DRAINAGE REPORT FOR COTTONWOOD MALL AND SAD-223 PART 2

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Prepared for:

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MASTER DRAINAGE PLAN FOR THE COTTONWOOD MALL

PURPOSE

The purpose of this report is to identify the drainage and management plan for site development plan approval for a regional shopping center site comprising approximately 90 acres, referred to as Cottonwood Mall, owned and to be developed by the Albuquerque Mall Company Limited Partnership, managed by Melvin Simon and Associates, Inc. In addition, this report provides the design computations and backup analysis required for work order approval for Part 2 of SAD-223, which includes all of the on-site water, sanitary sewer, and storm drainage facilities required for development of the mall site. The Master Drainage Report for SAD-223, prepared by Easterling and Associates, which has been submitted and approved, identifies the drainage management concepts which will govern this site. The Drainage Ordinance, Development Process Manual (DPM), North Coors Drainage Management Plan, and the Seven Bar Ranch Sector Development Plan have been utilized to prepare this report.

SITE LOCATION AND DESCRIPTION

The project site is generally located on a low plateau above the west bank of the Rio Grande, immediately north of the Calabacillas Arroyo. The site is located on the west side of North Coors Boulevard between Irving Boulevard and Alameda Boulevard, bordered on the north by the Seven Bar Loop Road, on the south and west by the Coors Bypass Road, and on the east by Corrales Road (old North Coors Road). Please refer to the project location map on Plate 1. The site is zoned SU-1 for Regional Shopping Center.

EXISTING CONDITIONS

The mall site is to be constructed at the southern portion of the old Alameda Airport. Existing buildings and asphalt parking areas that are still in place will be removed of prior to the earthwork operations.

To the south of the project is the V.T. Autopark across the Coors Bypass Road just west of Corrales Road. Infrastructure improvements for W.O. 3040, constructed as a requirement for the Autopark, included the southwestern 24' of the Coors Bypass Road along the project frontage, sanitary sewer and water lines required for the development, and the storm drain system that collects and discharges runoff to the Calabacillas Arroyo. The storm drain system constructed in the Coors Bypass Road collects runoff from the V.T. Autopark and a portion of the property west of the Autopark (formerly owned by ABQ Development), the Coors Bypass Road, and a portion of the southwesterly extension of Eagle Ranch Road.

Immediately northeast of the site is the Questa del Rio Property of A.J. Black, located on the west side of the Corrales Road south of Seven Bar Loop Road. The western and southern boundaries of this property are shared with the mall site. An existing arroyo which begins on the mall site and continues east across the Black's property conveys collected undeveloped runoff from the mall site east to Corrales Road. A single 60" culvert then conveys the flow under Corrales road into a detention pond for ultimate discharge into the existing Middle Rio Grande Conservancy District's Corrales Main Canal.

HYDROLOGIC ANALYSIS

The hydrologic computations identified within the proposed revision to the Development Process Manual, dated August, 1991 (DPM Update) are used to compute developed runoff rates and volumes. The computerized watershed model "HYMO" was used to compute the flow rates generated by the 100-year and 10-year storm, and to route the flows through storm sewers and ponds.

All flowrates for the individual basins were first calculated using the rational method as a check against the HYMO output. Stage/storage/discharge relationships were developed for each pond and outlet using the orifice and weir equations as applicable. The program was then used to route the hydrographs for each basin through the ponds and storm sewers that comprise the storm drainage facilities within the development.

All the calculations and comparisons of the peak flow rates and other miscellaneous hydrologic computations are listed in Appendix 1. Appendix 2 contains the output obtained from the HYMO analysis.

The basin boundaries, peak discharges, and conceptual proposed contours are shown on plate 1 of the enclosed plans. Also identified are the proposed storm sewers with diameters, and proposed ponding area with volumes. The proposed storm sewer diameters, lengths, slopes, manhole sizes and lateral information are shown on the preliminary plan and profile sheets developed for submittal to the DRC of SAD-223, Part 2.

DRAINAGE MANAGEMENT PLAN

The mall site was divided into three major basins (A, B. and C) which will ultimately drain to the Calabacillas Arroyo, and a fourth basin (Basin D) which will ultimately drain to the Corrales Main Canal as shown on the drainage plan (Plate 1). The approved drainage report for the V.T. Autopark development established the maximum flowrate of developed runoff that can be discharged into the existing storm sewer system within the Coors Bypass from the mall site to be 169 cfs. The remaining developed runoff from Basin D will be discharged into the southside of the Seven Bar Loop Road for collection and discharge across the Corrales Road into the Corrales Main Canal. This flow is governed by the North Coors Drainage Management Plan.

The three major basins (A, B, and C) are comprised of a series of contributing basins. Each contributing basin is provided a means of collecting the flow (junction boxes, inlets, or ponds), and a storm sewer lateral to convey the flow.

Basin A and Basin B were designed to collect and distribute approximately two-thirds of the developed flow generated from the shopping mall to the existing storm sewer. Basin C was designed to collect the flows generated in the outlots (Tracts C-1 through C-4) adjacent to the Corrales Road and route it to the existing storm system.

Basin A routes flows from the southwest corner of the site east along the south half of the site through a detention pond at the extreme south end of the site. Immediately downstream of the pond, runoff from Basin A combines with flow from Basin B at MH #12. The peak flowrate developed in the Basin A as identified in the HYMO output and released from the pond is 65.0

cfs. Basin B routes flows from the northwest corner of the site, along with offsite runoff collected from a portion of the Seven Bar Loop Road right-of-way, east along the north half of the site, then south to the manhole #12. The peak flow generated in Basin B at the intersecting manhole is 104.9 cfs. Basin C collects the runoff that develops in the outlots (Tracts C-1 through C-4) adjacent to the Corrales Road. The water is then conveyed north and west where it will join the flow from Basin B. The peak flowrate to be discharged into the existing storm sewer system in the Coors Bypass Road as identified in the HYMO output is 169.6 cfs.

Basin D is located at the northeast corner of the site. The flows generated in this basin will be collected in a small detention pond for discharge into the south half of the proposed Seven Bar Loop Road. Flows are then conveyed east to a series of storm sewer inlets which will collect the discharge conveyed by Seven Bar Loop Road. Collected runoff will be conveyed by a storm sewer to be constructed within Part 4 of SAD-223 south to the existing 60" culvert, where it will be conveyed under Corrales Road into a detention pond. The pond will ultimately into the Corrales Main Canal. The North Coors Drainage Management Plan identified 106 cfs to be discharged from the mall site in the developed condition to the existing arroyo (see the calculations given in Appendix 3). Due to the delay in the construction of improvements to the Corrales Main Canal, the total discharge to that facility allowed by the North Coors Drainage Management Plan is not utilized. The peak flowrate that was calculated for the 100-year, 6-hour storm which will be discharged from Basin D (developed) into the existing arroyo was 11.1 cfs. Of the 11.1 cfs, 7.7 cfs will be collected in a small detention pond at the northeast corner of the site and a total of 7.5 cfs will be released into the southern portion of the Seven Bar Loop Road.

Two offsite drainage basins will discharge onto the Cottonwood Mall site. These comprise flows from the south half of the Seven Bar Loop Road from the intersection with the Cottonwood Drive to the intersection with the Coors Bypass Road, and from the west half of the Coors Bypass Road from the intersection with the Seven Bar Loop Road to Mall Entrance number 2. Flows that develop in properties on the west and south side of the Coors Bypass Road that are not directly discharged into the Calabacillas Arroyo are conveyed either north or south in the Bypass Road. The drainage management plan for offsite basins is identified within the Master Drainage Report for SAD-223, prepared by Easterling and Associates.

The runoff collected on the roof areas will be released by a series of gutters and pipes into the storm sewer system. The openings that will be provided to allow the runoff collected on the roof into the gutter system will be sized so that no ponding will occur on the roof areas.

It was determined through several iterations that detention ponding will be necessary in order to meet the discharge requirements at the outlet to the existing storm sewer and the Seven Bar Loop Road. Size, shape, and depth of each pond will vary depending on the location and outlet conditions. The interior slopes of the ponds will be landscaped with sod and will be designed a to a maximum of a 3:1 (horizonal:vertical) slope. The bottom surface of the pond will be sodded or lined with gravel in order to collect sediment and provide for erosion control. Standpipe structures with perforated outlet pipes will be utilized to control the discharge from the detention ponds.

Extensive landscaping will be provided on the mall site at locations not utilized for parking or buildings. Landscaped areas will include any combination of grass, trees, shrubs, or bushes. The landscaping used will provide for erosion protection of side slopes and ponds, beautification

of the site, and provide a aesthetic buffer between the site and surrounding developments. The treatment provided for the individual landscaped areas are identified within the construction plans for Part 2 of SAD-223.

PHASING AND EROSION CONTROL

The construction of the majorit of the mall site will be completed in one phase. The parking lot expansion areas associated with major department store expansions and construction of the single future department store on the north side of the building, along with development of the surrounding Reserve Parcels will be constructed as need dictates. All of the infrastructure improvements required for the entire site will be completed during the initial construction. Roof drain laterals will be provided from the storm sewer system to within 5' of the building areas for the connection by the building contractors.

Soil erosion and dust control are recognized as significant problems for this development. As identified in the Seven Bar Ranch Sector Development Plan, this area will be subject to the Albuquerque/Bernalillo County Air Quality Control Board regulations and ordinances regarding soil erosion and dust control during development and construction. This includes obtaining a "Top Soil Disturbance Permit" which shall outline specific dust control plans and measures for this project. It is the responsibility of the contractor to obtain the necessary permit before mass grading operations start.

The entire site will be mass graded prior to the installation of the infrastructure. Extensive erosion control and wind protection will be necessary during the mass grading operations. These measures may include interim contour berms, snow fences, and site watering. The contour berms should follow the boundary of the site to keep flows collected during grading operations on the site and to stop sediment from damaging adjacent properties. Snow fences should be placed generally in the north/south directions along the eastern boundary of the site prior to grading operations in order to contain wind borne materials onsite. Water should be applied during all phases of the earthwork and especially at the end of the working day in order to form a crust surface. Those portions of the site that are not anticipated to be developed within one year shall be treated with hay mulch crimped into north/south furrows to provide for long term dust control.

CONCLUSIONS

The Cottonwood Mall is to be constructed between the Coos Bypass Road ad the Seven Bar Loop Road on the west side of the Corrales Road. The offsite infrastructure improvements include the construction of the north portion of the Coors Bypass Road, the southern half of the Seven Bar Loop Road, and channelization improvements to the Corrales Road.

The site has been designed to convey developed flows to the existing storm sewer system in the Coors Bypass Road, or to Seven Bar Loop Road, where it will be conveyed across Corrales Road through a detention pond into the Corrales Main Canal. The constraints on discharging developed runoff to the existing downstream facilities identified either within the drainage report prepared for the V.T. Autopark site or the North Coors Drainage Management Plan. Concepts for drainage management within the entire area have been outlined within the Master Drainage Report for SAD-223, prepared by Easterling and Associates.

Based on the hydrologic analysis contained herein, and previous research ad analysis, detention ponding will be necessary to control the discharge to the previously approved flowrates. The detention ponds will be landscaped and standpipe structures will be utilized for discharge. Roof flows will be collected by a series of gutters and pipes for discharge into the storm sewer. The maximum peak flowrate generated onsite by this project when fully developed has been computed to be 169.6 cfs, which is roughly equivalent to the 169 cfs allowed by the V.T. Autopark Drainage Management Plan.

The construction of the majority of the mall is to be completed in one phase and the required infrastructure will be installed with the initial construction. The entire project is to be graded in one complete operation, which will require dust and erosion control measures to be performed by the contractor. These measures shall include interim control berms, water protection, snow fences, and crimped hay mulch with native seeding. It will be the contractors responsibility to obtain the necessary permits and provide the control measures during construction.

6" ORIFICE, 9"DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV. 1.00 0.75

ENTER PIPE ELEV. AND PIPE DIAM.

-3.00 6

ELEVATION (FT)	DISCHARGE (CFS)
-2.00000	0.94504
-1.00000	1.33648
0.00000	1.63685
DISCHARGE AT TOP	1.83005

6" ORIFICE, 9"DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV. 1.00 0.75

ENTER PIPE ELEV. AND PIPE DIAM.

-3.009

ELEVATION (FT)	DISCHARGE (CFS)
-2.00000	2.12633
-1.00000	3.00709
0.0000	3.68291
DISCHARGE AT TOP	4.11762

12" ORIFICE, 9"DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV. 1.00 0.75

ENTER PIPE ELEV. AND PIPE DIAM.

-3.00 12

DISCHARGE (CFS)
3.78014
5.34593
6.54740
7.32022

15" ORIFICE, 9"DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV. 1.00 0.75

ENTER PIPE ELEV. AND PIPE DIAM.

-3.00 15

ELEVATION (FT)	DISCHARGE (CFS)
-2.00000	5.90648
-1.00000	8.35302
0.00000	10.23032
DISCHARGE AT TOP	11.43784

21" ORIFICE, 9"DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV.

1.00 0.75

ENTER PIPE ELEV. AND PIPE DIAM.

-3.0021

DISCHARGE	(CFS)
11.	57669
16.	37191
20.	05141
22.	41816
	11. 16. 20.

6" ORIFICE, 5' DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV. 1.00 5.00

ENTER PIPE ELEV. AND PIPE DIAM.

0.00 6

ELEVAT:	ION (FT)	DISCHARGE (CFS)
	1.00000	0.94504
	2.00000	1.33648
	3.00000	1.63685
	4.00000	1.89007
DISCHARGE	AT TOP	2.11316

9" ORIFICE, 5' DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV.

1.00 5.00

ENTER PIPE ELEV. AND PIPE DIAM.

0.00 9

ELEVATION (FT)	DISCHARGE (CFS)
1.00000	2.12633
2.00000	3.00709
3.00000	3.68291
4.00000	4.25266
DISCHARGE AT TOP	4.75462

9" ORIFICE, 2' DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV. 0.25 2.00

ENTER PIPE ELEV. AND PIPE DIAM.

-2.759

	ION (FT) -2.50000 -2.25000 -2.00000 -1.75000 -1.50000 -1.25000 -0.75000 -0.50000 0.25000 0.50000 0.75000 1.00000 1.25000	DISCHARGE (CFS) 1.06317 1.50354 1.84146 2.12633 2.37731 2.60421 2.81287 3.00709 3.18950 3.36202 3.52612 3.68291 3.83330 3.97800 4.11762 4.25266 4.38354 4.51063
DISCHARGE	AT TOP	4.63423

15" ORIFICE, 2' DEEP POND

ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV. 1.00 2.00

ENTER PIPE ELEV. AND PIPE DIAM.

-3.0015

ELEVATION (FT)	DISCHARGE (CFS)
-2.00000	5.90648
-1.00000	8.35302
0.0000	10.23032
1.00000	11.81295
DISCHARGE AT TOP	13.20728

27" ORIFICE, 8' DEEP POND
ALL INPUT VALUES IN FT. EXCEPT PIPE DIAM IN INCHES
ENTER INCREMENTAL ELEV. AND TOP OF DAM ELEV. 1.00 8.00

ENTER PIPE ELEV. AND PIPE DIAM.

-4.00 27

ELEVATION (FT)	DISCHARGE (CFS)
-3.00000	19.13698
-2.00000	27.06378
-1.00000	33.14622
0.0000	38.27396
1.00000	42.79159
2.00000	46.87583
3.00000	50.63169
4.00000	54.12755
5.00000	57.41094
6.00000	60.51644
7.00000	63.47018
DISCHARGE AT TOP	66.29244

SUMMARY OF HYDRAULIC CALCULATIONS COTTONWOOD MALL TO CALABACILLAS ARROYO

							COLLON	NWOOD MALL	P P	CALABACILLAS	CILLA	S ARROY	0	1				
Station	Structure Diam.	Diam.	œ	Area	Vel.	ĸ	B£	Length	ĦĒ	싎	H	Hmb	Bt Lo	Total	HGL (dn) HGL (up)	Low Point	HV EGL (dn)	EGL (up)
21+86.02	ARROYO	0	1 7 7 1	20 40	7	0000	9100		0.0	00.00	00.00	00.00	00.00	0.00	5033.8	2	0.67 5034.49	5034.49
22+30.02	BEND	90 0	1.262	20.40	0.00		0.0016	44.00	70.0	0.09	00.0	00.00	0.00	0.09	033.89 5033.9	6	0.66 5034.55	5034.65
22+70.02	BEND	φ σ	7,000	20.40	0.50		0.0010	40.00		60.0	00.0	00.00	0.00	000	5034.05 5034.1	2	0.65 5034.71	5034.80
22+94.38	INLET 23-1	20 0	248.6		0.40	6388	0.0015	24.30	0.04	00.00	0.05	00.00	00.00		5034.19 5034.27		0.61 5034.84	5034.88
25+69.38	INLET 23	20 O	170 5	36.46			0.0014	00.672	2.0	00.0	0.04	00.00	0.00	0.04	5034.67 5035.02	8	0.3 5035.28	5035.32
25+83.67	BEND	p 0	1,000	20.40			0.000	•	20.0	0.04	00.00	00.00	0.00	0.00	035.03 5035.07	7	0.3 5035.34	5035.38
26+07.83	INLET E5	8 G	170.5	38.48	4.43		0.0007	٠, ١	70.0	00.00	0.01	00.00	0.00	0.02	035.09 5035.1	1	0.3 5035.40	5035.41
26+64.47	INLET E4	\$ 0 0	169.1	38.48	4.59	0388	0.000,0	00.04	20.0	00.00	0.01	00.00	00.00	0.04	035.15 5035.	17	0.29 5035.45	5035.46
27+10.11	BEND	0 0 7 7	7.00.7	04.00	20.4		0.000	, ,	7 0	0.03	00.0	00.00	0.00		5035.20 5035.2	4	0.29 5035.49	5035.53
28+42.83	INLET E3	χ γ 7	106.2	28.48			0.000	137.72	9 6	00.00	0.01	00.00	0.00	0.03	035.33 5035.3	4	0.29 5035.62	5035.63
28+80.48	INLET E2	\$ O	164 1	20.40	06.4			67.63		00.00	0.01	00.00	0.00		5035.36 5035.3	80	0.28 5035.65	5035.66
29+48.09	INLET E1	φ ¢	104.I	2	4.20		0.000	ه د	20.0	00.00	0.01	00.00	0.00	0.04	035.42 5035.4	3	0.28 5035.70	5035.71
2+76.20	MH 12	0 G	103.0	20.40	62.4			46.022	. O	0.09	0.29	0.02	0.01		5035.57 5035.6	9 5043.10	0.57 5035.85	5036.26
5+38.99	MH 11	90	118.9	19.63	9 1		1200.0	• (00.0	0.07	90.0	0.03	0.00	0.15	036.24 5036.4	4 5047.72	0.52 5036.81	5036.96
8+52.35	MH 10	09	104.7	19.63	7.7		0.0019	L J	0.0	00.00	80.0	0.02	0.00		5037.03 5037.22	5046.17	0.44 5037.55	5037.66
13+02.35	WH 9	9 ;	104./	19.63	5.33		0.0016	2 2	0.73	0.05	60.0	0.02	00.00	0.15 5	037.94 5038.17	5053.88	0.37 5038.39	5038.54
16+99.01	MH 8	υ r	7.1.	15.90	4.83		0.0015	390.00	0.0	00.00	60.0	0.02	00.0		5038.79 5038.9	8 5048.90	0.28 5039.15	5039.26
18+25.17	INLET B15	υ , 1	6.79	15.90	47.4		0.0012	סינ	0.15	00.00	0.01	00.00	0.00	0.01 5	039.13 5039.1	7	0.25 5039.41	5039.42
20+17.51	MH 7	54	64.3	15.90			0.0011	93.5 5.5	0.21	0.03	0.18	0.02	0.00	0.23	5039.37 5039.45	5044.00	0.41 5039.63	5039.86
22+59.76	9 HW	42	49.2	9.62			0.0024	42	0.58	90.0	60.0	0.02	0.00		5040.03 5040.2	9 5049.81	0.31 5040.44	5040.60
27+09.76	MH 5	42	43.2	9.62	4.49	H	0.0018	50.0	0.83	00.0	0.19	0.02	0.00		5041.12 5041.3	1 5054.91	0.33 5041.43	5041.64
29+41.41	MH 4	36	32.5	7.07	4.60	199	0.0024	231.65	0.55	0.03	0.18	0.01	0.00		5041.86 5042.2	6 5046.56	0.15 5042.19	5042.41
33+67 89		36	22.2	7.07	3.14	199	0.0011	426.48	0.47	0.03	0.14	0.01			3 5042.7	5046.14	0.29 5042.89	5043.07
20.00.00		30	21.3	4.91	4.34	410	0.0027	134.68	0.36		•				7 14 5042 7	00 1000	06 6043	7 7 7
35+02.57	MH 4B	18	14.6	1.77	8.26	105	0.0193	54.42	1.05		•	•	0	.05		07.		** *** ***
MH4C TO M 1+00.00	MEKA BRANCH MH 4C	5	-	0	,	96	000	1 22	87 0	00.00	00.00	0.01	00.00		5042.73 5042.80	5046.14	0.09 5042.89	5042.89
3+39.72	MH 4A	77	A () (> 0	4	> 0	0.01	00.0	00.0	0.00	0.02	5043.48 5043.5	0 5046.98	0.09 5043.58	5043.59
		12	1.9	0.79	2.42	36	0.0028	77.33	0.22				_	27.0				

LOW HGL(up) Point HV RGL(dn) EGL(up)	5040.33 5049.81 0.19 5040.44 504 5041.16 5044.20 0.53 5041.44 504	5038.11 5053.88 0.84 5038.39 503 5043.35 5061.59 0.49 5043.34 504 5046.36 5062.30 0.03 5046.28 504	5036.00 5043.10 1.88 5036.12 5037 5037.71 5043.10 0.7 5038.22 5038 5038.96 5044.66 0.91 5039.54 5039 5040.40 5043.89 0.90 5041.23 5041 5041.15 5044.29 0.85 5041.89 5042 5042.62 0.93 5042.52 5042 5043.75 5047.79 0.91 5044.49 5044 5053.90 5053.94 1.23 5044.49 5047 5057.42 5062.00 0.42 5053.28 5054 5057.42 5062.00 0.42 5057.78 5057 5059.24 5061.00 1.42 5059.44 5060	5039.32 5044.66 0.37 5039.54 503
Total Losses HGL(dn)	01 0.07 5040.03 0.92 02 0.25 5041.25 0.94 0.15	01 0.56 5037.94 4.39 00 0.50 5042.50 2.44 06 0.10 5045.79 0.08	00 1.76 5035.83 0.34 5036.34 1.13 5038.84 1.37 5040.32 0.0 0.11 5040.32 0.0 0.11 5040.32 0.0 0.17 5041.67 0.0 0.16 5042.30 0.0 0.17 5041.56 0.10 5041.67 0.10 5041.67	01 0.14 5038.84 0.56
j Elmb Ht	.00 0.01 0.	.39 0.03 0. .36 0.03 0.	.59 0.05 000 0.04 020 0.04 003 0.05 025 0.05 016 0.00 039 0.05 089 0.04 000 0.02 0.	.00 0.03 0.
RE RD RJ	0.95 0.05 0 0.92 0.06 0	0.12 0 4.39 0.11 0 2.44 0.04 0	0.34 0.12 1 1.13 0.04 0 0.52 0.16 0 0.94 0.10 0 1.16 0.00 1 1.16 0.04 1 1.16 0.04 1 1.16 0.04 1 1.19 0.10 1 1.10 0.11 1 1.10 1 1	0.10 0
Length	274.02 56.26 174.04	226.12 213.64 3100.00	41.20 382.39 306.31 133.22 124.50 62.00 171.83 450.00 450.00	83.90
ßf	36 0.0034 36 0.0167 65 0.0009	65 0.0194 65 0.0114 36 0.0008	529 0.0083 1966 0.0030 1436 0.0044 1436 0.0044 1006 0.0064 1006 0.0055 1006 0.0054 310 0.0131 105 0.0077 36 0.0443	105 0.0067
Vel. K	3.45 5.86 1.55	3 7.33 3 5.62 9 1.27	8.13 6.73 1 7.64 1 7.39 1 7.39 1 7.72 1 7.67 1 8.90 5.21 5.21	4.87
Q Area	6.1 1.77 4.6 0.79 1.9 1.23	9.0 1.23 6.9 1.23 1.0 0.79	48.3 5.94 107.0 15.90 96.0 12.57 95.5 12.57 92.9 12.57 74.3 9.62 74.3 9.62 73.8 9.62 35.4 3.98 9.2 1.77 9.2 1.77	8.6 1.77
Structure Diam.	MH 6 18 MH 6A 18 GRATE POND 15	MH 9 15 MH 21B 15 MH 21A 12	MH 12A 54 MH 21 48 MH 21 48 MH 19 48 MH 19 42 INLET A8 42 MH 17 42 MH 16 27 MH 15 MH 15 MH 11 18 MH 15 MH 11 18 MH 11 18 MH 11 18 MH 11 18	1215 MH 21 18
Station 8		8D A-8 1+00.00 M 3+26.12 M 5+39.76 M	BASIN A 1+00.00 1+41.20 M 5+23.59 M 8+29.90 M 9+63.12 M 11+49.62 I 13+21.45 M 15+37.40 M 24+37.40 M	MH21 TO MH21D 1+00.00 MH

1000		1	(ı				ï	ì			Total				
SCRCTOD	Station Structure Diam. Q Area Vel. K	DI am.	2	Area	V-1.	4	SI	Length	H	9		THE STATE OF	HC	Losses HGL (dn) HGL (up) Point	HGL (up)		HV BOL (do	EGL(dn) EGL(up)
MH 18 TO MH 18A	MH 18A																	•
1+00.00 MH 18	MH 18									00.00	00.00	0.02	0.08	0.09 5041.6	7 5042 52 6	5044 50 0	09 5042	12 5042 K1
		30	12.1	4.91	12.1 4.91 2.46		410 0.0009	131.68	0.11		•		•	0.11		0	7500 00	10.2500 2
2+31.68	MH 18C							_		0.00		0.01	0.01	0.08 5042.6	3 5042.65	044.86 0	16 5042.	3 5042.81
		24	10.0		3.14 3.18	226	226 0.0020	172.76	0.34					0.34				
4+04.43	MH 18B	č	5		1				•	0.02		0.01 0.01 0.00	00.0	0.04 5042.99 5043.06 5045.00 0.12 5043.15 5043.18	9 5043.06	045.00 0.	12 5043.	5 5043.18
00 00.7		7.7	0.0		3.14 2.11	977	GTOO'O	1.4.85	0.25			0		0.26			1	
2+79.08	MH 18A	,	ı		(•	0		,	0.05		0.56 0.02 0.05	0.05	0.67 5043.3	2 5043.43	045.59 0	68 5043.4	4 5044.11
		12	5.2		0.79 6.62	36	36 0.0213	70.00	1.49	_				1.49				
MH15 TO 1	MH15A																	
1+00.00 MH 15	MH 15							_		0.27	0.25	0.02	0.00	0.54 5052.0	5 5052,34 5	059.00 1.	48 5053.2	8 5053.82
		21	23.5	2.41	23.5 2.41 9.77		158 0.0220	117.22	2.58					2.58				
2+17.22	INLET A2							_		0.10		1.67 0.04	0.07	1.88 5054.92 5057.87 5058.25 0.41 5056.40 5058.28	2 5057.87 5	058.25 0.	41 5056.4	0 5058.28
		18	9.1	1.77	5.15	105	0.0075	327.40	2.46					2.46				
5+44.62	MH 15A							_		0.05		0.71 0.01 0.02	0.02	0.79 5060.33 5061.41 5062.50 0.11 5060.74 5061.52	3 5061.41 5	062.50 0.	11 5060.7	4 5061.52
		12	2.1	0.79	2.67	36	0.0035	200.00	0.69					69.0				
BP1E GRATE	TE	18	2.7	1.77	1.77 1.53	105	105 0.0007	178.92	0.12					0.12				

Remarks: 100YR EVENT, 100YR ELEV IN CBC Manning's 'n': 0.0130 STATIONS REFER TO PNP SHEETS

STORM DRAIN DATA - 100 YEAR, 24 HOUR STORM COTTONWOOD MALL TO CALABACILLAS ARROYO

Station	Structure D	iam.	Q	Area	Vel.	K	Sf	Length
21+86.02	ARROYO	0.4	240 1	20.40	C 47	63.00	0 0015	44.00
22+30.02	BEND	84	249.1	38.48	6.47	6388	0.0015	44.00
22+70.02	BEND	84	248.4	38.48	6.45	6388	0.0015	40.00
22+94.38	INLET 23-1	84	248.6	38.48	6.46	6388	0.0015	24.36
25+69.38	INLET 23	84	242.9	38.48	6.31	6388	0.0014	275.00
25+83.67		84	169.6	38.48	4.41	6388	0.0007	25.76
		84	169.6	38.48	4.41	6388	0.0007	26.61
26+07.83		84	167.8	38.48	4.36	6388	0.0007	56.64
26+64.47		84	165.9	38.48	4.31	6388	0.0007	52.94
27+10.11	BEND	84	165.9	38.48	4.31	6388	0.0007	132.72
28+42.83	INLET E3	84	166.4	38.48	4.32	6388	0.0007	37.65
28+80.48	INLET E2	84	165.1	38.48	4.29	6388	0.0007	67.61
29+48.09	INLET E1	84	164.3	38.48	4.27	6388	0.0007	220.34
2+76.20	MH 12	60	104.9	19.63	5.34	2604	0.0016	
5+38.99	MH 11							
8+52.35	MH 10	60	103.7	19.63	5.28	2604	0.0016	
13+02.35	MH 9	60	95.2	19.63	4.85	2604	0.0013	450.00
16+99.01	MH 8	54	77.8	15.90	4.89	1966	0.0016	396.66
18+25.17	INLET B15	54	69.3	15.90	4.36	1966	0.0012	125.00
20+17.51	MH 7	54	66.4	15.90	4.17	1966	0.0011	193.50
		42	52.2	9.62	5.43	1006	0.0027	242.25
22+59.76	MH 6	42	46.7	9.62	4.85	1006	0.0022	450.00
27+09.76	MH 5	36	37.3	7.07	5.28	667	0.0031	231.65
29+41.41	MH 4	36	25.7	7.07	3.64	667	0.0015	426.48
33+67.89	MH 4C	30	23.7	4.91	4.83	410	0.0033	134.68
35+02.57	MH 4B	21	19.1	2.41			0.0145	
						-50	0.0140	22.20

Station	Sti	ructure	Diam.	Q	Area	Vel.	ĸ	Sf	Length
MH4C TO	MH4A	BRANCH							
1+00.00	MH	4C	10	1 0	0 70	2 42	36	0.0028	239.72
3+39.72	MH	4A	12	1.9	0.79	2.42			
			12	1.9	0.79	2.42	36	0.0028	77.33
MH5 TO M	M5A 1	BRANCH							
1+00.00	MH	5	1.0	11 /	1 77	C 15	105	0.0118	364 60
4+64.60	МН	5B	18	11.4	1.77	6.45	105		364.60
5+86.64	MH	5A	12	6.7	0.79	8.53	36	0.0354	122.04
			12	3.6	0.79	4.58	36	0.0102	20.00
4+64.60	MH	5B							
5+48.64		5C	12	1.0	0.79	1.27	36	0.0008	84.04
3140.04	1111	50	12	1.0	0.79	1.27	36	0.0008	90.00
		a a							
MH4 TO N	⁄IH4D								
2+73.50	MH	4							
4+16.87	MH	4D	12	1.8	0.79	2.29	36	0.0026	143.37
GRATE BE			12 12	1.8	0.79	2.29	36 36	0.0026	98.46 95.00
									
MH4 TO 1	ин3								
2+73.50	MH	4	24	11.2	3.14	3.57	226	0.0025	87.00
1+86.50	MH	3B	24	7.0	3.14	2.23	226	0.0010	86.50
1+00.00	MH	3						0.0005	
			24	5.0	3.14	1.59	226	0.0005	50.00

Station	Structure	Diam.	Q	Area	Vel.	K	Sf	Length
мн7 то мн	7A							
1+00.00	MH 7	21	10.2	2.41	4.24	158	0.0041	212.93
3+12.93 INFLOW B2 GRATE B24 GRATE B23 GRATE B13		12 12 12 15	4.6 1.0 1.0 5.7	0.79 0.79 0.79 1.23	5.86 1.27 1.27 4.64	36 36 36 65	0.0167 0.0008 0.0008 0.0078	80.00 80.00 70.00 188.10
MH8 TO GR	ATE B16							
1+00.00 GRATE B16	MH 8	15	10.4	1.23	8.47	65	0.0259	198.06
BASIN C								
1+00.00	мн 9	36	19.2	7.07	2.72	667	0.0008	74.71
1+74.71	мн 9в	36	19.2	7.07	2.72	667	0.0008	277.34
4+52.05	мн 9А	24	13.2	3.14	4.20	226	0.0034	
BASINS B-	-9 & B-10							
1+00.00	мн 6	18	6.1	1.77	3.45	105	0.0034	274.02
3+74.02 MH6A TO 0 MH6A TO 0	MH 6A GRATE GRATE POND	12 15	4.6	0.79	5.86 1.55	36 65	0.0167	56.26

BASIN A 1+00.00 MH 12 33 65.0 5.94 10.94 529 0.0151 41.20 1+41.20 MH 12A 54 124.6 15.90 7.83 1966 0.0040 382.39 5+23.59 MH 21 48 99.5 12.57 7.92 1436 0.0047 133.22 9+63.12 MH 19 48 98.8 12.57 7.56 1436 0.0044 124.50 10+87.62 MH 18 42 75.0 9.62 7.80 1006 0.0044 124.50 11+49.62 TNLET A8 42 67.5 9.62 7.02 1006 0.0045 171.83 13+21.45 MH 17 42 66.3 9.62 7.02 1006 0.0045 171.83 15+37.40 MH 16 27 31.0 3.98 7.80 310 0.0104 450.00 24+37.40 MH 14 18 10.7 1.77 6.05 105 0.0104 207.64 <th>Station</th> <th>Structure</th> <th>Diam.</th> <th>Q</th> <th>Area</th> <th>Vel.</th> <th>K</th> <th>Sf</th> <th>Length</th>	Station	Structure	Diam.	Q	Area	Vel.	K	Sf	Length
1+00.00 MH 12 33 65.0 5.94 10.94 529 0.0151 41.20 1+41.20 MH 12A 54 124.6 15.90 7.83 1966 0.0040 382.39 5+23.59 MH 21 48 99.5 12.57 7.92 1436 0.0048 306.31 8+29.90 MH 20 48 98.8 12.57 7.86 1436 0.0044 124.50 9+63.12 MH 19 48 95.4 12.57 7.59 1436 0.0044 124.50 10+87.62 MH 18 42 75.0 9.62 7.80 1006 0.0045 62.00 11+49.62 INLET A8 42 66.3 9.62 7.02 1006 0.0045 171.83 15+37.40 MH 16 27 31.0 3.98 7.80 310 0.0104 450.00 24+37.40 MH 14 18 10.7 1.77 6.05 105 0.0104 207.64 26+45.04 MH 21 27 25.0 3.98 6.29 310 0.0065 85.00	DACIN A								
1+41.20 MH 12A 33 65.0 5.94 10.94 529 0.0151 41.20 5+23.59 MH 21 48 99.5 12.57 7.92 1436 0.0048 306.31 8+29.90 MH 20 48 98.8 12.57 7.86 1436 0.0047 133.22 9+63.12 MH 19 48 95.4 12.57 7.59 1436 0.0044 124.50 10+87.62 MH 18 42 75.0 9.62 7.80 1006 0.0045 62.00 11+49.62 INLET A8 42 67.5 9.62 7.02 1006 0.0045 171.83 13+21.45 MH 17 42 66.3 9.62 6.89 1006 0.0045 171.83 15+37.40 MH 15 18 10.7 1.77 6.05 105 0.0104 450.00 24+37.40 MH 14 18 10.7 1.77 6.05 105 0.0104 450.00 MH21T 27 25.0 3.	BASIN A								
1+41.20 MH 12A 54 124.6 15.90 7.83 1966 0.0040 382.39 5+23.59 MH 21 48 99.5 12.57 7.92 1436 0.0048 306.31 8+29.90 MH 20 48 98.8 12.57 7.86 1436 0.0047 133.22 9+63.12 MH 19 48 95.4 12.57 7.59 1436 0.0044 124.50 10+87.62 MH 18 42 75.0 9.62 7.80 1006 0.0045 62.00 11+49.62 INLET A8 42 67.5 9.62 7.02 1006 0.0045 171.83 13+21.45 MH 16 27 31.0 3.98 7.80 310 0.0043 215.95 15+37.40 MH 15 18 10.7 1.77 6.05 105 0.0104 450.00 26+45.04 MH 13 15 9.5 1.23 7.74 65 0.0216 40.00									

Station	Structure	Diam.	Q	Area	Vel.	K	Sf	Length
MH 18 TO	MH 18A							
1+00.00	MH 18	30	20.1	4.91	4.09	410	0.0024	131.68
2+31.68 4+04.43	MH 18C	24	15.3	3.14	4.87	226	0.0046	172.76
5+79.08	MH 18A	24	8.7	3.14	2.77	226	0.0015	
		12	5.2	0.79	6.62	36	0.0213	70.00
MH15 TO N	MH15A							
1+00.00	MH 15	21	18.8	2.41	7.82	158	0.0141	117.22
2+17.22	INLET A2	15	9.1	1.23	7.42	65	0.0198	327.40
5+44.62 BP1E GRAS	MH 15A TE	12 18	4.0	0.79 1.77	5.09 1.53	36 105	0.0126 0.0007	

Remarks: 100YR EVENT, 100YR ELEV

STATIONS REFER TO PNP SHEETS

STORM DRAIN DATA - 10 YEAR, 24 HOUR STORM COTTONWOOD MALL TO CALABACILLAS ARROYO

Station	Structure Diam.	Q	Area	Vel.	K	Sf	Length
21+86.02	ARROYO	175 0	20 40	4 55	C2.00	-	4.4 0.0
22+30.02	BEND	175.2	38.48	4.55	6388	0.0008	44.00
22+70.02	BEND	174.8	38.48	4.54	6388	0.0007	40.00
22+94.38	84 INLET 23-1	175.4	38.48	4.56	6388	0.0008	24.36
25+69.38	84 INLET 23	174.4	38.48	4.53	6388	0.0007	275.00
25+83.67	84 BEND	130.3	38.48	3.39	6388	0.0004	25.76
26+07.83	84 INLET E5	130.3	38.48	3.39	6388	0.0004	26.61
26+64.47	84 INLET E4	129.3	38.48	3.36	6388	0.0004	56.64
27+10.11	BEND 84	126.5	38.48	3.29	6388	0.0004	52.94
	84	126.5	38.48	3.29	6388	0.0004	132.72
28+42.83	INLET E3	125.4	38.48	3.26	6388	0.0004	37.65
28+80.48	INLET E2 84	123.9	38.48	3.22	6388	0.0004	67.61
29+48.09	INLET E1 84	123.5	38.48	3.21	6388	0.0004	220.34
2+76.20	MH 12 60	71.9	19.63	3.66	2604	0.0008	262.79
5+38.99	MH 11 60	71.0	19.63	3.62	2604	0.0007	313.36
8+52.35	MH 10 60	66.1	19.63	3.37	2604	0.0006	450.00
13+02.35	MH 9 54	51.7	15.90	3.25	1966	0.0007	396.66
16+99.01	MH 8 54	46.0	15.90	2.89	1966	0.0005	125.00
18+25.17	INLET B15						
20+17.51	MH 7	44.3	15.90	2.79	1966	0.0005	193.50
22+59.76	42 MH 6	35.1	9.62	3.65	1006	0.0012	242.25
27+09.76	42 MH 5	31.3	9.62	3.25	1006	0.0010	450.00
29+41.41	36 MH 4	25.1	7.07	3.55	667	0.0014	231.65
33+67.89	36 MH 4C	16.6	7.07	2.35	667	0.0006	426.48
35+02.57	30 MH 4B	15.3	4.91	3.12	410	0.0014	134.68
55,02.57	21	12.4	2.41	5.16	158	0.0061	54.42

Station	St:	ructure	Diam.	Q	Area	Vel.	K	Sf	Length
MH4C TO M	H4A	BRANCH							
1+00.00	МН	4C	1.0	1 2	0.70	1 66	2.0	- 0.013	220 72
3+39.72	MH	4A	12	1.3	0.79	1.66	36	0.0013	239.72
			12	1.3	0.79	1.66	36	0.0013	77.33
мн5 то мн	5 A 1	BRANCH							
1+00.00	MH	5							
4+64.60	MH	5B	18	7.5	1.77	4.24	105	0.0051	364.60
5+86.64		5A	12	4.5	0.79	5.73	36	0.0160	122.04
J+00.04	1111	JA	12	2.4	0.79	3.06	36	0.0045	20.00
4+64.60	MH	5B							
5+48.64	MH	5C	12	1.0	0.79	1.27	36	0.0008	84.04
			12	1.0	0.79	1.27	36	0.0008	90.00
MH4 TO MH	4D								
2+73.50	MH	4	12	1.1	0.79	1 40	26	0.0010	143.37
4+16.87	MH	4D				1.40	36		
GRATE B3 GRATE B27			12 12	1.1 0.2	0.79 0.79	1.40 0.25	36 36	0.0010	98.46 95.00
мн4 то мн	3								
2+73.50	MH	4	2.4	0 1	3.14	2 67	226	0.0014	97 00
1+86.50	МН	3B	24	8.4			226		87.00
1+00.00	МН	3	24	4.6	3.14	1.46	226	0.0004	86.50
			24	4.2	3.14	1.34	226	0.0003	90.00

Station	Structure	e Diam.	Q	Area	Vel.	K	Sf	Length
MH7 TO MH	7A							
1+00.00 3+12.93 INFLOW B20	MH 7A	21 12	6.8	2.41	2.83	158 36	0.0018	212.93
GRATE B24 GRATE B23 GRATE B13	~~	12 12 15	0.2 0.2 3.6	0.79 0.79 1.23	0.25 0.25 2.93	36 36 65	0.0000 0.0000 0.0031	80.00 70.00 188.10
MH8 TO GR2	ATE B16 MH 8							. *
GRATE B16		15	6.8	1.23	5.54	65	0.0111	198.06
BASIN C								
1+00.00 1+74.71	MH 9B	36	14.3	7.07	2.02	667	0.0005	74.71
4+52.05	MH 9A	36	14.3	7.07	2.02	667	0.0005	277.34
		24	12.0	3.14	3.82	226	0.0028	50.26
BASINS B-S	9 & B-10							
1+00.00	мн 6	-	4 0					
3+74.02	мн ба	18	4.3	1.77	2.43	105	0.0017	
MH6A TO GI MH6A TO GI		12 15	2.9 1.7	0.79 1.23	3.69 1.39	3 6 6 5	0.0066 0.0007	56.26 174.04

Station	Structure	Diam.	Q	Area	Vel.	K	Sf	Length
BASIN A								
1+00.00	MH 12		.	5 0 4	• • •		_	
1+41.20	MH 12A	33	54.0	5.94	9.09	529	0.0104	41.20
5+23.59	MH 21	54	78.4	15.90	4.93	1966	0.0016	382.39
8+29.90	MH 20	48	63.3	12.57	5.04	1436	0.0019	306.31
9+63.12	MH 19	48	63.2	12.57	5.03	1436	0.0019	133.22
10+87.62	MH 18	48	61.2	12.57	4.87	1436	0.0018	124.50
11+49.62	INLET A8	42	48.0	9.62	4.99	1006	0.0023	62.00
		42	43.2	9.62	4.49	1006	0.0018	171.83
13+21.45	MH 17	42	42.4	9.62	4.41	1006	0.0018	215.95
15+37.40	MH 16	27	19.9	3.98	5.00	310	0.0041	450.00
19+87.40	MH 15	18	6.9	1.77	3.90	105	0.0043	450.00
24+37.40	MH 14	18	6.9	1.77	3.90	105	0.0043	207.64
26+45.04	MH 13	15	6.0	1.23	4.89	65	0.0086	40.00
		13	0.0	1.23	4.03	65	0.0000	40.00
MH21 TO M	IH21A							
1+00.00	MH 21	27	1 (1	2 00	4 05	210	0 0007	05 00
1+83.90	INLET A12	27	16.1	3.98	4.05	310	0.0027	85.00
4+12.93	MH 21D	27	12.1	3.98	3.04	310	0.0015	227.93
6+44.33	MH 21C	15	6.0	1.23	4.89	65	0.0086	231.40
9+41.23	MH 21B	15	6.0	1.23	4.89	65	0.0086	296.90
11+54.87	MH 21A	15	4.6	1.23	3.75	65	0.0051	213.64
11174.07	mi ain	12	1.0	0.79	1.27	36	0.0008	100.00

Station	Structure	Diam.	Q	Area	Vel.	K	Sf	Length
MH 18 TO	MH 18A							
1+00.00	MH 18	2.0				11	_	
2+31.68	MH 18C	30	13.2	4.91	2.69	410	0.0010	131.68
		24	10.1	3.14	3.21	226	0.0020	172.76
4+04.43		24	5.8	3.14	1.85	226	0.0007	174.85
5+79.08	MH 18A	12	3.5	0.79	4.46	36	0.0097	70.00
MH15 TO MH15A								
1+00.00	MH 15							
2+17.22	INLET A2	21	12.2	2.41	5.07	158	0.0059	117.22
		15	6.0	1.23	4.89	65	0.0086	327.40
5+44.62		12	2.1	0.79	2.67	36	0.0035	200.00
BP1E GRATE		18	1.6	1.77	0.91	105	0.0033	178.92

Remarks: 10 YEAR EVENT, 10 YEAR ELEV STATIONS REFER TO PNP SHEETS