

SUPPLEMENTAL CALCULATIONS

LOWE'S SUBDIVISION, LOT 3



Fred C. Arfman
01.24.12

JANUARY 24, 2012



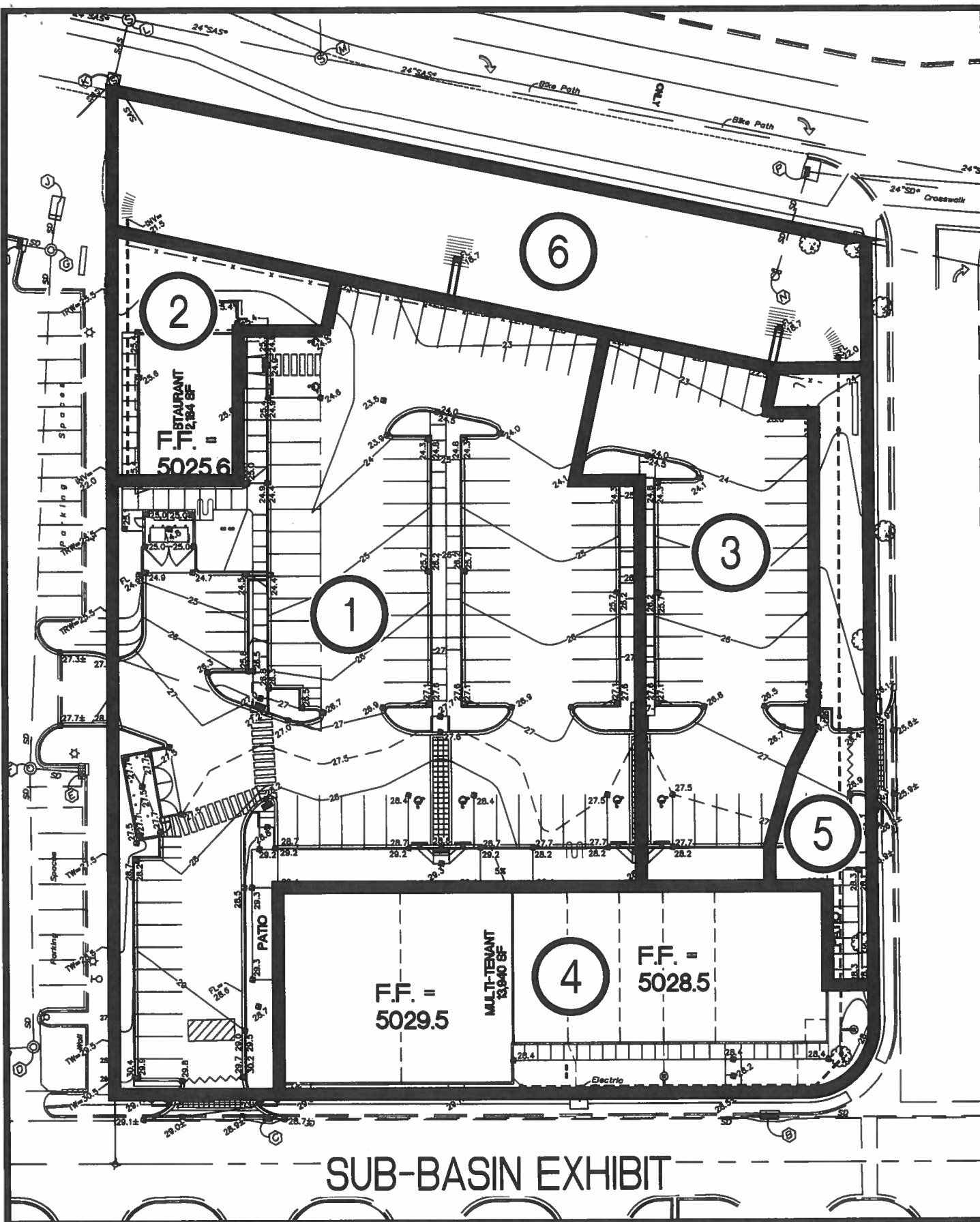
ISAACSON & ARFMAN, P.A.

Consulting Engineering Associates
Albuquerque, New Mexico

1899 CO-101.dwg Jan 24, 2012

PROJECT Lowe's Subdivision - Lot 3

JOB NO. 1899 BY BJB DATE 01-24-12



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North Arrow

AREA OF SITE: 102163 SF = 2.3

100-year, 6-hour

HISTORIC FLOWS:

DEVELOPED FLOWS:

EXCESS PRECIP:

| | Treatment SF | % | | Treatment SF | % | Precip. Zone | 1 |
|--------------|--------------|------|--------------|--------------|------|----------------|--------|
| Area A = | 20432.6 | 20% | Area A = | 0 | 0% | E _A | = 0.44 |
| Area B = | 71514.1 | 70% | Area B = | 10216 | 10% | E _B | = 0.67 |
| Area C = | 10216.3 | 10% | Area C = | 15324 | 15% | E _C | = 0.99 |
| Area D = | 0 | 0% | Area D = | 76622 | 75% | E _D | = 1.97 |
| Total Area = | 102163 | 100% | Total Area = | 102163 | 100% | | |

On-Site Weighted Excess Precipitation (100-Year, 6-Hour Storm)

$$\text{Weighted E} = \frac{E_A A_A + E_B A_B + E_C A_C + E_D A_D}{A_A + A_B + A_C + A_D}$$

| | | | | | |
|------------|---|----------|-------------|---|----------|
| Historic E | = | 0.66 in. | Developed E | = | 1.69 in. |
|------------|---|----------|-------------|---|----------|

On-Site Volume of Runoff: $V_{360} = E * A / 12$

| | | | | | |
|--------------------|---|---------|---------------------|---|----------|
| Historic V_{360} | = | 5585 CF | Developed V_{360} | = | 14413 CF |
|--------------------|---|---------|---------------------|---|----------|

On-Site Peak Discharge Rate: $Q_p = Q_{pA} A_A + Q_{pB} A_B + Q_{pC} A_C + Q_{pD} A_D / 43,560$

For Precipitation Zone 1

| | | | | | |
|----------|---|------|----------|---|------|
| Q_{pA} | = | 1.29 | Q_{pC} | = | 2.87 |
| Q_{pB} | = | 2.03 | Q_{pD} | = | 4.37 |

| | | | | | |
|----------------|---|---------|-----------------|---|---------|
| Historic Q_p | = | 4.6 CFS | Developed Q_p | = | 9.2 CFS |
|----------------|---|---------|-----------------|---|---------|

OVERALL BASIN CALCULATIONS



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| | | | |
|--|----------|-----------------------|---------------------------------|
| BASIN NO. | 1 | DESCRIPTION | DRAINS TO CENTER RUNDOWN |
| Area of basin flows = | 44900 SF | = | 1.0 Ac. |
| The following calculations are based on Treatment areas as shown in table to the right | | LAND TREATMENT | |
| Sub-basin Weighted Excess Precipitation (see formula above) | | A = 0% | |
| Weighted E = 1.89 in. | | B = 0% | |
| Sub-basin Volume of Runoff (see formula above) | | C = 8% | |
| V ₃₆₀ = 7078 CF | | D = 92% | |
| Sub-basin Peak Discharge Rate: (see formula above) | | | |
| Q _P = 4.4 cfs | | | |

| | | | |
|--|----------|-----------------------|--|
| BASIN NO. | 2 | DESCRIPTION | DRAINS TO PHASE II STORM DRAIN SYSTEM |
| Area of basin flows = | 5254 SF | = | 0.1 Ac. |
| The following calculations are based on Treatment areas as shown in table to the right | | LAND TREATMENT | |
| Sub-basin Weighted Excess Precipitation (see formula above) | | A = 0% | |
| Weighted E = 1.69 in. | | B = 10% | |
| Sub-basin Volume of Runoff (see formula above) | | C = 15% | |
| V ₃₆₀ = 741 CF | | D = 75% | |
| Sub-basin Peak Discharge Rate: (see formula above) | | | |
| Q _P = 0.5 cfs | | | |

| | | | |
|--|----------|-----------------------|-------------------------------|
| BASIN NO. | 3 | DESCRIPTION | DRAINS TO EAST RUNDOWN |
| Area of basin flows = | 13422 SF | = | 0.3 Ac. |
| The following calculations are based on Treatment areas as shown in table to the right | | LAND TREATMENT | |
| Sub-basin Weighted Excess Precipitation (see formula above) | | A = 0% | |
| Weighted E = 1.92 in. | | B = 0% | |
| Sub-basin Volume of Runoff (see formula above) | | C = 5% | |
| V ₃₆₀ = 2149 CF | | D = 95% | |
| Sub-basin Peak Discharge Rate: (see formula above) | | | |
| Q _P = 1.3 cfs | | | |

| | | | |
|--|----------|-----------------------|--|
| BASIN NO. | 4 | DESCRIPTION | DRAINS TO MAIN STORM DRAIN SYSTEM |
| Area of basin flows = | 17116 SF | = | 0.4 Ac. |
| The following calculations are based on Treatment areas as shown in table to the right | | LAND TREATMENT | |
| Sub-basin Weighted Excess Precipitation (see formula above) | | A = 0% | |
| Weighted E = 1.84 in. | | B = 4% | |
| Sub-basin Volume of Runoff (see formula above) | | C = 8% | |
| V ₃₆₀ = 2624 CF | | D = 88% | |
| Sub-basin Peak Discharge Rate: (see formula above) | | | |
| Q _P = 1.6 cfs | | | |

| | | | |
|--|----------|-----------------------|--|
| BASIN NO. | 5 | DESCRIPTION | DRAINS WITHIN LANDSCAPED AREA TO POND |
| Area of basin flows = | 5888 SF | = | 0.1 Ac. |
| The following calculations are based on Treatment areas as shown in table to the right | | LAND TREATMENT | |
| Sub-basin Weighted Excess Precipitation (see formula above) | | A = 0% | |
| Weighted E = 1.48 in. | | B = 15% | |
| Sub-basin Volume of Runoff (see formula above) | | C = 30% | |
| V ₃₆₀ = 727 CF | | D = 55% | |
| Sub-basin Peak Discharge Rate: (see formula above) | | | |
| Q _P = 0.5 cfs | | | |

| | | | |
|--|----------|-----------------------|----------------------|
| BASIN NO. | 6 | DESCRIPTION | EXISTING POND |
| Area of basin flows = | 15582 SF | = | 0.4 Ac. |
| The following calculations are based on Treatment areas as shown in table to the right | | LAND TREATMENT | |
| Sub-basin Weighted Excess Precipitation (see formula above) | | A = 0% | |
| Weighted E = 0.83 in. | | B = 50% | |
| Sub-basin Volume of Runoff (see formula above) | | C = 50% | |
| V ₃₆₀ = 1078 CF | | D = 0% | |
| Sub-basin Peak Discharge Rate: (see formula above) | | | |
| Q _P = 0.9 cfs | | | |

SUB-BASIN CALCULATIONS



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BASED ON 100-YEAR, 6-HOUR STORM

- BASIN 1: 4.4 CFS
Surface drains to proposed 2' bottom width 'U' shaped concrete channel with 1' radius ends. Total opening width = 4.0'. Per Weir Equation ($Q=CLH^{3/2}$) the opening capacity = 4.7 cfs. The depth within the 'U' shaped concrete channel = 0.29' (at 3% slope). See separate channel calculations.
- BASIN 2: 0.5 CFS
Approximately 0.4 cfs is discharged to the Phase II storm drain system. At a slope of 0.5%, a 12" storm drain has a full flow capacity of $3 \pm$ cfs.
- BASIN 3: 1.3 CFS
Surface drains to proposed 2' bottom width 'U' shaped concrete channel with 1' radius end (1 side only). Total opening width = 3.0'. Per Weir Equation ($Q=CLH^{3/2}$) the opening capacity = 3.5 cfs. The depth within the 'U' shaped concrete channel = 0.13' (at 3% slope). See separate channel calculations.
- BASIN 4: 1.6 CFS
Discharged to the main storm drain system. At a slope of 0.83%, a 12" storm drain has a full flow capacity of $3.8 \pm$ cfs.
- BASIN 5: 0.5 CFS
Surface drains within landscaping to enter pond.
- BASIN 6: 0.9 CFS
Captured within existing pond.

SUB-BASIN ANALYSIS



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Channel Report

Hydraflow Express Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc.

Tuesday, Jan 24 2012

<Name> **WEST CHANNEL**

Rectangular

Bottom Width (ft) = 2.00
Total Depth (ft) = 0.50

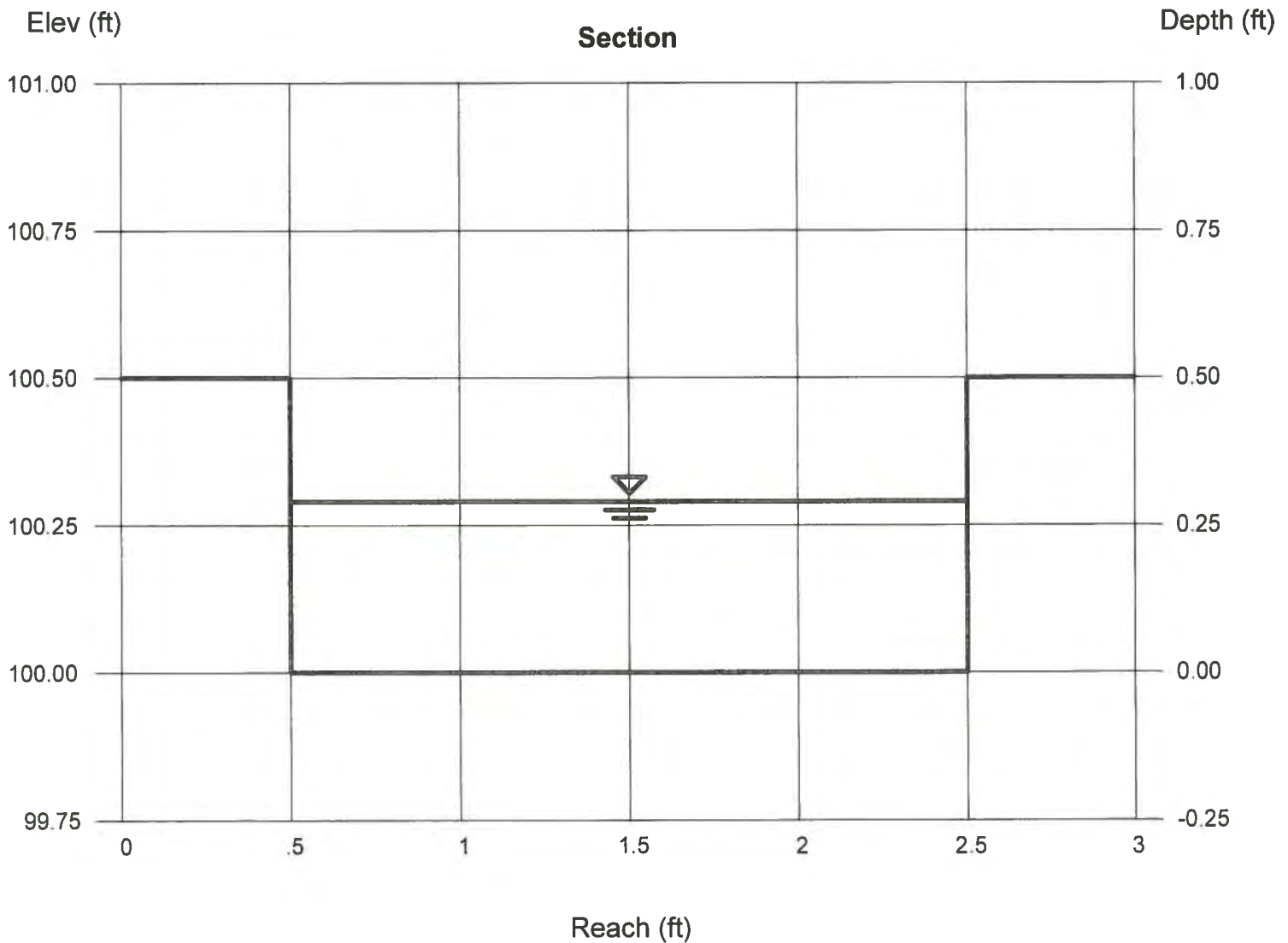
Invert Elev (ft) = 100.00
Slope (%) = 3.00
N-Value = 0.012

Calculations

Compute by: Known Q
Known Q (cfs) = 4.40

Highlighted

Depth (ft) = 0.29
Q (cfs) = 4.400
Area (sqft) = 0.58
Velocity (ft/s) = 7.59
Wetted Perim (ft) = 2.58
Crit Depth, Yc (ft) = 0.50
Top Width (ft) = 2.00
EGL (ft) = 1.18



Channel Report

Hydraflow Express Extension for AutoCAD® Civil 3D® 2012 by Autodesk, Inc.

Tuesday, Jan 24 2012

<Name> **EAST CHANNEL**



Rectangular

Bottom Width (ft) = 2.00
Total Depth (ft) = 0.50

Invert Elev (ft) = 100.00
Slope (%) = 3.00
N-Value = 0.012

Calculations

Compute by: Known Q
Known Q (cfs) = 1.30

Highlighted

Depth (ft) = 0.13
Q (cfs) = 1.300
Area (sqft) = 0.26
Velocity (ft/s) = 5.00
Wetted Perim (ft) = 2.26
Crit Depth, Yc (ft) = 0.24
Top Width (ft) = 2.00
EGL (ft) = 0.52

