PIEDRAS MARCADAS WATERSHED AND LYON BOULEVARD

Storm Drain Drainage Management Plan

May 9, 2003

I, Daniel J. Grochowski, hereby certify that I am a Registered Professional Engineer, registered in the state of New Mexico, and that the following report was prepared under my direction and is true and correct to the best of my knowledge and belief.

Daniel J. Grochowski, P.E.

NMPE No. 8766

EXECUTIVE SUMMARY

This analysis update report covers the area roughly bounded by Unser/Lyon Boulevard on the east, Paradise Boulevard on the north and Paseo del Norte (PDN) extension on the south, comprising almost 600 acres of the Piedras Marcadas Dam watershed. The primary focus of the study was to determine what portion of the watershed could discharge to the Albuquerque Metropolitan Arroyo Flood Control Authority's (AMAFCA) future Lyon Boulevard storm drain extension. In the past year, the study was expanded to include analysis of the Piedras Marcardas Dam capacity, specifically to assess how much of the Piedras Marcardas developed watershed must be diverted north to the Calabacillas Arroyo to maintain one foot of freeboard in the dam.

History

There has been development interest in this area; however, due to lack of existing drainage outfalls, development has been limited. Following is a summary of some of the issues:

- The National Park Service has stated objections to allowing storm water runoff above the "historic" (not necessarily undeveloped) flow rate to pass through the Petroglyph National Monument.
- Flow to the south and east is limited. The Draft Piedras Marcadas Drainage Management Plan Revision, prepared by Molzen-Corbin & Associates in May 1993, found that the Piedras Marcadas Dam capacity would be exceeded under fully developed watershed conditions. The feasible solution was to divert storm water to the Calabacillas Arroyo at two locations. One diversion was in the vicinity of Ventana Ranch Subdivision, which has already been built, and the other was at Lyon Boulevard, which is the subject of AMAFCA's current study.
- The diversion of the upper part of the watershed was completed with the Las Ventanas
 Dam and outfall pipe to the Calabacillas Arroyo.
- The existing 72-inch storm drain outfall to the Calabacillas Arroyo in Lyon Boulevard has limited capacity.
- Property owners in the area, including Albuquerque Public Schools (APS), have been interested in developing their property but have been constrained by lack of drainage outfalls.

 Bernalillo County and the City of Albuquerque have an interest in a storm drain outfall for the future Unser Boulevard extension that will ultimately connect to Lyon Boulevard from the south.

Since AMAFCA has the Lyon Diversion Storm Drain on its project schedule, AMAFCA sponsored the drainage study for the area. AMAFCA entered into an Agreement with the City, County and developers in March 2001 to prepare a "Mini" Drainage Management Plan. The primary purpose was to determine how existing and proposed development will impact AMAFCA facilities. AMAFCA contracted Bohannan Huston, Inc. (BHI) to perform the work.

Results of Study

BHI took the original hydrologic model from the 1993 Molzen-Corbin study and updated drainage basins and facility capacities to reflect construction since that time. Among these projects are:

- Las Ventanas Dam and 60-inch storm drain outfall to the Calabacillas Arroyo.
- The Lyon Boulevard 72-inch storm drain outfall to the Calabacillas Arroyo.
- The Paradise Boulevard storm drain from Lyon Boulevard to an existing storm drain stubout west of Golf Course Road. The ultimate outfall is the Piedras Marcadas Dam.
- Expansion of Piedras Marcadas Dam.

BHI used the 100-year flow rates from this analysis to determine storm drain options in the Lyon/Unser Boulevard corridor. The study was limited in scope to evaluate the following options:

- Option 1 Free discharge from the study area into a larger, proposed Lyon Boulevard outfall pipe. This option was used as a benchmark to compare the other options.
- Option 2 Utilize a single "regional" detention pond to reduce flow to minimize pipe sizes
 and to match the capacity of the existing outfall pipe.
- Option 3 Utilize a series of smaller detention ponds to reduce flow to minimize pipe sizes
 and to match the capacity of the outfall pipe.
- Option 4 Utilize detention ponding to reduce flow to minimize pipe sizes (Option 2 or 3).
 Maximize the existing outfall pipe capacity with pressure flow.

The results of the analysis also indicated that the capacity of the Piedras Marcadas Dam must also be taken into account. Although approximately 2.7 square miles have been diverted from the dam watershed to the Calabacillas Arroyo with the Las Ventanas Dam and Lyon Boulevard storm drain outfalls, it was necessary to evaluate the dam capacity with ultimate development. The current capacity, with one foot of freeboard, is 280 acre-feet. The study evaluated the additional drainage basin area that will need to be diverted to the Lyon Boulevard storm drain to maintain this capacity. An area of approximately 115 acres will be required to discharge to the Lyon Boulevard storm drain. Since the total discharge from this area is 400 cfs, and the additional capacity available in the outfall in Option 4 is 210 cfs, detention ponding will be required.

Construction Cost Estimates

Several construction cost scenarios were evaluated. The first was total project cost, from the future PDN to the existing 72-inch outfall to the Calabacillas Arroyo. The second was just the AMAFCA portion from the Paradise/Lyon intersection to the existing outfall. The third was the AMAFCA portion, excluding basalt excavation. This scenario was included as a comparison since construction within the basalt layer will significantly drive up the cost.

The County and APS have been interested in extending the Paradise Boulevard storm drain to the west. Therefore, this fourth scenario was included as an addition to the AMAFCA Lyon Boulevard storm drain portion.

Following is a summary of the construction cost estimates:

Storm Drain Option	Total Project Cost	Lyon Project Cost (AMAFCA)	Lyon Project Cost (excl. basalt) (AMAFCA)	Paradise/Lyon Project Cost	Flow from South (cfs)
1	\$24,831,000	\$7,800,000	\$3,477,000	\$9,153,000	1460
2	\$26,429,000	\$4,687,000	\$1,343,000	\$6,040,000	170
3	\$17,359,000	\$3,082,000	\$1,129,000	\$4,435,000	130
4	n/a	\$3,337,000	\$1,292,000	\$4,690,000	210

The recommended option is Option 4. The total project cost was not calculated since the storm drain option south of Paradise Boulevard could follow Option 2 or 3. The AMAFCA Lyon

storm drain project is \$255,000 more than Option 3 because it has a 90-inch storm drain connection to the existing outfall, while Option 3 has a 78-inch and 84-inch storm drain. Option 4 optimizes the use of the existing outfall and, with an increase of one pipe diameter, almost doubles the allowable flow from south of Paradise Boulevard.

I. INTRODUCTION

The Piedras Marcadas Watershed and Lyon Boulevard Storm Drain Analysis Update deals with an area of northwest Albuquerque that, up to this time, has had a very limited potential for development due to the lack of an outfall for developed flows. This area is approximately bounded by Unser/Lyon Boulevard on the east, Paradise Boulevard on the north, and on the south and west sides by the limits of the Piedras Marcadas Watershed. An attempt was made to include whole properties into the primary study area, and some area east of Unser Boulevard is included because it is possible to use the same system. There is an existing 72" storm drain line in the Unser/Lyon Boulevard Alignment from Irving Boulevard to the Calabacillas Arroyo. Past studies have proposed a southern extension of this storm drain to Paradise Boulevard. The intent of the primary analysis is to determine the feasibility of using the proposed Lyon Boulevard storm drain as the outfall point for the primary study area. The effects of recent developments in the entire watershed on the Piedras Marcadas Dam have also been included in this report. The Albuquerque Metropolitan Arroyo Flood Control Authority (AMAFCA), the chief sponsor of this study, the City, and area landowners have funded and provided needed information for this study.

Two past reports are foundational to the work done in this study. The first is the "Piedras Marcadas Drainage Management Plan" by Molzen-Corbin done in May 1993. It deals with drainage issues for the entire Piedras Marcadas Watershed. A number of developments have occurred in the watershed in the ten years since the report was completed, changing the area's hydrology. The other report is the "Conceptual Design Analysis for Lyon (Unser) Boulevard/Paradise Boulevard Storm Drain" by Bohannan Huston done in June 2000. The report evaluates a proposed storm drain down Paradise to Lyon and then continuing in Lyon connecting to the existing Lyon Boulevard Storm Drain.

As a starting point for this study, the existing section of storm drain, from Irving to the Calabacillas Arroyo, was analyzed to determine the existing capacity, which was determined to be 734 cfs based on Manning's Equation. In addition, the maximum area that could be routed to the storm drain was determined. The preliminary layout for the Paradise Boulevard Storm Drain west of Lyon Boulevard was also examined to determine whether or not it could be reduced due to addition

of storm drain line south of Paradise Boulevard. Three options were investigated for diverting the maximum drainage basin to the Lyon Boulevard Storm Drain System, and a fourth option was investigated for the storm drains in Paradise and Lyon Boulevards. The first option assumes an upsizing of the existing storm drain and an Unser Storm Drain that extends into the study area without detention ponds. The second option utilizes one detention pond to reduce flows to preserve the existing storm drain. The third option also looks to use the existing system, but makes use of several detention ponds rather than one. The fourth option looks at a pressure storm drain system in Paradise and Lyon Boulevards. The four options are discussed in further detail in Section III, below.

Since the watershed has undergone some development and improvements to the drainage system, the effects of that development have changed its hydrology. After revising the hydrology, other possible scenarios became apparent and are discussed in Section IV, below.

II. HYDROLOGY

Hydrologic modeling for this project was performed using the 1997 version of The Arid-Lands Hydrologic Model (AHYMO) in accordance with the City of Albuquerque Development Process Manual, Section 22.2, January 1993. Pipes were sized using Manning's Equation. Hydraulic grade lines were not calculated except for Option 4. Concrete box culverts were modeled as equivalent pipes in the AHYMO model. The 100-year storm event is used.

A. Drainage Basins

As mentioned above, the primary focus of the study area is bounded on the east, with some exceptions, by the proposed alignment for Unser Boulevard. This is because the Unser Corridor is a natural extension for the Lyon/Unser Storm Drain and is very nearly the outer limit of area that can physically be drained to the Calabacillas. There is some area east of Unser that is included because it could drain to the system and does not have another currently available outlet due to the presence of the Petroglyph National Monument downstream. The National Park Service has been very restrictive about allowing developed storm water flows to pass through the Monument.

In order to get as much area as possible to drain into the system, it was assumed that the storm drain trench at the intersection of Lyon and Paradise Boulevards should not be deeper than 30'. A hypothetical pipe line was taken from the intersection south at a 0.2% slope. The placement of the hypothetical pipe line was determined by maintaining at least two feet of cover above the soffitt in relation to the existing contours. The hypothetical pipe line was then used as the basis for the basin boundary. It is also the approximate location for the pipe lines in the three options. Other properties on the east that border the Unser alignment could be brought into the system if they are filled on the eastern portion of the property and the added flow does not overload the system. This may require the use of detention ponds on these sites. Due to the complexity of analyzing the feasibility of this option, these areas were not included in this study.

The sub-basins used in these options were developed from the basins in the Molzen-Corbin report "Piedras Marcadas Drainage Management Plan Revision" (1993) for the area south of Paradise Boulevard and the Bohannan-Huston report "Conceptual Design Analysis for Lyon (Unser) Boulevard/ Paradise Boulevard Storm Drain" (2000) for the area north of Paradise Boulevard. Plate 1 is a copy of the drainage basin map from the conceptual Lyon report. Plate 2 includes the basin maps from the Piedras Marcadas Report. Sub-basin 315 from the Piedras Marcadas report was the primary basin in the Lyon/Unser study area and was divided into Sub-basins 1 through 7. Sub-basins 3 and 6A are extended past the outer boundary of the Piedras Marcadas to include whole properties. This was the practice everywhere possible so that an owner would not have two separate drainage systems on the same property. Sub-basin 313 is a combination of sections from Molzen-Corbin's Sub-basins 313N and 313S. Sub-basins 311N, 311S, and 310 are located similarly to Molzen-Corbin's, except that there are changes due to the new mapping used (Bernalillo County, 1999), and the sub-basins end at the Unser alignment. Sub-basin 312 is only the very southern portion of Molzen-Corbin's original. Sub-basin 8 is within a portion of the proposed Unser Boulevard Corridor. The sub-basins can be seen in Exhibit 1.

B. Land Treatments

The land treatment percentages were determined based on zoning and the intended land uses as provided by the primary land owners in the area. The intended uses and zoning are also shown in Exhibit 1, and the land treatment percentages assigned to each basin are shown in Appendix A along with the AHYMO input and summary printouts. The land treatment percentages for the sub-basins, along with the 100-yr flow rates, volumes, and CFS/acre, are shown in Table 1. The land treatment percentages for the entire watershed analysis were not revised from the Molzen-Corbin report.

Table 1 – Sub-Basin Summary (Lyon Blvd. Storm Drain Options)

SUB- BASIN	AREA		% LAND T	REATMEN	Τ*	Q (100-YR)	VOLUME	CFS/Acre
	(acres)	Α	В	C	D	(CFS)	(acre-ft)	
1	22.7	0.0	12.9	18.1	69.0	88.5	3.8	3.91
2	16.0	0.0	9.3	11.6	79.1	65.2	2.9	4.09
3	64.4	0.0	9.7	12.3	78.0	185.1	11.6	2.87
4	103.7	0.0	9.0	12.2	78.9	361.6	18.8	3.49
5	27.7	0.0	14.7	19.6	65.7	106.5	4.5	3.84
6A	176.8	0.0	13.4	17.4	69.1	451.8	29.8	2.56
6B	48.3	0.0	15.0	20.0	65.0	184.9	7.9	3.83
7	21.4	0.0	9.6	10.9	79.5	66.5	3.9	3.10
313	38.0	0.0	12.7	16.6	70.7	122.5	6.5	3.22
310	7.3	0.0	15.0	20.0	65.0	27.9	1.2	3.83
311S	18.7	0.0	14.0	19.3	66.7	72.2	3.1	3.84
311N	32.4	0.0	8.2	10.9	80.9	109.8	6.0	3.39
312	8.2	0.0	8.6	12.1	79.3	33.1	1.5	4.07
8	11.2	0.0	0.0	10.0	90.0	29.8	2.2	2.65

^{*}Obtained from Section 22.2, Hydrology of the Development Process Manual, Volume 2.

For comparison purposes, Table 2 shows Molzen-Corbin's sub-basins within this area and the CFS/Acre for each. The areas of each sub-basin are not shown since the sub-basins' areas have changed, due to being cut off at the Unser Alignment, inclusion of whole properties, and changes due to new mapping. (Refer to Section II.A.)

Table 2 - Molzen-Corbin's Sub-Basins Within Study Area

SUB-BASIN	CFS/Acre
315W	3.50
315S	3.50
315N	3.50
313S	3.15
311S	3.50
310	3.50
311N	2.78
312	2.26

C. Paradise Boulevard Storm Drain Analysis

Part of the scope of the study was to examine the preliminary layout of the Paradise Boulevard Storm Drain, from Chamisa Ridge to Lyon/Unser Boulevard, to determine if the size of the system could be reduced based on a reduced drainage area. There was a reduction in area since the original study in an area east of the James Monroe Middle School. This area, which is included in the new Sub-basin 313, was originally in a sub-basin contributing to the Paradise Boulevard Storm Drain according to the 2000 Lyon Report. In addition, some of the other areas south of Paradise Boulevard have been developed at a lower density than was predicted by the 2000 Lyon Report. However, even with the area reduction and less impervious contributing areas, the flow rates were not reduced enough to require a smaller storm drain system. The majority of flow into the system is from the north side of Paradise Boulevard. Please refer to the 2000 "Conceptual Design Analysis for Lyon Boulevard/Paradise Boulevard Storm Drain" by Bohannan Huston for information, calculations and layout of the Paradise Boulevard storm drain.

III. LYON BLVD. STORM DRAIN OPTIONS

A. Option 1: Free Discharge, All New Storm Drain, Full Conveyance

Option 1 is a storm drain only option without detention and, consequently, includes expansion of the existing storm drain. This option requires concrete box culverts (CBC) as large as 12' X 12'. The entire network including flow rates can be seen on Exhibit 3. The flow

rate in the pipe network coming into the intersection of Paradise and Lyon is 1,453 cfs, and the box culvert size is 12' X 12' with a slope of 0.2%. Under this option, the storm drain on the north side of the intersection must be an 11' X 10' CBC, and the replacement of the existing storm drain must be 96" pipe. The total flow at the outfall to the Calabacillas is 1,983 cfs.

B. Option 2: Existing Storm Drain, 1 Large Detention Basin South of Paradise Blvd.

Option 2 maintains the existing storm drain as is and has one large detention pond to attenuate flows to its capacity. Option 2 is shown in Exhibit 4. A possible location for the pond was found to be near the intersection of Paradise and Lyon. This site is chosen because it can collect runoff from all of the basins in the study area. This is important since even the smaller sub-basins adjacent to the chosen pond site (311N&S, 312, 310, and 8) could overwhelm the existing storm drain if their flows are not attenuated. The pond would need to have storage of 65.4 ac-ft and would cover an area of approximately 8-9 acres. This option would also require very large concrete box culverts (12' X 12') upstream of the pond. The peak flow rate entering the pond is 1509 cfs, and the peak outflow is 174 cfs. The pipes north of the intersection to the existing storm drain would need to be 84" and 90".

C. Option 3: Existing Storm Drain, 4 Smaller Detention Basins South of Paradise Blvd.

There is more flexibility in Option 3, which is shown in Exhibit 5. Four detention ponds are used to attenuate flows in this option. The largest pipe in the system south of the intersection of Lyon and Paradise is 66", and the largest pipe north of the intersection is 84". The total amount of storage provided by the ponds is 113.6 ac-ft, and the approximate area needed for all four ponds is 15 acres. The peak outflow from the final pond, which enters the Lyon Boulevard storm drain, is 131 cfs.

D. Option 4: Existing Storm Drain, Full Conveyance under Pressure Flow Conditions Assuming 212 cfs from Area South of Paradise Blvd.

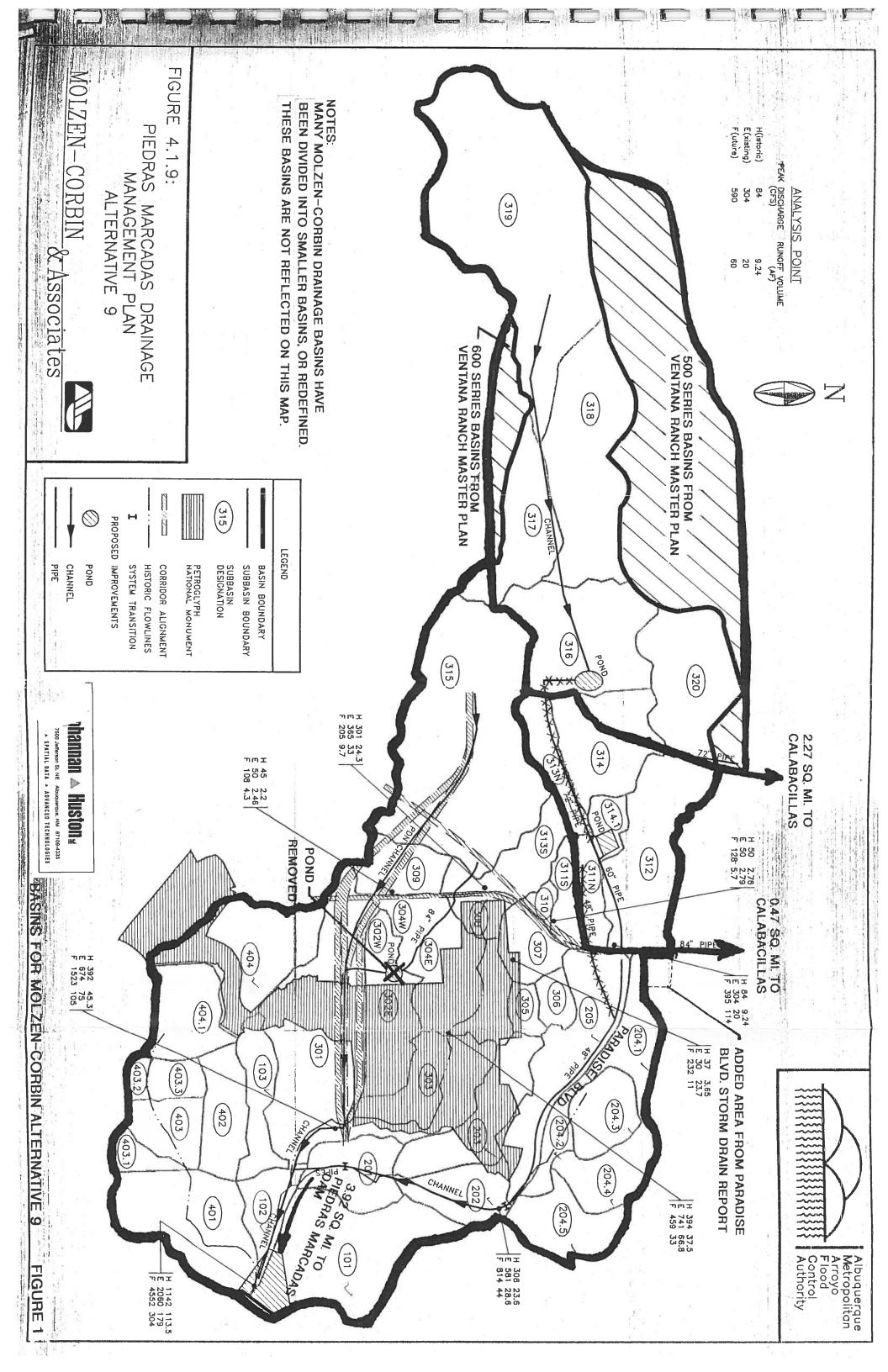
As mentioned in the introduction, Option 4 is exclusively for the Paradise and Lyon Boulevard Storm Drains. It includes a hydraulic grade line (HGL) analysis to determine the maximum flow rate that can be allowed from the south at the intersection of Paradise and Lyon, while tying to the existing storm drain. The maximum allowable flow rate is 212 cfs. The largest pipe size required is 90". Larger sizes were tried just north of the intersection, but the ultimate control of the system is the existing storm drain. Therefore, the 90" gave as much capacity as a larger diameter pipe. Exhibit 6 contains a plan and profile sheet showing Option 4, as well as a profile of the basalt along the Lyon Boulevard alignment.

IV. REVISED PIEDRAS MARCADAS DAM WATERSHED HYDROLOGY AND SCENARIOS

Subsequent to the development of the four options for the Lyon Blvd. storm drain, an outfall to the Piedras Marcadas Dam from developing areas upstream of the Petroglyph National Monument again became a possibility with the designation of the future Paseo del Norte alignment. In order to take advantage of this outfall in the Paseo del Norte corridor, the effects on the dam of all current and future development in the Piedras Marcadas watershed were investigated.

The total drainage area to the dam is nearly 4.0 square miles. The drainage area is slightly less than that reported in the Molzen-Corbin study primarily because Basin 311N is now shown as being diverted to the Calabacillas Arroyo via the future Lyon Boulevard storm drain. Figure 1 shows the overall area draining to the dam (Molzen-Corbin - Alternative 9) as well as the areas being diverted to the Calabacillas Arroyo.

The drainage area to the dam includes the area west of Lyon Boulevard and south of the drainage divide to the Calabacillas Arroyo. The four Options previously discussed assumed a diversion of a large portion of this area to the Calabacillas Arroyo via the future Lyon Boulevard storm drain. This diversion is not incorporated into the revised hydrology because it was not required to meet the capacity of the dam.



The Molzen-Corbin AHYMO model (Option 9) served as the base model for this analysis. It has been appended with the Ventana Ranch, Shenandoah and Rancho Sereno subdivisions. The Ventana Ranch Detention Dam, shown in Basin 316, has been constructed and is responsible for diverting over two square miles of the upper watershed to the Calabacillas Arroyo. The second diversion area to the Calabacillas Arroyo is the Lyon Boulevard storm drain. This diversion is planned for the future and was presented in the original Molzen-Corbin model, but with a different drainage area to the outlet.

In addition to these changes, the AHYMO model has been modified in a number of other ways. Most notably, the proposed pond in Basin 302/304 has been removed; the Shenandoah and Rancho Sereno Subdivision models, located within Basins 301 and 102 respectively, have been edited so that all the hydrographs are being added into the dam. A new basin has been created out of Basin 205 for the Paradise Ridge Subdivision. Routes have been added to reflect the new Paradise Boulevard storm drain.

When all the revisions were included, the model indicated a smaller drainage area to the dam than in the Molzen-Corbin report. Comparisons were made between the original AHYMO model and subsequent changes over the last ten years. It was discovered that when the subbasins were redefined, and the Shenandoah and Rancho Sereno Subdivisions were incorporated, the new drainage basin boundaries did not match the original basin boundaries in Basins 102 and 301. A new basin in 102 was added to account for this and area added to offsite Basin SHENO1E in 301.

The information used to calculate the required sediment storage in the dam was based on Dr. Richard Heggen's Sediment Study of the Piedras Marcadas Watershed as included in the Piedras Marcadas DMP. His results did not include any diversions to the Calabacillas Arroyo, so the total drainage area to the dam was larger than it is today. No reduction in sediment to the dam for the reduced area has been included in this analysis. From observations made during a site visit, it was noted that vegetation has grown in the dam basin. No account for any loss of capacity due to the vegetation has been made.



The results of the analysis of the capacity of the Piedras Marcadas Dam at the emergency spillway are as follows:

0.55 ft		Freeboard in the Piedras Marcadas Dam
11 ac-ft		Excess Capacity in the Piedras Marcadas Dam
	model by BHI	
292 ac-ft	2002 Revised AHYMO	100-Yr Runoff Volume
303 ac-ft		Available storage in Piedras Marcadas Dam
	1993	(5 x 0.31 ac-ft + 2.07 ac-ft)
3.6 ac-ft	Piedras Marcadas DMP,	Sediment Volume (5 x annual + 100-year)
307 ac-ft	Plan by BHI	of the emergency spillway)
	1995 Revised Grading	Piedras Marcadas Dam Design Capacity (to the crest 1995 Revised Grading
Volume (ac-ft)	Source	

In order to meet an AMAFCA requirement for one foot of freeboard below the emergency spillway, a maximum of 280 ac-ft of runoff volume can be allowed into the dam. The runoff volume into the Piedras Marcadas Dam cannot be reduced to the recommended 280 ac-ft while not exceeding the 212 cfs capacity of the Option 4 Lyon Boulevard storm drain if free discharge from all basins to Lyon Boulevard is assumed. Below are presented results for two scenarios that would satisfy the dam volume constraint (280 ac-ft) and the Lyon Blvd. storm drain capacity constraint (212 cfs). Refer to Figure 2.

A. Scenario 1: Do not Exceed Lyon Boulevard Storm Drain Capacity

To not exceed the Lyon Boulevard storm drain capacity, only Basins 311N and 311S can free discharge to Lyon Boulevard. The total 100-year flow from these basins is approximately 205 cfs. The runoff volume into the dam is reduced to 287 ac-ft. Recall that in the original model Basin 311N was already diverted north.

Scenario 2: Disregard Lyon Boulevard Storm Drain Capacity and Meet the Required Runoff Volume

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To reduce the total runoff volume into the dam to 280 ac-ft, Basins 311N, 311S, 310, 313SA and 315NE need to be diverted to the Lyon Boulevard storm drain. The total 100-year runoff from these basins is 400 cfs. The calculated runoff volume to the dam is 278 ac-ft.

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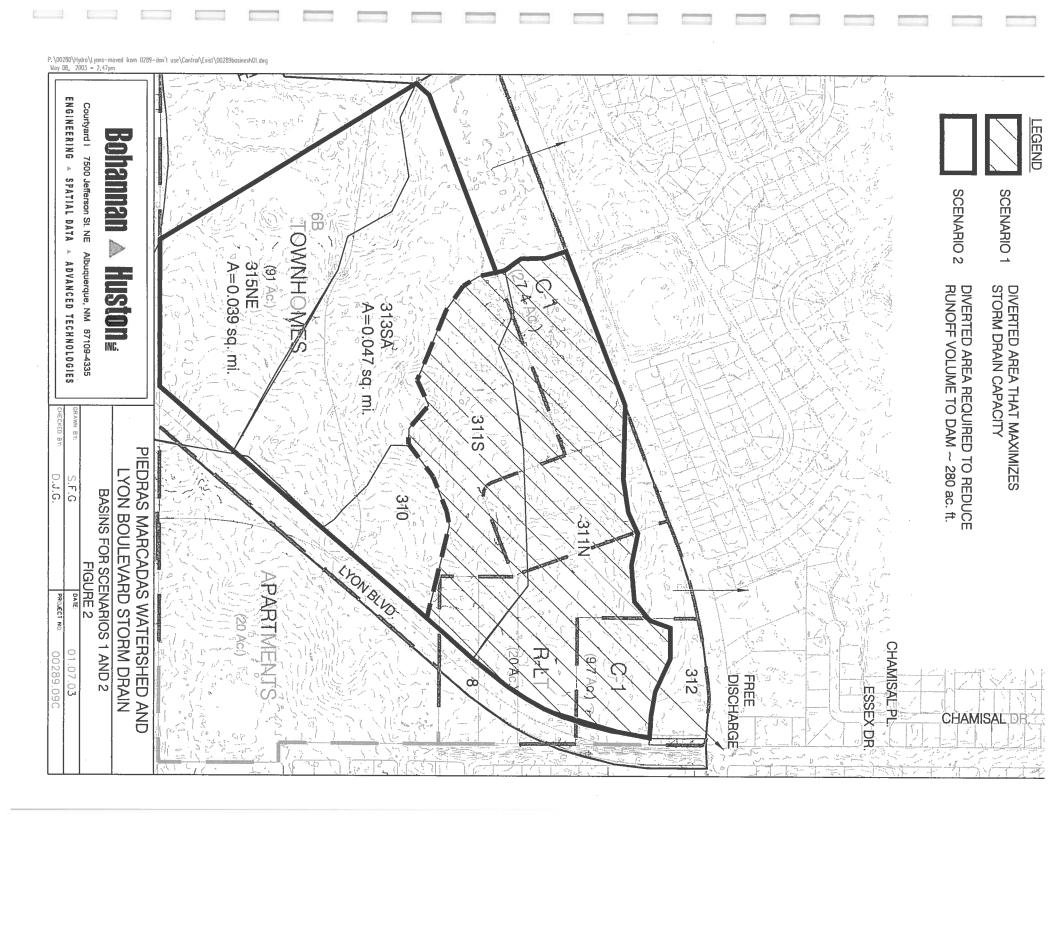
open to the river. Figure 2 illustrates the drainage areas corresponding to each scenario Blvd. storm drain, there is still approximately 45 ac-ft of capacity in the dam with the 36" pipe runoff would be enhanced. Even with none of the area shown in being diverted to the Lyon spillway (a 36" pipe) be opened. If the principle spillway were to be extended to the Rio downstream facilities are capable of accepting flows impounded in the dam can the principle Paradise Boulevard runoff from the sliver shown does not contribute to the total flow in the storm drain south of above. Note that the basin labeled "312" is actually only a very small portion of Basin 312 in Grande (approximately 4500'), the hydraulic capacity of the dam and its ability to accept more create a detention facility are possible and could prove very beneficial. Only after Piedras Marcadas Dam is currently operated as a retention dam; however, modifications to the AHYMO model. meet both criteria is to convert the Piedras Marcadas Dam from retention to detention. The would attenuate the flows in the second scenario to the 212 cfs capacity. Another option to The most obvious way to meet both limitations is to construct a detention pond(s) that The majority of the basin lies north of Paradise Boulevard. Therefore,

In general, the basin divides shown are based on topography and are similar to those of the Molzen-Corbin study. The exception is Basin 315NE, which was based on lot lines. It seemed prudent to create the basin in this manner so that the entirety of Lot 6 will be diverted to the storm drain, rather than having only, a portion of it diverted. Basins 313SA and 315NE were originally part of larger basins, 313S and 315N respectively, but were subdivided to suit this analysis.

V. COST ESTIMATE FOR THE FOUR LYON BLVD. OPTIONS

There are four design parameters that strongly impact the cost of the options; storm drain size, trench depth, detention pond size, and land costs. The first three are especially important because they affect the amount of basalt rock removal that will be necessary. In the areas where basalt rock removal was determined to be necessary there are no trenching costs, but there is a backfill cost since the basalt rock cannot be used as backfill. Where trenching is specified, the unit cost was based on the 1998 Unit Cost used by the City of Albuquerque with a 30% increase to





make it comparable to recent contractors' estimates for storm drain construction. The pond costs were determined based on the costs of recent AMAFCA dams and recently constructed ponds designed by Bohannan-Huston. The dams and ponds were placed in an Excel spreadsheet based on size and cost per acre-foot. An equation was derived for a fitted curve, and that equation was used to determine the cost per acre-foot for the ponds used in the estimate. A chart showing the points and fitted curve is shown in Appendix B. The reinforced concrete pipe / concrete box culverts costs were determined by using the 1998 Unit Cost, recent contractor bids, and information provided by a local supplier and local contractor. The 20% contingency used for the cost estimates in the preliminary report has been reduced to 10% for the cost estimates presented here because unit costs that are more accurate were used. The cost of the land was roughly estimated at \$50,000 per acre.

The most important aspect of the cost of any of the options is the presence of basalt rock. One area that is proven to have basalt is the area from the intersection of Paradise and Lyon Boulevards to the outfall. Basalt removal calculations were performed in this area based on information in the Conceptual Lyon Report (2000), which is based on borehole data. Refer to Appendix E. However, it is assumed that all the trenches south of Paradise Boulevard will also require basalt removal. This assumption is based on visual appraisal of the surface and borehole data provided in the "Unser Middle Transportation Corridor Study" done by Leedshill-Herkenhoff in 1992. Two boreholes that fall within the study area near the proposed Paseo Dei Norte alignment show basalt rock from 2-5 feet below the surface through 31-38 feet below the surface. The basalt removal greatly increases the costs of all options. The basalt rock removal volumes were calculated based on a typical trench prism in rock. This assumes vertical sides. It was also assumed that basalt rock removal will be necessary for the ponds unless they are located in a valley where a berm could be placed above ground to gain storage. The pond in Option 2, therefore, requires basalt rock removal, as do Ponds 1 and 3 in Option 3. The cost of basalt rock removal was based on current projects near the study area.

The estimated costs of the four options are shown below in Table 3. The estimated construction cost for the Paradise Boulevard portion of the storm drain system is \$1,353,000, assuming that there is no basalt rock removal. For detailed estimates, see Appendix C.



OPTION 4	OPTION 3	OPTION 2	OPTION 1	OPTION
N A	14,277,000	21,742,000	17,031,000	Primary Study Area
3,337,000	3,082,000	4,687,000	7,800,000	Lyon Boulevard Storm Drain
1,353,000	1,353,000	1,353,000	1,353,000	Paradise Boulevard Storm Drain
NA	17,359,000	26,429,000	24,831,000	Total without Paradise Blvd. Storm Drain
NA	18,712,000	27,782,000	26,184,000	Total with Paradise Blvd. Storm Drain

VI. CONCLUSION

A. Four original Lyon Blvd. storm drain options

Though Option 3 is the lowest cost option for the Paradise/Lyon Blvd. storm drain, Option 4 is the recommended option. Though slightly more expensive than Option 3, Option 4 will maximize use of the existing storm drain and allow a maximum area south of Paradise Blvd. to flow to the storm drain. There are also other advantages to Option 4, including constructability. All of the items in Option 4 are commonly constructed in the Albuquerque area, whereas the large box culverts required in the first two options are not. This could lead to more problems in design and construction. Having such large box culverts also increases the possibility for conflicts with existing utilities and will make the design and construction of future utilities in the area much more difficult. Although the Option 4 configuration is more costly than Option 3 by \$255,000, it allows approximately 80 cfs more than Option 3 into the Lyon Boulevard storm drain. This increased flow rate means that less ponding would be required south of Paradise Boulevard, which would reduce the pond costs. It is also recommended that more information be acquired concerning the basalt in the area, as this is the most expensive element of any plan.

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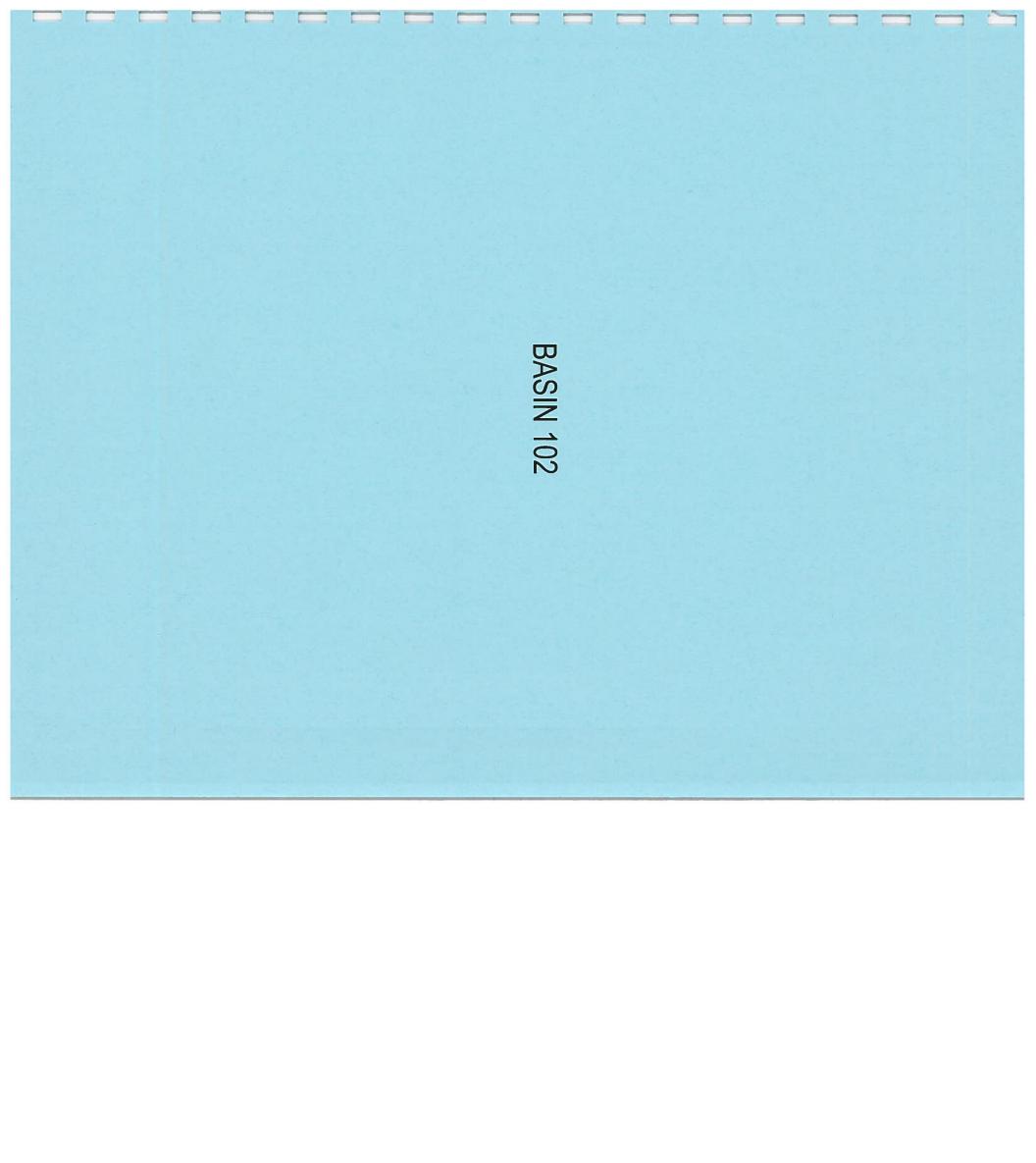
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After completion of the four options investigation, an outfall for developed runoff upstream of the Petroglyph National Monument to the Piedras Marcadas Dam through the Paseo del Norte corridor became a possibility. Additional hydrologic scenarios were studied to make use of this outfall.

The Piedras Marcadas Dam can accept a volume of 280 ac-ft. The watershed area that can flow with free discharge to the dam, based on Molzen-Corbin's development assumptions, can be maximized to make full use of this capacity. This allows for a reduction in the area flowing to the Lyon Blvd. storm drain compared to the four original options. Used in conjunction with the Option 4 storm drain, the area immediately south and west of the Lyon Blvd. /Paradise Blvd. intersection can flow to the storm drain at a maximum flow rate of 212 cfs. In order to accomplish this flow rate some detention ponding is necessary.

If the Piedras Marcadas Dam can be converted to a detention dam additional areas would be able to flow with free discharge to the dam. This assumes the conveyance facilities to the dam already in place can accept the added flow.

_											
School	Chamisa	R-LT	R-D	Town Homes	Apartments	Roadway	R-T	C-1	0-1		ZONE/USE
>	48	0	0	0	0	0	0	0	0	A	LAND 1
ת	10	15	13.5	15 5	15	0	15	ഗ	20	В	LAND TREATMENT PERCENTAGES
S N	25	25	13.5	20	15	10	20	(J)	20	ဂ	T PERCEN
20	17	60	73	65	70	90	65	90	60	O	ITAGES



- VERSION: 1997.02c RUN DATE (MON/DAY/YR) =07/03/2001 USER NO.= AHYMO-S-9702c1BohanHu-AH

COMMAND	HYDI IDENTIFI	ROGRAPH ICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	1 วพ
							(/	()	()	nena	NOTATIO	JIV
S		PROJECT	NAME:		BLVD STORM			:				
S *S*		TOD 110	0000		DRAINAGE MAN	AGEMENT PLAN						
S		JOB NO.		30C4.01								
S		DATE:	Julie 2	25, 2001								
S		INPUT F	ILE NA	ME: Opt	3 03.HYM							
S					Opt3 03.out							
S		FILES L	OCATIO	N: BHI	-MAIN\00280\	HYDRO\DESIGN\A	НҮМО					
	MENTS:											
S	7-2-01: I	Divided	Sub-ba	ısin 6 iı	nto 6A and 6	B and added a	pond					
S *S*	6 25 01	7 m	h									
S	6-25-01:	Added T	nree E	onas								
S	5-16-01:	Revised	Rasir	າຣ 1 ຄ.ວ ລາ	nd added Bas	in 7						
S	3 10 01.		20011	142 41	id dddca bas	111 /						
S	5-9-01: I	3asin 31	5 has	been bro	oken into se	veral smaller	basins					
S												
S												
*S		4-2-01	: Bas	ins are	based on the	ose used in pr	evious report	S				
*S						olzen-Corbin's						
*S *S		have b	as Arr	oyo Anai	ysis (1991)	; however, bas ew mapping and	ins					
*S					ea (based o		tne					
*S				nabic ai	ca (basea o	n Blope).						
*S //////	///////////////////////////////////////	///////	/////	////////	///////////////////////////////////////	///////////////////////////////////////	/////////					
RAINFALL	TYPE= 2										RAIN24=	2.700
SEDIMENT B	ULK										PK BF =	1.02
*S												
*S S	UB-BASIN 1	1 00		•	02540							
*S	HID	1.00	-	1	.03540	88.50	3.818	2.02214	1.500	3.906	PER IMP=	69.00
	asin 1 thro	igh 4.5	pipe	for 1350) ·							
ROUTE MCUN		RT1	1	12	03540	77.57	3.759	1.99087	1.550	3.424	CCODE =	. 2
*S S	UB-BASIN 2								2.000	3.121	ccopp -	
COMPUTE NM		2.00		2	.02490	65.15	2.902	2.18492	1.500	4.088	PER IMP=	79.10
	b-basin 2 am											
ADD HYD	Cub basis 2	RT1&2			.06030	136.94	6.660	2.07098	1.500	3.548		
ROUTE MCUN		RT2UP	upstr 13			0' of 66" pipe						
	B-BASIN 3	RIZUP	13	14	.06030	130.44	6.611	2.05566	1.550	3.380	CCODE =	. 2
COMPUTE NM		3.00	_	3	.10070	185.06	11.639	2.16716	1.650	2 071	PER IMP=	70 00
			am flo		go to Pond		11.037	2.10/10	1.030	2.0/1	PER IMP=	78.00
ADD HYD		RT2UP&3			.16100	308.27	18.250	2.12539	1.600	2.992		
	B-BASIN 4											
COMPUTE NM		4.00	-	4	.16200	361.61	18.848	2.18149	1.550	3.488	PER IMP=	78.80
	b-basin 4 to	_		_								
ADD HYD *S SU	B-BASIN 5	RT3UP&4	15& 4	17	.32300	653.99	37.098	2.15353	1.550	3.164		
COMPUTE NM		5.00	_	5	.04330	106 46	4 542	1 06670	1 500	2 040	555 745	
	Sub-basin 5			pipe for	400'	106.46	4.542	1.96678	1.500	3.842	PER IMP=	65.70
			F									
			FROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	2
	HYDI	ROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER		

COMMAND IDENTIFICATION	1 NO. NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE NOTATION
ROUTE MCUNGE RT5 *S Add Sub-basin 5 to Pond		.04330	96.17	4.442	1.92359	1.500	3.470 CCODE = .2
	5 18&17 19	.36630	739.66	41.540	2.12635	1.550	3.155
	0 - 30 1 Iflow	.03350	66.49	3.913	2.18983	1.600	3.101 PER IMP= 79.50
	7 19&30 20	.39980	801.79	45.453	2.13167	1.550	3.134
ROUTE RESERVOIR Pondlout *S Route Pond 1 Outflow thr	t 20 43 rough 60" pip	.39980 pe for 1645'	108.30	45.065	2.11347	2.300	.423 AC-FT= 27.690
ROUTE MCUNGE RT5UP *S SUB-BASIN 6A	P 43 21	.39980	107.92	45.030	2.11186	2.350	.422 CCODE = .2
*S Route Sub-basin 6A throu	A - 51 agh Pond 4	.27620	451.78	29.806	2.02337	1.650	2.556 PER IMP= 69.20
*S ROUTE FLOW THROUGH POND			54.33				
ROUTE RESERVOIR Pond4out *S Route Pond 4 outflow thr	: 51 52 rough 2000' o	.27620 of 42" pipe	64.33	29.393	1.99533	2.450	.364 AC-FT= 17.982
	A 52 53	.27620	64.32	29.384	1.99478	2.500	.364 CCODE = .2
*S Add Pond 4 outflow to 6B	3 - 6 3	.07550	184.93	7.873	1.95532	1.500	3.827 PER IMP= 65.00
*S SUB-BASIN 313	3 53& 6 54	.35170	186.00	37.258	1.98631	1.500	. 826
COMPUTE NM HYD 313.00 *S Add Sub-basin 313 to Basi	in 6	.05940	122.50	6.488	2.04812	1.550	3.222 PER IMP= 70.70
ADD HYD Pond2inflow *S ROUTE FLOW THROUGH POND 2	2	.41110	292.98	43.746	1.99524	1.500	1.114
*S ROUTE FLOW THROUGH POND ROUTE RESERVOIR Pond2out	WITH 42" OUT 22 41		10.22	42 425	3 03545	2 050	
*S Add outflow from Pond 2	to the Route			42.435	1.93545	3.950	.187 AC-FT= 14.199
*S Route Combined flow thro	2 21&41 23 Dugh 66" pipe	.81090 e for 700'	148.49	87.466	2.02243	2.500	. 286
	23 24		148.30	87.431	2.02162	2.550	.286 CCODE = .2
COMPUTE NM HYD 310.00 *S Add Sub-basin 310 to upst		.01140 _	27.94	1.189	1.95532	1.500	3.830 PER IMP= 65.00
ADD HYD RT313UP&310 *S Route Sub-basin 310 and	24& 8 25	.82230	149.03 pipe for 1000'	88.620	2.02070	2.550	. 283
ROUTE MCUNGE RT310UP *S SUB-BASIN 311S	25 26	.82230	148.77	88.578	2.01974	2.600	.283 CCODE = .2
*S Add Sub-basin 311S to ups		.02920 in pipe	72.19	3.090	1.98409	1.500	3.863 PER IMP= 66.70
ADD HYD RT310UP&311S *S Route Sub-basin 311S and	3 26& 9 27 1 upstream fl	.85150	150.59 " pipe for 150'	91.668	2.01852	2.550	. 276
ROUTE MCUNGE RT311SUP *S SUB-BASIN 311N	27 28	.85150	150.59	91.668	2.01852	2.550	.276 CCODE = .0
*S Add Sub-basin 311N to ups		.05060 in pipe	109.82	5.979	2.21552	1.550	3.391 PER IMP= 80.90
ADD HYD RT311SUP&311 *S SUB-BASIN 312	2S	.90210	210.02	97.647	2.02957	1.550	. 364
COMPUTE NM HYD 312.00 *S Add Sub-basin 312S to ups) - 11 stream flow i	.01270 into the pond	33.05	1.484	2.19032	1.500	4.066 PER IMP= 79.30
	FROM TO		PEAK	RUNOFF		TIME TO	CFS PAGE = 3
HYDROGRAPH		AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER
COMMAND IDENTIFICATION	NO. NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE NOTATION
ADD HYD RT311NUP&312	29&11 30	.91480	239.43	99.130	2.03180	1.550	.409

*S SUB-BASIN 8						
COMPUTE NM HYD 8.00 - 31 *S Add Sub-basin 8 to upstream flow into		.84 2.235	2.38065	1.700	2.649 PER IMP=	90.00
ADD HYD RT312SUP&8 30&31 32 *S ROUTE FLOW THROUGH POND WITH 60" OUTF	.93240 257	.78 101.365	2.03838	1.550	.432	
ROUTE RESERVOIR Pondout 32 41	.93240 131	.04 100.281	2.01660	3.700	.220 AC-FT=	16.017
*S Route POND OUTFLOW through 60" pipe f ROUTE MCUNGE RT311NUP 41 33	.93240 128		2.01133	3.800	.215 CCODE =	. 2
*S************************************	-)			
*\$***********						
S THE DOWNSTREAM FACE OF LAS VENTANAS D *S* BUENA VISTA AVE, TO LA PAZ RD, THRU B						
S NORTH SIDE OF PARADISE BLVD*******	****************	10 POND A1 * * * * * * * * * * * * * * * * * *				
S						
*S******* ***** PIEDRAS MARCADAS WATERS	HED***********	******				
*S******** CALC BASIN 316 FLOW ****	*****					
COMPUTE NM HYD 316.00 - 1 *S****** ROUTE 316 THRU 313N PARADISE*		.16 2.421	1.51308	1.500	3.133 PER IMP=	45.00
ROUTE MCUNGE RT316 1 2		.34 2.386	1.49151	1.750	2.778 CCODE =	. 1
*S********* CALC BASIN 313N FLOW ***		.51 2.500	1.47131	1.750	2.778 CCODE =	• T
COMPUTE NM HYD 313N - 3	.07800 135	.26 8.065	1.93878	1.600	2.709 PER IMP=	65.00
*S*** ADD RT316 TO 313N******* ADD HYD 313NUP 2& 3 4	.10800 171	.30 10.452	1.81453	1.700	2.478	
*S******** CALC BASIN 314 FLOW ****	*****					
COMPUTE NM HYD 314.00 - 5 *S*** ADD 313NUP TO 314******	.08900 185	.78 7.273	1.53229	1.500	3.262 PER IMP=	43.00
ADD HYD AP1-314UP 4& 5 6	-	.39 17.725	1.68702	1.550	2.351	
*S********** CALC BASIN 314.1 FLOW ** COMPUTE NM HYD AP2-314.1 - 7		.63 2.867	1.49321	1.500	3.239 PER IMP=	40.00
*S*** ADD 314UP TO 314.1 FOR DISCHARGE IN						
ADD HYD AP314.1UP 6& 7 8 *S****ROUTE AP314.1UP FLOW THROUGH PARK P		.30 20.592 RGE. ASSUME 48"	1.65707	1.550	2.436	
ROUTE RESERVOIR AP3-RT314.1P 8 9	.23300 108	.05 20.592	1.65707	2.050	.725 AC-FT=	9.449
*S****** ROUTE DISCHARGE THRU PIPE TO						
ROUTE MCUNGE 113.40 9 10 ************** CALC BASIN 312 FLOW ****		.02 20.584	1.65640	2.150	.724 CCODE =	.1
COMPUTE NM HYD 312.00 - 11		.49 19.641	1.82308	1.600	2.703 PER IMP=	59.10
*S*** ADD 113.4 TO 312******* ADD HYD AP4-312UP 10&11 12	.43500 403	.28 40.224	1.73380	1.600	1.449	
	(6/01)		6			
ADD HYD NewAP4 33&12 35 *S******** ROUTE DISCHARGE THRU PIPE TO		.97 140.243	1.92304	1.650	.484	
ROUTE MCUNGE RT312UP 35 13 *S********** CALC BASIN 312.1 FLOW **		.38 140.183	1.92221	1.650	.483 CCODE =	.1
COMPUTE NM HYD AP5-312.1 - 14		.56 1.361	1.82319	1.500	3.634 PER IMP=	59.00
*S*** ADD RT312UP TO 312.1******* ADD HYD AP312.1 13&14 15	1.38140 440	.17 141.544	1.92120	1.650	.498	
*S****** ROUTE THROUGH PIPE TO MH9 84"	*****					
ROUTE MCUNGE RT312.1 15 42 *S****** ROUTE DISCHARGE THRU PIPE TO		.48 141.520	1.92088	1.650	.496 CCODE =	. 2
FROM TO	PEAR	RUNOFF		TIME TO	CFS PAGE =	4
HYDROGRAPH ID ID	AREA DISCHA		RUNOFF	PEAK	PER PAGE	- 4
COMMAND IDENTIFICATION NO. NO.	(SQ MI) (CFS			(HOURS)	ACRE NOTATI	ON
ROUTE MCUNGE RT312.12 42 16 *S*CALABACILLAS WATERSHED***	1.38140 438	.48 141.520	1.92088	1.650	.496 CCODE =	.0
*S*********** CALC BASIN 101 FLOW ****	*****					
COMPUTE NM HYD 101.00 - 17		.51 4.959	1.82319	1.550	3.171 PER IMP=	59.00

	+ 6316 53673 165 576								
	* CALC BASIN 105 FLO								
COMPUTE NM HYD	105.00 -	18	.02100	48.83	2.042	1.82319	1.500	3.633 PER IMP=	59.00
*S*** ADD 101 TO	0 105******								
ADD HYD	105UP 17&18	19	.07200	146.78	7.001	1.82318	1.550	3.185	
*S***** ROUT	TE 105UP TO LYONS***	****							
ROUTE MCUNGE	RT105UP 19	20	.07200	146.47	6.985	1.81910	1.600	3.179 CCODE =	.1
*S*******	* CALC BASIN 105.1 F	FLOW *	*******				2.000	3.1/3 CCODE =	• ±
COMPUTE NM HYD	105.10 -	21	.00900	20.94	.875	1.82319	1.500	3.635 PER IMP=	59.00
*S*** ADD 105UP	TO 105.1******						2.500	J.OJJ IER INFE	33.00
ADD HYD	105.1UP 20&21	22	.08100	161.00	7.860	1.81954	1.600	3.106	
*S********	* CALC BASIN 107 FLO	*** WC	*******			2.01551	1.000	3.100	
COMPUTE NM HYD	107.00 -	23	.06700	119.80	6.515	1.82319	1.600	2.794 PER IMP=	FO 00
*S********	* CALC BASIN 108 FLO	>w * * *	*****	117.00	0.313	1.02517	1.000	2.794 PER IMP=	59.00
COMPUTE NM HYD	108.00 -	24	.01000	23.26	.972	1.82319	1.500	3.635 PER IMP=	
*S*** ADD 107 TO			.01000	23.20	. 572	1.02319	1.500	3.635 PEK IMP=	59.00
ADD HYD	108UP 23&24	25	.07700	137.35	7.487	1.82318	1 550	2 707	
	.1 TO AP108*****	23	:07700	137.33	7.407	1.02310	1.550	2.787	
ADD HYD	AP6-AP108UP 16&25	26	1.45840	560.91	140 000				
	* CALC BASIN 108.1 F			360.91	149.007	1.91572	1.650	.601	
COMPUTE NM HYD	108.10 ~	27		00					
		21	.01100	25.59	1.070	1.82319	1.500	3.634 PER IMP=	59.00
	TO 105.1UP******			•					
ADD HYD	AP7-AP108.1U 27&22		.09200	178.76	8.930	1.81997	1.600	3.036	
	TE DISCHARGE THRU PI								
ROUTE MCUNGE	RT312.1 26	29	1.45840	560.91	149.007	1.91572	1.650	.601 CCODE =	. 0
	.1 TO 108.1UP*****	r k							
ADD HYD	AP108.1UP 29&28	30	1.55040	728.51	157.937	1.91004	1.650	. 734	
FINISH									

- VERSION: 1997.02c

RUN DATE (MON/DAY/YR) =07/23/2003 USER NO.= AHYMO-S-9702c1BohanHu-AH

		FROM TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	1
COMMAND	HYDROGRAPH IDENTIFICATION	ID ID	AREA (SO MI)	DISCHARGE (CFS)	VOLUME (AC-FT)	RUNOFF	PEAK (HOURS)	PER ACRE	NOTATIO	
00111111			(52)	(0.07	(110 11)	(1110111111)	(HOURD)	nend	WOIRIL	214
*SUMMARY	1 MID. B	B. PIEDRAS- DE	V CONDS WITH	BULK - MODIFI	ED 7/95					
START									IME=	.00
RAINFALL TY									AIN24=	2.660
SEDIMENT BUL	K.							Р	K BF =	1.00
-	*****	******	******	*******	******					
_	YSIS FOR LAS VENT									
S	1010 1011 1110 11111	50551115	ION DIGILITION	INDIDIC I MA	*					
S TWO MAIN	SYSTEMS CONVEY F	LOWS TO THE L	ARGE POND IN	BASIN 316. T	THIS *					
S POND IS	CALLED "LAS VENTA	ANAS DRAINAGE	FACILITY NO.	1" (LVDF NO.	1). *					
S THE TWO I	MAIN SYSTEMS CONS	SIST OF ONE IN	THE NORTH A	ND ONE IN THE	SOUTH *					
S PART OF	THE SUBDIVISION.	NORTH IS THE	"WEST BRANC	H CALABACILLAS	*					
	N SYSTEM", AND SC	OUTH IS THE "N	ORTH BRANCH	PIEDRAS MARCAI	AS *					
S SYSTEM".					*					
-	*****				*****					
	BRANCH CALABACILI				*******					
S MAIN CHAI	NNEL IS "WEST BRA	ANCH CALABACIL	LAS DIVERSIO	N CHANNEL" ***						
~	**** CALC BASIN 5	502 FLOW ****	******							
COMPUTE NM H		- 1	.03400	74.39	3.148	1.73601	1.500	3 419 P	ER IMP=	59.00
	ROUTE DISCHARGE I	_		1100000		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1.500	3,		33.00
ROUTE	503W.1	1 2	.03400	70.85	3.148	1.73603	1.550	3.256		
*S***ROUTE	502 FLOW THROUGH	POND IN NEIGH	BORHOOD PARK	AT W SIDE OF	503W ****					
ROUTE RESERV	OIR 503W.2	2 3	.03400	13.24	3.148	1.73595	2.100	.608 A	C-FT=	1.647
*S******	ROUTE DISCHARGE 1	THRU 36" PIPE	IN BASIN 503	W (REACH 2) **	*****					
ROUTE	503W.3	3 2	.03400	13.24	3.148	1.73594	2.100	.608		
	**** CALC BASIN 5									
COMPUTE NM H			.14100	218.31	11.614	1.54445	1.600	2.419 F	ER IMP=	46.00
	503W FLOWS INTO C TO 42" PIPE IN F									
DIVIDE HYD	503M.1	RAINBOW (REACH	.11168	100.00	9.199	1.54445	1.450	1.399		
DIVIDE HID	503M.2		.02932	118.31	2.415	1.54445	1.600	6.304		
*S**** ROUT	E RAINBOW PIPE FI					1.51115	1.000	0.501		
ROUTE	503M.11	6 7	.11168	103.68	9.199	1.54445	1.500	1.451		
*S***ROUTE O	VERLAND FLOWS SOU	UTH ON RAINBOW	BLVD ****							
ROUTE	503M.21	4 8	.02932	117.74	2.416	1.54471	1.600	6.274		
*S*** ADD 50	3W OVERLAND AND E		RAINBOW & LO	OP RD******	*					
ADD HYD	503W.5		.14100	218.17	11.615	1.54450	1.600	2.418		
	3W FLOWS TO ROUTE			200 24	14 560					
ADD HYD	503W.6		.17500	228.34	14.762	1.58169	1.600	2.039		
COMPUTE NM H	**** CALC BASIN S		.07400	102.64	6.095	1.54445	1.650	2 167 1	ER IMP=	46 00
	504E FLOWS; (LOWI					1.54445	1.050	2.107 F	EK IMP=	40.00
DIVIDE HYD	504E.1		.03700	51.32	3.048	1.54444	1.650	2.167		
	504E.2		.03700	51.32	3.048	1.54444	1.650	2.167		
*S** ADD UPP	ER PART OF BASIN	504E TO ROUTE	D FLOWS FROM	503W POND **	*****					
ADD HYD	503W.7		.21200	278.35	17.810	1.57519	1.600	2.051		
	COMBINED FLOWS IN									
DIVIDE HYD	503W.71		.19523	185.00	16.401	1.57519	1.550	1.481		
+0+ DOIME 57	503W.72		.01677	93.35	1.409	1.57519	1.600	8.697		
-5- KOUTE PI	PE FLOWS IN 54" I	PIPE (REACH 3)	10 W BRANCH	CALABACILLAS	DIV CHAN ***					

BASIN 103

	нль	ROGRAPH	FROM ID	TO ID	AREA	PEAK DISCHARGE	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	1
COMMAND		CATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATIO	N
S		PROJECT	NAME:		BLVD STORM							
S *S*		JOB NO.	0028	MINI 1 0C4.01	DRAINAGE MAN	AGEMENT PLAN						
S		DATE: J										
S			,									
S		INPUT F	LE NA	ME: Op	t2_04.HYM							
S		OUTUPUT	FILE	NAME:	Opt2_04.out							
S		FILES LO	CATIO	N: BHI	-MAIN\00280\	HYDRO\DESIGN\A	MYMO					
	MMENTS:											
S	7-2-01:					B and adjusted						
S	6-01:			ge pond	near inters	ection of Para	dise					
S *S*		and Lyo	15									
S *S*	6-19-01:	Added ti	he BHT	study	of the LYONS	S SD done in 99						
S	0 15 01.				additional							
S												
S												
S	6-01: Ad	dded Basi	n 8									
S												
S	5-16-01:	Revised	Basir	ıs 1&2 a	nd added Bas	sin 7						
S	F 0 01	Di- 31	5 has	been by	okon into co	word smaller	basins					
S	5-9-01:	Basin 31	5 nas	been br	oken into se	everal smaller	Dasilis					
S *S*												
*S		4-2-01	: Bas	ins are	based on th	ose used in pr	evious report	S				
*S		in this	s area	. origi	nally from M	lolzen-Corbin's	Piedras					
*S						; however, bas						
*S						new mapping and						
*S		maximur	m drai	nable a	rea (based c	on slope).						
*S												
		//////////	/////	'///////	777777777777777777777777777777777777777	///////////////////////////////////////	///////////////////////////////////////				RAIN24=	2.700
	TYPE= 2										PK BF =	1.02
SEDIMENT	BOLK										rk bi	1.02
*S *S	SUB-BASIN 1											
COMPUTE 1		1.00	_	1	.03540	88.50	3.818	2.02214	1.500	3.906	PER IMP=	69.00
*S												
*S Route	Basin 1 thr	ough 4.5'	pipe	for 135	0'							_
ROUTE MC	UNGE	RT1	1	12	.03540	77.57	3.759	1.99087	1.550	3.424	CCODE =	. 2
*S	SUB-BASIN 2							0 10400	1 500	4 000	DED TMD	70 10
COMPUTE I		2.00	-	2	.02490	65.15	2.902	2.18492	1.500	4.088	PER IMP=	79.10
	Sub-basin 2					126.04	6.660	2.07098	1.500	3.548		
ADD HYD	o Cub bagin	RT1&2			.06030	136.94 20' of 66" pip		2.07090	1.500	3.540		
*S Route		RT2UP	13	14	.06030	130.44	6.611	2.05566	1.550	3.380	CCODE =	. 2
	SUB-BASIN 3	111201										
COMPUTE		3.00	_	3	.10070	185.06	11.639	2.16716	1.650	2.871	PER IMP=	78.00
*S Add	Sub-basin 3	to upstre	am fl	ow in p	i pe							
ADD HYD		RT2UP&3			.16100	308.27	18.250	2.12539	1.600	2.992		
*S Rout	e Sub-basin	3 and the	upst	ream flo	ow through 5	30' of 90" pip	е					
			EDOM	TO		PEAK	RUNOFF '		TIME TO	CFS	PAGE =	2
	ยข	DROGRAPH	FROM ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER	111011 -	1.86
	H I	DROGRAPH	עג	עג	ARBA	DISCHARGE	VOLIGILL	1011011	E 404 417	1 111		

COMMAND	IDENTIFICATION	NO. N	10. (SQ M	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATIO	N
ROUTE MCUNGE	RT3UP	15	.161	300.99	18.201	2.11970	1.600	2.921 CC	CODE =	. 2
COMPUTE NM H		am flow	4 .162	361.61	18.848	2.18149	1.550	3.488 PE	ER IMP=	78.80
ADD HYD	RT3UP&4 Sub-basin 4 and up	16& 4	.323		37.049	2.15069	1.550	3.091		
ROUTE MCUNGE			18 .323			2.14196	1.600	3.020 CC	CODE =	. 2
COMPUTE NM F		- am flow	5 .043	106.46	4.542	1.96678	1.500	3.842 PE	ER IMP=	65.70
ADD HYD	RT4UP&5 ub-basin 5 and ups	18& 5	.366			2.12126	1.550	3.017		
ROUTE MCUNGE			20 .366		41.204	2.10915	1.600	2.907 C	CODE =	. 2
COMPUTE NM F			30 .033 in pipe	50 66.49	3.913	2.18983	1.600	3.101 P	ER IMP=	79.50
ADD HYD	RT5UP&6&7 ub-basin 7 and up:	20&30	31 .399			2.11591	1.600	2.923		
ROUTE MCUNGI			21 .399			2.10870	1.600	2.852 C	CODE =	. 2
COMPUTE NM I			51 .276	20 451.78	29.806	2.02337	1.650	2.556 PI	ER IMP=	69.20
ROUTE MCUNG			52 . 276	20 451.17	29.806	2.02338	1.700	2.552 C	CODE =	. 2
COMPUTE NM 1		- outed 6A	6 .075	50 184.93	7.873	1.95532	1.500	3.827 P	ER IMP=	65.00
ADD HYD		52& 6	53 .351		37.679	2.00877	1.650	2.376		
ADD HYD		21&53			82.642	2.06193	1.650	2.606		
COMPUTE NM			7 .059 w in pipe	40 122.50	6.488	2.04812	1.550	3.222 P	ER IMP=	70.70
ADD HYD	RT6UP&313 ub-basin 313 and	22& 7	23 .810			2.06092	1.600	2.624		
ROUTE MCUNG						2.05476	1.650	2.589 C	CODE =	.2
COMPUTE NM			8 .011	40 27.94	1.189	1.95532	1.500	3.830 P	ER IMP=	65.00
ADD HYD	RT313UP&310 ub-basin 310 and	24&8	25 .822			2.05338	1.650	2.582		
ROUTE MCUNG			26 .822			2.04504	1.650	2.530 C	CODE =	. 2
COMPUTE NM			9 .029	20 72.19	3.090	1.98409	1.500	3.863 P	ER IMP=	66.70
ADD HYD	RT310UP&311S ub-basin 311S and	26& 9	27 .85:			2.04295	1.650	2.515		
ROUTE MCUNG	E RT311SUP SUB-BASIN 311N	27	28 .85	.50 1370.55	92.777	2.04295	1.650	2.515 C	CODE =	. 0
COMPUTE NM			10 .050	109.82	5.979	2.21552	1.550	3.391 P	ER IMP=	80.90
ADD HYD	RT311SUP&311 SUB-BASIN 312	28&10		210 1463.34	98.756	2.05262	1.650	2.535		
	UVDDOCDADE	FROM	TO AR:	PEAK EA DISCHARGE	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	3
COMMAND	HYDROGRAPH IDENTIFICATION		NO. (SQ)		(AC-FT)		(HOURS)	ACRE	NOTATIO	ON
COMPUTE NM	HYD 312.00	-	11 .01	270 33.05	1.484	2.19032	1.500	4.066 P	ER IMP=	79.30

*S Add Sub-basin 312S to upstream flow into the pond	
ADD HYD RT311NUP&312 29&11 30 .91480 1481	.53 100.239 2.05453 1.650 2.530
*S SUB-BASIN 8	
	.84 2.235 2.38065 1.700 2.649 PER IMP= 90.00
*S Add Sub-basin 8 to upstream flow into the pond	100 454
ADD HYD RT312SUP&8 30&31 32 .93240 1509	.49 102.474 2.06069 1.650 2.530
*S ROUTE FLOW THROUGH POND WITH 60" OUTFLOW PIPE	00 00 107 1 004E0 2 500 202 NG FFF 6F 410
ROUTE RESERVOIR Pondout 32 41 .93240 173	.98 99.187 1.99459 2.500 .292 AC-FT= 65.410
*S Route POND OUTFLOW through 72" pipe for 300'	03 00 166 1 00416 3 500 201 00000
ROUTE MCUNGE RT311NUP 41 33 .93240 173	
*S******************FROM FORMER BHI REPORT ON LYONS SD_ MODIFIE	ED FOR INCREASED
*S*** FLOWS *S**********************************	
S THE DOWNSTREAM FACE OF LAS VENTANAS DRAINAGE FACILITY DRAIN	
S THE DOWNSTREAM FACE OF LAS VENTANAS DRAINAGE FACILITY DRAIN *S* BUENA VISTA AVE, TO LA PAZ RD, THRU BASIN 314, AND FINALLY	
S NORTH SIDE OF PARADISE BLVD************************************	**************************************
S NORTH SIDE OF PARADISE BLVD	
*S************************************	*******
*S********* CALC BASIN 316 FLOW **********	
-	.16 2.421 1.51308 1.500 3.133 PER IMP= 45.00
*S****** ROUTE 316 THRU 313N PARADISE******	.10 2.122 1.32300 2.300 3.233 12.0 13.00
-	.34 2.386 1.49151 1.750 2.778 CCODE = .1
*S****************** CALC BASIN 313N FLOW ************	
	.26 8.065 1.93878 1.600 2.709 PER IMP= 65.00
*S*** ADD RT316 TO 313N*******	
	30 10.452 1.81453 1.700 2.478
*S******* CALC BASIN 314 FLOW **********	
	5.78 7.273 1.53229 1.500 3.262 PER IMP= 43.00
*S*** ADD 313NUP TO 314******	
	5.39 17.725 1.68702 1.550 2.351
*S******* CALC BASIN 314.1 FLOW **********	
COMPUTE NM HYD AP2-314.1 - 7 .03600 74	1.63 2.867 1.49321 1.500 3.239 PER IMP= 40.00
*S*** ADD 314UP TO 314.1 FOR DISCHARGE INTO POND*******	
	3.30 20.592 1.65707 1.550 2.436
*S****ROUTE AP314.1UP FLOW THROUGH PARK POND W/ ASSUMED DISCHA	ARGE. ASSUME 48" D
	3.05 20.592 1.65707 2.050 .725 AC-FT= 9.449
*S****** ROUTE DISCHARGE THRU PIPE TO UNSER LYONS ******	
ROUTE MCUNGE 113.40 9 10 .23300 108	3.02 20.584 1.65640 2.150 .724 CCODE = .1
*S******** CALC BASIN 312 FLOW **********	
COMPUTE NM HYD 312.00 - 11 .20200 349	9.49 19.641 1.82308 1.600 2.703 PER IMP= 59.10
*S*** ADD 113.4 TO 312******	
122 1112	3.28 40.224 1.73380 1.600 1.449
*S****ADD NEW FLOW FROM SOUTH UNSER SD (6/01)	
1	7.98 139.390 1.91134 1.650 .500
*S****** ROUTE DISCHARGE THRU PIPE TO ESSEX 84"******	1 650 405 6000
	5.37 139.330 1.91051 1.650 497 CCODE = .1
*S*********** CALC BASIN 312.1 FLOW **********	5
	2.56 1.361 1.82319 1.500 3.634 PER IMP= 59.00
*S*** ADD RT312UP TO 312.1*******	3 16 140 601 1 00060 1 660 E13
	3.16 140.691 1.90962 1.650 .513
*S****** ROUTE THROUGH PIPE TO MH9 84"******	
FROM TO PEAR	K RUNOFF TIME TO CFS PAGE = 4
HYDROGRAPH ID ID AREA DISCHA	
COMMAND IDENTIFICATION NO. NO. (SQ MI) (CFS	
CONTINUED IDENTIFICATION NO. NO. 130 MI) (CIT	of the sal through the state that the sales
ROUTE MCUNGE RT312-1 15 42 1.38140 449	9.64 140.663 1.90925 1.650 .509 CCODE2
*S****** ROUTE DISCHARGE THRU PIPE TO ALDER 84"*****	
	9.64 140.663 1.90925 1.650 .509 CCODE = .0
*S*CALABACILLAS WATERSHED***	

*S****** CA	LC BASIN 101 FLOW	********						
COMPUTE NM HYD	101.00 - 1	.7 .05100	103.51	4.959	1.82319	1.550	3.171 PER IMP=	59.00
*S********** CA								
COMPUTE NM HYD	105.00 - 1	.8 .02100	48.83	2.042	1.82319	1.500	3.633 PER IMP=	59.00
*S*** ADD 101 TO 10	5*****							
ADD HYD	105UP 17&18 1	.9 .07200	146.78	7.001	1.82318	1.550	3.185	
*S***** ROUTE 1	DSUP TO LYONS****	**						
ROUTE MCUNGE	RT105UP 19 2	.07200	146.47	6.985	1.81910	1.600	3.179 CCODE =	. 1
*S*********** CA	LC BASIN 105.1 FLO	W *********	* *					
COMPUTE NM HYD		.00900	20.94	. 875	1.82319	1.500	3.635 PER IMP=	59.00
*S*** ADD 105UP TO	105.1******							
ADD HYD		.08100	161.00	7.860	1.81954	1.600	3.106	
*S*********** CA	LC BASIN 107 FLOW	******						
COMPUTE NM HYD		.06700	119.80	6.515	1.82319	1.600	2.794 PER IMP=	59.00
*S***** CA		******						
COMPUTE NM HYD		.01000	23.26	. 972	1.82319	1.500	3.635 PER IMP=	59.00
*S*** ADD 107 TO 10								
ADD HYD		.07700	137.35	7.487	1.82318	1.550	2.787	
*S*** ADD RT312.1 T								
		26 1.45840		148.151	1.90471	1.650	.613	
*S****** CA								
COMPUTE NM HYD		.01100	25.59	1.070	1.82319	1.500	3.634 PER IMP=	59.00
*S*** ADD 108.1 TO								
		.09200		8.930	1.81997	1.600	3.036	
*S***** ROUTE D								
ROUTE MCUNGE		29 1.45840	572.08	148.151	1.90471	1.650	.613 CCODE =	. 0
*S*** ADD RT312.1 T								
	AP108.1UP 29&28	30 1.55040	739.68	157.081	1.89968	1.650	.745	
FINISH								

- VERSION: 1997.02c

RUN DATE (MON/DAY/YR) =07/05/2001 USER NO.= AHYMO-S-9702c1BohanHu-AH

	_											
COMMAND		ROGRAPH ICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE =	1
COMMINA	IDDMIII	ICATION	110.	110.	(50 111)	(CIS)	(AC II)	(INCIES)	(HOURS)	ACRE	NOTATIO	VIA.
S		PROJECT	NAME:	LYONS	BLVD STORM I	ORATN						
S		INCOLCI			DRAINAGE MANA							
S		JOB NO.	0028									
S		DATE:										
S												
S		INPUT F	ILE NA	ME: Op	t1_06.HYM							
S		OUTUPUT	FILE	NAME:	Opt1_06.out							
S		FILES L	OCATIO	N: BHI	-MAIN\00280\I	HYDRO\DESIGN\AH	YMO					
S COMME												
S	6-29-01:				into 6A and 6							
S	6-19-01:					SD done in 99						
S		and mod	lified	for the	additional:	tlows						
S												
S	C 01 3 m	D:	O									
S *S*	6-01: Ad	ded Basi	.11 8									
S	5-16-01.	Peviced	l Bacir	ne 1.2 =	nd added Bas	in 7						
S	3-10-01.	KEVISEO	Dasii	15 102 0	ind added bas	LII /						
S	5-9-01:	Basin 31	5 has	been br	oken into se	veral smaller b	asins					
S	5 7 02.											
S												
*S		4-2-01	: Bas	ins are	based on the	se used in pre	vious report	S				
*S		in thi	s area	, origi	nally from Mo	olzen-Corbin's	Piedras					
*S						however, basi						
*S						ew mapping and	the					
*S		maximu	m drai	nable a	rea (based or	n slope).						
*S	,,,,,,,,,		,,,,,,									
		///////////////////////////////////////	//////	(///////	///////////////////////////////////////	///////////////////////////////////////	/////////				DATNOA	2 700
RAINFALL T											RAIN24=	2.700
SEDIMENT BU	LK										PK BF =	1.02
	B-BASIN 1											
COMPUTE NM		1.00	_	1	03540	88.50	3.818	2.02214	1.500	3.906	PER IMP=	69.00
*S				_	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	00100				2,12,00		0,,00
*S Route Ba	sin 1 thro	ough 4.5	pipe	for 135	50'							
ROUTE MCUNG		RT1	ì	12	.03540	77.57	3.759	1.99087	1.550	3.424	CCODE =	. 2
*S SU	B-BASIN 2											
COMPUTE NM	HYD	2.00	-	2	.02490	65.15	2.902	2.18492	1.500	4.088	PER IMP=	79.10
*S Add Sub	-basin 2 a											
ADD HYD			12& 2		.06030	136.94	6.660	2.07098	1.500	3.548		
			_		_	0' of 66" pipe						
ROUTE MCUNG		RT2UP	13	14	.06030	130.44	6.611	2.05566	1.550	3.380	CCODE =	. 2
	-BASIN 3	2 00		2	10070	105.06	11 620	2 16716	1 (50	2 071	DED IMD	70 00
COMPUTE NM *S Add Sub		3.00	- 	3 ow in n	.10070	185.06	11.639	2.16716	1.650	2.871	PER IMP=	78.00
ADD HYD	-Dasili 3	RT2UP&3			.16100	308.27	18.250	2.12539	1.600	2.992		
	Sub-basin					0' of 90" pipe	10.230	2.12337	1.000	2.552		
ROUTE MCUNG		RT3UP		16	.16100	300.99	18.201	2.11970	1.600	2.921	CCODE =	. 2
	B-BASIN 4							0				
_												
			FROM			PEAK	RUNOFF		TIME TO	CFS	PAGE =	2
	HY	DROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER		
COMMAND	IDENTI	FICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATIO	NC

COMPUTE NM HYD 4.00 -		361.61	18.848	2.18149	1.550	3.488 PER IMP=	78.80
*S Add Sub-basin 4 to upstream flow: ADD HYD RT3UP&4 16& 4 1		638.94	37.049	2.15069	1.550	3.091	
*S Route Sub-basin 4 and upstream f						- · · · - · · ·	
ROUTE MCUNGE RT4UP 17 1: *S SUB-BASIN 5	8 .32300	624.22	36.899	2.14196	1.600	3.020 CCODE =	. 2
COMPUTE NM HYD 5.00 - S Add Sub-basin 5 to upstream flow		106.46	4.542	1.96678	1.500	3.842 PER IMP=	65.70
ADD HYD RT4UP&5 18& 5 1		707.27	41.441	2.12126	1.550	3.017	
*S Route Sub-basin 5 and upstream flo							
ROUTE MCUNGE RT5UP 19 2 *S SUB-BASIN 7	0 .36630	681.43	41.204	2.10915	1.600	2.907 CCODE =	. 2
COMPUTE NM HYD 7.00 - 3	0 .03350	66.49	3.913	2.18983	1.600	3.101 PER IMP=	79.50
*S Add Sub-basin 7 to upstream flow							
ADD HYD RT5UP&6&7 20&30 3		747.93	45.117	2.11591	1.600	2.923	
*S Route Sub-basin 7 and upstream flor ROUTE MCUNGE RT7UP 31 2			44 002	2 10070	1 600	2 052 00000	-
ROUTE MCUNGE RT7UP 31 2 *S SUB-BASIN 6A	1 .39980	729.73	44.963	2.10870	1.600	2.852 CCODE =	. 2
COMPUTE NM HYD 6A - 5	1 .27620	451.78	29.806	2.02337	1.650	2.556 PER IMP=	69,20
*S Route Sub-basin 6A through 2500'		151.70		2.0255.		I DR I.IF-	05.20
ROUTE MCUNGE RT6A 51 5		451.17	29.806	2.02338	1.700	2.552 CCODE =	. 2
*S SUB-BASIN 6B							
	6 .07550	184.93	7.873	1.95532	1.500	3.827 PER IMP=	65.00
*S Add Sub-Basin 6B to the Routed 6A	2 25120	E24 25	27 670	3 00033	1 (50	2 276	
ADD HYD RT6A&6B 52& 6 5 *S Add Sub-basin 6A and 6B to upstre		534.75	37.679	2.00877	1.650	2.376	
ADD HYD RT5UP&6 21&53 2		1253.30	82.642	2.06193	1.650	2.606	
*S SUB-BASIN 313	,5150			2.03203	2.330		
COMPUTE NM HYD 313.00	7 .05940	122.50	6.488	2.04812	1.550	3.222 PER IMP=	70.70
*S Add Sub-basin 313 to upstream flow							
ADD HYD RT6UP&313 22& 7 2			89.131	2.06092	1.600	2.624	
*S Route Sub-basin 313 and upstream			00 064	2 05476	1 (50	2 F00 CCODE	3
ROUTE MCUNGE RT313UP 23 2 *S SUB-BASIN 310	4 .81090	1343.45	88.864	2.05476	1.650	2.589 CCODE =	. 2
_	8 .01140	27.94	1.189	1.95532	1.500	3.830 PER IMP=	65.00
*S Add Sub-basin 310 to upstream flow		21.74	1.107	2.222	1.500	J.050 PER IMP	03.00
ADD HYD RT313UP&310 24& 8 2	5 .82230		90.053	2.05338	1.650	2.582	
*S Route Sub-basin 310 and upstream							
ROUTE MCUNGE RT310UP 25 2	6 .82230	1331.34	89.687	2.04504	1.650	2.530 CCODE =	. 2
*S SUB-BASIN 311S		5 0.00	2 22-				
	9 .02920	72.19	3.090	1.98409	1.500	3.863 PER IMP=	66.70
*S Add Sub-basin 311S to upstream flo ADD HYD RT310UP&311S 26& 9 2		1370.55	92.777	2.04295	1.650	2.515	
*S Route Sub-basin 311S and upstream			22.111	2.04233	1.000	ر ـ د . ـ ـ	
ROUTE MCUNGE RT311SUP 27 2			92.777	2.04295	1650	2.515 CCODE =	. 0
*S SUB-BASIN 311N							
	.05060	109.82	5.979	2.21552	1.550	3.391 PER IMP=	80.90
*S Add Sub-basin 311N to upstream flo							
ADD HYD RT311SUP&311 28&10 2				2.05262	1.650	2.535	
*S Route Sub-basin 311N and upstream ROUTE MCUNGE RT311NUP 29			98.074	2.03846	1.650	2.437 CCODE =	. 2
*S SUB-BASIN 312S	.50210	1407.20	20.074	2.03040	7.030	2.437 CCODE =	. 4
	10	201	BINIOEE		m	ana	
FROM T		PEAK	RUNOFF	DIMORE	TIME TO PEAK	CFS PAGE =	= 3
HYDROGRAPH ID I COMMAND IDENTIFICATION NO. N		DISCHARGE (CFS)	VOLUME (AC-FT)	RUNOFF (INCHES)	(HOURS)	PER ACRE NOTATI	LON
COMMUNICATION NO. IN	(50 MI)	(Cr5)	(110-11)	(INCILLS)	(11001037	ACKE MOTATI	. 014
COMPUTE NM HYD 312.00 - 1 *S Add Sub-basin 312S to upstream flo	.01270 ow in pipe	33.05	1.484	2.19032	1.500	4.066 PER IMP=	79.30

ADD HYD RT311NUP&312 30&11 31 .91480 *S Route Sub-basin 312S and upstream flow through 156" ROUTE MCUNGE RT312SUP 31 32 .91480	1425.39 pipe for 10 1425.39	99.558 00' 99.558	2.04057	1.650	2.435 2.435 CCODE =	. 0
*S SUB-BASIN 8 COMPUTE NM HYD 8.00 - 33 .01760	29.84	2.235	2.38065	1.700		
*S Add Sub-basin 8 to upstream flow in pipe	25.04	2.233	2.30003	1.700	2.649 PER IMP=	90.00
ADD HYD RT312SUP&8 32&33 34 .93240	1453.35	101.793	2.04699	1.650	2.435	
*S************************************	MODIFIED FO	R INCREASED				
*S*** FLOWS *S**********************************						
S THE DOWNSTREAM FACE OF LAS VENTANAS DRAINAGE FACILI						
S BUENA VISTA AVE, TO LA PAZ RD, THRU BASIN 314, AND	FINALLY TO F	OND AT****				
S NORTH SIDE OF PARADISE BLVD******************						
S						
*S*************PIEDRAS MARCADAS WATERSHED********	*******	******				
*S******** CALC BASIN 316 FLOW ************************************	60.16	0.404				
COMPUTE NM HYD 316.00 - 1 .03000 *S****** ROUTE 316 THRU 313N PARADISE******	60.16	2.421	1.51308	1.500	3.133 PER IMP=	45.00
ROUTE MCUNGE RT316 1 2 .03000	53.34	2.386	1.49151	1.750	2.778 CCODE =	7
*S******** CALC BASIN 313N FLOW *********	22.24	2.300	1.49131	1.750	2.778 CCODE =	. 1
COMPUTE NM HYD 313N - 3 .07800	135.26	8.065	1.93878	1.600	2.709 PER IMP=	65.00
*S*** ADD RT316 TO 313N******						00.00
ADD HYD 313NUP 2& 3 4 .10800	171.30	10.452	1.81453	1.700	2.478	
*S******** CALC BASIN 314 FLOW ************************************	105 50					
COMPUTE NM HYD 314.00 - 5 .08900 *S*** ADD 313NUP TO 314******	185.78	7.273	1.53229	1.500	3.262 PER IMP=	43.00
ADD HYD AP1-314UP 4& 5 6 .19700	296.39	17.725	1.68702	1.550	2.351	
*S******* CALC BASIN 314.1 FLOW *********	230.33	17.725	1.00702	1.330	2.331	
COMPUTE NM HYD AP2-314.1 - 7 .03600	74.63	2.867	1.49321	1.500	3.239 PER IMP=	40.00
*S*** ADD 314UP TO 314.1 FOR DISCHARGE INTO POND******						
ADD HYD AP314.1UP 6& 7 8 .23300	363.30	20.592	1.65707	1.550	2.436	
*S****ROUTE AP314.1UP FLOW THROUGH PARK POND W/ ASSUME ROUTE RESERVOIR AP3-RT314.1P 8 9 .23300		ASSUME 48" D		2.050	205 10 77	
********** ROUTE DISCHARGE THRU PIPE TO UNSER LYONS **	108.05	20.592	1.65707	2.050	.725 AC-FT=	9.449
ROUTE MCUNGE 113.40 9 10 .23300	108.02	20.584	1.65640	2.150	.724 CCODE =	. 1
*S****** CALC BASIN 312 FLOW **********	2-0102	20.301	1.05010	2.130	. /24 CCODE =	. 1
COMPUTE NM HYD 312.00 - 11 .20200	349.49	19.641	1.82308	1.600	2.703 PER IMP=	59.10
*S*** ADD 113.4 TO 312******						
ADD HYD AP4-312UP 10&11 12 .43500 *S****ADD NEW FLOW FROM SOUTH UNSER SD (6/01)	403.28	40.224	1.73380	1.600	1.449	
*S*****ADD NEW FLOW FROM SOUTH UNSER SD (6/01) ADD HYD NewAP4 34&12 35 1.36740	1853.85	142.017	1.94735	1.650	2 110	
*S****** ROUTE DISCHARGE THRU PIPE TO ESSEX 144" for			1.74/33	1.650	2 118	
ROUTE MCUNGE RT312UP 35 13 1.36740	1853.85	142.017	1.94735	1.650	2.118 CCODE =	. 0
*S******* CALC BASIN 312.1 FLOW **********					1	
COMPUTE NM HYD AP5-312.1 - 14 .01400	32.56	1.361	1.82319	1.500	3.634 PER IMP=	59.00
*S*** ADD RT312UP TO 312.1******* ADD HYD AP312.1 13&14 15 1.38140	1071 (4	1.2 200				
ADD HYD AP312.1 13&14 15 1.38140 *S************ ROUTE DISCHARGE THRU PIPE TO ALDER 144" for	1871.64	143.378	1.94609	1.650	2.117	
ROUTE MCUNGE RT312.1 15 16 1.38140	1857.49	143.306	1.94512	1.650	2.101 CCODE =	2
*S*CALABACILLAS WATERSHED***	11	113.000	1.71512	1.030	2.101 CCODE	
*S******* CALC BASIN 101 FLOW **********						
TDOW TO		n.n		100		
FROM TO HYDROGRAPH ID ID AREA	PEAK DISCHARGE	RUNOFF	DIMORE	TIME TO	CFS PAGE	= 4
COMMAND IDENTIFICATION NO. NO. (SQ MI)	(CFS)	VOLUME (AC-FT)	RUNOFF (INCHES)	PEAK (HOURS)	PER ACRE NOTAT	TON
(of htt)	(0.0)	(110-11)	(111011110)	(110011)	ACRE NOTAL	1 014
COMPUTE NM HYD 101.00 - 17 .05100	103.51	4.959	1.82319	1.550	3.171 PER IMP=	59.00
*S******* CALC BASIN 105 FLOW ************************************						
COMPUTE NM HYD 105.00 - 18 .02100 *S*** ADD 101 TO 105*******	48.83	2.042	1.82319	1.500	3.633 PER IMP=	59.00
"B" " ADD 101 10 105						

ADD HYD	105UP 17&18	19	.07200	146.78	7.001	1.82318	1.550	3.185		
*S****** ROUTE 105UP TO LYONS******										
ROUTE MCUNGE	RT105UP 19	20	.07200	146.47	6.985	1.81910	1.600	3.179 CCODE =	. 1	
*S******	CALC BASIN 105.1 F	LOW **	*********	•						
COMPUTE NM HYD	105.10 -	21	.00900	20.94	875	1.82319	1.500	3.635 PER IMP=	59.00	
*S*** ADD 105UP TO) 105.1******									
ADD HYD	105.1UP 20&21		.08100	161.00	7.860	1.81954	1.600	3.106		
*S******	CALC BASIN 107 FLC)M ****	******			**				
COMPUTE NM HYD	107.00	23	.06700	119.80	6.515	1.82319	1.600	2.794 PER IMP=	59.00	
*S******	CALC BASIN 108 FLC)M ****	*****							
COMPUTE NM HYD	108.00	24	.01000	23.26	.972	1.82319	1.500	3.635 PER IMP=	59.00	
*S*** ADD 107 TO 1	.08******									
ADD HYD	108UP 23&24	25	.07700	137.35	7.487	1.82318	1.550	2.787		
*S*** ADD RT312.1	TO AP108******									
ADD HYD A	AP6-AP108UP 16&25	26	1.45840	1979.92	150.793	1.93868	1.650	2.121		
*S******	CALC BASIN 108.1 F	FLOW **	******	r e						
COMPUTE NM HYD	108.10 -	27	.01100	25.59	1.070	1.82319	1.500	3.634 PER IMP=	59.00	
*S*** ADD 108.1 TO) 105.1UP******									
ADD HYD AF	77-AP108.1U 27&22	28	.09200	178.76	8.930	1.81997	1.600	3.036		
*S***** ROUTE	DISCHARGE THRU PI	PE TO	IRVING 144" 1	or 500'*****						
ROUTE MCUNGE	RT312.1 26	29	1.45840	1834.36	148.629	1.91085	1.700	1.965 CCODE =	. 2	
*S*** ADD RT312.1	TO 108.1UP******	**								
ADD HYD	AP108.1UP 29&28	30	1.55040	1983.23	157.559	1.90546	1.650	1.999		
FINISH										

COMMAND IDENTIFICATION NO. NO. (SQ MI) (CFS) (AC-FT) (INCHES) (HOURS) ACRE NOTAT ROUTE 318BW.1 1 4 .04300 91.05 3.981 1.73602 1.500 3.309 *S**********************************	
*S****** ADD 318A TO "TRIB A" ***********************************	59.00
ADD HYD 318BW.2 4& 6 3 .36100 547.85 32.964 1.71213 1.600 2.371	59.00
*S****** ROUTE THRU "TRIB A" CHAN IN 318BW ******	59.00
ROUTE 318BW.3 3 2 .36100 543.61 32.964 1.71213 1.650 2.353 *S**********************************	59.00
COMPUTE NM HYD 318BW - 1 .12200 248.67 11.296 1.73601 1.500 3.185 PER IMP= *S***********************************	
ADD HYD 318BW.4 2& 1 3 .48300 739.23 44.260 1.71816 1.600 2.391 ************************************	
COMPUTE NM HYD 319A - 1 .57200 935.79 52.960 1.73601 1.600 2.556 PER IMP= ************************************	59.00
ROUTE 319B.1 1 2 .57200 936.29 52.960 1.73601 1.600 2.558 *S**********************************	
COMPUTE NM HYD 319B - 1 .02300 48.22 1.959 1.59702 1.500 3.276 PER IMP= *S***********************************	50.00
ADD HYD 319B.2 1& 2 4 .59500 969.97 54.919 1.73064 1.600 2.547 *S***********************************	
ROUTE 318BW.5 4 5 .59500 970.10 54.919 1.73064 1.600 2.548 *S***********************************	
ADD HYD WELLSITE 3& 5 4 1.07800 1709.33 99.179 1.72505 1.600 2.478 **** ROUTE THRU 318BE; "N BRANCH PIEDRAS MARCADAS CHANNEL" ************************************	
ROUTE 318BE.1 4 3 1.07800 1693.32 99.179 1.72505 1.600 2.454 ***********************************	
COMPUTE NM HYD 318BE - 1 .14800 218.05 12.771 1.61791 1.600 2.302 PER IMP= *S***********************************	51.00
ADD HYD 318BE.2 3& 1 4 1.22600 1911.37 111.950 1.71212 1.600 2.436 ************************************	
COMPUTE NM HYD 317B - 1 .13400 215.23 11.878 1.66202 1.600 2.510 PER IMP= *S***********************************	54.00
ADD HYD 318BE.3 4& 1 2 1.36000 2126.60 123.827 1.70718 1.600 2.443 **S*********************************	
ROUTE 318BE.4 2 13 1.36000 2129.57 123.827 1.70718 1.650 2.447	
COMPUTE NM HYD 601.00 - 1 .02000 43.77 1.852 1.73601 1.500 3.419 PER IMP= *S***********************************	59.00
ROUTE 602.10 1 2 .02000 34.46 1.852 1.73604 1.550 2.692	
COMPUTE NM HYD 602.00 - 1 .06400 100.72 5.825 1.70653 1.600 2.459 PER IMP= *S***********************************	57.00
ADD HYD 602.20 2& 1 4 .08400 134.94 7.677 1.71354 1.600 2.510 *S***********************************	
ROUTE 602.30 4 5 .08400 109.23 7.677 1.71355 1.700 2.032	
COMPUTE NM HYD 317A - 20 .01700 37.20 1.574 1.73601 1.500 3.419 PER IMP= *S* FLOWS FROM BASIN 317A GO EAST, AND DO NOT ENTER LAS VENTANAS. PER ADDENDUM *S* DATED 7/20/95.	59.00
*S***ROUTE 601/602/317A OVERLAND NORTH ON UNIVERSE BLVD **** ROUTE 316SW.1 5 12 .08400 90.82 7.677 1.71355 1.850 1.689	
*S*** ADD OVERLAND FLOW TO N BRANCH PIEDRAS MARCADAS CHAN FLOWS ******** ADD HYD	

HYDROGRAPH ID ID AREA DISCHARGE VOLUME RUNOFF PEAK PER COMMAND IDENTIFICATION NO. NO. (SQ MI) (CFS) (AC-FT) (INCHES) (HOURS) ACRE NOTATION	1
COMMAND IDENTIFICATION NO. NO. (SQ MI) (CFS) (AC-FT) (INCHES) (HOURS) ACRE NOTATION	1
COMPUTE NM HYD 316SW - 1 .07600 130.48 7.144 1.76261 1.600 2.683 PER IMP= 6	50.00
ADD HYD 316SW.3 1& 4 5 1.52000 2297.59 138.648 1.71030 1.650 2.362 *S***** ROUTE COMBINED FLOWS THRU N BRANCH PM CHAN IN BASIN 316SW *******	
ROUTE 316SW.4 5 3 1.52000 2312.53 138.648 1.71030 1.650 2.377	
*S** SUM N BRANCH PIED MARC CHAN AND W BRANCH CALABACILLAS DIVERSION CHAN ***	
ADD HYD 316SW.5 23& 3 2 1.93600 2747.52 173.290 1.67830 1.650 2.217 *S***********************************	
COMPUTE NM HYD 316SE - 1 .06500 118.83 6.335 1.82754 1.550 2.856 PER IMP= 6	65.00
*S****** ADD 316SE TO SUMMED CHANNEL FLOWS **********	
ADD HYD 316SE.1 1& 2 3 2.00100 2848.25 179.626 1.68315 1.650 2.224	
*S***** CALC BASIN 314BM ********	
*S** NOTE: 314BM IS THE PART OF BASIN 314B THAT IS IN LVDF NO. 1****	
COMPUTE NM HYD 314BM - 1 .02740 38.70 1.214 .83098 1.500 2.207 PER IMP= 1 *S** ADD 314BM TO THE FLOWS GOING INTO LVDF NO. 1 *******	10.00
S SUM IS TOTAL INTO LAS VENTANAS DRAINAGE FACILITY NO. 1 IN BASIN 316	
ADD HYD 316SE.2 1& 3 2 2.02840 2870.51 180.841 1.67164 1.650 2.211	
S	
S	
*S** ROUTE SUMMED FLOWS THRU LAS VENTANAS DETENTION DAM	
*S** (FORMERLY KNOWN AS LVDF NO. 1)	
*S** USE 32" ORIFICE PLATE TO LIMIT PRINCIPAL SPILLWYA DISCHARGE	
*S** TO 80 CFS FOR WATER MATCHING THE CREST OF THE EMERGENCY SPILLWAY *S** AT ELEVATION 5405	
S AI ELEVATION 5405 *S* (EXISTING 100 YR FLOW INTO POND AREA=250CFS)	
*S** 5/31/00 Interpolated between 5404 and 5405 for outflow	
*S** 5/31/00 Changed storage to match "Reserved" Volumes	
ROUTE RESERVOIR POND ONE 2 4 2.02840 75.74 155.396 1.43644 3.450 .058 AC-FT= 13	3.111
S ROUTE LVDF NO. 1 DISCHARGE THRU 42" PIPE (REACH 6) NORTH TO 314BN	
ROUTE 314BN.1 4 3 2.02840 75.73 155.075 1.43347 3.550 .058	
*S******* CALC BASIN 315B ************************************	
*S*** NOTE: 315B DOES NOT GET INTO LVDF NO. 1 IN BASIN 316 ***********	
COMPUTE NM HYD 315B - 21 .04700 104.82 4.434 1.76881 1.500 3.485 PER IMP=	60.00
S FLOWS FROM 315B ARE NOT ALLOWED TO DISCHARGE OFF SITE AS IN EXIST CONDITIONS *S** ASSUME FLOWS CAN DISCHARGE OFFSITE, CHANGE ID FROM 1 TO 21 - DJG - 9/27/02	
*S***** CALC BASIN 314BS ************************************	
*S***** NOTE: FLOW FROM 314BS GOES EASTWARD OUT OF LAS VENTANAS (NO POND)	
COMPUTE NM HYD 314BS - 22 .02330 32.91 1.033 .83098 1.500 2.207 PER IMP=	10.00
*S***** CALC BASIN 314BN ********	
COMPUTE NM HYD 314BN - 1 .02740 37.36 1.214 .83098 1.500 2.131 PER IMP= : *S*** ADD 314BN TO PIPE DISCHARGE FROM LVDF NO. 1 ****	10.00
ADD HYD 320.10 3& 1 2 2.05580 75.90 156.289 1.42544 3.200 .058	
*S************************************	
COMPUTE NM HYD 320.00 - 1 .19000 286.27 15.853 1.56445 1.600 2.354 PER IMP=	49.00
S FLOWS FROM 320 ARE NOT ALLOWED TO DISCHARGE OFF SITE AS IN EXIST CONDITIONS *S* ROUTE 320 THRU "LVDF NO. 2" AT E. END OF 320, ORIFICE=30" ***	
·	9.713
S ROUTE LVDF NO. 2 DISCHARGE THROUGH 36" PIPE (REACH 7) EAST	J . 1 L J
ROUTE 320.11 4 5 .19000 31.76 15.853 1.56444 2.400 .261	
*S** ADD REACH 7 FLOWS TO REACH 6. BECOMES A 54" PIPE (REACH 8) ******	

FROM TO HYDROGRAPH ID ID AREA	PEAK DISCHARGE	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	5
COMMAND IDENTIFICATION NO. NO. (SQ MI		(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATIO	N
ADD HYD 320.20 2& 5 3 2.2458 *S***** ROUTE THRU 54" PIPE (REACH 8) NORTH TO IRVI:		172.142	1.43720	2.550	.075		
ROUTE 505.10 3 2 2.2458 *S***********************************	0 107.28	171.995	1.43597	2.600	.075		
COMPUTE NM HYD 505.00 - 1 .0220 **********************************	0 35.77	1.225	1.04368	1.500	2.540 I	PER IMP=	20.00
*S**** FLOW TOWARDS CALABACILLAS AT NE COR LAS VENT							
ADD HYD 505.20 1& 2 15 2.2678 *S****END OF LAS VENTANAS DRAINAGE ANALYSIS	0 108.80	173.219	1.43216	2.050	.075		
COMPUTE NM HYD 314A - 3 .0860		7.962	1.73598	1.600	2.611	PER IMP=	59.10
*S****GET NORTH PIECE (PANHANDLE) OF 313 INTO SYSTE *S**********************************		;*****					
COMPUTE NM HYD 313.10 - 6 .0650		6.018	1.73598	1.550	2.749 1	PER IMP=	59.10
*S***** ADD 314A/316R/313N FLOWS INTO LAST SECTION			11/3370	1.550	2.715	L Dic IIII -	37.10
ADD HYD 113.30 3&22 4 .1093		8.995	1.54305	1.550	2.423		
ADD HYD 113.20 4& 6 5 .1743		15.013	1.61500	1.550	2.545		
*S**** ROUTE 316R/314A/313N TOTAL INTO LAST SECTIO	N OF PIPE INTO PA	ARK POND***					
ROUTE 113.40 5 2 .1743	0 283.63	15.013	1.61500	1.600	2.543		
*S************************************	*****						
COMPUTE NM HYD 314.10 - 3 .0350		2.639	1.41366	1.500	3.075	PER IMP=	40.00
*S***** ADD 314.1 AND 314A/316R/313N FOR DISCH. IN							
ADD HYD 113.30 3& 2 4 .2093		17.652	1.58133	1.550	2.551		
*S****** ROUTE THRU PARK POND WITH ASSUMED DISCH		*****					
*S*** ASSUME 48" DISCHARGE PIPE ************							
ROUTE RESERVOIR 507.20 4 5 .2093		17.652	1.58133	2.000	.761	AC-FT=	7.683
*S***** ROUTE POND DISCH. THRU PIPE TO UNSER LYONS*							
ROUTE 113.40 5 2 .2093		17.652	1.58133	2.000	.761		
*S********** CALCULATE BASIN 312 ***********************************		10 536	1 77500	1 (50	2 256	DED IMD	EO 10
COMPUTE NM HYD 312.00 - 1 .2110 *S***** ADD POND DISCH. AND 312 ********	0 304.64	19.536	1.73598	1.650	2.256	PER IMP=	59.10
ADD HYD 113.30 1& 2 4 .4203	0 382.97	37.187	1.65896	1.650	1.424		
*S***** CALCULATE BASIN 311N *********	302.37	3/.10/	1.05050	1.650	1.424		
COMPUTE NM HYD 311N - 1 .0480	0 105.97	4.444	1.73598	1.500	3 450	PER IMP=	59 10
*S********* CALCULATE BASIN 311S *********		3.111	1.75570	1.500	3.430	PER IMP-	39.10
COMPUTE NM HYD 311S - 3 .0480		4.444	1.73598	1.500	3.450	PER IMP=	59.10
S ROUTE THRU STORM DRAIN TO BASIN			2110000	2.500	37130		33.10
ROUTE 311SR 3 6 .0480		4.444	1.73599	1.500	3.233		
*S***** ADD ROUTED 311S TO 311N *******							
S TOTAL FLOW IN LYON BLVD SD SOUT	H OF PARADISE						
S SIN 312 THAT IS SOUTH OF PARADI	SE IS ADDED IN O	N NORTH SIDE)					
S COMBINED 100 YR FLOW LIMITED TO	212 CFS						
ADD HYD 311T 6& 1 7 .0960	00 205.28	8.888	1.73598	1.500	3.341		
ADD HYD 113.40 7& 4 8 .5163	510.02	46.076	1.67329	1.600	1.543		
*S** NOW RT. 312/314/316R THRU PIPE TO CALABACILLLA							
ROUTE 112.20 8 14 .5163		46.076	1.67329	1.650	1.523		
*S************* ID14 IS DISCHARGE FROM 312 TO CAB.	*****						
*S**** DOWN TO PDN CHANNEL BASINS*****	to also also						
*S********** NOW CALCULATE BASIN 315W ************************************							
*S*** NOTE: (BHI ANALYSIS BY NM) FROM 315W COMPUTE NM HYD 315.10 - 3 .1330	293.36	12 214	1.73598	1.500	2 446	PER IMP=	E0 10
COMPUTE NM HYD 315.10 - 3 .1330 *S************ ADD 315B TO 315W	273.36	12.314	1./3598	1.500	3.446	FER IMP=	39.IU
ADD HYD 115.20 21& 3 1 .1800	398.18	16.748	1.74455	1.500	3.456		
S		20.720			5.450		

COMMAND IDEN	HYDROGRAPH TIFICATION	FROM TO	AREA	PEAK DISCHARGE	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS PER	PAGE =	
COMMAND IDEN	TIFICATION	NO. NO	. (SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
*S************************************	315.20 2	20& 1 19	.19700	435.38	18.322	1.74381	1.500	3.453		
*S**** ROUTE THIS ROUTE	FLOW TO WES	ST EDGE O 19 2		CHANNEL**** 395.88	18.322	1.74381	1.550	3.140		
*S********* NOW										
COMPUTE NM HYD	315.20 ADD 315S FLO	3 - NDQ TO PDN		396.83 W. EDGE 309**	16.665	1.73598	1.500	3.445	PER IMP=	59.10
ADD HYD *S**** ROUTE THIS	116.20 FLOW TO EAS			756.55 CHANNEL***	34.987	1.74007	1.500	3.136		
ROUTE *S************* CAI	116.00	1 2	.37700	763.83	34.987	1.74007	1.550	3.166		
COMPUTE NM HYD	3098	- 3		105.97	4.444	1.73598	1.500	3.450	PER IMP=	59 10
*S*****								3 7 1 2 3		37.10
ADD HYD *S**** ROUTE THIS		2& 3 1 302W IN P		856.22	39.431	1.73961	1.550	3.148		
ROUTE *S************ NOW	116.00	1 2 ASTN 315N		869.26	39.431	1.73961	1.550	3.196		
COMPUTE NM HYD	315.00	- 1	.18000	396.83	16.665	1.73598	1.500	3.445	PER IMP=	59.10
*S***** ROUTE	115.01	1 3		359.84	16.665	1.73598	1.550	3.124		
*S****** CAI	_	_			10.005	1.73598	1.550	3.124		
COMPUTE NM HYD	309.00	- 4		105.97	4.444	1.73598	1.500	3 450	PER IMP=	59.10
*S***** ROU						2.,3550	1.500	5.150	L DIC TIME	33.10
ROUTE	109.00	4 5	.04800	106.38	4.444	1.73599	1.500	3.463		
*S**ROUTE CULVERT	DISCHARGE T	HROUGH SM	IALL CHANNEL TO	THE TOP OF B30)2W****					
ROUTE	115.01	5 6	-	101.38	4.444	1.73599	1.550	3.300		
*S**INTERCEPTOR CH			-)4S**					
*S****** CAI					_					
COMPUTE NM HYD	304.00	- 4		77.28	3.241	1.73598	1.500	3.450	PER IMP=	59.10
*S ADD TO GET THE					21 110			2 4 6 7		
ADD HYD ADD HYD	304.10 304.20	-		461.22 528.60	21.110	1.73598	1.550	3.161		
*S *ROUTE 315N/309					24.350	1.73598	1.550	3.140		
ROUTE SISM/30:	7N/3045 FLOW: 115.01	8 9		534.96	24.350	1 72500	3 550	2 170		
*S***********				334.30	24.350	1.73598	1.550	3.178		
COMPUTE NM HYD	302.00	- 1		99.35	4.166	1.73598	1.500	2 450	PER IMP=	59.10
*S**** ADD INTERC		_			4.100	1.73396	1.500	3.450	PER IMP	39.10
ADD HYD	116.20			621.59	28.516	1.73598	1.550	3.153		
*S****ROUTE COMBIN				021.37	20.510	1.75570	1.550	3.133		
S REMOVE POND										
*S>>>ADD INTERCEP]**						
ADD HYD	116.30	2& 4	.73300	1490.85	67.948	1.73809	1.550	3.178		
COMPUTE NM HYD	SHENO1W	- 20	.10350	121.70	7.919	1.43452	1.700		PER IMP=	40.00
ADD HYD	116.31	5&20 5	.83650	1576.10	75.866	1.70052	1.550	2.944		
*S***ADD OUTFLOW								_		
*S**** ROUTE THIS	FLOW THRU	302E IN E	PDN CHANNEL****	•						
ROUTE	116.00	5 2		1556.35	75.866	1.70052	1.550	2.907		
*S*******										
COMPUTE NM HYD	302.00	- 1		76.85	2.679	.56450	1.550	1.349	PER IMP=	6.20
*S********										
ADD HYD		2& 1 19		1633.20	78.546	1.59128	1.550	2.757		
*S***** ID=19 IS	FLOW AT CUL	VEKI AT I	SON IN ROOS	•						

113	FROM TO		PEAK	RUNOFF	BIBIODD	TIME TO	CFS	PAGE =	7
	'DROGRAPH ID II IFICATION NO. NO		DISCHARGE (CFS)	VOLUME (AC-FT)	RUNOFF (INCHES)	PEAK (HOURS)	PER ACRE	NOTATI	ON
		(52)	(015)	(110 11)	(111011111)	(1100110)	ACRE	NOIAII	ON
*S******** CALC			*****						
COMPUTE NM HYD	313.00 - 3		173.55	8.240	1.73598	1.550	3.047	PER IMP=	59.10
*S****** ROUTE B					1 -0500				
ROUTE *S** ID12 IS DISCHA	113.40 3 12		175.14	8.240	1.73599	1.550	3.075		
*S****** CALCUL		******	HEAD OF P.N.	PARK CAINON**					
COMPUTE NM HYD	310.00 -	.01500	33.13	1.389	1.73598	1.500	3 451	PER IMP=	59.10
*S***** ROUTE CO					1.75550	1.500	3.431	PER IMP	33.10
ROUTE	110.00 1		33.27	1.389	1.73602	1.500	3.466		
*S***** TAKE DISCH	ARGE FROM CULVERT 2	AND ROUTE THRU	308,2 SECT.	*****					
ROUTE	108.00 12	.08900	161.64	8.240	1.73599	1.600	2.838		
*S****** CALC		*******	***						
COMPUTE NM HYD	308.00 -		47.78	1.746	.90934	1.500	2.074	PER IMP=	22.10
*S****** ADD R									
ADD HYD	108.10 3& 4		201.80	9.986	1.49791	1.550	2.523		
*S****** ROUTE '	104.10 1			0.006	1 40701	1 (50	1 000		
*S********* CALC			150.67	9.986	1.49791	1.650	1.883		
COMPUTE NM HYD		.06500	131.80	5.447	1.57132	1.500	3 168	PER IMP=	52.00
*S****** ROUT			_	3.447	1.5/152	1.500	3.100	FER IMF-	32.00
ROUTE	107.00 6 1		27.62	1.389	1.73601	1.550	2.877		
*S**** ADD 307/310/	311R INTO PLAYA II	J 307 *******							
ADD HYD	307.40 4&10	.08000	155.17	6.836	1.60219	1.500	3.031		
*S***** ROUTE	-	******	*****						
ROUTE RESERVOIR	507.20 9	· · · · · · · ·	104.75	6.176	1.44758	1.650	2.046	AC-FT=	2.222
*S**** ROUTE OUTFLO			50.60		1 44500				
ROUTE		.08000	72.68	6.175	1.44733	1.750	1.420		
*S***** ADD (3		.20500	218.85	16.161	1.47817	1.700	1.668		
*S******** CALC		.20300		10.101	1.4/01/	1.700	1.000		
COMPUTE NM HYD		.03100	68.49	2.873	1.73776	1.500	3.452	PER IMP=	59.20
*S***** ROUTE	THRU PLAYA IN BAS						5.102	2011	33.20
ROUTE RESERVOIR	506.00 3	.03100	16.96	2.216	1.34028	1.900	.855	AC-FT=	1.477
*S***** ROUTE PON	D DISCHARGE THRU 3)5 ********	*						
ROUTE		.03100	16.48	2.212	1.33808	2.050	.831		
*S***** CALCUL									
COMPUTE NM HYD		.02700	47.32	1.891	1.31316	1.500		PER IMP=	40.50
ADD HYD *S****** ROUTE 3		L .05800	47.39	4.103	1.32648	1.500	1.277		
ROUTE		.05800	45.24	4 102	1.32628	1.550	1.219		
*S***** ADD 305T T				4.103	1.32020	1.550	1.219		
ADD HYD		.26300	250.19	20.264	1.44468	1.700	1.486		
*S**** ROUTE REMAI				20.201		200	1.100		
ROUTE	104.80 3	.26300	248.77	20.263	1.44461	1.700	1.478		
*S********* CALC	ULATE BASIN 304 **	*******	****						
COMPUTE NM HYD		.18500	236.35	9.600	.97296	1.500	1.996	PER IMP=	25.00
*S**** ADD 304 TO									
ADD HYD		1 .44800	389.85	29.863	1.24984	1.600	1.360		
ROUTE *S*********		2 .44800	299.27	29.856	1.24957	1.800	1.044		
COMPUTE NM HYD		.16500	97.30	4.968	.56450	1.650	021	PER IMP=	6.20
*S***** ADD				4.900		1.050	. 361	IBK IMP=	0.20
		-							

		FROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	8
	HYDROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER		
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
ADD HYD	103.10		1	.61300	373.20	34.824	1.06517	1.750	.951		
	** ROUTE FLOW T										
ROUTE	103.20	1	2	.61300	373.07	34.824	1.06517	1.750	.951		
*S*** !!!!!!!!		Dr.									
	* ADD PDN CHANN										
ADD HYD ROUTE	103.10 101.00		5	1.53850	1868.78	113.369	1.38165	1.600	1.898		
	BASIN 301 WITH	5	13	1.53850	1900.73	113.368	1.38164	1.600	1.930		
	>>>CALCULATE BAS			ROM SHENANDOAH	ESTATES SUBDI	VISION					
COMPUTE NM HYI		- 2IN 2UI	10	.09600	40.09	2.395	.46784	1.700	653	PER IMP=	0.0
ROUTE RESERVO		10	11	.09600	38.41	2.395	.46786	1.750		PER IMP= AC-FT=	.00
ROUTE	PIPE		30	.09600	38.37	2.399	.46859	1.767	.625	AC-FI=	.324
	>>>CALCULATE BAS			.05000	30.37	2.333	.40033	1.767	.025		
COMPUTE NM HYI		-	11	.02860	25.26	.714	.46784	1.500	1 380	PER IMP=	.00
ROUTE RESERVO			12	.02860	20.28	.714	.46790	1.600		AC-FT=	.216
ROUTE	PIPE		31	.02860	20.54	.712	.46693	1.633	1.122	AC II-	.210
ADD HYD	TOTPIPE		32	.12460	53.47	3.111	.46820	1.667	.671		
ROUTE	TOTPIPE	32	33	.12460	53.41	3.111	.46820	1.667	.670		
*S>>>>>>	>>>CALCULATE BAS	SIN SHI	ENO3								
COMPUTE NM HYI	SHENO3	-	12	.04501	90.18	3.481	1.45009	1.500	3.130	PER IMP=	40.00
DIVIDE HYD	O3SD	12	30	.04052	57.00	3.134	1.45008	1.450	2.198		
	O3ST	and	20	.00449	33.18	.347	1.45008	1.500	11.557		
ROUTE	TOTPIPE	30	31	.04052	57.51	3.059	1.41550	1.500	2.217		
ADD HYD	TOTPIPE		30	.16512	103.99	6.171	.70068	1.633	.984		
ROUTE	CRSMT2		21	.00449	31.19	.339	1.41735	1.533	10.865		
DIVIDE HYD	O3SD		31	.00328	16.80	.248	1.41726	1.500	8.006		
	O3ST		22	.00121	14.39	.091	1.41726	1.533	18.632		
ADD HYD	TOTPIPE		33	.16840	108.34	6.418	.71457	1.600	1.005		
	>>>CALCULATE BAS										
COMPUTE NM HYI			1	.01820	35.23	1.392	1.43452	1.500		PER IMP=	40.00
DIVIDE HYD	ASD		10	.01461	16.00	1.118	1.43450	1.400	1.711		
ADD HYD	AST TOTPIPE		11 30	.00359	19.23	.274	1.43450	1.500	8.376		
ROUTE	PIPE		31	.18302 .18302	124.34	7.505	.76892	1.600	1.062		
ADD HYD		30 11&22	21	.00479	124.64	7.506	.76897	1.633	1.064		
DIVIDE HYD	CRESSSD		30	.00479	32.06 32.06	.364 .364	1.42505	1.500	10.448		
DIVIDE HID	CRESSST		22	.00000	.00	.000	1.42505	1.500	10.448		
ADD HYD	TOTPIPE		32	.18781	133.04	7.870	.78572	1.600	.000 1.107		
ROUTE	PIPE		30	.18781	133.83	7.870	.78568	1.533	1.113		
ROUTE	BURMART		21	.00000	.00	.000	.00000	033	.000		
	>>>CALCULATE BAS				.00	.000	.00000	.033	.000		
COMPUTE NM HY			1	.00420	8.43	.325	1.45009	1.500	3,135	PER IMP=	40.00
DIVIDE HYD	MARTSD		39	.00258	2.00	.199	1.45001	1.350	1.211	1211 1111 -	10.00
	MARTST		29	.00162	6.43	.125	1.45001	1.500	6.198		
ADD HYD	TOTPIPE	30&39	1	.19039	135.83	8.061	.79389	1.533	1.115		
ROUTE	PIPE	1	30	.19039	136.18	8.061	.79385	1.533	1.118		
ADD HYD		21&29	20	.00162	6.43	.125	1.44721	1.500	6.198		
ROUTE	CUMBURS1		21	.00162	5.28	.125	1.45039	1.567	5.092		
	>>>CALCULATE BA										
COMPUTE NM HY			3	.00670	12.90	.518	1.45009	1.500		PER IMP=	40.00
ADD HYD	B2ST	21& 3	20	.00832	17.61	.632	1.42436	1.533	3.307		

		FROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	9
	HYDROGRAPH	ID	ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER		
COMMAND	IDENTIFICATION	NO.	NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATI	ON
DIVIDE HYD	NBURSD	20	32	.00832	17 61	622	1 42426	1 522	2 205		
DIVIDE HID	NBURST		22	.00000	17.61 .00	.632 .000	1.42436	1.533 033	3.307		
ADD HYD	TOTPIPE		31	.19871	153.79	8.693	.82025	1.533	.000 1.209		
*S>>>>>>	>>>CALCULATE BAS			. 150, 1	133.73	0.055	.02023	1.555	1.209		
COMPUTE NM HY	D SHENB1	_	2	.01060	19.03	.719	1.27203	1.500	2.806	PER IMP=	30.00
DIVIDE HYD	B1SD	2	30	.00685	5.40	.465	1.27200	1.400	1.232	211	50.00
	BIST	and	20	.00375	13.63	.255	1.27200	1.500	5.677		
ADD HYD	B1ST	20&22	21	.00375	13.63	.254	1.27039	1.500	5.676		
ADD HYD	TOTPIPES	31&30	32	.20556	159.19	9.143	.83397	1.533	1.210		
	>>>CALCULATE BAS	SIN SHE	ENC1								
COMPUTE NM HY		-	4	.00570	11.16	.421	1.38510	1.500	3.060	PER IMP=	36.00
	>>>CALCULATE BAS	SIN SHE									
COMPUTE NM HY		-	49	.00280	5.62	.217	1.45009	1.500	3.138	PER IMP=	40.00
ADD HYD	ID		48	.00850	16.79	.638	1.40644	1.500	3.086		
ROUTE	CUMBURS4	48	22	.00850	13.96	.623	1.37463	1.567	2.566		
	>>>CALCULATE BA										
COMPUTE NM HY			5	.00350	6.10	.271	1.45009	1.550		PER IMP=	40.00
ADD HYD		22& 5	29	.01200	19.85	.888	1.38704	1.567	2.585		
DIVIDE HYD	SBURSD		35	.00940	9.00	.695	1.38704	1.433	1.496		
	SBURST		25	.00260	10.85	.192	1.38704	1.567	6.518		
ADD HYD	TOTPIPES		30	.21496	168.19	9.838	.85815	1.533	1.223		
ADD HYD		21&25	20	.00635	23.37	.447	1.31815	1.533	5.747		
DIVIDE HYD	BURSUMP		31	.00419	10.65	.294	1.31815	1.467	3.973		
ADD IIVD	BURESID		29	.00217	12.72	.152	1.31815	1.533	9.177		
ADD HYD ROUTE	TOTPIPES PIPE		32 31	.21914	178.84	10.133	.86695	1.533	1.275		
ROUTE	BASINABCT		22	.21914	179.14	10.133	.86695	1.533	1.277		
	>>>CALCULATE BA			.00217	13.11	.153	1.32054	1.533	9.457		
COMPUTE NM HY			9	.00270	5.42	.209	1 45000	1 500	2 120	DDD TWD	40.00
DIVIDE HYD	SFRYLSD		33	.00160	1.20	.124	1.45009	1.500 1.350		PER IMP=	40.00
DIVIDE HID	SFRYLST		25	.00110	4.22	.085	1.44997 1.44997	1.500	1.168		
ADD HYD	TOTPIPES		30	.22075	180.34	10.252	.87075	1.533	6.025		
ADD HYD		25&22	21	.00326	16.96	.237	1.36398	1.533	1.276		
ROUTE	PIPE		31	.22075	180.28	10.252	.87076	1.533	8.124 1.276		
	>>>CALCULATE BA			.22075	100.20	10.232	.07070	1.333	1.2/6		
COMPUTE NM HY			7	.00180	3.62	.139	1.45009	1.500	2 1/2	PER IMP=	40.00
ADD HYD		21& 7	23	.00506	20.33	.373	1.38329	1.533	6.275	FER IMP=	40.00
DIVIDE HYD	WCUMCCSD		35	.00364	8.80	.268	1.38329	1.467	3.778		
2212222	WCUMCCST		25	.00142	11.53	.105	1.38329	1.533	12.667		
ADD HYD	TOTPIPES		30	.22439	189.08	10.520	.87907	1.533	1.317		
*\$>>>>>>>	>>>CALCULATE BA							2.555	1.31,		
COMPUTE NM HY			6	.01820	36.47	1.408	1.45009	1.500	3.131	PER IMP=	40.00
DIVIDE HYD	NCCSD		36	.01547	19.20	1.197	1.45007	1.400	1.939	2 2010 21112 -	10.00
	NCCST		26	.00273	17.27	.211	1.45007	1.500	9.894		
ADD HYD	TOTPIPES			.23986	208.28	11.686	.91351	1.533	1.357		
ADD HYD		25&26		.00415	27.14	.313	1.41581	1.500	10.221		
ADD HYD	TOTPIPES		7	.24401	234.55	11.999	.92205	1.533	1.502		
ROUTE	PIPE	7	30	.24401	235.06	12.000	.92206	1.533	1.505		
*S>>>>>>	>>>CALCULATE BA	SIN SH	ENE1				_	_	-		
COMPUTE NM HY	D SHENE1	-	1	.01230	24.65	.951	1.45009	1.500	3.132	PER IMP=	40.00
	>>>CALCULATE BA	SIN SH	ENE2								
COMPUTE NM HY	D SHENE2	-	3	.00760	15.24	.588	1.45009	1.500	3.133	PER IMP=	40.00

	FROM TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	10
HYDROGRAF COMMAND IDENTIFICATIO		AREA	DISCHARGE (CFS)	VOLUME	RUNOFF	PEAK	PER	NOMBET	217
COMMAND IDENTIFICATIO	N NO. NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE	NOTATIO	JN
ADD HYD INLE	T 1& 3 10	.01990	39.89	1.539	1.45006	1.500	3.132		
ROUTE PIF	E 10 14	.01990	39.60	1.505	1.41812	1.500	3.109		
*S****** ADD FLOW FROM S	HENANDOAH TO FI	LOW IN MIDDLE	BRANCH AT GOL	F COURSE **					
ADD HYD 101.4	0 30&13 4	1.78251	2114.76	122.119	1.28455	1.600	1.854		
*S>>>>>> CALCULATE -	BASIN BETWEEN	CHANNEL AND	GOLF COURSE						
COMPUTE NM HYD 301.1	0 - 3	.02580	49.54	2.191	1.59219	1.500	3.000	PER IMP=	58.00
*S****** ADD FLOW FROM 3	01.1 TO MIDDLE		LF COURSE **						
	1 3& 4 15	1.80831	2149.16	124.221	1.28803	1.600	1.857		
*S**>>> TOTAL UPSTREAM OF									
*S*** ID 15 IS DISCHARGE UP									
*S********* NORTH BRAN				***					
*S********** CALCULA									
COMPUTE NM HYD 204.0		.10200	218.10	8.755	1.60944	1.500	3.341	PER IMP=	50.00
	ALL OF BASIN 20								
	.1 FLOW THRU 72								
ROUTE 201.2		.10200	194.68	8.755	1.60945	1.550	2.982		
*S****** CALCULAT									
COMPUTE NM HYD 204.3		.08500	118.37	5.604	1.23610	1.550	2.176	PER IMP=	30.00
*S***** ROUTE THRU I									
ROUTE RESERVOIR 204.3		.08500	.43	.744	.16407	13.650	.008	AC-FT=	5.000
*S****** ROUTE DISCHARGE					16166				
ROUTE 204.3		.08500	.41	.733	.16166	14.600	.008		
*S****** CALCULAT				6 262	1 22610	1 550	2 402	DDD 711D	20.00
COMPUTE NM HYD 204.4 ***********************************		.09500	151.56	6.263	1.23610	1.550	2.493	PER IMP=	30.00
ROUTE 204.4 1A		.09500	150.87	6.263	1.23610	1.550	2.481		
*S**** ADD 204.4R AND 204.3		.09300	130.07	0.203	1.23010	1.330	2.401		
	2 5& 6 7	.18000	150.91	6.996	.72872	1.550	1.310		
*S**** ROUTE THIS TOTAL AT					. /20/2	1.550	1.510		
ROUTE 204.3		.18000	145.23	6.989	.72806	1.600	1.261		
*S***** CALCULA				0.202	.,5000	1.000	1.201		
COMPUTE NM HYD 204.2		.04900	85.82	3.787	1.44917	1.550	2.736	PER IMP=	42.00
*S**** ADD 204.2 TO TOTAL F			03.02	3	2.1132.	1.330	2.750	I DK IIII -	12.00
	1 2& 3 1	.22900	219.23	10.777	.88236	1.600	1.496		
*S***** CALCULA									
COMPUTE NM HYD 204.5	0 - 3	.09000	72.56	4.440	.92497	1.700	1.260	PER IMP=	15.00
*S**** ADD 204.5 TO 204.2-2	04.4 SUBBASINS	******							
ADD HYD 204.9	9 1& 3 4	.31900	281.61	15.216	.89438	1.600	1.379		
*S***** *** ROUTE TH	U CULVERT UNDE	R P.H. BLVD.	******						
*S******* CULVERT CAL	THANDLE THIS	FLOW *****	*****						
*S****** ROUTE THRU PO	OND AREA TO SIM	ULATE FLOW OV	VER ROAD ****	***					
ROUTE RESERVOIR 506.0		.31900	305.71	15.214	.89426	1.600	1.497	AC-FT=	.350
*S********** CALCULAT	E BASIN 205.1 -	PARADISE RII	OGE SUB'D ****	*					
COMPUTE NM HYD 205.		.03500	79.85	3.396	1.81930	1.500	3.565	PER IMP=	62.13
*S**** ROUTE 205.1 FLOW IN			ISE BLVD. TO G	OLF COURSE RD					
S APPROXIMATELY AT BAS									
ROUTE 201.		.03500	66.81	3.396	1.81932	1.550	2.982		
*S***** CALCULAT									
COMPUTE NM HYD 205.		.17500	296.52	16.202	1.73598	1.600	2.648	PER IMP=	59.10
*S****** ADD 205.2 AND				10 500					
ADD HYD 205TO' *S******* ADD 205TOTA A	TA 2&66 67	.21000	361.29	19.598	1.74987	1.550	2.688		
*S*** ASSUME THIS IS TOTAL				OTTREE					
"" " AGOOM TITO TO TOTAL	TW LWWNIDE BD	ישי זפטט עפ	MESI OF GOLF C	OURSE					

COMMAND II	FRO HYDROGRAPH II DENTIFICATION NO) ID	AREA	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PAGE = PER ACRE NOTATIO	
ADD HYD	205TOT 67&6	54 68	.31200	555.96	28.354	1.70396	1.550	2.784	
ADD HYD	204.2-204.5 AND 204.00 3&6	58 1	.63100	844.23	43.568	1.29462	1.600	2.091	
ROUTE	OW IN 96" PIPE TO 201.20] * COMPUTE BASIN 20	L 2	.63100	832.44	43.566	1.29454	1.600	2.061	
COMPUTE NM HYD	203.00 - *** CALCULATE BASI	3	.12980	104.83	6.328	.91407	1.650	1.262 PER IMP=	24.00
COMPUTE NM HYD	202.10 - 202.1 FLOW THROUG	4	.04220	91.74	3.868	1.71856	1.500	3.397 PER IMP=	58.00
*S**** ROUTE FLO	OW IN 96" PIPE TO		SIN 202.2 **	******					
ROUTE		4 5	.04220	86.29	3.868	1.71857	1.550	3.195	
	OUTED BASIN 202.1				10 100	7 77744	7 600	1 614	
ADD HYD	203.00 5& THE UPPER BASINS		.17200	177.64	10.196	1.11144	1.600	1.614	
ADD HYD	201.10 6&		.80300	1010.08	53.761	1.25532	1.600	1.965	
	** COMPUTE BASIN 2				33.701	1.23332	1.000	1.905	
COMPUTE NM HYD	202.20 -	5	.04330	94.13	3.969	1.71856	1.500	3.397 PER IMP=	58.00
	.2 AND UPPER BASIN				0.12.02				
ADD HYD	202.30 4&		.84630	1075.37	57.730	1.27902	1.600	1.985	
	W HYDRAGRAPH THROU								
	OW IN 96" PIPE TO		SIN 202.2 **	******					
ROUTE		1 4	.84630	1080.88	57.729	1.27900	1.600	1.996	
-	** COMPUTE BASIN :								
COMPUTE NM HYD	202.30 -	3	.02050	43.78	1.879	1.71856	1.500	3.337 PER IMP=	58.00
COMPUTE NM HYD	* CALCULATE BASIN 202.40	5	.04010	87.18	3.675	1.71855	1.500	3.397 PER IMP=	58.00
	***** ADD 202.3 TO				3.675	1./1055	1.500	3.397 PER IMP=	36.00
ADD HYD	202.40 5&		.06060	130.96	5.554	1.71855	1.500	3.377	
	THE UPPER BASINS	_			3.331	11,1000	1.500	3.3	
ADD HYD	202.00 2&		.90690	1172.95	63.283	1.30837	1.600	2.021	
*S********	* CALCULATE BASIN	202.5 ***		***** CHECK	AREA				
COMPUTE NM HYD	202.50 -	3	.02050	44.57	1.879	1.71856	1.500	3.397 PER IMP=	58.00
*S***** ADD	ALL UPPER N. B. B	ASINS TO 2	02.35 *****	****					
ADD HYD	202.00 3&	5 6	.92740	1203.87	65.162	1.31744	1.600	2.028	
	IS TOTAL DISCHARGE								
	RTH BRANCH FLOW A'		LF COURSE TO	MIDDLE BRANCE	I ****				
*S****	ROUTE FLOW IN 9		*****	*****					
ROUTE		6 16	.92740	1215.06	65.161	1.31741	1.600	2.047	
	IS TOTAL DISCHAR								
	* MAIN BRANCH INTO ** CALCULATE BASI								
COMPUTE NM HYD	103.00 -	2	.05810	128.35	5.385	1.73776	1.500	3.452 PER IMP=	E0 20
	UTE THRU STORM DR.					1.75770	1.500	3.432 FER IMF-	33.20
ROUTE		2 3	.05810	128.35	5.385	1.73777	1.500	3.452	
	EHANDOAH BASIN E				21203	21.0,	2.300	3.135	
ADD HYD	103.10 3&		.07800	167.94	6.742	1.62072	1.500	3.364	
*S**>>> FLOW DO	WNSTREAM OF GOLF	COURSE IN	MIDDLE BEFOR	RE ADDING N. B	RANCH				
ADD HYD	103.20 15&	4 15	1.88631	2269.10	130.964	1.30178	1.600	1.880	
	LOW DOWNSTRAM OF								
ADD HYD	103.20 15&	16 17	2.81371	3484.14	194.179	1.29397	1.600	1.935	

	WDD0GD3 DU	FROM	TO		PEAK	RUNOFF		TIME TO	CFS	PAGE =	12
COMMAND 3	HYDROGRAPH DENTIFICATION		ID NO.	AREA (SQ MI)	DISCHARGE (CFS)	VOLUME (AC-FT)	RUNOFF (INCHES)	PEAK (HOURS)	PER ACRE	NOTATI	ON
ROUTE	102.10		13	2.81371	3446.32	194.180	1.29397	1.600	1.914		
*S**>>> TOTAL E											
COMPUTE NM HYD	RANCHO O1		1	.00566	7.49	.257	.85203	1 500	2 060	DED TWD	16.00
ROUTE	NORT&SER		4	.00566	6.39	.253	.83843	1.500 1.567	1.764	PER IMP=	16.00
COMPUTE NM HYD	RANCHO O2		2	.00786	8.57	.279	.66441	1.500		PER IMP=	9.00
ADD HYD	RANCHO12		1	.01352	14.35	.529	.73308	1.533	1.659	FER IMF=	9.00
DIVIDE HYD	SERENO		2	.00676	7.18	.264	.73308	1.533	1.659		
	BUTTER		3	.00676	7.18	.264	.73308	1.533	1.659		
ROUTE	SER&LARG		23	.00676	6.66	.264	.73264	1.600	1.539		
ROUTE	BUTTER&DAM	3	24	.00676	4.99	.264	.73170	1.633	1.154		
COMPUTE NM HYD	BASIN 102R	-	1	.01107	23.75	.971	1.64507	1.500		PER IMP=	52.00
ADD HYD	BUTTERTOT		55	.01783	26.31	1.211	1.27304	1.500	2.306		12
COMPUTE NM HYD	BASIN E1	-	1	.00215	4.62	.189	1.64506	1.500	3.361	PER IMP=	52.00
ADD HYD	SER&LARG	1&23	4	.00891	10.47	.448	.94276	1.567	1.837		
COMPUTE NM HYD	BASIN F1	-	1	.00807	16.84	.673	1.56383	1.500	3.261	PER IMP=	47.00
ROUTE	TO_BSN_H	1	3	.00807	16.51	.657	1.52590	1.500	3.197		
COMPUTE NM HYD	BASIN_H		2	.00192	3.84	.147	1.43384	1.500	3.123	PER IMP=	39.00
ADD HYD	LARG&DOR	2& 3	1	.00999	20.35	.800	1.50199	1.500	3.183		
ROUTE	TO_BSN_G		3	.00999	20.41	.800	1.50159	1.533	3.193		
COMPUTE NM HYD	BASIN_G		2	.00279	6.03	.247	1.66131	1.500	3.377	PER IMP=	53.00
ADD HYD	LARG&QUI		1	.01278	26.00	1.041	1.52706	1.533	3.179		
ROUTE	TOSERENO	1	3	.01278	26.36	1.041	1.52685	1.533	3.223		
COMPUTE NM HYD	BASIN_F2		2	.00415	9.11	.378	1.71006	1.500	3.429	PER IMP=	56.00
ADD HYD	LARG&SER		1	.01693	34.78	1.409	1.56067	1.533	3.210		
DIVIDE HYD	PIPE		2	.01550	23.00	1.290	1.56067	1.467	2.318		
	STRT		3	.00143	11.78	.119	1.56067	1.533	12.895		
ROUTE	STORMDRN		5	.01550	23.75	1.290	1.56053	1.467	2.394		
ADD HYD	SER&LARG		1	.01034	22.17	.567	1.02810	1.533	3.351		
ROUTE	TOCHANNL		4	.01034	22.39	.567	1.02775	1.533	3.384		
ADD HYD	CHNNLTOT		9	.02584	45.55	1.857	1.34738	1.533	2.754		
COMPUTE NM HYD	BASIN_B1 LARG&ENC		1	.00340	7.62	.322	1.77505	1.500		PER IMP=	60.00
ROUTE	BASIN B2		3	.00340	6.94	.313	1.72502	1.533	3.189	DDD 7110	
COMPUTE NM HYD ADD HYD	LARG&ENC		1 5	.00408	9.00	.376	1.72631	1.500		PER IMP=	57.00
COMPUTE NM HYD	BASIN A1		1	.00748 .00567	15.43 12.50	.678 .522	1.70078 1.72630	1.500 1.500	3.223	DED TWD	57.00
ROUTE	ALGR&ENC		3	.00567	11.48	.508	1.67856	1.533	3.446	PER IMP=	57.00
COMPUTE NM HYD	BASIN A2		2	.00426	9.15	.374	1.64507	1.500		PER IMP=	E2 00
ADD HYD	ENC&LARG		4	.00993	19.95	.872	1.64621	1.533	3.140	FER IMP=	32.00
ADD HYD	A1A2B1B2		7	.01741	35.22	1.550	1.66965	1.533	3.140		
ROUTE	A1A2B1B2		4	.01741	35.63	1.549	1.66875	1.533	3.198		
COMPUTE NM HYD			3	.00209	4.37	.174	1.56383	1.500		PER IMP=	47 00
ADD HYD	TOTA&B		7	.01950	39.69	1.719	1.65320	1.533	3.180	I DK IIII -	17.00
ROUTE	STORMDRN		10	.01950	39.75	1.719	1.65322	1.533	3.185		
COMPUTE NM HYD	BASIN C			.00046	. 82	.027	1.10888	1.500		PER IMP=	19.00
COMPUTE NM HYD	name .		4	.00024	.38	.010	.80017	1.500		PER IMP=	.00
COMPUTE NM HYD	_		11	.00045	.98	.036	1.51209	1.500			37.00
COMPUTE NM HYD	BASIN 12	-	12	.00168	3.45	.122	1.36719	1.500		PER IMP=	
*S*******											
ADD HYD	102.20	13& 9	14	2.83955	3485.60	195.999	1.29422	1.600	1.918		
*S*******	* ADD RANCHO2	BASIN :	I-2 INTO	CHANNEL AT	RANCHO SERENO)*****					
ADD HYD	102.20	14&12	13	2.84123	3488.03	196.088	1.29403	1.600	1.918		
*S*******	* ADD RANCHO2	BASIN :	I-1 INTO	O CHANNEL AT	RANCHO SERENO)******					

	FROM TO		PEAK	RUNOFF		TIME TO	CFS PAGE	= 13
HYDROGRAPH		AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER	
COMMAND IDENTIFICATION	NO. NO	. (SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE NOTAT	ION
ADD 114D 100 20	12511 05	0.04160	2400 71	106 100				
	13&11 97	2.84168	3488.71	196.123	1.29406	1.600	1.918	
*S******** ADD RANCHO E *S********** STORM DRAIN			FROM RANCHOIZ	AND				
		THIS RUNOFF GO	יבי הדפביינע דו	ד ממג אאמ סיינא	N I ATED			
	3& 4 88	.00070	1.20	.037	1.00255	1.500	2.677	
	88&10 98	.02020	40.88	1.756	1.63021	1.533	3.162	
	98&55 99	.03803	66.40	2.967	1.46275	1.533	2.728	
*S**>>****** CALCULATE M		_		2.507	1.402/3	1.333	2.720	
COMPUTE NM HYD 101.10		.17600	388.27	16.312	1.73776	1.500	3.447 PER IMP=	59.20
COMPUTE NM HYD 101.20			123.73	5.688	1.51815	1.550	2.752 PER IMP=	
ROUTE 402.10	2 1		124.15	5.688	1.51816	1.550	2.761	
COMPUTE NM HYD 101.30	- 2	.02675	54.99	2.166	1.51815	1.500	3.212 PER IMP=	44.19
*S****** ADD 101.3 to r	outed flow	from 101.2 ***	******	*****				
ADD HYD 101.11	2& 1 1	.09700	173.20	7.854	1.51815	1.550	2.790	
ROUTE 402.10	1 2	.09700	174.19	7.854	1.51815	1.550	2.806	
*S****** TOTAL FLOW IN	MIDDLE BRA	HCH DOWNSTREAM	OF RANCHO SER	ENA ********				
ADD HYD 101.11	2&97 18	2.93868	3643.25	203.792	1.30028	1.600	1.937	
ROUTE 102.10			3594.25	203.792	1.30028	1.600	1.911	
*S**>>> TOTAL FLOW IN MIDDLE								
*S****** ID 19 IS TOTAL F	LOW INTO D	AM from Middle	Branch ****	*****				
*S****** SOUTH BRA								
*S***** CALCULAT								
COMPUTE NM HYD 404.00			361.19	14.473	1.39167	1.500	2.894 PER IMP=	44.00
*S****** ROUTE THI								
ROUTE 404.01			318.67	14.473	1.39167	1.550	2.553	
*S******* CALCULATE				10 650		1 500	2 440 555 545	
COMPUTE NM HYD 404.10	_		253.87 ******	10.658	1.73776	1.500	3.449 PER IMP=	59.20
*S****** ADD 404.1 AND					1 50005	7 550	0. 700	
ADD HYD 404.02 *S*********** ROUTE THIS FLO	1& 2 3		540.23	25.132	1.52005	1.550	2.723	
ROUTE 403.01			542.29	25.132	1.52005	1.550	2.733	
*S********* CALCULATE				25.132	1.52005	1.550	2.733	
COMPUTE NM HYD 403.30			81.77	3.426	1.73601	1.500	3.453 PER IMP=	E9 00
*S***** ROUTE THIS FLOW					1.75001	1.500	3.433 FER IMF-	39.00
ROUTE 403.02			82.18	3.426	1.73602	1.500	3.470	
*S***** ADD 403.3R AN			******		1.,5002	1.500	5.170	
ADD HYD 403.03			614.68	28.557	1.54308	1.550	2.768	
COMPUTE NM HYD 403.20	- 2		30.95	1.296	1.73601	1.500	3.454 PER IMP=	59.00
*S****** ROUTE THIS FLOW								0,5,00
ROUTE 403.21	. 2 3	.01400	31.24	1.296	1.73605	1.500	3.487	
*S***** ADD 403.2R AND TOTA	L ROUTE IN	LARGE CHANNEL	(ID=4)******	******	•			
ADD HYD 403.22	3&4 1	.36100	642.56	29.853	1.55056	1.550	2.781	
*S*** DIVIDE TOTAL INFLOW; PI	PE CAP. W/	8-9' HEAD IS 20	65 CFS, REST I	S OVERFLOW***				
*S***** DIVIDE HYD BETWEEN	PIPE CAPAC	ITY AND STREET	FLOW****					
DIVIDE HYD 403.1	. 1 3	.28227	265.00	23.343	1.55056	1.450	1.467	
403.12			377.56	6.511	1.55056	1.550	7.493	
*S****** ROUTE PIPE				RD.*******	,			
ROUTE 403.19	-		267.05	23.343	1.55056	1.500	1.478	
*S***** ROUTE OVERFLOW					14			
ROUTE 403.2	_		354.13	6.511	1.55066	1.600	7.028	
*S***** ADD OVERLAND AND	PIPE FLOW	FROM MAIN CHAN	NEL THRU 403**	***				

1	FR YDROGRAPH I	OM TO	AREA	PEAK DISCHARGE	RUNOFF VOLUME	RUNOFF	TIME TO PEAK	CFS	PAGE =	14
		0. NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	PER ACRE	NOTATI	ON
ADD HYD	403.40 5&		.36100	619.17	29.854	1.55058	1.600	2.680		
COMPUTE NM HYD	403.00 -	2	.06800	127.74	6.296	1.73601	1.550	2.935	PER IMP=	59.00
ADD HYD *S*********	403.40 4&	2 3	.42900	736.09	36.150	1.57997	1.600	2.681		
COMPUTE NM HYD	402.00 -	2	.09300	205.42	8.611	1.73601	1.500	3.451	PER IMP=	59.00
ROUTE *S****** ADI	402.10	2 1	.09300	205.87	8.611	1.73602	1.500	3.459		
ADD HYD	402.20 1&	3 6	.52200	890.48	44.760	1.60777	1.550	2.665		
*S************************************	403.10 -	2	.03000	66.30	2.778	1.73601	1.500	3.453	PER IMP=	59.00
*S***** DIVIDE HYD	403.11	2 22	.02811	46.70	2.602	1.73600	1.450	2.596		
*S***** ROUTE		OW THRU PI				1.73600	1.500	16.173		
ROUTE *S****** ROUTE		ET FLOW DO		46.36 E*****	2.602	1.73603	1.550	2.577		
ROUTE *S*********	DO OVERLAND AN		.00189 W FROM 403.1*	9.08	.176	1.74010	1.550	7.492		
ADD HYD *S*** ADD 403.1ROU	403.19 1& ES AND TOTAL		.03000 6 FOR TOT. @ :	55.44 BUTTERFIELD <i>F</i>	2.778 AND G.C.****	1.73624	1.550	2.888		
ADD HYD *S*** DIVIDE HYD B	403.12 1& TWEEN PIPE CA		.55200 OVERLAND LEF	945.92 TOVER THRU 40	47.538 01***	1.61476	1.550	2.678		
DIVIDE HYD	401.10 401.20 an	7 77 d 3	.50218 .04982	618.00 327.92	43.248 4.291	1.61476 1.61476	1.500 1.550	1.923 10.284		
*S********* ROU' ROUTE	E NEW PIPE TO 401.10 7		01 PIPE TO DA .50218	M ********* 617.52	43.248	1.61475	1.700	1.921		
*S***** ROUTE		ET FLOW OV	ERLAND THRU 4		4.291	1.61491	1.650	6.813		
*S*********** A		D PIPE ROU			47.539			_		
*S*********		SIN 401 **	*****	*****		1.61477	1.650	2.362		
COMPUTE NM HYD	BASIN 401 TO R				19.073	1.73601	1.650	2.348	PER IMP=	59.00
*S************ TO	D=3 IS SOUTH B	RANCH FLOW	******	*******						
ADD HYD *S**** NOW ADD SOU *S********* TOTAL		(ID3) TO 1	•		66.612 *****	1.64772	1.650	2.358		
ADD HYD	100.00 19&	3 1	3.69668 1.10 DIRECTLY	4709.58	270.404	1.37152	1.600	1.991		
ADD HYD *S*	TOT1 1&	95 2	3.87268 O BASINS (BAS	4973.27	286.716	1.38816	1.600	2.007		
ADD HYD *S****** ROUTE	TOT2 2&	99 1	3.91071	5029.28	287.316	1.37754	1.600	2.009		
*S *S	MOVE - THIS	RATING CUR	VE DOES NOT R FLOW OUT ONLY							
FINISH	10 II ONIED	001221 00	1200 COT ONDI	INCO ENERGEI	ACI OFILLWAI.					

Geotechnical Investigation and Pavement Section Design APPENDIX E

Vinyard & Associates, Inc.

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4415-D Hawkins, NE Albuquerque, New Mexico 87109 (505) 345-1937

Geotechnical Engineering • Materials Testing • Environmental Engineering

REVISED GEOTECHNICAL INVESTIGATION

AND PAVEMENT SECTION DESIGN

UNSER BLVD. FROM PARADISE BLVD.

TO THE BERNALILLO COUNTY LINE

Prepared for:

Leedshill-Herkenhoff, Inc.

Project No.: 90-1-10

April 9, 1990

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