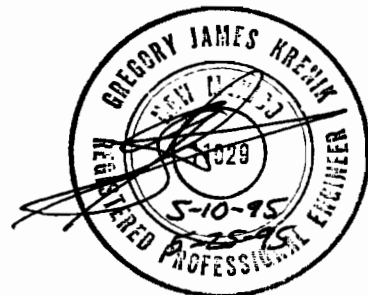


DRAINAGE CALCULATIONS
for
THE KNOLLS OF PARADISE HILLS
Lots 14-19, Block 44
Lots 27-31, Block 45

May 1995

MAY 25 1995





D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT CONGRESS HEIGHTS
SUBJECT DRAINAGE
BY RM DATE 17 APR 95
CHECKED _____ DATE _____
SHEET 1 OF 6

AREA IN SUBDIVISION

A = 2.6415 ACRES = 0.0041 SQ MILES

LAND TREATMENT

TYPE "A" = 0.0%

TYPE "B" = 28.70%

TYPE "C" = 28.71%

4.16 DU/AC TYPE "D" = 42.59% 43.24%

AHYMO RESULTS

TOTAL PEAK Q = 9.64 cfs @ 1.50 HRS

TOTAL PEAK V = 0.3245 Acre-Feet

POND LOCATION, SIZING & WATER SURFACE ELEVATION

- LOCATION

NORTHEAST CORNER LOT OF SUBDIVISION (SEE ATTACHMENTS)

- POND SIZING

ELEV.	AREA (ft ²)	V (Acre-Ft)
91 ⁰⁰	3375	0.0852
92 ⁰⁰	4050	0.1033
93 ⁰⁰	4950	0.1240
94 ⁰⁰	5850	0.1446
95 ⁰⁰	6750	0.1653
96 ⁰⁰	7650	
TOTAL		0.6224

FOR 100YR-10DAY STORM

$$V = 0.3245 + \left[\frac{(1.3820 * (3.67 - 2.20))}{12} \right] = 0.4913 = Q_{PEAK}$$

AREA IN CONGRESS

A = 0.2645 ACRES = 0.0004 SQ MILES

LAND TREATMENT

TYPE "A" = 0.0%

TYPE "B" = 10.42%

TYPE "C" = 0.0%

TYPE "D" = 89.58%

CONGRESS AVE

Q = 1.07 cfs @ 1.50 HRS

V = 0.039 Acre-Feet

ACADEMY ROAD

Q = 8.57 cfs @ 1.50 HRS

V = 0.2855 Acre-Feet

Temporary or Permanent

$Q_{CAPACITY} > Q_{PEAK}$

$0.6224 \text{ Acre-Feet} > 0.4913 \text{ Acre-Feet}$

∴ POND CONTAINS CAPACITY
FOR 100YR-10DAY STORM

MAY - 3 1995

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PROJECT CONGRESS HEIGHTS
SUBJECT DRAINAGE
BY ZM DATE 17 APR 95
CHECKED _____ DATE _____
SHEET 2 OF 6

POND LOCATION, SIZING, & WATER SURFACE ELEVATION (CONTINUED)

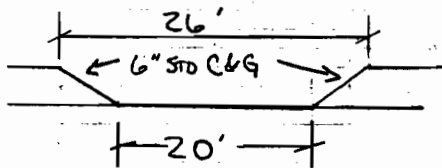
- MAXIMUM WATER SURFACE ELEVATION

ELEV.	V (Acre-Ft)
95 ⁰⁰	0.4571
X	0.4913
96 ⁰⁰	0.6224

X = 95²⁰ (INDICATED ON PLAN)

INLET & CHANNEL DESIGN (ACADEMY ROAD)

- INLET STRUCTURE (DRIVEWAY OPENING ON ACADEMY)



$$Q = C L H^{3/2}$$

$$C = 2.9 \quad L = 20' \quad H = 0.5'$$

$$Q = 2.9 * 20 * 0.5'$$

$$Q = 29 \text{ cfs}$$

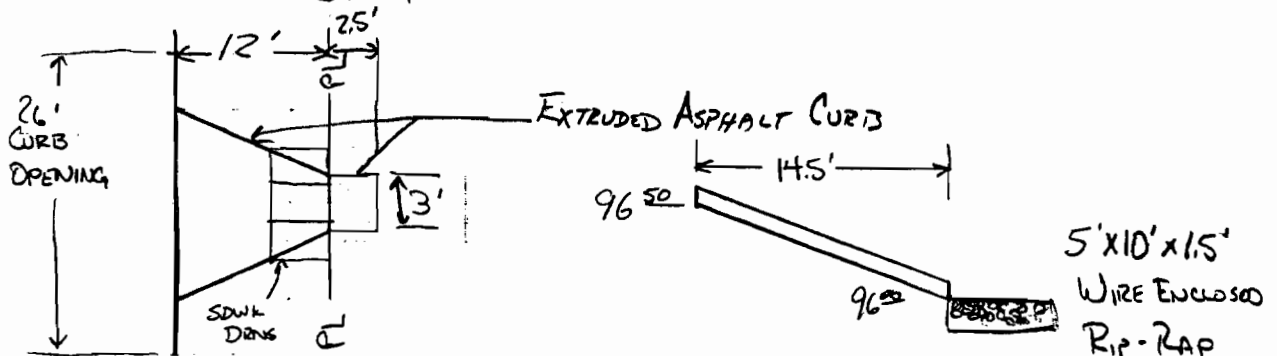
$$L = \frac{8.57}{2.9 (0.5)^{3/2}} = 8.36'$$

$$Q_{\text{CAPACITY}} > Q_{\text{PEAK}}$$

$$29 \text{ cfs} > 8.57 \text{ cfs (FROM AHYMO RESULTS OF ACADEMY ROAD)}$$

∴ INLET CAPACITY EXCEEDS DEVELOPED 100 YR - 6 HR
STORM RUNOFF, FOR ACADEMY

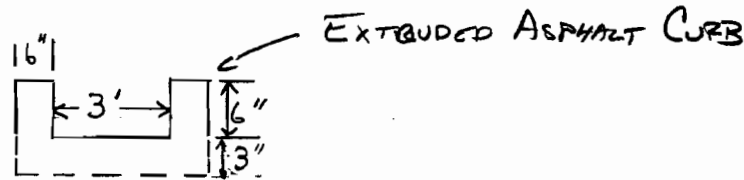
- CHANNEL DESIGN



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INLET & CHANNEL DESIGN (CONTINUED)



$$Q = \frac{K}{n} A R_h^{2/3} S^{1/2}$$

$$= \frac{1.49}{0.016} (1.5) \left(\frac{15}{4}\right)^{2/3} (0.0345)^{1/2}$$

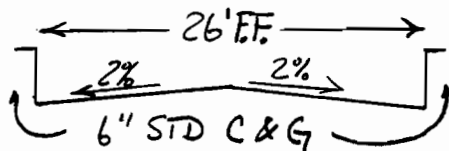
$Q = 13.50 \text{ cfs}$ CAPACITY OF ASPHALT CHANNEL

$$Q_{\text{CAPACITY}} > Q_{\text{PEAK}}$$

$$13.50 \text{ cfs} > 8.57 \text{ cfs}$$

∴ CHANNEL CONTAINS CAPACITY OF DEVELOPED STORM RUNOFF

STREET CAPACITY (ACADEMY ROAD)



Cross-section is not representative of the street.
 $S = 0.66\%$

$$Q = \frac{K}{n} A R_h^{2/3} S^{1/2}$$

$$= \frac{1.49}{0.017} (8.515) \left(\frac{8.55}{27}\right)^{2/3} (0.0066)^{1/2}$$

EGL

$$Q = 29.90 \text{ cfs} \text{ CAPACITY} \quad V = 29.9 / 8.515 = 3.51 \text{ fps}$$

$$Q_{\text{CAPACITY}} > Q_{\text{PEAK}}$$

$$29.90 \text{ cfs} > 8.570 \text{ cfs}$$

∴ STREET CAPACITY EXCEEDS DEVELOPED STORM RUN OFF



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PROJECT CONGRESS HEIGHTS
SUBJECT DRAINAGE
BY ZM DATE 18 Apr 25
CHECKED _____ DATE _____

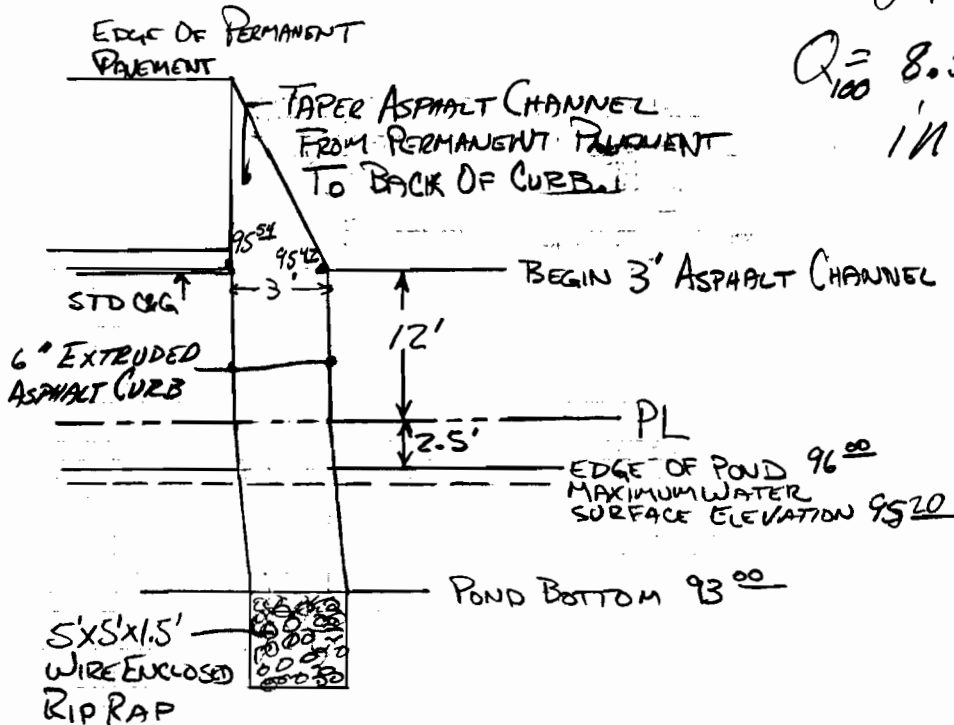
SHEET 4 OF 6

INLET & CHANNEL DESIGN (CONGRESS)

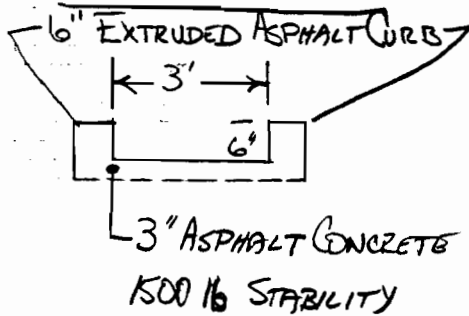
Check Capacity
of Congress.

$$Q_{100} = 8.57 + 1.07 = 9.64 \text{ cfs}$$

in half section.



- INLET DESIGN



$$Q = C L H^{3/2}$$

$$C = 2.9 \quad L = 3' \quad H = 0.5'$$

$$Q = 2.9(3)(.5)^{3/2}$$

$$Q = 3.08 \text{ cfs}$$

$$Q_{CAPACITY} > Q_{PEAK}$$

$$3.08 \text{ cfs} > 1.07 \text{ cfs (FROM APMO RESULTS CONGRESS AVE.)}$$

∴ INLET CAPACITY EXCEEDS DEVELOPED STORM RUNOFF FOR CONGRESS

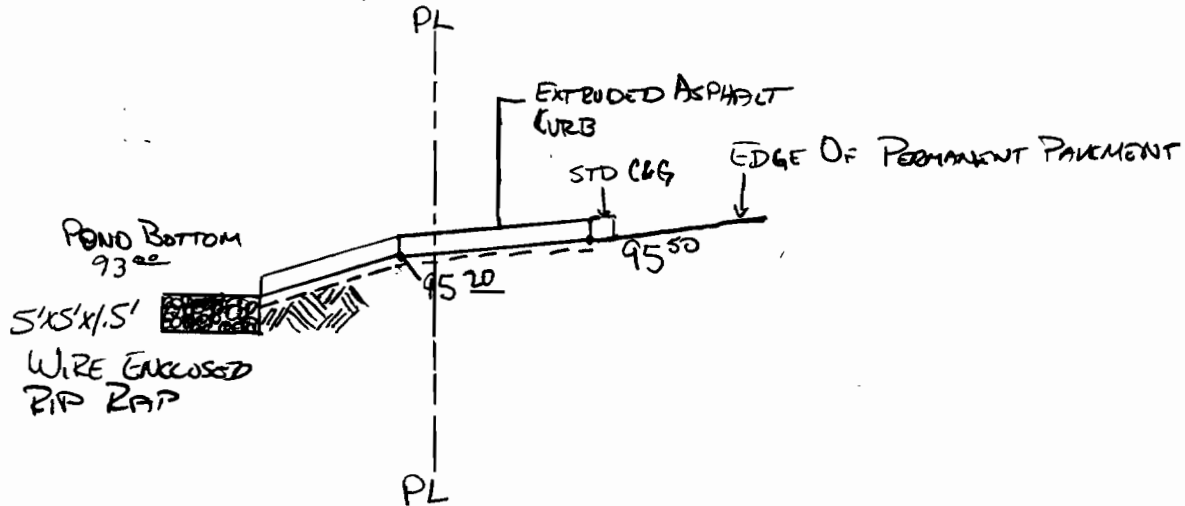
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PROJECT CONGRESS HEIGHTS
SUBJECT DRAINAGE
BY RM DATE 8 APR 95
CHECKED _____ DATE _____
SHEET 5 OF 6

- CHANNEL DESIGN



NOTE: MINIMUM SLOPE ON CHANNEL WILL BE FROM FLOWLINE ON CONGRESS TO MAXIMUM WATER SURFACE ELEVATION IN POND. WILL BE DETERMINED WITH CHANNEL FLOWING @ 1/2 CAPACITY

$$Q = \frac{K}{n} A R_h^{2/3} S^{1/2}$$

$$= \frac{1.49}{0.016} (0.75) \left(\frac{0.75}{3.5}\right)^{2/3} (0.0167)^{1/2}$$

$$Q = 3.23 \text{ cfs}$$

$$Q_{\text{CAPACITY}} > Q_{\text{PEAK}}$$

$$3.23 \text{ cfs} > 1.07 \text{ cfs}$$

∴ CHANNEL CONTAINS CAPACITY TO CONVEY 100YR-6HR STORM FROM CONGRESS TO POND

EMERGENCY SPILLWAY & CHANNEL

$$Q = 9.64 \text{ cfs}$$

$$Q = CLH^{3/2}$$

$$H = 0.5 \quad C = 2.9 \quad Q = 9.64$$

$$L = Q/C H^{3/2}$$

$$L = 9.64 / 2.9 (0.5)^{3/2}$$

$$L = 9.40' \quad \text{CONSTRUCT OPENING TO 10'}$$

∴ EMERGENCY SPILLWAY
OPENING 10' WILL
CONVEY 100YR EVENT

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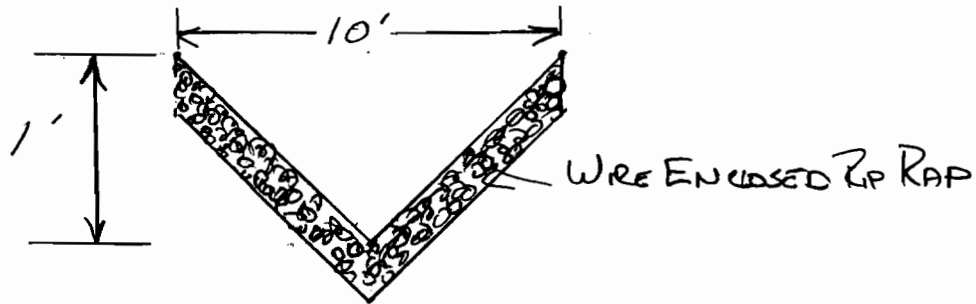


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PROJECT CONGRESS HEIGHTS
SUBJECT DRAINAGE
BY RM DATE 27 APR 95
CHECKED _____ DATE _____
SHEET 6 OF 6

EMERGENCY SPILLWAY & CHANNEL (CONTINUED)

CHANNEL WIRE ENCLOSED RIP RAP V SHAPED CHANNEL



$$Q = \frac{K}{n} A R_h^{2/3} S^{1/2}$$
$$= \frac{1.49}{0.025} 5 \left(\frac{5}{10.2} \right)^{2/3} (0.1)^{1/2}$$

$$Q = 61.45 \text{ cfs Flowing @ Full Capacity} > 18.52 \text{ cfs}$$

∴ EMERGENCY SPILLWAY & CHANNEL CONTAIN CAPACITY
FOR 100 YR - LHR STORM



PROJECT THE KNOLLS OF PRADE HILLS
SUBJECT DRAINAGE RE CALCS ^{SELECTED LOTS}
BY RM DATE 13 JUN 85
CHECKED _____ DATE _____
SHEET 1 OF 2

NO CHANGES IN LAND TREATMENTS OR AREA FROM AHYMO

$$A = 76415 \text{ Acres} \quad Q = 8.57 \text{ cfs} \quad V_{TK} = 0.2855 \text{ Acres} \cdot \text{FT}$$

- OFFSITE FLOWS

$$A = 3.94284 \text{ Acres} = 0.0061659 \text{ miles}$$

LAND TREATMENTS

$$\overline{\text{Type "A"}} = 100\%$$

TYPE "C" = 0.0 %

Type "B" = 0.0%

TYPE "D" = 0.0%

AHYMD RESULTS

$$Q_{PK} = 5.12 \text{ cfs} \quad \eta_{PK} = 0.1443 \text{ AUZE TECT}$$

- ADDITION OF OFFSITE FLOWS & ACADEMY FOR STREET SECTION
AHVMO RESULTS * SECTION TAKEN

* SECTION TAKEN

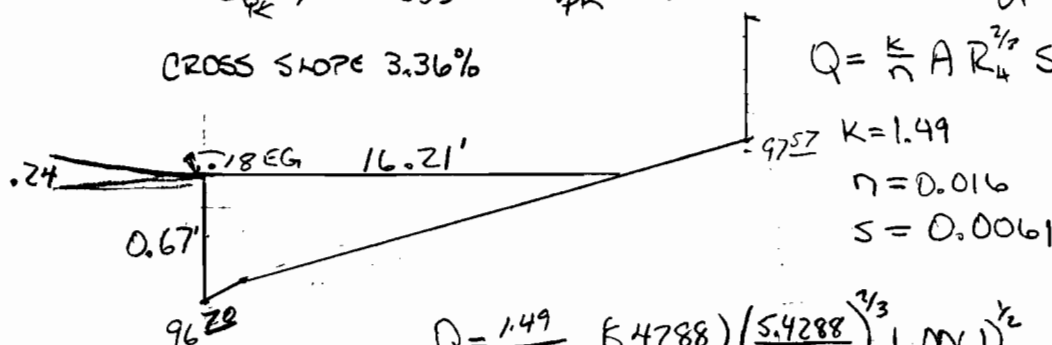
@ SOUTHWESTERN SIDE
OF CURB OPENING PRIOR
2/14/14 TO ENTERING INLET

$$Q_{pk} = 13.58 \text{ cfs}$$

$$V_{PK} = 0.4298 \text{ AIRS FEET}$$

CROSS SLOPE 3.36%

$$Q = \frac{K}{\gamma} A R_4^{2/3} S^{1/2}$$



$$EG = d + \frac{1}{2}g$$

$$= 0.67 + \left(\frac{34}{2} \right) \frac{1}{2}g$$

$$\underline{\underline{F_9 = 0.85}}$$

$$Q = \frac{1.49}{0.016} (5.4288) \left(\frac{5.4288}{16.8938} \right)^{2/3} (0.0061)^{1/2}$$

$$V = Q/A = 3.411 \text{ fps}$$

$$Q = 18.52 \text{ cfs} > 13.58 \text{ cfs}$$

STREET SECTION CONTAINS CAPACITY FOR 100 YR EVENT
E.G. REMAINS WITHIN RIGHT OF WAY



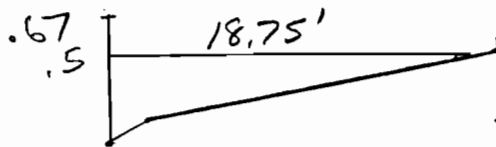
CONGRESS

NO CHANGES IN LAND TREATMENTS OR AREA

$$A = 0.2645 \text{ ACRES}$$

AHYMO RESULTS

$$Q_{PK} = 1.07 \text{ cfs} \quad V_{PK} = 0.039 \text{ ACRE-Feet}$$



ASSUME FLOW DEPTH @ 0.5'

$$Q = \frac{K}{n} A R^{2/3} S^{1/2}$$

$$K = 1.49$$

$$n = 0.016$$

$S = 0.0350$ MIN SLOPE ON CONGRESS

$$Q = \frac{1.49}{0.016} (4.6875) \left(\frac{18.75}{19.25} \right)^{2/3} (0.035)^{1/2}$$

$$Q = 3.85 \text{ cfs} \gg 1.07 \text{ cfs} + 18.52 = 19.59 \text{ cfs}$$

∴ STREET SECTION CONTAINS CAPACITY FOR 100YR EVENT ON CONGRESS. EG WILL NOT BE A FACTOR DUE TO THE AMOUNT OF FLOW IN CONGRESS AT THIS POINT

POND

NO CHANGE

$$V_{\text{PROVIDED}} = 0.6224 \text{ AC}$$

$$V_{\text{OFFSITE}} = 0.1443 \text{ ACRE-Feet}$$

$$+ V_{\text{SUBDIVISION CONGRESS}} = 0.4913 \text{ ACRE-Feet}$$

$$V_{\text{ENTERING POND}} = 0.63560 \text{ ACRE-Feet}$$

RETAINED VOLUME @ ELEV. 95[±]

4.00

$$V_{\text{RT}} = 0.4913 \text{ ACRE-Feet}$$

∴ DURING 100YR EVENT OFFSITE FLOWS WILL DISCHARGE THROUGH EMERGENCY SPILLWAY ELEV. 95[±]. THE ON SITE FLOW WILL BE RETAINED.