



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

February 6, 2004

Bradley T. Dixon, PE
Bohannon Huston, Inc
7500 Jefferson NE
Albuquerque, NM 87109

**Re: Ventana Ranch West Subdivision Drainage Management Plan, Addendum 1
Engineer's Stamp dated 12-24-03, (B8/D1)**

Dear Mr. Dixon,

Based upon the information provided in your submittal dated 12-24-03, the above referenced addendum to Master Plan cannot be approved until the following comments are addressed

- Please address the area just west of Basin 601 and north of Paseo del Norte. This area must drain through your site as well.
- Please include any existing platting within the boundaries of your upstream basin and include any tract bisected by your developed-basin boundary line in its entirety. It is possible that the offsite runoff may increase.
- The design of your proposed pipe should be for the 944 cfs planned for at eastern edge of the Tracts 1 and 3, not 811 as shown.

If you have any questions, you can contact me at 924-3986.

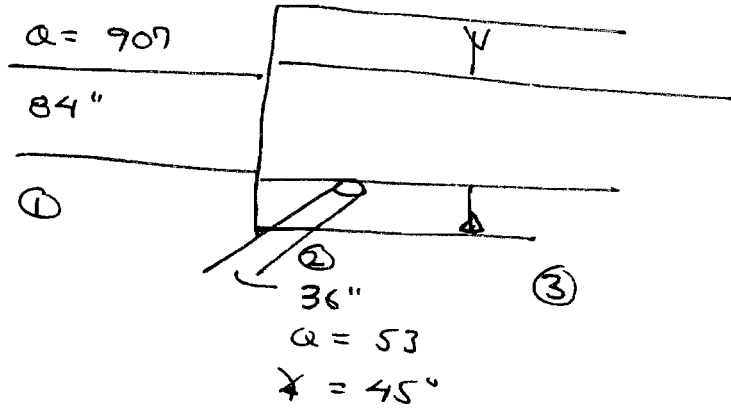
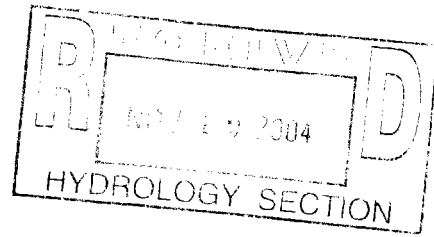
Sincerely,

Bradley L. Bingham, PE
City Hydrologist

C: Lynn Mazur, AMAFCA
file

North Branch
Piedras Mercedes Arroyo

84" Storm Drain
+ 36" SD Side Flow



Evaluate the effect of the 36" SD on the channel hydraulics

1) Try Straight Momentum Balance

$$M_1 + M_2 \cos \theta = M_3$$

$$\begin{aligned} M_1 &= \frac{Q^2}{5A} + A\bar{Y} && \text{(At exit of 84")} \\ &= \frac{907^2}{(32.2)(38.5)} + (38.5)(7/2) \\ &= 801 \text{ ft}^3 \end{aligned}$$

$$M_2 = \frac{Q^2}{5A} + A\bar{Y}$$

$$\begin{aligned} D &= 22" \\ A &= 4.53 \text{ ft}^2 && V = 11.7 \text{ fps} \\ &&& \theta = 22" \end{aligned}$$

PROJECT NAME
PROJECT NO.
SUBJECT

SHEET 1 OF 3
BY
CH'D DATE 11/14/04
DATE

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$$\begin{aligned}
 M_2 &= \frac{53^3}{(32.2)(4.5^3)} + (4.5^3) (\approx (1.0)(^2/3)) \\
 &= 19.2 + 5.5 \\
 &= 24.7
 \end{aligned}$$

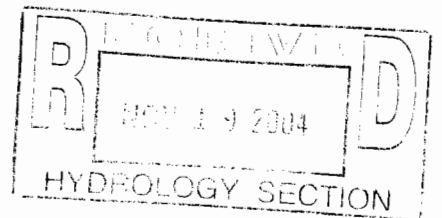
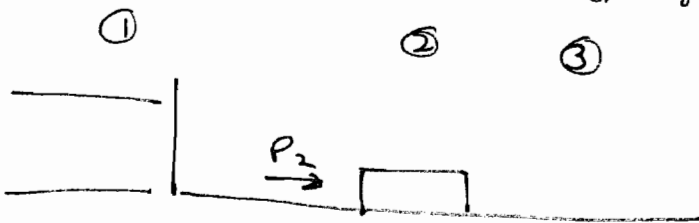
Solve for M_3

$$\begin{aligned}
 M_3 &= M_1 + M_2 \cos \theta \\
 &= 801 + 17.5 \\
 &= 818 \text{ ft}^3
 \end{aligned}$$

From M_3 Rating Curve (loc 3. out)

818 would occur above 8.0' depth channel
 However slope of channel (1.67%) and lack
 of downstream control indicates no hydraulic
 jump would occur

Try analysis assuming 36" flow crests
 a "hydraulic" block across bottom of
 channel to mimic effect of 45" "spout".



PROJECT NAME
 PROJECT NO.
 SUBJECT

SHEET 2 OF 3
 BY DATE
 CH'D DATE

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$$M_1 = P_2 + M_3$$

$$M_1 = 801 \text{ ft}^3$$

$$P_2 = \frac{1}{2} (1.83) [(2)(7 - 1.83)] 24.48$$

(Eq. from chow Pg. 52

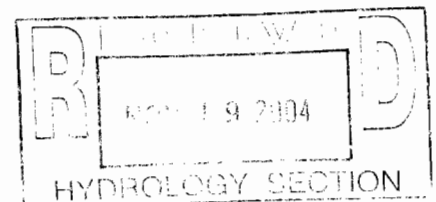
$$P_2 = 232 \text{ ft}^3$$

$$\begin{aligned} M_3 &= M_1 - P_2 \\ &= 801 - 232 \\ &= 569 \text{ ft}^3 \end{aligned}$$

From M Rating Curve

$$\text{Depth} \approx 3.5'$$

$$\text{Meaning's Depth} = 2.95'$$



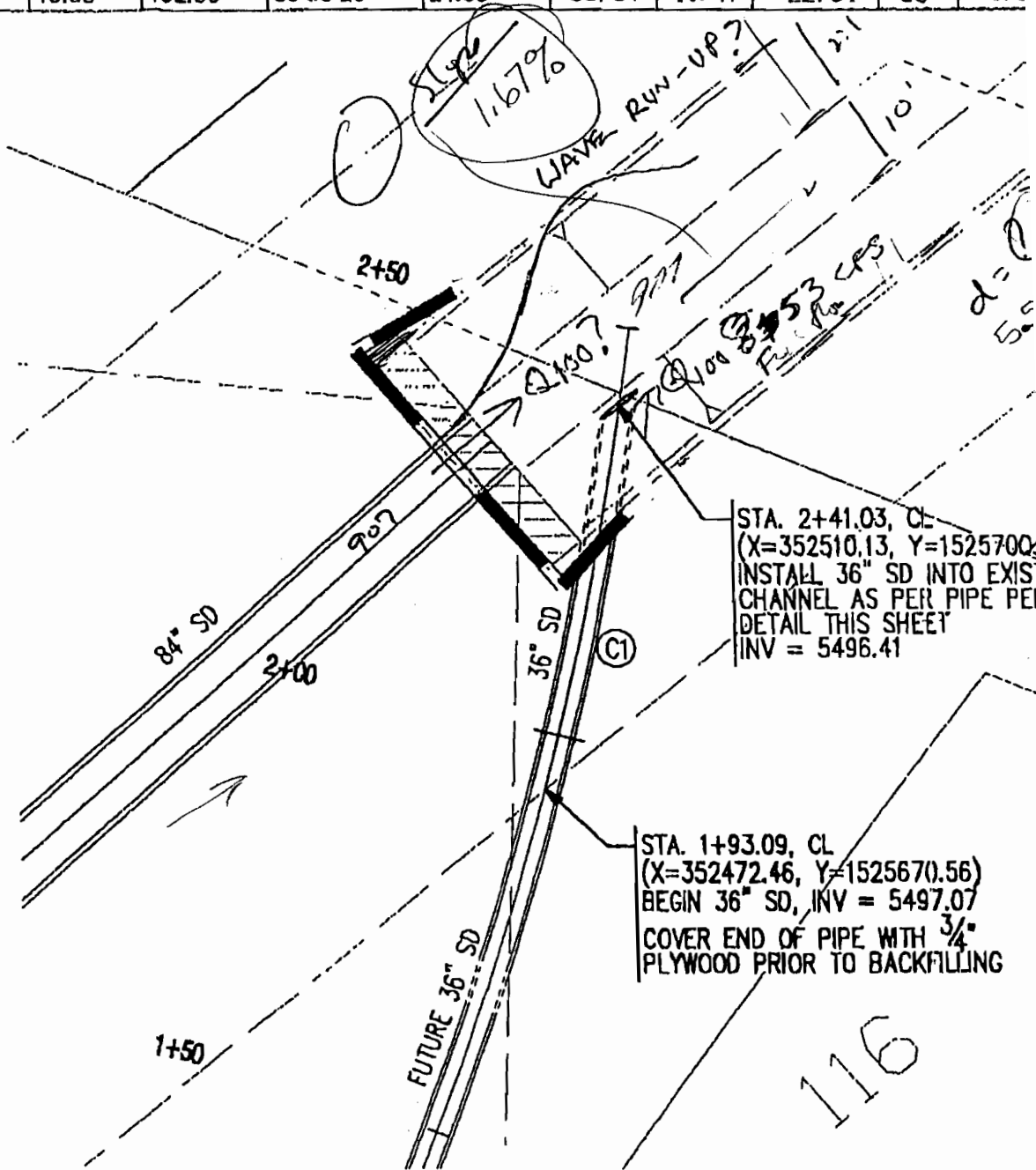
PROJECT NAME
PROJECT NO.
SUBJECT

SHEET 3 OF 3
BY DATE
CH'D DATE

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ENGINEERING
SPATIAL DATA
ADVANCED TECHNOLOGIES

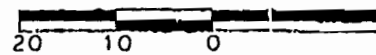
STORM DRAIN Curve Table									
ID	ARC	RADIUS	DELTA	TANGENT	Q(cfs)	V(cfs)	DEPTH	SIZE	SLOPE
C1	48.00'	402.00'	06°50'29"	24.03'	53.34	11.47	22.51"	36"	1.2



R. D. [Name]

 No. 182004

 HYDROLOGY SECTION

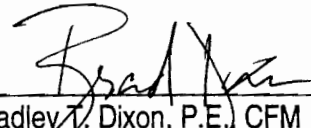
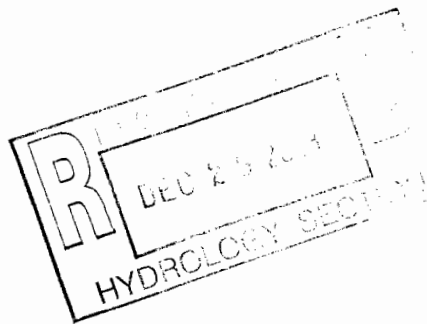


STORM DRAIN

PERMIT

**ADDENDUM NO. 1
FOR THE
VENTANA RANCH WEST SUBDIVISION
DRAINAGE MANANAGEMENT PLAN**

I, Bradley T. Dixon, hereby certify that I am a Registered Professional Engineer, registered in the state of New Mexico, and that the following report was prepared under my direction and is true and correct to the best of my knowledge and belief.



Bradley T. Dixon, P.E., CFM
NMPE No. 16163



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Appendix B AHYMO Model – Existing Conditions Upstream – Developed Conditions in Ventana Ranch West
Appendix C AHYMO Model – Developed Conditions Upstream – Developed Conditions in Ventana Ranch West
Appendix D Hydraulic Analysis

I. INTRODUCTION

This report constitutes Addendum No. 1 for the Ventana Ranch West Drainage Management Plan, Bohannon Huston, October 10, 2003 (DMP), which was prepared for Sandia Properties Limited Company. It proposes the use of a 96-inch reinforced concrete storm drain pipe (RCP) instead of open channel for the extension of Tributary B of the North Branch of the Piedras Marcadas Arroyo through Ventana Ranch West (VRW), a proposed subdivision in northwest Albuquerque (Figure 1). This storm drain extension will be similar to the West Branch Calabacillas Storm Drain Diversion, an 84" – 96" storm drain in Ventana Ranch that drains into Las Ventanas Dam, and the 84" storm drain through the West Pointe subdivision in Ventana Ranch, which discharges into Tributary A of the North Branch of the Piedras Marcadas Arroyo.

Tributary B currently exists as a concrete-lined open channel within Ventana Ranch, which bounds VRW to the east. The DMP proposed that Tributary B be extended as a grouted basalt channel through VRW to its western boundary. This would have required the construction of a 2-barrel 10'x7' concrete box culvert for the north-south entrance road into VRW from Paseo del Norte. It also would have complicated the grading of the adjacent tracts, Tracts 1, 2, 2A, and 3, where significant fill is proposed to avoid trenching through underlying basalt bedrock. By extending Tributary B as an RCP, these shortcomings are avoided. Also, vehicular access into Tracts 1, 2, 2A, and 3 can be improved by consolidating their entrance roads along the alignment of the previously proposed open channel.

II. HYDROLOGY

Because an open channel was proposed as the extension of Tributary B, the hydrologic models that were presented in the DMP accounted for fully developed conditions within the watershed upstream of VRW. In this condition, the 100-year peak discharge rate entering the channel would be 811 cfs. However, for the design of an RCP rather than an open channel, there are two conditions to consider. In the first condition, VRW will be constructed, with the RCP in place, and the land in the upstream watershed will be undeveloped. In this case, the headwater at the inlet to the RCP should not cause a backwater effect that would impact the upstream property. In the second condition, the

upstream property will also be developed, and the RCP through VRW will presumably be extended to the west as additional RCP. In this case (fully developed conditions), the hydraulic grade line (HGL) for the RCP through VRW should be below finished ground elevations. For these two conditions, the flows from the upstream watershed were modeled using undeveloped and developed land treatments, respectively. The two AHYMO models are shown herein in Appendices B and C. The first model reflects undeveloped conditions in the Tributary B watershed upstream from VRW and developed conditions within VRW. The flow rate entering Ventana Ranch West is approximately 311 cfs. The second model reflects developed conditions throughout, and the flow rate at the VRW boundary is approximately 811 cfs. Figure 2 shows the drainage basins as well as the 100-year peak discharge rates for both of the models.

III. HYDRAULIC ANALYSIS

Schematic plan and profile views of the 96-inch RCP are shown in Figure 3. Based upon these schematics, the pipe will be approximately 1110 feet long and have a slope of approximately 1.2%. Please note that the inlet to the pipe has been depressed approximately 6 feet below existing ground to 1) allow additional headwater depth at the inlet to the pipe before water backs up onto the upstream property and 2) provide flexibility for the vertical alignment of the pipe should it be extended into the upstream property in the future. It is anticipated that the design for the pipe will include a concrete lined transition from the upstream arroyo to prohibit headcutting upstream from the pipe and/or silt deposition at the pipe inlet.

InRoads Storm and Sanitary's Drainage Structure Analyzer was used to determine the headwater depth for the pipe under each of the hydrologic scenarios described above (Appendix D). For the first scenario, in which the upstream watershed is undeveloped, the headwater depth is 6.6 feet, and the headwater elevation is approximately 5516.10'. The existing ground elevation at the VRW property line is approximately 5516.50'. Therefore, the backwater created by the pipe dissipates before the VRW property line. In the second scenario, the headwater depth is 15.7 feet. This means that, while the pipe is under pressure throughout VRW, the HGL will stay well below the proposed ground surface.

IV. DESIGN AND CONSTRUCTION CONSIDERATIONS

Currently, it is assumed that the proposed RCP will run within the rights-of-way for the entrance roads into Tracts 1, 2, 2A, and 3. This will provide the City of Albuquerque with access for maintenance of the pipe. If the pipe does not follow a roadway alignment, a drainage easement will be granted to the City with an access road that meets the City's requirements.

Because of the proposed depth of fill over the RCP, it is likely that some or all of the pipe will have to be Class IV. The extent of Class IV pipe will be determined at the time of final design.

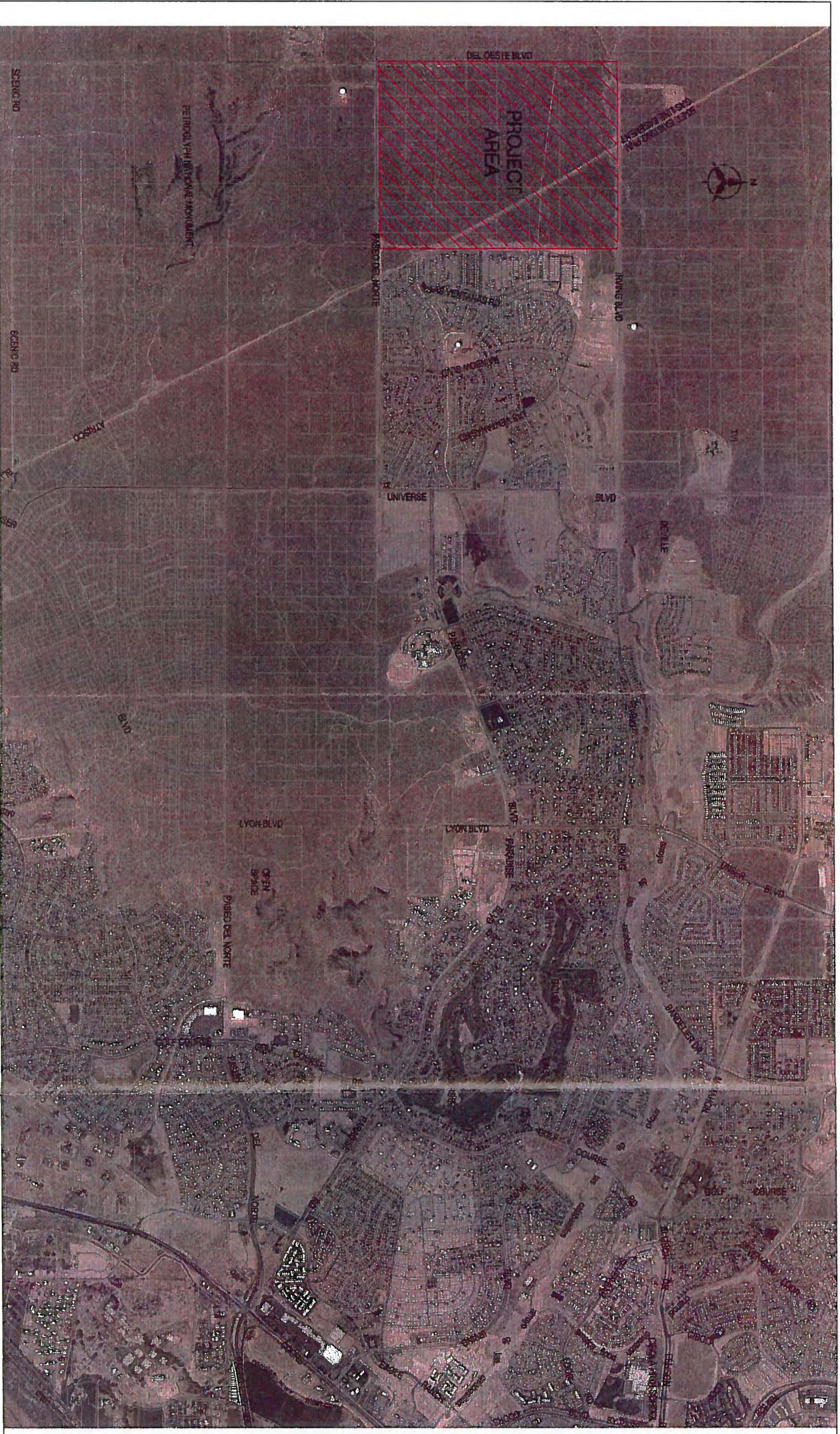
During final design, the flow rates through the RCP will be updated, and the pipe's velocities and hydraulic grade line will be determined. Also, the design ground surface elevations along the alignment of the RCP will be finalized. At that time, the size of the RCP will be reevaluated to confirm that the pipe size is minimized while keeping the HGL below finished ground.

V. CONCLUSIONS AND RECOMMENDATIONS

Based on the analyses described herein, the open channel extension of Tributary B of the North Branch of the Piedras Marcadas Arroyo, which was proposed in the Ventana Ranch West Drainage Management Plan, could be replaced by a 96-inch RCP without causing storm water to back up onto the upstream property prior to its development and without the HGL for the RCP through VRW being higher than proposed finished ground elevations. This would result in lower capital costs, facilitate grading of the adjacent tracts in Ventana Ranch West, and improve vehicular ingress and egress for the tracts.

APPENDIX A

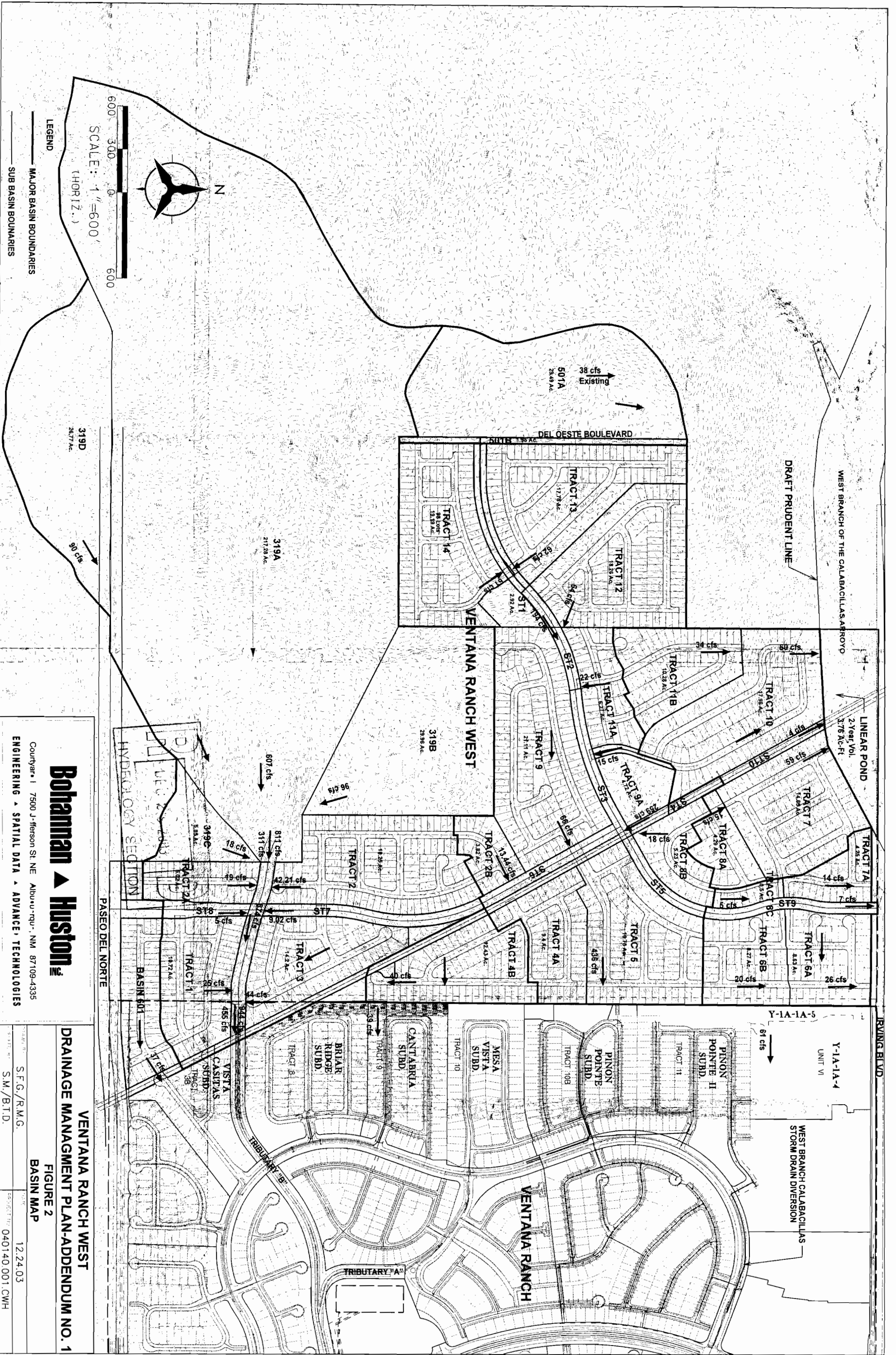
FIGURES



Courtyard | 7500 Jefferson St. NE Albuquerque, NM 87109-4335
 ENGINEERING & SPATIAL DATA & ADVANCED TECHNOLOGIES

**VENTANA RANCH WEST
 DRAINAGE MANAGEMENT PLAN-ADDENDUM NO. 1**

FIGURE 1 VICINITY MAP	
DRAWN BY: S.F.G./R.M.G.	DATE: 12.24.03
CHECKED BY: S.M./B.T.D.	PROJECT NO: 040140.001.CWH

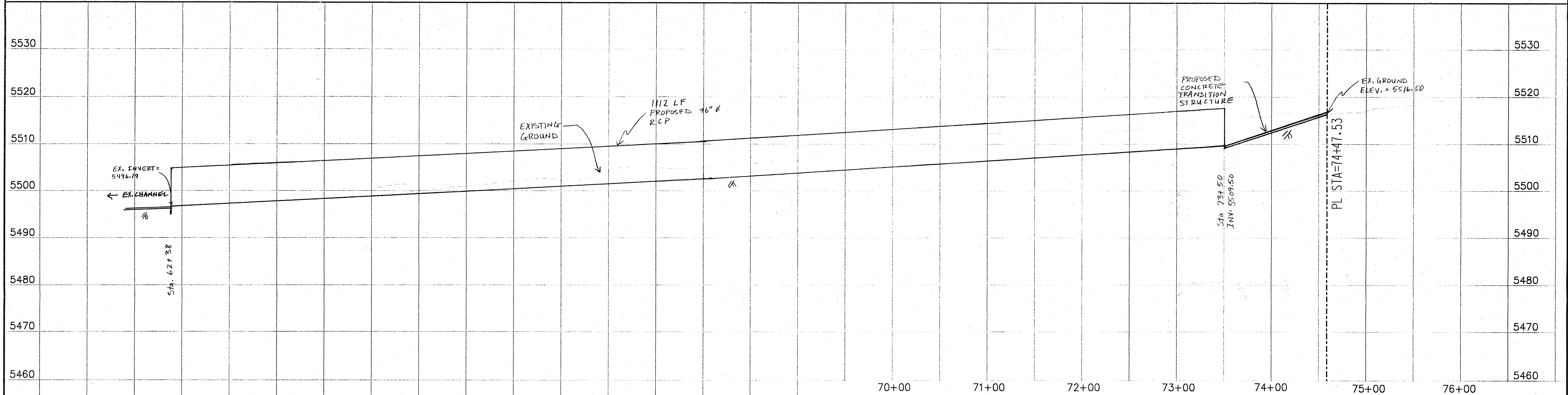
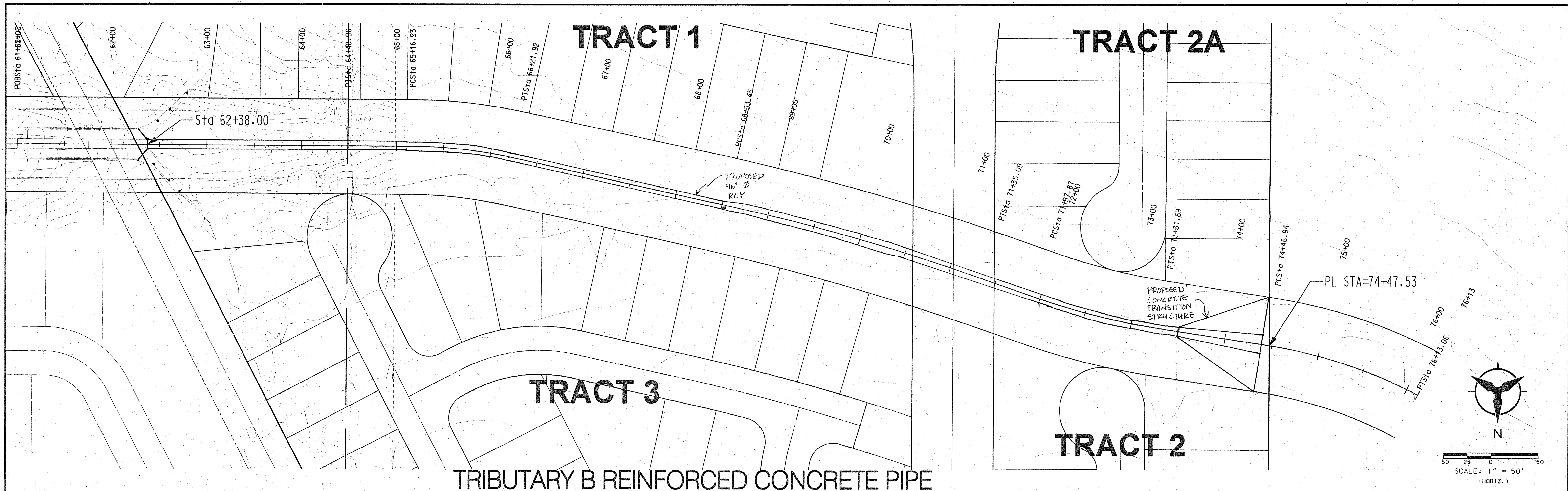


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**VENTANA RANCH WEST
 DRAINAGE MANAGEMENT PLAN-ADDENDUM NO. 1**

FIGURE 2 BASIN MAP	S.F.G./R.M.G.	12.24.03
	S.M./B.T.D.	040140 001.CWH



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Engineering & Spatial Data & Advanced Technologies

7500 Jefferson St. NE Albuquerque, NM 87109-4335

BHI JOB NO. 040140

SCALE: 1" = 50' (HORIZ.)
1" = 10' (VERT.)

VENTANA RANCH WEST
DRAINAGE MANAGEMENT PLAN-ADDENDUM NO. 1

FIGURE 3
RCP SCHEMATIC PLAN & PROFILE

DEC 29 2003

DRAWN BY: D.M.	DATE: 12.24.03
CHECKED BY: B.D.	PROJECT NO. 040140.001.CWH

APPENDIX B

AHYMO MODEL

EXISTING CONDITIONS UPSTREAM

DEVELOPED CONDITIONS IN VENTANA RANCH WEST

AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
1997.02c RUN DATE (MON/DAY/YR) =12/12/2003
INPUT FILE = VW319EX.HYM
USER NO.= AHYMO-S-9702c1BohanHu-AH

- VERSION:

RUNOFF COMMAND (INCHES)	PEAK (HOURS)	TIME TO PEAK (HOURS)	CFS HYDROGRAPH PER ACRE	FROM PAGE = ID	TO ID	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)
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*S* PROJECT NAME: VENTANA WEST, ALBUQUERQUE, NM
*S* JOB NO. 040140
*S* DATE: August 2003
*S*
*S* INPUT FILE NAME: VWEST319.HYM
*S* OUTPUT FILE NAME: VWEST319.OUT
*S* FILES LOCATION: BHI-MAIN\040140\HYDRO\STUDIES\AHYMO\
*S* COMMENTS:
*S*
*S* RENAMED VW319EX.HYM TO REFLECT UNDEVELOPED CONDITIONS
*S* IN SUB-BASIN 319.
*S*
*S* Each sub-basin is reposed like this: PD.319
*S* C stands for Piedras Marcadas Arroyo
*S*
*S* d Mannings n Calculated with procedure outlined in ALB. DPM.
*S*
*S* Percent impervious determine utilizing Albuquerque DPM procedures.
*S*
*S* rges into the Tributary B for the North Piedras Marcadas Nor

```

RAINFALL TYPE= 2

RAIN24= 2.660

SEDIMENT BULK

PK BF = 1.02

```

*S**** COMPUTE BASIN 319D****
COMPUTE NM HYD PD.319D - 1 .04183 33.83 1.077
.48262 1.550 1.264 PER IMP= .00
*S*ROUTE C0.319D THROUGH CHANNEL SEG 1
ROUTE 319.30 1 2 .04183 34.74 1.077
.48265 1.550 1.298
*S**** COMPUTE BASIN 319A****
COMPUTE NM HYD PD.319A - 3 .33950 239.94 8.739
.48262 1.600 1.104 PER IMP= .00
*S**** COMPUTE BASIN 319B****
COMPUTE NM HYD PD.319B - 4 .04700 35.23 1.210
.48262 1.550 1.171 PER IMP= .00
*S**** ADD 319A AND 319B ****
ADD HYD PD.319 4& 3 5 .38650 272.58 9.948
.48262 1.600 1.102
*S**** COMPUTE BASIN 319C****
COMPUTE NM HYD PD.319C - 6 .00910 6.47 .234
.48262 1.550 1.112 PER IMP= .00
*S**** ADD 319A/B AND 319C ****
ADD HYD PD.319 5& 6 7 .39560 278.76 10.183
.48262 1.600 1.101
*S**** ADD 319A/B/C AND 319D ****
ADD HYD PD.319 7& 2 8 .43743 310.50 11.259
.48262 1.600 1.109
*S*ROUTE C0.319 THROUGH CHANNEL SEG 1

```


				vw319EX.SUM				
ROUTE		319.10	8	9	.43743	314.54	11.259	
.48263	1.600	1.124						
*S**** COMPUTE TRACT 2A****								
COMPUTE NM HYD		T2A	-	10	.00780	18.56	.777	
1.86682	1.500	3.718	PER	IMP= 62.00				
*S**** ADD TRACT 2A TO BASIN 319****								
ADD HYD		PD.319	9&10	11	.44523	327.32	12.036	
.50687	1.600	1.149						
*S**** COMPUTE TRACT 2****								
COMPUTE NM HYD		T2	-	12	.02852	42.21	2.693	
1.77035	1.650	2.312	PER	IMP= 56.00				
*S**** ADD BASIN 2 TO BASIN 319****								
□								
TIME TO	CFS	FROM	TO	PEAK	RUNOFF			
		PAGE =	2					
		HYDROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	
RUNOFF	PEAK	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	
COMMAND	(HOURS)	ACRE	NOTATION					
(INCHES)								
ADD HYD		PD.319	12&11	13	.47375	366.55	14.729	
.58293	1.600	1.209						
*S*ROUTE C0.319 THROUGH CHANNEL SEG 2								
ROUTE		319.20	13	14	.47375	365.17	14.729	
.58294	1.600	1.204						
*S**** COMPUTE STREET 8****								
COMPUTE NM HYD		ST8	-	15	.00220	5.09	.208	
1.77357	1.500	3.618	PER	IMP= 56.20				
*S**** COMPUTE STREET 7****								
COMPUTE NM HYD		ST7	-	16	.00475	9.02	.473	
1.86682	1.550	2.968	PER	IMP= 62.00				
*S**** ADD STREET 7 AND 8****								
ADD HYD		PD.319.2	15&16	17	.00695	13.53	.681	
1.83720	1.550	3.042						
*S**** ADD STREET 7 AND 8 TO BASIN 319****								
ADD HYD		PD.319	17&14	18	.48070	377.59	15.410	
.60107	1.600	1.227						
*S*ROUTE C0.319 THROUGH CHANNEL SEG 3								
ROUTE		319.20	18	19	.48070	393.36	15.410	
.60107	1.600	1.279						
*S**** COMPUTE TRACT 1****								
COMPUTE NM HYD		T1	-	20	.01680	25.22	1.621	
1.80894	1.650	2.345	PER	IMP= 58.40				
*S**** COMPUTE TRACT 3****								
COMPUTE NM HYD		T3	-	21	.02220	43.60	1.986	
1.67710	1.550	3.068	PER	IMP= 50.20				
*S**** ADD TRACT 1 AND 3****								
ADD HYD		PD.319.3	21&20	22	.03900	63.00	3.606	
1.73387	1.550	2.524						
*S**** ADD TRACT 1 AND 3 TO BASIN 319****								
ADD HYD		PD.319	22&19	23	.51970	455.28	19.016	
.68608	1.600	1.369						
FINISH								

APPENDIX C

AHYMO MODEL

DEVELOPED CONDITIONS UPSTREAM

DEVELOPED CONDITIONS IN VENTANA RANCH WEST

AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
 1997.02c RUN DATE (MON/DAY/YR) =10/09/2003
 INPUT FILE = vwest319.hym
 USER NO.= AHYMO-S-9702c1BohanHu-AH

- VERSION:

RUNOFF COMMAND (INCHES)	PEAK (HOURS)	CFS HYDROGRAPH PER IDENTIFICATION ACRE	FROM PAGE = ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)
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*S* PROJECT NAME: VENTANA WEST, ALBUQUERQUE, NM
*S* JOB NO. 040140
*S* DATE: August 2003
*S*
*S* INPUT FILE NAME: VWEST319.HYM
*S* OUTPUT FILE NAME: VWEST319.OUT
*S* FILES LOCATION: BHI-MAIN\040140\HYDRO\STUDIES\AHYMO\
*S* COMMENTS:
*S*
*S* Each sub-basin is reposedited like this: PD.319
*S* C stands for Piedras Marcadas Arroyo
*S*
*S* d Mannings n Calculated with procedure outlined in ALB. DPM.
*S* Percent impervious determine utilizing Albuquerque DPM procedures.
*S*
*S* rges into the Tributary B for the North Piedras Marcadas Nor

```

RAINFALL TYPE= 2

RAIN24= 2.660

SEDIMENT BULK

PK BF = 1.02

```

*S**** COMPUTE BASIN 319D****
COMPUTE NM HYD PD.319D - 1 .04183 89.88 4.004
1.79460 1.500 3.358 PER IMP= 59.00
*S*ROUTE C0.319D THROUGH CHANNEL SEG 1
ROUTE 319.30 1 2 .04183 89.88 4.004
1.79461 1.550 3.357
*S**** COMPUTE BASIN 319A****
COMPUTE NM HYD PD.319A - 3 .33950 607.30 32.494
1.79460 1.600 2.795 PER IMP= 59.00
*S**** COMPUTE BASIN 319B****
COMPUTE NM HYD PD.319B - 4 .04700 95.67 4.498
1.79460 1.550 3.180 PER IMP= 59.00
*S**** ADD 319A AND 319B ****
ADD HYD PD.319 4& 3 5 .38650 702.52 36.993
1.79460 1.550 2.840
*S**** COMPUTE BASIN 319C****
COMPUTE NM HYD PD.319C - 6 .00910 18.18 .871
1.79460 1.550 3.122 PER IMP= 59.00
*S**** ADD 319A/B AND 319C ****
ADD HYD PD.319 5& 6 7 .39560 720.70 37.864
1.79460 1.550 2.847
*S**** ADD 319A/B/C AND 319D ****
ADD HYD PD.319 7& 2 8 .43743 810.58 41.867
1.79460 1.550 2.895
*S*ROUTE C0.319 THROUGH CHANNEL SEG 1
ROUTE 319.10 8 9 .43743 811.63 41.867
1.79460 1.550 2.899
*S**** COMPUTE TRACT 2A****

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VWEST319.SUM

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COMPUTE NM HYD          T2A - 10          .00780      18.56      .777
1.86682  1.500  3.718 PER IMP= 62.00
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ADD HYD          PD.319  9&10  11          .44523      828.00     42.644
1.79586  1.550  2.906
*S**** COMPUTE TRACT 2****
COMPUTE NM HYD          T2 - 12          .02852      42.21      2.693
1.77035  1.650  2.312 PER IMP= 56.00
*S**** ADD BASIN 2 TO BASIN 319****
ADD HYD          PD.319  12&11  13         .47375      860.57     45.337
1.79432  1.550  2.838
*S*ROUTE C0.319 THROUGH CHANNEL SEG 2
ROUTE          319.20  13  14          .47375      860.81     45.337
1.79432  1.550  2.839
*S**** COMPUTE STREET 8****

```

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□
          TIME TO      CFS      FROM TO      PEAK      RUNOFF
          COMMAND      IDENTIFICATION      NO. NO.      DISCHARGE      VOLUME
(RUNOFF) (HOURS)      ACRE      NOTATION      (SQ MI)      (CFS)      (AC-FT)
          ST8 - 15          .00220      5.09      .208
1.77357  1.500  3.618 PER IMP= 56.20
*S**** COMPUTE STREET 7****
          ST7 - 16          .00475      9.02      .473
1.86682  1.550  2.968 PER IMP= 62.00
*S**** ADD STREET 7 AND 8****
ADD HYD          PD.319.2  15&16  17         .00695      13.53      .681
1.83720  1.550  3.042
*S**** ADD STREET 7 AND 8 TO BASIN 319****
ADD HYD          PD.319  17&14  18         .48070      874.35     46.018
1.79494  1.550  2.842
*S*ROUTE C0.319 THROUGH CHANNEL SEG 3
ROUTE          319.20  18  19         .48070      882.45     46.018
1.79494  1.600  2.868
*S**** COMPUTE TRACT 1****
COMPUTE NM HYD          T1 - 20          .01680      25.22      1.621
1.80894  1.650  2.345 PER IMP= 58.40
*S**** COMPUTE TRACT 3****
COMPUTE NM HYD          T3 - 21          .02220      43.60      1.986
1.67710  1.550  3.068 PER IMP= 50.20
*S**** ADD TRACT 1 AND 3****
ADD HYD          PD.319.3  21&20  22         .03900      63.00      3.606
1.73387  1.550  2.524
*S**** ADD TRACT 1 AND 3 TO BASIN 319****
ADD HYD          PD.319  22&19  23         .51970      944.37     49.624
1.79036  1.600  2.839
FINISH

```

APPENDIX D

HYDRAULIC ANALYSIS

Analyzer Report

=====
Drainage Structure Analyzer

Culvert Hydraulic Analysis

Date: Tuesday, December 23, 2003 01:37:19 PM
=====

Input Data

Shape Circular
Material RC C76-A
Roughness 0.013000
Entrance Edge Square edge w/ headwall
Number of Barrels 1
Length 1110.00 ft
Slope 1.200%
Tailwater 7.00 ft
Inlet Control Equation Entrance Loss
Size (W x T): 96.00 x 8.0000
Flow Rate 311.0 cfs

Output Results

Flow Rate 311.0 cfs
Control Inlet
Capacity 999.1 cfs
Manning's Velocity 17.55 ft/s
Headwater 6.59 ft
Critical Depth 4.45 ft
Normal Depth 3.06 ft
Size (W x T): 96.00 x 8.0000

Analyzer Report

=====
Drainage Structure Analyzer

Culvert Hydraulic Analysis

Date: Tuesday, December 23, 2003 01:36:58 PM

=====
Input Data

Shape Circular
Material RC C76-A
Roughness 0.013000
Entrance Edge Square edge w/ headwall
Number of Barrels 1
Length 1110.00 ft
Slope 1.200%
Headwater 7.00 ft
Inlet Control Equation Entrance Loss
Size (W x T): 96.00 x 8.0000
Flow Rate 811.0 cfs

Output Results

Flow Rate 811.0 cfs
Inlet Control Inlet
Capacity 999.1 cfs
Manning's Velocity 22.14 ft/s
Headwater 15.67 ft
Critical Depth 7.08 ft
Normal Depth 5.47 ft
Size (W x T): 96.00 x 8.0000