

PIEDRAS MARCADAS

WATERSHED AND

LYON BOULEVARD

Storm Drain

Drainage Management Plan

JULY 29, 2003

Approved by
AMAFCA (Lynn)

Prepared for:

Albuquerque Metropolitan Arroyo

Flood Control Authority

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Albuquerque, NM 87107

Bohannan Huston Inc.

- ENGINEERING
- ADVANCED TECHNOLOGIES
- SPATIAL DATA

TABLE OF CONTENTS

EXECUTIVE SUMMARY.....	1
I. INTRODUCTION.....	5
II. HYDROLOGY.....	6
A. Drainage Basins	6
B. Land Treatments	8
C. Paradise Boulevard Storm Drain Analysis	9
III. LYON BLVD. STORM DRAIN OPTIONS	9
A. Option 1: Free Discharge, All New Storm Drain, Full Conveyance.....	9
B. Option 2: Existing Storm Drain, 1 Large Detention Basin South of Paradise Blvd.....	10
C. Option 3: Existing Storm Drain, 4 Smaller Detention Basins South of Paradise Blvd.	10
D. Option 4: Existing Storm Drain, Full Conveyance under Pressure Flow Conditions Assuming 212 cfs from Area South of Paradise Blvd.	11
IV. REVISED PIEDRAS MARCADAS DAM WATERSHED HYDROLOGY AND SCENARIOS..	11
A. Scenario 1: Do not Exceed Lyon Boulevard Storm Drain Capacity	14
B. Scenario 2: Disregard Lyon Boulevard Storm Drain Capacity and Meet the Required Runoff Volume.....	14
V. COST ESTIMATE FOR THE FOUR LYON BLVD. OPTIONS.....	15
VI. CONCLUSION.....	18
A. Four original Lyon Blvd. storm drain options	18
B. Additional Scenarios.....	19

TABLES

Table 1 – Sub-Basin Summary (Lyon Blvd. Storm Drain Options)	8
Table 2 – Molzen-Corbin's Sub-Basins Within Study Area.....	9
Table 3 – Estimated Construction Cost	18

FIGURES

Figure 1 –Basins for Molzen-Corbin Alternative 9	12
Figure 2 – Basins for Scenarios 1 and 2.....	16

APPENDICES

APPENDIX A – Land Treatments for Intended Uses (Primary Study Area) and AHYMO Input and Summary (Primary Study Area and Entire Piedras Marcadas Watershed)	
APPENDIX B – Curve for Pond Cost Estimation	
APPENDIX C – Detailed Cost Estimates	
APPENDIX D – Hydraulic Analysis Report for Option 4	
APPENDIX E – Basalt Profile	

EXHIBITS

EXHIBIT 1 – Storm Drain Basin Map
EXHIBIT 2 – Piedras Marcadas Dam LOMR Basin Maps
EXHIBIT 3 – Storm Drain Option 1
EXHIBIT 4 – Storm Drain Option 2
EXHIBIT 5 – Storm Drain Option 3
EXHIBIT 6 – Storm Drain Option 4

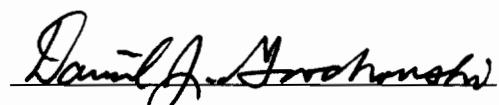
PLATES

PLATE 1 – Exhibit from "Conceptual Design Analysis for Lyon (Unser) Boulevard / Paradise Boulevard Storm Drain" (2000)
PLATE 2 – Exhibits from "Piedras Marcadas Drainage Management Plan Revision"

PIEDRAS MARCADAS WATERSHED AND LYON BOULEVARD
Storm Drain Drainage Management Plan

May 9, 2003

I, Daniel J. Grochowski, hereby certify that I am a Registered Professional Engineer, registered in the state of New Mexico, and that the following report was prepared under my direction and is true and correct to the best of my knowledge and belief.



Daniel J. Grochowski, P.E.

NMPE No. 8766

EXECUTIVE SUMMARY

This analysis update report covers the area roughly bounded by Unser/Lyon Boulevard on the east, Paradise Boulevard on the north and Paseo del Norte (PDN) extension on the south, comprising almost 600 acres of the Piedras Marcadas Dam watershed. The primary focus of the study was to determine what portion of the watershed could discharge to the Albuquerque Metropolitan Arroyo Flood Control Authority's (AMAFCA) future Lyon Boulevard storm drain extension. In the past year, the study was expanded to include analysis of the Piedras Marcadas Dam capacity, specifically to assess how much of the Piedras Marcadas developed watershed must be diverted north to the Calabacillas Arroyo to maintain one foot of freeboard in the dam.

History

There has been development interest in this area; however, due to lack of existing drainage outfalls, development has been limited. Following is a summary of some of the issues:

- The National Park Service has stated objections to allowing storm water runoff above the "historic" (not necessarily undeveloped) flow rate to pass through the Petroglyph National Monument.
- Flow to the south and east is limited. The Draft Piedras Marcadas Drainage Management Plan Revision, prepared by Molzen-Corbin & Associates in May 1993, found that the Piedras Marcadas Dam capacity would be exceeded under fully developed watershed conditions. The feasible solution was to divert storm water to the Calabacillas Arroyo at two locations. One diversion was in the vicinity of Ventana Ranch Subdivision, which has already been built, and the other was at Lyon Boulevard, which is the subject of AMAFCA's current study.
- The diversion of the upper part of the watershed was completed with the Las Ventanas Dam and outfall pipe to the Calabacillas Arroyo.
- The existing 72-inch storm drain outfall to the Calabacillas Arroyo in Lyon Boulevard has limited capacity.
- Property owners in the area, including Albuquerque Public Schools (APS), have been interested in developing their property but have been constrained by lack of drainage outfalls.

- Bernalillo County and the City of Albuquerque have an interest in a storm drain outfall for the future Unser Boulevard extension that will ultimately connect to Lyon Boulevard from the south.

Since AMAFCA has the Lyon Diversion Storm Drain on its project schedule, AMAFCA sponsored the drainage study for the area. AMAFCA entered into an Agreement with the City, County and developers in March 2001 to prepare a "Mini" Drainage Management Plan. The primary purpose was to determine how existing and proposed development will impact AMAFCA facilities. AMAFCA contracted Bohannan Huston, Inc. (BHI) to perform the work.

Results of Study

BHI took the original hydrologic model from the 1993 Molzen-Corbin study and updated drainage basins and facility capacities to reflect construction since that time. Among these projects are:

- Las Ventanas Dam and 60-inch storm drain outfall to the Calabacillas Arroyo.
- The Lyon Boulevard 72-inch storm drain outfall to the Calabacillas Arroyo.
- The Paradise Boulevard storm drain from Lyon Boulevard to an existing storm drain stub-out west of Golf Course Road. The ultimate outfall is the Piedras Marcadas Dam.
- Expansion of Piedras Marcadas Dam.

BHI used the 100-year flow rates from this analysis to determine storm drain options in the Lyon/Unser Boulevard corridor. The study was limited in scope to evaluate the following options:

- Option 1 – Free discharge from the study area into a larger, proposed Lyon Boulevard outfall pipe. This option was used as a benchmark to compare the other options.
- Option 2 – Utilize a single "regional" detention pond to reduce flow to minimize pipe sizes and to match the capacity of the existing outfall pipe.
- Option 3 – Utilize a series of smaller detention ponds to reduce flow to minimize pipe sizes and to match the capacity of the outfall pipe.
- Option 4 – Utilize detention ponding to reduce flow to minimize pipe sizes (Option 2 or 3). Maximize the existing outfall pipe capacity with pressure flow.

The results of the analysis also indicated that the capacity of the Piedras Marcadas Dam must also be taken into account. Although approximately 2.7 square miles have been diverted from the dam watershed to the Calabacillas Arroyo with the Las Ventanas Dam and Lyon Boulevard storm drain outfalls, it was necessary to evaluate the dam capacity with ultimate development. The current capacity, with one foot of freeboard, is 280 acre-feet. The study evaluated the additional drainage basin area that will need to be diverted to the Lyon Boulevard storm drain to maintain this capacity. An area of approximately 115 acres will be required to discharge to the Lyon Boulevard storm drain. Since the total discharge from this area is 400 cfs, and the additional capacity available in the outfall in Option 4 is 210 cfs, detention ponding will be required.

Construction Cost Estimates

Several construction cost scenarios were evaluated. The first was total project cost, from the future PDN to the existing 72-inch outfall to the Calabacillas Arroyo. The second was just the AMAFCA portion from the Paradise/Lyon intersection to the existing outfall. The third was the AMAFCA portion, excluding basalt excavation. This scenario was included as a comparison since construction within the basalt layer will significantly drive up the cost.

The County and APS have been interested in extending the Paradise Boulevard storm drain to the west. Therefore, this fourth scenario was included as an addition to the AMAFCA Lyon Boulevard storm drain portion.

Following is a summary of the construction cost estimates:

Storm Drain Option	Total Project Cost	Lyon Project Cost (AMAFCA)	Lyon Project Cost (excl. basalt) (AMAFCA)	Paradise/Lyon Project Cost	Flow from South (cfs)
1	\$24,831,000	\$7,800,000	\$3,477,000	\$9,153,000	1460
2	\$26,429,000	\$4,687,000	\$1,343,000	\$6,040,000	170
3	\$17,359,000	\$3,082,000	\$1,129,000	\$4,435,000	130
4	n/a	\$3,337,000	\$1,292,000	\$4,690,000	210

The recommended option is Option 4. The total project cost was not calculated since the storm drain option south of Paradise Boulevard could follow Option 2 or 3. The AMAFCA Lyon

storm drain project is \$255,000 more than Option 3 because it has a 90-inch storm drain connection to the existing outfall, while Option 3 has a 78-inch and 84-inch storm drain. Option 4 optimizes the use of the existing outfall and, with an increase of one pipe diameter, almost doubles the allowable flow from south of Paradise Boulevard.

I. INTRODUCTION

The Piedras Marcadas Watershed and Lyon Boulevard Storm Drain Analysis Update deals with an area of northwest Albuquerque that, up to this time, has had a very limited potential for development due to the lack of an outfall for developed flows. This area is approximately bounded by Unser/Lyon Boulevard on the east, Paradise Boulevard on the north, and on the south and west sides by the limits of the Piedras Marcadas Watershed. An attempt was made to include whole properties into the primary study area, and some area east of Unser Boulevard is included because it is possible to use the same system. There is an existing 72" storm drain line in the Unser/Lyon Boulevard Alignment from Irving Boulevard to the Calabacillas Arroyo. Past studies have proposed a southern extension of this storm drain to Paradise Boulevard. The intent of the primary analysis is to determine the feasibility of using the proposed Lyon Boulevard storm drain as the outfall point for the primary study area. The effects of recent developments in the entire watershed on the Piedras Marcadas Dam have also been included in this report. The Albuquerque Metropolitan Arroyo Flood Control Authority (AMAFCA), the chief sponsor of this study, the City, and area landowners have funded and provided needed information for this study.

Two past reports are foundational to the work done in this study. The first is the "Piedras Marcadas Drainage Management Plan" by Molzen-Corbin done in May 1993. It deals with drainage issues for the entire Piedras Marcadas Watershed. A number of developments have occurred in the watershed in the ten years since the report was completed, changing the area's hydrology. The other report is the "Conceptual Design Analysis for Lyon (Unser) Boulevard/Paradise Boulevard Storm Drain" by Bohannan Huston done in June 2000. The report evaluates a proposed storm drain down Paradise to Lyon and then continuing in Lyon connecting to the existing Lyon Boulevard Storm Drain.

As a starting point for this study, the existing section of storm drain, from Irving to the Calabacillas Arroyo, was analyzed to determine the existing capacity, which was determined to be 734 cfs based on Manning's Equation. In addition, the maximum area that could be routed to the storm drain was determined. The preliminary layout for the Paradise Boulevard Storm Drain west of Lyon Boulevard was also examined to determine whether or not it could be reduced due to addition

of storm drain line south of Paradise Boulevard. Three options were investigated for diverting the maximum drainage basin to the Lyon Boulevard Storm Drain System, and a fourth option was investigated for the storm drains in Paradise and Lyon Boulevards. The first option assumes an upsizing of the existing storm drain and an Unser Storm Drain that extends into the study area without detention ponds. The second option utilizes one detention pond to reduce flows to preserve the existing storm drain. The third option also looks to use the existing system, but makes use of several detention ponds rather than one. The fourth option looks at a pressure storm drain system in Paradise and Lyon Boulevards. The four options are discussed in further detail in Section III, below.

Since the watershed has undergone some development and improvements to the drainage system, the effects of that development have changed its hydrology. After revising the hydrology, other possible scenarios became apparent and are discussed in Section IV, below.

II. HYDROLOGY

Hydrologic modeling for this project was performed using the 1997 version of The Arid-Lands Hydrologic Model (AHYMO) in accordance with the City of Albuquerque Development Process Manual, Section 22.2, January 1993. Pipes were sized using Manning's Equation. Hydraulic grade lines were not calculated except for Option 4. Concrete box culverts were modeled as equivalent pipes in the AHYMO model. The 100-year storm event is used.

A. Drainage Basins

As mentioned above, the primary focus of the study area is bounded on the east, with some exceptions, by the proposed alignment for Unser Boulevard. This is because the Unser Corridor is a natural extension for the Lyon/Unser Storm Drain and is very nearly the outer limit of area that can physically be drained to the Calabacillas. There is some area east of Unser that is included because it could drain to the system and does not have another currently available outlet due to the presence of the Petroglyph National Monument downstream. The National Park Service has been very restrictive about allowing developed storm water flows to pass through the Monument.

In order to get as much area as possible to drain into the system, it was assumed that the storm drain trench at the intersection of Lyon and Paradise Boulevards should not be deeper than 30'. A hypothetical pipe line was taken from the intersection south at a 0.2% slope. The placement of the hypothetical pipe line was determined by maintaining at least two feet of cover above the soffitt in relation to the existing contours. The hypothetical pipe line was then used as the basis for the basin boundary. It is also the approximate location for the pipe lines in the three options. Other properties on the east that border the Unser alignment could be brought into the system if they are filled on the eastern portion of the property and the added flow does not overload the system. This may require the use of detention ponds on these sites. Due to the complexity of analyzing the feasibility of this option, these areas were not included in this study.

The sub-basins used in these options were developed from the basins in the Molzen-Corbin report "Piedras Marcadas Drainage Management Plan Revision" (1993) for the area south of Paradise Boulevard and the Bohannan-Huston report "Conceptual Design Analysis for Lyon (Unser) Boulevard/ Paradise Boulevard Storm Drain" (2000) for the area north of Paradise Boulevard. Plate 1 is a copy of the drainage basin map from the conceptual Lyon report. Plate 2 includes the basin maps from the Piedras Marcadas Report. Sub-basin 315 from the Piedras Marcadas report was the primary basin in the Lyon/Unser study area and was divided into Sub-basins 1 through 7. Sub-basins 3 and 6A are extended past the outer boundary of the Piedras Marcadas to include whole properties. This was the practice everywhere possible so that an owner would not have two separate drainage systems on the same property. Sub-basin 313 is a combination of sections from Molzen-Corbin's Sub-basins 313N and 313S. Sub-basins 311N, 311S, and 310 are located similarly to Molzen-Corbin's, except that there are changes due to the new mapping used (Bernalillo County, 1999), and the sub-basins end at the Unser alignment. Sub-basin 312 is only the very southern portion of Molzen-Corbin's original. Sub-basin 8 is within a portion of the proposed Unser Boulevard Corridor. The sub-basins can be seen in Exhibit 1.

B. Land Treatments

The land treatment percentages were determined based on zoning and the intended land uses as provided by the primary land owners in the area. The intended uses and zoning are also shown in Exhibit 1, and the land treatment percentages assigned to each basin are shown in Appendix A along with the AHYMO input and summary printouts. The land treatment percentages for the sub-basins, along with the 100-yr flow rates, volumes, and CFS/acre, are shown in Table 1. The land treatment percentages for the entire watershed analysis were not revised from the Molzen-Corbin report.

Table 1 – Sub-Basin Summary (Lyon Blvd. Storm Drain Options)

SUB-BASIN	AREA (acres)	% LAND TREATMENT *				Q (100-YR) (CFS)	VOLUME (acre-ft)	CFS/Acre
		A	B	C	D			
1	22.7	0.0	12.9	18.1	69.0	88.5	3.8	3.91
2	16.0	0.0	9.3	11.6	79.1	65.2	2.9	4.09
3	64.4	0.0	9.7	12.3	78.0	185.1	11.6	2.87
4	103.7	0.0	9.0	12.2	78.9	361.6	18.8	3.49
5	27.7	0.0	14.7	19.6	65.7	106.5	4.5	3.84
6A	176.8	0.0	13.4	17.4	69.1	451.8	29.8	2.56
6B	48.3	0.0	15.0	20.0	65.0	184.9	7.9	3.83
7	21.4	0.0	9.6	10.9	79.5	66.5	3.9	3.10
313	38.0	0.0	12.7	16.6	70.7	122.5	6.5	3.22
310	7.3	0.0	15.0	20.0	65.0	27.9	1.2	3.83
311S	18.7	0.0	14.0	19.3	66.7	72.2	3.1	3.84
311N	32.4	0.0	8.2	10.9	80.9	109.8	6.0	3.39
312	8.2	0.0	8.6	12.1	79.3	33.1	1.5	4.07
8	11.2	0.0	0.0	10.0	90.0	29.8	2.2	2.65

*Obtained from Section 22.2, Hydrology of the Development Process Manual, Volume 2.

For comparison purposes, Table 2 shows Molzen-Corbin's sub-basins within this area and the CFS/Acre for each. The areas of each sub-basin are not shown since the sub-basins' areas have changed, due to being cut off at the Unser Alignment, inclusion of whole properties, and changes due to new mapping. (Refer to Section II.A.)

Table 2 – Molzen-Corbin’s Sub-Basins Within Study Area

SUB-BASIN	CFS/Acre
315W	3.50
315S	3.50
315N	3.50
313S	3.15
311S	3.50
310	3.50
311N	2.78
312	2.26

C. Paradise Boulevard Storm Drain Analysis

Part of the scope of the study was to examine the preliminary layout of the Paradise Boulevard Storm Drain, from Chamisa Ridge to Lyon/Unser Boulevard, to determine if the size of the system could be reduced based on a reduced drainage area. There was a reduction in area since the original study in an area east of the James Monroe Middle School. This area, which is included in the new Sub-basin 313, was originally in a sub-basin contributing to the Paradise Boulevard Storm Drain according to the 2000 Lyon Report. In addition, some of the other areas south of Paradise Boulevard have been developed at a lower density than was predicted by the 2000 Lyon Report. However, even with the area reduction and less impervious contributing areas, the flow rates were not reduced enough to require a smaller storm drain system. The majority of flow into the system is from the north side of Paradise Boulevard. Please refer to the 2000 “Conceptual Design Analysis for Lyon Boulevard/Paradise Boulevard Storm Drain” by Bohannan Huston for information, calculations and layout of the Paradise Boulevard storm drain.

III. LYON BLVD. STORM DRAIN OPTIONS

A. Option 1: Free Discharge, All New Storm Drain, Full Conveyance

Option 1 is a storm drain only option without detention and, consequently, includes expansion of the existing storm drain. This option requires concrete box culverts (CBC) as large as 12' X 12'. The entire network including flow rates can be seen on Exhibit 3. The flow

rate in the pipe network coming into the intersection of Paradise and Lyon is 1,453 cfs, and the box culvert size is 12' X 12' with a slope of 0.2%. Under this option, the storm drain on the north side of the intersection must be an 11' X 10' CBC, and the replacement of the existing storm drain must be 96" pipe. The total flow at the outfall to the Calabacillas is 1,983 cfs.

B. Option 2: Existing Storm Drain, 1 Large Detention Basin South of Paradise Blvd.

Option 2 maintains the existing storm drain as is and has one large detention pond to attenuate flows to its capacity. Option 2 is shown in Exhibit 4. A possible location for the pond was found to be near the intersection of Paradise and Lyon. This site is chosen because it can collect runoff from all of the basins in the study area. This is important since even the smaller sub-basins adjacent to the chosen pond site (311N&S, 312, 310, and 8) could overwhelm the existing storm drain if their flows are not attenuated. The pond would need to have storage of 65.4 ac-ft and would cover an area of approximately 8-9 acres. This option would also require very large concrete box culverts (12' X 12') upstream of the pond. The peak flow rate entering the pond is 1509 cfs, and the peak outflow is 174 cfs. The pipes north of the intersection to the existing storm drain would need to be 84" and 90".

C. Option 3: Existing Storm Drain, 4 Smaller Detention Basins South of Paradise Blvd.

There is more flexibility in Option 3, which is shown in Exhibit 5. Four detention ponds are used to attenuate flows in this option. The largest pipe in the system south of the intersection of Lyon and Paradise is 66", and the largest pipe north of the intersection is 84". The total amount of storage provided by the ponds is 113.6 ac-ft, and the approximate area needed for all four ponds is 15 acres. The peak outflow from the final pond, which enters the Lyon Boulevard storm drain, is 131 cfs.

**D. Option 4: Existing Storm Drain, Full Conveyance under Pressure Flow
Conditions Assuming 212 cfs from Area South of Paradise Blvd.**

As mentioned in the introduction, Option 4 is exclusively for the Paradise and Lyon Boulevard Storm Drains. It includes a hydraulic grade line (HGL) analysis to determine the maximum flow rate that can be allowed from the south at the intersection of Paradise and Lyon, while tying to the existing storm drain. The maximum allowable flow rate is 212 cfs. The largest pipe size required is 90". Larger sizes were tried just north of the intersection, but the ultimate control of the system is the existing storm drain. Therefore, the 90" gave as much capacity as a larger diameter pipe. Exhibit 6 contains a plan and profile sheet showing Option 4, as well as a profile of the basalt along the Lyon Boulevard alignment.

IV. REVISED PIEDRAS MARCADAS DAM WATERSHED HYDROLOGY AND SCENARIOS

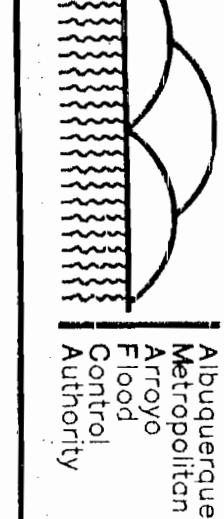
Subsequent to the development of the four options for the Lyon Blvd. storm drain, an outfall to the Piedras Marcadas Dam from developing areas upstream of the Petroglyph National Monument again became a possibility with the designation of the future Paseo del Norte alignment. In order to take advantage of this outfall in the Paseo del Norte corridor, the effects on the dam of all current and future development in the Piedras Marcadas watershed were investigated.

The total drainage area to the dam is nearly 4.0 square miles. The drainage area is slightly less than that reported in the Molzen-Corbin study primarily because Basin 311N is now shown as being diverted to the Calabacillas Arroyo via the future Lyon Boulevard storm drain. Figure 1 shows the overall area draining to the dam (Molzen-Corbin - Alternative 9) as well as the areas being diverted to the Calabacillas Arroyo.

The drainage area to the dam includes the area west of Lyon Boulevard and south of the drainage divide to the Calabacillas Arroyo. The four Options previously discussed assumed a diversion of a large portion of this area to the Calabacillas Arroyo via the future Lyon Boulevard storm drain. This diversion is not incorporated into the revised hydrology because it was not required to meet the capacity of the dam.

N

ANALYSIS POINT	
PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AF)
H(Historic) E(existing) F(future)	84 304 590
	9.24 20 50



2.27 SQ. MI. TO
CALABACILLAS

0.47 SQ. MI. TO
CALABACILLAS

ADDED AREA FROM PARADISE
BLVD. STORM DRAIN REPORT

500 SERIES BASINS FROM
VENTANA RANCH MASTER PLAN

600 SERIES BASINS FROM
VENTANA RANCH MASTER PLAN

319

318

CHANNEL

POND

314

313

311

310

308

307

306

305

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The Molzen-Corbin AHYMO model (Option 9) served as the base model for this analysis. It has been appended with the Ventana Ranch, Shenandoah and Rancho Sereno subdivisions. The Ventana Ranch Detention Dam, shown in Basin 316, has been constructed and is responsible for diverting over two square miles of the upper watershed to the Calabacillas Arroyo. The second diversion area to the Calabacillas Arroyo is the Lyon Boulevard storm drain. This diversion is planned for the future and was presented in the original Molzen-Corbin model, but with a different drainage area to the outlet.

In addition to these changes, the AHYMO model has been modified in a number of other ways. Most notably, the proposed pond in Basin 302/304 has been removed; the Shenandoah and Rancho Sereno Subdivision models, located within Basins 301 and 102 respectively, have been edited so that all the hydrographs are being added into the dam. A new basin has been created out of Basin 205 for the Paradise Ridge Subdivision. Routes have been added to reflect the new Paradise Boulevard storm drain.

When all the revisions were included, the model indicated a smaller drainage area to the dam than in the Molzen-Corbin report. Comparisons were made between the original AHYMO model and subsequent changes over the last ten years. It was discovered that when the subbasins were redefined, and the Shenandoah and Rancho Sereno Subdivisions were incorporated, the new drainage basin boundaries did not match the original basin boundaries in Basins 102 and 301. A new basin in 102 was added to account for this and area added to offsite Basin SHENO1E in 301.

The information used to calculate the required sediment storage in the dam was based on Dr. Richard Heggen's Sediment Study of the Piedras Marcadas Watershed as included in the Piedras Marcadas DMP. His results did not include any diversions to the Calabacillas Arroyo, so the total drainage area to the dam was larger than it is today. No reduction in sediment to the dam for the reduced area has been included in this analysis. From observations made during a site visit, it was noted that vegetation has grown in the dam basin. No account for any loss of capacity due to the vegetation has been made.

The results of the analysis of the capacity of the Piedras Marcadas Dam at the emergency spillway are as follows:

	Source	Volume (ac-ft)
Piedras Marcadas Dam Design Capacity (to the crest of the emergency spillway)	1995 Revised Grading Plan by BHI	307 ac-ft
Sediment Volume (5 x annual + 100-year) (5 x 0.31 ac-ft + 2.07 ac-ft)	Piedras Marcadas DMP, 1993	3.6 ac-ft
Available storage in Piedras Marcadas Dam		303 ac-ft
100-Yr Runoff Volume	2002 Revised AHYMO model by BHI	292 ac-ft
Excess Capacity in the Piedras Marcadas Dam		11 ac-ft
Freeboard in the Piedras Marcadas Dam		0.55 ft

In order to meet an AMAFCA requirement for one foot of freeboard below the emergency spillway, a maximum of 280 ac-ft of runoff volume can be allowed into the dam. The runoff volume into the Piedras Marcadas Dam cannot be reduced to the recommended 280 ac-ft while not exceeding the 212 cfs capacity of the Option 4 Lyon Boulevard storm drain if free discharge from all basins to Lyon Boulevard is assumed. Below are presented results for two scenarios that would satisfy the dam volume constraint (280 ac-ft) and the Lyon Blvd. storm drain capacity constraint (212 cfs). Refer to Figure 2.

A. Scenario 1: Do not Exceed Lyon Boulevard Storm Drain Capacity

To not exceed the Lyon Boulevard storm drain capacity, only Basins 311N and 311S can free discharge to Lyon Boulevard. The total 100-year flow from these basins is approximately 205 cfs. The runoff volume into the dam is reduced to 287 ac-ft. Recall that in the original model Basin 311N was already diverted north.

B. Scenario 2: Disregard Lyon Boulevard Storm Drain Capacity and Meet the Required Runoff Volume

To reduce the total runoff volume into the dam to 280 ac-ft, Basins 311N, 311S, 310, 313SA and 315NE need to be diverted to the Lyon Boulevard storm drain. The total 100-year runoff from these basins is 400 cfs. The calculated runoff volume to the dam is 278 ac-ft.

The most obvious way to meet both limitations is to construct a detention pond(s) that would attenuate the flows in the second scenario to the 212 cfs capacity. Another option to meet both criteria is to convert the Piedras Marcadas Dam from retention to detention. The Piedras Marcadas Dam is currently operated as a retention dam; however, modifications to create a detention facility are possible and could prove very beneficial. Only after downstream facilities are capable of accepting flows impounded in the dam can the principle spillway (a 36" pipe) be opened. If the principle spillway were to be extended to the Rio Grande (approximately 4500'), the hydraulic capacity of the dam and its ability to accept more runoff would be enhanced. Even with none of the area shown in being diverted to the Lyon Blvd. storm drain, there is still approximately 45 ac-ft of capacity in the dam with the 36" pipe open to the river. Figure 2 illustrates the drainage areas corresponding to each scenario above. Note that the basin labeled "312" is actually only a very small portion of Basin 312 in the AHYMO model. The majority of the basin lies north of Paradise Boulevard. Therefore, runoff from the sliver shown does not contribute to the total flow in the storm drain south of Paradise Boulevard.

In general, the basin divides shown are based on topography and are similar to those of the Molzen-Corbin study. The exception is Basin 315NE, which was based on lot lines. It seemed prudent to create the basin in this manner so that the entirety of Lot 6 will be diverted to the storm drain, rather than having only, a portion of it diverted. Basins 313SA and 315NE were originally part of larger basins, 313S and 315N respectively, but were subdivided to suit this analysis.

V. COST ESTIMATE FOR THE FOUR LYON BLVD. OPTIONS

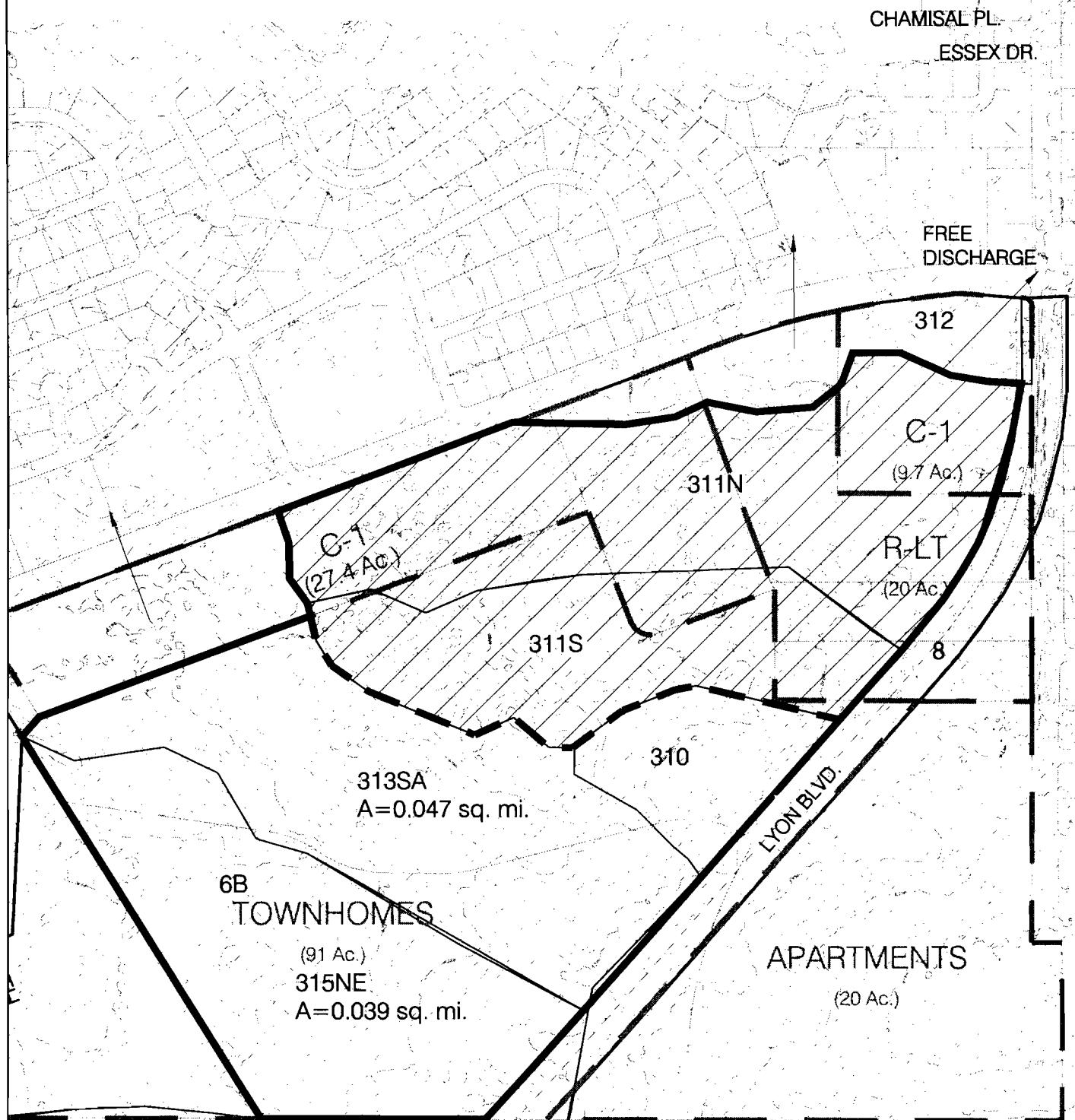
There are four design parameters that strongly impact the cost of the options; storm drain size, trench depth, detention pond size, and land costs. The first three are especially important because they affect the amount of basalt rock removal that will be necessary. In the areas where basalt rock removal was determined to be necessary there are no trenching costs, but there is a backfill cost since the basalt rock cannot be used as backfill. Where trenching is specified, the unit cost was based on the 1998 Unit Cost used by the City of Albuquerque with a 30% increase to

LEGEND

SCENARIO 1

DIVERTED AREA THAT MAXIMIZES
STORM DRAIN CAPACITY

SCENARIO 2

DIVERTED AREA REQUIRED TO REDUCE
RUNOFF VOLUME TO DAM ~ 280 ac. ft.**Bohannan ▲ Huston**

Courtyard I 7500 Jefferson St. NE Albuquerque, NM 87109-4335

ENGINEERING ▲ SPATIAL DATA ▲ ADVANCED TECHNOLOGIES

**PIEDRAS MARCADAS WATERSHED AND
LYON BOULEVARD STORM DRAIN****BASINS FOR SCENARIOS 1 AND 2****FIGURE 2**

DRAWN BY	S.F.G.	DATE	01.07.03
CHECKED BY	D.J.G.	PROJECT NO	00289.09C

make it comparable to recent contractors' estimates for storm drain construction. The pond costs were determined based on the costs of recent AMAFCA dams and recently constructed ponds designed by Bohannan-Huston. The dams and ponds were placed in an Excel spreadsheet based on size and cost per acre-foot. An equation was derived for a fitted curve, and that equation was used to determine the cost per acre-foot for the ponds used in the estimate. A chart showing the points and fitted curve is shown in Appendix B. The reinforced concrete pipe / concrete box culverts costs were determined by using the 1998 Unit Cost, recent contractor bids, and information provided by a local supplier and local contractor. The 20% contingency used for the cost estimates in the preliminary report has been reduced to 10% for the cost estimates presented here because unit costs that are more accurate were used. The cost of the land was roughly estimated at \$50,000 per acre.

The most important aspect of the cost of any of the options is the presence of basalt rock. One area that is proven to have basalt is the area from the intersection of Paradise and Lyon Boulevards to the outfall. Basalt removal calculations were performed in this area based on information in the Conceptual Lyon Report (2000), which is based on borehole data. Refer to Appendix E. However, it is assumed that all the trenches south of Paradise Boulevard will also require basalt removal. This assumption is based on visual appraisal of the surface and borehole data provided in the "Unser Middle Transportation Corridor Study" done by Leedshill-Herkenhoff in 1992. Two boreholes that fall within the study area near the proposed Paseo Del Norte alignment show basalt rock from 2-5 feet below the surface through 31-38 feet below the surface. The basalt removal greatly increases the costs of all options. The basalt rock removal volumes were calculated based on a typical trench prism in rock. This assumes vertical sides. It was also assumed that basalt rock removal will be necessary for the ponds unless they are located in a valley where a berm could be placed above ground to gain storage. The pond in Option 2, therefore, requires basalt rock removal, as do Ponds 1 and 3 in Option 3. The cost of basalt rock removal was based on current projects near the study area.

The estimated costs of the four options are shown below in Table 3. The estimated construction cost for the Paradise Boulevard portion of the storm drain system is \$1,353,000, assuming that there is no basalt rock removal. For detailed estimates, see Appendix C.

Table 3 – Estimated Construction Cost

OPTION	Primary Study Area	Lyon Boulevard Storm Drain	Paradise Boulevard Storm Drain	Total without Paradise Blvd. Storm Drain	Total with Paradise Blvd. Storm Drain
OPTION 1	17,031,000	7,800,000	1,353,000	24,831,000	26,184,000
OPTION 2	21,742,000	4,687,000	1,353,000	26,429,000	27,782,000
OPTION 3	14,277,000	3,082,000	1,353,000	17,359,000	18,712,000
OPTION 4	NA	3,337,000	1,353,000	NA	NA

VI. CONCLUSION

A. Four original Lyon Blvd. storm drain options

Though Option 3 is the lowest cost option for the Paradise/Lyon Blvd. storm drain, Option 4 is the recommended option. Though slightly more expensive than Option 3, Option 4 will maximize use of the existing storm drain and allow a maximum area south of Paradise Blvd. to flow to the storm drain. There are also other advantages to Option 4, including constructability. All of the items in Option 4 are commonly constructed in the Albuquerque area, whereas the large box culverts required in the first two options are not. This could lead to more problems in design and construction. Having such large box culverts also increases the possibility for conflicts with existing utilities and will make the design and construction of future utilities in the area much more difficult. Although the Option 4 configuration is more costly than Option 3 by \$255,000, it allows approximately 80 cfs more than Option 3 into the Lyon Boulevard storm drain. This increased flow rate means that less ponding would be required south of Paradise Boulevard, which would reduce the pond costs. It is also recommended that more information be acquired concerning the basalt in the area, as this is the most expensive element of any plan.

B. Additional Scenarios

After completion of the four options investigation, an outfall for developed runoff upstream of the Petroglyph National Monument to the Piedras Marcadas Dam through the Paseo del Norte corridor became a possibility. Additional hydrologic scenarios were studied to make use of this outfall.

The Piedras Marcadas Dam can accept a volume of 280 ac-ft. The watershed area that can flow with free discharge to the dam, based on Molzen-Corbin's development assumptions, can be maximized to make full use of this capacity. This allows for a reduction in the area flowing to the Lyon Blvd. storm drain compared to the four original options. Used in conjunction with the Option 4 storm drain, the area immediately south and west of the Lyon Blvd. /Paradise Blvd. intersection can flow to the storm drain at a maximum flow rate of 212 cfs. In order to accomplish this flow rate some detention ponding is necessary.

If the Piedras Marcadas Dam can be converted to a detention dam additional areas would be able to flow with free discharge to the dam. This assumes the conveyance facilities to the dam already in place can accept the added flow.

ZONE/USE	LAND TREATMENT PERCENTAGES			
	A	B	C	D
O-1	0	20	20	60
C-1	0	5	5	90
R-T	0	15	20	65
Roadway	0	0	10	90
Apartments	0	15	15	70
Town Homes	0	15	20	65
R-D	0	13.5	13.5	73
R-LT	0	15	25	60
Chamisa	48	10	25	17
School	0	15	25	60

AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -

INPUT FILE = Opt1_06.HYM
RUN DATE (MON/DAY/YR) = 07/05/2001
USER NO. = AHYMO-S-9702c1BcohanHu AH

COMMAND HYDROGRAPH FROM TO PEAK RUNOFF
IDENTIFICATION ID ID AREA VOLUME
NO. NO. (SQ MI) (CFS) (AC- FT)

VERSION: 1997.02C TIME TO CFS
PAGE = 1
RUNOFF PER
VOLUME ACRE
(INCHES) NOTATION

PROJECT NAME: LYONS BLVD STORM DRAIN

JOB NO. 00280C4.01
DATE: JUNE, 2001

INPUT FILE NAME: Opt1_06.HYM
OUTPUT FILE NAME: Opt1_06.out
FILES LOCATION: BHI-MAIN\00280\HYDRO\DESIGN\AHYMO

COMMENTS:

6-29-01: Divided Sub-basin 6 into 6A and 6B
6-19-01: Added the BHI study of the LYONS SD done in 99
and modified for the additional flows

*S 6-01: Added Basin 8

*S 5-16-01: Revised Basins 1&2 and added Basin 7

*S 5-9-01: Basin 315 has been broken into several smaller basins

*S 4-2-01: Basins are based on those used in previous reports
in this area, originally from Molzen-Corbin's Piedras
Marcadas Arroyo Analysis (1991); however, basins
have been modified to reflect new mapping and the
maximum drainable area (based on slope).

*S ///

RAINFALL TYPE= 2
SEDIMENT BULK
*S COMPUTE NM HYD SUB-BASIN 1
*S ROUTE MCUNGE ROUTE 1 through 4.5' pipe for 1350'
ROUTE MCUNGE RT1 1 12 .03540 77.57
*S SUB-BASIN 2 COMPUTE NM HYD 2.00 - 2 .02490 65.15
*S Add Sub-basin 2 and the Routed Sub-basin 1
ADD HYD RT1&2 12& 2 13 .06030 136.94
*S Route Sub-basin 2 and the upstream flow through 920' of 66" pipe
ROUTE MCUNGE RT2UP 13 14 .06030 130.44
*S SUB-BASIN 3 COMPUTE NM HYD 3.00 - 3 .10070 185.06
*S Add Sub-basin 3 to upstream flow in pipe
ADD HYD RT2UP&3 14& 3 15 .16100 308.27
*S Route Sub-basin 3 and the upstream flow through 530' of 90" pipe
ROUTE MCUNGE RT3UP 15 16 .16100 300.99
*S SUB-BASIN 4

TIME TO CFS
PAGE = 1
RUNOFF PER
VOLUME ACRE
(INCHES) NOTATION

COMMAND HYDROGRAPH FROM TO PEAK RUNOFF
IDENTIFICATION ID ID AREA VOLUME
NO. NO. (SQ MI) (CFS) (AC- FT)

TIME TO CFS
PAGE = 2
RUNOFF PER
VOLUME ACRE
(INCHES) NOTATION

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COMPUTE NM HYD      4.00   -     4    .16200   361.61   18.848   2.18149   1.550   3.488 PER IMP= 78.80
  *S Add Sub-basin 4 to upstream flow in pipe
  ADD HYD          RT3UP&4 16& 4 17   .32300   638.94   37.049   2.15069   1.550   3.091
  *S Route Sub-basin 4 and upstream flow through 465' of 114" pipe
ROUTE MCUNGE        RT4UP   17 18   .32300   624.22   36.899   2.14196   1.600   3.020 CCODE = .2
  *S SUB-BASIN 5
COMPUTE NM HYD      5.00   -     5    .04330   106.46   4.542   1.96678   1.500   3.842 PER IMP= 65.70
  *S Add Sub-basin 5 to upstream flow in pipe
  ADD HYD          RT4UP&5 18& 5 19   .36630   707.27   41.441   2.12126   1.550   3.017
  *S Route Sub-basin 5 and upstream flow through 120" pipe for 885'
ROUTE MCUNGE        RT5UP   19 20   .36630   681.43   41.204   2.10915   1.600   2.907 CCODE = .2
  *S SUB-BASIN 7
COMPUTE NM HYD      7.00   -     30   .03350   66.49   3.913   2.18983   1.600   3.101 PER IMP= 79.50
  *S Add Sub-basin 7 to upstream flow in pipe
  ADD HYD          RT5UP&6&7 20&30 31   .39980   747.93   45.117   2.11591   1.600   2.923
  *S Route Sub-basin 7 and upstream flow through 126" pipe for 760'
ROUTE MCUNGE        RT7UP   31 21   .39980   729.73   44.963   2.10870   1.600   2.852 CCODE = .2
  *S SUB-BASIN 6A
COMPUTE NM HYD      6A   -     51   .27620   451.78   29.806   2.02337   1.650   2.556 PER IMP= 69.20
  *S Route Sub-basin 6A through 2500' of 66" pipe
ROUTE MCUNGE        RT6A   51 52   .27620   451.17   29.806   2.02338   1.700   2.552 CCODE = .2
  *S SUB-BASIN 6B
COMPUTE NM HYD      6B   -     6    .07550   184.93   7.873   1.95532   1.500   3.827 PER IMP= 65.00
  *S Add Sub-Basin 6B to the Routed 6A
  ADD HYD          RT6A&6B 52& 6 53   .35170   534.75   37.679   2.00877   1.650   2.376
  *S Add Sub-basin 6A and 6B to upstream flow in pipe
  ADD HYD          RT5UP&6 21&53 22   .75150   1253.30   82.642   2.06193   1.650   2.606
  *S SUB-BASIN 313
COMPUTE NM HYD      313.00   -     7    .05940   122.50   6.488   2.04812   1.550   3.222 PER IMP= 70.70
  *S Add Sub-basin 313 to upstream flow in pipe
  ADD HYD          RT6UP&313 22& 7 23   .81090   1361.68   89.131   2.06092   1.600   2.624
  *S Route Sub-basin 313 and upstream flow through 156" pipe for 700'
ROUTE MCUNGE        RT313UP 23 24   .81090   1343.45   88.864   2.05476   1.650   2.589 CCODE = .2
  *S SUB-BASIN 310
COMPUTE NM HYD      310.00   -     8    .01140   27.94   1.189   1.95532   1.500   3.830 PER IMP= 65.00
  *S Add Sub-basin 310 to upstream flow in pipe
  ADD HYD          RT313UP&310 24& 8 25   .82230   1358.65   90.053   2.05318   1.650   2.582
  *S Route Sub-basin 310 and upstream flow through 156" pipe for 1000'
ROUTE MCUNGE        RT310UP 25 26   .82230   1331.34   89.687   2.04504   1.650   2.530 CCODE = .2
  *S SUB-BASIN 311S
COMPUTE NM HYD      311.01   -     9    .02920   72.19   3.090   1.98409   1.500   3.863 PER IMP= 66.70
  *S Add Sub-basin 311S to upstream flow in pipe
  ADD HYD          RT310UP&311S 26& 9 27   .85150   1370.55   92.777   2.04295   1.650   2.515
  *S Route Sub-basin 311S and upstream flow through 156" pipe for 150'
ROUTE MCUNGE        RT311SUP 27 28   .85150   1370.55   92.777   2.04295   1.650   2.515
  *S SUB-BASIN 311N
COMPUTE NM HYD      311.02   -     10   .05060   109.82   5.979   2.21552   1.550   3.391 PER IMP= 80.90
  *S Add Sub-basin 311N to upstream flow in pipe
  ADD HYD          RT311SUP&311 28&10 29   .90210   1463.34   98.756   2.05262   1.650   2.535
  *S Route Sub-basin 311N and upstream flow through 156" pipe for 1250'
ROUTE MCUNGE        RT311NUP 29 30   .90210   1407.20   98.074   2.03846   1.650   2.437 CCODE = .2
  *S SUB-BASIN 312S

FROM TO           PEAK DISCHARGE (CFS) RUNOFF VOLUME (AC-FT) RUNOFF (INCHES) TIME TO PEAK (HOURS)
HYDROGRAPH ID ID AREA (SQ MI) NO. NO. PER ACRE CFS PAGE = 3
IDENTIFICATION NO. NO. (SQ MI) NO. NO. PER ACRE NOTATION
COMMAND          312.00 -   11   .01270   33.05   1.484 2.19032 1.500
COMPUTE NM HYD      312.00 -   11   .01270   33.05   1.484 2.19032 1.500

```

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ADD HYD RT311NU&312 30&11 31 .91480 1425.39 99.558 2.04057 1.650 2.435
  *S Route Sub-basin 312S and upstream flow through 156" pipe for 100'
ROUTE MCUNGE RT312SUP 31 32 .91480 1425.39 99.558 2.04057 1.650 2.435 CCODE = .0
  *S SUB-BASIN 8

COMPUTE NM HYD 8.00 - 33 .01760 29.84 2.235 2.38065 1.700 2.649 PER IMP= 90.00
  *S Add Sub-basin 8 to upstream flow in pipe
ADD HYD RT312SUP&8 32&33 34 .93240 1453.35 101.793 2.04699 1.650 2.435
*****END *****
```

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ADD HYD          105UP 17&18   19    .07200    146.78    7.001    1.82318    1.550    3.185
*S***** ROUTE 105UP TO LYONS*****      .07200    146.47    6.985    1.81910    1.600    3.179 CCODE = .1
ROUTE MCUNGE    RT105UP 19     20    .07200    146.47    6.985    1.81910    1.600    3.179 CCODE = .1
*S***** CALC BASIN 105.1 FLOW *****      .00900    20.94    .875    1.82319    1.500    3.635 PER IMP= 59.00
COMPUTE NM HYD  105.10   -    21    .00900    20.94    .875    1.82319    1.500    3.635 PER IMP= 59.00
*S*** ADD 105UP TO 105.1*****      -    .00900    20.94    .875    1.82319    1.500    3.635 PER IMP= 59.00
ADD HYD          105.1UP 20&21   22    .08100    161.00    7.860    1.819.4    1.600    3.106
*S***** CALC BASIN 107 FLOW *****      .08100    161.00    7.860    1.819.4    1.600    3.106
COMPUTE NM HYD  107.00   -    23    .06700    119.80    6.515    1.82319    1.600    2.794 PER IMP= 59.00
*S***** CALC BASIN 108 FLOW *****      .06700    119.80    6.515    1.82319    1.600    2.794 PER IMP= 59.00
COMPUTE NM HYD  108.00   -    24    .01000    23.26    .972    1.82319    1.500    3.635 PER IMP= 59.00
*S*** ADD 107 TO 108*****      -    .01000    23.26    .972    1.82319    1.500    3.635 PER IMP= 59.00
ADD HYD          108UP 23&24   25    .07700    137.35    7.487    1.82318    1.550    2.787
*S*** ADD RT312.1 TO AP108*****      .07700    137.35    7.487    1.82318    1.550    2.787
ADD HYD          AP6-AP108UP 16&25  26    1.45840    1979.92    150.793    1.93868    1.650    2.121
*S***** CALC BASIN 108.1 FLOW *****      1.45840    1979.92    150.793    1.93868    1.650    2.121
COMPUTE NM HYD  108.10   -    27    .01100    25.59    1.070    1.82319    1.500    3.634 PER IMP= 59.00
*S*** ADD 108.1 TO 105.1UP*****      -    .01100    25.59    1.070    1.82319    1.500    3.634 PER IMP= 59.00
ADD HYD          AP7-AP108.1U 27&22  28    .09200    178.76    8.930    1.81997    1.600    3.036
*S***** ROUTE DISCHARGE THRU PIPE TO IRVING 144" for 500*****      .09200    178.76    8.930    1.81997    1.600    3.036
ROUTE MCUNGE    RT312.1  26     29    1.45840    1834.36    148.629    1.91085    1.700    1.965 CCODE = .2
*S*** ADD RT312.1 TO 108.1UP*****      1.45840    1834.36    148.629    1.91085    1.700    1.965 CCODE = .2
ADD HYD          AP108.1UP 29&28  30    1.55040    1983.23    157.559    1.90546    1.650    1.999
FINISH

```


COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATION
ROUTE MCUNGE		RT3UP	15	16	.16100	300.99	18.201	2.11970	1.600	2.921 CCODE = .2
*S	SUB-BASIN 4									
COMPUTE NM HYD	4.00	-	4		.16200	361.61	18.848	2.18149	1.550	3.488 PER IMP= 78.80
*S	Add Sub-basin 4 to upstream flow in pipe									
ADD HYD	RT3UP&4 16& 4	17			.32300	638.94	37.049	2.15069	1.550	3.091
*S	Route Sub-basin 4 and upstream flow through 465' of 114" pipe									
ROUTE MCUNGE	RT4UP	17	18		.32300	624.22	36.899	2.14196	1.600	3.020 CCODE = .2
*S	SUB-BASIN 5									
COMPUTE NM HYD	5.00	-	5		.04330	106.46	4.542	1.96678	1.500	3.842 PER IMP= 65.70
*S	Add Sub-basin 5 to upstream flow in pipe									
ADD HYD	RT4UP&5 18& 5	19			.36630	707.27	41.441	2.12126	1.550	3.017
*S	Route Sub-basin 5 and upstream flow through 120" pipe for 885'									
ROUTE MCUNGE	RT5UP	19	20		.36630	681.43	41.204	2.10915	1.600	2.907 CCODE = .2
*S	SUB-BASIN 7									
COMPUTE NM HYD	7.00	-	30		.03350	66.49	3.913	2.18983	1.600	3.101 PER IMP= 79.50
*S	Add Sub-basin 7 to upstream flow in pipe									
ADD HYD	RT5UP&6&7 20&30	31			.39980	747.93	45.117	2.11591	1.600	2.923
*S	Route Sub-basin 7 and upstream flow through 126" pipe for 760'									
ROUTE MCUNGE	RT7UP	31	21		.39980	729.73	44.963	2.10870	1.600	2.852 CCODE = .2
*S	SUB-BASIN 6A									
COMPUTE NM HYD	6A	-	51		.27620	451.78	29.806	2.02337	1.650	2.556 PER IMP= 69.20
*S	Route Sub-basin 6A through 2500' of 66" pipe									
ROUTE MCUNGE	RT6A	51	52		.27620	451.17	29.806	2.02338	1.700	2.552 CCODE = .2
*S	SUB-BASIN 6B									
COMPUTE NM HYD	6B	-	6		.07550	184.93	7.873	1.95532	1.500	3.827 PER IMP= 65.00
*S	Add Sub-Basin 6B to the Routed 6A									
ADD HYD	RT6A&6B 52& 6	53			.35170	534.75	37.679	2.00877	1.650	2.376
*S	Add Sub-basin 6A and 6B to upstream flow in pipe									
ADD HYD	RT5UP&6 21&53	22			.75150	1253.30	82.642	2.06193	1.650	2.606
*S	SUB-BASIN 313									
COMPUTE NM HYD	313.00	-	7		.05940	122.50	6.488	2.04812	1.550	3.222 PER IMP= 70.70
*S	Add Sub-basin 313 to upstream flow in pipe									
ADD HYD	RT6UP&313 22& 7	23			.81090	1361.68	89.131	2.06092	1.600	2.624
*S	Route Sub-basin 313 and upstream flow through 156" pipe for 700'									
ROUTE MCUNGE	RT313UP	23	24		.81090	1343.45	88.864	2.05476	1.650	2.589 CCODE = .2
*S	SUB-BASIN 310									
COMPUTE NM HYD	310.00	-	8		.01140	27.94	1.189	1.95532	1.500	3.830 PER IMP= 65.00
*S	Add Sub-basin 310 to upstream flow in pipe									
ADD HYD	RT313UP&310 24& 8	25			.82230	1358.65	90.053	2.05338	1.650	2.582
*S	Route Sub-basin 310 and upstream flow through 156" pipe for 1000'									
ROUTE MCUNGE	RT310UP	25	26		.82230	1331.34	89.687	2.04504	1.650	2.530 CCODE = .2
*S	SUB-BASIN 311S									
COMPUTE NM HYD	311.01	-	9		.02920	72.19	3.090	1.98409	1.500	3.863 PER IMP= 66.70
*S	Add Sub-basin 311S to upstream flow in pipe									
ADD HYD	RT310UP&311S 26& 9	27			.85150	1370.55	92.777	2.04295	1.650	2.515
*S	Route Sub-basin 311S and upstream flow through 156" pipe for 150'									
ROUTE MCUNGE	RT311SUP	27	28		.85150	1370.55	92.777	2.04295	1.650	2.515 CCODE = .0
*S	SUB-BASIN 311N									
COMPUTE NM HYD	311.02	-	10		.05060	109.82	5.979	2.21552	1.550	3.391 PER IMP= 80.90
*S	Add Sub-basin 311N to upstream flow in pipe									
ADD HYD	RT311SUP&311 28&10	29			.90210	1463.34	98.756	2.05262	1.650	2.535
*S	SUB-BASIN 312S									
COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA NO.	DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 3 NOTATION
COMPUTE NM HYD	312.00	-	11							
COMPUTE NM HYD										

COMMAND PAGE = 3
 COMPUTE NM HYD 312.00 - 11 .01270 33.05 1.484 2.19032 1.500 4.066 PER IMP= 79.30

*S Add Sub-basin 312S to upstream flow into the pond
 ADD HYD RT311NUP&312 29&11 30 .91480 1481.53 100.239 2.05453 1.650 2.530
 *S SUB-BASIN 8
 COMPUTE NM HYD 8.00 - 31 .01760 29.84 2.235 2.38065 1.700 2.649 PER IMP= 90.00
 *S Add Sub-basin 8 to upstream flow into the pond
 ADD HYD RT312SUP&8 30&31 32 .93240 1509.49 102.474 2.06069 1.650 2.530
 *S ROUTE FLOW THROUGH POND WITH 60" OUTFLOW PIPE
 ROUTE RESERVOIR Pond 32 41 .93240 173.98 99.187 1.99459 2.500 .292 AC-FT= 65.410
 *S Route POND OUTFLOW through 72" pipe for 300'
 ROUTE MCUNGE RT311NUP 41 33 .93240 173.93 99.166 1.99416 2.500 .291 CCODE = .2
 *S***** FROM FORMER BHI REPORT ON LYONS SD MODIFIED FOR INCREASED
 *S***** FLOWS
 *S*****
 S* THE DOWNSTREAM FACE OF LAS VENTANAS DRAINAGE FACILITY DRAINS EAST TO **
 S* BUENA VISTA AVE, TO LA PAZ RD, THRU BASIN 314, AND FINALLY TO POND AT**
 S* NORTH SIDE OF PARADISE BLVD**
 *S*****
 *S*****PIEDRAS MARCadas WATERSHED*****
 *S***** CALC BASIN 316 FLOW*****
 COMPUTE NM HYD 316.00 - 1 .03000 60.16 2.421 1.51308 1.500 3.133 PER IMP= 45.00
 *S***** ROUTE 316 THRU 313N PARADISE*****
 ROUTE MCUNGE RT316 1 2 .03000 53.34 2.386 1.49151 1.750 2.778 CCODE = .1
 *S***** CALC BASIN 313N FLOW*****
 COMPUTE NM HYD 313N - 3 .07800 135.26 8.065 1.93878 1.600 2.709 PER IMP= 65.00
 *S*** ADD RT316 TO 313N*****
 ADD HYD 313NUP 2& 3 4 .10800 171.30 10.452 1.81453 1.700 2.478
 *S***** CALC BASIN 314 FLOW*****
 COMPUTE NM HYD 314.00 - 5 .08900 185.78 7.273 1.53229 1.500 3.262 PER IMP= 43.00
 *S*** ADD 313NUP TO 314*****
 ADD HYD API-314UP 4& 5 6 .19700 296.39 17.725 1.68702 1.550 2.351
 *S***** CALC BASIN 314.1 FLOW*****
 COMPUTE NM HYD AP2 314.1 - 7 .03600 74.63 2.867 1.49321 1.500 3.239 PER IMP= 40.00
 *S*** ADD 314UP TO 314.1 FOR DISCHARGE INTO POND*****
 ADD HYD AP314.1UP 6& 7 8 .23300 363.30 20.592 ASSUME 48" D 1.65707 1.550 2.436
 *S*****ROUTE AP314.1UP FLOW THROUGH PARK POND W/ ASSUMED DISCHARGE.
 ROUTE RESERVOIR AP3-RT314.1P 8 9 .23300 108.05 20.592 1.65707 2.050 725 AC-FT= 9.449
 *S***** ROUTE DISCHARGE THRU PIPE TO UNSER LYONS *****
 ROUTE MCUNGE 113.40 9 10 .23300 108.02 20.584 1.65640 2.150 .724 CCODE = .1
 *S***** CALC BASIN 312 FLOW*****
 COMPUTE NM HYD 312.00 - 11 .20200 349.49 19.641 1.82308 1.600 2.703 PER IMP= 59.10
 *S*** ADD 113.4 TO 312*****
 ADD HYD AP4 312UP 10&1 12 .43500 403.28 40.224 1.73380 1.600 1.449
 *S*** ADD NEW FLOW FROM SOUTH UNSER SD (6/01)
 ADD HYD NewAP4 33&12 35 1.36740 437.98 139.390 1.91134 1.650 .500
 *S***** ROUTE DISCHARGE THRU PIPE TO ESSEX 84"*****
 ROUTE MCUNGE RT312UP 35 13 1.36740 435.37 139.330 1.91051 1.650 .497 CCODE = .1
 *S***** CALC BASIN 312.1 FLOW*****
 COMPUTE NM HYD AP5-312.1 - 14 .01400 32.56 1.361 1.82319 1.500 3.634 PER IMP= 59.00
 *S*** ADD RT312UP TO 312.1*****
 ADD HYD AP312.1 13&14 15 1.38140 453.16 140.691 1.90962 1.650 .513
 *S***** ROUTE THROUGH PIPE TO MH9 84"*****
 *S*****
 COMMAND HYDROGRAPH FROM TO PEAK RUNOFF TIME TO CFS PAGE = 4
 IDENTIFICATION ID ID AREA DISCHARGE VOLUME PEAK (CFS) (AC-FT) (INCHES) (HOURS)
 NO. NO. (SQ MI) (CFS) (AC-FT)
 ROUTE MCUNGE RT312.1 15 42 1.38140 449.64 140.663 1.90925 1.650 .509 CCODE = .2
 *S***** ROUTE DISCHARGE THRU PIPE TO ALDER 84"*****
 ROUTE MCUNGE RT312.12 42 16 1.38140 449.64 140.663 1.90925 1.650 .509 CCODE = .0
 *S*CALABACILLAS WATERSHED**

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***** CALC BASIN 101 FLOW ****
COMPUTE NM HYD    101.00   -     17    .05100    103.51    4.959    1.82319    1.550    3.171 PER IMP= 59.00
***** CALC BASIN 105 FLOW ****
COMPUTE NM HYD    105.00   -     18    .02100    48.83    2.042    1.82319    1.500    3.633 PER IMP= 59.00
* S** ADD 101 TO 105***** *
ADD HYD          105UP 17&18  19    .07200    146.78    7.001    1.82318    1.550    3.185
***** ROUTE 105UP TO LYONS*****
ROUTE MCUNGE    RT105UP 19    20    .07200    146.47    6.985    1.81910    1.600    3.179 CCODE = .1
***** CALC BASIN 105.1 FLOW ****
COMPUTE NM HYD    105.10   -     21    .00900    20.94    .875    1.82319    1.500    3.635 PER IMP= 59.00
* S** ADD 105UP TO 105.1*****
ADD HYD          105.1UP 20&21  22    .08100    161.00    7.860    1.81954    1.600    3.106
***** CALC BASIN 107 FLOW ****
COMPUTE NM HYD    107.00   -     23    .06700    119.80    6.515    1.82319    1.600    2.794 PER IMP= 59.00
***** CALC BASIN 108 FLOW ****
COMPUTE NM HYD    108.00   -     24    .01000    23.26    .972    1.82319    1.500    3.635 PER IMP= 59.00
* S** ADD 107 TO 108*****
ADD HYD          108UP 23&24  25    .07700    137.35    7.487    1.82318    1.550    2.787
***** ADD RT312.1 TO AP108*****
ADD HYD          AP6-AP108UP 16&25  26    1.45840    572.08    148.151    1.90471    1.650    .613
***** CALC BASIN 108.1 FLOW ****
COMPUTE NM HYD    108.10   -     27    .01100    25.59    1.070    1.82319    1.500    3.634 PER IMP= 59.00
* S** ADD 108.1 TO 105.1UP*****
ADD HYD          AP7-AP108.1U 27&22  28    .09200    178.76    8.930    1.81997    1.600    3.036
***** ROUTE DISCHARGE THRU PIPE TO IRVING 90" ****
ROUTE MCUNGE    RT312.1  26    29    1.45840    572.08    148.151    1.90471    1.650    .613 CCODE = .0
* S** ADD RT312.1 TO 108.1UP*****
ADD HYD          AP108.1UP 29&28  30    1.55040    739.68    157.081    1.89968    1.650    .745
FINISH

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AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
INPUT FILE = Opt3 03.HYM

- VERSION : 1997.02.C RUN DATE (MON/DAY/YR) =07/03/2001
- USER NO. : AHYMO-S-9702C1BohanHu-AH

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1		
\$	PROJECT NAME:	LYONS BLVD STORM DRAIN MINI DRAINAGE MANAGEMENT PLAN								NOTATION		
\$	JOB NO.	00280C4_01										
\$	DATE:	June 25, 2001										
\$	INPUT FILE NAME:	Opt3_03.HYM										
\$	OUTPUT FILE NAME:	Opt3_03.out										
\$	FILES LOCATION:	BHI-MAIN\00280\HYDRO\DESIGN\AHYMO										
\$	COMMENTS:											
\$	7-2-01:	Divided Sub-basin 6 into 6A and 6B and added a pond										
\$	6-25-01:	Added Three Ponds										
\$	5-16-01:	Revised Basins 1&2 and added Basin 7										
\$	5-9-01:	Basin 315 has been broken into several smaller basins										
\$	4-2-01:	Basins are based on those used in previous reports in this area, originally from Molzen-Corbin's Piedras Marcadas Arroyo Analysis (1991); however, basins have been modified to reflect new mapping and the maximum drainable area (based on slope).										
\$	/	/										
\$	RAINFALL TYPE= 2											
\$	SEDIMENT BULK											
\$	SUB-BASIN 1											
\$	COMPUTE NM HYD	1.00 - 1					.03540	88.50	3.818	2.02214	1.500	3.906 PER IMP= 69.00
\$	ROUTE MCUNGEB	RT1 1 12					.03540	77.57	3.759	1.99087	1.550	3.424 CCODE = .2
\$	SUB-BASIN 2	2.00 - 2					.02490	65.15	2.902	2.18492	1.500	4.088 PER IMP= 79.10
\$	COMPUTE NM HYD	Add Sub-basin 2 and the Routed Sub-basin 1					.06030	136.94	6.660	2.07098	1.500	3.548
\$	ADD HYD	RT1&2 12& 2 13					.06030	of 6"	pipe			
\$	ROUTE MCUNGEB	Route Sub-basin 2 and the upstream flow through 920' RT2UP 13 14					.06030	130.44	6.611	2.05566	1.550	3.380 CCODE = .2
\$	SUB-BASIN 3	3.00 - 3					.10070	185.06	11.639	2.16716	1.650	2.871 PER IMP= 78.00
\$	COMPUTE NM HYD	Add Sub-basin 3 to upstream flow (will go to Pond 1) RT2UP&3 14& 3 15					.16100	308.27	18.250	2.12539	1.600	2.992
\$	SUB-BASIN 4	4.00 - 4					.16200	361.61	18.848	2.18149	1.550	3.488 PER IMP= 78.80
\$	COMPUTE NM HYD	Add Sub-basin 4 to upstream flow to go to Pond 1 RT3UP&4 15& 4 17					.32300	653.99	37.098	2.15353	1.550	3.164
\$	SUB-BASIN 5	5.00 - 5					.04330	106.46	4.542	1.96678	1.500	3.842 PER IMP= 65.70
\$	ROUTE MCUNGEB											
\$	SUB-BASIN 2											
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\$	SUB-BASIN 2											

COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATION
ROUTE MCUNGE		RT5	5	18	.04330	96.17	4.442	1.92359	1.500	3.470 CCODE = .2
*S Add Sub-basin 5 to Pond 1 Inflow										
ADD HYD	RT4UP&5	18&17	19	.36630	739.66	41.540	2.12635	1.550	3.155	
*S SUB-BASIN 7										
COMPUTE NM HYD	7.00	-	30	.03350	66.49	3.913	2.18983	1.600	3.101 PER IMP=	79.50
*S Add Sub-basin 7 to Pond1 Iflow										
ADD HYD	RT5UP&6&7	19&30	20	.39980	801.79	45.453	2.13167	1.550	3.134	
*S ROUTE FLOW THROUGH POND 1										
ROUTE RESERVOIR	Pondout	20	43	.39980	108.30	45.065	2.11347	2.300	.423 AC-FT=	27.690
*S Route Pond 1 Outflow through 60" pipe for 1645'										
ROUTE MCUNGE	RT5UP	43	21	.39980	107.92	45.030	2.11186	2.350	.422 CCODE =	.2
*S SUB-BASIN 6A										
COMPUTE NM HYD	6A	-	51	.27620	451.78	29.806	2.02337	1.650	2.556 PER IMP=	69.20
*S Route Sub-basin 6A through Pond 4										
*S ROUTE FLOW THROUGH POND WITH 42" OUTFLOW PIPE										
ROUTE RESERVOIR	Pond4out	51	52	.27620	64.33	29.393	1.99533	2.450	.364 AC-FT=	17.982
*S Route Pond 4 outflow through 2000' of 42" pipe										
ROUTE MCUNGE	RT6A	52	53	.27620	64.32	29.384	1.99478	2.500	.364 CCODE =	.2
*S SUB-BASIN 6B										
COMPUTE NM HYD	6B	-	6	.07550	184.93	7.873	1.95532	1.500	3.827 PER IMP=	65.00
*S Add Pond 4 outflow to 6B										
ADD HYD	P4RT&6B	53& 6	54	.35170	186.00	37.258	1.98631	1.500	.826	
*S SUB-BASIN 313										
COMPUTE NM HYD	313.00	-	7	.05940	122.50	6.488	2.04812	1.550	3.222 PER IMP=	70.70
*S Add Sub-basin 313 to Basin 6										
ADD HYD	Pond2inflow	54& 7	22	.41110	292.98	43.746	1.99524	1.500	1.114	
*S ROUTE FLOW THROUGH POND 2										
*S ROUTE FLOW THROUGH POND WITH 42" OUTFLOW PIPE										
ROUTE RESERVOIR	Pond2out	22	41	.41110	49.22	42.435	1.93545	3.950	.187 AC-FT=	14.199
*S Add outflow from Pond 2 to the Routed outflow from Pond 1										
ADD HYD	P1RT&P2 21&41	23	.81090	148.49	87.466	2.02243	2.500	.286		
*S Route Combined flow through 66" pipe for 700'										
ROUTE MCUNGE	RT313UP	23	24	.81090	148.30	87.431	2.02162	2.550	.286 CCODE =	.2
*S SUB-BASIN 310										
COMPUTE NM HYD	310.00	-	8	.01140	27.94	1.189	1.95532	1.500	3.830 PER IMP=	65.00
*S Add Sub-basin 310 to upstream flow in pipe										
ADD HYD	RT313UP&310 24& 8	25	.82230	149.03	88.620	2.02070	2.550	.283		
*S Route Sub-basin 310 and upstream flow through 66" pipe for 1000'										
ROUTE MCUNGE	RT310UP	25	26	.82230	148.77	88.578	2.01974	2.600	.283 CCODE =	.2
*S SUB-BASIN 311S										
COMPUTE NM HYD	311.01	-	9	.02920	72.19	3.090	1.98409	1.500	3.863 PER IMP=	66.70
*S Add Sub-basin 311S to upstream flow in pipe										
ADD HYD	RT310UP&311S 26& 9	27	.85150	150.59	91.668	2.01852	2.550	.276		
*S Route Sub-basin 311S and upstream flow through 66" pipe for 150'										
ROUTE MCUNGE	RT311SUP	27	28	.85150	150.59	91.668	2.01852	2.550	.276 CCODE =	.0
*S SUB-BASIN 311N										
COMPUTE NM HYD	311.02	-	10	.05060	109.82	5.979	2.21552	1.550	3.391 PER IMP=	80.90
*S Add Sub-basin 311N to upstream flow in pipe										
ADD HYD	RT311SUP&311 28&10	29	.90210	210.02	97.647	2.02957	1.550	.364		
*S SUB-BASIN 312S										
COMPUTE NM HYD	312.00	-	11	.01270	33.05	1.484	2.19032	1.500	4.066 PER IMP=	79.30
*S Add Sub-basin 312S to upstream flow into the pond										
FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)		RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)			TIME TO PEAK (HOURS)	CFS PER ACRE
COMMAND	HYDROGRAPH IDENTIFICATION								PAGE = 3	PAGE NOTATION
ADD HYD	RT311NUP&312 29&11	30	.91480	239.43	99.1330	2.03180				.409

*S COMPUTE NM HYD SUB-BASIN 8
 8.00 - 31 .01760
 *S Add Sub-basin 8 to upstream flow into the pond
 ADD HYD RT312SUP&8 30&31 32 .93240
 *S ROUTE FLOW THROUGH POND WITH 60" OUTFLOW PIPE
 ROUTE RESERVOIR Pondout 32 41 .93240
 *S Route POND OUTFLOW through 60" pipe for 1350,
 ROUTE MCUNGE RT311NUP 41 33 .93240
 *S***** FROM FORMER BHI REPORT ON LYONS SD_ MODIFIED FOR INCREASED
 *S*** FLOWS

*S***** CALC BASIN 316 FLOW
 COMPUTE NM HYD 316.00 - 1 .03000
 *S***** ROUTE 316 THRU 313N PARADISE*****
 ROUTE MCUNGE RT316 1 2 .03000
 *S***** CALC BASIN 313N FLOW *****
 COMPUTE NM HYD 313N - 3 .07800
 *S** ADD RT316 TO 313N*****
 ADD HYD 313NUP 2& 3 4 .10800
 *S***** CALC BASIN 314 FLOW *****
 COMPUTE NM HYD 314.00 - 5 .08900
 *S*** ADD 313NUP TO 314*****
 ADD HYD AP1-314UP 4& 5 6 .19700
 *S***** CALC BASIN 314.1 FLOW *****
 COMPUTE NM HYD AP2-314.1 - 7 .03600
 *S** ADD 314UP TO 314.1 FOR DISCHARGE INTO POND*****
 ADD HYD AP314.1UP 6& 7 8 .23300
 *S***ROUTE AP314.1UP FLOW THROUGH PARK POND W/ ASSUMED DISCHARGE.
 ROUTE RESERVOIR AP3-RT314.1P 8 9 .23300
 *S***** ROUTE DISCHARGE 'THRU PIPE TO UNSR LYONS *****
 ROUTE MCUNGE 113.40 9 10 .23300
 *S***** CALC BASIN 312 FLOW *****
 COMPUTE NM HYD 312.00 - 11 .20200
 *S*** ADD 113.4 TO 312*****
 ADD HYD AP4-312UP 10&11 12 .43500
 *S***ADD NEW FLOW FROM SOUTH UNSR SD (6/01)
 ADD HYD NewAp4 33&12 35 1 .36740
 *S***** ROUTE DISCHARGE 'THRU PIPE TO ESSEX 84"*****
 ROUTE MCUNGE RT312UP 35 13 1 .36740
 *S***** CALC BASIN 312.1 FLOW *****
 COMPUTE NM HYD AP5-312.1 - 14 .01400
 *S*** ADD RT312UP TO 312.1*****
 ADD HYD AP312.1 13&14 15 1 .38140
 *S***** ROUTE THROUGH PIPE TO MH9 84"*****
 ROUTE MCUNGE RT312.1 15 42 1 .38140
 *S***** ROUTE DISCHARGE 'THRU PIPE TO ALDER 78"*****

COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =
ROUTE MCUNGE	RT312.12	42	16	1.38140	438.48	141.520	1.92088	1.650	.496 CCODE =	4
*S CALABACILLAS WATERSHED***										
COMPUTE NM HYD	101.00 -	17	.05100	103.51	4.959	1.82319	1.550	3.171 PER IMP=	59.00	

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***** CALC BASIN 105 FLOW ****
COMPUTE NM HYD 105.00 - 18 .02100 48.83 2.042 1.82319 1.500 3.633 PER IMP= 59.00
*S*** ADD 101 TO 105*****
ADD HYD 105UP 17&18 19 .07200 146.78 7.001 1.82318 1.550 3.185
*S*** ROUTE 105UP TO LYONS*****
ROUTE MCUNGE RT105UP 19 20 .07200 146.47 6.985 1.81910 1.600 3.179 CCODE = .1
*S*** CALC BASIN 105.1 FLOW ****
COMPUTE NM HYD 105.10 - 21 .00900 20.94 .875 1.82319 1.500 3.635 PER IMP= 59.00
*S*** ADD 105UP TO 105.1*****
ADD HYD 105.1UP 20&21 22 .08100 161.00 7.860 1.81954 1.600 3.106
*S*** CALC BASIN 107 FLOW ****
COMPUTE NM HYD 107.00 - 23 .06700 119.80 6.515 1.82319 1.600 2.794 PER IMP= 59.00
*S*** CALC BASIN 108 FLOW ****
COMPUTE NM HYD 108.00 - 24 .01000 23.26 .972 1.82319 1.500 3.635 PER IMP= 59.00
*S*** ADD 107 TO 108*****
ADD HYD 108UP 23&24 25 .07700 137.35 7.487 1.82318 1.550 2.787
*S*** ADD RT312.1 TO AP108*****
ADD HYD AP6-AP108UP 16&25 26 1.45840 560.91 149.007 1.91572 1.650 .601
*S*** CALC BASIN 108.1 FLOW ****
COMPUTE NM HYD 108.10 - 27 .01100 25.59 1.070 1.82319 1.500 3.634 PER IMP= 59.00
*S*** ADD 108.1 TO 105.1UP*****
ADD HYD AP7-AP108.1U 27&22 28 .09200 178.76 8.930 1.81997 1.600 3.036
*S*** ROUTE DISCHARGE THRU PIPE TO IRVING 78" ****
ROUTE MCUNGE RT312.1 26 29 1.45840 560.91 149.007 1.91572 1.650 .601 CCODE = .0
*S*** ADD RT312.1 TO 108.1UP*****
ADD HYD AP108.1UP 29&28 30 1.55040 728.51 157.937 1.91004 1.650 .734
FINISH

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AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
INPUT FILE = P:\00289\hydro\PMDam\Pmd102.HYD

RUN DATE (MON/DAY/YR) = 07/23/2003
USER NO. = AHYMO-S-9702c1BohanHu-AH

* SUMMARY
 * START
 * RAINFALL TYPE= 2
 * SEDIMENT BULK
 * S***** ANALYSIS FOR LAS VENTANAS SUBDIVISION DRAINAGE MASTER PLAN *****
 * S* TWO MAIN SYSTEMS CONVEY FLOWS TO THE LARGE POND IN BASIN 316. THIS
 * S* POND IS CALLED "LAS VENTANAS DRAINAGE FACILITY NO. 1" (LVDF NO. 1).
 * S* THE TWO MAIN SYSTEMS CONSIST OF ONE IN THE NORTH AND ONE IN THE SOUTH.
 * S* PART OF THE SUBDIVISION. NORTH IS THE "WEST BRANCH CALABACILLAS"
 * S* DIVERSION SYSTEM", AND SOUTH IS THE "NORTH BRANCH PIEDRAS MARCADAS"
 * S* SYSTEM".
 * S***** W BRANCH CALABACILLAS DIVERSION SYSTEM FOR LAS VENTANAS *****
 * S* MAIN CHANNEL IS "WEST BRANCH CALABACILLAS DIVERSION CHANNEL" *****
 * S*
 * S***** CALC BASIN 502 FLOW *****
 * S* COMPUTE NM HYD 502.00 - 1 .03400 PIPE (REACH 1)*****
 * S***** ROUTE DISCHARGE THRU BASIN 503W 36" PIPE (REACH 1)*****
 ROUTE 503W.1 1 2 .03400 70.85 3.148 1.73603 1.550 3.256
 * S***** ROUTE 502 FLOW THROUGH POND IN NEIGHBORHOOD PARK AT W SIDE OF 503W *****
 ROUTE RESERVOIR 503W.2 2 3 .03400 13.24 3.148 1.73595 2.100 .608 AC-FT= 1.647
 * S***** ROUTE DISCHARGE THRU 36" PIPE IN BASIN 503W (REACH 2) *****
 ROUTE 503W.3 3 2 .03400 13.24 3.148 1.73594 2.100 .608
 * S***** CALC BASIN 503W FLOW *****
 * S* COMPUTE NM HYD 503W - 1 .14100 218.31 11.614 1.54445 1.600 2.419 PER IMP= 46.00
 * S* DIVIDE 503W FLOWS INTO OVERLAND & PIPE FLOWS (REACH 4) *****
 * S* 100 CFS TO 42" PIPE IN RAINBOW (REACH 4) *****
 DIVIDE HYD 503M.1 1 6 .11168 100.00 9.199 1.54445 1.450 1.399
 503M.2 and 4 .02932 118.31 2.415 1.54445 1.600 6.304
 * S***** ROUTE RAINBOW PIPE FLOWS SOUTH TO RAINBOW & LOOP RD INTERSECTION*****
 ROUTE 503M.11 6 7 .11168 103.68 9.199 1.54445 1.500 1.451
 * S***** ROUTE OVERLAND FLOWS SOUTH ON RAINBOW BLVD *****
 ROUTE 503M.21 4 8 .02932 117.74 2.416 1.54471 1.600 6.274
 * S*** ADD 503W OVERLAND AND PIPE FLOWS AT RAINBOW & LOOP RD*****
 ADD HYD 503W.5 7 & 8 .14100 218.17 11.615 1.54450 1.600 2.418
 * S*** ADD 503W FLOWS TO ROUTED FLOWS FROM 503W POND *****
 ADD HYD 503W.6 2 & 9 3 .17500 228.34 14.762 1.58169 1.600 2.039
 * S***** CALC BASIN 504E FLOW *****
 * S* COMPUTE NM HYD 504E - 1 .07400 102.64 6.095 1.54445 1.650 2.167 PER IMP= 46.00
 * S* DIVIDE 504E FLOWS; (LOWER PART OF 504E IS ADDED LATER AT PARK) *****
 DIVIDE HYD 504E.1 1 2 .03700 51.32 3.048 1.54444 1.650 2.167
 504E.2 and 5 .03700 51.32 3.048 1.54444 1.650 2.167
 * S** ADD UPPER PART OF BASIN 504E TO ROUTED FLOWS FROM 503W POND *****
 ADD HYD 503W.7 3 & 5 4 .21200 278.35 17.810 1.57519 1.600 2.051
 * S* DIVIDE COMBINED FLOWS INTO OVERLAND AND PIPE FLOWS *****
 DIVIDE HYD 503W.71 4 7 .19523 185.00 16.401 1.57519 1.550 1.481
 503W.72 and 8 .01677 93.35 1.409 1.57519 1.600 8.697
 * S* DIVIDE FLOWS IN 5A" PIPE (REACH 3) TO W BRANCH CALABACILLAS DIV CHAN ****

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	
ROUTE	503M.4	7	3	.19523	184.99	16.401	1.57519	1.800	1.481	2	
ROUTE	503M.41	8	9	.01677	71.91	1.409	1.57565	1.700	6.699		
ROUTE	503M.42	9 & 3	10	.21200	256.77	17.811	1.57522	1.700	1.892		
S	***** CALC BASIN 503M FLOW *****										
ROUTE	503M.4	7	3	.19523	184.99	16.401	1.57519	1.800	1.481		
ROUTE	503M.41	8	9	.01677	71.91	1.409	1.57565	1.700	6.699		
ROUTE	503M.42	9 & 3	10	.21200	256.77	17.811	1.57522	1.700	1.892		
S	***** COMPUTE NM HYD *****										
ROUTE	503M.3	1	7	.07200	91.01	5.931	1.54445	1.700	1.975 PER IMP=	46.00	
ROUTE	503M.5	10 & 7	8	.28400	34.8-14	23.741	1.56742	1.700	1.915		
ROUTE	503M.6	8	7	.28400	33.8-28	23.741	1.56742	1.750	1.861		
ROUTE	503M.7	2 & 7	5	.32100	38.1-74	26.789	1.56477	1.750	1.858		
ROUTE	316NW	-	1	.05500	113.32	4.624	1.57621	1.500	3.219 PER IMP=	50.00	
ROUTE	316NW.1	5 & 1	2	.37600	431.65	31.412	1.56644	1.700	1.794		
ROUTE	316NW.2	2	3	.37600	427.05	31.412	1.56644	1.750	1.775		
ROUTE	316NE	-	1	.04000	76.70	3.230	1.51399	1.500	2.996 PER IMP=	47.00	
ROUTE	316NE.1	3 & 1	23	.41600	457.73	34.642	1.56139	1.750	1.719		
S	***** COMPUTE NM HYD *****										
ROUTE	316NE.1	3 & 1	23	.41600	457.73	34.642	1.56139	1.750	1.719		
S	***** SUM IS TOTAL OF FLOWS FROM W BR CALABACILLAS DIVERSION SYSTEM *****										
ROUTE	316NE.1	3 & 1	23	.41600	457.73	34.642	1.56139	1.750	1.719		
S	***** COMPUTE NM HYD *****										
ROUTE	503E.1	-	1	.08000	112.72	6.590	1.54445	1.650	2.202 PER IMP=	46.00	
S	***** COMPUTE NM HYD *****										
ROUTE	504W.1	1	2	.27300	421.40	25.276	1.73601	1.600	2.412 PER IMP=	59.00	
ROUTE	504W.2	1 & 2	5	.31800	482.42	28.983	1.70890	1.600	2.370		
ROUTE	504W.3	5	6	.31800	478.07	28.983	1.70891	1.650	2.349		
S	***** COMPUTE NM HYD *****										
ROUTE	318A	-	1	.04500	93.13	3.707	1.54445	1.500	3.234 PER IMP=	46.00	
ROUTE	318A	-	1	.04500	93.13	3.707	1.54445	1.500	3.234 PER IMP=	46.00	
S	***** COMPUTE NM HYD *****										
ROUTE	318A	-	1	.04500	93.43	3.981	1.73601	1.500	3.395 PER IMP=	59.00	
S	***** ROUTE 318A THRU 36" PIPE IN 318BW (REACH 5) *****										
S	***** ROUTE 318A DIVE FLOWS EAST TO "TRIB A" CHAN *****										

COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION
ROUTE	318BW.1	1	4	.04300	91.05	3.981	1.73602	1.500	3.309	
*S***** ADD	318A TO "TRIB A"	*	*	*****						
ADD HYD	318BW.2	4 & 6	3	.36100	547.85	32.964	1.71213	1.600	2.371	
*S***** ROUTE	THRU "TRIB A"	CHAN IN	318BW	*****						
ROUTE	318BW.3	3	2	.36100	543.61	32.964	1.71213	1.650	2.353	
*S***** CALC BASIN	318BW FLOW	*****	*****	*****						
COMPUTE NM HYD	318BW	-	1	.12200	248.67	11.296	1.73601	1.500	3.185 PER IMP=	59.00
*S***** ADD	318BW TO ROUTED 501/504W/318A IN "TRIB A"	*****	*****	*****						
ADD HYD	318BW.4	2& 1	3	.48300	739.23	44.260	1.71816	1.600	2.391	
*S***** CALC BASIN	319A FLOW	*****	*****	*****						
COMPUTE NM HYD	319A	-	1	.57200	935.79	52.960	1.73601	1.600	2.556 PER IMP=	59.00
*S***** ROUTE	319A DISCHARGE EAST THRU "TRIB B"	CHAN IN	319B	*****						
ROUTE	319B.1	1	2	.57200	936.29	52.960	1.73601	1.600	2.558	
*S***** CALC BASIN	319B FLOW	*****	*****	*****						
COMPUTE NM HYD	319B	-	1	.02300	48.22	1.959	1.59702	1.500	3.276 PER IMP=	50.00
*S***** ADD	319A TO 319B "TRIB B" CHAN FLOWS	*****	*****	*****						
ADD HYD	319B.2	1& 2	4	.59500	969.97	54.919	1.73064	1.600	2.547	
*S***** ROUTE	COMBINED 319A+B DISCHARGE IN "TRIB B"	IN	318BW	*****						
ROUTE	318BW.5	4	5	.59500	970.10	54.919	1.73064	1.600	2.548	
*S***** ADD	"TRIB A" TO "TRIB B" FLOWS AT WELL SITE PARK	*****	*****	*****						
ADD HYD	WELLSITE 3 & 5	4	1	.07800	1709.33	99.179	1.72505	1.600	2.478	
*S***** ROUTE	THRU 318BE; "N BRANCH PIEDRAS MARGADAS CHANNEL"	*****	*****	*****						
ROUTE	318BE.1	4	3	1.07800	1693.32	99.179	1.72505	1.600	2.454	
*S***** CALC BASIN	318BE FLOW	*****	*****	*****						
COMPUTE NM HYD	318BE	-	1	.14800	218.05	12.771	1.61791	1.600	2.302 PER IMP=	51.00
*S***** ADD	318BE TO N BRANCH PIEDRAS MARC CHAN	*****	*****	*****						
ADD HYD	318BE.2	3 & 1	4	1.22600	1911.37	111.950	1.71212	1.600	2.436	
*S***** CALC BASIN	317B	*****	*****	*****						
COMPUTE NM HYD	317B	-	1	.13400	215.23	11.878	1.66202	1.600	2.510 PER IMP=	54.00
*S***** ADD	317B TO CHAN FLOWS (NOW INCLUDES 501/504W/318A+B/319A+B)	*****	*****	*****						
ADD HYD	318BE.3	4 & 1	2	1.36000	2126.60	123.827	1.70718	1.600	2.443	
*S***** ROUTE	COMBINED FLOWS EAST IN N BRANCH PIEDRAS MARC CHAN	*****	*****	*****						
ROUTE	318BE.4	2	13	1.36000	2129.57	123.827	1.70718	1.650	2.447	
*S***** CALC BASIN	601	*****	*****	*****						
COMPUTE NM HYD	601.00	-	1	.02000	43.77	1.852	1.73601	1.500	3.419 PER IMP=	59.00
*S***** ROUTE	601 FLOWS THRU 602, OVERLAND DOWN PASSEONIRTE	*****	*****	*****						
ROUTE	602.1	2	0.2000	.34 .46	1.852	1.73604	1.550	2.692		
*S***** CALC BASIN	602	*****	*****	*****						
COMPUTE NM HYD	602.00	-	1	.06400	100.72	5.825	1.70653	1.600	2.459 PER IMP=	57.00
*S***** ADD	602 FLOW TO 601 FLOWS	*****	*****	*****						
ADD HYD	602.20	2 & 1	4	.08400	134.94	7.677	1.71354	1.600	2.510	
*S***** ROUTE	601/602 FLOWS OVERLAND DOWN PDN	*****	*****	*****						
ROUTE	602.30	4	5	.08400	109.23	7.677	1.71355	1.700	2.032	
*S***** CALC BASIN	317A	*****	*****	*****						
COMPUTE NM HYD	317A	-	20	.01700	37.20	1.574	1.73601	1.500	3.419 PER IMP=	59.00
S	FLOWS FROM BASIN 317A GO EAST, AND DO NOT ENTER LAS VENTANAS.	*****	*****	*****						
S	DATED 7/20/95.	*****	*****	*****						
ROUTE	316SW.1	5	12	.08400	90.82	7.677	1.71355	1.850	1.689	
*S*** ADD OVERLAND FLOW TO N BRANCH PIEDRAS MARCADAIS CHAN FLOWS	*****	*****	*****	*****						
ADD HYD	316SW.2	13&12	4	1.44400	2179.07	131.504	1.70755	1.650	2.358	
*S***** CALC BASIN	316SW	*****	*****	*****						

COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 6 NOTATION
***** ADD 317A TO 315B AND 315W									
ADD HYD	315.20	20& 1	19	.19700	435.38	18.322	1.74381	1.500	3.453
ROUTE	116.00	19	2	.19700	395.88	18.322	1.74381	1.550	3.140
ROUTE	116.20	2& 3	1	.37700	756.55	34.987	1.74007	1.500	3.136
ROUTE	116.00	1	2	.37700	763.83	34.987	1.74007	1.550	3.166
ROUTE	116.20	2& 3	1	.42500	856.22	39.431	1.73961	1.550	3.148
ROUTE	116.00	1	2	.42500	869.26	39.431	1.73961	1.550	3.196
ROUTE	115.01	1	3	.18000	359.84	16.665	1.73598	1.500	3.445 PER IMP= 59.1
ROUTE	115.01	3	4	.04800	105.97	4.444	1.73598	1.500	3.450 PER IMP= 59.1
ROUTE	109.00	4	5	.04800	106.38	4.444	1.73599	1.500	3.463
ROUTE	115.01	5	6	.04800	101.38	4.444	1.73599	1.550	3.300
ROUTE	115.01	8	9	.26300	534.96	24.350	1.73598	1.550	3.178
ROUTE	116.20	9& 1	4	.30800	621.59	28.516	1.73598	1.550	3.153
ROUTE	116.00	5	2	.83650	1556.35	75.866	1.70052	1.550	2.907
ROUTE	116.30	2& 4	5	.73300	1490.85	67.948	1.73809	1.550	3.178
ROUTE	-	20		.10350	121.70	7.919	1.43452	1.700	1.837 PER IMP= 40.0
ROUTE	116.31	5&20	5	.83650	1576.10	75.866	1.70052	1.550	2.944
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757
***** ADD INTERCEPTOR FLOW TO THE PDN CHANNEL FLOW***									
ADD HYD	SHENO1W								
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757
***** ROUTE THIS FLOW THRU SHENO1W TO FLOW FROM 302W									
ROUTE	116.00	5	2	.83650	1556.35	75.866	1.70052	1.550	2.907
ROUTE	116.30	2& 4	5	.08900	76.85	2.679	.56450	1.550	1.349 PER IMP=
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757
***** ROUTE THIS FLOW AT CULVERT AT PDN IN R302*****									
ROUTE	116.00	5	2	.83650	1556.35	75.866	1.70052	1.550	2.907
ROUTE	116.30	2& 4	5	.08900	76.85	2.679	.56450	1.550	1.349 PER IMP=
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757
***** REMOVE POND PER AMAFCA INSTRUCTION									
ROUTE	116.00	5	2	.83650	1556.35	75.866	1.70052	1.550	2.907
ROUTE	116.30	2& 4	5	.08900	76.85	2.679	.56450	1.550	1.349 PER IMP=
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757
***** ROUTE THIS FLOW AT CULVERT AT PDN IN R302*****									
ROUTE	116.00	5	2	.83650	1556.35	75.866	1.70052	1.550	2.907
ROUTE	116.30	2& 4	5	.08900	76.85	2.679	.56450	1.550	1.349 PER IMP=
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757
***** ADD OUTFLOW FROM SHENO1W TO FLOW FROM 302W									
ROUTE	116.00	5	2	.83650	1556.35	75.866	1.70052	1.550	2.907
ROUTE	116.30	2& 4	5	.08900	76.85	2.679	.56450	1.550	1.349 PER IMP=
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757
***** ROUTE THIS FLOW THRU 302E IN PDN CHANNEL*****									
ROUTE	116.00	5	2	.83650	1556.35	75.866	1.70052	1.550	2.907
ROUTE	116.30	2& 4	5	.08900	76.85	2.679	.56450	1.550	1.349 PER IMP=
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757
***** COMPUTE NM HYD 302E FLOW TO PDN CHANNEL @ EAST END OF 302E*****									
ROUTE	116.00	5	2	.83650	1556.35	75.866	1.70052	1.550	2.907
ROUTE	116.30	2& 4	5	.08900	76.85	2.679	.56450	1.550	1.349 PER IMP=
ROUTE	116.20	2& 1	19	.92550	1633.20	78.546	1.59128	1.550	2.757

COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	DISCHARGE (CFS)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = NOTATION
*S***** * * * * * CALCULATE BASIN 313S *											
COMPUTE NM HYD	313.00	-	3	.08900	173.55	8.240	1.73598	1.550	3.047 PER IMP=	59.1	
*S***** * * * * * ROUTE B313S FLOW	ROUTE 113.40	3	12	.08900	175.14	8.240	1.73599	1.550	3.047 PER IMP=	59.1	
*S** ID12 IS DISCHARGE THRU PROPOSED CULVERT TWO AND HEAD OF P.N. PARK CAYNON**											
*S***** * * * * * CALCULATE BASIN 310 *** * * * * *											
COMPUTE NM HYD	310.00	-	1	.01500	33.13	1.389	1.73598	1.500	3.451 PER IMP=	59.1	
*S***** * * * * * ROUTE COMBINED (11/20/02:NOW ONLY BASIN 310) FLOWS THRU CULVERT ONE	ROUTE 110.00	1	6	.01500	33.27	1.389	1.73602	1.500	3.466		
*S***** * * * * * TAKE DISCHARGE FROM CULVERT 2 AND ROUTE THRU 308,2 SECT. *** * * * * *	ROUTE 108.00	12	3	.08900	161.64	8.240	1.73599	1.600	2.838		
*S***** * * * * * CALCULATE BASIN 308 *** * * * * *	ROUTE 308.00	-	4	.03600	47.78	1.746	.90934	1.500	2.074 PER IMP=	22.1	
*S***** * * * * * ADD ROUTE FROM 313 AND 308 *** * * * * *	ADD HYD	108.10	3& 4	1	.12500	201.80	9.986	1.49791	1.550	2.523	
*S***** * * * * * ROUTE THIS FLOW PART WAY DOWN MAIN BRANCH *** * * * * *	ROUTE 104.10	1	3	.12500	150.67	9.986	1.49791	1.650	1.883		
*S***** * * * * * CALCULATE BASIN 307 *** * * * * *	COMPUTE NM HYD	307.00	-	4	.06500	131.80	5.447	1.57132	1.500	3.168 PER IMP=	52.0
*S***** * * * * * ROUTE CULVERT 1 DISCHARGE THRU 307 *** * * * * *	ROUTE 107.00	6	10	.01500	27.62	1.389	1.73601	1.550	2.877		
*S***** * * * * * ADD 307/310/311R INTO PLAYA IN 307 *** * * * * *	ADD HYD	307.40	4&10	9	.08000	155.17	6.836	1.60219	1.500	3.031	
*S***** * * * * * ROUTE THRU PLAYA IN 307 *** * * * * *	ROUTE 507.20	9	4	.08000	104.75	6.176	1.44758	1.650	2.046 AC-FT=	2.222	
*S***** * * * * * ROUTE OUTFLOW TO PM MAIN BRANCH *** * * * * *	ROUTE 104.40	4	5	.08000	72.68	6.175	1.44733	1.750	1.420		
*S***** * * * * * ADD (307+308) AT PM POINT *** * * * * *	ADD HYD	104.20	3& 5	4	.20500	218.85	16.161	1.47817	1.700	1.668	
*S***** * * * * * CALCULATE BASIN 306 *** * * * * *	COMPUTE NM HYD	306.00	-	3	.03100	68.49	2.873	1.73776	1.500	3.452 PER IMP=	59.2
*S***** * * * * * ROUTE THRU PLAYA IN BASIN 306 *** * * * * *	ROUTE RESERVOIR	506.00	3	1	.03100	16.96	2.216	1.34028	1.900	.855 AC-FT=	1.477
*S***** * * * * * ROUTE POND DISCHARGE THRU 305 *** * * * * *	ROUTE 105.00	1	5	.03100	16.48	2.212	1.33808	2.050	.831		
*S***** * * * * * CALCULATE BASIN 305 *** * * * * *	COMPUTE NM HYD	305.00	-	3	.02700	47.32	1.891	1.31316	1.500	2.739 PER IMP=	40.5
*S***** * * * * * ROUTE 305T TO 307-308 ROUTES AT MAIN BRANCH PART WAY DOWN 304*** * * * * *	ADD HYD	105.10	5& 3	1	.05800	47.39	4.103	1.32648	1.500	1.277	
*S***** * * * * * ROUTE REMAINING 700, TO END OF BASIN 304 *** * * * * *	ROUTE 104.60	1	5	.05800	45.24	4.103	1.32628	1.550	1.219		
*S***** * * * * * CALCULATE BASIN 304 *** * * * * *	COMPUTE NM HYD	304.00	-	3	.18500	236.35	9.600	.97296	1.500	1.996 PER IMP=	25.0
*S***** * * * * * ADD 304 TO ALL FLOWS @ END OF 304 TO GET TOTAL FLOW THERE *** * * * * *	ADD HYD	104.11	2& 3	1	.26300	250.19	20.264	1.44468	1.700	1.486	
*S***** * * * * * ROUTE 103.00	ROUTE 103.00	1	2	.44800	389.85	29.863	1.24984	1.600	1.360		
*S***** * * * * * CALCULATE BASIN 303 *** * * * * *	COMPUTE NM HYD	303.00	-	3	.16500	97.30	4.968	.56450	1.650	.921 PER IMP=	6.2

AHYMO PROGRAM SUMMARY TABLE (AHYMO 97) -
INPUT FILE = P:\00289\hydro\PMdAm\PMd103.HYM

- VERSION: 1997.02C RUN DATE (MON/DAY/YR) =07/23/2003
USER NO.= AHYMO-S-9702c1BohanHu-AH

*SUMMARY
START
RAINFALL TYPE= 2
SEDIMENT BULK
S

*S***** ANALYSIS FOR LAS VENTANAS SUBDIVISION DRAINAGE MASTER PLAN *****
S
S TWO MAIN SYSTEMS CONVEY FLOWS TO THE LARGE POND IN BASIN 316. THIS *
S POND IS CALLED "LAS VENTANAS DRAINAGE FACILITY NO. 1" (LVDF NO. 1). *
S THE TWO MAIN SYSTEMS CONSIST OF ONE IN THE NORTH AND ONE IN THE SOUTH *
S PART OF THE SUBDIVISION. NORTH IS THE "WEST BRANCH CALABACILLAS" *
S DIVERSION SYSTEM", AND SOUTH IS THE "NORTH BRANCH PIEDRAS MARCADAS" *
S SYSTEM". *
*S***** W BRANCH CALABACILLAS DIVERSION SYSTEM FOR LAS VENTANAS *****
S MAIN CHANNEL IS "WEST BRANCH CALABACILLAS DIVERSION CHANNEL" *****
S

*S***** CALC BASIN 502 FLOW *****
COMPUTE NM HYD 502.00 - 1 .03400 74.39 3.148 1.73601 1.500 3.419 PER IMP= 59.00
*S***** ROUTE DISCHARGE THRU BASIN 503W 36" PIPE (REACH 1)*****
ROUTE 503W.1 1 2 .03400 70.85 3.148 1.73603 1.550 3.256
*S***ROUTE 502 FLOW THROUGH POND IN NEIGHBORHOOD PARK AT W SIDE OF 503W *****
ROUTE RESERVOIR 503W.2 2 3 .03400 13.24 3.148 1.73595 2.100 .608 AC-FT= 1.647
*S***** ROUTE DISCHARGE THRU 36" PIPE IN BASIN 503W (REACH 2) *****
ROUTE 503W.3 3 2 .03400 13.24 3.148 1.73594 2.100 .608
*S***** CALC BASIN 503W FLOW *****
COMPUTE NM HYD 503W - 1 -14100 218.31 11.614 1.54445 1.600 2.419 PER IMP= 46.00
S DIVIDE 503W FLOWS INTO OVERLAND & PIPE FLOWS *****
S 100 CFS TO 42" PIPE IN RAINBOW (REACH 4) *****
DIVIDE HYD 503M.1 1 6 .11168 100.00 9.199 1.54445 1.450 1.399
503M.2 and 4 .02932 118.31 2.415 1.54445 1.600 6.304
*S*** ROUTE RAINBOW PIPE FLOWS SOUTH TO RAINBOW & LOOP RD INTERSECTION*****
ROUTE 503M.11 6 7 .11168 103.68 9.199 1.54445 1.500 1.451
*S***ROUTE OVERLAND FLOWS SOUTH ON RAINBOW BLVD ****
ROUTE 503M.21 4 8 .02932 1117.74 2.416 1.54471 1.600 6.274
*S*** ADD 503W OVERLAND AND PIPE FLOWS AT RAINBOW & LOOP RD*****
ADD HYD 503W.5 7& 8 9 .14100 218.17 11.615 1.54450 1.600 2.418
*S*** ADD 503W FLOWS TO ROUTED FLOWS FROM 503W POND *****
ADD HYD 503W.6 2& 9 3 .17500 228.34 14.762 1.58169 1.600 2.039
*S***** CALC BASIN 504E FLOW *****
COMPUTE NM HYD 504E - 1 .07400 102.64 6.095 1.54445 1.650 2.167 PER IMP= 46.00
S DIVIDE 504E FLOWS; (LOWER PART OF 504E IS ADDED LATER AT PARK) *****
DIVIDE HYD 504E.1 1 2 .03700 51.32 3.048 1.54444 1.650 2.167
504E.2 and 5 .03700 51.32 3.048 1.54444 1.650 2.167
*S** ADD UPPER PART OF BASIN 504E TO ROUTED FLOWS FROM 503W POND *****
ADD HYD 503W.7 3& 5 4 .21200 278.35 17.810 1.57519 1.600 2.051
S DIVIDE COMBINED FLOWS INTO OVERLAND AND PIPE FLOWS *****
DIVIDE HYD 503W.71 4 7 .19523 185.00 16.401 1.57519 1.550 1.481
503W.72 and 8 .01677 93.35 1.409 1.57519 1.600 8.697
S ROUTE PIPE FLOWS IN 54" PIPE (REACH 3) TO W BRANCH CALABACILLAS DIV CHAN ***

*S***** ADD 318A TO "TRIB A" **** .04300

ADD HYD 318BW.2 4& 6 .36100

*S***** ROUTE THRU "TRIB A" CHAN IN 318BW *****

ROUTE 318BW.3 3 2 .36100

*S***** CALC BASIN 318BW FLOW *****

COMPUTE NM HYD 318BW - 1 .12200

*S***** ADD 318BW TO ROUTED 501/504W/318A IN "TRIB A" *****

ADD HYD 318BW.4 2& 1 .48300

*S***** CALC BASIN 319A FLOW *****

COMPUTE NM HYD 319A - 1 .57200

*S***** ROUTE 319A DISCHARGE EAST THRU "TRIB B" CHAN IN 319B *****

ROUTE 319B.1 1 2 .57200

*S***** CALC BASIN 319B FLOW *****

COMPUTE NM HYD 319B - 1 .02300

*S***** ADD 319A TO 319B "TRIB B" CHAN FLOWS *****

ADD HYD 319B.2 1& 2 .4 .59500

*S***** ROUTE COMBINED 319A+B DISCHARGE IN "TRIB B" IN 318BW *****

ROUTE 318BW.5 4 5 .59500

*S***** ADD "TRIB A" TO "TRIB B" FLOWS AT WELL SITE PARK *****

ADD HYD WELLSITE 3& 5 4 1.07800

*S***** ROUTE THRU 318BE; "N BRANCH PIEDRAS MARCADAS CHANNEL"

ROUTE 318BE.1 4 3 1.07800

*S***** CALC BASIN 318BE FLOW *****

COMPUTE NM HYD 318BE - 1 .14800

*S***** ADD 318BE TO N BRANCH PIEDRAS MARC CHAN *****

ADD HYD 318BE.2 3& 1 4 1.22600

*S***** CALC BASIN 317B *****

COMPUTE NM HYD 317B - 1 .13400

*S***** ADD 317B TO CHAN FLOWS (NOW INCLUDES 501/504W/318A+B/319A+B)

ADD HYD 318BE.3 4& 1 2 1.36000

*S***** ROUTE COMBINED FLOWS EAST IN N BRANCH FIEDRAS MARC CHAN *****

ROUTE 318BE.4 2 13 1.36000

*S***** CALC BASIN 601 *****

COMPUTE NM HYD 601.00 - 1 .02000

*S***** ROUTE 601 FLOWS THRU 602, OVERLAND DOWN PASEOdelNORTE

ROUTE 602.10 1 2 .02000

*S***** CALC BASIN 602 *****

COMPUTE NM HYD 602.00 - 1 .06400

*S***** ROUTE 602 FLOW TO 601 FLOWS *****

ADD HYD 602.20 2& 1 4 .08400

*S***** ROUTE 601/602 FLOWS OVERLAND DOWN PDN

ROUTE 602.30 4 5 .08400

*S***** CALC BASIN 317A *****

COMPUTE NM HYD 317A - 20 .01700

*S***** FLOWS FROM BASIN 317A GO EAST, AND DO NOT ENTER LAS VENTANAS.

*S***** DATED 7/20/95.

ROUTE 316SW.1 5 12 .08400

*S***** ADD OVERLAND FLOW TO N BRANCH PIEDRAS MARCADAS CHAN FLOWS *****

ADD HYD 316SW.2 13&12 4 1.44400

*S***** CALC BASIN 316SW *****

PAGE = 3

COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 5 NOTATION
ADD HYD ROUTE	320.20 2& 5 3 PIPE (REACH 8) NORTH TO IRVING BLVD ***				2.24580	107.29	172.142	1.43720	.075
*S***** ROUTE NM HYD	505.10 3 2.24580 BASIN 505 *****					107.28	171.995	1.43597	.075
*S***** ADD 505 FLOW TO FLOWS *****	- 1 .02200					35.77	1.225	1.04368	2.540 PER IMP= 20.00
*S*** FLOW TOWARDS CALABACILLAS AT NE COR LAS VENTANAS DRAINAGE									
ADD HYD	505.20 1& 2 15 2.26780					108.80	173.219	1.43216	.075
*S*** END OF LAS VENTANAS DRAINAGE ANALYSIS									
COMPUTE NM HYD	314A - 3 .08600					143.70	7.962	1.73598	2.611 PER IMP= 59.10
*S***** GET NORTH PIECE (PANHANDLE) OF 313 INTO SYSTEM TO CALABACILLAS*****									
COMPUTE NM HYD	313.10 - 6 .06500					114.35	6.018	1.73598	2.749 PER IMP= 59.10
*S***** ADD 314A/3116R/313N FLOWS INTO LAST SECTION OF PIPE INTO PARK POND***	113.30 3&22 4 .10930					169.50	8.995	1.54305	2.423
ADD HYD	113.20 4& 6 5 .17430					283.85	15.013	1.61500	2.545
*S***** ROUTE 316R/314A/313N TOTAL INTO LAST SECTION OF PIPE INTO PARK POND***	113.40 5 2 .17430					283.63	15.013	1.61500	1.600
ROUTE									2.543
*S***** CALCULATE BASIN 314.1 *****									
COMPUTE NM HYD	314.10 - 3 .03500					68.88	2.639	1.41366	1.500
*S***** ADD 314.1 AND 314A/316R/313N FOR DISCH. INTO POND*****	113.30 3& 2 4 .20930					341.67	17.652	1.58133	1.550
*S***** ROUTE THRU PARK POND WITH ASSUMED DISCHARGE *****									2.551
*S*** ASSUME 48" DISCHARGE PIPE *****									
ROUTE RESERVOIR	507.20 4 5 .20930					101.94	17.652	1.58133	2.000
*S***** ROUTE POND DISCH. THRU PIPE TO UNSER LYONS*****	113.40 5 2 .20930					101.94	17.652	1.58133	2.000
ROUTE									761
*S***** CALCULATE BASIN 312 *****									
COMPUTE NM HYD	312.00 - 1 .21100					304.64	19.536	1.73598	1.650
*S***** ADD POND DISCH. AND 312 *****	113.30 1& 2 4 .42030					382.97	37.187	1.65896	1.650
ADD HYD									1.424
*S*** CALCULATE BASIN 311N *****									
COMPUTE NM HYD	311N - 1 .04800					105.97	4.444	1.73598	1.500
*S***** CALCULATE BASIN 315NE (PORTION OF 315N THAT IS BOUNDED BY *****)									
S AND "TRACT 6" BOUNDARY AS SHOWN ON MAP IN LYON BLVD SD DMP)	315NE - 40 .03900					86.10	3.611	1.73598	1.500
ROUTE THRU STORM DRAIN TO BASIN 313SA									3.450 PER IMP= 59.10
ROUTE									
*S***** CALCULATE BASIN 313SA (AREA NORTH OF LYON/UNSER) *****	315NER 40 41 .03900					83.50	3.611	1.73600	1.500
COMPUTE NM HYD	313SA - 42 .04700					103.76	4.352	1.73598	1.500
S ADD ROUTED 315NE AND 313SA									3.450 PER IMP= 59.10
ROUTE									
*S***** CALCULATE BASIN 310 *****									
COMPUTE NM HYD	310.00 - 45 .01500					33.13	1.389	1.73598	1.500
S ADD ROUTED 313SA AND 310	313SA310 41&42 43 .08600					187.27	7.962	1.73598	1.500
S ROUTE THRU STORM DRAIN TO BASIN 310	313SAR 43 44 .08600					180.21	7.962	1.73599	1.500
ROUTE									3.274
*S***** CALCULATE BASIN 311S *****									
COMPUTE NM HYD	311S - 48 .04800					105.97	4.444	1.73598	1.500
S ADD ROUTED 310 AND 311S									3.450 PER IMP= 59.10

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 12	NOTATION
COMPUTE NM HYD	103.00	-	2	.05810	128.35	5.385	1.73776	1.500	3.452 PER IMP=	59.20	
*S***** ROUTE	ROUTE	103.10	2	3	0.05810	128.35	5.385	1.73777	1.500	3.452	
*S**>> ADD SHEHANDDOAH BASIN E FLOWS TO BASIN 103 *****	ADD HYD	103.10	3&14	4	.07800						
*S**>> FLOW DOWNSTREAM OF GOLF COURSE IN MIDDLE BEFORE ADDING N. BRANCH	ADD HYD	103.20	15& 4	15	1.78531	2175.21	121.921				
*S**>> TOTAL FLOW DOWNSTREAM OF GOLF COURSE MIDDLE AND NORTH BRANCHES	ADD HYD	103.20	15&16	17	2.71271	3390.24	185.137	1.27965	1.600	1.904	
ROUTE	ROUTE	102.10	17	13	2.71271	3354.39	185.137	1.27965	1.600	1.953	
*S**>> TOTAL FLOW IN MIDDLE BRANCH UPSTREAM OF RANCHO SERENA	*S*>>***** CALCULATE BASIN 102 *****										
COMPUTE NM HYD	RANCHO_01	-	1	.00566	7.49						
ROUTE	NORT&SER	1	4	.00566	6.39						
COMPUTE NM HYD	RANCHO_02	-	2	.00786	8.57						
ADD HYD	RANCHO12	2& 4	1	.01352	14.35						
DIVIDE HYD	SERENO	1	2	.00676	7.18						
ROUTE	BUTTER and	3	.00676	7.18							
ROUTE	SER&LARG	2	23	.00676	6.66						
ROUTE	BUTTER&DAM	3	24	.00676	4.99						
COMPUTE NM HYD	BASIN_102R	-	1	.01107	23.75						
ADD HYD	BUTTERTOT	1&24	55	.01783	26.31						
ROUTE	BASIN_E1	-	1	.00215	4.62						
ADD HYD	SER&LARG	1&23	4	.00891	10.47						
ROUTE	BASIN_F1	-	1	.00807	16.84						
ROUTE	TO_BSN_H	1	3	.00807	16.51						
COMPUTE NM HYD	BASIN_H	-	2	.00192	3.84						
ADD HYD	LARG&DOR	2& 3	1	.00999	20.35						
ROUTE	TO_BSN_G	1	3	.00999	20.41						
COMPUTE NM HYD	BASIN_G	-	2	.00279	6.03						
ADD HYD	LARG&QUI	2& 3	1	.01278	26.00						
ROUTE	TOSERENO	1	3	.01278	26.36						
COMPUTE NM HYD	BASIN_F2	-	2	.00415	9.11						
ADD HYD	LARG&SER	2& 3	1	.01693	34.78						
DIVIDE HYD	PIPE	1	2	.01550	23.00						
ROUTE	STRAT and	3	.00143	11.78							
ROUTE	STORMDRN	2	5	.01550	23.75						
ADD HYD	SER&LARG	4& 3	1	.01034	22.17						
ROUTE	TOCHANNEL	1	4	.01034	22.39						
ADD HYD	CHNLNTOT	4& 5	9	.02584	45.55						
COMPUTE NM HYD	BASIN_B1	-	1	.00340	7.62						
ROUTE	LARG&ENC	1	3	.00340	6.94						
COMPUTE NM HYD	BASIN_B2	-	1	.00408	9.00						
ADD HYD	LARG&ENC	1& 3	5	.00748	15.43						
COMPUTE NM HYD	BASIN_A1	-	1	.00567	12.50						
ROUTE	ALGR&ENC	1	3	.00567	11.48						
COMPUTE NM HYD	BASIN_A2	-	2	.00426	9.15						
ADD HYD	ENCL&ARG	2& 3	4	.00993	19.95						
ADD HYD	A1A2B1B2	4& 5	7	.01741	35.22						
ROUTE	A1A2B1B2	7	4	.01741	35.63						
COMPUTE NM HYD	BASINAS	-	3	.00209	4.37						

ADD HYD ROUTE STORMDRN TOTAL BASINS 3 & 4 7 .01950 39.69 1.719 1.65320 1.533 3.180

COMPUTE NM HYD BASIN_C - 3 .01950 39.75 1.719 1.65322 1.533 3.185

COMPUTE NM HYD BASIN_D - 4 .00046 .82 .027 1.10888 1.500 2.797 PER IMP= 19.00

COMPUTE NM HYD BASIN_I_1 - 11 .00024 .38 .010 1.80017 1.500 2.445 PER IMP= .00

COMPUTE NM HYD BASIN_I_2 - 12 .00045 .98 .036 1.51209 1.500 3.388 PER IMP= 37.00

COMPUTE NM HYD BASIN_I_3 - 12 .00168 3.45 .122 1.36719 1.500 3.209 PER IMP= 27.00

*S***** ADD RANCHO2 BASINS (F-H) INTO CHANNEL AT RANCHO SERENO ***

ADD HYD 102.20 13& 9 14 2.73855 3393.67 186.958

*S***** ADD RANCHO2 BASIN I-2 INTO CHANNEL AT RANCHO SERENO***

ADD HYD 102.20 14&12 13 2.74023 3396.11 187.048

*S***** ADD RANCHO2 BASIN I-1 INTO CHANNEL AT RANCHO SERENO***

ADD HYD 102.30 13&11 97 2.74068 3396.79 187.084

*S***** ADD RANCHO BASINS C, D, DIVIDED FLOW FROM RANCHO12 AND

S STORM DRAIN FLOW FROM BASINS A AND B ASSUME ALL THIS RUNOFF GOES DIRECTLY INTO DAM. ADD IN LATER

ADD HYD 102.40 3& 4 88 .00070 1.20 .037 1.00255 1.500 2.677

ADD HYD 102.50 88&10 98 .02020 40.88 1.756 1.63021 1.533 3.162

ADD HYD 102.60 98&55 99 .03803 66.40 2.967 1.46275 1.533 2.728

S>>> CALCULATE MC BASIN 101.1 *****

COMPUTE NM HYD 101.10 - 95 .17600 388.27 16.312 1.73776 1.500 3.447 PER IMP= 59.20

COMPUTE NM HYD 101.20 - 2 .07025 123.73 5.688 1.51815 1.550 2.752 PER IMP= 44.19

ROUTE 402.10 2 1 .07025 124.15 5.688 1.51816 1.550 2.761

COMPUTE NM HYD 101.30 - 2 .02675 54.99 2.166 1.51815 1.500 3.212 PER IMP= 44.19

*S***** ADD 101.3 to routed flow from 101.2 *****

ADD HYD 101.11 2& 1 1 .09700 173.20 7.854

ROUTE 402.10 1 2 .09700 174.19 7.854

*S***** TOTAL FLOW IN MIDDLE BRANCH DOWNSTREAM OF RANCHO SERENA *****

ADD HYD 101.11 2&97 18 2.83768 3551.33 194.752

ROUTE 102.10 18 19 2.83768 3503.29 194.753

S>>> TOTAL FLOW IN MIDDLE BRANCH UPSTREAM OF RANCHO SERENA

*S***** ID 19 IS TOTAL FLOW INTO DAM from Middle Branch *****

*S***** SOUTH BRANCH *****

*S***** CALCULATE BASIN 404 *****

COMPUTE NM HYD 404.00 - 2 .19500 361.19 14.473 1.39167 1.500 2.894 PER IMP= 44.00

*S***** ROUTE THIS FLOW THRU 404.1 *****

ROUTE 404.01 2 1 .19500 318.67 14.473 1.39167 1.550 2.553

*S***** CALCULATE BASIN 404.1 *****

COMPUTE NM HYD 404.10 - 2 .11500 253.87 10.658

*S***** ADD 404.1 AND 404 ROUTE *****

ADD HYD 404.02 1& 2 3 .31000 540.23 25.132

*S***** ROUTE THIS FLOW THRU 403.3 LARGE CHANNEL*****

ROUTE 403.01 3 1 .31000 542.29 25.132

*S***** ROUTE THIS FLOW THRU 10' CONCRETE CHANNEL *****

COMPUTE NM HYD 403.30 - 2 .03700 81.77 3.426

ROUTE 403.02 2 3 *****

*S***** ADD 403.3R AND TOTAL ROUTE *****

ADD HYD 403.03 3& 1 4 .34700 614.68 28.557

COMPUTE NM HYD 403.20 - 2 .01400 30.95 1.296

*S***** ROUTE THIS FLOW THRU 10' CONCRETE CHANNEL (S.) *****

ROUTE 403.21 2 3 .01400 31.24 1.296

*S***** ADD 403.2R AND TOTAL ROUTE IN LARGE CHANNEL (ID=4) *****

OPTION 1 - TOTAL

ITEM #	SHORT DESCRIPTION	QUANTITY	UNIT	UNIT PRICE	COST
343.132	ART PVMT,R&R,W/M	3000	SY	\$25.00	\$75,000.00
701.200	TRCH, BF, > 60" SWR, 8'-12'	1300	LF	\$46.00	\$59,800.00
701.320	BF MATL, SELECT	149000	CY	\$6.00	\$894,000.00
910.023	54" RCP, III	1400	LF	\$106.00	\$148,400.00
910.027	66" RCP, III	3400	LF	\$135.00	\$459,000.00
910.035	90" RCP, III	530	LF	\$243.00	\$128,790.00
910.037	96" RCP, III	910	LF	\$290.00	\$263,900.00
910.0XX	114" RCP, III	470	LF	\$475.00	\$223,250.00
910.0XX	120" RCP, III	890	LF	\$580.00	\$516,200.00
910.0XX	10' X 9' CBC	760	LF	\$620.00	\$471,200.00
910.0XX	11' X 10' CBC	800	LF	\$680.00	\$544,000.00
910.0XX	11' X 11' CBC	1600	LF	\$710.00	\$1,136,000.00
910.0XX	12' X 12' CBC	3100	LF	\$770.00	\$2,387,000.00
910.105	DRNG LN REM, >48"	910	LF	\$18.00	\$16,380.00
920.210X	MH, TEE TYPE	28	EA	\$5,500.00	\$154,000.00
1020.00X	BASALT ROCK REMOVAL	199570	CY	\$50.00	\$9,978,500.00
<hr/>					
SUB TOTAL					
10% Contingencies					
SUB TOTAL					
22% Soft Costs					
SUB TOTAL					
6% Tax					
ESTIMATED CONSTRUCTION COST					
<hr/>					
\$17,455,000.00					
\$1,746,000.00					
\$19,201,000.00					
\$4,224,000.00					
\$23,425,000.00					
\$1,406,000.00					
<hr/>					
\$24,831,000.00					

OPTION 2 - TOTAL

ITEM #	SHORT DESCRIPTION	QUANTITY	UNIT	UNIT PRICE	COST
343.132	ART PVMT,R&R,W/M	3000	SY	\$25.00	\$75,000.00
701.200	TRCH, BF, > 60" SWR, 8'-12'	400	LF	\$46.00	\$18,400.00
701.320	BF MATL, SELECT	111000	CY	\$6.00	\$666,000.00
910.023	54" RCP, III	1400	LF	\$106.00	\$148,400.00
910.027	66" RCP, III	3400	LF	\$135.00	\$459,000.00
910.030	72" RCP, IV	300	LF	\$185.50	\$55,650.00
910.032	84" RCP, III	150	LF	\$210.00	\$31,500.00
910.033	84" RCP, IV	1700	LF	\$224.00	\$380,800.00
910.035	90" RCP, III	1000	LF	\$242.50	\$242,500.00
910.0XX	114" RCP, III	470	LF	\$475.00	\$223,250.00
910.0XX	120" RCP, III	890	LF	\$580.00	\$516,200.00
910.0XX	10' X 9' CBC	760	LF	\$620.00	\$471,200.00
910.0XX	12' X 12' CBC	1900	LF	\$770.00	\$1,463,000.00
920.210X	MH, TEE TYPE	28	EA	\$5,500.00	\$154,000.00
	65.4 ac-ft DETENTION POND	1	LS	\$838,900.00	\$838,900.00
1020.00X	BASALT ROCK REMOVAL	250000	CY	\$50.00	\$12,500,000.00
=====					
SUB TOTAL \$18,244,000.00					
10% Contingencies \$1,824,000.00					
SUB TOTAL \$20,068,000.00					
22% Soft Costs \$4,415,000.00					
SUB TOTAL \$24,483,000.00					
Land for Pond (9 acres) \$450,000.00					
SUB TOTAL \$24,933,000.00					
6% Tax \$1,496,000.00					
ESTIMATED CONSTRUCTION COST \$26,429,000.00					

OPTION 3 - TOTAL

ITEM #	SHORT DESCRIPTION	QUANTITY	UNIT	UNIT PRICE	COST
343.132	ART PVMT,R&R,W/M	3000	SY	\$25.00	\$75,000.00
701.200	TRCH, BF, > 60" SWR, 8'-12'	400	LF	\$46.00	\$18,400.00
701.320	BF MATL, SELECT	71200	CY	\$6.00	\$427,200.00
910.019	42" RCP, III	2000	LF	\$70.00	\$140,000.00
910.023	54" RCP, III	1800	LF	\$106.00	\$190,800.00
910.025	60" RCP, III	1900	LF	\$121.00	\$229,900.00
910.026	60" RCP, IV	1300	LF	\$134.00	\$174,200.00
910.027	66" RCP, III	3000	LF	\$135.00	\$405,000.00
910.0XX	78" RCP, III	800	LF	\$180.00	\$144,000.00
910.0XX	78" RCP, IV	200	LF	\$197.00	\$39,400.00
910.033	84" RCP, IV	1400	LF	\$224.00	\$313,600.00
920.210X	MH, TEE TYPE	28	EA	\$5,500.00	\$154,000.00
	14.2 ac-ft DETENTION POND	1	LS	\$335,200.00	\$335,200.00
	16 ac-ft DETENTION POND	1	LS	\$360,100.00	\$360,100.00
	18.0 ac-ft DETENTION POND	1	LS	\$386,500.00	\$386,500.00
	27.7 ac-ft DETENTION POND	1	LS	\$500,700.00	\$500,700.00
1020.00X	BASALT ROCK REMOVAL	155000	CY	\$50.00	\$7,750,000.00
=====					
SUB TOTAL					
10% Contingencies					
SUB TOTAL					
22% Soft Costs					
SUB TOTAL					
Land for Ponds (15 acres)					
SUB TOTAL					
6% Tax					
ESTIMATED CONSTRUCTION COST					
\$11,644,000.00					
\$1,164,000.00					
\$12,808,000.00					
\$2,818,000.00					
\$15,626,000.00					
\$750,000.00					
\$16,376,000.00					
\$983,000.00					
\$17,359,000.00					

PARADISE PORTION-ASSUMES NO BASALT EXCAVATION NECESSARY

ITEM #	SHORT DESCRIPTION	QUANTITY	UNIT	UNIT PRICE	COST
910.018	REM&REPL AC PVMT.	15900	SY	\$23.00	\$365,700.00
910.018	33" RCP, IV	500	LF	\$42.50	\$21,250.00
910.022	48" RCP, IV	1000	LF	\$70.00	\$70,000.00
910.028	60" RCP, IV	500	LF	\$107.00	\$53,500.00
910.028	66" RCP, IV	500	LF	\$135.00	\$67,500.00
910.030	72" RCP, IV	1060	LF	\$130.00	\$137,800.00
910.033	84" RCP, IV	500	LF	\$185.00	\$92,500.00
701.110	TRCH, BF, 18-36" SWR, 8-12'	500	LF	\$15.00	\$7,500.00
701.150	TRCH, BF, 42"-60" SWR, <8'	500	LF	\$22.00	\$11,000.00
701.160	TRCH, BF, 42"-60" SWR, 8'-12'	1000	LF	\$25.00	\$25,000.00
701.200	TRCH, BF, > 60" SWR, 8'-12'	2060	LF	\$35.00	\$72,100.00
920.210X	MH, TEE TYPE	3	EA	\$5,500.00	\$16,500.00
920.210	MH, 8'DIA, C or E, 6'-10' D	3	EA	\$4,300.00	\$12,900.00
SUB TOTAL					
SUB TOTAL \$953,000.00					
10% Contingencies \$95,000.00					
SUB TOTAL \$1,048,000.00					
22% Soft Costs \$231,000.00					
SUB TOTAL \$1,279,000.00					
5.8125% Tax \$74,000.00					
ESTIMATED CONSTRUCTION COST \$1,353,000.00					

OPTION 1 - PARADISE AND LYON BOULEVARDS STORM DRAINS ONLY

<u>ITEM #</u>	<u>SHORT DESCRIPTION</u>	<u>QUANTITY</u>	<u>UNIT</u>	<u>UNIT PRICE</u>	<u>COST</u>
343.132	ART PVMT,R&R,W/M	3000	SY	\$25.00	\$75,000.00
701.200	TRCH, BF, > 60" SWR, 8'-12'	1300	LF	\$46.00	\$59,800.00
701.320	BF MATL, SELECT	48895	CY	\$6.00	\$293,370.00
910.037	96" RCP, III	910	LF	\$290.00	\$263,900.00
910.0XX	11' X 10' CBC	800	LF	\$680.00	\$544,000.00
910.0XX	11' X 11' CBC	1600	LF	\$710.00	\$1,136,000.00
910.105	DRNG LN REM, >48"	910	LF	\$18.00	\$16,380.00
920.210X	MH, TEE TYPE	11	EA	\$5,500.00	\$60,500.00
1020.00X	BASALT ROCK REMOVAL	60908	CY	\$50.00	\$3,045,400.00
<hr/>					
SUB TOTAL					
10% Contingencies					
SUB TOTAL					
22% Soft Costs					
SUB TOTAL					
5.8125% Tax					
ESTIMATED CONSTRUCTION COST					
PARADISE PORTION					
TOTAL					

OPTION 2 - PARADISE AND LYON BOULEVARDS STORM DRAINS ONLY

<u>ITEM #</u>	<u>SHORT DESCRIPTION</u>	<u>QUANTITY</u>	<u>UNIT</u>	<u>UNIT PRICE</u>	<u>COST</u>
343.132	ART PVMT,R&R,W/M	3000	SY	\$25.00	\$75,000.00
701.200	TRCH, BF, > 60" SWR, 8'-12'	400	LF	\$46.00	\$18,400.00
701.320	BF MATL, SELECT	43055	CY	\$6.00	\$258,330.00
910.032	84" RCP, III	150	LF	\$210.00	\$31,500.00
910.033	84" RCP, IV	1700	LF	\$224.00	\$380,800.00
910.035	90" RCP, III	500	LF	\$242.50	\$121,250.00
920.210X	MH, TEE TYPE	11	EA	\$5,500.00	\$60,500.00
1020.00X	BASALT ROCK REMOVAL	47109	CY	\$50.00	\$2,355,450.00
<hr/>					
SUB TOTAL					
10% Contingencies					
SUB TOTAL					
22% Soft Costs					
SUB TOTAL					
5.8125% Tax					
ESTIMATED CONSTRUCTION COST					
PARADISE PORTION					
TOTAL					
<hr/>					

OPTION 3 - PARADISE AND LYON BOULEVARDS STORM DRAINS ONLY

ITEM #	SHORT DESCRIPTION	QUANTITY	UNIT	UNIT PRICE	COST
343.132	ART PVMT,R&R,W/M	3000	SY	\$25.00	\$75,000.00
701.200	TRCH, BF, > 60" SWR, 8'-12'	400	LF	\$46.00	\$18,400.00
701.320	BF MATL, SELECT	24007	CY	\$6.00	\$144,042.00
910.0XX	78" RCP, III	800	LF	\$180.00	\$144,000.00
910.0XX	78" RCP, IV	200	LF	\$197.00	\$39,400.00
910.033	84" RCP, IV	1400	LF	\$224.00	\$313,600.00
920.210X	MH, TEE TYPE	11	EA	\$5,500.00	\$60,500.00
1020.00X	BASALT ROCK REMOVAL	27531	CY	\$50.00	\$1,376,550.00
<hr/>					
SUB TOTAL					
10% Contingencies					
SUB TOTAL					
22% Soft Costs					
SUB TOTAL					
5.8125% Tax					
ESTIMATED CONSTRUCTION COST					
PARADISE PORTION					
TOTAL					
<hr/>					

OPTION 4 - PARADISE AND LYON BOULEVARDS STORM DRAINS ONLY

ITEM #	SHORT DESCRIPTION	QUANTITY	UNIT	UNIT PRICE	COST
343.132	ART PVMT,R&R,W/M	3000	SY	\$25.00	\$75,000.00
701.200	TRCH, BF, > 60" SWR, 8'-12'	400	LF	\$46.00	\$18,400.00
701.320	BF MATL, SELECT	24334	CY	\$6.00	\$146,004.00
910.035	90" RCP, III	800	LF	\$242.50	\$194,000.00
910.035	90" RCP, IV	1600	LF	\$260.00	\$416,000.00
920.210X	MH, TEE TYPE	11	EA	\$5,500.00	\$60,500.00
1020.00X	BASALT ROCK REMOVAL	28804	CY	\$50.00	\$1,440,200.00
<hr/>					
SUB TOTAL					
10% Contingencies					
SUB TOTAL					
22% Soft Costs					
SUB TOTAL					
5.8125% Tax					
ESTIMATED CONSTRUCTION COST					
PARADISE PORTION					
TOTAL					
<hr/>					

Design Log

=====
Storm & Sanitary SelectCAD Design Log

Drainage File: P:\00280\Hydro\Design\Control\NewSelectCad\John.sdb

Design File: P:\00280\HYDRO\DESIGN\CONTROL\AMAFCA_BOARD03.DWG

Display Log: P:\00280\Hydro\Design\CONTROL\design.log

Date: Thursday, May 09, 2002 07:35:58 AM
=====

Designing pipe P6

WARNING: Full flow velocity is greater than maximum (10.00)

Results:

Total Flow: 107.0000 cfs

Status:	Fixed	Slope:	0.0097 ft/ft
Pipe Width:	48.0000 in	Pipe Height:	48.0000 in
Depth of Flow:	2.5990 ft	Flow Status:	Partial
Critical Depth:	3.1300 ft	Capacity:	141.4722 cfs
Velocity:	12.3747 ft/s	Flow Regime:	SuperCritical
Froude Number:	1.4497		

Designing manhole MH17

Results:

Total Flow: 107.0000 cfs

Status:	Fixed	Flow From:	Upstream
Chamber Width:	8.0000 ft	Chamber Length:	8.0000 ft

Designing pipe P7

WARNING: Full flow velocity is greater than maximum (10.00)

Results:

Total Flow: 107.0000 cfs

Status:	Fixed	Slope:	0.0307 ft/ft
Pipe Width:	48.0000 in	Pipe Height:	48.0000 in
Depth of Flow:	1.8200 ft	Flow Status:	Partial
Critical Depth:	3.1300 ft	Capacity:	251.7065 cfs
Velocity:	19.2165 ft/s	Flow Regime:	SuperCritical
Froude Number:	2.8666		

Designing pipe P26

Results: Total Flow: 169.8000 cfs Flow From: Injected Storm

Status: Fixed Slope: 0.0050 ft/ft
Pipe Width: 54.0000 in Pipe Height: 54.0000 in
Depth of Flow: 4.5000 ft Flow Status: Full
Critical Depth: 3.7900 ft Capacity: 139.0519 cfs
Velocity: 10.6763 ft/s
Froude Number: 0.0000 Flow Regime: Subcritical

Designing pipe P8

WARNING: Full flow velocity is greater than maximum (10.00)

Results: Total Flow: 276.8000 cfs Flow From: Upstream

Status: Fixed Slope: 0.0095 ft/ft
Pipe Width: 66.0000 in Pipe Height: 66.0000 in
Depth of Flow: 3.8790 ft Flow Status: Partial
Critical Depth: 4.6100 ft Capacity: 327.3063 cfs
Velocity: 15.4511 ft/s
Froude Number: 1.4415 Flow Regime: SuperCritical

Designing manhole MH15

Results: Total Flow: 276.8000 cfs Flow From: Upstream

Status: Fixed Chamber Length: 8.0000 ft
Chamber Width: 8.0000 ft

Designing pipe P9

WARNING: Full flow velocity is greater than maximum (10.00)

Results: Total Flow: 276.8000 cfs Flow From: Upstream

Status: Fixed Slope: 0.0045 ft/ft
Pipe Width: 72.0000 in Pipe Height: 72.0000 in
Depth of Flow: 4.7990 ft Flow Status: Partial
Critical Depth: 4.5500 ft Capacity: 283.1984 cfs
Velocity: 11.4151 ft/s
Froude Number: 0.8956 Flow Regime: Subcritical

Designing pipe P30
WARNING: Full flow velocity is greater than maximum (10.00)

Results: Total Flow: 121.2000 cfs

Status:	Fixed	Slope:	0.0200 ft/ft
Pipe Width:	48.0000 in	Pipe Height:	48.0000 in
Depth of Flow:	2.2250 ft	Flow Status:	Partial
Critical Depth:	3.3100 ft	Capacity:	203.1423 cfs
Velocity:	16.8679 ft/s		
Froude Number:	2.2123	Flow Regime:	SuperCritical

Designing manhole MH14

Results: Total Flow: 398.0000 cfs

Status:	Fixed	Flow From:	Upstream
Chamber Width:	8.0000 ft	Chamber Length:	8.0000 ft

Designing pipe P10
WARNING: Full flow velocity is greater than maximum (10.00)

Results: Total Flow: 398.0000 cfs

Status:	Fixed	Slope:	0.0181 ft/ft
Pipe Width:	72.0000 in	Pipe Height:	72.0000 in
Depth of Flow:	3.6930 ft	Flow Status:	Partial
Critical Depth:	5.3200 ft	Capacity:	569.7723 cfs
Velocity:	21.7918 ft/s		
Froude Number:	2.1724	Flow Regime:	SuperCritical

Designing pipe P0
WARNING: Full flow velocity is greater than maximum (10.CC)

Results: Total Flow: 212.0000 cfs

Status:	Fixed	Slope:	0.0200 ft/ft
Pipe Width:	72.0000 in	Pipe Height:	72.0000 in
Depth of Flow:	2.4650 ft	Flow Status:	Partial
Critical Depth:	3.9800 ft	Capacity:	598.9313 cfs
Velocity:	19.3604 ft/s		
Froude Number:	2.5069	Flow Regime:	SuperCritical

Designing manhole MH13

Results:
Total Flow: 610.0000 cfs

Status: Fixed
Chamber Width: 10.0000 ft
Chamber Length: 10.0000 ft

Designing pipe P11
WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 610.0000 cfs

Status: Fixed
Pipe Width: 90.0000 in
Depth of Flow: 6.1000 ft
Critical Depth: 6.3200 ft
Velocity: 15.8496 ft/s
Froude Number: 1.0890

Flow From: Upstream

Designing pipe P12
WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 610.0000 cfs

Status: Fixed
Pipe Width: 90.0000 in
Depth of Flow: 6.1000 ft
Critical Depth: 6.3200 ft
Velocity: 15.8496 ft/s
Froude Number: 1.0890

Flow From: Upstream

Designing pipe P31
WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 31.4000 cfs

Status: Fixed
Pipe Width: 24.0000 in
Depth of Flow: 1.6060 ft
Critical Depth: 1.8800 ft
Velocity: 11.6062 ft/s
Froude Number: 1.5695

Flow From: Injected Storm

Slope: 0.0064 ft/ft
Pipe Height: 90.0000 in
Flow Status: Partial
Capacity: 614.2974 cfs

Flow Regime: SuperCritical

Slope: 0.0064 ft/ft
Pipe Height: 90.0000 in
Flow Status: Partial
Capacity: 614.2974 cfs

Flow Regime: SuperCritical

Designing pipe P13

WARNING: Full flow velocity is greater than maximum (10.00)

Results:	Total Flow:	641.4000 cfs	Flow From:	Upstream
Status:	Fixed	Slope:	0.0064 ft/ft	
Pipe Width:	90.0000 in	Pipe Height:	90.0000 in	
Depth of Flow:	6.4960 ft	Flow Status:	Partial	
Critical Depth:	6.4500 ft	Capacity:	614.2974 cfs	
Velocity:	15.7741 ft/s	Flow Regime:	Critical	
Froude Number:	0.9857			

Designing pipe P14

WARNING: Full flow velocity is greater than maximum (10.00)

Results:	Total Flow:	641.4000 cfs	Flow From:	Upstream
Status:	Fixed	Slope:	0.0064 ft/ft	
Pipe Width:	90.0000 in	Pipe Height:	90.0000 in	
Depth of Flow:	6.4960 ft	Flow Status:	Partial	
Critical Depth:	6.4500 ft	Capacity:	614.2974 cfs	
Velocity:	15.7741 ft/s	Flow Regime:	Critical	
Froude Number:	0.9857			

Designing pipe P32

WARNING: Full flow velocity is greater than maximum (10.00)

Results:	Total Flow:	6.1000 cfs	Flow From:	Injected Storm
Status:	Fixed	Slope:	0.0200 ft/ft	
Pipe Width:	24.0000 in	Pipe Height:	24.0000 in	
Depth of Flow:	0.5910 ft	Flow Status:	Partial	
Critical Depth:	0.8700 ft	Capacity:	31.9929 cfs	
Velocity:	7.8402 ft/s	Flow Regime:	SuperCritical	
Froude Number:	2.1195			

Designing pipe P15

WARNING: Full flow velocity is greater than maximum (10.00)

Results:	Total Flow:	647.5000 cfs	Flow From:	Upstream
Status:	Fixed	Slope:	0.0114 ft/ft	
Pipe Width:	90.0000 in	Pipe Height:	90.0000 in	
Depth of Flow:	5.0270 ft	Flow Status:	Partial	

Critical Depth: 6.4800 ft
Velocity: 20.5651 ft/s
Froude Number: 1.7160

Capacity: 819.8627 cfs
Flow Regime: SuperCritical

Designing pipe P33

WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 100.2000 cfs

Status: Fixed
Pipe Width: 42.0000 in
Depth of Flow: 2.1660 ft
Critical Depth: 3.0700 ft
Velocity: 16.0163 ft/s
Froude Number: 2.0821

Slope: 0.0200 ft/ft
Pipe Height: 42.0000 in
Flow Status: Partial
Capacity: 142.2837 cfs
Flow Regime: SuperCritical

Designing pipe P16

WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 747.7000 cfs

Status: Fixed
Pipe Width: 90.0000 in
Depth of Flow: 5.6250 ft
Critical Depth: 6.8100 ft
Velocity: 21.0334 ft/s
Froude Number: 1.5852

Slope: 0.0114 ft/ft
Pipe Height: 90.0000 in
Flow Status: Partial
Capacity: 819.8627 cfs
Flow Regime: SuperCritical

Designing pipe P34

Results:
Total Flow: 12.2000 cfs

Status: Fixed
Pipe Width: 24.0000 in
Depth of Flow: 1.3070 ft
Critical Depth: 1.2500 ft
Velocity: 5.6043 ft/s
Froude Number: 0.9243

Slope: 0.0050 ft/ft
Pipe Height: 24.0000 in
Flow Status: Partial
Capacity: 15.9965 cfs
Flow Regime: Subcritical

Designing manhole MH7

Results:
Total Flow: 759.9000 cfs

Flow From: Upstream

Status: Fixed Chamber Width: 8.0000 ft Chamber Length: 8.0000 ft

Designing pipe P17
WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 759.9000 cfs Flow From: Upstream
Status: Fixed Slope: 0.0301 ft/ft
Pipe Width: 72.0000 in Pipe Height: 72.0000 in
Depth of Flow: 5.1300 ft Flow Status: Partial
Critical Depth: 5.9300 ft Capacity: 734.2267 cfs
Velocity: 29.5144 ft/s
Froude Number: 2.1080 Flow Regime: SuperCritical

Designing manhole MH6

Results:
Total Flow: 759.9000 cfs Flow From: Upstream
Status: Fixed Chamber Length: 8.0000 ft
Chamber Width: 8.0000 ft

Designing pipe P18
WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 759.9000 cfs Flow From: Upstream
Status: Fixed Slope: 0.0278 ft/ft
Pipe Width: 72.0000 in Pipe Height: 72.0000 in
Depth of Flow: 5.5880 ft Flow Status: Partial
Critical Depth: 5.9300 ft Capacity: 706.6490 cfs
Velocity: 27.7015 ft/s
Froude Number: 1.6244 Flow Regime: SuperCritical

Designing manhole MH5

Results:
Total Flow: 759.9000 cfs Flow From: Upstream
Status: Fixed Chamber Length: 8.0000 ft
Chamber Width: 8.0000 ft

Designing pipe P19

WARNING: Full flow velocity is greater than maximum (10.00)

Results:	Total Flow:	759.9000 cfs	Flow From:	Upstream
Status:	Fixed		Slope:	0.0622 ft/ft
Pipe Width:	72.0000 in		Pipe Height:	72.0000 in
Depth of Flow:	3.7680 ft		Flow Status:	Partial
Critical Depth:	5.9300 ft		Capacity:	1055.9190 cfs
Velocity:	40.6361 ft/s			
Froude Number:	3.9904		Flow Regime:	SuperCritical

Designing manhole MH4

Results:	Total Flow:	759.9000 cfs	Flow From:	Upstream
Status:	Fixed		Chamber Length:	8.0000 ft
Chamber Width:	8.0000 ft			

Designing Pipe P20

WARNING: Full flow velocity is greater than maximum (10.00)

Results:	Total Flow:	759.9000 cfs	Flow From:	Upstream
Status:	Fixed		Slope:	0.0543 ft/ft
Pipe Width:	72.0000 in		Pipe Height:	72.0000 in
Depth of Flow:	3.9480 ft		Flow Status:	Partial
Critical Depth:	5.9300 ft		Capacity:	987.1497 cfs
Velocity:	38.5057 ft/s			
Froude Number:	3.6465		Flow Regime:	SuperCritical

Designing manhole MH3

Results:	Total Flow:	759.9000 cfs	Flow From:	Upstream
Status:	Fixed		Chamber Length:	8.0000 ft
Chamber Width:	8.0000 ft			

Designing Pipe P21

WARNING: Full flow velocity is greater than maximum (10.00)

Results:	Total Flow:	759.9000 cfs	Flow From:	Upstream
Status:	Fixed		Slope:	0.0543 ft/ft
Pipe Width:	72.0000 in		Pipe Height:	72.0000 in

Status: Fixed
Pipe Width: 72.0000 in
Depth of Flow: 3.4150 ft
Critical Depth: 5.9300 ft
Velocity: 45.7079 ft/s
Froude Number: 4.8185

Slope: 0.0840 ft/ft
Pipe Height: 72.0000 in
Flow Status: Partial
Capacity: 1227.7918 cfs
Flow Regime: SuperCritical

Designing manhole MH2

Results:
Total Flow: 759.9000 cfs

Status: Fixed
Chamber Width: 8.0000 ft
Chamber Length: 8.0000 ft

Designing pipe P22

WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 759.9000 cfs

Status: Fixed
Pipe Width: 72.0000 in
Depth of Flow: 3.2700 ft
Critical Depth: 5.9300 ft
Velocity: 48.2141 ft/s
Froude Number: 5.2349

Slope: 0.0967 ft/ft
Pipe Height: 72.0000 in
Flow Status: Partial
Capacity: 1316.7411 cfs
Flow Regime: SuperCritical

Designing manhole MH1

Results:
Total Flow: 759.9000 cfs

Status: Fixed
Chamber Width: 8.0000 ft
Chamber Length: 8.0000 ft

WARNING: Full flow velocity is greater than maximum (10.00)

Results:
Total Flow: 759.9000 cfs

Status: Fixed
Pipe Width: 72.0000 in
Depth of Flow: 3.4580 ft
Critical Depth: 5.9300 ft
Velocity: 45.0167 ft/s

Slope: 0.0808 ft/ft
Pipe Height: 72.0000 in
Flow Status: Partial
Capacity: 1203.5279 cfs
Flow Regime: SuperCritical

HGL/EGL Computations:

Table A:

Rim	Struct	2						Dnstrm					
		HGLup	ID	Q	L	V	d	dc	v / 2g	Sf	Soffit EGLdn	HGLdn	Tot Loss EGLup
(ft)	(ft)	(in)	(cfs)	(ft)	(ft/s)	(ft)	(ft)	(ft)	(ft/ft)	(ft)	(ft)	(ft)	(ft)
Outfall	-	-	-	-	-	-	-	-	-	-	-	-	-
5259.50	-	P23	72	759.90	92.95	45.02	-	-	31.49	0.0322	5259.25	-	5259.50
5263.87	-	MH1	-	-	-	-	-	-	-	-	-	5263.87	-
5263.87	5273.00	P22	72	759.90	25.12	48.21	3.27	5.93	36.13	-	5267.08	-	5264.35
5265.99	-	MH2	-	-	-	-	-	-	-	-	-	5265.99	-
5265.99	5272.50	P21	72	759.90	50.18	45.71	3.41	5.93	32.47	-	5268.83	-	5266.24
5269.77	-	MH3	-	-	-	-	-	-	-	-	-	5269.77	-
5269.77	5274.00	P20	72	759.90	63.86	38.51	3.95	5.93	23.04	-	5272.66	-	5270.61
5273.64	-	MH4	-	-	-	-	-	-	-	-	-	5273.64	-
5273.64	5278.00	P19	72	759.90	350.68	40.64	3.77	5.93	25.66	-	5275.99	-	5273.76
5295.02	-	MH5	-	-	-	-	-	-	-	-	-	5295.02	-
5295.02	5300.50	P18	72	759.90	96.04	27.70	5.59	5.93	11.93	-	5297.55	-	5297.14
5299.59	-	MH6	-	-	-	-	-	-	-	-	-	5299.59	-
5299.59	5311.50	P17	72	759.90	231.68	26.88	-	-	11.23	0.0322	5300.00	5310.81	5299.59
5307.05	-	MH7	-	-	-	-	-	-	-	-	-	5318.27	5318.27
5308.57	5312.00	P16	90	747.70	498.71	16.92	-	-	4.45	0.0095	5308.52	5319.79	5308.57
5320.07	-	Junction	-	-	-	-	-	-	-	-	-	5324.52	5320.07
												0.61	5325.13

5320.68	-	90	647.50	500.03	14.66	-	-	3.34	0.0071	5314.16	5325.13	5320.68	3.56	5328.69	
P15	-	-	-	-	-	-	-	-	-	-	-	-	0.05	5328.74	
5325.35	-	Junction	-	-	-	-	-	-	-	-	-	-	3.49	5332.23	
5325.40	-	P14	90	641.40	500.01	14.52	-	-	3.28	0.0070	5319.86	5328.74	5325.40	3.49	5332.23
5328.96	-	Junction	-	-	-	-	-	-	-	-	-	-	0.00	5332.23	
5328.96	-	P13	90	641.40	120.00	14.52	-	-	3.28	0.0070	5323.06	5332.23	5328.96	0.84	5333.07
5329.79	-	Junction	-	-	-	-	-	-	-	-	-	-	-	-	
5329.91	-	P12	90	610.00	380.01	13.81	-	-	2.96	0.0063	5323.83	5333.19	5329.91	2.40	5335.59
5332.63	-	Junction	-	-	-	-	-	-	-	-	-	-	0.00	5335.59	
5332.63	-	P11	90	610.00	351.24	13.81	-	-	2.96	0.0063	5326.26	5335.59	5332.63	2.22	5337.80
5334.84	-	MH13	-	-	-	-	-	-	-	-	-	-	0.55	5340.22	
5336.71	5340.00	P10	72	398.00	61.79	14.08	-	-	3.08	0.0088	5336.48	5339.67	5336.71	1.87	5339.67
5337.14	-	MH14	-	-	-	-	-	-	-	-	-	-	1.32	5341.54	
5338.46	5340.00	P9	72	276.80	500.00	9.79	-	-	1.49	0.0043	5337.80	5341.54	5338.46	2.14	5343.67
5342.19	-	MH15	-	-	-	-	-	-	-	-	-	-	0.36	5344.03	
5342.55	5343.00	P8	66	276.80	500.02	11.65	-	-	2.11	0.0068	5339.56	5344.03	5342.55	3.40	5347.43
5345.32	-	Junction	-	-	-	-	-	-	-	-	-	-	-	-	
5345.68	-	P26	54	169.80	26.85	10.68	-	-	1.77	0.0075	5343.29	5347.79	5345.68	0.20	5347.99
5346.22	-	New Branch	-	-	-	-	-	-	-	-	-	-	-	-	
5307.05	-	MH7	-	-	-	-	-	-	-	-	-	-	3.49	5321.76	
5310.54	5312.00	P34	24	12.20	21.05	3.88	-	-	0.23	0.0029	5303.02	5321.76	5310.54	0.06	5321.82
5321.59	-	New Branch	-	-	-	-	-	-	-	-	-	-	-	-	
5320.07	-	P33	42	100.20	22.65	10.41	-	-	1.69	0.0099	5310.16	5324.52	5320.07	0.22	5324.75
5323.06	-	New Branch	-	-	-	-	-	-	-	-	-	-	-	-	
5325.35	-	P32	24	6.10	27.65	1.94	-	-	0.06	0.0007	5314.36	5328.69	5325.35	0.02	5328.71

Table B:

-	Junction	-	0.17	-	-	0.19	Neg	0.36		-	-	-	-	-	-
-	P26	0.20	-	-	-	-	0.20		-	-	-	-	-	-	-
-	New Branch	-	-	-	-	-	-	-		-	-	-	-	-	-
-	MH7	-	-	3.49	-	-	3.49		6.33	1.103	1.000	0.516	0.546	1.000	-
1.000	0.311	P34	0.06	-	-	-	0.06		-	-	-	-	-	-	-
-	New Branch	-	-	-	-	-	-	-		-	-	-	-	-	-
-	P33	-	0.22	-	-	-	0.22		-	-	-	-	-	-	-
-	New Branch	-	-	-	-	-	-	-		-	-	-	-	-	-
-	P32	-	0.02	-	-	-	0.02		-	-	-	-	-	-	-
-	New Branch	-	-	-	-	-	-	-		-	-	-	-	-	-
-	P31	-	0.63	-	-	-	0.63		-	-	-	-	-	-	-
-	New Branch	-	-	-	-	-	-	-		-	-	-	-	-	-
-	MH13	-	-	0.50	-	-	0.50		13.87	0.135	1.000	0.723	1.724	1.000	-
1.000	0.169	P0	0.11	-	-	-	0.11		-	-	-	-	-	-	-
-	New Branch	-	-	-	-	-	-	-		-	-	-	-	-	-
-	MH14	-	-	0.57	-	-	0.57		5.70	1.436	1.000	0.485	0.267	1.000	-
1.000	0.186	P30	0.17	-	-	-	0.17		-	-	-	-	-	-	-
-	New Branch	-	-	-	-	-	-	-		-	-	-	-	-	-
-	P7	-	2.78	-	-	-	2.78		-	-	-	-	-	-	-
-	MH17	-	-	-	-	-	-	-		-	-	-	-	-	-
-	P6	-	-	-	-	-	-	-	SuperCrt		-	-	-	-	-

V
Vinyard & Associates, Inc.**A**4415-D Hawkins, NE
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Geotechnical Engineering • Materials Testing • Environmental Engineering

REVISED GEOTECHNICAL INVESTIGATION

AND PAVEMENT SECTION DESIGN

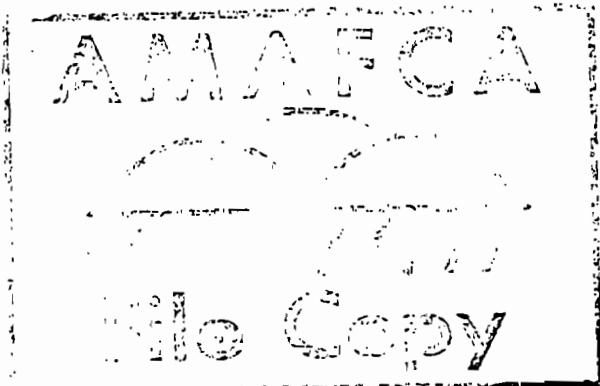
UNSER BLVD. FROM PARADISE BLVD.TO THE BERNALILLO COUNTY LINE

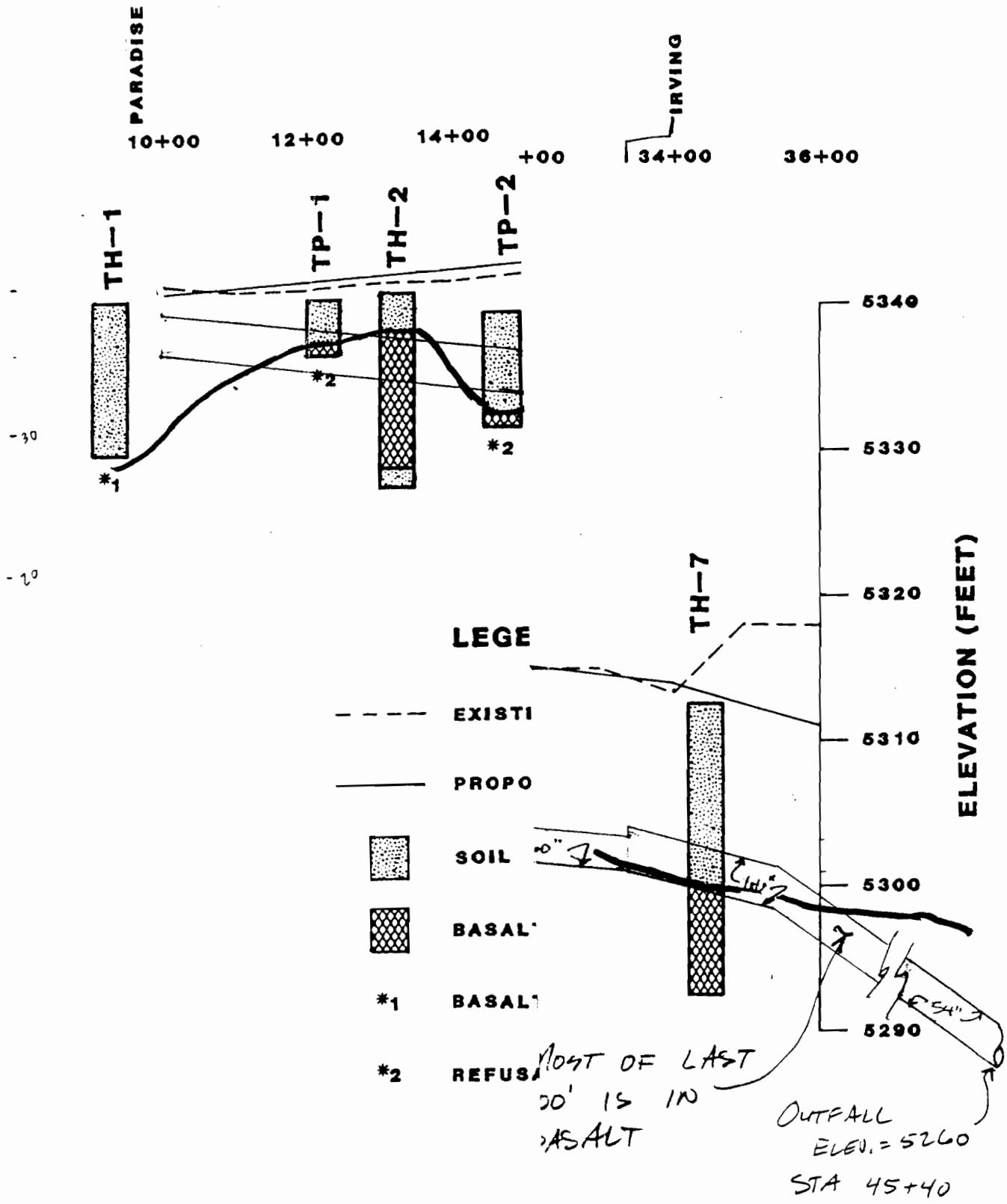
Prepared for:

Leedshall-Herkenhoff, Inc.

Project No.: 90-1-10

April 9, 1990





PROJECT NO.: 90-1-10

FIGURE NO.: 23

EXHIBIT 1

Storm Drain Basin Map
(Primary Study Area)