CITY OF ALBUQUERQUE



Richard J. Berry, Mayor

September 20, 2016

Scott J. Steffen, P.E. Bohannan Huston, Inc. 7500 Jefferson St NE Courtyard 1 Albuquerque, NM, 87109

RE: Taos II @ The Trails Grading and Drainage Plan & Report Stamp Date 7-13-16 (File:C09D00G1)

Dear Mr. Steffen:

Based upon the information provided in your submittal received 7-14-2016, the above referenced Grading and Drainage Plan & Report is approved for Preliminary Plat with the following conditions:

PO Box 1293

Albuquerque

New Mexico 87103

www.cabq.gov

- 1. The Work Order Set will need to include sufficient survey information to show that the tie in to the existing Hearthstone Roadway section is completed with a smooth transition.
- 2. If the project is phased, the Work Order Set will be expected to include temporary/desiltation ponds where needed.
- 3. Forward a copy of any correspondence related to the permission for grading that will be needed for the perched access road from Oakridge St. on the adjacent property prior to Hydrology's sign off of the DRC Set.
- 4. The DRC Set will need to include enough survey information at the West end of Hearthstone to ensure that a smooth transition to the existing road.

Prior to approval for Grading Permit, the following items will need to be addressed. Segments of the existing Grading and Drainage Plan & Report can be replaced where needed:

 Consolidate the discrepancy with the allowable discharge as described by the Update to the Amendment to the Drainage Master Plan, by RESPEC and Thompson Engineering, dated 9-14-2016. The allowable discharge on Table 7 is approximately 52 cfs, and the subdivision is proposed to discharge approximately 58 cfs. Although the discrepancy might not be significant, Pond F5, (the outfall for Taos II), will not have much freeboard to work with.

CITY OF ALBUQUERQUE



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- 2. The improvements referenced on the Infrastructure List need to be shown on the Grading Plan:
 - a. The Improvements related to Ponds F, F5 and D. The orifice plate can be included by reference or as a specific note/exhibit of the improvements required.
 - b. The outfall conditions into Pond F5. Note that the Drainage Master Plan elevations are based on NGVD 29 datum.
- 3. It is not clear where the wall drain detail will be used since it appears that all lots drain to the roadway. Any planned rear-lot ponding would require an easement.
- 4. An approved ESC Plan will be required.

Principal Engineer, Planning Dept. Development Review Services

If you have any questions, you can contact me at 924-3986.

PO Box 1293

Albuquerque

New Mexico 87103

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Orig: Drainage file

Sincerely,

Abiel Carrillo, P.E.

DRAINAGE REPORT FOR TAOS II AT THE TRAILS SUBDIVISION

JULY 2016

Prepared for: Real Capital Solutions 371 Centennial Parkway – Suite 200 Louisville, CO 80027

Prepared by:

Bohannan 🛦 Huston

Engineering Spatial Data Advanced Technologies



DRAINAGE REPORT FOR TAOS II @ THE TRAILS SUBDIVISION

JULY 13, 2016

Prepared for: **REAL CAPITAL SOLUTIONS 371 CENTENNIAL PARKWAY, SUITE 200 LOUISVILLE, CO 80027**

> Prepared by: BOHANNAN HUSTON, INC. COURTYARD I 7500 JEFFERSON STREET NE ALBUQUERQUE, NM 87109

Prepared By:

Scott J. Steffen, P.E. Vice President



Bohannan 🛦 Huston

Date

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APPENDIX B – STREET HYDRAULICS AND STORM DRAIN INLET ANALYSIS

EXHIBITS

- EXHIBIT 1 PRELIMINARY PLAT
- EXHIBIT 2 BASIN MAP
- EXHIBIT 3 GRADING PLAN
- **EXHIBIT 4 STORM DRAIN CAPACITY CALCULATIONS**
- EXHIBIT 5 SUPPLEMENTAL EXHIBITS FROM TRAILS UNITS 1-3 DMP

I. PURPOSE

This report establishes a drainage management plan for Taos II at the Trails. The proposed development consists of 109 single family detached residential lots on approximately 17.4 acres. This project is located within the Volcano Trails Sector Plan area, in northwest Albuquerque, east of The Trails Heritage Unit 2 and west of Tract 2 The Trails Unit 2. Taos II at the Trails is in the Trails Units 1-3 Drainage Master Plan (DMP) area and has free discharge of developed flows to Pond F5. Flows from Pond F5 are conveyed through an existing 42-inch storm drain that runs through the Sierra at the Trails subdivision, ultimately reaching the Trails storm drain outfall in Universe Boulevard. The Trails drainage outfall is to the Boca Negra Dam through a storm drain in Universe Boulevard. Flows in excess of the storm drain capacity surge to detention ponds east of Universe Boulevard. This report is submitted in support of grading approval and preliminary plat approval by the DRB.

II. CONCEPTS AND METHODOLOGIES

Drainage conditions were analyzed utilizing the 100-year, 24-hour storm event (P₆₀=1.84 in, P₃₆₀=2.20 in, P₁₄₄₀=2.66 in), in accordance with the City of Albuquerque DPM. The use of the 24-hour storm event is consistent with the Trails Units 1-3 DMP. The Aridlands Hydrologic Model (AHYMO) was utilized to determine peak flow rates for design of the storm drainage improvements within the project. The results are included in Appendix A. Street capacity and storm drain inlet calculations supporting this study are located in Appendix B.

The following document was referenced in the preparation of this report:

• Update to the Amendment to the Drainage Master Plan for the Trails Units 1, 2, and 3 prepared by Respec, Inc., dated July 2016.

III. SITE LOCATION AND CHARACTERISTICS

Taos II at the Trails is currently undeveloped with grades ranging from one percent to three percent. The site generally slopes from west to east. It is bounded by Paseo Del Norte Blvd to the north, Tract 2 at the Trails Unit 2 to the east, Heritage at the Trails Unit 2 to the west and Tract OS-3 to the south. Access to Taos II will be from Hearthstone Road through the Heritage subdivision and from Oakridge Street through Tract 2 at the Trails.

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IV. DEVELOPED HYDRAULIC AND HYDROLOGIC CONDITIONS

Taos II at the Trails is a proposed single-family residential development with 109 lots on 17.4 acres. Proposed street and lot configurations are shown on the *Preliminary Plat*, **Exhibit 1.** Taos II at the Trails, is represented by Basin D5, F6, and F8 in the Trails Units 1-3 DMP. The DMP allows for full discharge of developed flows from Taos II at the Trails to the storm drain southeast of the development.

The percent impervious land treatment for the proposed conditions is determined from Table A-5 of the DPM, Section 22.2. The composite percent impervious land treatment value used in the Trails DMP AHYMO analysis that encompasses Taos II is 59.0%. The composite percent impervious land treatment for Taos II at the Trails' (D varies between 42-60% for sub basins) is 58.9%.

A. OFFSITE FLOWS

Limited offsite flows reach Taos II at the Trails. No flows reach the site from Paseo del Norte (PdN) to the north, as the site is higher in elevation than Paseo del Norte. DMP Basin J10 (14.3 cfs) identifies the flows in PdN across the Taos II frontage for the full build out scenario for PdN. The DMP identifies storm drain and inlet requirements for PdN (see Exhibit 5). A single inlet is required in PdN at the Taos II east boundary. There is no storm drain required in PdN across the Taos frontage. PdN is currently only 2 lanes wide with no permanent curb and gutter or storm drain improvements. Construction of PdN improvements across existing Trails subdivision frontage has been deferred so that the PdN can be built as a single project in lieu of piece meal construction with the development each Tract. This same approach holds for Taos II.

No flows reach the site from the east as Taos II at the Trails is greater in elevation than Tract 2. There is no flow from the south as Taos II is higher in elevation than Tract OS-3. Flow enters Taos II at the Trails in Hearthstone Road from the Heritage subdivision to the west. Existing inlets in Heritage at the east end of Hearthstone Road capture 8 cfs from Basin H1 (13.4 cfs), with the remaining 5.4 cfs of flow continuing into Taos II as bypass flow in Hearthstone Road. This 5.4 cfs was analyzed in the street hydraulic and storm drain analyses for Taos II at the Trails.

B. ONSITE FLOWS

Developed flows from Taos II at the Trails will be directed to Pond F5 utilizing the proposed street network combined with the proposed storm drain system (see Basin Map for basin locations and the Grading Plan for storm drain and inlet locations). Flows from Taos II will combine with flows from Basins F5 and F7 per the Amended DMP. Pond F5 grading is

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shown on the Taos II Grading Plan (Exhibit 3). The total runoff from Taos II at the Trails is 53.5 cfs. This is slightly less than the combined Basin D5, D6, and F8 runoff (58.3 cfs) in the Trails Units 1-3 DMP. The difference is due to DMP Basin D5 including the portion of Pond D in Tract OS-3, which is not included in the Taos II analysis. The Amended DMP reduces the size of Pond D. The revised Pond D grading is shown on the Taos II Grading Plan (Exhibit 3).

Basin 1 (8.8 cfs), Basin 2 (15.8 cfs), Basin 3 (6.4 cfs), and Basin 5 (3.6 cfs) drain to a low point in Red Stone Road at AP#1. Basin 4 (18.9 cfs) drains to a low point in Red Stone Road at point AP#2. The storm drain inlets at the low points in Red Stone Road are in a sump condition and have capacity that is greater than two times the one-hundred year flow. The roadway high points are below the right-of-way elevations at the low point in the street. The Pond F5 serves as an emergency overflow for both points AP#1 and AP #2. See Exhibit 4 for storm drain capacity calculations.

A summary of the developed onsite flows is presented in the table below.

100 Year – 6 Hour Storm									
Basin	Area		LAND T	REATMENT		Q(100)			
ID	(AC.)	Α	В	С	D	(CFS)			
1	2.8	0.0%	20.0%	20.0%	60.0%	8.8			
2	5.0	0.0%	19.5%	19.5%	61.0%	15.8			
3	2.1	0.0%	20.5%	20.5%	59.0%	6.4			
4	6.1	0.0%	20.0%	20.0%	60.0%	18.9			
5	1.3	0.0%	29.0%	29.0%	42.0%	3.6			

Table 1 – Taos II at the Trails Onsite Proposed ConditionsBasin Data Table

C. FIRST FLUSH REQUIREMENTS

This project is required to meet the first flush requirements of the new City Drainage Ordinance. The first flush requirement will be met with on lot ponding and is calculated as 0.34 in. (0.44 in. - 0.1 in. initial abstraction) times the roof area that can drain to the on lot pond (taken as one half the pad area). There are two pad sizes, 30 feet x 85 feet and 35 feet x 85 feet, in this project with a first flush requirement of 36 and 42 cubic feet respectively.

First flush will be accommodated by a combination of ponding between the back of curb and sidewalk, supplemented by onsite front yard ponding on each lot. 30 cubic-feet per

3

lot can be stored in the landscape strip between the sidewalk and curb within the Right-of-Way. As a result, a maximum of 12 cubic-feet per lot of ponding (42 cubic-feet required minus 30 cubic-feet) is needed within the lot itself. This on-lot storage can be accomplished by a small bermed pond at the low side of each lot in front of the pad and consists of either an 8-inch or 12-inch berm. This on-lot front yard pond will be constructed as part of the landscaping by the building contractor.

V. CONCLUSION

This report provides a detailed study of the developed runoff and street capacities for the proposed Taos II at the Trails Subdivision. Included is the preliminary plat, proposed conditions basin map, grading plan, and all necessary hydrologic and hydraulic analyses. The proposed drainage plan for Taos II at the Trails can be safely conveyed by the existing and proposed improvements in this drainage plan. This drainage plan maintains the overall drainage pattern of the area, is consistent with the Trails Units 1-3 DMP and allows for the safe management of storm runoff in the fully developed condition as well as interim conditions.

APPENDICES

APPENDIX A: DEVELOPED CONDITIONS AHYMO SUMMARY, OUTPUT, AND INPUT FILES

APPENDIX B: STREET HYDRAULICS AND STORM DRAIN INLET ANALYSIS

APPENDIX A

DEVELOPED CONDITIONS AHYMO SUMMARY, OUTPUT, AND INPUT FILES

DEVELOPED CONDITIONS AHYMO SUMMARY FILE

AHYMO PROG INPUT FILE	RAM SUMMARY TABLE = DEV_Cond.HYM	(AHYMO	D_97) -		-	VERSION: 199	17.02c t	RUN DATE JSER NO.= A	(MON/DA HYMO-S-	Y/YR) =06/ 9702c1Boha	/30/2016 inHu-AH
	HYDROGRAPH	FROM	TO ID	AREA	PEAK	RUNOFF	RUNOFF	TIME TO PEAK	CFS	PAGE =	: 1
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
*S TAOS II *S 100 YEAU *S	AT THE TRAILS SUE R - 24 HOUR STORM	BDIVISI	ION DRA	INAGE BASIN (D) PROPOSED						
START		נשמת								TIME=	.00
RAINFALL T	YPE= 2	DEFF	40151							RAIN24=	2.660
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*S	*COMPUT	TE ONSI	TE BAS	INS*							
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COMPUTE NM I	HYD I.UU	-	L + + + + + + +	.00439	8.//	.410	1.//62/	1.500	3.123	PER IMP=	60.00
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COMPUTE NM 1	HYD 3.00	-	3	.00321	6.39	. 301	1.75997	1.500	3.110	PER IMP=	59.00
*S COMPUTE I	BASIN 4**********	*****	******	*****	******	****					
COMPUTE NM 1	HYD 4.00	-	4	.00948	18.94	.898	1.77627	1.500	3.121	PER IMP=	60.00
*S COMPUTE 1	BASIN 5**********	*****	******	* * * * * * * * * * * * * * *	* * * * * * * * * * * * *	* * * *					
COMPUTE NM 1	HYD 5.00	-	5	.00197	3.62	.156	1.48295	1.500	2.871	PER IMP=	42.00
*S COMPUTE 1	BASIN H1********	******	*****	* * * * * * * * * * * * * * *	*******	* * * * *					
COMPUTE NM 1	HYD H1	-	6	.00703	13.39	.604	1.61332	1.500	2.979	PER IMP=	50.00
*S DIVIDE B	ASIN HERITAGE	~	0.0	00504	F 20	451	1 (1200	1 400	1 600		
DIVIDE HYD	BYPASS.D	6	20	.00524	5.39	.451	1.61328	1.400	1.608		
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ADD HYD	TEMP.B	20& 1	11	.00963	14.16	.866	1.68756	1.500	2.299		
*S ADD BASI	NS TEMP A AND TEMP	BTO	CREATE	TEMP C *****	*****	*****					
ADD HYD	TEMP.C	10&11	12	.02071	36.35	1,920	1.73866	1.500	2.743		
*S ADD BASI	NS TEMP C AND 5 TO	CREAT	TE AP.1	*****	******	****					
ADD HYD	AP.1	12& 5	14	.02267	39.96	2.076	1.71645	1.500	2.754		
*S											
FINISH											

DEVELOPED CONDITIONS AHYMO OUTPUT FILE

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   100 YEAR - 24 HOUR STORM
*S
*S
  REVISED 2005 AHYMO TO REFLECT UPDATED LAND TREATMENTS
*CONVERT TO NMHYMO
START
************
                      TIME=0.0 HR PUNCH CODE=0
                   ****
LOCATION
                    NM
     Soil infiltration values (LAND FACTORS) for this location are not available.
     The following default values were used.
                         Initial Abstr.(in)
                                                 Unif. Infilt.(in/hour)
     Land Treatment
                         0.65
                                                 1.67
           Α
           в
                         0.50
                                                 1.25
           С
                         0 35
                                                 0 83
           D
                         0.10
                                                 0.04
*****
*100 YEAR - 24 HOUR
RAINFALL
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                            RAIN ONE=1.84 IN RAIN SIX=2.20 IN
                            RAIN DAY=2.66 IN DT=0.10 HRS
                                          END TIME = 24.000000 HOURS
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.0908 .1071 .1906 .4476
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                        .100000 HOURS
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                          .0060
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                         .0640 .0764 .0908 .1071 .1906 .4476
1.3314 1.5028 1.6393 1.7527 1.8488 1.9308
                   .0532
                   .9796
                  1.9485 1.9639 1.9776 1.9899 2.0013 2.0117 2.0215
2.0306 2.0393 2.0475 2.0553 2.0627 2.0698 2.0766

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*S *S *S COMPUTE NM HYD ID=1 HYD=1 AREA=0.004389 PER A=0 PER B=20 PER C=20 PER D=60 TP=-0.1333 RAINFALL=-1 K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420 UNIT PEAK = 10.397 CFS UNIT VOLUME = 1.029 B = 526.28 P60 = 1.8400 AREA = .002633 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000

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 TP =
 .133300HR
 K/TP RATIO =
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 SHAPE CONSTANT, N =
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 UNIT PEAK =
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 CFS
 UNIT VOLUME =
 1.004
 B =
 354.44
 P60 =
 1.8400

 AREA =
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 IA =
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 INCHES
 INF =
 1.04000
 INCHES PER HOUR

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 .072649HR
 TP =
 .133300HR
 K/TP RATIO =
 .545000
 SHAPE CONSTANT, N =
 7.1

 UNIT PEAK =
 18.951
 CFS
 UNIT VOLUME =
 1.029
 B =
 526.28
 P60 =
 1.8400

 AREA =
 .004800 SQ MI
 IA =
 .10000 INCHES
 INF =
 .04000 INCHES PER HOUR

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 .133300HR
 K/TP RATIO =
 .889153
 SHAPE CONSTANT, N =
 3.5

 UNIT PEAK =
 8.1601
 CFS
 UNIT VOLUME =
 1.006
 B =
 354.44
 P60 =
 1.8400

 AREA =
 .003069 SQ MI
 IA =
 .42500
 INCHES
 INF =
 1.04000
 INCHES
 PER HOUR

 SHAPE CONSTANT, N = 3.989065 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000 ID=2 CODE=1 PRINT HYD OUTFLOW HYDROGRAPH REACH 2.00 RUNOFF VOLUME = 1.79256 INCHES = .7523 ACRE-FEET PEAK DISCHARGE RATE = 15.79 CFS AT 1.500 HOURS BASIN AREA = .0079 SQ. MI. ID=3 HYD=3 AREA=0.003211 PER A=0 PER B=20.5 PER C=20.5 PER D=59 TP=-0.1333 RAINFALL=-1 COMPUTE NM HYD K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420 UNIT PEAK = 7.4795 CFS UNIT VOLUME = 1.029 B = 526.28 P60 = 1.8400 AREA = .001894 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000 K = .118524HR TP = .133300HR K/TP RATIO = .889153 SHAPE CONSTANT, N = 3.989065 UNIT PEAK = 3.5006 CFS UNIT VOLUME = 1.004 B = 354.44 P60 = 1.8400 AREA = .001317 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000 PRINT HYD TD=3 CODE=1

OUTFLOW HYDROGRAPH REACH 3.00

2

RUNOFF VOLUME = 1.75997 INCHES = .3014 ACRE-FEET PEAK DISCHARGE RATE = 6.39 CFS AT 1.500 HOURS BASIN AREA = .0032 SQ. MI. COMPUTE NM HYD ID=4 HYD=4 AREA=0.009483 PER A=0 PER B=20 PER C=20 PER D=60 TP=-0.1333 RAINFALL=-1

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 TP =
 .133300HR
 K/TP RATIO =
 .545000
 SHAPE CONSTANT, N =
 7.1

 UNIT PEAK =
 22.464
 CFS
 UNIT VOLUME =
 1.029
 B =
 526.28
 P60 =
 1.8400

 AREA =
 .005690 SQ MI
 IA =
 .10000
 INCHES
 INF =
 .04000
 INCHES
 PER HOUR

 SHAPE CONSTANT, N = 7.106420 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000 TD=4 CODE=1 PRINT HYD OUTFLOW HYDROGRAPH REACH 4.00 RUNOFF VOLUME = 1.77627 INCHES .8984 ACRE-FEET RUNOFF VOLUME = 1.77627 INCHES = .8984 ACRE-FEET PEAK DISCHARGE RATE = 18.94 CFS AT 1.500 HOURS BASIN AREA = .0095 SQ. MI. * PUNCH HYD TD=4COMPUTE NM HYD ID=5 HYD=5 AREA=0.001969 PER A=0 PER B=29 PER C=29 PER D=42 TP=-0.1333 RAINFALL=-1

 K =
 .072649HR
 TP =
 .133300HR
 K/TP RATIO =
 .545000
 SHAPE CONSTANT, N =
 7.1

 UNIT PEAK =
 3.2650
 CFS
 UNIT VOLUME =
 1.027
 B =
 526.28
 P60 =
 1.8400

 AREA =
 .000827 SQ MI
 IA =
 .10000 INCHES
 INF =
 .04000 INCHES PER HOUR

 SHAPE CONSTANT, N = 7.106420 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000

 K =
 .118524HR
 TP =
 .133300HR
 K/TP RATIO =
 .889153
 SHAPE CONSTANT, N =
 3.9

 UNIT PEAK =
 3.0366
 CFS
 UNIT VOLUME =
 1.004
 B =
 354.44
 P60 =
 1.8400

 AREA =
 .001142
 SQ
 MI
 IA =
 .42500
 INCHES
 INF =
 1.04000
 INCHES
 PER HOUR

 SHAPE CONSTANT, N = 3.989065 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000 ID=5 CODE=1 PRINT HYD OUTFLOW HYDROGRAPH REACH 5.00 RUNOFF VOLUME = 1.48295 INCHES RUNOFF VOLUME = 1.48295 INCHES = .1557 ACRE-FEET PEAK DISCHARGE RATE = 3.62 CFS AT 1.500 HOURS BASIN AREA = .0020 SQ. MI. COMPUTE NM HYD ID=6 HYD=H1 AREA=0.007025 PER A=0 PER B=25 PER C=25 PER D=50 TP=-0.1333 RAINFALL=-1

 K =
 .072649HR
 TP =
 .133300HR
 K/TP RATIO =
 .545000
 SHAPE CONSTANT, N =
 7.106420

 UNIT PEAK =
 13.868
 CFS
 UNIT VOLUME =
 1.029
 B =
 526.28
 P60 =
 1.8400

 AREA =
 .003513 SQ MI
 IA =
 .10000 INCHES
 INF =
 .04000 INCHES PER HOUR

 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000 K = .118524HR TP = .133300HR K/TP RATIO = .889153 SHAPE CONSTANT, N = 3.989065 UNIT PEAK = 9.3396 CFS UNIT VOLUME = 1.006 B = 354.44 P60 = 1.8400 AREA = .003513 SQ MI IA = .42500 INCHES INF = 1.04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .100000 PRINT HYD ID=6 CODE=1

HYDROGRAPH FROM AREA H1

RUNOFF VOLUME = 1.61332 INCHES = .6045 ACRE-FEET
PEAR DISCHARGE RAIE - IS.39 CrS AI 1.500 HOURS DASIN AREA0070 SQ. MI.
*
*S DIVIDE BASIN HERITAGE ************************************
DIVIDE HYD ID=6 Q=5.39 ID=20 HYD NO=BYPASS.D
ID=21 HYD NO=POND.D
FRINI HID ID-20 CODE-1
HYDROGRAPH FROM AREA BYPASS.D
RUNOFF VOLUME = 1.61328 INCHES = .4506 ACRE-FEET
PEAR DISCHARGE RAIE = 5.39 CFS AI 1.400 HOURS BASIN AREA = .0052 SQ. MI.
PRINT HYD ID=21 CODE=1
HIDROGRAPH FROM AREA POND.D
PEAK DISCHARGE RATE = 8.00 CFS AT 1.500 HOURS BASIN AREA = .0018 SQ. MI.
*
ADD HYD ID=10 HYD=TEMP.A ID I=2 II=3
PRINT HYD ID=10 CODE=1
HYDROGRAPH FROM AREA TEMP.A
RUNOFF VOLUME = 1.78305 INCHES = 1.0537 ACRE-FEET
PEAK DISCHARGE RATE = 22.18 CFS AT 1.500 HOURS BASIN AREA = .0111 SQ. MI.

*

*

HYDROGRAPH FROM AREA TEMP.B

RUNOFF VOLUME =	1.68756 INCHES	=	.8664 ACRE-FEET	
PEAK DISCHARGE RATE	= 14.16 CFS	AT	1.500 HOURS BASIN AREA =	.0096 SQ. MI.

*S AI ADD H PRINT	*S ADD BASINS TEMP A AND TEMP B TO CREATE TEMP C ***********************************							
	HYDROGRAPH FROM AREA TEMP.C							
F	NOFF VOLUME = 1.73866 INCHES = 1.9200 ACRE-FEET AK DISCHARGE RATE = 36.35 CFS AT 1.500 HOURS BASIN AREA = .0207 SQ. MI.							
* *S AI ADD H PRINT	BASINS TEMP C AND 5 TO CREATE AP.1 ************************************							
	HYDROGRAPH FROM AREA AP.1							
F	NOFF VOLUME = 1.71645 INCHES = 2.0757 ACRE-FEET AK DISCHARGE RATE = 39.96 CFS AT 1.500 HOURS BASIN AREA = .0227 SQ. MI.							
* PUNCH *S FINIS	HYD ID=14							
1	RMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 08:03:45							

DEVELOPED CONDITIONS AHYMO INPUT FILE

*S TAOS II AT THE TRAILS SUBDIVISION DRAINAGE BASIN (D) PROPOSED *S 100 YEAR - 24 HOUR STORM *S * REVISED 2005 AHYMO TO REFLECT UPDATED LAND TREATMENTS * *CONVERT TO NMHYMO TIME=0.0 HR PUNCH CODE=0 START LOCATION NM *100 YEAR - 24 HOUR TYPE=2 RAIN OUARTER=0 RAINFALL RAIN ONE=1.84 IN RAIN SIX=2.20 IN RAIN DAY=2.66 IN DT=0.10 HRS *S *S *S *COMPUTE ONSITE BASINS* *s *S *S *S *S COMPUTE BASIN 1 COMPUTE NM HYD ID=1 HYD=1 AREA=0.004389 PER A=0 PER B=20 PER C=20 PER D=60 TP=-0.1333 RAINFALL=-1 PRINT HYD ID=1 CODE=1 * *S COMPUTE BASIN 2 ID=2 HYD=2 AREA=0.007869 PER A=0 PER B=19.5 COMPUTE NM HYD PER C=19.5 PER D=61 TP=-0.1333 RAINFALL=-1 PRINT HYD ID=2 CODE=1 *S COMPUTE BASIN 3 ID=3 HYD=3 AREA=0.003211 PER A=0 PER B=20.5 COMPUTE NM HYD PER C=20.5 PER D=59 TP=-0.1333 RAINFALL=-1 PRINT HYD ID=3 CODE=1 * *S COMPUTE BASIN 4 ID=4 HYD=4 AREA=0.009483 PER A=0 PER B=20 COMPUTE NM HYD PER C=20 PER D=60 TP=-0.1333 RAINFALL=-1

ID=4 CODE=1 PRINT HYD PUNCH HYD ID=4 *S COMPUTE BASIN 5 ID=5 HYD=5 AREA=0.001969 PER A=0 PER B=29 COMPUTE NM HYD PER C=29 PER D=42 TP=-0.1333 RAINFALL=-1 PRINT HYD ID=5 CODE=1 *S COMPUTE BASIN H1 COMPUTE NM HYD ID=6 HYD=H1 AREA=0.007025 PER A=0 PER B=25 PER C=25 PER D=50 TP=-0.1333 RAINFALL=-1 PRINT HYD ID=6 CODE=1 *S DIVIDE BASIN HERITAGE DIVIDE HYD ID=6 Q=5.39 ID=20 HYD NO=BYPASS.D ID=21 HYD NO=POND.D PRINT HYD ID=20 CODE=1 PRINT HYD ID=21 CODE=1 *S ADD BASINS 2 AND 3 TO CREATE TEMP A ADD HYD ID=10 HYD=TEMP.A ID I=2 II=3 PRINT HYD ID=10 CODE=1 *S ADD BASINS DIVIDE H1 AND 1 TO CREATE TEMP B ADD HYD ID=11 HYD=TEMP.B ID I=20 II=1 PRINT HYD ID=11 CODE=1 * *S ADD BASINS TEMP A AND TEMP B TO CREATE TEMP C ADD HYD ID=12 HYD=TEMP.C ID I=10 II=11 PRINT HYD ID=12 CODE=1 *S ADD BASINS TEMP C AND 5 TO CREATE AP.1 ***** ID=14 HYD=AP.1 ID I=12 II=5 ADD HYD PRINT HYD ID=14 CODE=1 PUNCH HYD ID=14 *S FINISH

APPENDIX B

STREET HYDRAULICS AND STORM DRAIN INLET ANALYSIS





















- EXHIBIT 1: PRELIMINARY PLAT
- EXHIBIT 2: BASIN MAP
- **EXHIBIT 3: GRADING PLAN**
- EXHIBIT 4: STORM DRAIN CAPACITY CALCULATIONS
- EXHIBIT 5: SUPPLEMENTAL EXHIBITS FROM TRAILS UNITS 1-3 DMP

PRELIMINARY PLAT



BASIN MAP



GRADING PLAN





	LEGEND
91.62	PROPOSED SPOT ELEVATION
× ^{92.46}	EXISTING SPOT ELEVATION
======	EXISTING CURB & GUTTER
	PROPOSED MOUNTABLE CU
	PROPOSED STANDARD CUR
5470 —	EXISTING CONTOUR W/ INE
	FLOW ARROW
	PROPOSED RETAINING WALL
	PROPOSED SLOPE
	PROPOSED STORM DRAIN
۲	PROPOSED STORM DRAIN I
	PROPOSED STORM DRAIN I
-~~~-	HIGH POINT



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				<u>-</u> ORMAT	DATE	DATE	DATE	DATE	-ORMAT	DATE		
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				BENCH		STAMPED	N (NAD		-ACTOR =		ON = 54	
MALL						S TABLET	C POSITIC	,200.29	O-GRID	16'20"	S ELEVATI	
CARDEN CARDEN						CS BRASS	EOGRAPHI M STATE	= 1,499	ROUND-T	α = -00	AVD 1988	
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	Design Review Committee	City Engineer A	e levorq		Mo./I	Day/	/Yr.		Mo./	′Day,	/Yr.	
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	City Project No.	 xxx	Zone Map No.	7	She	et	۲.	;	Of		3	
	l			-	1							

STORM DRAIN CAPACITY CALCULATIONS



TAOS II AT THE TRAILS

PROPOSED STORM DRAIN NETWORK

JULY 2016

STORM INLET SUMMARY										
		UPSTREAM								
	STREET	HALF ST	UPSTREAM	FLOW CAPTURED	BYPASS					
INLET	GRADE (%)	FLOW (CFS)	DEPTH (FT)	BY INLET (CFS)	FLOW (CFS)	INLET TYPE				
1	N/A SUMP	20.0	0.61	20.0	0.0	А				
2	N/A SUMP	20.0	0.61	20.0	0.0	А				
3	N/A SUMP	9.5	0.42	9.5	0.0	А				
4	N/A SUMP	9.5	0.42	9.5	0.0	А				

STORM DRAIN PIPE SUMMARY									
			MAX						
			CAPACITY OF						
			FULL	FLOW					
SDP	SIZE (IN)	SLOPE (%)	PIPE(CFS)	(CFS)					
1	30	1.0%	41.02	40.0					
2	24	1.0%	22.62	20.0					
3	18	1.0%	10.50	9.5					
4	24	1.0%	22.62	18.9					

NOTES: 1. ALL INLETS ABOVE ARE SINGLE GRATE.

LEGEND

PROPOSED	STORM	DRAIN	PIPE	
PROPOSED	STORM	DRAIN	MANHOLE	۲
PROPOSED	STORM	DRAIN	INLET	



SUPPLEMENTAL EXHIBITS FROM TRAILS UNITS 1-3 DMP





DETENTION POND CHARACTERISTICS

POND	DRAIN	Q100	Q100	BYPASS	MAX	V100	TOP	BOTTOM	WSEL
	AREA	IN	OUT	Q	VOL		ELEV	ELEV	
	(AC)	(CFS)	(CFS)	(CFS)	(ac-ft)	(ac-ft)			
OFF 1	127.9	37.00	9.25		2.44	2.302	6	0	5.80
A5	179.6	121.19	16.29		4.61	4.256	5516	5511	5515.76
A6	204.2	84.21	16.19		4.72	3.241	5506	5500	5504.73
В	12.8	34.80	3:36		0.99	0.930	5519	5515	5518.86
D1 -	222.5	65.02	14.46		6.06	5.360	5475	5471	5474.48
D	274.7	146.48	5.93	13.77	6.24	4.035	5436.9	5429.5	5435.03
E	118.2	194.46	20.22		7.17	6.412	5452	5440	5451.44
F5	18.9	62.89	19.84		1.40	1.386	5426	5421	5425.97
F	373.1	259.49	17.58	6.20	11.76	10.293	5424.3	5415.08	5423.51
G	405.5	111.28	7.00	17.61	7.21	2.948	5422.5	5415.67	5419.83
H	149.8	97.80	4.50	21.60	3.02	2.205	5422	5418.65	5421.42
J	57.9	141.18	6.05	26.34	7.94	3.771	5417	5414	5415.66
K	670.8	239.15	15.75	44.91	14.84	8.346	5409	5404.85	5407.77

ANALYSIS POINT PEAK FLOWS

ANALYSIS POINT	PEAK FLOW
AP-A5	16.29 CFS
AP-A6	16.19 CFS
AP-D1	14.46 CFS
AP-D	19.42 CFS
AP-E	20.22 CFS
AP-F5	27.40 CFS
AP-F	23.78 CFS
AP-G	24.61 CFS
AP-H	26.10 CFS
AP-J	32.39 CFS
AP-K	60.66 CFS

DEVELOPED DRAINAGE BASIN CHARACTERISTICS

BASIN	AREA		LAND TRE	Q	VOL		
	ACRES	A	B	C	D	CFS	AC-FT
OFFSITE 1	127.87	100	0	0	0	37.00	4.426
Al	15.50	0	12.5	12.5	75	51.68	2.610
A2	8.52	0	33	33	34	23.43	0.960
A3	3.21	0	5	5	90	11.41	0.606
A4	7.59	0	7.5	7.5	85	26.39	1.381
A5	11.71	0	17	17	66	37.55	1 820
A6	16.97	0	19	19	62	53.44	2 5 58
A7	675	<u> </u>	12.5	12.5	75	22.52	1 137
C	9.08	12.8	28.4	28.4	30.4	22.52	0.035
<u>D</u> 1	11.62	<u></u>	10	10	62	25.20	1 752
D2	22.12		285	28.5	12	50.00	1.752
D3	3.71		20.3	20.3	45	12 18	2.705
DJ	1055	0	00.5	2005	42	15.10	1569
D4	12.33		20.5	20.3	43	30.12	1.508
_D5	8.73	0	<u> </u>	23	54	26.55	1.224
100	5.00	0	18	18	04	15.89	0.764
	14.13	0	21.7	21.8	56.5	43.39	2.025
FZ	3.67	<u> </u>	3	<u> </u>	90	13.02	0.692
F3	22.80	0	21.7	21.8	56.5	70.02	3.267
F4	24.91	0	25	25	50	74.16	3.349
F5	11.85	0	12.5	12.5	75	39.52	1.996
F7	7.02	0	7.5	7:5	85	24.42	1.278
<u>F8</u>	5.00	0	18	18	64	15.89	0.764
Gl	16.20	0	25	25	50	48.23	2.178
<u>G2</u>	16.19	0	25	25	50	48.22	2.177
OFFSITE 2	51.52	100	0	0	0	13.87	1.783
В	12.79	0	34	34	32	34.80	1.407
E1.1	11.91	-0	28.1	28.1	43.8	34.41	1.501
E1.2	12.76	0	28.1	28.1	43.8	36.78	1.608
E2	5.55	0	30.7	30.7	38.6	15.63	0.660
E3	15,50	0	22	22	56	47.48	2.210
E4	3.69	0	5	5	90	13.11	0.697
E5	17.28	18.8	23.8	26.4	31	43.19	1.762
E6	3.12	. 0	5	5	90	11.09	0.590
E7	2.90	16.5	24.8	20.6	38.1	7.55	0.324
Р	4.51	43	25	25	7	8.41	0.273
H1	11.00	0	26.6	26.6	46.8	32.26	1 431
H2	535	0	5	5	90	19.16	1018
H3	7.62	0	20	20	60	23.70	1 1 28
T1	3.31	<u> </u>	12.5	125	75	11.04	0.557
12	10.92	<u> </u>	12.5	12.5	75	36.40	1 830
13	271	<u> </u>	10	10	62	11 70	1.039
14	5.71 6.44	<u>~</u>	12.5	12 3	75	21.70	1 004
15	0.94	×	14.7	1 <i>4</i>	1.5	41.41	1.064
16	0.80	~ ~ ~	<u>,</u>	<u> </u>	90	3.05	0.162
10	2.70	<u> </u>		2	<u> </u>	9.59	0.510
10	2.84	0	2	>	90	10.09	0.536
18	5.78	0	70	30	0	12.31	0.355
<u>, 10</u>	3.51	0	7.5	7.5	85	12.20	0.638
110	4.02	0	5	5	90	14.27	0.759
111	4.79	0	5	5	90	16.65	0.886
J12	9.08	100	0	0	0	10.65	0.314
K1	17.11	0	19	19	62	50.54	2.579
К2	9.51	0	15	15	70	29.39	1.537
K3	5.85	0	5	5	90	20.76	1.104
K4	8.58	0	70	30	0	18.28	0.527
K5	15.13	0	19	19	62	47.63	2.281
К6	1.41	0	- 5	5	90	5.01	0.266
					·		



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