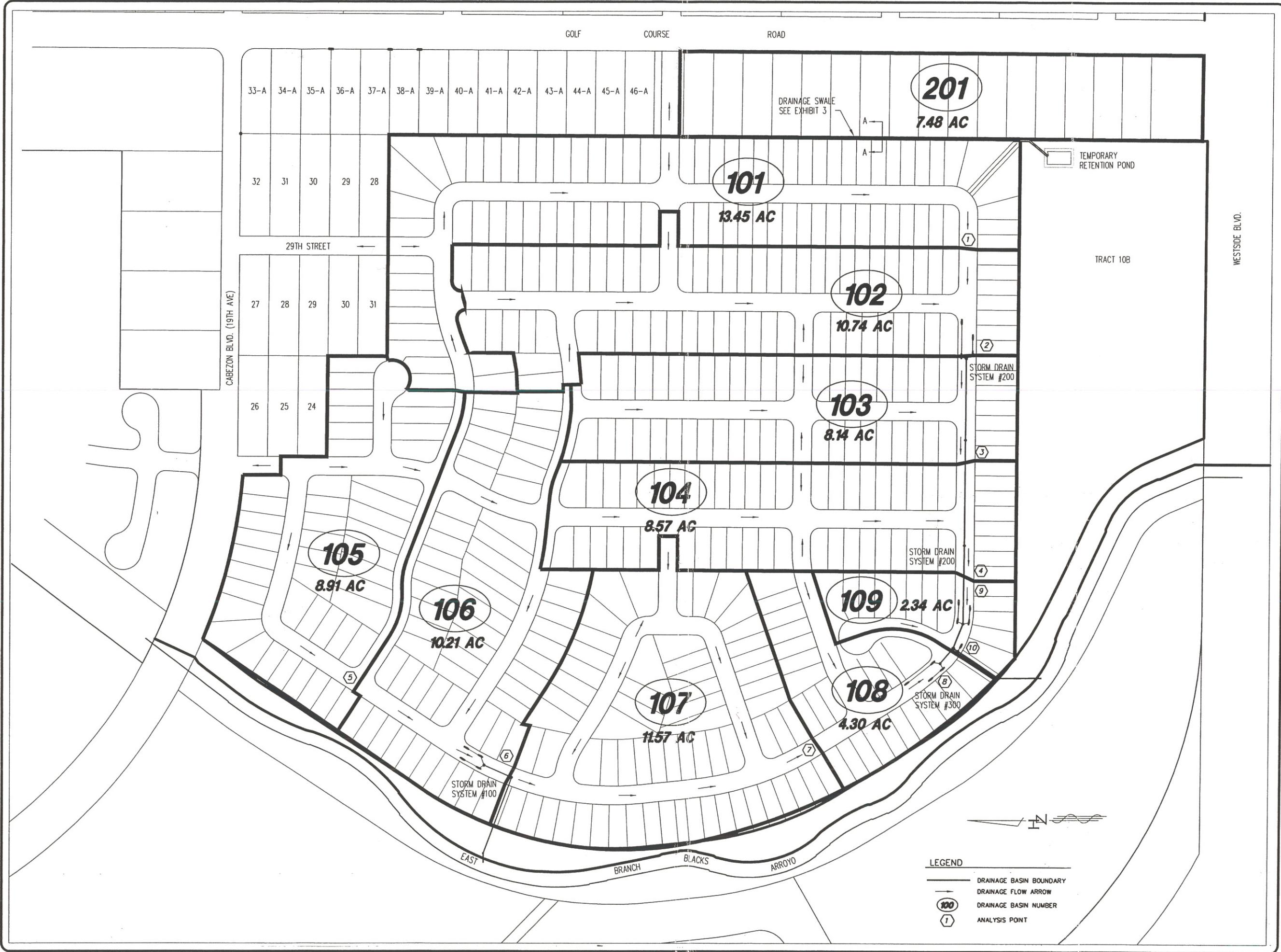
CONCLUSION

Table 3 compares the findings of the analysis of the Tract 10A Subdivision with the results of both the approved **Cabezon Communities Phase II Drainage Management Plan** and the **Cabezon Communities Drainage Implementation Plan**

Table 3
Runoff Comparison for Tract 6A

Description	Basin Area (Mi ²)	Time to Peak (hr)	100-Yr Runoff Volume (Ac-ft)	100-Yr Peak Discharge (Ft ³ /s)
Wilson & Co. DMP	0.130	1.50	12.60	301
Wilson & Co. DIP	0.130	1.50	12.60	295
HZI Plan	0.122	1.50	11.74	275

The Wilson & Co. DMP allows for 301 cfs to flow directly from Tract 10A. The total discharge from the developed subdivision is 275 cfs. Therefore this report does comply with the **Cabezon Communities Phase II Drainage Management Plan** and the **Cabezon Communities Drainage Implementation Plan**.



NO.	REVISION
DATE	

Designed By	HUTT-ZOLLARS
Hutt-Zollars, Inc.	Rio Rancho
333 Rio Rancho Drive NE, Suite 101	Phone (505) 892-3259
Rio Rancho, New Mexico 87124	Fax (505) 892-3259
Designed For:	

CURB NORTH, INC.

BASIN MAP

**CABEZON REDEVELOPMENT
TRACT 10A SUBDIVISION**

DATE: NOV. 2, 2005
DRAWN: RJS
DESIGNED: RJS
CHECKED: JLL
PROJ. NO: 17-0575-01

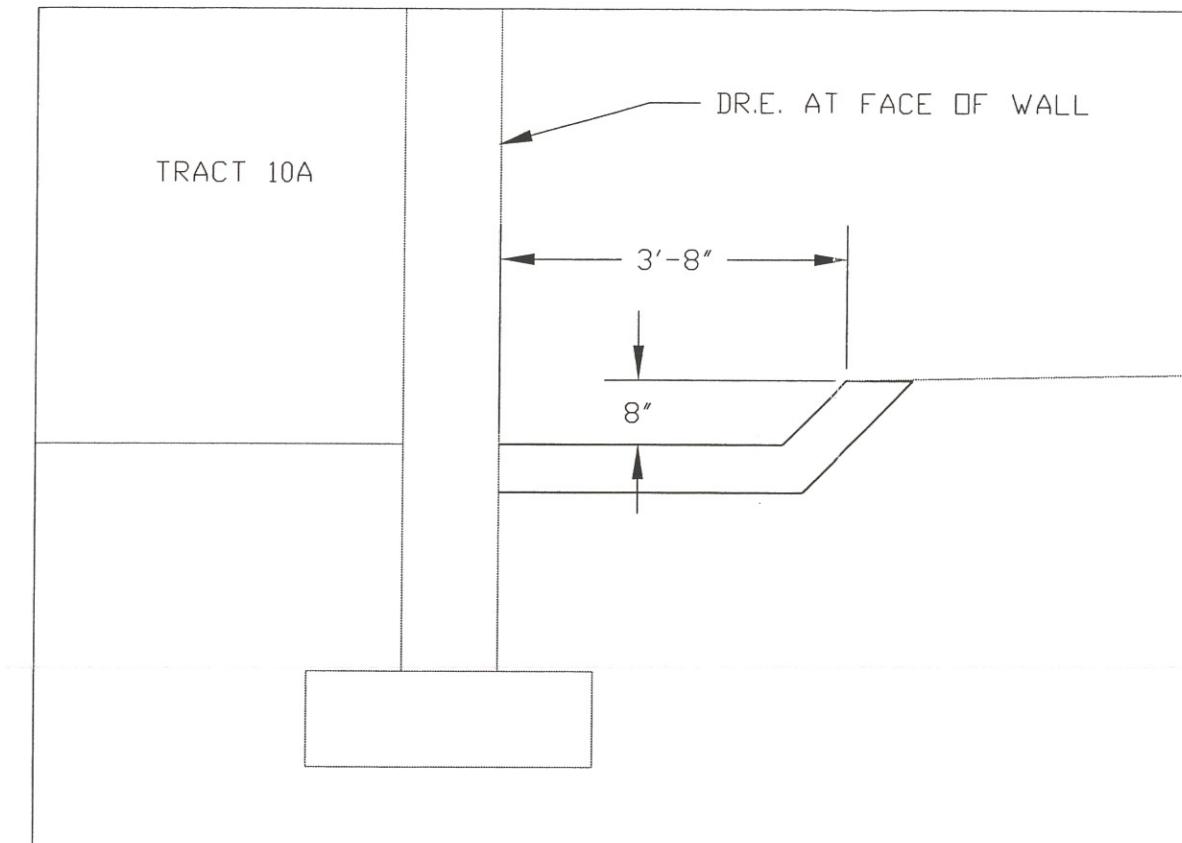
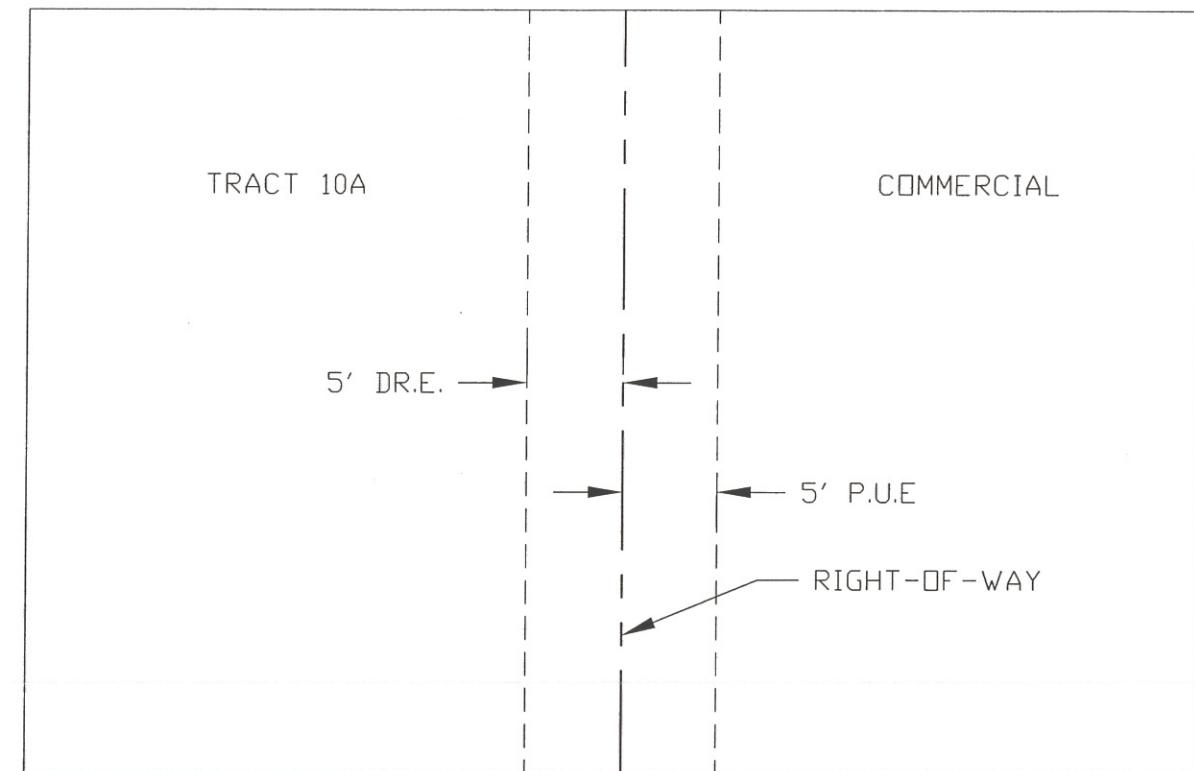


EXHIBIT 3

Designed For:

CURB NORTH, INC.

DRAINAGE SWALE DETAIL

**CABEZON TRACT 10A
RIO RANCHO, NM**

Designed By:

HUITT-ZOLLARS

Huitt-Zollars, Inc.
333 Rio Rancho Drive NE, Suite 101
Rio Rancho, New Mexico 87124
Phone (505) 892-5141 Fax (505) 892-3259

FIRM
FLOOD INSURANCE RATE MAP

SANDOVAL COUNTY,
NEW MEXICO AND
INCORPORATED AREAS

(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
RIO RANCHO, CITY OF	350146	0894	C

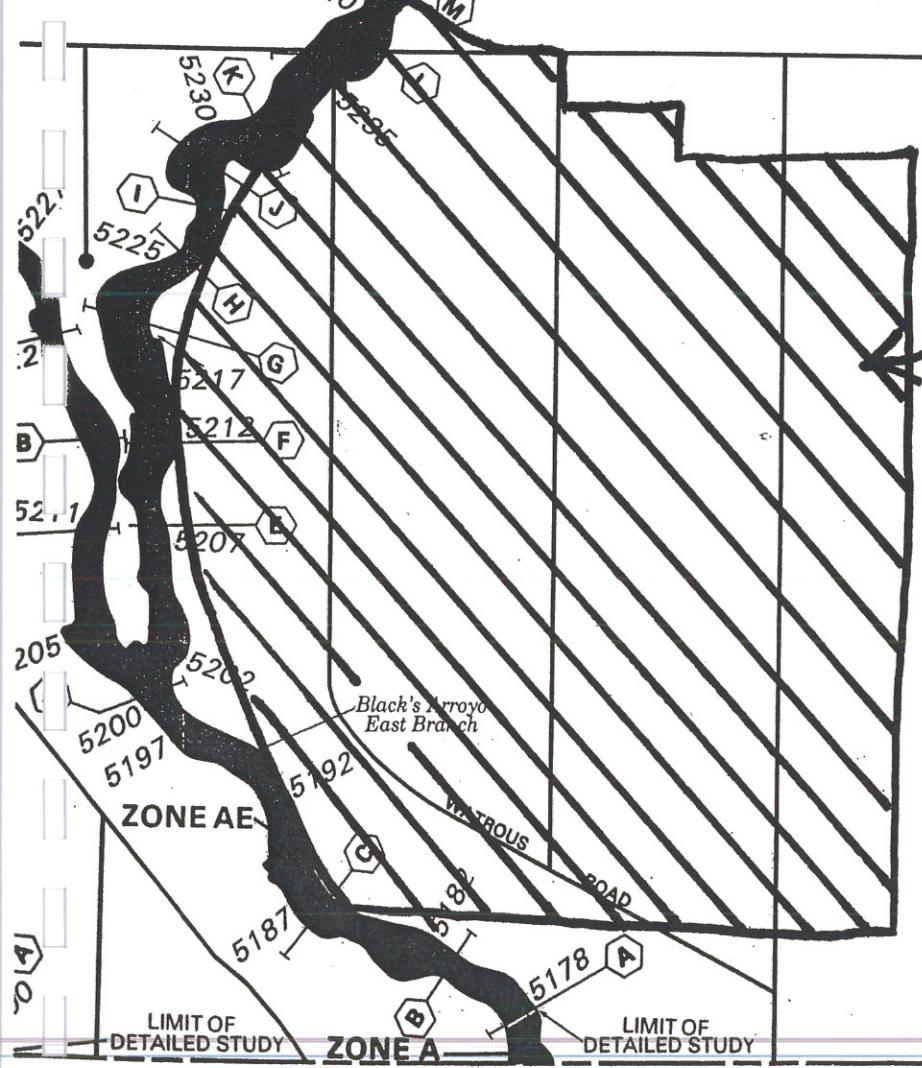
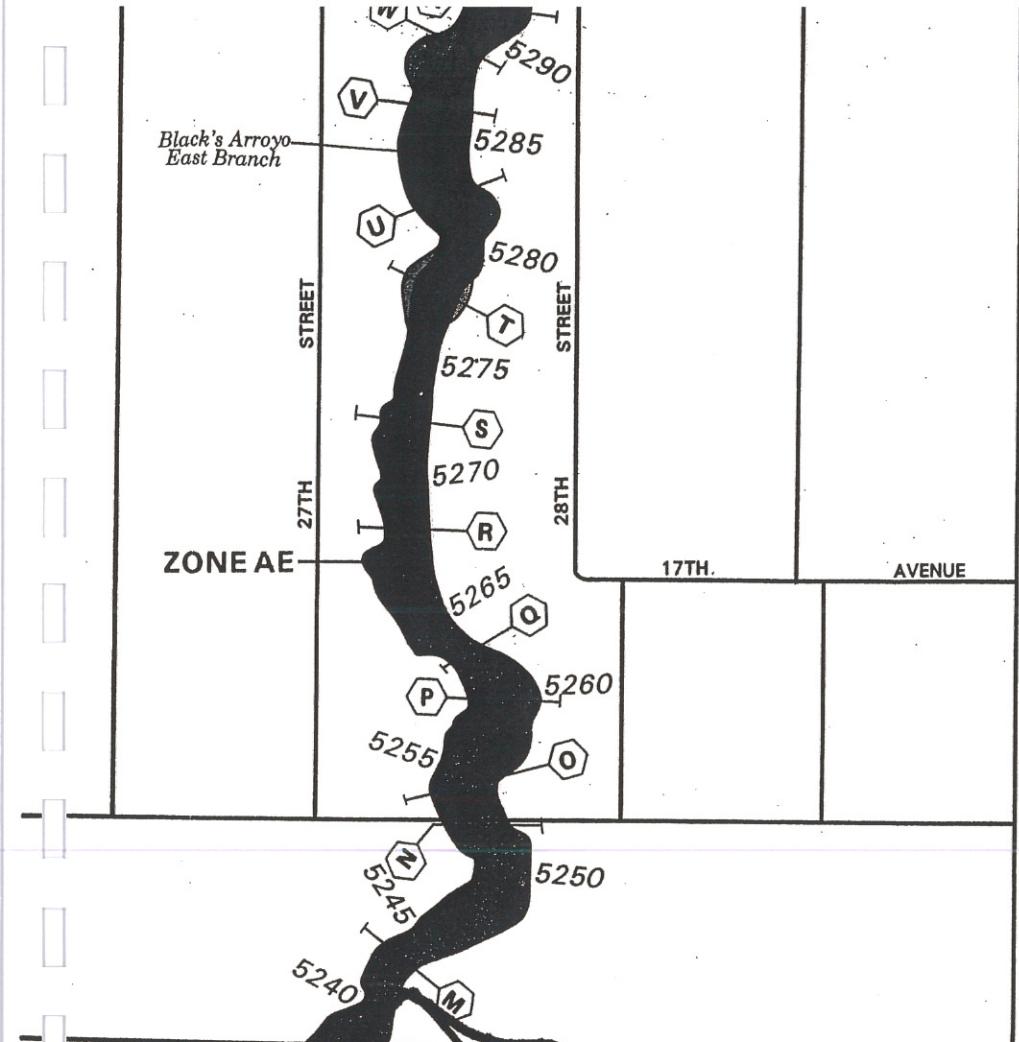
MAP NUMBER
35043C0894 C

EFFECTIVE DATE:
JULY 16, 1996



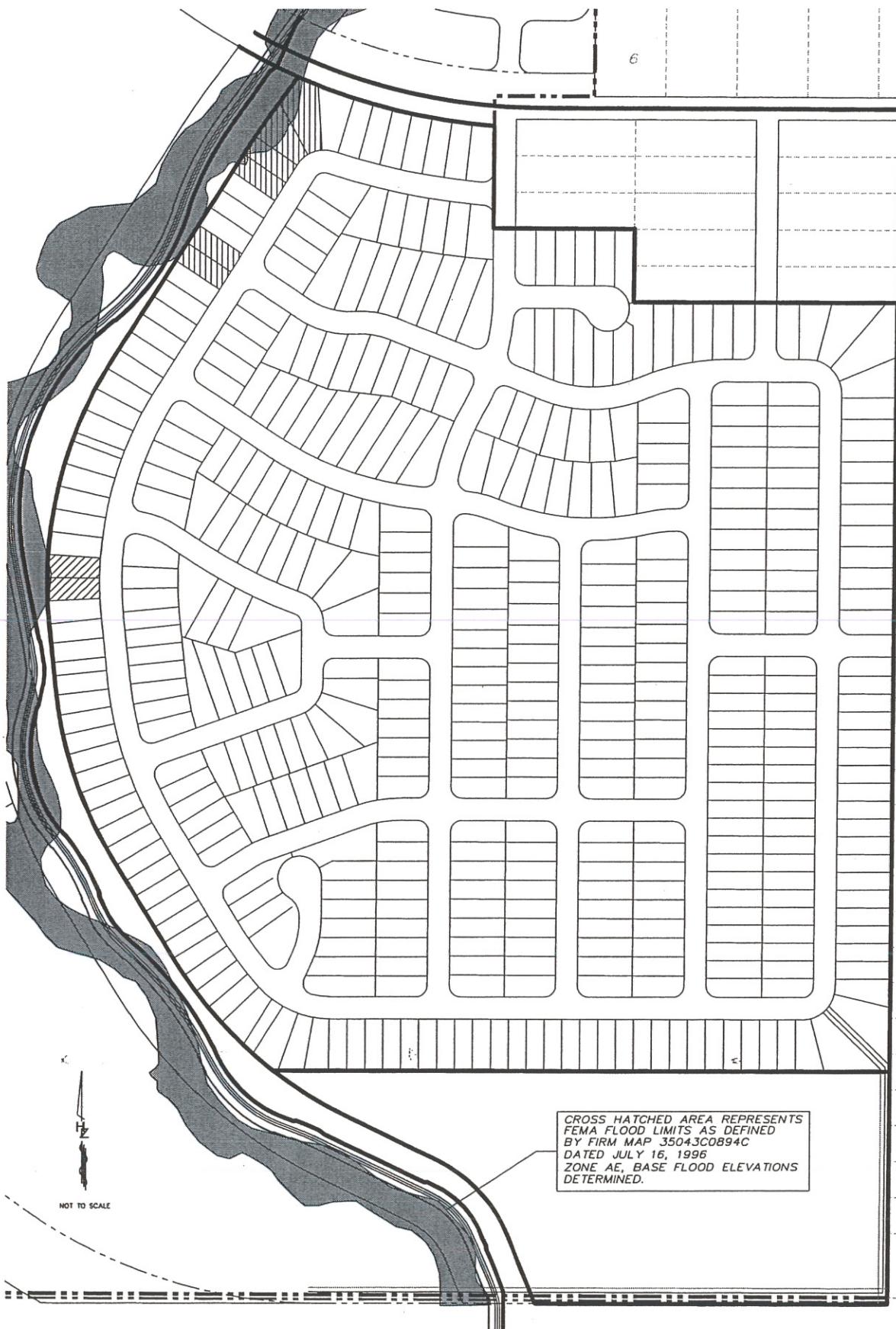
Federal Emergency Management Agency

Project
Area



A-1

T. 12 N.



Designed For:

CURB NORTH, LLC

EXISTING FEMA FLOOD ZONE
TRACT 10A CABEZON REDEVELOPMENT
NOVEMBER 2005

Designed By:

HUITT-ZOLLARS
Huitt-Zollars, Inc.
333 Rio Rancho Drive NE, Suite 101
Rio Rancho, New Mexico 87124
Phone (505) 862-5141 Fax (505) 862-3259

A-2

Cabezon Tract 10A
100-Year 24-Hour Duration Storm-Developed
AHYMO Summary File

(s16.67h8.5v0T_&18D
AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
INPUT FILE = G:\Proj\1705751\DRN_ST-1\AHYMO\CAB10A-1.DAT
- VERSION: 1997.02C RUN DATE (MON/DAY/YR) =09/26/2006
USER NO.= AHYMO-I-9702a01000150-SH

COMMAND	HYDROGRAPH IDENTIFICATION	FROM NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION
START LOCATION	RIO RANCHO									TIME= .00
*S	CABEZON TRACT 10A									
*S	FN:CAB10_DEV.DAT - HYMO PER JAN 1997 DPM REVISIONS									
*S										
*S	RAINFALL TYPE= 2									RAIN24= 2.700
*S	*****									
*S	BULK FOR SEDIMENT - DEVELOPED									
*S	SEDIMENT BULK									
*S	-----									
*S	COMPUTE ONSITE BASIN 101									
COMPUTE NM HYD	101.00 - 1	.02102	47.33	2.018	1.80021	1.500	3.518 PER IMP= 55.60			
*S	-----									
*S	COMPUTE ONSITE BASIN 102									
COMPUTE NM HYD	102.00 - 2	.01678	37.78	1.611	1.80021	1.500	3.518 PER IMP= 55.60			
*S	-----									
*S	ADD 101 TO 102									
ADD HYD	AP.2 1& 2 3	.03780	85.11	3.629	1.80019	1.500	3.518			
*S	-----									
*S	DIVIDE AP.2									
*S	ID=4 IS 68.00 CFS INTO INLETS									
*S	ID=5 IS 17.11 CFS BYPASSING INLET TO BASIN103									
DIVIDE HYD	AP.2.TO.INLE 3 4	.03649	68.00	3.503	1.80019	1.450	2.912			
	AP.2.BYPASS and 5	.00131	17.11	.126	1.80019	1.500	20.355			
*S	-----									
*S	COMPUTE ONSITE BASIN 103									
COMPUTE NM HYD	103.00 - 6	.01272	28.64	1.221	1.80021	1.500	3.519 PER IMP= 55.60			
*S	-----									
*S	ADD 103 TO AP.2.BYPASS									
ADD HYD	AP.3 5& 6 7	.01403	45.76	1.347	1.80018	1.500	5.095			
*S	-----									
*S	COMPUTE ONSITE BASIN 104									
COMPUTE NM HYD	104.00 - 8	.01339	30.15	1.286	1.80021	1.500	3.519 PER IMP= 55.60			
*S	-----									
*S	ADD 104 TO AP.3									
ADD HYD	AP.4 7& 8 9	.02742	75.91	2.633	1.80019	1.500	4.325			
*S	-----									
*S	COMPUTE ONSITE BASIN 105									
COMPUTE NM HYD	105.00 - 10	.01392	31.35	1.336	1.80021	1.500	3.518 PER IMP= 55.60			
*S	-----									
*S	COMPUTE ONSITE BASIN 106									
COMPUTE NM HYD	106.00 - 11	.01595	35.92	1.531	1.80021	1.500	3.518 PER IMP= 55.60			
*S	-----									
*S	ADD 105 TO 106									
ADD HYD	AP.5 10&11 12	.02987	67.26	2.868	1.80019	1.500	3.518			
*S	-----									
*S	DIVIDE AP.6									
*S	ID=13 IS 52.00 CFS INTO INLETS									
*S	ID=14 IS 15.26 CFS BYPASSING INLET TO BASIN103									
DIVIDE HYD	#100 12 13	.02861	52.00	2.747	1.80019	1.450	2.840			
	AP.6.BYPASS and 14	.00126	15.26	.121	1.80019	1.500	18.887			
*S	-----									
*S	COMPUTE ONSITE BASIN 107									
COMPUTE NM HYD	107.00 - 15	.01808	40.71	1.736	1.80021	1.500	3.518 PER IMP= 55.60			
*S	-----									
*S	ADD 107 TO AP.6.BYPASS									
ADD HYD	AP.7 14&15 16	.01934	55.97	1.857	1.80019	1.500	4.521			
*S	-----									
*S	COMPUTE ONSITE BASIN 108									
COMPUTE NM HYD	108.00 - 17	.00672	15.14	.645	1.80021	1.500	3.521 PER IMP= 55.60			
*S	-----									
*S	COMPUTE ONSITE BASIN 109									
COMPUTE NM HYD	109.00 - 18	.00366	8.25	.351	1.80021	1.500	3.523 PER IMP= 55.60			
*S	-----									
*S	ADD 108 TO AP.7									

Cabezon Tract 10A
100-Year 24-Hour Duration Storm-Developed
AHYMO Summary File

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION
ADD HYD	AP.8 16&17	19		.02606	71.11	2.502	1.80019	1.500	4.263	
*S-										
*S ADD 109 TO AP.4										
ADD HYD	AP.9 18& 9	20		.03108	84.16	2.984	1.80018	1.500	4.231	
*S-										
*S DIVIDE AP-8										
*S ID=21 IS 54.00 CFS INTO INLETS										
*S ID=22 IS 17.11 CFS BYPASSING TO SUMP										
DIVIDE HYD	AP.8 TO INLE	19 21		.02515	54.00	2.415	1.80019	1.450	3.355	
	AP.8.BYPASS and	22		.00091	17.11	.088	1.80018	1.500	29.267	
*S-										
*S DIVIDE AP-9										
*S ID=23 IS 60.00 CFS INTO INLETS										
*S ID=24 IS 24.16 CFS BYPASSING TO SUMP										
DIVIDE HYD	AP.9.TO.INLE	20 23		.02957	60.00	2.839	1.80018	1.450	3.171	
	AP.9.BYPASS and	24		.00152	24.16	.146	1.80018	1.500	24.868	
*S-										
*S ADD SUMP INLET TOTAL										
ADD HYD	AP.10 22&24	25		.00243	41.27	.233	1.80018	1.500	26.521	
*S-										
*S ADD INLET FLOWS										
ADD HYD	#200A 4&21	26		.06164	122.00	5.918	1.80019	1.450	3.093	
*S-										
*S ADD INLET FLOWS										
ADD HYD	#300 23&25	27		.03200	101.27	3.072	1.80018	1.500	4.945	
*S-										
*S ADD SOUTH OUTFALL										
ADD HYD	#200 26&27	28		.09363	223.27	8.990	1.80019	1.500	3.726	
*S-										
*S ADD TOTAL DISCHARGE										
ADD HYD	TOTAL 28&13	29		.12224	275.27	11.736	1.80019	1.500	3.519	
*S-										
*S COMPUTE COMMERCIAL BASIN 201										
COMPUTE NM HYD	201.D -	30		.00781	21.05	1.010	2.42469	1.500	4.212 PER IMP= 90.00	
*S-										
*S COMPUTE COMMERCIAL BASIN 201										
COMPUTE NM HYD	201.H -	31		.00781	6.47	.184	.44094	1.500	1.295 PER IMP= .00	
*S-										
FINISH										
s0p10h4099T&l6D_										

Cabezon Tract 10A
100-Year 24-Hour Duration Storm-Developed
AHYMO Output File

(s16.67h8.5v0T_&l8D

AHYMO PROGRAM (AHYMO_97) - Version: 1997.02c
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 START TIME (HR:MIN:SEC) = 09:23:46 USER NO.= AHYMO-I-9702a01000150-SH
 INPUT FILE = G:\Proj\170575-1\DRN_ST-1\AHYMO\CAB10A-1.DAT

START TIME=0.0 CODE 0 LINES -6
 LOCATION RIO RANCHO
 City of Rio Rancho soil infiltration values (LAND FACTORS) used for computations.
 Land Treatment Initial Abstr.(in) Unif. Infilt.(in/hour)
 A 0.65 1.67
 B 0.50 1.25
 C 0.35 0.83
 D 0.10 0.04

*S
 *S CABEZON TRACT 10A
 *S
 *S FN:CAB10_DEV.DAT - HYMO PER JAN 1997 DPM REVISIONS
 *S
 *S
 *S RAINFALL TYPE=-2 RAIN QUARTER=0.0 RAIN ONE=1.8
 RAIN SIX=2.2 RAIN DAY=2.7 DT=.05

COMPUTED 24-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.
 DT = .050000 HOURS END TIME = 24.000000 HOURS

*
 *S*****
 *S BULK FOR SEDIMENT - DEVELOPED
 SEDIMENT BULK CODE=1 BULK FACTOR=1.05
 *S-----
 *S COMPUTE ONSITE BASIN 101
 COMPUTE NM HYD ID=1 HYD=101 AREA=0.02102 SQ MI
 %A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 46.245 CFS UNIT VOLUME = .9989 B = 526.28 P60 = 1.8000
 AREA = .011687 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 24.851 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .009333 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=1 CODE=10

PARTIAL HYDROGRAPH 101.00

TIME HRS	FLOW CFS						
.000	.0	5.000	.3	10.000	.3	15.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2
1.000	.2	6.000	.3	11.000	.3	16.000	.2
1.500	47.3	6.500	.3	11.500	.2	16.500	.2
2.000	9.4	7.000	.3	12.000	.2	17.000	.2
2.500	1.4	7.500	.3	12.500	.2	17.500	.2
3.000	.5	8.000	.3	13.000	.2	18.000	.2
3.500	.3	8.500	.3	13.500	.2	18.500	.2
4.000	.3	9.000	.3	14.000	.2	19.000	.2
4.500	.3	9.500	.3	14.500	.2	19.500	.2
						20.000	.2
						20.500	.2
						21.000	.2
						21.500	.2
						22.000	.2
						22.500	.2
						23.000	.2
						23.500	.2
						24.000	.2
						24.500	.0

RUNOFF VOLUME = 1.80021 INCHES = 2.0181 ACRE-FEET
 PEAK DISCHARGE RATE = 47.33 CFS AT 1.500 HOURS BASIN AREA = .0210 SQ. MI.

*S-----
 *S COMPUTE ONSITE BASIN 102
 COMPUTE NM HYD ID=2 HYD=102 AREA=0.01678 SQ MI
 %A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 36.917 CFS UNIT VOLUME = .9988 B = 526.28 P60 = 1.8000
 AREA = .009330 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 19.838 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .007450 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=2 CODE=10

Cabezon Tract 10A
100-Year 24-Hour Duration Storm-Developed
AHYMO Output File

PARTIAL HYDROGRAPH 102.00

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.2	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.2	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.2	21.000	.1
1.500	37.8	6.500	.3	11.500	.2	16.500	.2	21.500	.1
2.000	7.5	7.000	.3	12.000	.2	17.000	.2	22.000	.1
2.500	1.1	7.500	.2	12.500	.2	17.500	.2	22.500	.1
3.000	.4	8.000	.2	13.000	.2	18.000	.2	23.000	.1
3.500	.3	8.500	.2	13.500	.2	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.2	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.2	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.80021 INCHES = 1.6111 ACRE-FEET
 PEAK DISCHARGE RATE = 37.78 CFS AT 1.500 HOURS BASIN AREA = .0168 SQ. MI.

*S-----

*S ADD 101 TO 102

ADD HYD

ID=3 HYD=AP.2 IDi=1 IDii=2

PRINT HYD

ID=3 CODE=10

HYDROGRAPH FROM AREA AP.2

TIME HRS	FLOW CFS								
.000	.0	5.000	.5	10.000	.5	15.000	.4	20.000	.3
.500	.0	5.500	.5	10.500	.5	15.500	.4	20.500	.3
1.000	.3	6.000	.6	11.000	.5	16.000	.4	21.000	.3
1.500	85.1	6.500	.6	11.500	.4	16.500	.4	21.500	.3
2.000	16.9	7.000	.6	12.000	.4	17.000	.4	22.000	.3
2.500	2.6	7.500	.5	12.500	.4	17.500	.3	22.500	.3
3.000	1.0	8.000	.5	13.000	.4	18.000	.3	23.000	.3
3.500	.6	8.500	.5	13.500	.4	18.500	.3	23.500	.3
4.000	.5	9.000	.5	14.000	.4	19.000	.3	24.000	.3
4.500	.5	9.500	.5	14.500	.4	19.500	.3	24.500	.0

RUNOFF VOLUME = 1.80019 INCHES = 3.6292 ACRE-FEET
 PEAK DISCHARGE RATE = 85.11 CFS AT 1.500 HOURS BASIN AREA = .0378 SQ. MI.

*S-----

*S DIVIDE AP.2

*S ID=4 IS 68.00 CFS INTO INLETS

*S ID=5 IS 17.11 CFS BYPASSING INLET TO BASIN103

DIVIDE HYD

ID=3 Q=68.0 IDi=4 HYD=AP.2.TO.INLETS

IDii=5 HYD=AP.2.BYPASS

*S-----

*S COMPUTE ONSITE BASIN 103

COMPUTE NM HYD

ID=6 HYD=103 AREA=0.01272 SQ MI

%A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR

MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 27.985 CFS UNIT VOLUME = .9987 B = 526.28 P60 = 1.8000
 AREA = .007072 SQ MI IA = .10000 INCHES INF = .040000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 15.038 CFS UNIT VOLUME = 1.000 B = 354.14 P60 = 1.8000
 AREA = .005648 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD

ID=6 CODE=10

PARTIAL HYDROGRAPH 103.00

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1	21.000	.1
1.500	28.6	6.500	.2	11.500	.1	16.500	.1	21.500	.1
2.000	5.7	7.000	.2	12.000	.1	17.000	.1	22.000	.1
2.500	.9	7.500	.2	12.500	.1	17.500	.1	22.500	.1
3.000	.3	8.000	.2	13.000	.1	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.1	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.80021 INCHES = 1.2213 ACRE-FEET
 PEAK DISCHARGE RATE = 28.64 CFS AT 1.500 HOURS BASIN AREA = .0127 SQ. MI.

*S-----

*S ADD 103 TO AP.2.BYPASS

Cabezon Tract 10A
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AHYMO Output File

ADD HYD ID=7 HYD=AP.3 IDi=5 IDii=6
 PRINT HYD ID=7 CODE=10

HYDROGRAPH FROM AREA AP.3

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1	21.000	.1
1.500	45.8	6.500	.2	11.500	.1	16.500	.1	21.500	.1
2.000	5.7	7.000	.2	12.000	.1	17.000	.1	22.000	.1
2.500	.9	7.500	.2	12.500	.1	17.500	.1	22.500	.1
3.000	.3	8.000	.2	13.000	.1	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.1	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.80018 INCHES = 1.3473 ACRE-FEET
 PEAK DISCHARGE RATE = 45.76 CFS AT 1.500 HOURS BASIN AREA = .0140 SQ. MI.

*S-----

*S COMPUTE ONSITE BASIN 104

COMPUTE NM HYD ID=8 HYD=104 AREA=0.01339 SQ MI
 %A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 29.459 CFS UNIT VOLUME = .9987 B = 526.28 P60 = 1.8000
 AREA = .007445 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 15.830 CFS UNIT VOLUME = 1.000 B = 354.14 P60 = 1.8000
 AREA = .005945 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=8 CODE=10

PARTIAL HYDROGRAPH 104.00

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.1	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1	20.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1	21.000	.1
1.500	30.2	6.500	.2	11.500	.2	16.500	.1	21.500	.1
2.000	6.0	7.000	.2	12.000	.2	17.000	.1	22.000	.1
2.500	.9	7.500	.2	12.500	.1	17.500	.1	22.500	.1
3.000	.3	8.000	.2	13.000	.1	18.000	.1	23.000	.1
3.500	.2	8.500	.2	13.500	.1	18.500	.1	23.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.80021 INCHES = 1.2856 ACRE-FEET
 PEAK DISCHARGE RATE = 30.15 CFS AT 1.500 HOURS BASIN AREA = .0134 SQ. MI.

*S-----

*S ADD 104 TO AP.3

ADD HYD ID=9 HYD=AP.4 IDi=7 IDii=8
 PRINT HYD ID=9 CODE=10

HYDROGRAPH FROM AREA AP.4

TIME HRS	FLOW CFS								
.000	.0	5.000	.3	10.000	.3	15.000	.3	20.000	.2
.500	.0	5.500	.4	10.500	.3	15.500	.3	20.500	.2
1.000	.2	6.000	.4	11.000	.3	16.000	.3	21.000	.2
1.500	75.9	6.500	.4	11.500	.3	16.500	.2	21.500	.2
2.000	11.7	7.000	.4	12.000	.3	17.000	.2	22.000	.2
2.500	1.8	7.500	.4	12.500	.3	17.500	.2	22.500	.2
3.000	.7	8.000	.4	13.000	.3	18.000	.2	23.000	.2
3.500	.4	8.500	.4	13.500	.3	18.500	.2	23.500	.2
4.000	.3	9.000	.3	14.000	.3	19.000	.2	24.000	.2
4.500	.3	9.500	.3	14.500	.3	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.80019 INCHES = 2.6329 ACRE-FEET
 PEAK DISCHARGE RATE = 75.91 CFS AT 1.500 HOURS BASIN AREA = .0274 SQ. MI.

*S-----

*S COMPUTE ONSITE BASIN 105

COMPUTE NM HYD ID=10 HYD=105 AREA=0.01392 SQ MI
 %A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR
 MASS RAINFALL=-1

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K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 30.625 CFS UNIT VOLUME = .9988 B = 526.28 P60 = 1.8000
 AREA = .007740 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 16.457 CFS UNIT VOLUME = 1.000 B = 354.14 P60 = 1.8000
 AREA = .006180 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=10 CODE=10

PARTIAL HYDROGRAPH 105.00

TIME HRS	FLOW CFS						
.000	.0	5.000	.2	10.000	.2	15.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1
1.500	31.3	6.500	.2	11.500	.2	16.500	.1
2.000	6.2	7.000	.2	12.000	.2	17.000	.1
2.500	.9	7.500	.2	12.500	.2	17.500	.1
3.000	.4	8.000	.2	13.000	.2	18.000	.1
3.500	.2	8.500	.2	13.500	.1	18.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1

RUNOFF VOLUME = 1.80021 INCHES = 1.3365 ACRE-FEET
 PEAK DISCHARGE RATE = 31.35 CFS AT 1.500 HOURS BASIN AREA = .0139 SQ. MI.

*S-

*S COMPUTE ONSITE BASIN 106

COMPUTE NM HYD ID=11 HYD=106 AREA=0.01595 SQ MI

%A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR

MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 35.091 CFS UNIT VOLUME = .9988 B = 526.28 P60 = 1.8000
 AREA = .008868 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 18.857 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .007082 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=11 CODE=10

PARTIAL HYDROGRAPH 106.00

TIME HRS	FLOW CFS						
.000	.0	5.000	.2	10.000	.2	15.000	.2
.500	.0	5.500	.2	10.500	.2	15.500	.2
1.000	.1	6.000	.2	11.000	.2	16.000	.2
1.500	35.9	6.500	.2	11.500	.2	16.500	.2
2.000	7.1	7.000	.2	12.000	.2	17.000	.1
2.500	1.1	7.500	.2	12.500	.2	17.500	.1
3.000	.4	8.000	.2	13.000	.2	18.000	.1
3.500	.3	8.500	.2	13.500	.2	18.500	.1
4.000	.2	9.000	.2	14.000	.2	19.000	.1
4.500	.2	9.500	.2	14.500	.2	19.500	.1

RUNOFF VOLUME = 1.80021 INCHES = 1.5314 ACRE-FEET
 PEAK DISCHARGE RATE = 35.92 CFS AT 1.500 HOURS BASIN AREA = .0160 SQ. MI.

*S-----

*S ADD 105 TO 106

ADD HYD ID=12 HYD=AP.5 IDi=10 IDii=11

PRINT HYD ID=12 CODE=10

HYDROGRAPH FROM AREA AP.5

TIME HRS	FLOW CFS						
.000	.0	5.000	.4	10.000	.4	15.000	.3
.500	.0	5.500	.4	10.500	.4	15.500	.3
1.000	.2	6.000	.4	11.000	.4	16.000	.3
1.500	67.3	6.500	.5	11.500	.3	16.500	.3
2.000	13.3	7.000	.4	12.000	.3	17.000	.3
2.500	2.0	7.500	.4	12.500	.3	17.500	.3
3.000	.8	8.000	.4	13.000	.3	18.000	.3
3.500	.5	8.500	.4	13.500	.3	18.500	.3

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4.000 .4	9.000 .4	14.000 .3	19.000 .3	24.000 .2
4.500 .4	9.500 .4	14.500 .3	19.500 .3	24.500 .0

RUNOFF VOLUME = 1.80019 INCHES = 2.8678 ACRE-FEET
 PEAK DISCHARGE RATE = 67.26 CFS AT 1.500 HOURS BASIN AREA = .0299 SQ. MI.

*S-----
 *S DIVIDE AP-6
 *S ID=13 IS 52.00 CFS INTO INLETS
 *S ID=14 IS 15.26 CFS BYPASSING INLET TO BASIN103
 DIVIDE HYD ID=12 Q=52.0 IDi=13 HYD=#100
 IDii=14 HYD=AP.6.BYPASS

*S-----
 *S COMPUTE ONSITE BASIN 107
 COMPUTE NM HYD ID=15 HYD=107 AREA=0.01808 SQ MI
 %A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 39.777 CFS UNIT VOLUME = .9989 B = 526.28 P60 = 1.8000
 AREA = .010052 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 21.375 CFS UNIT VOLUME = 1.001 B = 354.14 P60 = 1.8000
 AREA = .008028 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=15 CODE=10

PARTIAL HYDROGRAPH 107.00

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	5.000	.2	10.000	.2	15.000	.2
.500	.0	5.500	.2	10.500	.2	15.500	.2
1.000	.1	6.000	.3	11.000	.2	16.000	.2
1.500	40.7	6.500	.3	11.500	.2	16.500	.2
2.000	8.1	7.000	.3	12.000	.2	17.000	.2
2.500	1.2	7.500	.3	12.500	.2	17.500	.2
3.000	.5	8.000	.3	13.000	.2	18.000	.2
3.500	.3	8.500	.3	13.500	.2	18.500	.2
4.000	.2	9.000	.2	14.000	.2	19.000	.2
4.500	.2	9.500	.2	14.500	.2	19.500	.2

RUNOFF VOLUME = 1.80021 INCHES = 1.7359 ACRE-FEET
 PEAK DISCHARGE RATE = 40.71 CFS AT 1.500 HOURS BASIN AREA = .0181 SQ. MI.

*S-----
 *S ADD 107 TO AP.6.BYPASS
 ADD HYD ID=16 HYD=AP.7 IDi=14 IDii=15
 PRINT HYD ID=16 CODE=10

HYDROGRAPH FROM AREA AP.7

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	5.000	.2	10.000	.2	15.000	.2
.500	.0	5.500	.2	10.500	.2	15.500	.2
1.000	.1	6.000	.3	11.000	.2	16.000	.2
1.500	56.0	6.500	.3	11.500	.2	16.500	.2
2.000	8.1	7.000	.3	12.000	.2	17.000	.2
2.500	1.2	7.500	.3	12.500	.2	17.500	.2
3.000	.5	8.000	.3	13.000	.2	18.000	.2
3.500	.3	8.500	.3	13.500	.2	18.500	.2
4.000	.2	9.000	.2	14.000	.2	19.000	.2
4.500	.2	9.500	.2	14.500	.2	19.500	.2

RUNOFF VOLUME = 1.80019 INCHES = 1.8571 ACRE-FEET
 PEAK DISCHARGE RATE = 55.97 CFS AT 1.500 HOURS BASIN AREA = .0193 SQ. MI.

*S-----
 *S COMPUTE ONSITE BASIN 108
 COMPUTE NM HYD ID=17 HYD=108 AREA=0.00672 SQ MI
 %A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 14.784 CFS UNIT VOLUME = .9983 B = 526.28 P60 = 1.8000
 AREA = .003736 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 7.9446 CFS UNIT VOLUME = .9996 B = 354.14 P60 = 1.8000

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AREA = .002984 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=17 CODE=10

PARTIAL HYDROGRAPH 108.00

TIME HRS	FLOW CFS								
.000	.0	5.000	.1	10.000	.1	15.000	.1	20.000	.1
.500	.0	5.500	.1	10.500	.1	15.500	.1	20.500	.1
1.000	.0	6.000	.1	11.000	.1	16.000	.1	21.000	.1
1.500	15.1	6.500	.1	11.500	.1	16.500	.1	21.500	.1
2.000	3.0	7.000	.1	12.000	.1	17.000	.1	22.000	.1
2.500	.5	7.500	.1	12.500	.1	17.500	.1	22.500	.1
3.000	.2	8.000	.1	13.000	.1	18.000	.1	23.000	.1
3.500	.1	8.500	.1	13.500	.1	18.500	.1	23.500	.1
4.000	.1	9.000	.1	14.000	.1	19.000	.1	24.000	.0
4.500	.1	9.500	.1	14.500	.1	19.500	.1	24.500	.0

RUNOFF VOLUME = 1.80021 INCHES = .6452 ACRE-FEET
 PEAK DISCHARGE RATE = 15.14 CFS AT 1.500 HOURS BASIN AREA = .0067 SQ. MI.

*S-----

*S COMPUTE ONSITE BASIN 109
 COMPUTE NM HYD ID=18 HYD=109 AREA=0.00366 SQ MI
 %A=0 %B=22.2 %C=22.2 %D=55.6 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 8.0523 CFS UNIT VOLUME = .9979 B = 526.28 P60 = 1.8000
 AREA = .002035 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .118383HR TP = .133000HR K/TP RATIO = .890100 SHAPE CONSTANT, N = 3.984532
 UNIT PEAK = 4.3270 CFS UNIT VOLUME = .9984 B = 354.14 P60 = 1.8000
 AREA = .001625 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=18 CODE=10

PARTIAL HYDROGRAPH 109.00

TIME HRS	FLOW CFS								
.000	.0	5.000	.0	10.000	.0	15.000	.0	20.000	.0
.500	.0	5.500	.0	10.500	.0	15.500	.0	20.500	.0
1.000	.0	6.000	.1	11.000	.0	16.000	.0	21.000	.0
1.500	8.3	6.500	.1	11.500	.0	16.500	.0	21.500	.0
2.000	1.6	7.000	.1	12.000	.0	17.000	.0	22.000	.0
2.500	.2	7.500	.1	12.500	.0	17.500	.0	22.500	.0
3.000	.1	8.000	.1	13.000	.0	18.000	.0	23.000	.0
3.500	.1	8.500	.1	13.500	.0	18.500	.0	23.500	.0
4.000	.0	9.000	.0	14.000	.0	19.000	.0	24.000	.0
4.500	.0	9.500	.0	14.500	.0	19.500	.0	24.500	.0

RUNOFF VOLUME = 1.80021 INCHES = .3514 ACRE-FEET
 PEAK DISCHARGE RATE = 8.25 CFS AT 1.500 HOURS BASIN AREA = .0037 SQ. MI.

*S-----

*S ADD 108 TO AP.7
 ADD HYD ID=19 HYD=AP.8 IDi=16 IDii=17
 PRINT HYD ID=19 CODE=10

HYDROGRAPH FROM AREA AP.8

TIME HRS	FLOW CFS								
.000	.0	5.000	.3	10.000	.3	15.000	.2	20.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2	20.500	.2
1.000	.2	6.000	.4	11.000	.3	16.000	.2	21.000	.2
1.500	71.1	6.500	.4	11.500	.3	16.500	.2	21.500	.2
2.000	11.1	7.000	.4	12.000	.3	17.000	.2	22.000	.2
2.500	1.7	7.500	.4	12.500	.3	17.500	.2	22.500	.2
3.000	.6	8.000	.4	13.000	.3	18.000	.2	23.000	.2
3.500	.4	8.500	.3	13.500	.3	18.500	.2	23.500	.2
4.000	.3	9.000	.3	14.000	.3	19.000	.2	24.000	.2
4.500	.3	9.500	.3	14.500	.3	19.500	.2	24.500	.0

RUNOFF VOLUME = 1.80019 INCHES = 2.5022 ACRE-FEET
 PEAK DISCHARGE RATE = 71.11 CFS AT 1.500 HOURS BASIN AREA = .0261 SQ. MI.

*S-----

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100-Year 24-Hour Duration Storm-Developed
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*S ADD 109 TO AP.4

ADD HYD ID=20 HYD=AP.9 IDi=18 IDii=9
 PRINT HYD ID=20 CODE=10

HYDROGRAPH FROM AREA AP.9

TIME HRS	FLOW CFS								
.000	.0	5.000	.4	10.000	.4	15.000	.3	20.000	.2
.500	.0	5.500	.4	10.500	.4	15.500	.3	20.500	.2
1.000	.2	6.000	.4	11.000	.4	16.000	.3	21.000	.2
1.500	84.2	6.500	.5	11.500	.3	16.500	.3	21.500	.2
2.000	13.3	7.000	.4	12.000	.3	17.000	.3	22.000	.2
2.500	2.0	7.500	.4	12.500	.3	17.500	.3	22.500	.2
3.000	.8	8.000	.4	13.000	.3	18.000	.3	23.000	.2
3.500	.5	8.500	.4	13.500	.3	18.500	.3	23.500	.2
4.000	.4	9.000	.4	14.000	.3	19.000	.3	24.000	.2
4.500	.4	9.500	.4	14.500	.3	19.500	.3	24.500	.0

RUNOFF VOLUME = 1.80018 INCHES = 2.9843 ACRE-FEET
 PEAK DISCHARGE RATE = 84.16 CFS AT 1.500 HOURS BASIN AREA = .0311 SQ. MI.

*S-----

*S DIVIDE AP-8

*S ID=21 IS 54.00 CFS INTO INLETS

*S ID=22 IS 17.11 CFS BYPASSING TO SUMP

DIVIDE HYD ID=19 Q=54.0 IDi=21 HYD=AP.8.TO.INLETS IDii=22 HYD=AP.8.BYPASS

*S-----

*S DIVIDE AP-9

*S ID=23 IS 60.00 CFS INTO INLETS

*S ID=24 IS 24.16 CFS BYPASSING TO SUMP

DIVIDE HYD ID=20 Q=60.0 IDi=23 HYD=AP.9.TO.INLETS IDii=24 HYD=AP.9.BYPASS

*S-----

*S ADD SUMP INLET TOTAL

ADD HYD ID=25 HYD=AP.10 IDi=22 IDii=24

PRINT HYD ID=25 CODE=10

HYDROGRAPH FROM AREA AP.10

TIME HRS	FLOW CFS								
.000	.0	.500	.0	1.000	.0	1.500	41.3		

RUNOFF VOLUME = 1.80018 INCHES = .2335 ACRE-FEET
 PEAK DISCHARGE RATE = 41.27 CFS AT 1.500 HOURS BASIN AREA = .0024 SQ. MI.

*S-----

*S ADD INLET FLOWS

ADD HYD ID=26 HYD=#200A IDi=4 IDii=21

PRINT HYD ID=26 CODE=10

HYDROGRAPH FROM AREA #200A

TIME HRS	FLOW CFS								
.000	.0	5.000	.8	10.000	.8	15.000	.6	20.000	.5
.500	.0	5.500	.8	10.500	.8	15.500	.6	20.500	.5
1.000	.5	6.000	.9	11.000	.8	16.000	.6	21.000	.5
1.500	122.0	6.500	1.0	11.500	.7	16.500	.6	21.500	.5
2.000	28.0	7.000	.9	12.000	.7	17.000	.6	22.000	.5
2.500	4.3	7.500	.9	12.500	.7	17.500	.6	22.500	.5
3.000	1.6	8.000	.9	13.000	.7	18.000	.6	23.000	.5
3.500	1.0	8.500	.9	13.500	.7	18.500	.5	23.500	.5
4.000	.8	9.000	.8	14.000	.7	19.000	.5	24.000	.5
4.500	.8	9.500	.8	14.500	.6	19.500	.5	24.500	.0

RUNOF VOLUME = 1.80019 INCHES = 5.9176 ACRE-FEET
 PEAK DISCHARGE RATE = 122.00 CFS AT 1.450 HOURS BASIN AREA = .0616 SQ. MI.

*S-----

*S ADD INLET FLOWS

ADD HYD ID=27 HYD=#300 IDi=23 IDii=25

PRINT HYD ID=27 CODE=10

HYDROGRAPH FROM AREA #300

TIME HRS	FLOW CFS								
.000	.0	5.000	.4	10.000	.4	15.000	.3	20.000	.2
.500	.0	5.500	.4	10.500	.4	15.500	.3	20.500	.2
1.000	.2	6.000	.4	11.000	.4	16.000	.3	21.000	.2
1.500	101.3	6.500	.5	11.500	.3	16.500	.3	21.500	.2
2.000	13.3	7.000	.4	12.000	.3	17.000	.3	22.000	.2
2.500	2.0	7.500	.4	12.500	.3	17.500	.3	22.500	.2
3.000	.8	8.000	.4	13.000	.3	18.000	.3	23.000	.2
3.500	.5	8.500	.4	13.500	.3	18.500	.3	23.500	.2

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4.000 .4	9.000 .4	14.000 .3	19.000 .3	24.000 .2
4.500 .4	9.500 .4	14.500 .3	19.500 .3	24.500 .0

RUNOFF VOLUME = 1.80018 INCHES = 3.0720 ACRE-FEET
 PEAK DISCHARGE RATE = 101.27 CFS AT 1.500 HOURS BASIN AREA = .0320 SQ. MI.

*S-----

*S ADD SOUTH OUTFALL

ADD HYD ID=28 HYD=#200 IDi=26 IDii=27
 PRINT HYD ID=28 CODE=10

HYDROGRAPH FROM AREA #200

TIME HRS	FLOW CFS						
.000	.0	5.000	1.2	10.000	1.2	15.000	.9
.500	.0	5.500	1.3	10.500	1.1	15.500	.9
1.000	.7	6.000	1.4	11.000	1.1	16.000	.9
1.500	223.3	6.500	1.4	11.500	1.1	16.500	.9
2.000	41.3	7.000	1.4	12.000	1.0	17.000	.9
2.500	6.3	7.500	1.3	12.500	1.0	17.500	.8
3.000	2.3	8.000	1.3	13.000	1.0	18.000	.8
3.500	1.4	8.500	1.3	13.500	1.0	18.500	.8
4.000	1.2	9.000	1.2	14.000	1.0	19.000	.8
4.500	1.2	9.500	1.2	14.500	.9	19.500	.8

RUNOFF VOLUME = 1.80019 INCHES = 8.9896 ACRE-FEET
 PEAK DISCHARGE RATE = 223.27 CFS AT 1.500 HOURS BASIN AREA = .0936 SQ. MI.

*S-----

*S ADD TOTAL DISCHARGE

ADD HYD ID=29 HYD=TOTAL IDi=28 IDii=13
 PRINT HYD ID=29 CODE=10

HYDROGRAPH FROM AREA TOTAL

TIME HRS	FLOW CFS						
.000	.0	5.000	1.6	10.000	1.5	15.000	1.2
.500	.0	5.500	1.7	10.500	1.5	15.500	1.2
1.000	.9	6.000	1.8	11.000	1.5	16.000	1.2
1.500	275.3	6.500	1.9	11.500	1.4	16.500	1.2
2.000	54.6	7.000	1.8	12.000	1.4	17.000	1.1
2.500	8.3	7.500	1.8	12.500	1.4	17.500	1.1
3.000	3.1	8.000	1.7	13.000	1.3	18.000	1.1
3.500	1.9	8.500	1.7	13.500	1.3	18.500	1.1
4.000	1.6	9.000	1.6	14.000	1.3	19.000	1.1
4.500	1.5	9.500	1.6	14.500	1.2	19.500	1.0

RUNOFF VOLUME = 1.80019 INCHES = 11.7362 ACRE-FEET
 PEAK DISCHARGE RATE = 275.27 CFS AT 1.500 HOURS BASIN AREA = .1222 SQ. MI.

*S-----

*S COMPUTE COMMERCIAL BASIN 201

COMPUTE NM HYD ID=30 HYD=201.D AREA=0.00781 SQ MI
 %A=0 %B=0 %C=10 %D=90 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 27.813 CFS UNIT VOLUME = .9987 B = 526.28 P60 = 1.8000
 AREA = .007029 SQ MI IA = .10000 INCHES INF = .040000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .104841HR TP = .133000HR K/TP RATIO = .788276 SHAPE CONSTANT, N = 4.552994
 UNIT PEAK = 2.2930 CFS UNIT VOLUME = .9963 B = 390.49 P60 = 1.8000
 AREA = .000781 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD

ID=30 CODE=10

HYDROGRAPH FROM AREA 201.D

TIME HRS	FLOW CFS						
.000	.0	5.000	.2	10.000	.2	15.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.1
1.000	.1	6.000	.2	11.000	.2	16.000	.1
1.500	21.1	6.500	.2	11.500	.1	16.500	.1
2.000	5.0	7.000	.2	12.000	.1	17.000	.1
2.500	.7	7.500	.2	12.500	.1	17.500	.1
3.000	.3	8.000	.2	13.000	.1	18.000	.1
3.500	.2	8.500	.2	13.500	.1	18.500	.1
4.000	.2	9.000	.2	14.000	.1	19.000	.1
4.500	.2	9.500	.2	14.500	.1	19.500	.1

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RUNOFF VOLUME = 2.42469 INCHES = 1.0100 ACRE-FEET
PEAK DISCHARGE RATE = 21.05 CFS AT 1.500 HOURS BASIN AREA = .0078 SQ. MI.

*S-----

*S COMPUTE COMMERCIAL BASIN 201
COMPUTE NM HYD ID=31 HYD=201.H AREA=.00781 SQ MI
%A=100 %B=0 %C=0 %D=0 TP=0.133 HR
MASS RAINFALL=-1

K = .165076HR TP = .133000HR K/TP RATIO = 1.241174 SHAPE CONSTANT, N = 2.871844
UNIT PEAK = 15.925 CFS UNIT VOLUME = .9974 B = 271.20 P60 = 1.8000
AREA = .007810 SQ MI IA = .65000 INCHES INF = 1.67000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=31 CODE=10

HYDROGRAPH FROM AREA 201.H

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.000	.0	2.000	.6	3.000	.1
.500	.0	1.500	6.5	2.500	.2	3.500	.0
						4.000	.0
						4.500	.0

RUNOFF VOLUME = .44094 INCHES = .1837 ACRE-FEET
PEAK DISCHARGE RATE = 6.47 CFS AT 1.500 HOURS BASIN AREA = .0078 SQ. MI.

*S-----
FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 09:23:46

(s0p10h4099T_&16D

CABEZON TRACT 10A
Street Flow Analysis

Analysis Point	Hydrograph ID	Q (cfs)	Road Slope	Q Half Street (cfs)	Flow Depth (ft)	Velocity (ft/s)	Depth x Velocity	Inlet Type	Q Inlet (cfs)	Q Bypass (cfs)	Inlet #1			Inlet #2			Notes
											Inlet #1	Flow Depth (ft)	Q Inlet (cfs)	Inlet Type	Q Inlet (cfs)	Flow Depth (ft)	Q Bypass (cfs)
1	101	47.3	0.51%	23.7	0.65	3.2	2.1	NONE	0	23.7	0.65	0.0	23.7	BYPASS FLOW TO BASIN 102			
2	102	85.1	0.51%	42.6	0.87	3.8	3.3	DOUBLE C	17	25.6	0.87	17	8.6	2-DOMBLE C BATTERY, BYPASS TO BASIN 103			
3	103	45.8	0.51%	22.9	0.6	3	1.8	NONE	0.00	22.9	NONE	0.6	0	BYPASS FLOW TO BASIN 104			
4	104	75.91	0.51%	37.96	0.78	3.6	2.8	NONE	0	38.0	NONE	0.78	0	38.0	BYPASS FLOW TO BASIN 109		
5	105	31.35	1.44%	-15.68	0.48	3.8	1.8	NONE	0.00	15.68	NONE	0.48	0	15.675	BYPASS FLOW TO BASIN 106		
6	106	67.26	1.44%	33.63	0.62	5.4	3.3	DOUBLE C	13	20.63	0.62	13	7.63	2-DOMBLE C BATTERY, BYPASS TO BASIN 107			
7	107	55.97	2.29%	27.99	0.5	4	2.0	NONE	0	27.985	NONE	0.5	0	27.985	BYPASS FLOW TO BASIN 108		
8	108	71.11	2.3%	35.56	0.56	5.8	3.248	DOUBLE C	13.5	22.055	DOUBLE C	0.56	13.5	8.555	2-DOMBLE C BATTERY, BYPASS FLOW TO SUMP		
9	109	84.16	0.5%	42	0.83	2.8	2.324	DOUBLE C	15	27	DOUBLE C	0.83	15	12.08	2-DOMBLE C BATTERY, BYPASS FLOW TO SUMP		
10		41.26	SUMP	NA				SUMP	41.26	0					COLLECT 41.26 IN SUMP INLET		

Assumptions

1. Street Flow Depths and Velocities taken from City of Albuquerque Plate 22.3 D-1
2. Double C Grate Capacities taken from City of Albuquerque Plate 22.3 D-6
3. Triple C Grate Capacities were extrapolated from the Double C Capacities.
4. All Grate Capacities do not account for curb opening inflow. Therefore, inlet inflows shown are conservative and provide a safety factor for items such as inlet clogging

Cabezon Tract10A Headloss Calculations

EQUATION FROM MODERN SEWER DESIGN, THIRD EDITION, 1995

Headloss, FT	# PIPES
J-101	1.47
J-201	1.98
J-204	2.40
J-205	5.58
J-301	1.06

CALCULATED VALUES

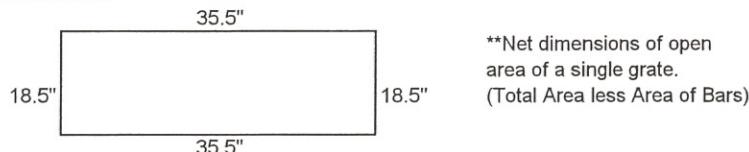
Descript	Angle	coeff	K
I-103	45	0.0033	0.15
I-104	45	0.0033	0.15
J-102	90	0.0033	0.30
J-103	30	0.0033	0.10
I-203	45	0.0033	0.15
I-204	45	0.0033	0.15
I-207	60	0.0033	0.20
I-208	60	0.0033	0.20
J-206	20	0.0033	0.07
I-303	60	0.0033	0.20
I-304	30	0.0033	0.10

Inlet Worksheet (Sump Condition) for Basin 109

Objective: Design a Double Type C Inlet in Sump Condition for a maximum 100-year flow of: 41.3

- 1 Inlet to collect discharge before overtopping curb.
 Standard 8" curb and gutter.
 $D_{max}=10.75 \text{ in}$ (0.9 ft) - Not 8" because standard inlet has 10.75" depression.

- 2 Grate Dimensions



Weir Perimeter - Double 'C' = $2*18.5" + 4*35.5" =$ 14.92 ft
 Area of Orifice - Double 'C' = $18.5" \times 2*35.5" =$ 9.12 sq. ft

- 3 Calculate Orifice and Weir Flow into Grate at Design Depth (0.9 ft)

Orifice Equation	Weir Equation
$Q = 0.6 \times A \times (2 \times g \times h)^{1/2}$	$Q=2.65 \times P \times H^{1/2}$
Where	Where
A = 9.12 sq. ft.	P = 14.9 ft
g = 32.2 ft ^2/sec	H = 0.9 ft
h = 0.9 ft	
Therefore	Therefore
Q = 41.7 cfs	Q = 37.5 cfs

Weir Equation controls
 Double "C" Inlet Grate Capacity @ TBC = 37.5 cfs

- 4 Calculate Inlet Throat Capacity Using Weir Equation at Design Depth (6.25 in)

Weir Equation
$Q=2.65 \times P \times H^{1/2}$
Where
P = 7.0 ft
H = 0.52 ft
Therefore
Q = 13.3 cfs

Double "C" Inlet Throat Capacity = 13.3 cfs

- 5 Calculate Inlet Capacity with a grate clogging factor of 25%

Total Capacity 50.8 cfs
 Minus Grate Clogging Factor of 25% 9.38 cfs

Therefore Capacity of Double C Inlet in Sump Condition = 41.4 cfs.

Worksheet

Worksheet for Irregular Channel

Project Description

Worksheet	Irregular Channel
Flow Element	Irregular Channel
Method	Manning's Formul.
Solve For	Discharge

Input Data

Channel Slope	042000 ft/ft
Water Surface Elev.	0.67 ft

Options

Current Roughness Method	Lotter's Method
Open Channel Weighting	Lotter's Method
Closed Channel Weighting	Horton's Method

Results

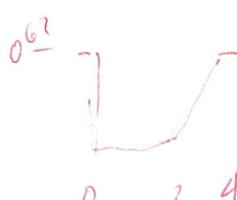
Mannings Coeffic	0.017
Elevation Range	0.00 to 0.67
Discharge	24.67 cfs
Flow Area	2.2 ft ²
Wetted Perimeter	4.62 ft
Top Width	3.67 ft
Actual Depth	0.67 ft
Critical Elevation	1.18 ft
Critical Slope	0.007191 ft/ft
Velocity	11.04 ft/s
Velocity Head	1.89 ft
Specific Energy	2.56 ft
Froude Number	2.49
Flow Type	Supercritical

Roughness Segments

Start Station	End Station	Mannings Coefficient
0+00	0+04	0.017

Natural Channel Points

Station (ft)	Elevation (ft)
0+00	0.67
0+00	0.00
0+03	0.00
0+04	0.67



Cross Section

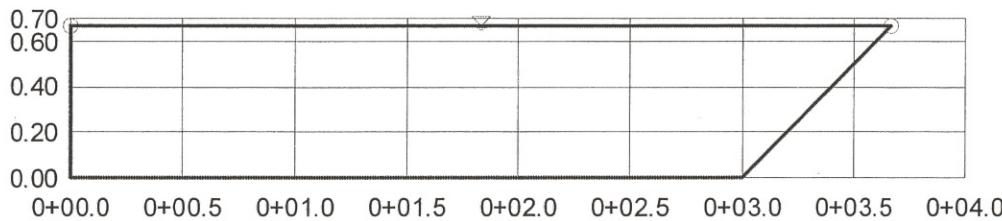
Cross Section for Irregular Channel

Project Description

Worksheet	Irregular Channel
Flow Element	Irregular Channel
Method	Manning's Formul.
Solve For	Discharge

Section Data

Mannings Coefficie	0.017
Channel Slope	0.042000 ft/ft
Water Surface Elev.	0.67 ft
Elevation Range	.00 to 0.67
Discharge	24.67 cfs



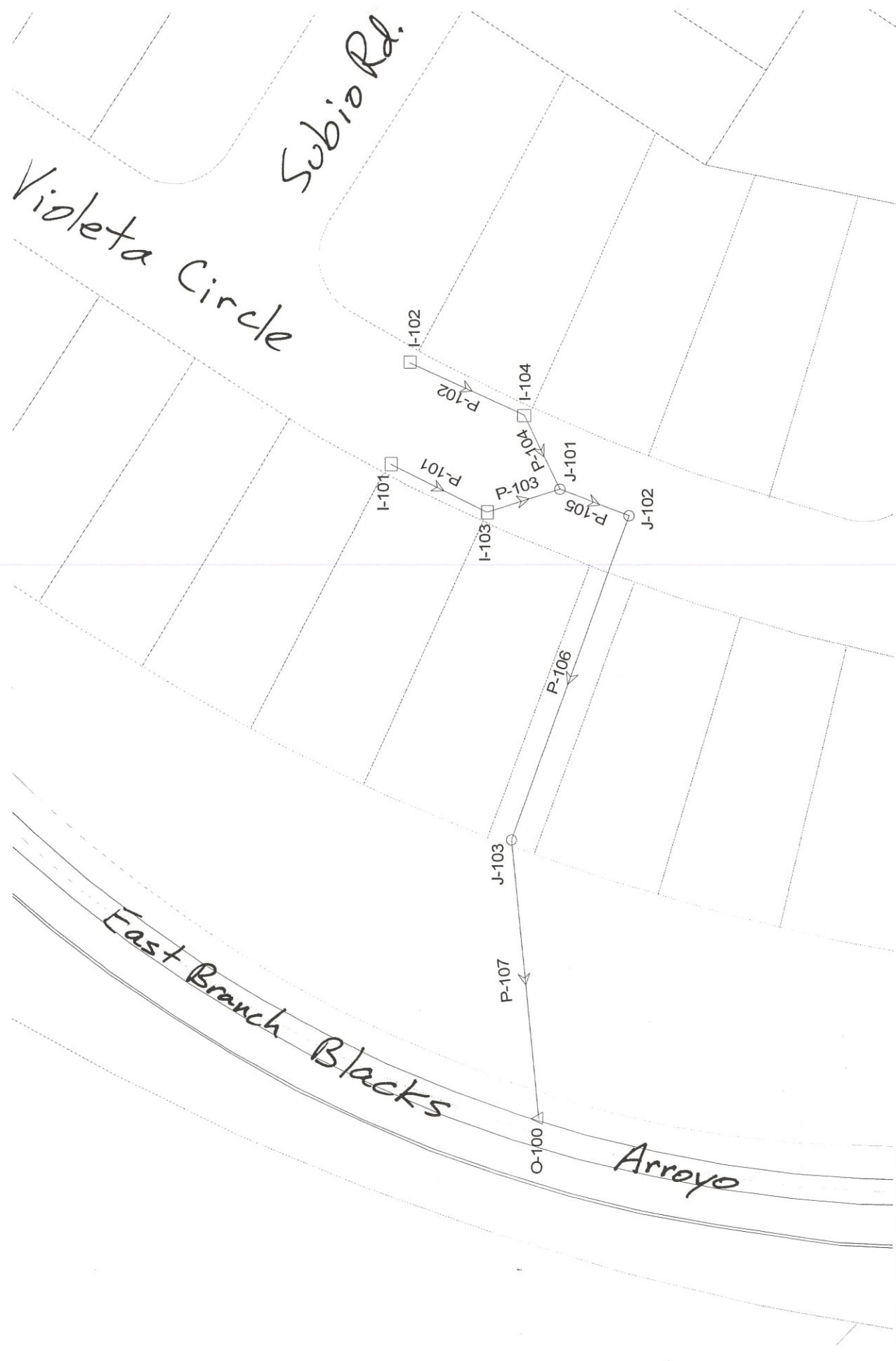
V:1
H:1
NTS

Scenario: Base

Combined Pipe\Node Report

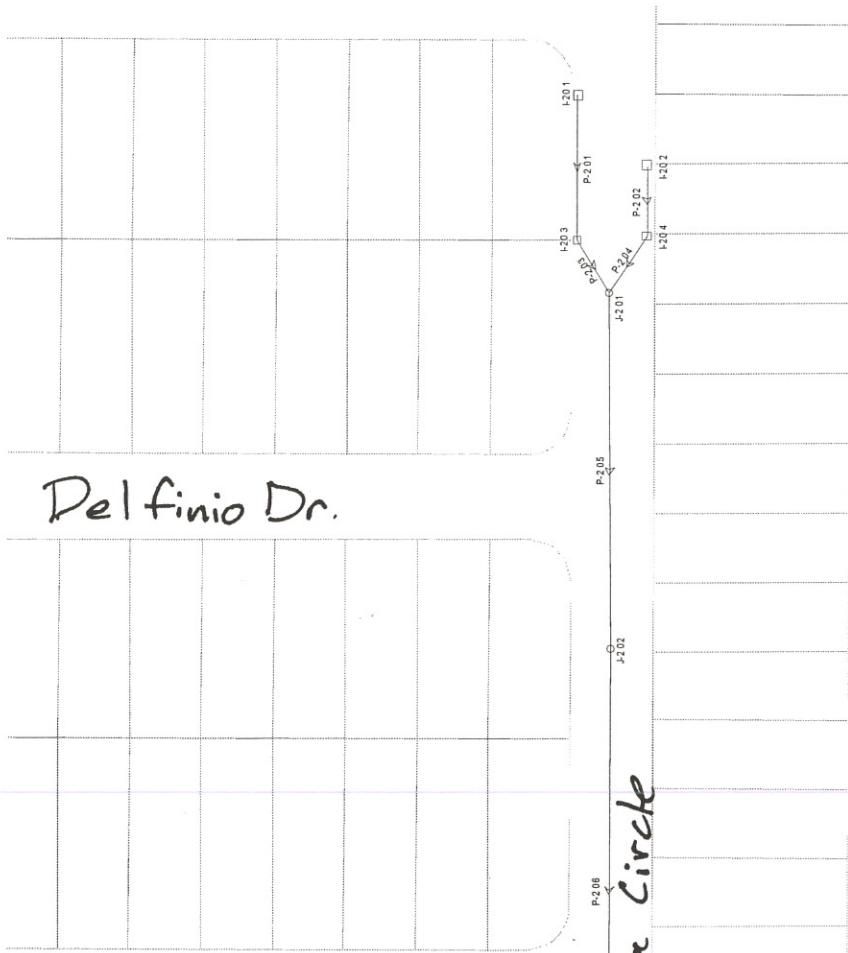
Label	Length (ft)	Section Size	Total Flow (cfs)	Full Capacity (cfs)	Average Velocity (ft/s)	Upstream Node	Downstream Node	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Constructed Slope (ft/ft)	Hydraulic Grade Line In (ft)	Upstream Ground Elevation (ft)	Hydraulic Grade Line Out (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)
P-101	44.00	18 inch	13.00	16.38	7.36	I-101	I-103	5,232.04	5,230.97	0.024318	5,234.42	5,234.59	5,233.75	5,233.95	
P-102	52.00	18 inch	13.00	13.19	7.36	I-102	I-104	5,232.20	5,231.38	0.015769	5,234.57	5,234.74	5,233.78	5,233.96	
P-103	31.00	24 inch	26.00	47.55	8.28	I-103	J-101	5,230.87	5,229.50	0.044194	5,233.11	5,233.95	5,232.70	5,233.87	
P-104	33.00	24 inch	26.00	46.26	8.28	I-104	J-101	5,230.88	5,229.50	0.041818	5,233.14	5,233.96	5,232.70	5,233.87	
P-105	31.00	36 inch	52.00	136.58	18.01	J-101	J-102	5,229.40	5,228.10	0.041935	5,231.75	5,233.87	5,231.30	5,233.48	
P-106	140.00	36 inch	52.00	136.68	18.02	J-102	J-103	5,228.00	5,222.12	0.042000	5,230.35	5,233.48	5,225.08	5,233.00	
P-107	113.00	36 inch	52.00	141.41	18.48	J-103	O-100	5,222.02	5,216.94	0.044956	5,224.37	5,233.00	5,218.28	5,223.00	
P-201	85.00	24 inch	17.00	28.40	5.41	I-201	I-203	5,196.00	5,194.66	0.015765	5,198.93	5,198.46	5,198.45	5,198.99	
P-202	42.00	24 inch	17.00	41.45	5.41	I-202	I-204	5,196.07	5,194.66	0.033571	5,198.71	5,199.21	5,198.47	5,199.00	
P-203	36.00	30 inch	34.00	36.17	6.93	I-203	J-201	5,194.56	5,194.28	0.007778	5,198.00	5,198.99	5,197.76	5,199.13	
P-204	39.00	30 inch	34.00	34.75	6.93	I-204	J-201	5,194.56	5,194.28	0.007179	5,198.02	5,199.00	5,197.76	5,199.13	
P-205	209.00	42 inch	68.00	100.60	11.23	J-201	J-202	5,194.18	5,192.09	0.010000	5,196.76	5,198.13	5,195.19	5,198.09	
P-206	285.00	42 inch	68.00	100.60	11.23	J-202	J-203	5,191.99	5,189.14	0.010000	5,194.57	5,198.09	5,193.52	5,196.64	
P-207	215.00	42 inch	68.00	100.60	7.07	J-203	J-204	5,189.04	5,186.89	0.010000	5,193.14	5,196.64	5,192.15	5,195.55	
P-208	43.00	24 inch	15.00	39.33	11.67	I-206	I-208	5,192.98	5,191.68	0.030233	5,194.38	5,195.52	5,194.35	5,195.16	
P-209	36.00	24 inch	15.00	39.72	11.76	I-205	I-207	5,192.97	5,191.86	0.030833	5,194.53	5,195.51	5,194.53	5,195.34	
P-210	24.00	24 inch	30.00	77.13	23.01	I-208	J-204	5,191.58	5,188.79	0.116250	5,193.44	5,195.16	5,192.15	5,195.55	
P-211	26.00	24 inch	30.00	76.46	22.87	I-207	J-204	5,191.76	5,188.79	0.114231	5,193.62	5,195.34	5,192.15	5,195.55	
P-212	66.00	48 inch	128.00	143.64	12.92	J-204	J-205	5,186.79	5,186.13	0.010000	5,190.18	5,195.55	5,189.93	5,196.00	
P-213	125.00	48 inch	223.27	263.91	23.56	J-205	J-206	5,186.03	5,181.81	0.033760	5,189.93	5,196.00	5,184.93	5,193.00	
P-214	82.00	48 inch	223.27	454.22	35.99	J-206	O-2	5,181.71	5,173.51	0.100000	5,185.61	5,193.00	5,175.98	5,179.00	
P-215	15.00	24 inch	41.27	63.98	21.64	I-209	J-205	5,192.56	5,191.36	0.080000	5,194.52	5,195.10	5,192.92	5,196.00	
P-301	75.00	18 inch	13.50	17.11	10.73	I-301	I-303	5,195.50	5,193.51	0.026533	5,196.87	5,198.04	5,195.22	5,196.49	
P-302	40.00	18 inch	13.50	19.15	11.74	I-302	I-304	5,195.00	5,193.67	0.033250	5,196.37	5,197.53	5,195.38	5,196.65	
P-303	30.00	24 inch	27.00	64.38	19.59	I-303	J-301	5,193.41	5,190.98	0.081000	5,195.22	5,196.49	5,193.27	5,196.11	
P-304	45.00	24 inch	27.00	54.27	17.25	I-304	J-301	5,193.57	5,190.98	0.057556	5,195.38	5,196.65	5,193.27	5,196.11	
P-305	57.00	36 inch	54.00	192.53	23.37	J-301	J-205	5,190.88	5,186.13	0.083333	5,193.27	5,196.11	5,189.93	5,196.00	

Scenariο: Base

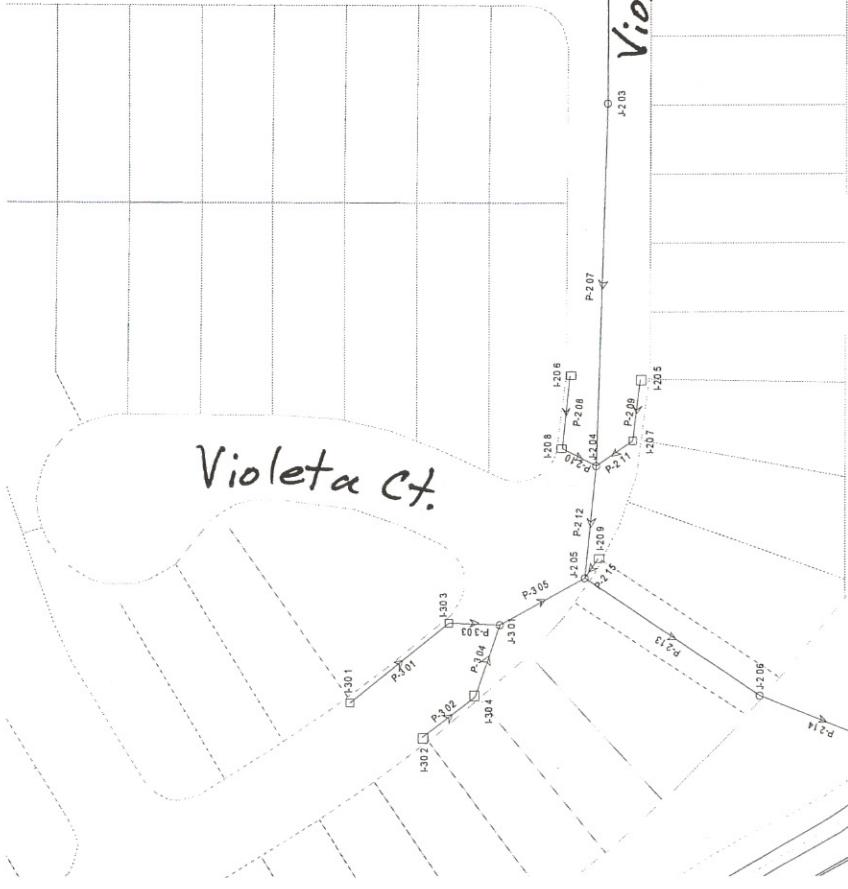


Scenario: Base

Delfino Dr.



Vista de Colinas Dr.



Violeta cf.

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