

Team Radio Drainage Report

Prepared For:

*Team Broadcasting Inc.
4131 Barbara Loop SE, Suite 2B
Rio Rancho, NM 87124
(505) 338-1438*

Prepared By:

*Mark Goodwin & Associates, PA
PO BOX 90606
Albuquerque, NM 87199
(505) 828-2200*



Contents

| | |
|--|---|
| Legal Description & Vicinity Map | 3 |
| Floodplain | 3 |
| Stormwater Management Plan | 3 |
| Upstream Offsite Flows | 3 |
| Basin Map | 4 |
| Hydrology..... | 5 |
| Hydraulic Calculations..... | 6 |
| Storm Water Quality Calculations | 6 |
| Survey | 6 |
| Benchmark | 6 |
| Soils..... | 7 |
| Planning History | 7 |
| North Coors Drainage Management Plan | 8 |
| Appendix..... | 9 |



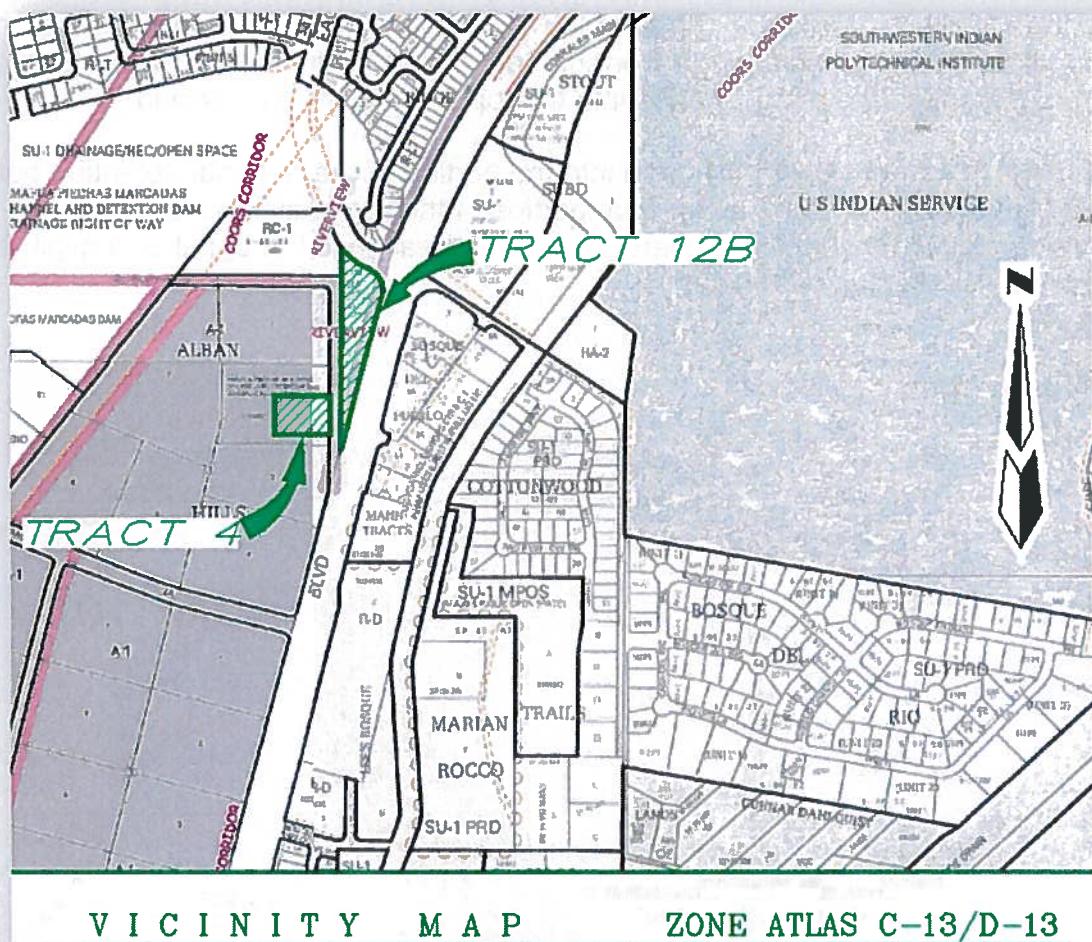
Legal Description & Vicinity Map

Parcel 12B Riverview

Addition containing 2.1483 acres in the City of Albuquerque and Tract 4 of the Piedras Marcadas Channel and Detention Dam Right of Way containing 4.23 acres in AMAFCA's jurisdiction.

Floodplain

There are not any special Flood Hazard Zones on or near this site as shown on Flood Insurance Rate Map Number 35001c0116G revised September 26, 2008.



Stormwater Management Plan

The peak 100 year stormwater runoff rates from this site will be less than the rate established by the *North Coors Drainage Management Plan – Middle Area* (Smith Feb '97) such that the capacity of the downstream double 21" RCPs is not exceeded. The *North Coors Drainage Management Plan – Middle Area* (Smith Feb '97) is accepted by AMAFCA and by the City of Albuquerque. When several of the culverts under Coors Blvd. were plugged as part of the construction of the *Bosque Del Pueblo Final Grading & Drainage Plan* (Greiner, 1989), a de facto pond was created on these properties unknown to the owners until recently. The Team Radio development will construct a new improved regional pond in accordance with an AMAFCA Turnkey Agreement date September 26, 2014. Drainage infrastructure west of the Team Radio site will then be maintained by AMAFCA. The new regional pond will cut the peak 100-YR flow rate from the 39.1 acre upstream offsite basins plus the onsite 2 acre basin to about half of the originally planned runoff rate (90 cfs reduced 53.21 cfs).

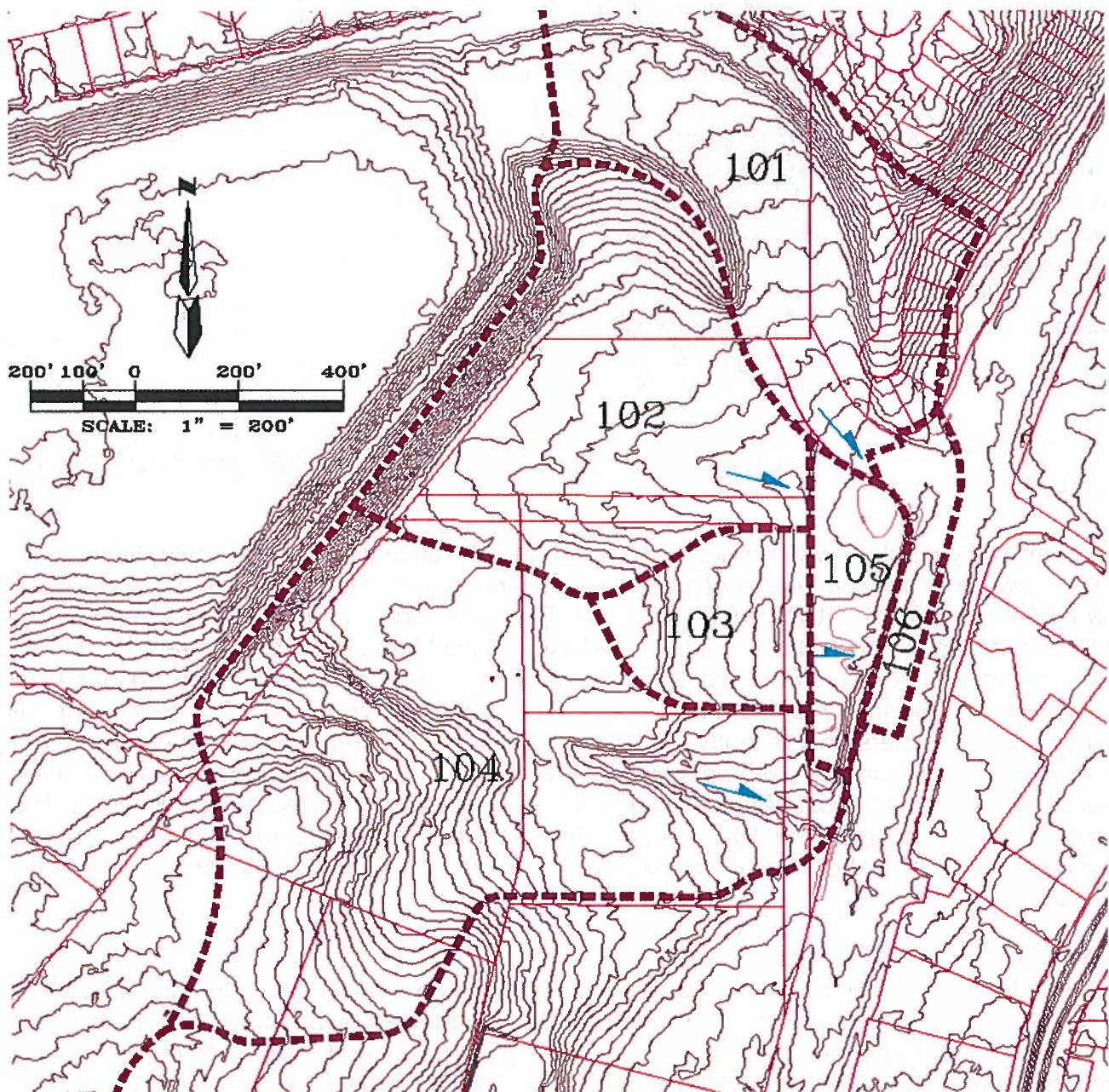
Upstream Offsite Flows

Drainage from Eagle Ranch Road and from Coors Blvd., Basins 101 and 106 respectively will be conveyed through Parcel 12B in a storm drain to be constructed by the developer and maintained by the City of Albuquerque. It will outfall into an existing 60" culvert under Coors Blvd., NMDOT owned and Maintained. The 60" culvert will be extended as part of the construction by the developer. Offsite flows from Basins 102 and 103 are diverted by a roadside ditch west of Calle Nortena to a sump in Calle Nortena where they flow on the surface over the Calle Nortena roadway and into this

site. There they will be joined by the onsite drainage (basin 105) and all will be conveyed on the surface through the parking lot to a concrete rundown that will drain the first flush into the onsite Storm Water Quality pond. The rundown will drain higher flows into the regional detention pond located on both sides of Calle Nortena near the 60" outfall under Coors Blvd. At peak stage the regional detention pond spreads into the top 0.57' of the SWQ pond.

Offsite flows from Basin 104 drain into the portion of the regional detention pond located on the AMAFCA right of way Tract 4. That portion of the regional pond is connected to the portion on Parcel 12B by a 48" RCP which is oversized so that head loss through it is negligible and the pond is at the same elevation on both sides.

Basin Map



Hydrology

AHYMO S4 is used for the hydrology calculations as contained in the Appendix of the Drainage Report. Ground cover is based on existing conditions in basin 101, the *North Coors Drainage Management Plan – Middle Area* (Smith Feb '97) in basins 102,103, and 104, and ground cover is based on Post development conditions in basins 105 and 106. The input and output results are summarized in the following table.

| HYDROLOGY SUMMARY | | | | | | | | | | | | | | |
|-------------------|-------------------|------|---------|------------------|------|------|-------|-------------------------------------|--------|------------------------------------|-------|------------------------------------|-------|----------|
| Description | AHYMO BASIN ID | AREA | | Ground Cover (%) | | | | Peak 100-YR Flow Q_{100} (cfs) | | Peak 10-YR Flow Q_{100} (cfs) | | Peak 10-YR Flow Q_{100} (cfs) | | |
| | | (Ac) | (Sq mi) | A | B | C | D | Incr | Total | Incr | Total | Incr | Total | (Ac.Ft.) |
| Eagle Ranch RD. | 101 | 8.5 | 0.01328 | 0.0 | 0.0 | 76.0 | 24.0 | 30.06 | 30.06 | 18.02 | 18.02 | 8.89 | 8.89 | 0.078 |
| Offsite west | 102 | 10.4 | 0.01625 | 50.0 | 16.6 | 16.7 | 16.7 | 26.72 | 58.72 | 12.59 | 30.61 | 3.72 | 12.61 | 0.067 |
| Offsite west | 103 | 2.2 | 0.00344 | 50.0 | 16.6 | 16.7 | 16.7 | 5.62 | 62.33 | 2.65 | 33.26 | 0.78 | 13.39 | 0.014 |
| Alban/AMAFCA | 104 | 16.7 | 0.02609 | 50.0 | 16.6 | 16.7 | 16.7 | 43.04 | 105.37 | 20.28 | 53.54 | 6.00 | 19.39 | 0.107 |
| Onsite | 105 | 2.0 | 0.00313 | 0.0 | 0.0 | 20.0 | 80.0 | 8.51 | 113.82 | 5.53 | 59.07 | 3.38 | 22.77 | 0.061 |
| Coors Rd | 106 | 1.3 | 0.00203 | 0.0 | 0.0 | 0.0 | 100.0 | 5.83 | 119.62 | 3.88 | 62.85 | 2.48 | 25.21 | 0.050 |
| Discharge from | Pond | | | | | | | 53.21 | | 40.41 | | 18.65 | | |

Precipitation values are from DPM Section 22.2, Table A-2, Zone 1. The Pond volume calculations were performed using the conic equation with the following results.

| Pond volume Calculations | | | | | | Outfall Hydraulic Calculations | | | | | | |
|--------------------------|---------------|-----------------|-------------|---------------------|-------------|--------------------------------|-------------|------|---------|--------|---------|-----------------|
| Elevation | AMAFCA Parcel | Team Radio Site | | Total On & Off-site | | Double 21" RCPs | | | 60" RCP | | | Outlet Capacity |
| | | Area (SF) | Vol (Ac-Ft) | Area (SF) | Vol (Ac-Ft) | Area (SF) | Vol (Ac-Ft) | HW/D | Q (cfs) | H (ft) | Q (cfs) | Q (cfs) |
| 5001.0 | 1,098 | 0.00 | 1,867 | 0.00 | 2,965 | 0.00 | 2.29 | 46.0 | 7.7 | 44.4 | 0.13 | 7.0 |
| 5002.0 | 10,582 | 0.12 | 3,635 | 0.06 | 14,217 | 0.18 | 2.86 | 54.4 | 8.7 | 48.0 | 0.33 | 22.0 |
| 5003.0 | 15,936 | 0.42 | 5,635 | 0.17 | 21,571 | 0.59 | 3.43 | 63.0 | 9.7 | 50.5 | 0.53 | 46.0 |
| 5004.0 | 19,201 | 0.82 | 7,985 | 0.32 | 27,186 | 1.14 | 4.00 | 68.0 | 10.7 | 52.6 | 0.73 | 82.0 |
| 5005.0 | 22,769 | 1.30 | 16,700 | 0.60 | 39,469 | 1.90 | 4.57 | 75.0 | 11.7 | 55.4 | 0.93 | 122.0 |
| 5006.0 | 26,640 | 1.87 | 34,740 | 1.18 | 61,380 | 3.05 | 5.14 | 80.0 | 12.7 | 57.6 | 1.13 | 160.0 |
| | | | | | | | | | | | | |

The pond discharge is set equal to the smallest of three capacity calculations as summarized in the table above. Inlet control at the 60" RCP on the west side of Coors limits discharge rates at depths of 2' and less while the discharge rate at greater depths is limited by outlet control in the double 21" RCPs. The following table summarizes the pond routing results. The capacity is established by the two nomographs for Concrete Pipe Culverts Flowing Full and for Concrete Pipe Culverts with Inlet Control from the Bureau of Public Roads Jan 1963 as contained in the Appendix of the Drainage Report.

The Team Radio Pond Summary Table

| Event Recurrence Interval | Peak Inflow (cfs) | Peak Outflow (cfs) | Peak Storage Volume | Peak Stage (ft) |
|---------------------------|-------------------|--------------------|---------------------|-----------------|
| 2-YR | 25.21 | 18.65 | 0.14 | 5001.77 |
| 10-YR | 62.85 | 40.41 | 0.49 | 5002.77 |
| 100-YR | 119.62 | 53.34 | 1.34 | 5004.26 |

Hydraulic Calculations

HGL calculations for the storm drain that parallels Coors Rd between Eagle Ranch Road and the existing 60" RCP under Coors Rd begin at the downstream end with the 100yr pond elevation at the moment when the peak flow rate enters the storm drain at Eagle Ranch Rd. From AHYMO the peak of basin 101 occurs at 1.53 hours when the pond stage is 5003.26. The peak flow rate in the 36" RCP is equal to 35.89cfs, the sum of basins 101 and 106.

Alternatively when the peak stage of the pond occurs, at 1.73 hours, the peak inflow is 52.47cfs which is 44% of the peak flow. At that moment the beginning HGL elevation at the downstream end is 5004.26 and the prorated flow in the 36" pipe is 15.74cfs.

The hydraulic grade line elevation was calculated using WSPGW at each of these two moments of the 100 year storm, peak inflow and peak pond stage, and the higher of the two elevations is shown on the pipe profiles along with the peak flow rate and corresponding velocity. The flow rates in the storm drains in Eagle Ranch Rd. are based on the record drawings for Eagle Ridge Subdivision, City Project # 702181.

The backwater effect of the pond on the 100 year surface drainage from The Team Radio site, including drainage from upstream offsite basins 102 and 103 that drain on the surface through The Team Radio site, was analyzed using HEC-RAS for the moment in the hydrograph where the peak flow rate of 41 cfs occurs, at 1.53 hours, when the pond stage is 5003.26. The analysis determined that the 100-yr elevation at The Team Radio site is 5004.85 which is higher than the peak 100 year pond stage of 5004.26. The lowest parking lot elevation is 5004.20 where the normal 100 year flow depth is 0.82' using Plate 22.3 D-4 for 41cfs at 0.50% slope compared to 0.65' depth backwater from the concrete spillway.

Storm Water Quality Calculations

The required volume is based on a 0.6" precipitation event that produces 0.46" runoff from impervious surfaces only and is shown for each basin in the Hydrology Summary table on page 5. The required volume for The Team Radio site is 0.61 ac-ft. The concrete spillway is designed to drain north into the SWQ pond(s) until the 0.67 ac-ft pond(s) fill up to elevation 5003.70, then it spills south into the detention pond.

Survey

The existing conditions as shown on the plans were surveyed by Aldrich Land Surveying revised October 27, 2014.

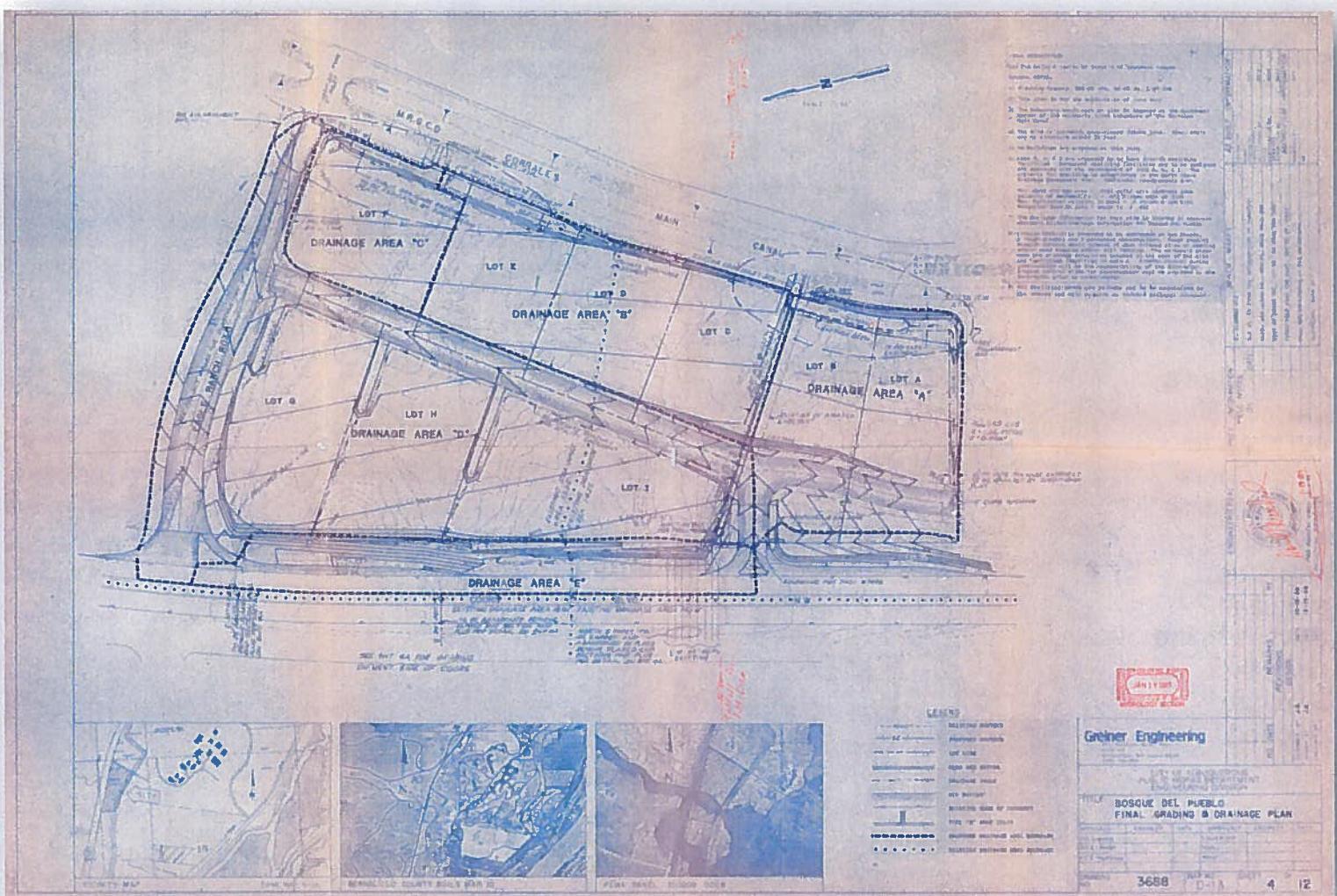
Benchmark

All elevations in this report are based on NGVD29 ASC Monument "R. Alameda B. No. 2" Elev. = 5058.25. Add 2.83' to the elevations in this report to convert to NAVD 88.

Soils

Earthwork construction is to be in accordance with the Geotechnical Engineering Services Job No. 1-40102, 101.7 The Team Office Building by GeoTest Inc. February 11, 2014.

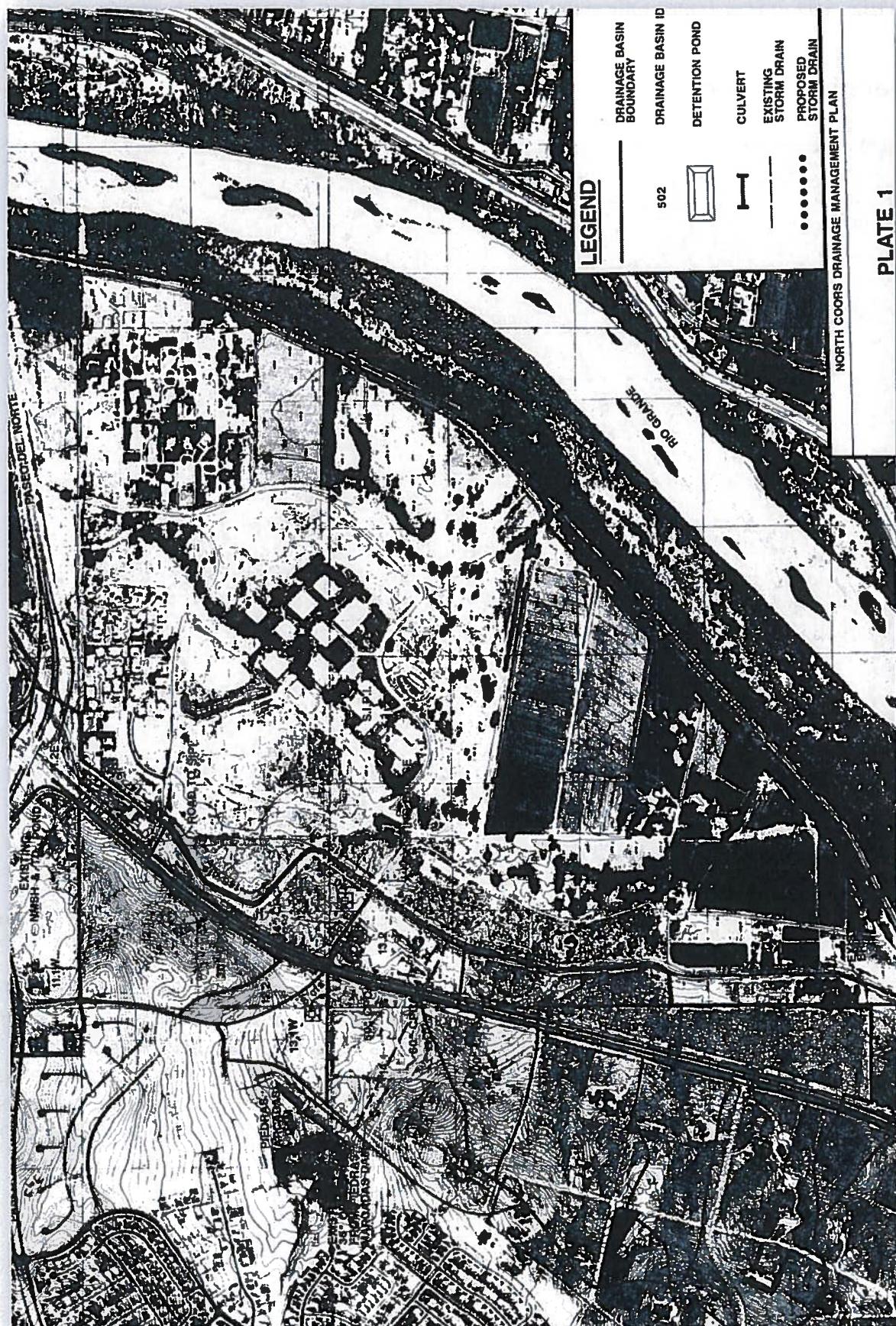
Planning History



The Piedras Marcadas Dam was constructed in 1984. Then the *Bosque Del Pueblo Final Grading & Drainage Plan* (Greiner, 1989) shows the plugging of several storm drain culverts under Coors leaving only the two existing 60" RCPs to drain this 41 acre basin, and that plan also shows the two 21" RCPs that were constructed through the downstream property thus limiting the discharge to the Corrales Main Canal to about 45 cfs. Because that is the maximum amount of flow that will fit through the two 21" pipes without overtopping Coors at the north end of this site and Calle Nortena at the south end of this site.

North Coors Drainage Management Plan

Then the North Coors Drainage Management Plan Middle Area (Smith, 1997) shows the following 100 Year discharge rates for the same 41 acre basin that drains through the existing two 60"/21" culverts but it planned for the flows to cross Coors Blvd. at three different locations, including 2 culverts to the north that were plugged.



Summary of North Coors DMP, 1997

| Area | | 100 Yr Flow Rate (cfs) | | Discharge per acre (cfs/ac) | Allowable Discharge |
|--------------|----------------|---------------------------------|---------------|-----------------------------------|------------------------|
| Basin | ID | (Sq Mi) | (Ac) | | |
| 12.2W | 0.00691 | 4.42 | 15.2 | 3.44 | 15 |
| 13.1W | 0.01020 | 6.53 | 20.67 | 3.17 | 8 |
| 14.1W | 0.05117 | 32.75 | 66.95 | 2.04 | 67 |
| Total | 0.06828 | 43.70 | 102.82 | | 90 |

Appendix

AHYMO 100 YR Input

2014-10-17 100 yr final

0.0 HRS PUNCH CODE=0 PRINT LINES=-6
 THE TEAM OFFICE BUILDING 100-YR, 6-HR DEVELOPED

START
 *S
 CONDITIONS
 LOCATION
 RAINFALL
 ALBUQUERQUE
 TYPE=1 RAIN QUARTER=0.0 RAIN ONE=1.87
 RAIN SIX=2.22 RAIN DAY=2.66 DT=.01
 COMPUTE NM HYD ID=1 HYD=101 DA=0.0133 SQ MI
 PER A=0 B=0 C=76 D=24
 TP=0.133333 HRS RAIN=-1
 PRINT HYD ID=1 CODE=1
 COMPUTE NM HYD ID=2 HYD=102 DA=0.0162 SQ MI
 PER A=50 B=16.6 C=16.7 D=16.7
 TP=0.133333 HRS RAIN=-1
 PRINT HYD ID=2 CODE=1
 COMPUTE NM HYD ID=3 HYD=103 DA=0.0034 SQ MI
 PER A=50 B=16.6 C=16.7 D=16.7
 TP=0.133333 HRS RAIN=-1
 PRINT HYD ID=3 CODE=1
 COMPUTE NM HYD ID=4 HYD=104 DA=0.0261 SQ MI
 PER A=50 B=16.6 C=16.7 D=16.7
 TP=0.133333 HRS RAIN=-1
 PRINT HYD ID=4 CODE=1
 COMPUTE NM HYD ID=5 HYD=105 DA=0.0031 SQ MI
 PER A=0 B=0 C=20 D=80
 TP=0.133333 HRS RAIN=-1
 PRINT HYD ID=5 CODE=1
 COMPUTE NM HYD ID=6 HYD=106 DA=0.0020 SQ MI
 PER A=0 B=0 C=0 D=100
 TP=0.133333 HRS RAIN=-1
 PRINT HYD ID=6 CODE=1
 ADD HYD ID=7 HYD=200 IDS= 1 & 2
 ADD HYD ID=8 HYD=201 IDS= 7 & 3
 ADD HYD ID=9 HYD=202 IDS= 8 & 4
 ADD HYD ID=10 HYD=203 IDS= 9 & 5
 ADD HYD ID=11 HYD=204 IDS= 10 & 6
 PRINT HYD ID=11 CODE=1
 ROUTE RESERVOIR ID=12 HYD=305 INFLOW ID=11 CODE=5

| OUTFLOW (CFS) | STORAGE (AC FT) | ELEV (FT) |
|---------------|-----------------|-----------|
| 0 | 0.00 | 5000 |
| 7 | 0.01 | 5001 |
| 22 | 0.18 | 5002 |
| 46 | 0.59 | 5003 |
| 52.6 | 1.14 | 5004 |
| 55.4 | 1.90 | 5005 |
| 57.6 | 3.05 | 5006 |

 PRINT HYD ID=12 CODE=1
 FINISH

← (s16.67h8.5vOT-&18D
AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4)
INPUT FILE = C:\Users\doug\Desktop\2014-10-17 100 yr final.txt

| COMMAND | HYDROGRAPH IDENTIFICATION NO. | FROM ID NO. | TO ID NO. | AREA (SQ MI) | PEAK DISCHARGE (CFS) | RUNOFF VOLUME (AC-FT) | RUNOFF (INCHES) | TIME TO PEAK (HOURS) | CFS PER ACRE | PAGE = 1 |
|---------------------------|--|-------------|-----------|--------------|----------------------|-----------------------|-----------------|----------------------|-----------------------|--------------|
| START *S | THE TEAM OFFICE BUILDING 100-YR, 6-HR DEVELOPED CONDITIONS ALBUQUERQUE | | | | | | | | | TIME= 0.00 |
| RAINFALL, TYPE= 1 NOAA 14 | | | | | | | | | | RAIN6= 2.220 |
| COMPUTE NM HYD | 101.00 | - | 1 | 0.01330 | 30.06 | 0.923 | 1.30184 | 1.530 | 3.531 PER IMP= 24.00 | |
| COMPUTE NM HYD | 102.00 | - | 2 | 0.01620 | 26.72 | 0.833 | 0.96382 | 1.540 | 2.578 PER IMP= 16.70 | |
| COMPUTE NM HYD | 103.00 | - | 3 | 0.00340 | 5.62 | 0.175 | 0.96382 | 1.540 | 2.584 PER IMP= 16.70 | |
| COMPUTE NM HYD | 104.00 | - | 4 | 0.02610 | 43.04 | 1.342 | 0.96382 | 1.540 | 2.577 PER IMP= 16.70 | |
| COMPUTE NM HYD | 105.00 | - | 5 | 0.00310 | 8.51 | 0.297 | 1.79603 | 1.530 | 4.289 PER IMP= 80.00 | |
| COMPUTE NM HYD | 106.00 | - | 6 | 0.00200 | 5.83 | 0.210 | 1.97253 | 1.520 | 4.557 PER IMP= 100.00 | |
| ADD HYD | 200.00 | 1& 2 | 7 | 0.02950 | 56.72 | 1.756 | 1.11619 | 1.530 | 3.004 | |
| ADD HYD | 201.00 | 7& 3 | 8 | 0.03290 | 62.33 | 1.931 | 1.10044 | 1.530 | 2.960 | |
| ADD HYD | 202.00 | 8& 4 | 9 | 0.05900 | 105.37 | 3.273 | 1.04000 | 1.540 | 2.790 | |
| ADD HYD | 203.00 | 9& 5 | 10 | 0.06210 | 113.82 | 3.569 | 1.07773 | 1.540 | 2.864 | |
| ADD HYD | 204.00 | 10& 6 | 11 | 0.06410 | 119.62 | 3.780 | 1.10565 | 1.530 | 2.916 | |
| ROUTE RESERVOIR FINISH | 305.00 | 11 | 12 | 0.06410 | 53.34 | 3.780 | 1.10565 | 1.730 | 1.300 AC-FT= 1.341 | |

← (s010h4099T-&16D

AHYMO 100 -YR Summary

AHYMO PROGRAM (AHYMO-S4) - Version: S4.01a - Rel: 01a
 RUN DATE (MON/DAY/YR) = 10/17/2014
 START TIME (HR:MIN:SEC) = 16:45:39 USER NO.= AHYMO_Temp_User:20122010
 INPUT FILE = C:\Users\ Doug\Desktop\2014-10-17 100 yr final.txt

| | |
|--|--|
| START | 0.0 HRS PUNCH CODE=0 PRINT LINES=-6 |
| * S | THE TEAM OFFICE BUILDING 100-YR, 6-HR DEVELOPED CONDITIONS |
| LOCATION | ALBUQUERQUE |
| City of Albuquerque soil infiltration values (LAND FACTORS) used for computations. | |
| Land Treatment | Initial Abstr. (in) |
| A | 0.65 |
| B | 0.50 |
| C | 0.35 |
| D | 0.10 |
| TYPE=1 RAIN QUARTER=0.0 RAIN ONE=1.87 | |
| RAINFALL | DT=.01 |
| RAIN SIX=2.22 | RAIN DAY=2.66 |

RAINFALL

TYPE=1 RAIN QUARTER=0.0 RAIN ONE=1.87
 DT=.01
 RAIN SIX=2.22 RAIN DAY=2.66 DT=.01

6-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1
 DT = 0.010000 HOURS END TIME = 6.000000 HOURS

| | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|
| 0.0000 | 0.0005 | 0.0009 | 0.0014 | 0.0019 | 0.0023 | 0.0028 |
| 0.0033 | 0.0037 | 0.0042 | 0.0048 | 0.0053 | 0.0058 | 0.0063 |
| 0.0068 | 0.0073 | 0.0079 | 0.0084 | 0.0090 | 0.0096 | 0.0101 |
| 0.0107 | 0.0113 | 0.0119 | 0.0125 | 0.0130 | 0.0137 | 0.0144 |
| 0.0150 | 0.0157 | 0.0163 | 0.0170 | 0.0177 | 0.0183 | 0.0195 |
| 0.0209 | 0.0223 | 0.0238 | 0.0252 | 0.0266 | 0.0280 | 0.0294 |
| 0.0309 | 0.0325 | 0.0341 | 0.0357 | 0.0373 | 0.0389 | 0.0405 |
| 0.0421 | 0.0437 | 0.0454 | 0.0472 | 0.0489 | 0.0507 | 0.0524 |
| 0.0542 | 0.0559 | 0.0577 | 0.0595 | 0.0613 | 0.0631 | 0.0650 |
| 0.0668 | 0.0686 | 0.0705 | 0.0723 | 0.0742 | 0.0761 | 0.0780 |
| 0.0799 | 0.0819 | 0.0838 | 0.0857 | 0.0876 | 0.0896 | 0.0917 |
| 0.0939 | 0.0960 | 0.0982 | 0.1004 | 0.1025 | 0.1047 | 0.1068 |
| 0.1092 | 0.1116 | 0.1141 | 0.1165 | 0.1190 | 0.1214 | 0.1239 |
| 0.1263 | 0.1298 | 0.1352 | 0.1406 | 0.1460 | 0.1514 | 0.1568 |
| 0.1622 | 0.1676 | 0.1730 | 0.1803 | 0.1875 | 0.1948 | 0.2020 |
| 0.2093 | 0.2165 | 0.2238 | 0.2310 | 0.2402 | 0.2503 | 0.2605 |
| 0.2706 | 0.2807 | 0.2909 | 0.3010 | 0.3112 | 0.3230 | 0.3382 |
| 0.3534 | 0.3687 | 0.3839 | 0.3991 | 0.4144 | 0.4296 | 0.4448 |
| 0.4711 | 0.4974 | 0.5237 | 0.5499 | 0.5762 | 0.6025 | 0.6288 |
| 0.6551 | 0.7105 | 0.7805 | 0.8506 | 0.9206 | 0.9906 | 1.0606 |
| 1.1307 | 1.2007 | 1.2603 | 1.2991 | 1.3379 | 1.3767 | 1.4156 |
| 1.4544 | 1.4932 | 1.5320 | 1.5708 | 1.5903 | 1.6098 | 1.6293 |
| 1.6488 | 1.6683 | 1.6878 | 1.7073 | 1.7268 | 1.7415 | 1.7538 |
| 1.7661 | 1.7784 | 1.7907 | 1.8029 | 1.8152 | 1.8275 | 1.8385 |
| 1.8471 | 1.8556 | 1.8641 | 1.8726 | 1.8811 | 1.8896 | 1.8982 |
| 1.9067 | 1.9129 | 1.9191 | 1.9254 | 1.9316 | 1.9378 | 1.9441 |
| 1.9503 | 1.9565 | 1.9618 | 1.9665 | 1.9712 | 1.9759 | 1.9806 |
| 1.9854 | 1.9901 | 1.9948 | 1.9987 | 2.0010 | 2.0033 | 2.0056 |

92

| | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|
| 2.0079 | 2.0102 | 2.0125 | 2.0148 | 2.0171 | 2.0191 | 2.0211 |
| 2.0232 | 2.0252 | 2.0272 | 2.0293 | 2.0313 | 2.0333 | 2.0351 |
| 2.0368 | 2.0385 | 2.0401 | 2.0418 | 2.0435 | 2.0452 | 2.0468 |
| 2.0484 | 2.0500 | 2.0515 | 2.0530 | 2.0546 | 2.0561 | 2.0576 |
| 2.0592 | 2.0607 | 2.0622 | 2.0637 | 2.0651 | 2.0666 | 2.0681 |
| 2.0696 | 2.0710 | 2.0725 | 2.0735 | 2.0742 | 2.0749 | 2.0756 |
| 2.0763 | 2.0770 | 2.0777 | 2.0784 | 2.0791 | 2.0798 | 2.0805 |
| 2.0812 | 2.0819 | 2.0826 | 2.0833 | 2.0839 | 2.0846 | 2.0853 |
| 2.0859 | 2.0865 | 2.0872 | 2.0878 | 2.0885 | 2.0891 | 2.0897 |
| 2.0904 | 2.0910 | 2.0916 | 2.0922 | 2.0928 | 2.0934 | 2.0941 |
| 2.0947 | 2.0953 | 2.0959 | 2.0965 | 2.0971 | 2.0977 | 2.0983 |
| 2.0989 | 2.0995 | 2.1001 | 2.1006 | 2.1012 | 2.1018 | 2.1023 |
| 2.1029 | 2.1035 | 2.1040 | 2.1046 | 2.1051 | 2.1057 | 2.1062 |
| 2.1068 | 2.1073 | 2.1079 | 2.1084 | 2.1090 | 2.1095 | 2.1100 |
| 2.1106 | 2.1111 | 2.1116 | 2.1122 | 2.1127 | 2.1132 | 2.1138 |
| 2.1143 | 2.1148 | 2.1153 | 2.1158 | 2.1163 | 2.1168 | 2.1173 |
| 2.1178 | 2.1183 | 2.1188 | 2.1193 | 2.1198 | 2.1202 | 2.1207 |
| 2.1212 | 2.1217 | 2.1222 | 2.1227 | 2.1232 | 2.1236 | 2.1241 |
| 2.1246 | 2.1251 | 2.1256 | 2.1260 | 2.1265 | 2.1269 | 2.1274 |
| 2.1279 | 2.1283 | 2.1288 | 2.1292 | 2.1297 | 2.1301 | 2.1306 |
| 2.1310 | 2.1315 | 2.1319 | 2.1324 | 2.1328 | 2.1332 | 2.1337 |
| 2.1341 | 2.1346 | 2.1350 | 2.1354 | 2.1359 | 2.1363 | 2.1367 |
| 2.1372 | 2.1376 | 2.1380 | 2.1385 | 2.1389 | 2.1393 | 2.1397 |
| 2.1402 | 2.1406 | 2.1410 | 2.1414 | 2.1418 | 2.1423 | 2.1427 |
| 2.1431 | 2.1435 | 2.1439 | 2.1443 | 2.1447 | 2.1452 | 2.1456 |
| 2.1460 | 2.1464 | 2.1468 | 2.1472 | 2.1476 | 2.1480 | 2.1484 |
| 2.1488 | 2.1492 | 2.1496 | 2.1500 | 2.1504 | 2.1508 | 2.1512 |
| 2.1516 | 2.1520 | 2.1524 | 2.1528 | 2.1532 | 2.1535 | 2.1539 |
| 2.1543 | 2.1547 | 2.1551 | 2.1555 | 2.1559 | 2.1562 | 2.1566 |
| 2.1570 | 2.1574 | 2.1578 | 2.1582 | 2.1585 | 2.1589 | 2.1593 |
| 2.1597 | 2.1600 | 2.1604 | 2.1608 | 2.1612 | 2.1615 | 2.1619 |
| 2.1623 | 2.1626 | 2.1630 | 2.1634 | 2.1637 | 2.1641 | 2.1645 |
| 2.1648 | 2.1652 | 2.1656 | 2.1659 | 2.1663 | 2.1666 | 2.1670 |
| 2.1674 | 2.1677 | 2.1681 | 2.1684 | 2.1688 | 2.1691 | 2.1695 |
| 2.1699 | 2.1702 | 2.1706 | 2.1709 | 2.1713 | 2.1716 | 2.1720 |
| 2.1723 | 2.1727 | 2.1730 | 2.1733 | 2.1737 | 2.1740 | 2.1744 |
| 2.1747 | 2.1751 | 2.1754 | 2.1757 | 2.1761 | 2.1764 | 2.1768 |
| 2.1771 | 2.1774 | 2.1778 | 2.1781 | 2.1784 | 2.1788 | 2.1791 |
| 2.1794 | 2.1798 | 2.1801 | 2.1804 | 2.1808 | 2.1811 | 2.1814 |
| 2.1818 | 2.1821 | 2.1824 | 2.1827 | 2.1831 | 2.1834 | 2.1837 |
| 2.1840 | 2.1844 | 2.1847 | 2.1850 | 2.1853 | 2.1856 | 2.1860 |
| 2.1863 | 2.1866 | 2.1869 | 2.1872 | 2.1876 | 2.1879 | 2.1882 |
| 2.1885 | 2.1888 | 2.1891 | 2.1894 | 2.1898 | 2.1901 | 2.1904 |
| 2.1907 | 2.1910 | 2.1913 | 2.1916 | 2.1919 | 2.1922 | 2.1926 |
| 2.1929 | 2.1932 | 2.1935 | 2.1938 | 2.1941 | 2.1944 | 2.1947 |
| 2.1950 | 2.1953 | 2.1956 | 2.1959 | 2.1962 | 2.1965 | 2.1968 |
| 2.1971 | 2.1974 | 2.1977 | 2.1980 | 2.1983 | 2.1986 | 2.1989 |
| 2.1992 | 2.1995 | 2.1998 | 2.2001 | 2.2004 | 2.2007 | 2.2009 |
| 2.2012 | 2.2015 | 2.2018 | 2.2021 | 2.2024 | 2.2027 | 2.2030 |
| 2.2033 | 2.2036 | 2.2038 | 2.2041 | 2.2044 | 2.2047 | 2.2050 |
| 2.2053 | 2.2056 | 2.2058 | 2.2061 | 2.2064 | 2.2067 | 2.2070 |

2.2073 2.2075 2.2078 2.2081 2.2084 2.2087 2.2089
 2.2092 2.2095 2.2098 2.2101 2.2103 2.2106 2.2109
 2.2112 2.2114 2.2117 2.2120 2.2123 2.2125 2.2128
 2.2131 2.2133 2.2136 2.2139 2.2142 2.2144 2.2147
 2.2150 2.2152 2.2155 2.2158 2.2160 2.2163 2.2166
 2.2168 2.2171 2.2174 2.2176 2.2179 2.2182 2.2184
 2.2187 2.2189 2.2192 2.2195 2.2197 2.2200

COMPUTE NM HYD ID=1 HYD=101 DA=0.0133 SQ MI
 PER A=0 B=0 C=76 D=24
 TP=0.133333 HRS RAIN=-1

$K = 0.072666 \text{HR}$ $TP = 0.133333 \text{HR}$ $K/TP \text{ RATIO} = 0.545000$ SHAPE CONSTANT, $N = 7.106428$
 UNIT PEAK = 12.599 CFS UNIT VOLUME = 0.9990 $B = 526.28$ $P60 = 1.8700$
 AREA = 0.003192 SQ MI $IA = 0.10000 \text{ INCHES}$ $INF = 0.04000 \text{ INCHES PER HOUR}$
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 101.00

RUNOFF VOLUME = 1.30184 INCHES = 0.9234 ACRE-FEET
 PEAK DISCHARGE RATE = 30.06 CFS AT 1.530 HOURS BASIN AREA = 0.0133 SQ. MI.

COMPUTE NM HYD ID=2 HYD=102 DA=0.0162 SQ MI
 PER A=50 B=16.6 C=16.7 D=16.7
 TP=0.133333 HRS RAIN=-1

$K = 0.072666 \text{HR}$ $TP = 0.133333 \text{HR}$ $K/TP \text{ RATIO} = 0.545000$ SHAPE CONSTANT, $N = 7.106428$
 UNIT PEAK = 10.678 CFS UNIT VOLUME = 0.9988 $B = 526.28$ $P60 = 1.8700$
 AREA = 0.002705 SQ MI $IA = 0.10000 \text{ INCHES}$ $INF = 0.04000 \text{ INCHES PER HOUR}$
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=2 CODE=1

PARTIAL HYDROGRAPH 102.00

$K = 0.145614 \text{HR}$ $TP = 0.133333 \text{HR}$ $K/TP \text{ RATIO} = 1.092107$ SHAPE CONSTANT, $N = 3.235735$
 UNIT PEAK = 30.415 CFS UNIT VOLUME = 0.9995 $B = 300.52$ $P60 = 1.8700$
 AREA = 0.013495 SQ MI $IA = 0.55996 \text{ INCHES}$ $INF = 1.41790 \text{ INCHES PER HOUR}$
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

RUNOFF VOLUME = 0.96382 INCHES = 0.8327 ACRE-FEET
PEAK DISCHARGE RATE = 26.72 CFS AT 1.540 HOURS BASIN AREA = 0.0162 SQ. MI.

```
COMPUTE NM HYD ID=3 HYD=103 DA=0.0034 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1

K = 0.072666HHR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 2.2412 CFS UNIT VOLUME = 0.9945 B = 526.28 P60 = 1.8700
AREA = 0.000568 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=3 CODE=1
PARTIAL HYDROGRAPH 103.00
```

RUNOFF VOLUME = 0.96382 INCHES = 0.1748 ACRE-FEET
PEAK DISCHARGE RATE = 5.62 CFS AT 1.540 HOURS BASIN AREA = 0.0034 SQ. MI.

```
COMPUTE NM HYD ID=4 HYD=104 DA=0.0261 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1

K = 0.072666HHR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 17.204 CFS UNIT VOLUME = 0.9993 B = 526.28 P60 = 1.8700
AREA = 0.004359 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=4 CODE=1
PARTIAL HYDROGRAPH 104.00
```

RUNOFF VOLUME = 0.96382 INCHES = 1.3416 ACRE-FEET
PEAK DISCHARGE RATE = 43.04 CFS AT 1.540 HOURS BASIN AREA = 0.0261 SQ. MI.

COMPUTE NM HYD ID=5 HYD=105 DA=0.0031 SQ MI
PER A=0 B=0 C=20 D=80
TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 9.7887 CFS UNIT VOLUME = 0.9987 B = 526.28 P60 = 1.8700
AREA = 0.002480 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

K = 0.105893HR TP = 0.133333HR K/TP RATIO = 0.794199 SHAPE CONSTANT, N = 4.514592
UNIT PEAK = 1.8048 CFS UNIT VOLUME = 0.9924 B = 388.14 P60 = 1.8700
AREA = 0.000620 SQ MI IA = 0.35000 INCHES INF = 0.83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=5 CODE=1
PARTIAL HYDROGRAPH 105.00

RUNOFF VOLUME = 1.79603 INCHES = 0.2969 ACRE-FEET
PEAK DISCHARGE RATE = 8.51 CFS AT 1.530 HOURS BASIN AREA = 0.0031 SQ. MI.

COMPUTE NM HYD ID=6 HYD=106 DA=0.0020 SQ MI
PER A=0 B=0 C=0 D=100
TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 7.8942 CFS UNIT VOLUME = 0.9984 B = 526.28 P60 = 1.8700
AREA = 0.002000 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=6 CODE=1
PARTIAL HYDROGRAPH 106.00

RUNOFF VOLUME = 1.97253 INCHES = 0.2104 ACRE-FEET
PEAK DISCHARGE RATE = 5.83 CFS AT 1.520 HOURS BASIN AREA = 0.0020 SQ. MI.

ADD HYD ID=7 HYD=200 IDS= 1 & 2

ADD HYD
ADD HYD
ADD HYD
ADD HYD
PRINT HYD

ID=8 HYD=201 IDS= 7 & 3
ID=9 HYD=202 IDS= 8 & 4
ID=10 HYD=203 IDS= 9 & 5
ID=11 HYD=204 IDS= 10 & 6
ID=11 CODE=1

PARTIAL HYDROGRAPH 204.00

RUNOFF VOLUME = 1.10565 INCHES = 3.7798 ACRE-FEET
PEAK DISCHARGE RATE = 119.62 CFS AT 1.530 HOURS BASIN AREA = 0.0641 SQ. MI.

| ROUTE RESERVOIR | ID=12 HYD=305 INFLOW OUTFLOW (CFS) | ID=11 CODE=5 STORAGE (AC FT) | ELEV (FT) | |
|-----------------|---------------------------------------|---------------------------------|-------------------|------------------|
| TIME (HRS) | INFLOW (CFS) | ELEV (FEET) | VOLUME (AC-FT) | OUTFLOW (CFS) |
| * | * | * | * | * |
| 0.00 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.05 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.10 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.15 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.20 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.25 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.30 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.35 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.40 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.45 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.50 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.55 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.60 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.65 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.70 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.75 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.80 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.85 | 0.02 | 5000.00 | 0.000 | 0.01 |
| 0.90 | 0.31 | 5000.03 | 0.000 | 0.19 |
| 0.95 | 0.90 | 5000.10 | 0.001 | 0.69 |
| 1.00 | 1.62 | 5000.19 | 0.002 | 1.35 |
| 1.05 | 2.68 | 5000.33 | 0.003 | 2.31 |

| TIME (HRS) | INFLOW (CFS) | ELEV (FEET) | VOLUME (AC-FT) | OUTFLOW (CFS) |
|---------------|-----------------|----------------|-------------------|------------------|
| 1.10 | 5000.49 | 0.005 | 3.46 | |
| 1.15 | 5.00 | 0.007 | 4.60 | |
| 1.20 | 6.32 | 0.008 | 5.85 | |
| 1.25 | 8.18 | 0.011 | 7.08 | |
| 1.30 | 11.46 | 0.020 | 7.90 | |
| 1.35 | 18.93 | 0.044 | 10.02 | |
| 1.40 | 41.00 | 0.110 | 15.79 | |
| 1.45 | 81.48 | 0.271 | 27.33 | |
| 1.50 | 113.28 | 0.537 | 42.92 | |
| 1.55 | 118.64 | 0.832 | 48.90 | |
| 1.60 | 103.94 | 1.087 | 51.96 | |
| 1.65 | 82.35 | 1.255 | 53.02 | |
| 1.70 | 61.99 | 1.332 | 53.31 | |
| 1.75 | 46.12 | 1.334 | 53.31 | |
| 1.80 | 34.44 | 1.279 | 53.11 | |
| 1.85 | 26.21 | 1.184 | 52.76 | |
| 1.90 | 20.62 | 1.064 | 51.69 | |
| 1.95 | 16.89 | 0.931 | 50.09 | |
| 2.00 | 14.11 | 0.791 | 48.41 | |
| 2.05 | 11.73 | 0.648 | 46.69 | |
| 2.10 | 9.81 | 0.508 | 41.17 | |
| 2.15 | 8.37 | 0.390 | 34.27 | |
| 2.20 | 7.23 | 0.292 | 28.57 | |
| 2.25 | 6.29 | 0.212 | 23.88 | |
| 2.30 | 5.51 | 0.147 | 19.09 | |
| 2.35 | 4.86 | 0.099 | 14.83 | |
| 2.40 | 4.29 | 0.063 | 11.69 | |
| 2.45 | 3.67 | 0.036 | 9.33 | |
| 2.50 | 3.07 | 0.016 | 7.50 | |
| 2.55 | 2.60 | 0.005 | 3.29 | |
| 2.60 | 2.24 | 0.003 | 2.39 | |
| 2.65 | 1.95 | 0.003 | 2.05 | |
| 2.70 | 1.70 | 0.003 | 1.79 | |
| 2.75 | 1.49 | 0.002 | 1.56 | |
| | | | | |
| 3.86 | 5000.49 | 0.005 | 3.46 | |
| 5.00 | 5000.66 | 0.007 | 4.60 | |
| 6.32 | 5000.84 | 0.008 | 5.85 | |
| 8.18 | 5001.01 | 0.011 | 7.08 | |
| 11.46 | 5001.06 | 0.020 | 7.90 | |
| 18.93 | 5001.20 | 0.044 | 10.02 | |
| 41.00 | 5001.59 | 0.110 | 15.79 | |
| 81.48 | 5002.22 | 0.271 | 27.33 | |
| 113.28 | 5002.87 | 0.537 | 42.92 | |
| 118.64 | 5003.44 | 0.832 | 48.90 | |
| 103.94 | 5003.90 | 1.087 | 51.96 | |
| 82.35 | 5004.15 | 1.255 | 53.02 | |
| 61.99 | 5004.25 | 1.332 | 53.31 | |
| 46.12 | 5004.25 | 1.334 | 53.31 | |
| 34.44 | 5004.18 | 1.279 | 53.11 | |
| 26.21 | 5004.06 | 1.184 | 52.76 | |
| 20.62 | 5003.86 | 1.064 | 51.69 | |
| 16.89 | 5003.62 | 0.931 | 50.09 | |
| 14.11 | 5003.37 | 0.791 | 48.41 | |
| 11.73 | 5003.10 | 0.648 | 46.69 | |
| 9.81 | 5002.80 | 0.508 | 41.17 | |
| 8.37 | 5002.51 | 0.390 | 34.27 | |
| 7.23 | 5002.27 | 0.292 | 28.57 | |
| 6.29 | 5002.08 | 0.212 | 23.88 | |
| 5.51 | 5001.81 | 0.147 | 19.09 | |
| 4.86 | 5001.52 | 0.099 | 14.83 | |
| 4.29 | 5001.31 | 0.063 | 11.69 | |
| 3.67 | 5001.16 | 0.036 | 9.33 | |
| 3.07 | 5001.03 | 0.016 | 7.50 | |
| 2.60 | 5000.47 | 0.005 | 3.29 | |
| 2.24 | 5000.34 | 0.003 | 2.39 | |
| 1.95 | 5000.29 | 0.003 | 2.05 | |
| 1.70 | 5000.25 | 0.003 | 1.79 | |
| 1.49 | 5000.22 | 0.002 | 1.56 | |
| | | | | |
| 2.80 | 1.31 | 5000.20 | 0.002 | 1.37 |
| 2.85 | 1.15 | 5000.17 | 0.002 | 1.20 |
| 2.90 | 1.01 | 5000.15 | 0.002 | 1.06 |
| 2.95 | 0.89 | 5000.13 | 0.001 | 0.93 |
| 3.00 | 0.79 | 5000.12 | 0.001 | 0.83 |
| 3.05 | 0.71 | 5000.11 | 0.001 | 0.74 |
| 3.10 | 0.63 | 5000.09 | 0.001 | 0.66 |
| 3.15 | 0.56 | 5000.08 | 0.001 | 0.59 |
| 3.20 | 0.50 | 5000.07 | 0.001 | 0.52 |
| 3.25 | 0.45 | 5000.07 | 0.001 | 0.47 |
| 3.30 | 0.41 | 5000.06 | 0.001 | 0.43 |
| 3.35 | 0.37 | 5000.06 | 0.001 | 0.39 |
| 3.40 | 0.34 | 5000.05 | 0.001 | 0.35 |

| TIME (HRS) | INFLOW (CFS) | ELEV (FEET) | VOLUME (AC-FT) | OUTFLOW (CFS) |
|---------------|-----------------|----------------|-------------------|------------------|
| 3.45 | 5000.05 | 0.000 | 0.32 | |
| 3.50 | 0.28 | 5000.04 | 0.000 | 0.29 |
| 3.55 | 0.26 | 5000.04 | 0.000 | 0.27 |
| 3.60 | 0.24 | 5000.04 | 0.000 | 0.25 |
| 3.65 | 0.22 | 5000.03 | 0.000 | 0.23 |
| 3.70 | 0.20 | 5000.03 | 0.000 | 0.21 |
| 3.75 | 0.19 | 5000.03 | 0.000 | 0.19 |
| 3.80 | 0.18 | 5000.03 | 0.000 | 0.18 |
| 3.85 | 0.17 | 5000.02 | 0.000 | 0.18 |
| 3.90 | 0.17 | 5000.02 | 0.000 | 0.17 |
| 3.95 | 0.16 | 5000.02 | 0.000 | 0.16 |
| 4.00 | 0.16 | 5000.02 | 0.000 | 0.16 |
| 4.05 | 0.15 | 5000.02 | 0.000 | 0.15 |
| 4.10 | 0.15 | 5000.02 | 0.000 | 0.15 |
| 4.15 | 0.15 | 5000.02 | 0.000 | 0.15 |
| 4.20 | 0.15 | 5000.02 | 0.000 | 0.15 |
| 4.25 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.30 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.35 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.40 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.45 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.50 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.55 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.60 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.65 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.70 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 4.75 | 0.15 | 5000.02 | 0.000 | 0.14 |
| 4.80 | 0.15 | 5000.02 | 0.000 | 0.14 |
| 4.85 | 0.15 | 5000.02 | 0.000 | 0.15 |
| 4.90 | 0.15 | 5000.02 | 0.000 | 0.15 |
| 4.95 | 0.16 | 5000.02 | 0.000 | 0.16 |
| 5.00 | 0.16 | 5000.02 | 0.000 | 0.16 |
| 5.05 | 0.16 | 5000.02 | 0.000 | 0.16 |
| 5.10 | 0.17 | 5000.02 | 0.000 | 0.17 |
| 5.15 | 0.17 | 5000.02 | 0.000 | 0.17 |
| 5.20 | 0.18 | 5000.02 | 0.000 | 0.18 |
| 5.25 | 0.18 | 5000.03 | 0.000 | 0.18 |
| 5.30 | 0.18 | 5000.03 | 0.000 | 0.18 |
| 5.35 | 0.19 | 5000.03 | 0.000 | 0.19 |
| 5.40 | 0.19 | 5000.03 | 0.000 | 0.19 |
| 5.45 | 0.19 | 5000.03 | 0.000 | 0.19 |
| 5.50 | 0.20 | 5000.03 | 0.000 | 0.20 |
| 5.55 | 0.20 | 5000.03 | 0.000 | 0.20 |

| INT HYD | RUNOFF VOLUME = | 1.10565 INCHES | = | 3.7798 ACRE-FEET |
|--------------|-----------------------------------|----------------------------------|-------------------|------------------|
| | PEAK DISCHARGE RATE = | 53.34 CFS | AT | 1.730 HOURS |
| | MAXIMUM WATER SURFACE ELEVATION = | 5004.264 | BASIN AREA = | 0.0641 SQ. MI. |
| | MAXIMUM STORAGE = | 1.3407 AC-FT | INCREMENTAL TIME= | 0.010000HRS |
| ID=12 CODE=1 | HYDROGRAPH FROM AREA | 305.00 | | |
| 5.80 | 0.22 | 5000.03 | 0.000 | 0.22 |
| 5.85 | 0.23 | 5000.03 | 0.000 | 0.23 |
| 5.90 | 0.23 | 5000.03 | 0.000 | 0.23 |
| 5.95 | 0.24 | 5000.03 | 0.000 | 0.24 |
| 6.00 | 0.24 | 5000.03 | 0.000 | 0.24 |
| 6.05 | 0.24 | 5000.03 | 0.000 | 0.24 |
| 6.10 | 0.21 | 5000.03 | 0.000 | 0.22 |
| 6.15 | 0.13 | 5000.02 | 0.000 | 0.16 |
| 6.20 | 0.08 | 5000.01 | 0.000 | 0.10 |
| 6.25 | 0.05 | 5000.01 | 0.000 | 0.06 |
| 6.30 | 0.03 | 5000.01 | 0.000 | 0.04 |
| 6.35 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 6.40 | 0.02 | 5000.00 | 0.000 | 0.02 |
| 6.45 | 0.02 | 5000.00 | 0.000 | 0.02 |
| 6.50 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 6.55 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 6.60 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 6.65 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 6.70 | 0.00 | 5000.00 | 0.000 | 0.00 |
| | PEAK DISCHARGE = | 53.339 CFS - PEAK OCCURS AT HOUR | 1.73 | |
| | MAXIMUM WATER SURFACE ELEVATION = | 5004.264 | | |
| | MAXIMUM STORAGE = | 1.3407 AC-FT | | |

AHYMO 10 YR Input

2014-10-17 10 yr final

```

START          0.0 HRS PUNCH CODE=0 PRINT LINES=-6
*S
LOCATION      THE TEAM OFFICE BUILDING 10-YR, 6-HR DEVELOPED CONDITIONS
RAINFALL      ALBUQUERQUE
              TYPE=1 RAIN QUARTER=0.0 RAIN ONE=1.25
              RAIN SIX=1.47 RAIN DAY=1.77 DT=.01
              ID=1 HYD=101 DA=0.0133 SQ MI
              PER A=0 B=0 C=76 D=24
              TP=0.133333 HRS RAIN=-1
PRINT HYD     ID=1 CODE=1
COMPUTE NM HYD ID=2 HYD=102 DA=0.0162 SQ MI
                PER A=50 B=16.6 C=16.7 D=16.7
                TP=0.133333 HRS RAIN=-1
PRINT HYD     ID=2 CODE=1
COMPUTE NM HYD ID=3 HYD=103 DA=0.0034 SQ MI
                PER A=50 B=16.6 C=16.7 D=16.7
                TP=0.133333 HRS RAIN=-1
PRINT HYD     ID=3 CODE=1
COMPUTE NM HYD ID=4 HYD=104 DA=0.0261 SQ MI
                PER A=50 B=16.6 C=16.7 D=16.7
                TP=0.133333 HRS RAIN=-1
PRINT HYD     ID=4 CODE=1
COMPUTE NM HYD ID=5 HYD=105 DA=0.0031 SQ MI
                PER A=0 B=0 C=20 D=80
                TP=0.133333 HRS RAIN=-1
PRINT HYD     ID=5 CODE=1
COMPUTE NM HYD ID=6 HYD=106 DA=0.0020 SQ MI
                PER A=0 B=0 C=0 D=100
                TP=0.133333 HRS RAIN=-1
PRINT HYD     ID=6 CODE=1
ADD HYD       ID=7 HYD=200 IDS= 1 & 2
ADD HYD       ID=8 HYD=201 IDS= 7 & 3
ADD HYD       ID=9 HYD=202 IDS= 8 & 4
ADD HYD       ID=10 HYD=203 IDS= 9 & 5
ADD HYD      ID=11 HYD=204 IDS= 10 & 6
PRINT HYD    ID=11 CODE=1
ROUTE RESERVOIR ID=12 HYD=305 INFLOW ID=11 CODE=5
                  OUTFLOW (CFS)   STORAGE (AC FT)   ELEV (FT)
                  0             0.00           5000
                  7             0.01           5001
                  22            0.18           5002
                  46            0.59           5003
                  52.6          1.14           5004
                  55.4          1.90           5005
                  57.6          3.05           5006
PRINT HYD    ID=12 CODE=1
FINISH

```


~(s16.67h8.5v0T~&18D
AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4)
INPUT FILE = C:\Users\doug\Desktop\2014-10-17 10 yr final.txt

- Ver. S4.01a, Rel: 01a RUN DATE (MON/DAY/YR) =10/17/2014
USER NO.= AHYMO_Temp_User:20122010

AHYMO 10-TR Summary

| COMMAND | HYDROGRAPH IDENTIFICATION NO. | FROM ID NO. | TO ID NO. | AREA (SQ MI) | PEAK DISCHARGE (CFS) | RUNOFF VOLUME (AC-FT) | RUNOFF (INCHES) | TIME TO PEAK (HOURS) | CFS PER ACRE | PAGE = 1 NOTATION |
|------------------------|---|-------------|-----------|--------------|----------------------|-----------------------|-----------------|----------------------|-----------------------|----------------------|
| START *S | THE TEAM OFFICE BUILDING 10-YR, ALBUQUERQUE | | | | | | | | TIME= 0.00 | |
| RAINFALL LOCATION | TYPE= 1 NOAA 14 | | | | | | | | RAIN6= 1.470 | |
| COMPUTE NM HYD | 101.00 | - | 1 | 0.01330 | 18.02 | 0.509 | 0.71827 | 1.530 | 2.117 PER IMP= 24.00 | |
| COMPUTE NM HYD | 102.00 | - | 2 | 0.01620 | 12.59 | 0.384 | 0.44449 | 1.540 | 1.214 PER IMP= 16.70 | |
| COMPUTE NM HYD | 103.00 | - | 3 | 0.00340 | 2.65 | 0.081 | 0.44449 | 1.540 | 1.218 PER IMP= 16.70 | |
| COMPUTE NM HYD | 104.00 | - | 4 | 0.02610 | 20.28 | 0.619 | 0.44449 | 1.540 | 1.214 PER IMP= 16.70 | |
| COMPUTE NM HYD | 105.00 | - | 5 | 0.00310 | 5.53 | 0.182 | 1.10139 | 1.530 | 2.789 PER IMP= 80.00 | |
| COMPUTE NM HYD | 106.00 | - | 6 | 0.00200 | 3.88 | 0.132 | 1.23822 | 1.520 | 3.028 PER IMP= 100.00 | |
| ADD HYD | 200.00 | 1& 2 | 7 | 0.02950 | 30.59 | 0.893 | 0.56790 | 1.540 | 1.620 | |
| ADD HYD | 201.00 | 7& 3 | 8 | 0.03290 | 33.24 | 0.974 | 0.55514 | 1.540 | 1.579 | |
| ADD HYD | 202.00 | 8& 4 | 9 | 0.05900 | 53.52 | 1.593 | 0.50618 | 1.540 | 1.417 | |
| ADD HYD | 203.00 | 9& 5 | 10 | 0.06210 | 59.01 | 1.775 | 0.53589 | 1.540 | 1.485 | |
| ADD HYD | 204.00 | 10& 6 | 11 | 0.06410 | 62.85 | 1.907 | 0.55780 | 1.540 | 1.532 | |
| ROUTE RESERVOIR FINISH | 305.00 | 11 | 12 | 0.06410 | 40.41 | 1.907 | 0.55780 | 1.660 | 0.985 AC-FT= 0.494 | |

AHYMO PROGRAM (AHYMO-S4)
 RUN DATE (MON/DAY/YR) = 10/17/2014
 START TIME (HR:MIN:SEC) = 16:55:48
 INPUT FILE = C:\Users\dcoug\Desktop\2014-10-17 10 yr final.txt

START 0.0 HRS PUNCH CODE=0 PRINT LINES=--6
 *S THE TEAM OFFICE BUILDING 10-YR, 6-HR DEVELOPED CONDITIONS
 LOCATION ALBUQUERQUE
 City of Albuquerque soil infiltration values (LAND FACTORS) used for computations.
 Land Treatment Initial Abstr. (in) Unif. Infiltr. (in/hour)
 A 0.65 1.67
 B 0.50 1.25
 C 0.35 0.83
 D 0.10 0.04

RAINFALL TYPE=1 RAIN QUARTER=0.0 RAIN ONE=1.25
 RAIN SIX=1.47 RAIN DAY=1.77 DT=.01

6-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1
 DT = 0.010000 HOURS END TIME = 6.000000 HOURS
 0.0000 0.0003 0.0006 0.0009 0.0012 0.0015 0.0018
 0.0021 0.0023 0.0027 0.0030 0.0033 0.0036 0.0040
 0.0043 0.0046 0.0049 0.0053 0.0056 0.0060 0.0064
 0.0067 0.0071 0.0075 0.0078 0.0082 0.0086 0.0090
 0.0094 0.0099 0.0103 0.0107 0.0111 0.0115 0.0123
 0.0132 0.0140 0.0149 0.0158 0.0167 0.0176 0.0185
 0.0194 0.0204 0.0214 0.0224 0.0234 0.0244 0.0254
 0.0264 0.0274 0.0285 0.0296 0.0307 0.0318 0.0329
 0.0340 0.0351 0.0362 0.0374 0.0385 0.0397 0.0408
 0.0420 0.0431 0.0443 0.0454 0.0466 0.0478 0.0490
 0.0502 0.0514 0.0526 0.0539 0.0551 0.0563 0.0576
 0.0590 0.0604 0.0617 0.0631 0.0644 0.0658 0.0671
 0.0686 0.0702 0.0717 0.0732 0.0748 0.0763 0.0779
 0.0794 0.0817 0.0853 0.0889 0.0925 0.0961 0.0997
 0.1033 0.1070 0.1106 0.1154 0.1203 0.1251 0.1299
 0.1348 0.1396 0.1445 0.1493 0.1555 0.1622 0.1690
 0.1758 0.1826 0.1894 0.1961 0.2029 0.2108 0.2210
 0.2312 0.2414 0.2515 0.2617 0.2719 0.2821 0.2922
 0.3098 0.3274 0.3450 0.3625 0.3801 0.3977 0.4152
 0.4328 0.4699 0.5167 0.5635 0.6103 0.6571 0.7039
 0.7507 0.7975 0.8374 0.8633 0.8893 0.9152 0.9411
 0.9671 0.9930 1.0190 1.0449 1.0580 1.0710 1.0840
 1.0971 1.1101 1.1231 1.1362 1.1492 1.1590 1.1673
 1.1755 1.1837 1.1919 1.2001 1.2083 1.2165 1.2239
 1.2296 1.2353 1.2410 1.2467 1.2524 1.2580 1.2637
 1.2694 1.2736 1.2778 1.2819 1.2861 1.2903 1.2944
 1.2986 1.3028 1.3063 1.3094 1.3126 1.3157 1.3189
 1.3220 1.3252 1.3284 1.3309 1.3324 1.3338 1.3353

- Version: S4.01a - Rel: 01a

| | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|
| 1.3367 | 1.3382 | 1.3396 | 1.3410 | 1.3425 | 1.3438 | 1.3450 |
| 1.3463 | 1.3476 | 1.3489 | 1.3502 | 1.3514 | 1.3527 | 1.3539 |
| 1.3549 | 1.3559 | 1.3570 | 1.3580 | 1.3591 | 1.3601 | 1.3612 |
| 1.3622 | 1.3632 | 1.3641 | 1.3651 | 1.3661 | 1.3670 | 1.3680 |
| 1.3689 | 1.3699 | 1.3708 | 1.3718 | 1.3727 | 1.3736 | 1.3745 |
| 1.3755 | 1.3764 | 1.3773 | 1.3779 | 1.3784 | 1.3788 | 1.3793 |
| 1.3797 | 1.3801 | 1.3806 | 1.3810 | 1.3815 | 1.3819 | 1.3823 |
| 1.3828 | 1.3832 | 1.3836 | 1.3841 | 1.3845 | 1.3849 | 1.3853 |
| 1.3857 | 1.3861 | 1.3865 | 1.3869 | 1.3873 | 1.3877 | 1.3882 |
| 1.3885 | 1.3889 | 1.3893 | 1.3897 | 1.3901 | 1.3905 | 1.3909 |
| 1.3913 | 1.3917 | 1.3920 | 1.3924 | 1.3928 | 1.3932 | 1.3935 |
| 1.3939 | 1.3943 | 1.3947 | 1.3950 | 1.3954 | 1.3957 | 1.3961 |
| 1.3964 | 1.3968 | 1.3971 | 1.3975 | 1.3978 | 1.3982 | 1.3985 |
| 1.3989 | 1.3992 | 1.3996 | 1.3999 | 1.4003 | 1.4006 | 1.4009 |
| 1.4013 | 1.4016 | 1.4019 | 1.4023 | 1.4026 | 1.4029 | 1.4033 |
| 1.4036 | 1.4039 | 1.4042 | 1.4045 | 1.4049 | 1.4052 | 1.4055 |
| 1.4058 | 1.4061 | 1.4064 | 1.4067 | 1.4070 | 1.4073 | 1.4077 |
| 1.4080 | 1.4083 | 1.4086 | 1.4089 | 1.4092 | 1.4095 | 1.4098 |
| 1.4101 | 1.4104 | 1.4107 | 1.4110 | 1.4113 | 1.4116 | 1.4118 |
| 1.4121 | 1.4124 | 1.4127 | 1.4130 | 1.4133 | 1.4136 | 1.4138 |
| 1.4141 | 1.4144 | 1.4147 | 1.4150 | 1.4152 | 1.4155 | 1.4158 |
| 1.4161 | 1.4163 | 1.4166 | 1.4169 | 1.4172 | 1.4174 | 1.4177 |
| 1.4180 | 1.4183 | 1.4185 | 1.4188 | 1.4191 | 1.4193 | 1.4196 |
| 1.4199 | 1.4201 | 1.4204 | 1.4207 | 1.4209 | 1.4212 | 1.4214 |
| 1.4217 | 1.4220 | 1.4222 | 1.4225 | 1.4227 | 1.4230 | 1.4233 |
| 1.4235 | 1.4238 | 1.4240 | 1.4243 | 1.4245 | 1.4248 | 1.4250 |
| 1.4253 | 1.4255 | 1.4258 | 1.4261 | 1.4263 | 1.4266 | 1.4268 |
| 1.4270 | 1.4273 | 1.4275 | 1.4278 | 1.4280 | 1.4283 | 1.4285 |
| 1.4288 | 1.4290 | 1.4293 | 1.4295 | 1.4297 | 1.4300 | 1.4302 |
| 1.4305 | 1.4307 | 1.4309 | 1.4312 | 1.4314 | 1.4316 | 1.4319 |
| 1.4321 | 1.4324 | 1.4326 | 1.4328 | 1.4331 | 1.4333 | 1.4335 |
| 1.4338 | 1.4340 | 1.4342 | 1.4345 | 1.4347 | 1.4349 | 1.4351 |
| 1.4354 | 1.4356 | 1.4358 | 1.4361 | 1.4363 | 1.4365 | 1.4367 |
| 1.4370 | 1.4372 | 1.4374 | 1.4376 | 1.4379 | 1.4381 | 1.4383 |
| 1.4385 | 1.4387 | 1.4390 | 1.4392 | 1.4394 | 1.4396 | 1.4398 |
| 1.4401 | 1.4403 | 1.4405 | 1.4407 | 1.4409 | 1.4411 | 1.4414 |
| 1.4416 | 1.4418 | 1.4420 | 1.4422 | 1.4424 | 1.4426 | 1.4429 |
| 1.4431 | 1.4433 | 1.4435 | 1.4437 | 1.4439 | 1.4441 | 1.4443 |
| 1.4445 | 1.4448 | 1.4450 | 1.4452 | 1.4454 | 1.4456 | 1.4458 |
| 1.4460 | 1.4462 | 1.4464 | 1.4466 | 1.4468 | 1.4470 | 1.4472 |
| 1.4474 | 1.4476 | 1.4478 | 1.4480 | 1.4482 | 1.4484 | 1.4486 |
| 1.4488 | 1.4490 | 1.4492 | 1.4494 | 1.4496 | 1.4498 | 1.4500 |
| 1.4502 | 1.4504 | 1.4506 | 1.4508 | 1.4510 | 1.4512 | 1.4514 |
| 1.4516 | 1.4518 | 1.4520 | 1.4522 | 1.4524 | 1.4526 | 1.4528 |
| 1.4530 | 1.4532 | 1.4534 | 1.4535 | 1.4537 | 1.4539 | 1.4541 |
| 1.4543 | 1.4545 | 1.4547 | 1.4549 | 1.4551 | 1.4553 | 1.4554 |
| 1.4556 | 1.4558 | 1.4560 | 1.4562 | 1.4564 | 1.4566 | 1.4568 |
| 1.4569 | 1.4571 | 1.4573 | 1.4575 | 1.4577 | 1.4579 | 1.4580 |
| 1.4582 | 1.4584 | 1.4586 | 1.4588 | 1.4590 | 1.4591 | 1.4593 |
| 1.4595 | 1.4597 | 1.4599 | 1.4600 | 1.4602 | 1.4604 | 1.4606 |
| 1.4608 | 1.4609 | 1.4611 | 1.4613 | 1.4615 | 1.4617 | 1.4618 |

| | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|
| 1.4620 | 1.4622 | 1.4624 | 1.4625 | 1.4627 | 1.4629 | 1.4631 |
| 1.4632 | 1.4634 | 1.4636 | 1.4638 | 1.4639 | 1.4641 | 1.4643 |
| 1.4645 | 1.4646 | 1.4648 | 1.4650 | 1.4651 | 1.4653 | 1.4655 |
| 1.4657 | 1.4658 | 1.4660 | 1.4662 | 1.4663 | 1.4665 | 1.4667 |
| 1.4668 | 1.4670 | 1.4672 | 1.4673 | 1.4675 | 1.4677 | 1.4678 |
| 1.4680 | 1.4682 | 1.4683 | 1.4685 | 1.4687 | 1.4688 | 1.4690 |
| 1.4692 | 1.4693 | 1.4695 | 1.4697 | 1.4698 | 1.4700 | |

COMPUTE NM HYD ID=1 HYD=101 DA=0.0133 SQ MI
 PER A=0 B=0 C=76 D=24
 TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
 UNIT PEAK = 12.599 CFS UNIT VOLUME = 0.9990 B = 526.28 P60 = 1.2500
 AREA = 0.003192 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 101.00

RUNOFF VOLUME = 0.71827 INCHES = 0.5095 ACRE-FEET
 PEAK DISCHARGE RATE = 18.02 CFS AT 1.530 HOURS BASIN AREA = 0.0133 SQ. MI.

COMPUTE NM HYD ID=2 HYD=102 DA=0.0162 SQ MI
 PER A=50 B=16.6 C=16.7 D=16.7
 TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
 UNIT PEAK = 10.678 CFS UNIT VOLUME = 0.9988 B = 526.28 P60 = 1.2500
 AREA = 0.002705 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=2 CODE=1

PARTIAL HYDROGRAPH 102.00

| | | | |
|---|---------------------|-------------------------------|------------------------------|
| K = 0.157603HR | TP = 0.133333HR | K/TP RATIO = 1.182028 | SHAPE CONSTANT, N = 3.002506 |
| UNIT PEAK = 28.544 | CFS | UNIT VOLUME = 0.9995 | B = 282.03 |
| AREA = 0.013495 SQ MI | IA = 0.55996 INCHES | INF = 1.41790 INCHES PER HOUR | P60 = 1.2500 |
| RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000 | | | |

RUNOFF VOLUME = 0.44449 INCHES = 0.3840 ACRE-FEET
PEAK DISCHARGE RATE = 12.59 CFS AT 1.540 HOURS BASIN AREA = 0.0162 SQ. MI.

COMPUTE NM HYD ID=3 HYD=103 DA=0.0034 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 2.2412 CFS UNIT VOLUME = 0.9945 B = 526.28 P60 = 1.2500
AREA = 0.000568 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

RUNOFF VOLUME = 0.44449 INCHES = 0.0806 ACRE-FEET
PEAK DISCHARGE RATE = 2.65 CFS AT 1.540 HOURS BASIN AREA = 0.0034 SQ. MI.

PRINT HYD ID=3 CODE=1

PARTIAL HYDROGRAPH 103.00

COMPUTE NM HYD ID=4 HYD=104 DA=0.0261 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 17.204 CFS UNIT VOLUME = 0.9993 B = 526.28 P60 = 1.2500
AREA = 0.004359 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=4 CODE=1

PARTIAL HYDROGRAPH 104.00

RUNOFF VOLUME = 0.44449 INCHES = 0.6187 ACRE-FEET
PEAK DISCHARGE RATE = 20.28 CFS AT 1.540 HOURS BASIN AREA = 0.0261 SQ. MI.

COMPUTE NM HYD ID=5 HYD=105 DA=0.0031 SQ MI
PER A=0 B=0 C=20 D=80
TP=0.133333 HRS RAIN=-1

K = 0.072666HHR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 9.7887 CFS UNIT VOLUME = 0.9987 B = 526.28 P60 = 1.2500
AREA = 0.002480 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

K = 0.108042HHR TP = 0.133333HR K/TP RATIO = 0.810320 SHAPE CONSTANT, N = 4.414318
UNIT PEAK = 1.7759 CFS UNIT VOLUME = 0.9922 B = 381.91 P60 = 1.2500
AREA = 0.000620 SQ MI IA = 0.35000 INCHES INF = 0.83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=5 CODE=1

PARTIAL HYDROGRAPH 105.00

RUNOFF VOLUME = 1.10139 INCHES = 0.1821 ACRE-FEET
PEAK DISCHARGE RATE = 5.53 CFS AT 1.530 HOURS BASIN AREA = 0.0031 SQ. MI.

COMPUTE NM HYD ID=6 HYD=106 DA=0.0020 SQ MI
PER A=0 B=0 C=0 D=100
TP=0.133333 HRS RAIN=-1

K = 0.072666HHR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 7.8942 CFS UNIT VOLUME = 0.9984 B = 526.28 P60 = 1.2500
AREA = 0.002000 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=6 CODE=1

PARTIAL HYDROGRAPH 106.00

RUNOFF VOLUME = 1.23822 INCHES = 0.1321 ACRE-FEET
PEAK DISCHARGE RATE = 3.88 CFS AT 1.520 HOURS BASIN AREA = 0.0020 SQ. MI.

ADD HYD ID=7 HYD=200 IDS= 1 & 2

ADD HYD
 ADD HYD
 ADD HYD
 ADD HYD
 ADD HYD
 PRINT HYD

ID=8 HYD=201 IDS= 7 & 3
 ID=9 HYD=202 IDS= 8 & 4
 ID=10 HYD=203 IDS= 9 & 5
 ID=11 HYD=204 IDS= 10 & 6
 ID=11 CODE=1

PARTIAL HYDROGRAPH 204.00

RUNOFF VOLUME = 0.55780 INCHES = 1.9069 ACRE-FEET
 PEAK DISCHARGE RATE = 62.85 CFS AT 1.540 HOURS BASIN AREA = 0.0641 SQ. MI.

| ROUTE RESERVOIR | ID=12 HYD=305 INFLOW | ID=11 CODE=5 | STORAGE (AC FT) | ELEV (FT) |
|-----------------|----------------------|--------------|-----------------|---------------|
| TIME (HRS) | INFLOW (CFS) | ELEV (FEET) | VOLUME (AC-FT) | OUTFLOW (CFS) |
| 0.00 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.05 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.10 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.15 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.20 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.25 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.30 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.35 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.40 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.45 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.50 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.55 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.60 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.65 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.70 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.75 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.80 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.85 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.90 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 0.95 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 1.00 | 0.00 | 5000.00 | 0.000 | 0.00 |
| 1.05 | 0.25 | 5000.02 | 0.000 | 0.13 |

| TIME (HRS) | INFLOW (CFS) | ELEV (FEET) | VOLUME (AC-FT) | OUTFLOW (CFS) |
|---------------|-----------------|----------------|-------------------|------------------|
| 1.10 | 5000.13 | 0.001 | 0.89 | |
| 1.27 | 5000.30 | 0.003 | 2.12 | |
| 1.15 | 5000.48 | 0.005 | 3.35 | |
| 1.20 | 5000.65 | 0.007 | 4.55 | |
| 1.25 | 5000.86 | 0.009 | 5.99 | |
| 1.30 | 5001.02 | 0.013 | 7.23 | |
| 1.35 | 5001.13 | 0.032 | 8.92 | |
| 1.40 | 5001.53 | 0.100 | 14.92 | |
| 1.45 | 5002.11 | 0.224 | 24.58 | |
| 1.50 | 5002.44 | 0.361 | 32.58 | |
| 1.55 | 5002.62 | 0.434 | 36.86 | |
| 1.60 | 5002.68 | 0.457 | 38.23 | |
| 1.65 | 5002.77 | 0.494 | 40.37 | |
| 1.70 | 5002.73 | 0.480 | 39.54 | |
| 1.75 | 5002.62 | 0.434 | 36.86 | |
| 1.80 | 5002.47 | 0.373 | 33.30 | |
| 1.85 | 5002.31 | 0.308 | 29.50 | |
| 1.90 | 5002.16 | 0.245 | 25.80 | |
| 1.95 | 5002.02 | 0.186 | 22.38 | |
| 2.00 | 5001.75 | 0.137 | 18.17 | |
| 2.05 | 5001.51 | 0.097 | 14.69 | |
| 2.10 | 5001.33 | 0.065 | 11.89 | |
| 2.15 | 5001.18 | 0.040 | 9.66 | |
| 2.20 | 5001.06 | 0.020 | 7.90 | |
| 2.25 | 5000.63 | 0.006 | 4.44 | |
| 2.30 | 5000.42 | 0.004 | 2.91 | |
| 2.35 | 5000.36 | 0.004 | 2.49 | |
| 2.40 | 5000.31 | 0.003 | 2.18 | |
| 2.45 | 5000.27 | 0.003 | 1.87 | |
| 2.50 | 5000.22 | 0.002 | 1.53 | |
| 2.55 | 5000.18 | 0.002 | 1.26 | |
| 2.60 | 5000.15 | 0.001 | 1.05 | |
| 2.65 | 5000.13 | 0.001 | 0.89 | |
| 2.70 | 5000.11 | 0.001 | 0.76 | |
| 2.75 | 5000.09 | 0.001 | 0.65 | |
| 2.80 | 5000.08 | 0.001 | 0.56 | |
| 2.85 | 5000.07 | 0.001 | 0.48 | |
| 2.90 | 5000.06 | 0.001 | 0.42 | |
| 2.95 | 5000.05 | 0.001 | 0.36 | |
| 3.00 | 5000.05 | 0.000 | 0.32 | |
| 3.05 | 5000.04 | 0.000 | 0.28 | |
| 3.10 | 5000.04 | 0.000 | 0.25 | |
| 3.15 | 5000.03 | 0.000 | 0.22 | |
| 3.20 | 5000.03 | 0.000 | 0.19 | |
| 3.25 | 5000.02 | 0.000 | 0.17 | |
| 3.30 | 5000.02 | 0.000 | 0.15 | |
| 3.35 | 5000.02 | 0.000 | 0.14 | |
| 3.40 | 5000.02 | 0.000 | 0.12 | |

| TIME (HRS) | INFLOW (CFS) | ELEV (FEET) | VOLUME (AC-FT) | OUTFLOW (CFS) |
|---------------|-----------------|----------------|-------------------|------------------|
| 3.45 | 5000.02 | 0.000 | 0.11 | |
| 3.50 | 0.09 | 5000.01 | 0.000 | 0.10 |
| 3.55 | 0.08 | 5000.01 | 0.000 | 0.09 |
| 3.60 | 0.07 | 5000.01 | 0.000 | 0.08 |
| 3.65 | 0.06 | 5000.01 | 0.000 | 0.07 |
| 3.70 | 0.06 | 5000.01 | 0.000 | 0.06 |
| 3.75 | 0.05 | 5000.01 | 0.000 | 0.05 |
| 3.80 | 0.04 | 5000.01 | 0.000 | 0.05 |
| 3.85 | 0.04 | 5000.01 | 0.000 | 0.04 |
| 3.90 | 0.04 | 5000.01 | 0.000 | 0.04 |
| 3.95 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.00 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.05 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.10 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.15 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.20 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.25 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.30 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.35 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.40 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.45 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.50 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.55 | 0.02 | 5000.00 | 0.000 | 0.02 |
| 4.60 | 0.02 | 5000.00 | 0.000 | 0.02 |
| 4.65 | 0.02 | 5000.00 | 0.000 | 0.02 |
| 4.70 | 0.02 | 5000.00 | 0.000 | 0.02 |
| 4.75 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.80 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.85 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.90 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 4.95 | 0.04 | 5000.01 | 0.000 | 0.04 |
| 5.00 | 0.04 | 5000.01 | 0.000 | 0.04 |
| 5.05 | 0.05 | 5000.01 | 0.000 | 0.05 |
| 5.10 | 0.06 | 5000.01 | 0.000 | 0.05 |
| 5.15 | 0.06 | 5000.01 | 0.000 | 0.06 |
| 5.20 | 0.06 | 5000.01 | 0.000 | 0.06 |
| 5.25 | 0.07 | 5000.01 | 0.000 | 0.07 |
| 5.30 | 0.07 | 5000.01 | 0.000 | 0.07 |
| 5.35 | 0.08 | 5000.01 | 0.000 | 0.08 |
| 5.40 | 0.08 | 5000.01 | 0.000 | 0.08 |
| 5.45 | 0.09 | 5000.01 | 0.000 | 0.08 |
| 5.50 | 0.09 | 5000.01 | 0.000 | 0.09 |
| 5.55 | 0.10 | 5000.01 | 0.000 | 0.09 |
| 5.60 | 0.10 | 5000.01 | 0.000 | 0.10 |
| 5.65 | 0.11 | 5000.02 | 0.000 | 0.11 |
| 5.70 | 0.11 | 5000.02 | 0.000 | 0.11 |
| 5.75 | 0.12 | 5000.02 | 0.000 | 0.12 |

| | | | | |
|------|------|---------|-------|------|
| 5.80 | 0.12 | 5000.02 | 0.000 | 0.12 |
| 5.85 | 0.13 | 5000.02 | 0.000 | 0.13 |
| 5.90 | 0.13 | 5000.02 | 0.000 | 0.13 |
| 5.95 | 0.14 | 5000.02 | 0.000 | 0.13 |
| 6.00 | 0.14 | 5000.02 | 0.000 | 0.14 |
| 6.05 | 0.15 | 5000.02 | 0.000 | 0.15 |
| 6.10 | 0.13 | 5000.02 | 0.000 | 0.14 |
| 6.15 | 0.08 | 5000.01 | 0.000 | 0.10 |
| 6.20 | 0.05 | 5000.01 | 0.000 | 0.06 |
| 6.25 | 0.03 | 5000.00 | 0.000 | 0.03 |
| 6.30 | 0.02 | 5000.00 | 0.000 | 0.02 |
| 6.35 | 0.01 | 5000.00 | 0.000 | 0.02 |
| 6.40 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 6.45 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 6.50 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 6.55 | 0.00 | 5000.00 | 0.000 | 0.01 |
| 6.60 | 0.00 | 5000.00 | 0.000 | 0.00 |

PEAK DISCHARGE = 40.408 CFS - PEAK OCCURS AT HOUR 1.66
 MAXIMUM WATER SURFACE ELEVATION = 5002.767
 MAXIMUM STORAGE = 0.4945 AC-FT INCREMENTAL TIME= 0.010000HRS

PRINT HYD ID=12 CODE=1

HYDROGRAPH FROM AREA 305.00

RUNOFF VOLUME = 0.55780 INCHES = 1.9069 ACRE-FEET
 PEAK DISCHARGE RATE = 40.41 CFS AT 1.660 HOURS BASIN AREA = 0.0641 SQ. MI.

FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 16:55:48

← (50p10h4099T+&16D

AHYMO 2 YR Input

2014-10-17 2 yr final

START 0.0 HRS PUNCH CODE=0 PRINT LINES=-6
*S THE TEAM OFFICE BUILDING 2-YR, 6-HR DEVELOPED CONDITIONS
LOCATION ALBUQUERQUE
RAINFALL TYPE=1 RAIN QUARTER=0.0 RAIN ONE=0.81
RAIN SIX=0.95 RAIN DAY=1.15 DT=.01
COMPUTE NM HYD ID=1 HYD=101 DA=0.0133 SQ MI
PER A=0 B=0 C=76 D=24
TP=0.133333 HRS RAIN=-1
PRINT HYD ID=1 CODE=1
COMPUTE NM HYD ID=2 HYD=102 DA=0.0162 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1
PRINT HYD ID=2 CODE=1
COMPUTE NM HYD ID=3 HYD=103 DA=0.0034 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1
PRINT HYD ID=3 CODE=1
COMPUTE NM HYD ID=4 HYD=104 DA=0.0261 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1
PRINT HYD ID=4 CODE=1
COMPUTE NM HYD ID=5 HYD=105 DA=0.0031 SQ MI
PER A=0 B=0 C=20 D=80
TP=0.133333 HRS RAIN=-1
PRINT HYD ID=5 CODE=1
COMPUTE NM HYD ID=6 HYD=106 DA=0.0020 SQ MI
PER A=0 B=0 C=0 D=100
TP=0.133333 HRS RAIN=-1
PRINT HYD ID=6 CODE=1
ADD HYD ID=7 HYD=200 IDS= 1 & 2
ADD HYD ID=8 HYD=201 IDS= 7 & 3
ADD HYD ID=9 HYD=202 IDS= 8 & 4
ADD HYD ID=10 HYD=203 IDS= 9 & 5
ADD HYD ID=11 HYD=204 IDS= 10 & 6
PRINT HYD ID=11 CODE=1
ROUTE RESERVOIR ID=12 HYD=305 INFLOW ID=11 CODE=5
OUTFLOW (CFS) STORAGE (AC FT) ELEV (FT)
0 0.00 5000
7 0.01 5001
22 0.18 5002
46 0.59 5003
52.6 1.14 5004
55.4 1.90 5005
57.6 3.05 5006
PRINT HYD ID=12 CODE=1
FINISH

~(s16.67h8.5v0T~&18D
AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4)
INPUT FILE = C:\Users\doug\Desktop\2014-10-17 2 yr final.txt

- Ver. S4.01a, Rel: 01a

RUN DATE (MON/DAY/YR) =10/17/2014
USER NO. = AHYMO_Temp_User:20122010

| COMMAND | HYDROGRAPH IDENTIFICATION NO. | FROM ID NO. | TO ID NO. | AREA (SQ MI) | PEAK DISCHARGE (CFS) | RUNOFF VOLUME (AC-FT) | RUNOFF (INCHES) | TIME TO PEAK (HOURS) | CFS PER ACRE | PAGE = 1 |
|-----------------|--|-------------|-----------|--------------|----------------------|-----------------------|-----------------|----------------------|----------------|----------|
| START | | | | | | | | | | NOTATION |
| *S | THE TEAM OFFICE BUILDING 2-YR, 6-HR DEVELOPED CONDITIONS | | | | | | | | | |
| LOCATION | RAINFALL TYPE= 1 NOAA 14 | | | | | | | | | |
| COMPUTE NM HYD | 101.00 | - | 1 | 0.01330 | 8.89 | 0.239 | 0.33685 | 1.540 | 1.044 PER IMP= | 24.00 |
| COMPUTE NM HYD | 102.00 | - | 2 | 0.01620 | 3.72 | 0.121 | 0.13993 | 1.540 | 0.359 PER IMP= | 16.70 |
| COMPUTE NM HYD | 103.00 | - | 3 | 0.00340 | 0.78 | 0.025 | 0.13993 | 1.540 | 0.361 PER IMP= | 16.70 |
| COMPUTE NM HYD | 104.00 | - | 4 | 0.02610 | 6.00 | 0.195 | 0.13993 | 1.540 | 0.359 PER IMP= | 16.70 |
| COMPUTE NM HYD | 105.00 | - | 5 | 0.00310 | 3.38 | 0.106 | 0.63910 | 1.530 | 1.703 PER IMP= | 80.00 |
| COMPUTE NM HYD | 106.00 | - | 6 | 0.00200 | 2.48 | 0.080 | 0.74705 | 1.520 | 1.940 PER IMP= | 100.00 |
| ADD HYD | 200.00 | 1& 2 | 7 | 0.02950 | 12.61 | 0.360 | 0.22869 | 1.540 | 0.668 | |
| ADD HYD | 201.00 | 7& 3 | 8 | 0.03290 | 13.40 | 0.385 | 0.21951 | 1.540 | 0.636 | |
| ADD HYD | 202.00 | 8& 4 | 9 | 0.05900 | 19.39 | 0.580 | 0.18430 | 1.540 | 0.514 | |
| ADD HYD | 203.00 | 9& 5 | 10 | 0.06210 | 22.75 | 0.686 | 0.20700 | 1.540 | 0.572 | |
| ADD HYD | 204.00 | 10& 6 | 11 | 0.06410 | 25.21 | 0.765 | 0.22385 | 1.540 | 0.615 | |
| ROUTE RESERVOIR | 305.00 | 11 | 12 | 0.06410 | 18.65 | 0.765 | 0.22385 | 1.630 | 0.455 AC-FT= | 0.142 |
| FINISH | | | | | | | | | | |

~(s0p10h4099T~&16D

AHYMO 2-YR Summary

~ (s16.67h8.5v0t~&18D

AHYMO PROGRAM (AHYMO-S4)
RUN DATE (MON/DAY/YR) = 10/17/2014
START TIME (HR:MIN:SEC) = 16:58:35
USER NO.= AHYMO_Temp_User:20122010
INPUT FILE = C:\Users\doug\Desktop\2014-10-17 2 yr final.txt

Version: S4.01a - Rel: 01a

START 0.0 HRS PUNCH CODE=0 PRINT LINES=-6
*S THE TEAM OFFICE BUILDING 2-YR, 6-HR DEVELOPED CONDITIONS
LOCATION ALBUQUERQUE

City of Albuquerque soil infiltration values (LAND FACTORS) used for computations.

| Land Treatment | Initial Abstr. (in) | Unif. Infiltr. (in/hour) |
|----------------|---------------------|--------------------------|
| A | 0.65 | 1.67 |
| B | 0.50 | 1.25 |
| C | 0.35 | 0.83 |
| D | 0.10 | 0.04 |

RAINFALL TYPE=1 RAIN QUARTER=0.0 RAIN ONE=0.81
RAIN SIX=0.95 RAIN DAY=1.15 DT=.01

6-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1
DT = 0.010000 HOURS END TIME = 6.000000 HOURS

| DT | Rainfall (in) | Time (hrs) |
|--------|---------------|------------|
| 0.0000 | 0.0002 | 0.0004 |
| 0.0013 | 0.0015 | 0.0017 |
| 0.0027 | 0.0029 | 0.0031 |
| 0.0043 | 0.0045 | 0.0048 |
| 0.0060 | 0.0063 | 0.0065 |
| 0.0084 | 0.0089 | 0.0095 |
| 0.0124 | 0.0130 | 0.0136 |
| 0.0168 | 0.0175 | 0.0182 |
| 0.0216 | 0.0223 | 0.0230 |
| 0.0267 | 0.0274 | 0.0282 |
| 0.0320 | 0.0327 | 0.0335 |
| 0.0375 | 0.0384 | 0.0393 |
| 0.0437 | 0.0446 | 0.0456 |
| 0.0505 | 0.0520 | 0.0543 |
| 0.0660 | 0.0684 | 0.0707 |
| 0.0864 | 0.0896 | 0.0927 |
| 0.1130 | 0.1174 | 0.1218 |
| 0.1489 | 0.1555 | 0.1621 |
| 0.1998 | 0.2112 | 0.2226 |
| 0.2795 | 0.3035 | 0.3339 |
| 0.4855 | 0.5159 | 0.5417 |
| 0.6257 | 0.6426 | 0.6594 |
| 0.7100 | 0.7184 | 0.7269 |
| 0.7608 | 0.7661 | 0.7714 |
| 0.7958 | 0.7995 | 0.8032 |
| 0.8217 | 0.8244 | 0.8271 |
| 0.8406 | 0.8433 | 0.8455 |
| 0.8557 | 0.8578 | 0.8598 |

AHYMO ZYR Output

| | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|
| 0.8652 | 0.8661 | 0.8670 | 0.8679 | 0.8689 | 0.8697 | 0.8705 |
| 0.8713 | 0.8721 | 0.8729 | 0.8738 | 0.8746 | 0.8754 | 0.8761 |
| 0.8768 | 0.8774 | 0.8781 | 0.8788 | 0.8794 | 0.8801 | 0.8808 |
| 0.8814 | 0.8820 | 0.8826 | 0.8832 | 0.8839 | 0.8845 | 0.8851 |
| 0.8857 | 0.8863 | 0.8869 | 0.8875 | 0.8881 | 0.8887 | 0.8892 |
| 0.8898 | 0.8904 | 0.8910 | 0.8914 | 0.8917 | 0.8920 | 0.8923 |
| 0.8925 | 0.8928 | 0.8931 | 0.8934 | 0.8937 | 0.8940 | 0.8942 |
| 0.8945 | 0.8948 | 0.8950 | 0.8953 | 0.8956 | 0.8959 | 0.8961 |
| 0.8964 | 0.8966 | 0.8969 | 0.8972 | 0.8974 | 0.8977 | 0.8979 |
| 0.8982 | 0.8984 | 0.8987 | 0.8989 | 0.8992 | 0.8994 | 0.8997 |
| 0.8999 | 0.9001 | 0.9004 | 0.9006 | 0.9009 | 0.9011 | 0.9013 |
| 0.9016 | 0.9018 | 0.9021 | 0.9023 | 0.9025 | 0.9027 | 0.9030 |
| 0.9032 | 0.9034 | 0.9036 | 0.9039 | 0.9041 | 0.9043 | 0.9045 |
| 0.9047 | 0.9050 | 0.9052 | 0.9054 | 0.9056 | 0.9058 | 0.9061 |
| 0.9063 | 0.9065 | 0.9067 | 0.9069 | 0.9071 | 0.9073 | 0.9075 |
| 0.9077 | 0.9079 | 0.9081 | 0.9083 | 0.9086 | 0.9088 | 0.9090 |
| 0.9092 | 0.9094 | 0.9095 | 0.9097 | 0.9099 | 0.9101 | 0.9103 |
| 0.9105 | 0.9107 | 0.9109 | 0.9111 | 0.9113 | 0.9115 | 0.9117 |
| 0.9119 | 0.9121 | 0.9123 | 0.9125 | 0.9126 | 0.9128 | 0.9130 |
| 0.9132 | 0.9134 | 0.9135 | 0.9137 | 0.9139 | 0.9141 | 0.9143 |
| 0.9145 | 0.9146 | 0.9148 | 0.9150 | 0.9152 | 0.9153 | 0.9155 |
| 0.9157 | 0.9159 | 0.9160 | 0.9162 | 0.9164 | 0.9166 | 0.9167 |
| 0.9169 | 0.9171 | 0.9173 | 0.9174 | 0.9176 | 0.9178 | 0.9179 |
| 0.9181 | 0.9183 | 0.9184 | 0.9186 | 0.9188 | 0.9189 | 0.9191 |
| 0.9193 | 0.9194 | 0.9196 | 0.9198 | 0.9199 | 0.9201 | 0.9203 |
| 0.9204 | 0.9206 | 0.9208 | 0.9209 | 0.9211 | 0.9212 | 0.9214 |
| 0.9216 | 0.9217 | 0.9219 | 0.9220 | 0.9222 | 0.9224 | 0.9225 |
| 0.9227 | 0.9228 | 0.9230 | 0.9231 | 0.9233 | 0.9235 | 0.9236 |
| 0.9238 | 0.9239 | 0.9241 | 0.9242 | 0.9244 | 0.9245 | 0.9247 |
| 0.9248 | 0.9250 | 0.9252 | 0.9253 | 0.9255 | 0.9256 | 0.9258 |
| 0.9259 | 0.9261 | 0.9262 | 0.9264 | 0.9265 | 0.9267 | 0.9268 |
| 0.9269 | 0.9271 | 0.9272 | 0.9274 | 0.9275 | 0.9277 | 0.9278 |
| 0.9280 | 0.9281 | 0.9283 | 0.9284 | 0.9286 | 0.9287 | 0.9288 |
| 0.9290 | 0.9291 | 0.9293 | 0.9294 | 0.9296 | 0.9297 | 0.9298 |
| 0.9300 | 0.9301 | 0.9303 | 0.9304 | 0.9305 | 0.9307 | 0.9308 |
| 0.9310 | 0.9311 | 0.9312 | 0.9314 | 0.9315 | 0.9316 | 0.9318 |
| 0.9319 | 0.9321 | 0.9322 | 0.9323 | 0.9325 | 0.9326 | 0.9327 |
| 0.9329 | 0.9330 | 0.9331 | 0.9333 | 0.9334 | 0.9335 | 0.9337 |
| 0.9338 | 0.9339 | 0.9341 | 0.9342 | 0.9343 | 0.9345 | 0.9346 |
| 0.9347 | 0.9349 | 0.9350 | 0.9351 | 0.9353 | 0.9354 | 0.9355 |
| 0.9356 | 0.9358 | 0.9359 | 0.9360 | 0.9362 | 0.9363 | 0.9364 |
| 0.9365 | 0.9367 | 0.9368 | 0.9369 | 0.9370 | 0.9372 | 0.9373 |
| 0.9374 | 0.9376 | 0.9377 | 0.9378 | 0.9379 | 0.9381 | 0.9382 |
| 0.9409 | 0.9410 | 0.9411 | 0.9412 | 0.9413 | 0.9415 | 0.9416 |
| 0.9417 | 0.9418 | 0.9419 | 0.9420 | 0.9422 | 0.9423 | 0.9424 |
| 0.9425 | 0.9426 | 0.9427 | 0.9429 | 0.9430 | 0.9431 | 0.9432 |
| 0.9433 | 0.9434 | 0.9436 | 0.9437 | 0.9438 | 0.9440 | 0.9441 |
| 0.9441 | 0.9442 | 0.9444 | 0.9445 | 0.9446 | 0.9447 | 0.9448 |

| | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|
| 0.9449 | 0.9450 | 0.9451 | 0.9453 | 0.9454 | 0.9455 | 0.9456 |
| 0.9457 | 0.9458 | 0.9459 | 0.9460 | 0.9461 | 0.9463 | 0.9464 |
| 0.9465 | 0.9466 | 0.9467 | 0.9468 | 0.9469 | 0.9470 | 0.9471 |
| 0.9472 | 0.9473 | 0.9475 | 0.9476 | 0.9477 | 0.9478 | 0.9479 |
| 0.9480 | 0.9481 | 0.9482 | 0.9483 | 0.9484 | 0.9485 | 0.9486 |
| 0.9487 | 0.9488 | 0.9489 | 0.9491 | 0.9492 | 0.9493 | 0.9494 |
| 0.9495 | 0.9496 | 0.9497 | 0.9498 | 0.9499 | 0.9500 | |

COMPUTE NM HYD ID=1 HYD=101 DA=0.0133 SQ MI
 PER A=0 B=0 C=76 D=24
 TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
 UNIT PEAK = 12.599 CFS UNIT VOLUME = 0.9990 B = 526.28 P60 = .81000
 AREA = 0.003192 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 101.00

RUNOFF VOLUME = 0.33685 INCHES = 0.2389 ACRE-FEET
 PEAK DISCHARGE RATE = 8.89 CFS AT 1.540 HOURS BASIN AREA = 0.0133 SQ. MI.

COMPUTE NM HYD ID=2 HYD=102 DA=0.0162 SQ MI
 PER A=50 B=16.6 C=16.7 D=16.7
 TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
 UNIT PEAK = 10.678 CFS UNIT VOLUME = 0.9988 B = 526.28 P60 = .81000
 AREA = 0.002705 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=2 CODE=1

PARTIAL HYDROGRAPH 102.00

K = 0.160412HR TP = 0.133333HR K/TP RATIO = 1.203095 SHAPE CONSTANT, N = 2.954084
 UNIT PEAK = 28.143 CFS UNIT VOLUME = 0.9995 B = 278.06 P60 = .81000
 AREA = 0.013495 SQ MI IA = 0.55996 INCHES INF = 1.41790 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

RUNOFF VOLUME = 0.13993 INCHES = 0.1209 ACRE-FEET
PEAK DISCHARGE RATE = 3.72 CFS AT 1.540 HOURS BASIN AREA = 0.0162 SQ. MI.

COMPUTE NM HYD ID=3 HYD=103 DA=0.0034 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1

K = 0.072666HHR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 2.2412 CFS UNIT VOLUME = 0.9945 B = 526.28 P60 = .81000
AREA = 0.000568 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=3 CODE=1

PARTIAL HYDROGRAPH 103.00

RUNOFF VOLUME = 0.13993 INCHES = 0.0254 ACRE-FEET
PEAK DISCHARGE RATE = 0.78 CFS AT 1.540 HOURS BASIN AREA = 0.0034 SQ. MI.

COMPUTE NM HYD ID=4 HYD=104 DA=0.0261 SQ MI
PER A=50 B=16.6 C=16.7 D=16.7
TP=0.133333 HRS RAIN=-1

K = 0.072666HHR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 17.204 CFS UNIT VOLUME = 0.9993 B = 526.28 P60 = .81000
AREA = 0.004359 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=4 CODE=1

PARTIAL HYDROGRAPH 104.00

RUNOFF VOLUME = 0.13993 INCHES = 0.1948 ACRE-FEET
PEAK DISCHARGE RATE = 6.00 CFS AT 1.540 HOURS BASIN AREA = 0.0261 SQ. MI.

COMPUTE NM HYD ID=5 HYD=105 DA=0.0031 SQ MI
PER A=0 B=0 C=20 D=80
TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 9.7887 CFS UNIT VOLUME = 0.9987 B = 526.28 P60 = .81000
AREA = 0.002480 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

K = 0.112435HR TP = 0.133333HR K/TP RATIO = 0.843267 SHAPE CONSTANT, N = 4.224349
UNIT PEAK = 1.7199 CFS UNIT VOLUME = 0.9917 B = 369.86 P60 = .81000
AREA = 0.0006620 SQ MI IA = 0.35000 INCHES INF = 0.83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=5 CODE=1

PARTIAL HYDROGRAPH 105.00

RUNOFF VOLUME = 0.63910 INCHES = 0.1057 ACRE-FEET
PEAK DISCHARGE RATE = 3.38 CFS AT 1.530 HOURS BASIN AREA = 0.0031 SQ. MI.

COMPUTE NM HYD ID=6 HYD=106 DA=0.0020 SQ MI
PER A=0 B=0 C=0 D=100
TP=0.133333 HRS RAIN=-1

K = 0.072666HR TP = 0.133333HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 7.8942 CFS UNIT VOLUME = 0.9984 B = 526.28 P60 = .81000
AREA = 0.002000 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.010000

PRINT HYD ID=6 CODE=1

PARTIAL HYDROGRAPH 106.00

RUNOFF VOLUME = 0.74705 INCHES = 0.0797 ACRE-FEET
PEAK DISCHARGE RATE = 2.48 CFS AT 1.520 HOURS BASIN AREA = 0.0020 SQ. MI.

ADD HYD ID=7 HYD=200 IDS= 1 & 2

ADD HYD ID=8 HYD=201 IDS= 7 & 3
 ADD HYD ID=9 HYD=202 IDS= 8 & 4
 ADD HYD ID=10 HYD=203 IDS= 9 & 5
 ADD HYD ID=11 HYD=204 IDS= 10 & 6
 PRINT HYD ID=11 CODE=1

PARTIAL HYDROGRAPH 204.00

RUNOFF VOLUME = 0.22385 INCHES = 0.7652 ACRE-FEET
 PEAK DISCHARGE RATE = 25.21 CFS AT 1.540 HOURS BASIN AREA = 0.0641 SQ. MI.

| ROUTE RESERVOIR | | ID=12 HYD=305 INFLOW | ID=11 CODE=5 | STORAGE (AC FT) | ELEV (FT) |
|-----------------|--------------|----------------------|----------------|-----------------|-----------|
| | | OUTFLOW (CFS) | | 0.00 | 5000 |
| TIME (HRS) | INFLOW (CFS) | ELEV (FEET) | VOLUME (AC-FT) | OUTFLOW (CFS) | |
| 0.00 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.05 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.10 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.15 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.20 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.25 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.30 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.35 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.40 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.45 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.50 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.55 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.60 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.65 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.70 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.75 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.80 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.85 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.90 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 0.95 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 1.00 | 0.00 | 5000.00 | 0.000 | 0.00 | |
| 1.05 | 0.00 | 5000.00 | 0.000 | 0.00 | |

| TIME (HRS) | INFLOW (CFS) | ELEV (FEET) | VOLUME (AC-FT) | OUTFLOW (CFS) |
|---------------|-----------------|----------------|-------------------|------------------|
| 0.00 | 5000.00 | 0.00 | 0.000 | 0.00 |
| 0.05 | 5000.01 | 0.00 | 0.000 | 0.04 |
| 0.10 | 5000.08 | 0.001 | 0.001 | 0.55 |
| 0.15 | 5000.45 | 0.005 | 0.002 | 1.74 |
| 0.20 | 5000.68 | 0.007 | 0.002 | 3.16 |
| 0.25 | 5001.00 | 0.010 | 0.005 | 4.74 |
| 0.30 | 5001.75 | 0.013 | 0.007 | 7.02 |
| 0.35 | 5001.41 | 0.010 | 0.010 | 8.51 |
| 0.40 | 5001.28 | 0.014 | 0.012 | 12.08 |
| 0.45 | 5001.77 | 0.014 | 0.012 | 15.96 |
| 0.50 | 5001.68 | 0.012 | 0.012 | 18.28 |
| 0.55 | 5001.55 | 0.010 | 0.010 | 13.15 |
| 0.60 | 5001.41 | 0.008 | 0.008 | 18.53 |
| 0.65 | 5001.28 | 0.007 | 0.007 | 17.26 |
| 0.70 | 5001.16 | 0.007 | 0.007 | 7.84 |
| 0.75 | 5001.06 | 0.002 | 0.002 | 15.28 |
| 0.80 | 5000.67 | 0.007 | 0.007 | 4.66 |
| 0.85 | 5000.41 | 0.004 | 0.004 | 2.89 |
| 0.90 | 5000.31 | 0.003 | 0.003 | 9.36 |
| 0.95 | 5000.25 | 0.002 | 0.002 | 7.84 |
| 1.00 | 5000.20 | 0.002 | 0.002 | 1.41 |
| 1.05 | 5000.17 | 0.002 | 0.002 | 1.16 |
| 1.10 | 5000.14 | 0.001 | 0.001 | 0.97 |
| 1.15 | 5000.12 | 0.001 | 0.001 | 1.74 |
| 1.20 | 5000.10 | 0.001 | 0.001 | 0.68 |
| 1.25 | 5000.08 | 0.001 | 0.001 | 0.56 |
| 1.30 | 5000.06 | 0.001 | 0.001 | 0.43 |
| 1.35 | 5000.05 | 0.000 | 0.000 | 0.33 |
| 1.40 | 5000.04 | 0.000 | 0.000 | 0.26 |
| 1.45 | 5000.03 | 0.000 | 0.000 | 0.21 |
| 1.50 | 5000.02 | 0.000 | 0.000 | 0.17 |
| 1.55 | 5000.02 | 0.000 | 0.000 | 0.14 |
| 1.60 | 5000.02 | 0.000 | 0.000 | 0.02 |
| 1.65 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 1.70 | 5000.00 | 0.000 | 0.000 | 0.03 |
| 1.75 | 5000.00 | 0.000 | 0.000 | 0.03 |
| 1.80 | 5000.00 | 0.000 | 0.000 | 0.03 |
| 1.85 | 5000.00 | 0.000 | 0.000 | 0.02 |
| 1.90 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 1.95 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.00 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.05 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.10 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.15 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.20 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.25 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.30 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.35 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.40 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.45 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.50 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.55 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.60 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.65 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.70 | 5000.00 | 0.000 | 0.000 | 0.01 |
| 2.75 | 5000.00 | 0.000 | 0.000 | 0.01 |

| | | | | |
|-----------------------------------|----------------------------------|-------------------|-------------|------|
| 3.45 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 3.50 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 3.55 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 3.60 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 3.65 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 3.70 | 0.01 | 5000.00 | 0.000 | 0.01 |
| 3.75 | 0.00 | 5000.00 | 0.000 | 0.00 |
| PEAK DISCHARGE = | 18.652 CFS - PEAK OCCURS AT HOUR | 1.63 | | |
| MAXIMUM WATER SURFACE ELEVATION = | 5001.777 | | | |
| MAXIMUM STORAGE = | 0.1421 AC-FT | INCREMENTAL TIME= | 0.010000HRS | |

PRINT HYD ID=12 CODE=1

HYDROGRAPH FROM AREA

305.00

| | | | |
|-----------------------|----------------|----|-----------------------------|
| RUNOFF VOLUME = | 0.22385 INCHES | = | 0.7652 ACRE-FEET |
| PEAK DISCHARGE RATE = | 18.65 CFS | AT | 1.630 HOURS |
| | | | BASIN AREA = 0.0641 SQ. MI. |

FINISH

NORMAL PROGRAM FINISH
END TIME (HR:MIN:SEC) = 16:58:35

↔ (s0p10h4099r~&16D

dmg

D. Mark Goodwin & Associates, P.A.
Consulting Engineers
P.O. BOX 90606, ALBUQUERQUE, NM 87199
(505) 828-2200 FAX 797-9539

PROJECT Team Radio
SUBJECT Outfall Pipe
BY Doug H. DATE 10-8-2014
CHECKED _____ DATE _____
SHEET 1 OF 1

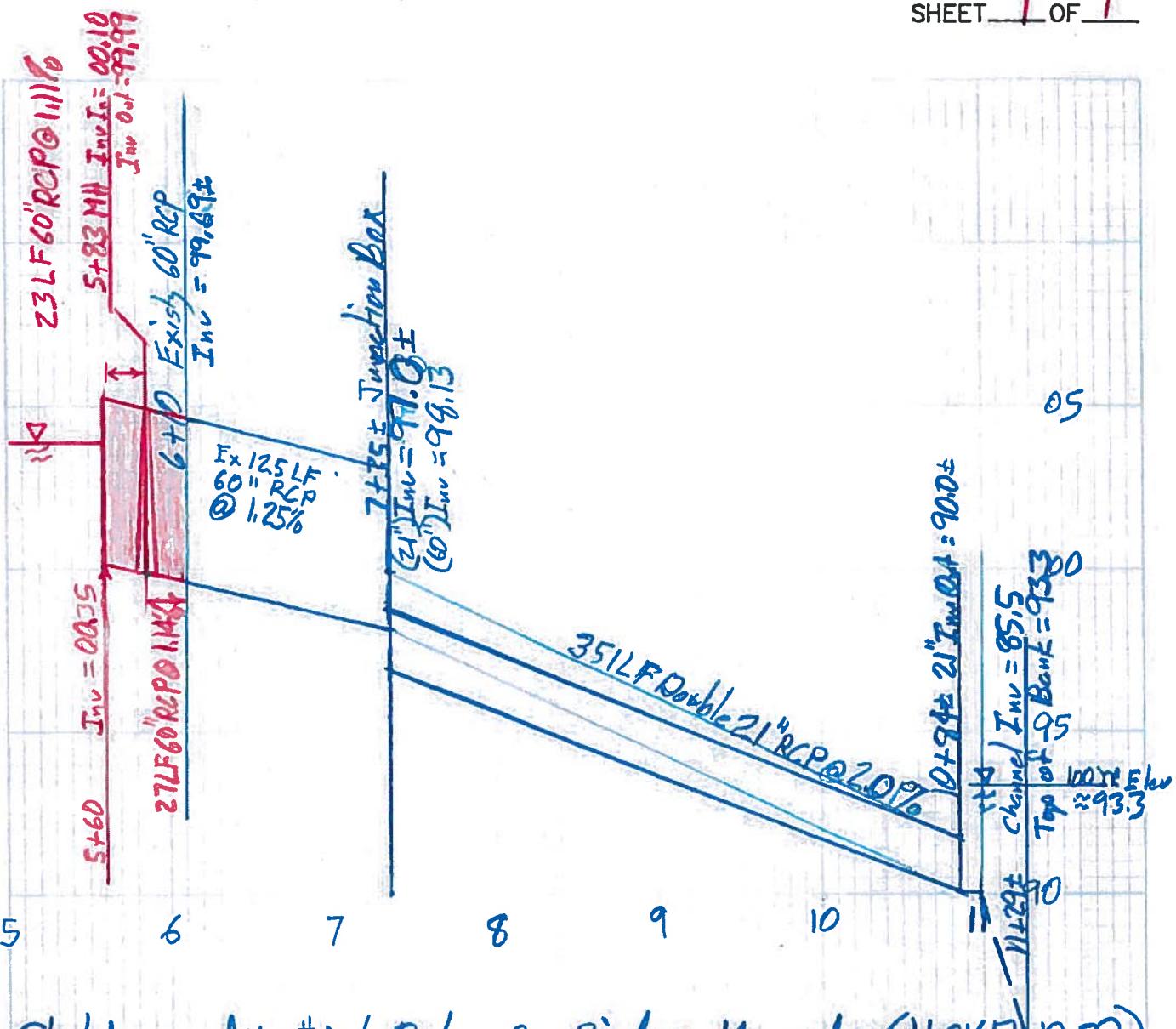
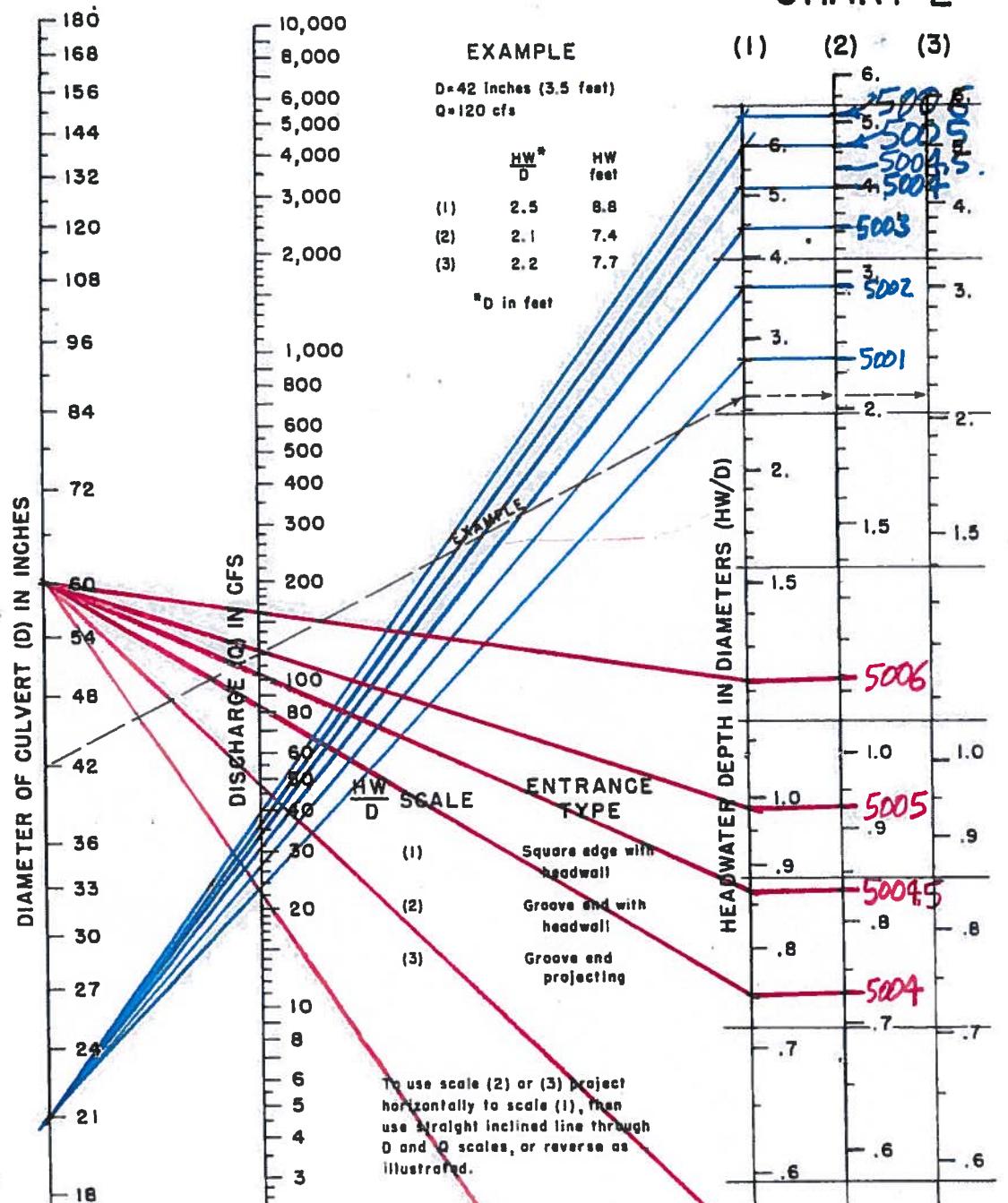


CHART 2



HEADWATER SCALES 263
REVISED MAY 1964

BUREAU OF PUBLIC ROADS JAN. 1963

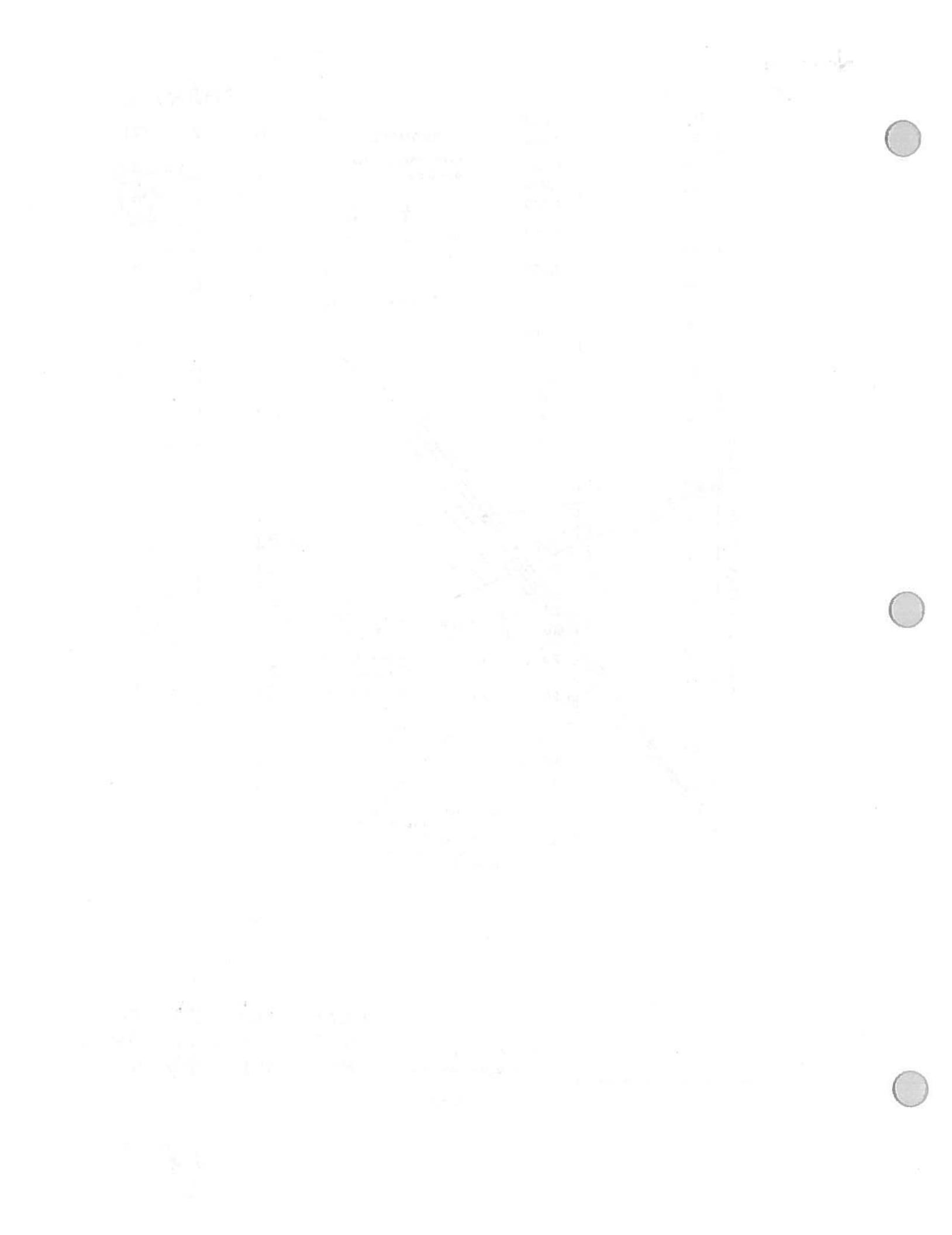
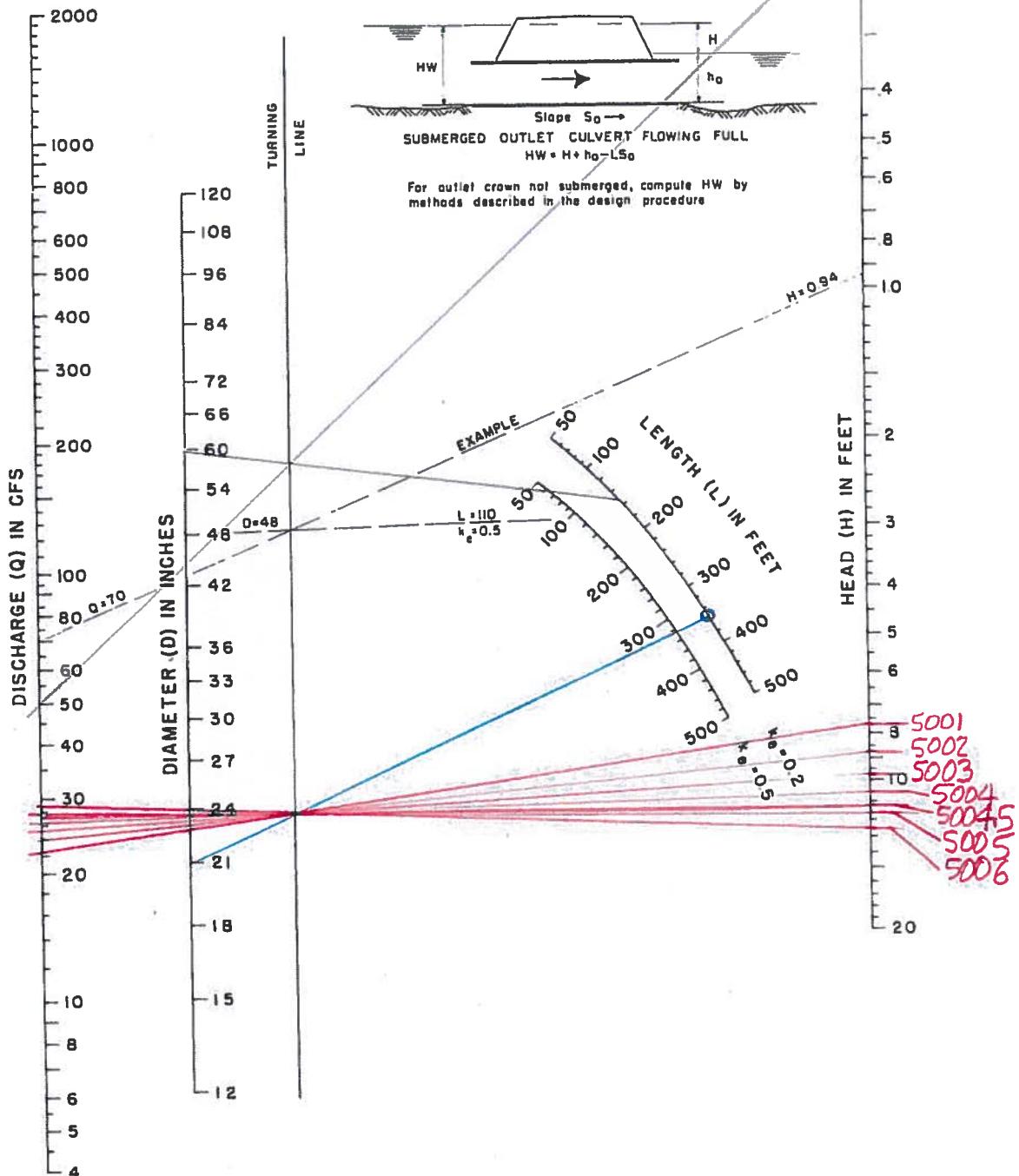


CHART 9



BUREAU OF PUBLIC ROADS JAN 1963

The Team Radio

100 Year Postdeveloped conditions (Peak pond stage with 44% of peak fло

W October 20, 2014

| | Invert | Depth | Water | Q | Vel | Energy | Super | Critical | Flow | Top | Height | Base | Wt | No Wth |
|-----------|----------|-------|----------|-------|-------|--------|---------|----------|-------|---------|---------|------|---------|--------|
| Station | Elev | (FT) | Elev | (CFS) | (FPS) | Head | Grd.El. | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip | |
| L/Elem | Ch Slope | | | | | | | | | | | | | |
| 1179.620 | 5000.200 | 4.060 | 5004.260 | 15.78 | 1.64 | .04 | 5004.30 | .00 | 1.21 | .00 | 3.500 | .000 | 1 .0 | |
| 240.380 | .0021 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |
| 1420.000 | 5000.700 | 3.621 | 5004.321 | 15.78 | 1.64 | .04 | 5004.36 | .00 | 1.21 | .00 | 3.500 | .000 | 1 .0 | |
| 61.545 | .0022 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |
| 1481.545 | 5000.836 | 3.500 | 5004.336 | 15.78 | 1.64 | .04 | 5004.38 | .00 | 1.21 | .00 | 3.500 | .000 | 1 .0 | |
| 161.491 | .0022 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |
| 1643.036 | 5001.192 | 3.175 | 5004.368 | 15.78 | 1.72 | .05 | 5004.41 | .00 | 1.21 | 2.03 | 3.500 | .000 | 1 .0 | |
| 89.344 | .0022 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |
| 1732.380 | 5001.390 | 2.993 | 5004.383 | 15.78 | 1.80 | .05 | 5004.43 | .00 | 1.21 | 2.46 | 3.500 | .000 | 1 .0 | |
| JUNCT STR | .0083 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |
| 1738.380 | 5001.440 | 2.959 | 5004.399 | 13.22 | 1.88 | .05 | 5004.45 | .00 | 1.16 | .69 | 3.000 | .000 | 1 .0 | |
| 100.310 | .0022 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |
| JUNCT STR | .0083 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |
| 1838.690 | 5001.660 | 2.771 | 5004.431 | 13.22 | 1.94 | .06 | 5004.49 | .04 | 1.16 | 1.59 | 3.000 | .000 | 1 .0 | |
| 1844.690 | 5001.710 | 2.672 | 5004.382 | 6.69 | 2.13 | .07 | 5004.45 | .00 | .92 | .00 | 2.000 | .000 | 1 .0 | |
| 74.951 | .0102 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |
| 1919.641 | 5002.471 | 2.000 | 5004.471 | 6.69 | 2.13 | .07 | 5004.54 | .00 | .92 | .00 | 2.000 | .000 | 1 .0 | |
| 19.039 | .0102 | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | .00 | 00 PIPE | |

The Team Radio

100 Year Postdeveloped conditions

October 20, 2014

| | Invert | Depth | Water | O | Vel | Vel | Energy | Super | Critical | Flow | Top | Base | Wt | No Wth |
|-----------|----------|-------|----------|-------|-------|------|---------|-------|----------|-------|-------------------|------|---------|--------|
| Station | Elev | (FT) | Elev | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | [Dia.-FT] or I.D. | ZL | Prs/Pip | |
| L/Elem | Ch Slope | | | | | | | | | | | | | |
| 1179.620 | 5000.200 | 3.060 | 5003.260 | 35.89 | 4.02 | .25 | 5003.51 | .00 | 1.86 | 2.32 | 3.500 | .000 | .00 | |
| 161.300 | .0021 | - | - | - | - | - | .0012 | .19 | 3.06 | .36 | 2.33 | .013 | .00 | |
| 1340.920 | 5000.536 | 2.893 | 5003.429 | 35.89 | 4.22 | .28 | 5003.71 | .00 | 1.86 | 2.65 | 3.500 | .000 | .00 | |
| 79.080 | .0021 | - | - | - | - | - | .0013 | .10 | 2.89 | .42 | 2.33 | .013 | .00 | |
| 1420.000 | 5000.700 | 2.816 | 5003.517 | 35.89 | 4.33 | .29 | 5003.81 | .00 | 1.86 | 2.77 | 3.500 | .000 | .00 | |
| 128.199 | .0022 | - | - | - | - | - | .0014 | .18 | 2.82 | .44 | 2.28 | .013 | .00 | |
| 1548.199 | 5000.983 | 2.682 | 5003.666 | 35.89 | 4.54 | .32 | 5003.98 | .00 | 1.86 | 2.96 | 3.500 | .000 | .00 | |
| 134.726 | .0022 | - | - | - | - | - | .0015 | .21 | 2.68 | .49 | 2.28 | .013 | .00 | |
| 1682.924 | 5001.281 | 2.560 | 5003.841 | 35.89 | 4.76 | .35 | 5004.19 | .00 | 1.86 | 3.10 | 3.500 | .000 | .00 | |
| 49.456 | .0022 | - | - | - | - | - | .0017 | .08 | 2.56 | .54 | 2.28 | .013 | .00 | |
| 1732.380 | 5001.390 | 2.521 | 5003.911 | 35.89 | 4.84 | .36 | 5004.27 | .00 | 1.86 | 3.14 | 3.500 | .000 | .00 | |
| JUNCT STR | .0083 | - | - | - | - | - | .0018 | .01 | 2.52 | .55 | 2.28 | .013 | .00 | |
| 1738.380 | 5001.440 | 2.644 | 5004.084 | 30.06 | 4.56 | .32 | 5004.41 | .00 | 1.78 | 1.94 | 3.000 | .000 | .00 | |
| 100.310 | .0022 | - | - | - | - | - | .0018 | .18 | 2.64 | .44 | 2.36 | .013 | .00 | |
| 1838.690 | 5001.660 | 2.600 | 5004.260 | 30.06 | 4.62 | .33 | 5004.59 | .31 | 1.78 | 2.04 | 3.000 | .000 | .00 | |
| JUNCT STR | .0083 | - | - | - | - | - | .0032 | .02 | 2.91 | .46 | 2.36 | .013 | .00 | |
| 1844.690 | 5001.710 | 2.537 | 5004.247 | 15.21 | 4.84 | .36 | 5004.61 | .00 | 1.41 | .00 | 2.000 | .000 | .00 | |
| 109.310 | .0102 | - | - | - | - | - | .0045 | .49 | 2.54 | .00 | 1.19 | .013 | .00 | |

Program Package Serial Number: 1454

WATER SURFACE PROFILE LISTING

The Team Radio

100 Year Postdeveloped conditions

October 20, 2014

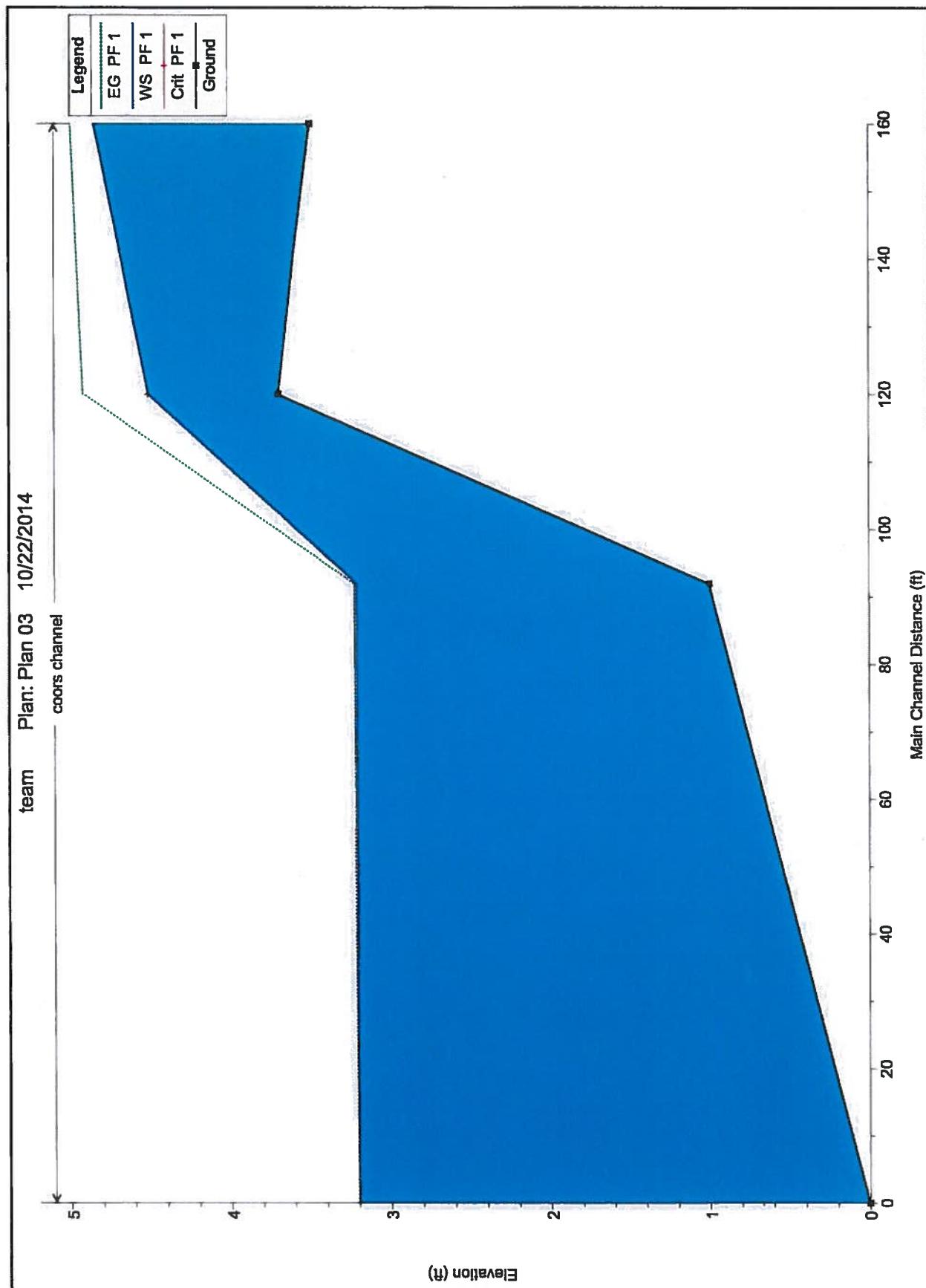
| | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height / | Base | Wt | No Wth |
|----------|----------|-------|----------|-------|-------|-------|---------|-------|----------|-------------------|----------|---------|-------|--------|
| Station | Elev | (FT) | Elev | (CES) | (FPS) | Head | Grd.El. | Elev | Depth | Dia.-FT or I.D. | ZL | Prs/Pip | - - | - - |
| L/Elem | Ch Slope | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - |
| 1954.000 | 5002.820 | 2.047 | 5004.867 | 15.21 | 4.84 | .36 | 5005.23 | .00 | 1.41 | .00 | 2.000 | .000 | .00 | 1 .0 |
| - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - | - - |

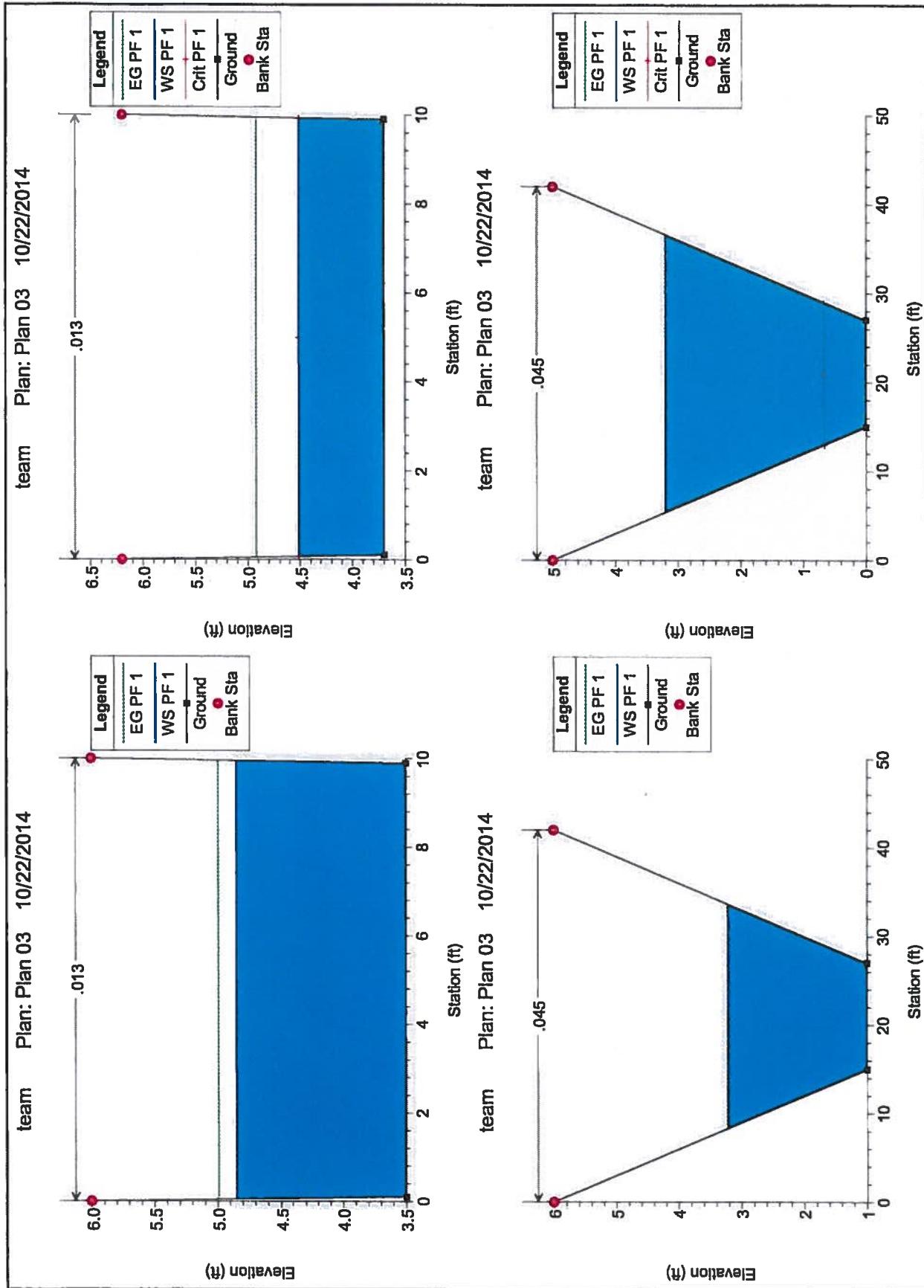
Date:10-21-2014 Time:10:16:42

| Profile: PF 1 | | | | | | | | | | | | |
|---------------|-----------|---------|---------|----------|-----------|-----------|-----------|------------|----------|-----------|-----------|-------------|
| Reach | River Sta | Profile | Q Total | Mn Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vet Chnl | Flow Area | Top Width | Froude # Ch |
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| channel | 1180 | PF 1 | 41.00 | 0.00 | 3.20 | 0.67 | 3.21 | 0.000117 | 0.59 | 69.12 | 31.20 | 0.07 |
| channel | 1272 | PF 1 | 41.00 | 1.00 | 3.21 | | 3.23 | 0.000490 | 0.99 | 41.23 | 25.27 | 0.14 |
| channel | 1300 | PF 1 | 41.00 | 3.70 | 4.51 | 4.51 | 4.92 | 0.003251 | 5.13 | 7.99 | 9.86 | 1.01 |
| channel | 1340 | PF 1 | 41.00 | 3.50 | 4.85 | | 5.00 | 0.000668 | 3.08 | 13.31 | 9.91 | 0.47 |

HEC-RAS Plan: Plan 03 River: coors Reach: channel

| Reach | River Sta | Profile | E.G. Elev (ft) | W.S. Elev (ft) | Vet Head (ft) | Fracn Loss (ft) | G & E Loss (ft) | Q Left (cfs) | Q Channel (cfs) | Q Right (cfs) | Top Width (ft) |
|---------|-----------|---------|-------------------|-------------------|------------------|--------------------|--------------------|-----------------|--------------------|------------------|-------------------|
| channel | 1180 | PF 1 | 3.21 | 3.20 | 0.01 | | | | 41.00 | | 31.20 |
| channel | 1272 | PF 1 | 3.23 | 3.21 | 0.02 | 0.02 | 0.00 | | 41.00 | | 25.27 |
| channel | 1300 | PF 1 | 4.92 | 4.51 | 0.41 | 0.03 | 0.12 | | 41.00 | | 9.86 |
| channel | 1340 | PF 1 | 5.00 | 4.85 | 0.15 | 0.05 | 0.03 | | 41.00 | | 9.91 |





Plan: Plan 03 coors channel RS: 1340 Profile: PF 1

| | | 5.00 | Element | Left OB | Channel | Right OB |
|--------------------|----------|------------------------|-------------------|---------|---------|----------|
| E.G. Elev (ft) | | 0.15 | Wt. n-Val. | | 0.013 | |
| Vel Head (ft) | | 4.85 | Reach Len. (ft) | 40.00 | 40.00 | 40.00 |
| W.S. Elev (ft) | | | Flow Area (sq ft) | | 13.31 | |
| Crit W.S. (ft) | | | | | | |
| E.G. Slope (ft/ft) | 0.000668 | Area (sq ft) | | | 13.31 | |
| Q Total (cfs) | 41.00 | Flow (cfs) | | | 41.00 | |
| Top Width (ft) | 9.91 | Top Width (ft) | | | 9.91 | |
| Vel Total (ft/s) | 3.08 | Avg. Vel. (ft/s) | | | 3.08 | |
| Max Ch Dpth (ft) | 1.35 | Hydr. Depth (ft) | | | 1.34 | |
| Conv. Total (cfs) | 1586.1 | Conv. (cfs) | | | 1586.1 | |
| Length Wtd. (ft) | 40.00 | Wetted Per. (ft) | | | 12.50 | |
| Min Ch El (ft) | 3.50 | Shear (lb/sq ft) | | | 0.04 | |
| Alpha | 1.00 | Stream Power (lb/ft s) | 10.00 | | 0.00 | |
| Frtn Loss (ft) | 0.05 | Cum Volume (acre-ft) | | | 0.14 | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | | | 0.08 | |

Plan: Plan 03 coors channel RS: 1300 Profile: PF 1

| | | 4.92 | Element | Left OB | Channel | Right OB |
|--------------------|----------|------------------------|-------------------|---------|---------|----------|
| E.G. Elev (ft) | | 0.41 | Wt. n-Val. | | 0.013 | |
| Vel Head (ft) | | 4.51 | Reach Len. (ft) | 28.00 | 28.00 | 28.00 |
| W.S. Elev (ft) | | | Flow Area (sq ft) | | 7.99 | |
| Crit W.S. (ft) | | | | | | |
| E.G. Slope (ft/ft) | 0.003251 | Area (sq ft) | | | 7.99 | |
| Q Total (cfs) | 41.00 | Flow (cfs) | | | 41.00 | |
| Top Width (ft) | 9.86 | Top Width (ft) | | | 9.86 | |
| Vel Total (ft/s) | 5.13 | Avg. Vel. (ft/s) | | | 5.13 | |
| Max Ch Dpth (ft) | 0.81 | Hydr. Depth (ft) | | | 0.81 | |
| Conv. Total (cfs) | 719.1 | Conv. (cfs) | | | 719.1 | |
| Length Wtd. (ft) | 28.00 | Wetted Per. (ft) | | | 11.43 | |
| Min Ch El (ft) | 3.70 | Shear (lb/sq ft) | | | 0.14 | |
| Alpha | 1.00 | Stream Power (lb/ft s) | 10.00 | | 0.00 | |
| Frtn Loss (ft) | 0.03 | Cum Volume (acre-ft) | | | 0.13 | |
| C & E Loss (ft) | 0.12 | Cum SA (acres) | | | 0.07 | |

Plan: Plan 03 coors channel RS: 1272 Profile: PF 1

| | | 3.23 | Element | Left OB | Channel | Right OB |
|----------------|--|------|-------------------|---------|---------|----------|
| E.G. Elev (ft) | | 0.02 | Wt. n-Val. | | 0.045 | |
| Vel Head (ft) | | 3.21 | Reach Len. (ft) | 92.00 | 92.00 | 92.00 |
| W.S. Elev (ft) | | | Flow Area (sq ft) | | | 41.23 |
| Crit W.S. (ft) | | | | | | |

Plan: Plan 03 coors channel RS: 1272 Profile: PF 1 (Continued)

| | | | | |
|--------------------|----------|------------------------|-------|--------|
| E.G. Slope (ft/ft) | 0.000490 | Area (sq. ft) | | 41.23 |
| Q Total (cfs) | 41.00 | Flow (cfs) | | 41.00 |
| Top Width (ft) | 25.27 | Top Width (ft) | | 25.27 |
| Vel Total (ft/s) | 0.99 | Avg. Vel. (ft/s) | | 0.99 |
| Max Ch Depth (ft) | 2.21 | Hydr. Depth (ft) | | 1.63 |
| Conv. Total (cfs) | 1852.1 | Conv. (cfs) | | 1852.1 |
| Length Wtd. (ft) | 92.00 | Wetted Per. (ft) | | 25.99 |
| Min Ch El (ft) | 1.00 | Shear (lb/sq ft) | | 0.05 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 42.00 | 0.00 |
| Fricn Loss (ft) | 0.02 | Cum Volume (acre-ft) | | 0.12 |
| C & E Loss (ft) | 0.00 | Cum SA (acres) | | 0.06 |

Plan: Plan 03 coors channel RS: 1180 Profile: PF 1

| | Element | Left OB | Channel | Right OB |
|--------------------|----------|------------------------|---------|----------|
| E.G. Elev (ft) | 3.21 | | | |
| Vel Head (ft) | 0.01 | Wt n Vel. | | 0.045 |
| W.S. Elev (ft) | 3.20 | Reach Len. (ft) | | |
| Crit W.S. (ft) | 0.67 | Flow Area (sq ft) | | 69.12 |
| E.G. Slope (ft/ft) | 0.000117 | Area (sq ft) | | 69.12 |
| Q Total (cfs) | 41.00 | Flow (cfs) | | 41.00 |
| Top Width (ft) | 31.20 | Top Width (ft) | | 31.20 |
| Vel Total (ft/s) | 0.59 | Avg. Vel. (ft/s) | | 0.59 |
| Max Ch Depth (ft) | 3.20 | Hydr. Depth (ft) | | 2.22 |
| Conv. Total (cfs) | 3794.9 | Conv. (cfs) | | 3794.9 |
| Length Wtd. (ft) | | Wetted Per. (ft) | | 32.24 |
| Min Ch El (ft) | 0.00 | Shear (lb/sq ft) | | 0.02 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 42.00 | 0.00 |
| Fricn Loss (ft) | | Cum Volume (acre-ft) | | 0.00 |
| C & E Loss (ft) | | Cum SA (acres) | | |

STREET CAPACITY

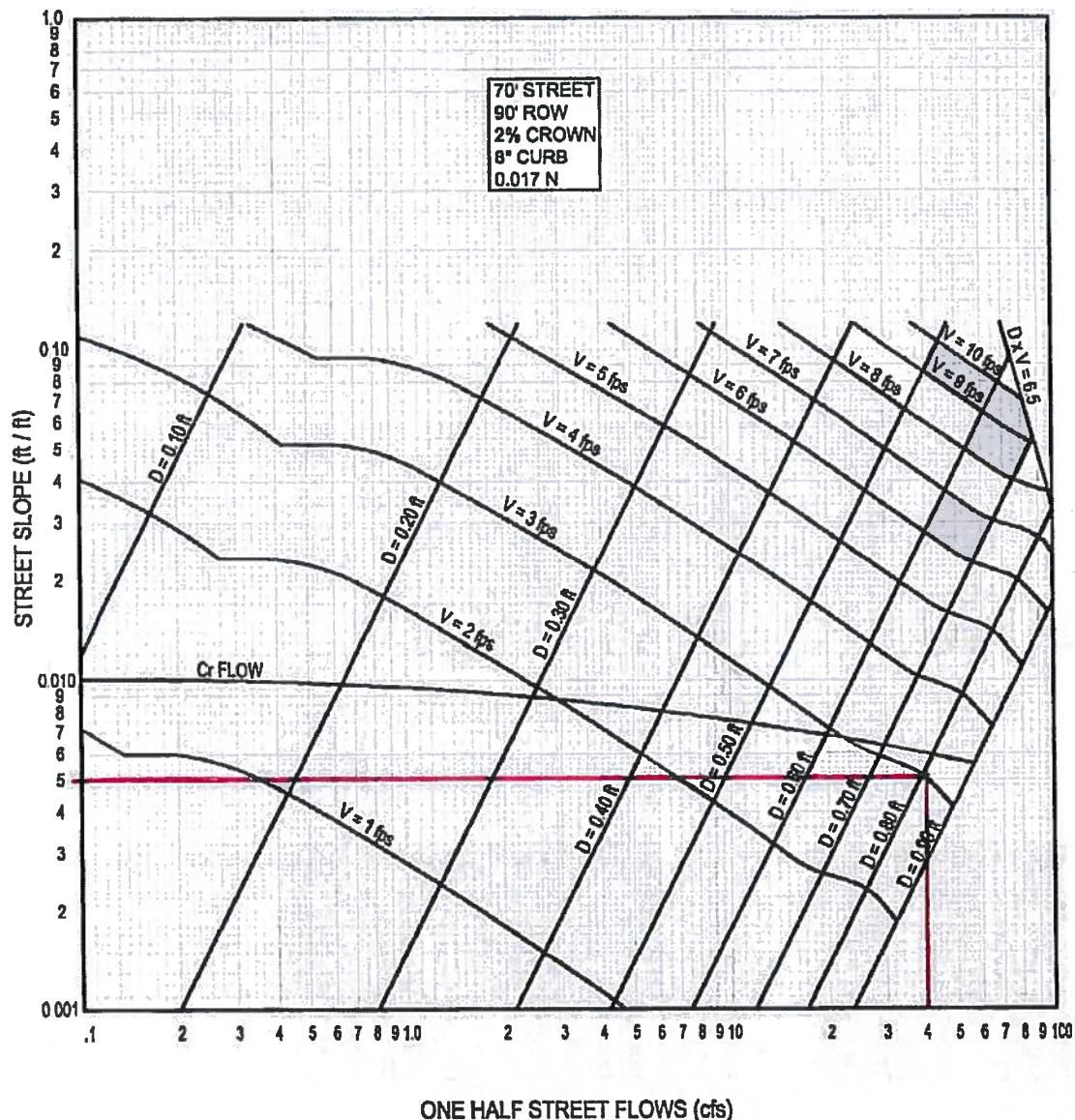


PLATE 22.3 D-4