

THOMPSON Engineering Consultants, Inc.

February 11, 2014

Mr. Curtis Cherne, P.E.
Principal Engineer, Planning Department
Development and Building Services
City of Albuquerque
P.O. Box 1293
Albuquerque, NM 87103

Re: ADDITIONAL HYDROLOGIC ANALYSIS FOR THE AMENDMENT TO THE TRAILS DRAINAGE MASTER PLAN

Dear Mr. Cherne:

At our last meeting on the review of the Trails DMP, you requested that we analyze developed conditions hydrology with no orifice plates downstream of Ponds D, F, and G to determine the affect on the Pond K detention volume. We have completed this AHYMO model and have included the AHYMO summary table with this letter.

The table below gives the results of the AHYMO model in the November 2013 DMP compared to the February 2014 AHYMO model removing the orifice plates downstream of Ponds D, F, and G. Please note that the interim capacity of Pond K is 14.84 ac-ft with the current configuration of the original Pond K and the temporary berm to the north. As Unit 4 develops Pond K will be revised to reduce the footprint to maximize the developable area in Unit 4.

POND	CAPACITY (ac-ft)	NOV 13 VOLUME (ac-ft)	FEB 14 VOLUME (ac-ft)
D	6.24	5.079	2.348
F	11.76	11.001	6.320
G	7.21	2.955	7.858
K	14.84 (INTERIM)	8.203	16.526

In comparing the results of the two AHYMO models the February 2014 model increases the volume in Ponds G and K significantly and reduces the volume in Ponds D and F. The February 2014 model shows that Ponds G and K capacities are exceeded and therefore discharge over the emergency spillway, while only about 50% of the capacity of Ponds D and F is being used.

Another consequence of the February 2014 model is that the capacity of the storm drains downstream of Ponds D and F are exceeded surcharging the storm drain system. The HGL is higher than the manhole rim elevation resulting in storm water spilling into the streets. Downstream of Pond F the HGL is as much as 3.75 feet higher than the manhole rim elevation, and downstream of Pond D the HGL is as much as 25.6 feet higher than the manhole rim elevation (see attached HGL spreadsheets). Therefore, orifice plates are required in the storm drains downstream of Ponds D and F to limit the peak flow discharging from these ponds to the downstream storm drains.

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In conclusion, removing the orifice plates results in surcharging the downstream storm drains and the capacity of Ponds G and K being exceeded. Orifice plates are required to limit the amount of flow discharging from the upstream ponds to the downstream storm drains so that their capacity is not exceeded. Also, orifice plates control the peak flow discharging from Ponds D, F, and G, which results in maximizing the detention volume in these ponds. This follows the previous DMP, which includes an intricate system of storm drains and surge ponds with orifice plates that was analyzed and designed by Wilson and Company in 2004 and constructed in 2006. Therefore, this update of the Trails DMP should use the November 2013 model maximizing the available volume in Ponds D, F, and G while limiting the volume in Pond K.

If you should have any questions about this additional analysis, please call.

Sincerely,



David B. Thompson, P.E.

COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	CFS PER ACRE	PAGE = 3 NOTATION
COMPUTE NM HYD	BASIN.E1	-	30	.03341	58.79	2.410	1.35259	2.749 PER IMP= 34.00
ADD HYD	OFFB.E1	72&30	73	.13389	61.76	5.600	.78423	.721 PER IMP= 64.00
COMPUTE NM HYD	BASIN.E2	-	32	.01348	27.42	1.324	1.84145	3.178 PER IMP= 64.00
ROUTE MCUNGE	RUE.E2	32	76	.01348	25.29	1.314	1.82775	2.932 CCODE = .1
COMPUTE NM HYD	BASIN.E3	-	33	.01197	22.82	1.030	1.61331	2.978 PER IMP= 50.00
COMPUTE NM HYD	BASIN.E4	-	34	.00577	13.11	.697	2.26513	3.550 PER IMP= 90.00
ADD HYD	E3.E4	33&34	74	.01774	35.93	1.727	1.82529	3.164 PER IMP=
ADD HYD	E3E4.E1BOFF	74&73	75	.15163	97.69	7.327	.90603	1.007 CCODE = .0
ROUTE MCUNGE	RTE.E1E4	75	77	.15163	97.69	7.327	.98127	1.160 PER IMP= 42.00
ADD HYD	E1E4.E2	77&76	78	.16511	122.58	8.641	1.48295	2.863 PER IMP= 42.00
COMPUTE NM HYD	BASIN.E5	-	35	.04042	80.67	3.482	1.08687	1.519 PER IMP=
ADD HYD	E1E4.E5	78&35	80	.20913	203.25	12.123	1.08687	1.519 PER IMP=
COMPUTE NM HYD	BASIN.E6	-	36	.00488	11.09	.590	2.26512	3.550 PER IMP= 90.00
ADD HYD	E1E6	80&36	40	.21401	214.33	12.712	1.11374	1.565 PER IMP=
ROUTE RESERVOIR	BYPASS E	40	61	.10345	15.50	6.145	1.11374	1.300 PER IMP=
DIVIDE HYD	SURGE E and POND E	62	61	.11056	19.83	6.574	1.11374	2.810 PER IMP=
ADD HYD	TOTAL E	61&37	37	.11056	6.83	6.574	1.11484	.097 AC-FT= 6.053
ROUTE MCUNGE	RTE.PONDE	40	38	.21401	22.33	12.718	1.11427	2.400 PER IMP=
COMPUTE NM HYD	BASIN.P	-	32	.00845	10.08	.327	1.72623	1.865 PER IMP= 7.00
COMPUTE NM HYD	BASIN.H1	-	33	.01825	37.78	1.856	1.90663	1.500 PER IMP= 68.00
ADD HYD	PONDE.H1	38&33	43	.23226	57.68	14.576	1.17670	.388 PER IMP=
COMPUTE NM HYD	BASIN.H2	-	34	.00836	19.16	1.018	2.28220	1.500 PER IMP=
ADD HYD	P.H2	32&34	44	.01681	29.25	1.345	1.50001	2.718 PER IMP=
ADD HYD	PH2.H1	44&43	45	.24907	86.93	15.921	1.19852	1.500 PER IMP=
COMPUTE NM HYD	BASIN.H3	-	35	.01191	23.79	1.128	1.77627	1.500 PER IMP=
ADD HYD	PH1H3	45&35	46	.26098	110.72	17.049	1.22489	1.500 PER IMP=
ROUTE RESERVOIR	BYPASS.H	46	47	.21051	21.60	13.752	1.22489	1.300 PER IMP=
ROUTE MCUNGE	SURGE.H and POND.H	48	30	.05047	89.12	3.297	1.22489	1.500 PER IMP=
ADD HYD	BYPASS.RTE.H	49&47	31	.05047	5.20	3.297	1.22489	2.300 PER IMP=
COMPUTE NM HYD	BASIN.K1	-	20	.02673	50.54	2.579	1.22499	2.400 PER IMP=
ADD HYD	POND.K1	31&20	32	.28771	73.46	19.628	1.22490	2.400 PER IMP=
ROUTE MCUNGE	RTE.K1	32	33	.28771	73.46	19.628	1.22490	2.400 PER IMP=
COMPUTE NM HYD	BASIN.K2	-	21	.01486	29.39	1.537	1.93922	1.500 PER IMP=
ADD HYD	K1.K2	33&21	34	.30257	102.85	21.165	1.31157	1.500 PER IMP=
COMPUTE NM HYD	BASIN.K3	-	22	.00648	14.12	.783	2.26512	1.500 PER IMP=
ADD HYD	POND.K3	79&22	24	.61872	108.40	43.460	1.31704	2.700 PER IMP=
COMPUTE NM HYD	BASIN.K4	-	23	.01340	18.28	.527	.73726	1.500 PER IMP= .00
ADD HYD	K3.K4	24&23	25	.63212	108.63	43.987	1.30475	.269 PER IMP= .0
COMPUTE NM HYD	BASIN.J1	-	81	.00517	11.04	.557	2.02669	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J2	-	82	.01706	36.40	1.839	2.02669	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J3	-	83	.00580	11.70	.560	1.80886	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J4	-	84	.01006	21.47	1.084	2.02069	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J5	-	85	.00134	3.05	.162	2.26513	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J6	-	86	.00422	9.59	.510	2.26512	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J7	-	87	.00444	10.09	.536	2.26512	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J8	-	88	.00903	12.31	.355	.73726	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J9	-	89	.00548	12.20	.638	2.18365	1.500 PER IMP= .0
COMPUTE NM HYD	BASIN.J12	-	12	.01419	10.65	.314	.41534	1.500 PER IMP= .0
ADD HYD	J10J11.J6	86&10	11	.01783	38.60	2.144	.25428	1.500 PER IMP= .0

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COMMAND	HYDROGRAPH IDENTIFICATION NO.	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 4 NOTATION
ADD HYD	J10J11J6.J9	11&89	95	.023331	50.80	2.782	2.23766	1.500	3.405
ADD HYD	J10J11J6J9.J	85&95	90	.02465	53.86	2.944	2.23914	1.500	3.414
ROUTE MCUNGE	RTE.J5J6	90	91	.02465	53.86	2.944	2.23914	1.500	3.414 CCODE = .0
ADD HYD	J1.J4	81&84	93	.01523	32.51	1.641	2.02065	1.500	3.335
ADD HYD	J1J4.J5J6J9	91&93	94	.03988	86.37	4.585	2.15570	1.500	3.384
ROUTE MCUNGE	RTE.J145J9	94	92	.03988	86.37	4.585	2.15570	1.500	3.384 CCODE = .0
ADD HYD	J2.J3	82&83	95	.02286	48.10	2.398	1.96692	1.500	3.288
ADD HYD	J2J3.J7	95&87	94	.02730	58.19	2.934	2.01541	1.500	3.330
ADD HYD	J1456J9.J237	94&92	96	.06718	144.56	7.519	2.09869	1.500	3.362
ADD HYD	J1J7.J8	96&88	97	.07621	156.87	7.875	1.93737	1.500	3.216
ADD HYD	J1J8.J12	97&12	98	.09040	167.52	8.189	1.69846	1.500	2.895
DIVIDE HYD	BYPASS J	98	83	.04558	26.34	4.129	1.69846	1.300	.903
ROUTE RESERVOIR	SURGE and POND J	84	84	.04482	141.18	4.060	1.69846	1.500	4.922
ADD HYD	BYPASS SURGE	90&83	97	.09040	6.05	4.059	1.69831	2.100	.211 AC-FT= 3.771
ROUTE MCUNGE	RTE.J5J6	97	91	.09040	32.39	8.188	1.69835	2.000	.560
COMPUTE NM HYD	BASIN.K5	-	30	.02364	47.63	2.281	1.69667	2.100	.559 CCODE = .1
COMPUTE NM HYD	BASIN.K6	-	31	.00220	5.01	.266	2.26512	1.500	3.148 PER IMP= 62.00
ADD HYD	K5.K6	30&31	41	.02584	52.64	2.546	1.84768	1.500	3.555 PER IMP= 90.00
ADD HYD	K5K6.PONDJ.R3	41&91	43	.11624	80.50	10.726	1.73022	1.500	1.082
ADD HYD	K5K6PONDJ.R3	43&25	44	.74836	152.43	54.714	1.37084	1.500	.318
ADD HYD	PONDJK13.K1R	34&44	96	1.05093	255.27	75.878	1.35377	1.500	.380
DIVIDE HYD	BYPASS K	96	97	.67318	42.18	48.605	1.35377	1.300	.098
ROUTE RESERVOIR	SURGE K and POND K	98	70	.37775	213.09	27.274	1.35377	1.500	.881
ADD HYD	BYPASS.ROUTE	70&97	99	1.05093	39.60	27.273	1.35374	3.900	.164 AC-FT= 16.526
ROUTE MCUNGE	RTE.PONDK	99	1	1.05093	81.78	75.878	1.35376	3.900	.122
COMPUTE NM HYD	UNIVROWNORTH	-	2	.00727	80.03	75.641	1.34953	4.500	.119 CCODE = .2
ADD HYD	UNIVN. PONDK	1& 2	3	1.05820	16.51	.878	2.26512	1.500	3.550 PER IMP= 90.00
ROUTE MCUNGE	RTE.UNIVN	3	4	1.05820	80.16	76.518	1.35582	4.500	.118
COMPUTE NM HYD	UNIVROWSOUTH	-	5	.00727	79.15	76.408	1.35387	4.900	.117 CCODE = .2
ADD HYD	UNIVNS. PONDK	4& 5	6	1.06546	16.51	.878	2.26512	1.500	3.550 PER IMP= 90.00
					79.28	77.286	1.36008	4.900	.116

*S*****END OF TRAILS DRAINAGE ANALYSIS

FINISH

**SUMMARY OF HYDRAULIC CALCULATIONS
CLOSED CONDUIT**

PROJECT: TRAILS DMP														LINE: POND G TO POND F			PROJECT: TRAILS DMP														LINE: POND G TO POND F			DATE: 2/10/14 SHEET: 1 of 1			BY: DBT							
100-year	STATION		STRUCTURE		D		Q		A		V		K		Sf		L		DELT A		D		ANGLE		JUNCTION		LOSSES		ht		hmh		ht		hmisc		SUM		E.G.		H.G.		GROUND ELEV.	
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	Comment:																					
POND G	60	126	19.64	6.41	2606	0.0023	158																																					
MH	54	126	15.90	7.92	1968	0.0041	374																																					
MH	48	126	12.57	10.03	1437	0.0077	238																																					
MH	48	126	12.57	10.03	1437	0.0077	267																																					
MH	48	0	12.57	0.00	1437	0.0000	88																																					
MH	12	0	0.79	0.00	35.63	0.0000	600																																					
REMARKS:																																												
Manning's n: 0.013																																												

POND F TO POND D

SUMMARY OF HYDRAULIC CALCULATIONS													BY: DBT						
CLOSED CONDUIT													DATE: 2/10/14						
PROJECT: TRAILS DMP		LINE: POND F TO POND D		LOSSES									SHEET: 1 of 1						
100 year	1	2	3	4	5	6	7	8	9	10	11	12	JUNCTION	ht	hmisc	SUM			
STATION	STRUCT	D	Q	A	V	K		Sf	L	DELTA	D	ANGLE	hf	hb	hj	E.G.			
POND F		30	64.5	4.91	13.14	410.3	0.0247	280					0.00		0.00	0.00	5423.83	2.68	5421.15
MH		30	64.5	4.91	13.14	410.3	0.0247	55	90				6.92	0.54	0.00	0.13	5430.75	2.68	5428.07
MH		30	64.5	4.91	13.14	410.3	0.0247		90				1.36				5431.42	2.68	5428.74
MH		30	64.5	4.91	13.14	410.3	0.0247		903				0.54	0.00	0.13	0.00	5432.78	2.68	5430.10
MH		30	64.5	4.91	13.14	410.3	0.0247						22.31				5433.45	2.68	5430.77
MH		30	0	4.91	0.00	410.3	0.0000	320					0.00	0.00	0.00	0.00	5435.76	2.68	5430.80
MH		30	0	4.91	0.00	410.3	0.0000	235					0.00	0.00	0.00	0.00	5435.76	0.00	5430.14
MH		12	0	0.79	0.00	35.63	0.0000	600					0.00	0.00	0.00	0.00	5455.76	0.00	5455.76
REMARKS:													Manning's n: 0.013						