

**FINAL
DRAINAGE STUDY**

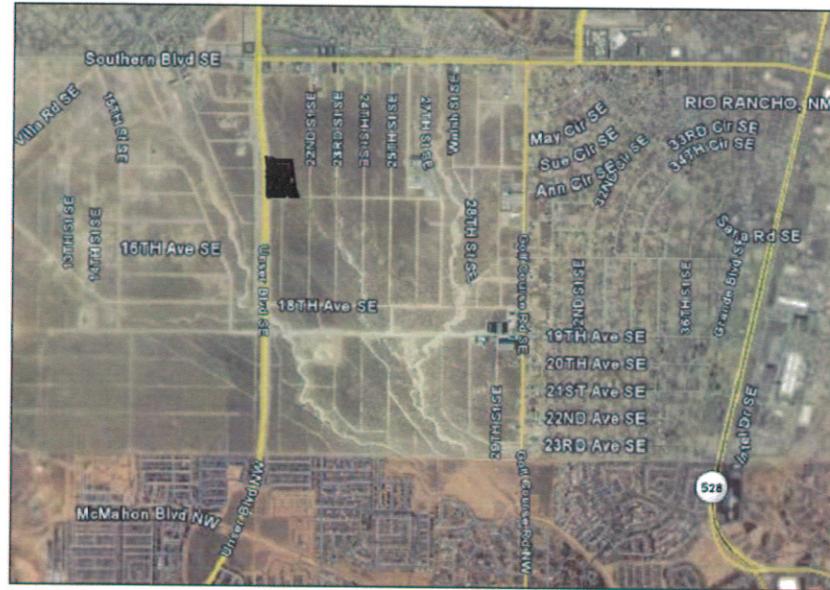
**CABEZON COMMONS
CABEZON TRACT 11
COMMERCIAL PROPERTY**

*Rio Rancho Estates Unit 16
Rio Rancho, New Mexico*

for

**CURB NORTH, LLC.
5160 SAN FRANCISCO NE
ALBUQUERQUE, NEW MEXICO 87109**

March 13, 2008

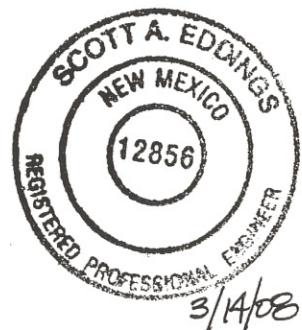


Prepared By:

**HUITT-ZOLLARS, Inc.
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**FINAL
DRAINAGE STUDY**

**CABEZON COMMONS
CABEZON TRACT 11
COMMERCIAL PROPERTY**



I, Scott A. Eddings, being first duly sworn, upon my oath state that I am a registered professional engineer, qualified in Civil engineering, and that the accompanying report was prepared by me or under my supervision and is true and correct to the best of my knowledge and belief.



Registered Professional Engineer

**DRAINAGE STUDY
FOR
CABEZON COMMONS
TRACT 11 COMMERCIAL PROPERTY**

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FINAL DRAINAGE STUDY FOR CABEZON COMMONS

PURPOSE

This drainage report addresses the storm water runoff and proposed infrastructure needed to convey the runoff from the Tract 11 Commercial Property of the Cabezon Redevelopment. This report will also demonstrate that the development of this project complies with the approved Cabezon Communities Phase I Drainage Management Plan and the Cabezon Communities Drainage Implementation Plan.

PROJECT LOCATION AND DESCRIPTION



Exhibit 1 – Vicinity Map

The project is located at the northeast corner of the intersection of Unser Boulevard and Cabezon Boulevard. See **Exhibit 1**. The site is a commercial tract that is currently undeveloped but has been cleared of natural vegetation. The development is bounded by; The Yucatan at Cabezon subdivision to the north and east, Cabezon Blvd to the south and Unser Blvd to the west.

ZONING AND PLATTING STATUS

The zoning for this project is C-1, Commercial, of approximately 10.36 acres. The project is located in Tract 11 within Rio Rancho Estates Unit 16. The site is being replatted to subdivide the property and this report is an attachment to the Preliminary Plat submittal for this project.

FLOOD HAZARD ZONES

Per FEMA's Flood Insurance Rate Map (FIRM) 35043C0894 C, dated July 16, 1996, no portion of the project site is located within a FEMA 100-year Flood Hazard Zone. See **Appendix A-1**.

JURISDICTIONS OF PUBLIC AGENCIES

Local

This project is located entirely within the City of Rio Rancho (CoRR) Municipal Limits and is therefore within their jurisdiction and must comply with the City's development requirements.

Regional

This project is located within the jurisdiction of the Southern Sandoval County Arroyo Flood Control Authority (SSCAFCA) and is therefore subject to their review.

RELATED REPORTS

The ***Cabezon Communities Phase I Drainage Management Plan (DMP)*** prepared by Wilson & Company, Engineers & Architects and dated February 2004. This study provides an overall drainage plan for this area, based on the Cabezon Communities Master Plan. The City and SSCAFCA approved the report. It determined the pre-developed drainage patterns for the area and the conceptual design for storm drain facilities in Cabezon.

The ***Cabezon Communities Drainage Implementation Plan (DIP)*** prepared by Wilson & Company, Engineers & Architects and dated February 19, 2004. This study provides permissible discharge rates for individual tracts and details the major infrastructure for the development.

The ***Final Drainage Study, Cabezon Redevelopment, Yucatan at Cabezon Subdivision*** prepared by Huitt-Zollars, Inc. and dated June 29, 2004. This study analyzed the developed runoff for Tract 3, which lies north and east of Tract 11. A review of this study indicates that Tract 3 is discharging less than allowed by the DMP. This finding was used as the basis for increasing the allowed discharge from Tract 11.

METHODOLOGY

This drainage study is based on the procedures outlined in the CoRR's "Grading and Drainage Design Requirements and Policies for Land Development in Rio Rancho (Revised 3-18-93)." That policy states, "The minimum criteria for hydrology and hydraulic calculations and design shall be as described in the Development Process Manual Section 22.2, City of Albuquerque (CoA DPM), latest revision, or the AHYMO version of the ARS HYMO Computer Program." This drainage study follows the procedures outlined in both the CoA DPM Section 22.2 and the AHYMO Computer Program.

PRECIPITATION

Because this project will utilize an on-site detention pond, the 100-yr 24-hr design storm was used for this analysis. The AHYMO Computer Program requires the 1, 6 and 24-hour precipitation values. These values were obtained from the ***Cabezon Communities Phase I DMP*** and are shown on **Table 1**.

Table 1
Precipitation Values

Return Period (yrs)	24 hr Rainfall (in)	6 hr Rainfall (in)	1 hr Rainfall (in)
100	2.7	2.2	1.8

LAND TREATMENTS

The land treatments used in the AHYMO Computer model are as described by Table A-4 of the CoA DPM Section 22.2, 1993 revision, and are summarized in **Table 2**.

Table 2
Land Treatment Classifications

Treatment	Land Condition
A	Soil uncompacted by human activity with 0 to 10 percent slopes. Native grasses, weeds and shrubs in typical densities with minimal disturbance to grading, groundcover and infiltration capacity. Croplands. Unlined Arroyos.
B	Irrigated lawns, parks and golf courses with 0 to 10 percent slopes. Soil uncompacted by human activity with slopes greater than 10 percent and less than 20 percent.
C	Soil compacted by human activity. Unpaved parking, roads and trail. Most vacant lots. Gravel or rock on plastic (desert landscaping)
D	Impervious areas, pavement and roofs.

The land treatments for Tract 11 were taken from the **Cabezon Communities Phase 1 DMP** and are as follows. **Historic**; %A = 95, %B = 5, %C = 0, and %D = 0. **Developed**; %A = 0, %B = 0, %C = 15, %D = 85.

STORM DRAIN HYDRAULICS

Storm Drains were modeled using Haestad Method's "StormCad" software. Head losses were entered based on the coefficients used in the Standard Method. The storm drain was designed based on peak discharges as indicated in the AHYMO model and the storm drain design is included in **Appendix D**.

EXISTING PRE-DEVELOPMENT CONDITIONS

The project site has been cleared of most vegetation and is rough graded. The site generally slopes from northwest to southeast. Runoff currently sheet flows off the site and into Cabezon Boulevard, where it is collected by an existing storm drain system. The existing storm drain for Cabezon Blvd is a 36" RCP, which lies behind the curb, on the north side of the street. It collects runoff via a series of grate inlets in the median of the street. Cabezon Blvd is reverse-crowned to facilitate the collection of runoff into the inlets.

A review of the **Final Drainage Study, Cabezon Redevelopment, Yucatan at Cabezon Subdivision** indicates that the discharge from Tract 3 is less than that allowed by the **Cabezon Communities Phase I DMP**. Based on this finding, it was

determined that Tract 11 would be allowed to discharge more than allowed by the DMP, to make up the difference from Tract 3.

ULTIMATE DEVELOPED CONDITIONS

The runoff from the commercial development will be collected by an on-site detention pond (**Pond A**) at the southeast corner of the property. A 24" RCP outfall pipe will drain **Pond A** into the existing storm drain system on the north side of Cabezon Blvd. This storm drain continues east on Cabezon Blvd, turns south on Trail Side Road and drains into the existing detention pond in Tract 17. The operation of **Pond A** is shown in **Table 3**.

Table 3
Onsite Detention Pond A 100-Yr Flood Routing Summary

Data / Result Description	Unit	DETENTION POND
Detention Pond AHYMO Hydrograph Number		POND.A
Return Period / Duration	Yr/ Hr	100/24
Total Drainage Area	Mi ²	0.0154
Inflow Time to Peak	Hrs	1.50
Inflow Peak Discharge	Ft ³ /s	44.4
Inflow Total Runoff Volume	Ac-ft	2.04
Outflow Time to Peak	Hrs	1.65
Outflow Peak Discharge	Ft ³ /s	26.59
Outflow Maximum Storage Volume at Peak	Ac-ft	0.4161
Outflow Total Runoff Volume	Ac-ft	2.04
Dead Storage Volume	Ac-Ft	N/A
Total Reservoir Storage Time	Hrs	24.00
Reservoir Invert Elevation	Ft	5322
Emergency Spillway Elevation	Ft	5326.5
Top of Embankment Elevation	Ft	5326.5
Maximum Water Surface Elevation	Ft	5325.59
Maximum Water Depth	Ft	3.59

CONCLUSION

Table 4 compares the findings of the analysis of Tract 11 with the results of both the approved **Cabezon Communities Phase I Drainage Management Plan** and the **Cabezon Communities Drainage Implementation Plan**. This comparison also includes Tract 3 in order to compare the total allowed runoff for the two Tracts to the actual discharge.

Table 4
Runoff Comparison for Tracts 3 & 11

Description	Tract 3 100-Yr Peak Discharge (Ft ³ /s)	Tract 11 100-Yr Peak Discharge (Ft ³ /s)	Total 100-Yr Peak Discharge (Ft ³ /s)
Wilson & Co. DMP	270	14	284
Wilson & Co. DIP	270	14	284
HZI Plan	256	26.59	282.59

As **Table 4** shows, the Wilson & Co. DMP allows for 14 cfs discharging from Tract 11 and 270 cfs discharging from Tract 3. The discharge from the developed Tract 11 is 26.59 cfs, and the discharge from the developed Tract 3 is 256 cfs. Since the total discharge of 282.59 is less than the total allowed discharge of 284 cfs, this report does comply with both the **Cabezon Communities Phase I Drainage Management Plan** and the **Cabezon Communities Drainage Implementation Plan**.

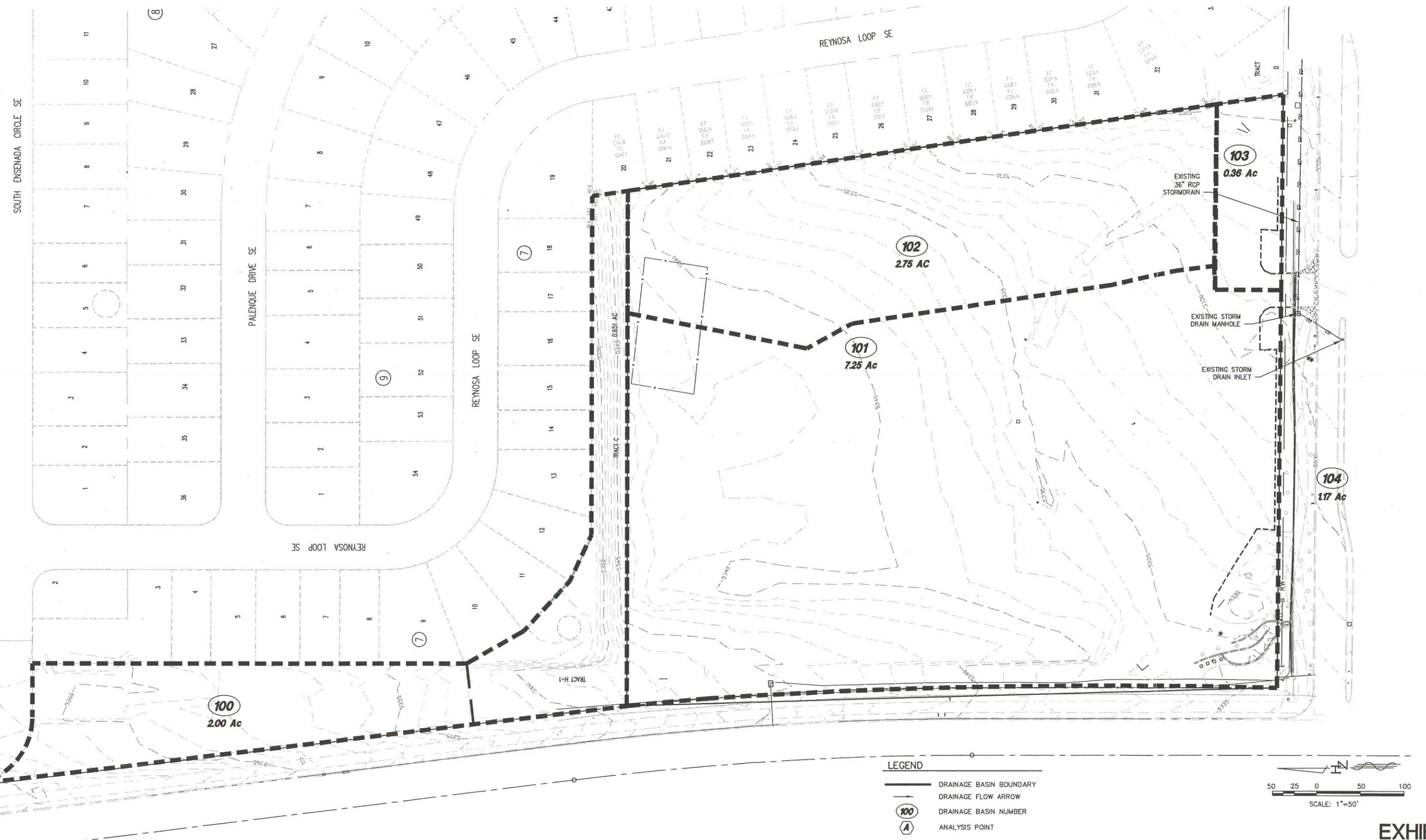


EXHIBIT 2

Designed For:

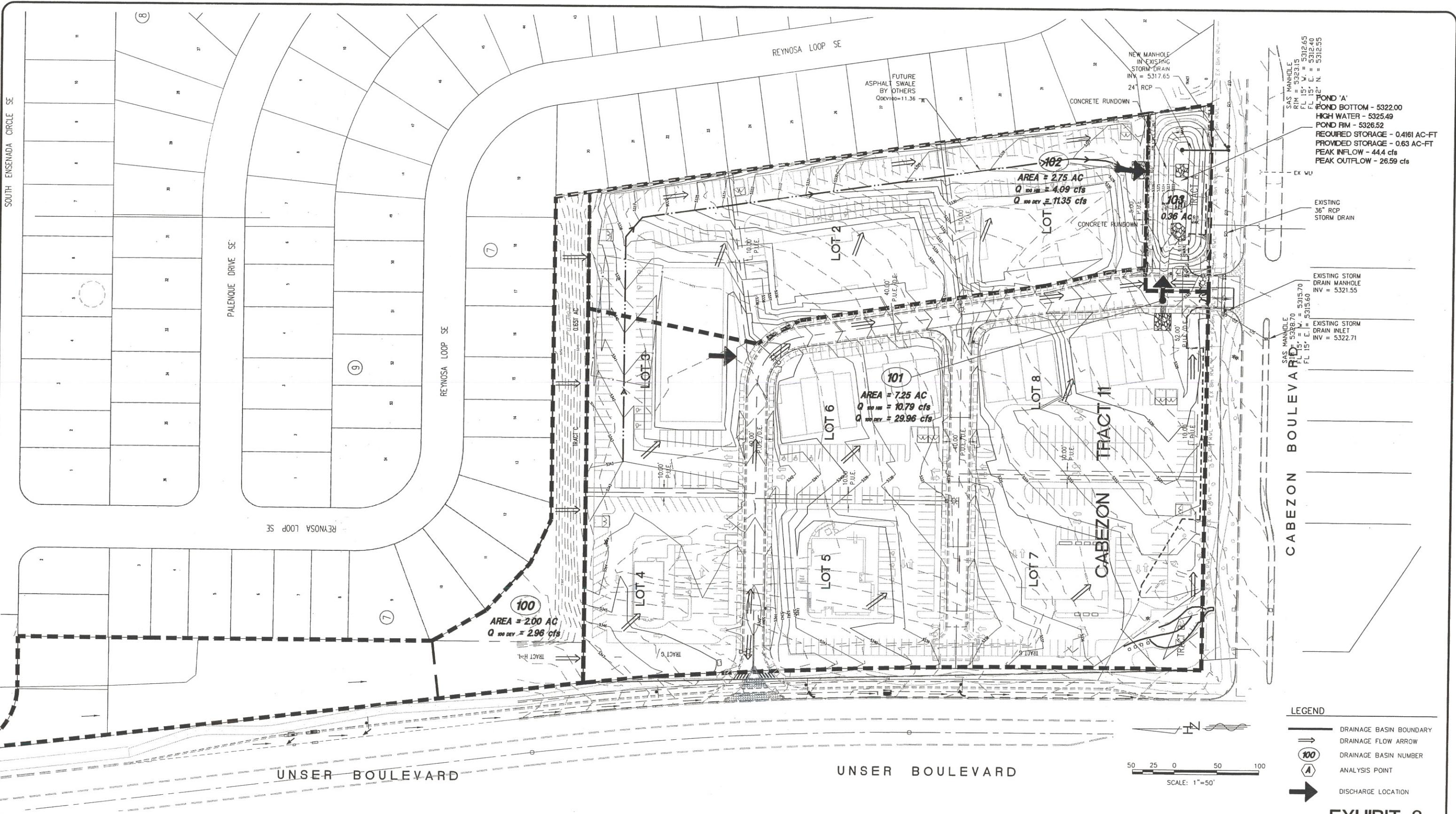
CURB NORTH, LLC

EXISTING BASIN MAP

CABEZON COMMONS
RIO RANCHO, NM

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Designed For:

CURB NORTH, LLC.

DEVELOPED BASIN MAP

CABEZON TRACT 11
RIO RANCHO, NM

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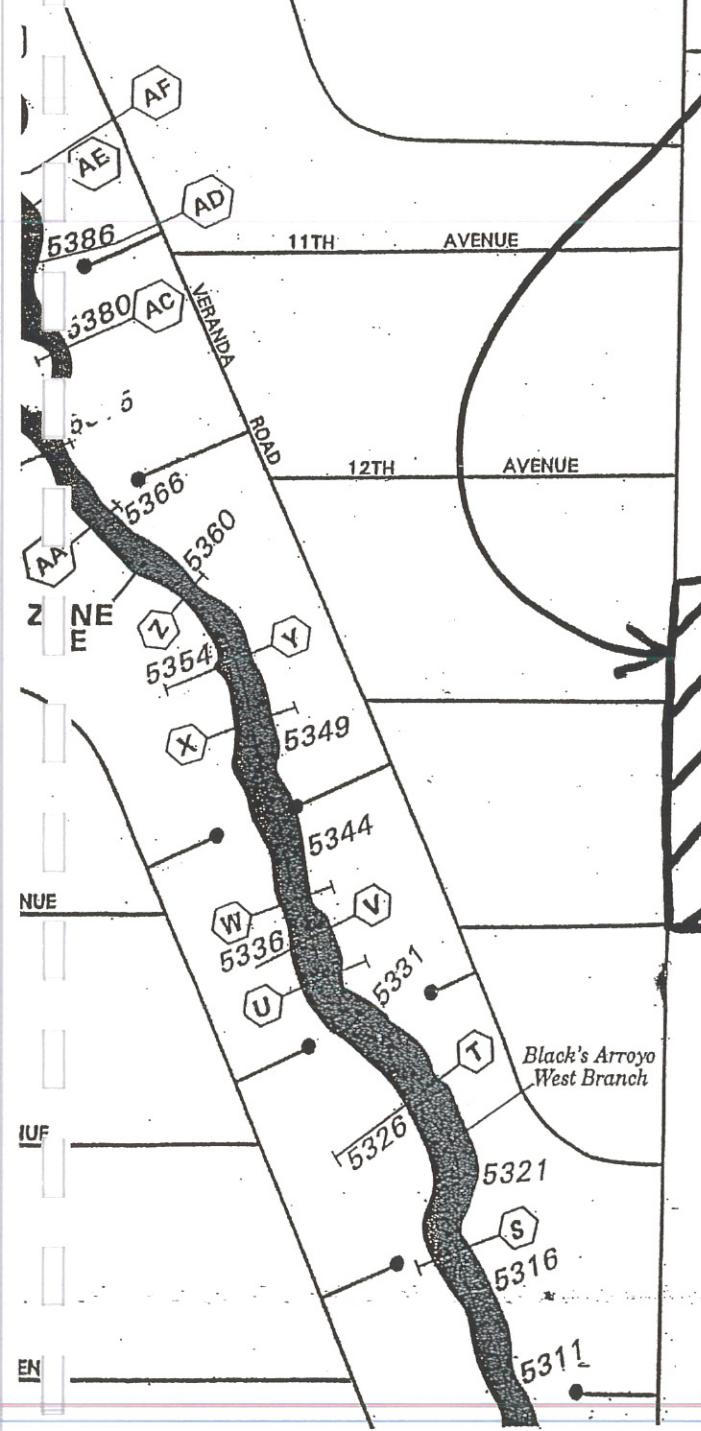
UNSER

BOULEVARD

SOUTHERN

BOULEVARD

Project
Area



FIRM
FLOOD INSURANCE RATE MAP

SANDOVAL COUNTY,
NEW MEXICO AND
INCORPORATED AREAS

(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:

COMMUNITY
RIO RANCHO, CITY OF

NUMBER 350140 PANEL 0894 SUFFIX C

MAP NUMBER
35043C0894 CEFFECTIVE DATE:
JULY 16, 1996

Federal Emergency Management Agency

Cabezon Tract 11
100-Year 24-Hour Duration Storm
AHYMO Summary File

67h8.5v0T_&18D
 HYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
 INPUT FILE = G:\Proj\170568-1\DRN_ST-1\AHYMO\CAB11--1.DAT

- VERSION: 1997.02c RUN DATE (MON/DAY/YR) =08/13/2007

USER NO.= AHYMO-I-9702a01000150-SH

COMMAND	HYDROGRAPH IDENTIFICATION	FROM NO.	TO ID	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1
										TIME= .00
START LOCATION										
*S										
*S CABEZON TRACT 11 COMMERCIAL										
*S										
*S FN:CAB11-COMM.DAT - HYMO PER JAN 1997 DPM REVISIONS										
*S										
*S										
RAINFALL TYPE= 2										RAIN24= 2.700
*S*****										
*S BULK FOR SEDIMENT - HISTORIC										PK BF = 1.18
SEDIMENT BULK										
*S										
*S COMPUTE OFFSITE BASIN HISTORIC										
COMPUTE NM HYD 100.HIS - 1				.00310	2.96	.084	.50620	1.500	1.493 PER IMP= .00	
*S										
*S COMPUTE ONSITE BASIN HISTORIC										
COMPUTE NM HYD 101.HIS - 2				.01131	10.79	.305	.50620	1.500	1.490 PER IMP= .00	
*S										
*S COMPUTE ONSITE BASIN HISTORIC										
COMPUTE NM HYD 102.HIS - 3				.00428	4.09	.116	.50620	1.500	1.492 PER IMP= .00	
*S										
*S COMPUTE ONSITE POND DEVELOPED										
COMPUTE NM HYD PONDA.DEV - 12				.00006	.13	.004	1.12644	1.500	3.509 PER IMP= .00	
*S										
*S BULK FOR SEDIMENT - DEVELOPED										PK BF = 1.05
SEDIMENT BULK										
*S										
*S COMPUTE ONSITE BASIN DEVELOPED										
COMPUTE NM HYD 101.DEV - 10				.01131	29.96	1.415	2.34567	1.500	4.139 PER IMP= 85.00	
*S										
*S COMPUTE ONSITE BASIN DEVELOPED										
COMPUTE NM HYD 102.DEV - 11				.00428	11.35	.535	2.34567	1.500	4.142 PER IMP= 85.00	
*S										
*S ADD HISTORIC OFFSITE BASIN 100 TO DEVELOPED ONSITE BASIN 101										
ADD HYD 20.00 1610 20 .01441 32.92 1.499 1.94992 1.500 3.569										
ADD ID 20 TO BASIN 102										
ADD HYD 21.00 11&20 21 .01869 44.27 2.034 2.04053 1.500 3.701										
*S										
*S ADD ID 21 TO POND										
ADD HYD 22.00 21&12 22 .01875 44.40 2.038 2.03760 1.500 3.700										
*S										
*S ROUTE THROUGH POND.A										
ROUTE RESERVOIR POND.A 22 7 .01875 26.59 2.038 2.03760 1.650 2.216 AC-FT= .416										
*S										
*S COMPUTE OFFSITE BASIN DEVELOPED										
COMPUTE NM HYD 103.DEV - 8 .00183 4.94 .237 2.42469 1.500 4.222 PER IMP= 90.00										
*S										
*S ADD POND.A TO CAB.BLVD										
ADD HYD STORMDRAIN 7 & 8 9 .02058 29.85 2.274 2.07199 1.600 2.266										
*S										
FINISH										
(s0p10h4099T_&16D_										

Cabezon Tract 11
100-Year 24-Hour Duration Storm
AHYMO Output File

67h8.5vOT_&18D

AHYMO PROGRAM (AHYMO_97) - Version: 1997.02c
 RUN DATE (MON/DAY/YR) = 08/13/2007
 START TIME (HR:MIN:SEC) = 10:24:39 USER NO.= AHYMO-I-9702a01000150-SH
 INPUT FILE = G:\Proj\170568-1\DRN_ST~1\AHYMO\CAB11~~1.DAT

START TIME=0.0 CODE 0 LINES -6
 LOCATION RIO RANCHO
 City of Rio Rancho soil infiltration values (LAND FACTORS) used for computations.
 Land Treatment Initial Abstr.(in) Unif. Infilt.(in/hour)
 A 0.65 1.67
 B 0.50 1.25
 C 0.35 0.83
 D 0.10 0.04

*S
 *S CABEZON TRACT 11 COMMERCIAL
 *S
 *S FN:CAB11-COMM.DAT - HYMO PER JAN 1997 DPM REVISIONS
 *S
 *S
 *S
 RAINFALL TYPE=-2 RAIN QUARTER=0.0 RAIN ONE=1.8
 RAIN SIX=2.2 RAIN DAY=2.7 DT=.05

COMPUTED 24-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.
 DT = .050000 HOURS END TIME = 24.000000 HOURS

*S*****
 *S BULK FOR SEDIMENT - HISTORIC
 SEDIMENT BULK CODE=1 BULK FACTOR=1.18
 *S-
 *S COMPUTE OFFSITE BASIN HISTORIC
 COMPUTE NM HYD ID=1 HYD=100.HIS AREA=0.0031 SQ MI
 %A=95 %B=5 %C=0 %D=0 TP=0.133 HR
 MASS RAINFALL=-1

K = .163419HR TP = .133000HR K/TP RATIO = 1.228711 SHAPE CONSTANT, N = 2.898105
 UNIT PEAK = 6.3726 CFS UNIT VOLUME = .9961 B = 273.41 P60 = 1.8000
 AREA = .003100 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.18000 AT PEAK FLOW.

PRINT HYD ID=1 CODE=10

HYDROGRAPH FROM AREA 100.HIS

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.000	.0	2.000	.3	3.000	.0
.500	.0	1.500	3.0	2.500	.1	3.500	.0

RUNOFF VOLUME = .50620 INCHES = .0837 ACRE-FEET
 PEAK DISCHARGE RATE = 2.96 CFS AT 1.500 HOURS BASIN AREA = .0031 SQ. MI.

*S-
 *S COMPUTE ONSITE BASIN HISTORIC

COMPUTE NM HYD ID=2 HYD=101.HIS AREA=0.01131 SQ MI
 %A=95 %B=5 %C=0 %D=0 TP=0.133 HR
 MASS RAINFALL=-1

K = .163419HR TP = .133000HR K/TP RATIO = 1.228711 SHAPE CONSTANT, N = 2.898105
 UNIT PEAK = 23.250 CFS UNIT VOLUME = .9977 B = 273.41 P60 = 1.8000
 AREA = .011310 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.18000 AT PEAK FLOW.

PRINT HYD ID=2 CODE=10

HYDROGRAPH FROM AREA 101.HIS

TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	TIME HRS	FLOW CFS
.000	.0	1.000	.0	2.000	1.0	3.000	.1
.500	.0	1.500	10.8	2.500	.4	3.500	.0

RUNOFF VOLUME = .50620 INCHES = .3053 ACRE-FEET
 PEAK DISCHARGE RATE = 10.79 CFS AT 1.500 HOURS BASIN AREA = .0113 SQ. MI.

*S-
 *S COMPUTE ONSITE BASIN HISTORIC

COMPUTE NM HYD ID=3 HYD=102.HIS AREA=0.00428 SQ MI
 %A=95 %B=5 %C=0 %D=0 TP=0.133 HR
 MASS RAINFALL=-1

K = .163419HR TP = .133000HR K/TP RATIO = 1.228711 SHAPE CONSTANT, N = 2.898105
 UNIT PEAK = 8.7983 CFS UNIT VOLUME = .9967 B = 273.41 P60 = 1.8000

Cabezon Tract 11
100-Year 24-Hour Duration Storm
AHYMO Output File

AREA = .004280 SQ MI IA = .64250 INCHES INF = 1.64900 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.18000 AT PEAK FLOW.

PRINT HYD ID=3 CODE=10

HYDROGRAPH FROM AREA 102.HIS

TIME HRS	FLOW CFS								
.000	.0	1.000	.0	2.000	.4	3.000	.0	4.000	.0
.500	.0	1.500	4.1	2.500	.1	3.500	.0		

RUNOFF VOLUME = .50620 INCHES = .1155 ACRE-FEET
 PEAK DISCHARGE RATE = 4.09 CFS AT 1.500 HOURS BASIN AREA = .0043 SQ. MI.

*S-----

*S COMPUTE ONSITE POND DEVELOPED
 COMPUTE NM HYD ID=12 HYD=PONDA.DEV AREA=0.00006 SQ MI
 %A=0 %B=0 %C=100 %D=0 TP=0.133 HR
 MASS RAINFALL=-1

K = .104841HR TP = .133000HR K/TP RATIO = .788276 SHAPE CONSTANT, N = 4.552994
 UNIT PEAK = .17616 CFS UNIT VOLUME = .9337 B = 390.49 P60 = 1.8000
 AREA = .000060 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.18000 AT PEAK FLOW.

PRINT HYD ID=12 CODE=10

HYDROGRAPH FROM AREA PONDA.DEV

TIME HRS	FLOW CFS								
.000	.0	.500	.0	1.000	.0	1.500	.1	2.000	.0

RUNOFF VOLUME = 1.12644 INCHES = .0036 ACRE-FEET
 PEAK DISCHARGE RATE = .13 CFS AT 1.500 HOURS BASIN AREA = .0001 SQ. MI.

S-----

S BULK FOR SEDIMENT - DEVELOPED
 SEDIMENT BULK CODE=1 BULK FACTOR=1.05

*S-----

*S COMPUTE ONSITE DRAIN DEVELOPED
 COMPUTE NM HYD ID=10 HYD=101.DEV AREA=0.01131 SQ MI
 %A=0 %B=0 %C=15 %D=85 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 38.040 CFS UNIT VOLUME = .9989 B = 526.28 P60 = 1.8000
 AREA = .009614 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .104841HR TP = .133000HR K/TP RATIO = .788276 SHAPE CONSTANT, N = 4.552994
 UNIT PEAK = 4.9809 CFS UNIT VOLUME = .9992 B = 390.49 P60 = 1.8000
 AREA = .001697 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=10 CODE=10

HYDROGRAPH FROM AREA 101.DEV

TIME HRS	FLOW CFS								
.000	.0	5.000	.2	10.000	.2	15.000	.2	20.000	.1
.500	.0	5.500	.2	10.500	.2	15.500	.2	20.500	.1
1.000	.1	6.000	.3	11.000	.2	16.000	.2	21.000	.1
1.500	30.0	6.500	.3	11.500	.2	16.500	.2	21.500	.1
2.000	7.0	7.000	.3	12.000	.2	17.000	.2	22.000	.1
2.500	1.0	7.500	.3	12.500	.2	17.500	.2	22.500	.1
3.000	.4	8.000	.2	13.000	.2	18.000	.2	23.000	.1
3.500	.3	8.500	.2	13.500	.2	18.500	.2	23.500	.1
4.000	.2	9.000	.2	14.000	.2	19.000	.1	24.000	.1
4.500	.2	9.500	.2	14.500	.2	19.500	.1	24.500	.0

RUNOFF VOLUME = 2.34567 INCHES = 1.4149 ACRE-FEET
 PEAK DISCHARGE RATE = 29.96 CFS AT 1.500 HOURS BASIN AREA = .0113 SQ. MI.

*S-----

*S COMPUTE ONSITE BASIN DEVELOPED
 COMPUTE NM HYD ID=11 HYD=102.DEV AREA=0.00428 SQ MI
 %A=0 %B=0 %C=15 %D=85 TP=0.133 HR
 MASS RAINFALL=-1

Cabezon Tract 11
100-Year 24-Hour Duration Storm
AHYMO Output File

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 14.395 CFS UNIT VOLUME = .9983 B = 526.28 P60 = 1.8000
 AREA = .003638 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .104841HR TP = .133000HR K/TP RATIO = .788276 SHAPE CONSTANT, N = 4.552994
 UNIT PEAK = 1.8849 CFS UNIT VOLUME = .9954 B = 390.49 P60 = 1.8000
 AREA = .000642 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=11 CODE=10

HYDROGRAPH FROM AREA 102.DEV

TIME HRS	FLOW CFS						
.000	.0	5.000	.1	10.000	.1	15.000	.1
.500	.0	5.500	.1	10.500	.1	15.500	.1
1.000	.0	6.000	.1	11.000	.1	16.000	.1
1.500	11.3	6.500	.1	11.500	.1	16.500	.1
2.000	2.7	7.000	.1	12.000	.1	17.000	.1
2.500	.4	7.500	.1	12.500	.1	17.500	.1
3.000	.1	8.000	.1	13.000	.1	18.000	.1
3.500	.1	8.500	.1	13.500	.1	18.500	.1
4.000	.1	9.000	.1	14.000	.1	19.000	.1
4.500	.1	9.500	.1	14.500	.1	19.500	.1

RUNOFF VOLUME = 2.34567 INCHES = .5354 ACRE-FEET
 PEAK DISCHARGE RATE = 11.35 CFS AT 1.500 HOURS BASIN AREA = .0043 SQ. MI.

*S-----
 *S ADD HISTORIC OFFSITE BASIN 100 TO DEVELOPED ONSITE BASIN 101
 ADD HYD ID=20 HYD=20 IDS 1 AND 10
 PRINT HYD ID=20 CODE=10

OUTFLOW HYDROGRAPH REACH 20.00

TIME HRS	FLOW CFS						
.000	.0	5.000	.2	10.000	.2	15.000	.2
.500	.0	5.500	.2	10.500	.2	15.500	.2
1.000	.1	6.000	.3	11.000	.2	16.000	.2
1.500	32.9	6.500	.3	11.500	.2	16.500	.2
2.000	7.0	7.000	.3	12.000	.2	17.000	.2
2.500	1.1	7.500	.3	12.500	.2	17.500	.2
3.000	.4	8.000	.2	13.000	.2	18.000	.2
3.500	.3	8.500	.2	13.500	.2	18.500	.2
4.000	.2	9.000	.2	14.000	.2	19.000	.1
4.500	.2	9.500	.2	14.500	.2	19.500	.0

RUNOFF VOLUME = 1.94992 INCHES = 1.4986 ACRE-FEET
 PEAK DISCHARGE RATE = 32.92 CFS AT 1.500 HOURS BASIN AREA = .0144 SQ. MI.

*S-----
 *S ADD ID 20 TO BASIN 102
 ADD HYD ID=21 HYD=21 IDS 11 AND 20
 PRINT HYD ID=21 CODE=10

OUTFLOW HYDROGRAPH REACH 21.00

TIME HRS	FLOW CFS						
.000	.0	5.000	.3	10.000	.3	15.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2
1.000	.2	6.000	.4	11.000	.3	16.000	.2
1.500	44.3	6.500	.4	11.500	.3	16.500	.2
2.000	9.9	7.000	.4	12.000	.3	17.000	.2
2.500	1.5	7.500	.3	12.500	.3	17.500	.2
3.000	.6	8.000	.3	13.000	.3	18.000	.2
3.500	.4	8.500	.3	13.500	.3	18.500	.2
4.000	.3	9.000	.3	14.000	.2	19.000	.2
4.500	.3	9.500	.3	14.500	.2	19.500	.0

RUNOFF VOLUME = 2.04053 INCHES = 2.0340 ACRE-FEET
 PEAK DISCHARGE RATE = 44.27 CFS AT 1.500 HOURS BASIN AREA = .0187 SQ. MI.

*S-----
 *S ADD ID 21 TO POND
 ADD HYD ID=22 HYD=22 IDS 21 AND 12
 PRINT HYD ID=22 CODE=10

OUTFLOW HYDROGRAPH REACH 22.00

TIME	FLOW								
------	------	------	------	------	------	------	------	------	------

Cabezon Tract 11
100-Year 24-Hour Duration Storm
AHYMO Output File

HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	.3	10.000	.3	15.000	.2	20.000	.2
.500	.0	5.500	.3	10.500	.3	15.500	.2	20.500	.2
1.000	.2	6.000	.4	11.000	.3	16.000	.2	21.000	.2
1.500	44.4	6.500	.4	11.500	.3	16.500	.2	21.500	.2
2.000	9.9	7.000	.4	12.000	.3	17.000	.2	22.000	.2
2.500	1.5	7.500	.3	12.500	.3	17.500	.2	22.500	.2
3.000	.6	8.000	.3	13.000	.3	18.000	.2	23.000	.2
3.500	.4	8.500	.3	13.500	.3	18.500	.2	23.500	.2
4.000	.3	9.000	.3	14.000	.2	19.000	.2	24.000	.2
4.500	.3	9.500	.3	14.500	.2	19.500	.2	24.500	.0

RUNOFF VOLUME = 2.03760 INCHES = 2.0376 ACRE-FEET
 PEAK DISCHARGE RATE = 44.40 CFS AT 1.500 HOURS BASIN AREA = .0188 SQ. MI.

*S-----
 *S ROUTE THROUGH POND.A
 ROUTE RESERVOIR

ID=7 HYD=POND.A INFLOW=22 CODE=10
 OUTFLOW STORAGE ELEV
 0.00 0.00 5322.0
 3.92 0.062 5323.0
 13.27 0.165 5324.0
 23.25 0.313 5325.0
 29.64 0.510 5326.0

* * * * *

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
---------------	-----------------	----------------	-------------------	------------------

.00	.00	5322.00	.000	.00
.50	.00	5322.00	.000	.00
1.00	.17	5322.01	.000	.02
1.50	44.40	5324.94	.305	22.70
2.00	9.94	5324.28	.206	16.05
2.50	1.46	5322.75	.046	2.92
3.00	.57	5322.23	.014	.91
3.50	.37	5322.11	.007	.45
4.00	.31	5322.09	.005	.34
4.50	.30	5322.08	.005	.30
5.00	.31	5322.08	.005	.30
5.50	.32	5322.08	.005	.32
6.00	.35	5322.09	.005	.34
6.50	.37	5322.09	.006	.37
7.00	.36	5322.09	.006	.36
7.50	.35	5322.09	.006	.35
8.00	.34	5322.09	.005	.34
8.50	.33	5322.08	.005	.33
9.00	.32	5322.08	.005	.32
9.50	.31	5322.08	.005	.31
10.00	.30	5322.08	.005	.30
10.50	.29	5322.08	.005	.30
11.00	.29	5322.07	.005	.29
11.50	.28	5322.07	.004	.28
12.00	.27	5322.07	.004	.27
12.50	.26	5322.07	.004	.27
13.00	.26	5322.07	.004	.26
13.50	.25	5322.07	.004	.26
14.00	.25	5322.06	.004	.25
14.50	.24	5322.06	.004	.24
15.00	.24	5322.06	.004	.24
15.50	.23	5322.06	.004	.23
16.00	.23	5322.06	.004	.23
16.50	.22	5322.06	.004	.23
17.00	.22	5322.06	.004	.22
17.50	.22	5322.06	.003	.22
18.00	.21	5322.05	.003	.21
18.50	.21	5322.05	.003	.21
19.00	.21	5322.05	.003	.21
19.50	.20	5322.05	.003	.20
20.00	.20	5322.05	.003	.20
20.50	.20	5322.05	.003	.20
21.00	.19	5322.05	.003	.19
21.50	.19	5322.05	.003	.19
22.00	.18	5322.05	.003	.19
22.50	.19	5322.05	.003	.18
23.00	.18	5322.05	.003	.18
23.50	.18	5322.05	.003	.18
24.00	.17	5322.04	.003	.18
24.50	.01	5322.01	.001	.04
25.00	.00	5322.00	.000	.00

PEAK DISCHARGE = 26.593 CFS - PEAK OCCURS AT HOUR 1.65

MAXIMUM WATER SURFACE ELEVATION = 5325.523

MAXIMUM STORAGE = .4161 AC-FT INCREMENTAL TIME=.050000HRS

PRINT HYD

ID=7 CODE=10

HYDROGRAPH FROM AREA POND.A

TIME HRS	FLOW CFS								
.000	.0	5.500	.3	11.000	.3	16.500	.2	22.000	.2

Cabezon Tract 11
100-Year 24-Hour Duration Storm
AHYMO Output File

.500	.0	6.000	.3	11.500	.3	17.000	.2	22.500	.2
1.000	.0	6.500	.4	12.000	.3	17.500	.2	23.000	.2
1.500	22.7	7.000	.4	12.500	.3	18.000	.2	23.500	.2
2.000	16.0	7.500	.4	13.000	.3	18.500	.2	24.000	.2
2.500	2.9	8.000	.3	13.500	.3	19.000	.2	24.500	.0
3.000	.9	8.500	.3	14.000	.2	19.500	.2	25.000	.0
3.500	.4	9.000	.3	14.500	.2	20.000	.2		
4.000	.3	9.500	.3	15.000	.2	20.500	.2		
4.500	.3	10.000	.3	15.500	.2	21.000	.2		
5.000	.3	10.500	.3	16.000	.2	21.500	.2		

RUNOFF VOLUME = 2.03760 INCHES = 2.0376 ACRE-FEET
 PEAK DISCHARGE RATE = 26.59 CFS AT 1.650 HOURS BASIN AREA = .0188 SQ. MI.

*S-----
 *S COMPUTE OFFSITE BASIN DEVELOPED
 COMPUTE NM HYD ID=8 HYD=103 DEV AREA=0.00183 SQ MI
 %A=0 %B=0 %C=10 %D=90 TP=0.133 HR
 MASS RAINFALL=-1

K = .072485HR TP = .133000HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420
 UNIT PEAK = 6.5171 CFS UNIT VOLUME = .9976 B = 526.28 P60 = 1.8000
 AREA = .001647 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

K = .104841HR TP = .133000HR K/TP RATIO = .788276 SHAPE CONSTANT, N = 4.552994
 UNIT PEAK = .53729 CFS UNIT VOLUME = .9793 B = 390.49 P60 = 1.8000
 AREA = .000183 SQ MI IA = .35000 INCHES INF = .83000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .050000

BULKING FACTOR APPLIED TO HYDROGRAPH. FACTOR = 1.05000 AT PEAK FLOW.

PRINT HYD ID=8 CODE=10

HYDROGRAPH FROM AREA 103.DEV

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.000	.0	10.000	.0	15.000	.0	20.000	.0
.500	.0	5.500	.0	10.500	.0	15.500	.0	20.500	.0
1.000	.0	6.000	.0	11.000	.0	16.000	.0	21.000	.0
1.500	4.9	6.500	.0	11.500	.0	16.500	.0	21.500	.0
2.000	1.2	7.000	.0	12.000	.0	17.000	.0	22.000	.0
2.500	.2	7.500	.0	12.500	.0	17.500	.0	22.500	.0
3.000	.1	8.000	.0	13.000	.0	18.000	.0	23.000	.0
3.500	.0	8.500	.0	13.500	.0	18.500	.0	23.500	.0
4.000	.0	9.000	.0	14.000	.0	19.000	.0	24.000	.0
4.500	.0	9.500	.0	14.500	.0	19.500	.0	24.500	.0

RUNOFF VOLUME = 2.42469 INCHES = .2366 ACRE-FEET
 PEAK DISCHARGE RATE = 4.94 CFS AT 1.500 HOURS BASIN AREA = .0018 SQ. MI.

*S-----
 *S ADD POND.A TO CAB.BLVD
 ADD HYD ID=9 HYD=STORMDRAIN IDi=7 IDii=8
 PRINT HYD ID=9 CODE=10

HYDROGRAPH FROM AREA STORMDRAIN

TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW	TIME	FLOW
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
.000	.0	5.500	.4	11.000	.3	16.500	.3	22.000	.2
.500	.0	6.000	.4	11.500	.3	17.000	.2	22.500	.2
1.000	.0	6.500	.4	12.000	.3	17.500	.2	23.000	.2
1.500	27.6	7.000	.4	12.500	.3	18.000	.2	23.500	.2
2.000	17.2	7.500	.4	13.000	.3	18.500	.2	24.000	.2
2.500	3.1	8.000	.4	13.500	.3	19.000	.2	24.500	.0
3.000	1.0	8.500	.4	14.000	.3	19.500	.2	25.000	.0
3.500	.5	9.000	.4	14.500	.3	20.000	.2		
4.000	.4	9.500	.4	15.000	.3	20.500	.2		
4.500	.3	10.000	.3	15.500	.3	21.000	.2		
5.000	.3	10.500	.3	16.000	.3	21.500	.2		

RUNOFF VOLUME = 2.07199 INCHES = 2.2742 ACRE-FEET
 PEAK DISCHARGE RATE = 29.85 CFS AT 1.600 HOURS BASIN AREA = .0206 SQ. MI.

*S-----
 FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 10:24:39

(s0p10h4099T_&16D

Detention Pond Rating Curve

POND A

Pond Designation 6:1 SIDE SLOPES

Elevation	Area	Average Area	Volume	Accumulative Volume
	sf	sf	Ac-Ft	Ac-Ft
5322.0	1900			
		2708	0.062	0.062
5323.0	3516			
		4466	0.103	0.165
5324.0	5415			
		6466	0.148	0.313
5325.0	7516			
		8633	0.198	0.511
5326.0	9750			
		5191	0.119	0.630
5326.5	11013			
		0	0.000	0.630
5326.5	11013			

Rating Table Report

POND A OUTFALL

Range Data:

	Minimum	Maximum	Increment
Allowable HW E	5,322.00	5,326.00	0.50 ft

HW Elev. (ft)	Discharge (cfs)
5,322.00	0.00
5,322.50	1.05
5,323.00	3.92
5,323.50	8.17
5,324.00	13.27
5,324.50	18.66
5,325.00	23.25
5,325.50	26.64
5,326.00	29.64

Cross Section

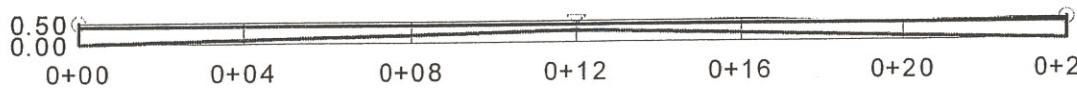
Cross Section for Irregular Channel

Project Description

Worksheet	24' WIDE PAVEMENT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Discharge

Section Data

Mannings Coefficie ^r	0.01600
Channel Slope	0.028000 ft/ft
Water Surface Elev.	0.40 ft
Elevation Range	.00 to 0.50
Discharge	36.20 cfs



V:1
H:1
NTS

$$Q_{100 \text{ YR}} = 29.96 \text{ cfs} \therefore \underline{\underline{\text{OK}}}$$

Concrete Valley within roadway must
carry approx. 15 cfs.

C-3

Cross Section

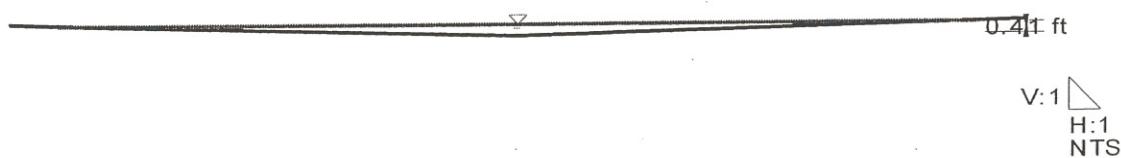
Cross Section for Triangular Channel

Project Description

Worksheet	Triangular Channe
Flow Element	Triangular Channe
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coeffic	0.016
Channel Slope	020000 ft/ft
Depth	0.41 ft → <u>OK</u> <u>0.5' TBC</u>
Left Side Slope	40.00 H : V
Right Side Slope	40.00 H : V
Discharge	30.00 cfs



Paving transition for pond Rundown

Basin 101

C4

Cross Section

Cross Section for Rectangular Channel

Project Description

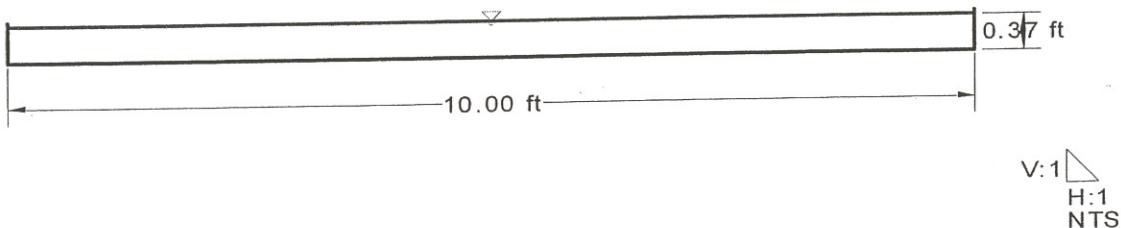
Worksheet	Rectangular Chann
Flow Element	Rectangular Chann
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coeffic	0.013
Channel Slope	020000 ft/ft
Depth	0.37 ft
Bottom Width	10.00 ft
Discharge	29.96 cfs

→ OK

Actual Depth of Channel = 0.5'



V:1
H:1
NTS

Concrete Channel @ Pond Inlet

Basin 101

L-5

Cross Section

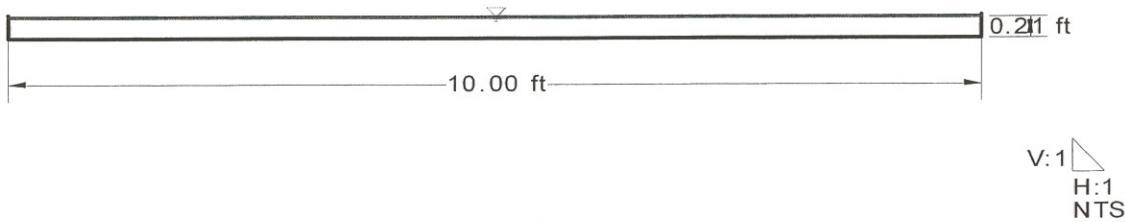
Cross Section for Rectangular Channel

Project Description

Worksheet CONCRETE RUNDOW
Flow Element Rectangular Channel
Method Manning's Formula
Solve For Channel Depth

Section Data

Mannings Coeffic 0.013
Channel Slope 020000 ft/ft
Depth 0.21 ft - OK - channel height is 0.5'
Bottom Width 10.00 ft
Discharge 11.35 cfs



Basin 102

C-6

Asphalt Swale Parking Area - Basin 102

Worksheet for Triangular Channel

Project Description

Worksheet Asphalt Swale - Basin
Flow Element Triangular Channel
Method Manning's Formula
Solve For Channel Depth

Input Data

Mannings Coeffic 0.020
Channel Slope 010000 ft/ft
Left Side Slope 50.00 H : V
Right Side Slope 50.00 H : V
Discharge 11.40 cfs

Results

Depth 0.32 ft
Flow Area 5.2 ft²
Wetted Perime 32.23 ft
Top Width 32.23 ft
Critical Depth 0.32 ft
Critical Slope 0.010768 ft/ft
Velocity 2.20 ft/s
Velocity Head 0.07 ft
Specific Energ 0.40 ft
Froude Number 0.96
Flow Type Subcritical

24" Sidewalk Culvert
Worksheet for Rectangular Channel

Project Description	
Worksheet	24" Sidewalk Culvert
Flow Element	Rectangular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data	
Mannings Coeffic	0.013
Channel Slope	020000 ft/ft
Depth	0.40 ft
Bottom Width	2.00 ft

Results	
Discharge	5.61 cfs
Flow Area	0.8 ft ²
Wetted Perimetr	2.80 ft
Top Width	2.00 ft
Critical Depth	0.63 ft
Critical Slope	0.005503 ft/ft
Velocity	7.01 ft/s
Velocity Head	0.76 ft
Specific Energy	1.16 ft
Froude Number	1.95
Flow Type	Supercritical

— 11.4 Required. Use 3·24" S.W.C.

Combined Pipe\Node Report

Label	Length (ft)	Section Size	Total Flow (cfs)	Full Capacity (cfs)	Average Velocity (ft/s)	Upstream Node	Downstream Node	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Constructed Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Ground Grade Line In (ft)	Ground Grade Line Out (ft)	Downstream Ground Elevation (ft)
P-1	58.00	24 inch	4.94	31.99	7.39	I-1	J-1	5,322.71	5,321.55	0.020000	5,323.49	5,327.70	5,322.39	5,328.57
P-2	195.00	36 inch	4.94	94.32	7.05	J-1	J-2	5,321.55	5,317.65	0.020000	5,322.25	5,328.57	5,319.86	5,324.00
P-3	92.00	36 inch	29.92	94.32	11.84	J-2	O-1	5,317.65	5,315.81	0.020000	5,319.42	5,324.00	5,317.02	5,323.00
P-4	55.00	24 inch	24.98	63.62	19.03	I-2	J-2	5,322.00	5,317.65	0.079091	5,323.76	5,326.00	5,319.86	5,324.00

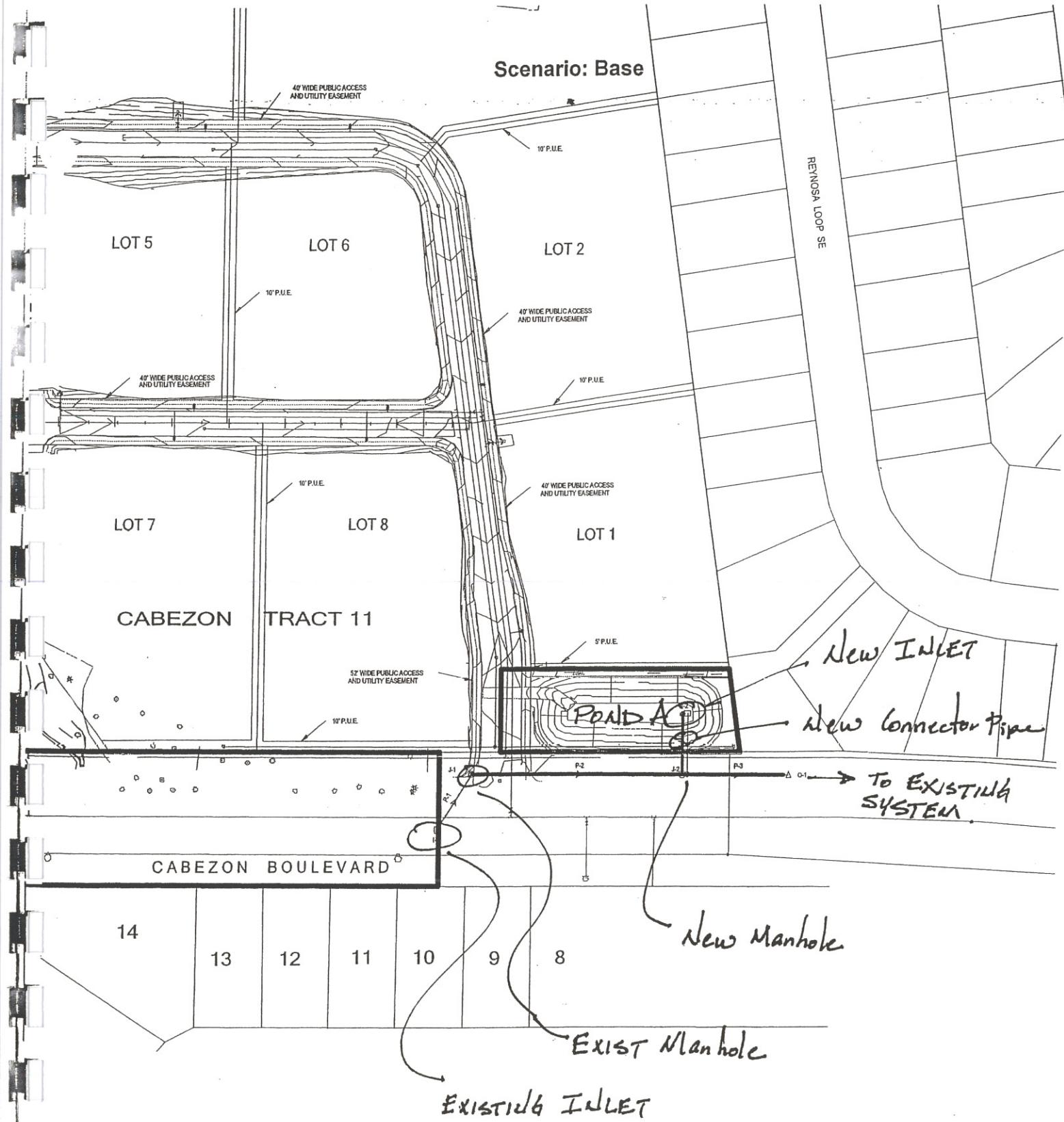
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 09/15/06 09:57:24 AM

Huitt-Zollars, Inc. 37 Brookside Road Waterbury, CT 06708 USA +1-203-755-1666
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Project Engineer: hzi
 StormCAD v5.5 [5.5.5003]
 Page 1 of 1

D-1

Scenario: Base



D-2