CITY OF ALBUQUERQUE



June 15, 2015

Bruce Stidworthy Bohannan-Huston, Inc. 7500 Jefferson St. NE Courtyard 1 Albuquerque, NM 87109

RE: Paseo del Norte Sports Complex, Tract A, Loop Industrial Park Grading and Drainage Plan Engineer's Stamp Date 6-11-2015 (File: C17-D008)

Dear Mr. Stidworthy:

Based upon the information provided in your submittal received 6-11-15, the above referenced plan is approved for Building Permit. Please attach a copy of this approved plan in the construction sets when submitting for a building permit. Also, please have an Erosion and Sediment Control Plan approved prior to Building Permit approval.

Albuquerque Prior to Certificate of Occupancy release, Engineer Certification per the DPM Checklist will be required. Additionally, it will be required to submit any construction work within COA right-of-way through the DRC Process.

If you have any questions, you can contact me at 924-3924. New Mexico 87103

www.cabq.gov

Sincerely,

Jeanne Wolfenbarger, P.E. Senior Engineer, Planning Dept. Development Review Services



City of Albuquerque

Planning Department

Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV 02/2013)

Project Title:	Building Permit #:	City Drainage #:
DRB#: EPC#:		Work Order#:
Legal Description:		
City Address:		
Engineering Firm:		Contact:
Address:		
Phone#: Fax#:		E-mail:
Owner:		Contact:
Address:		
Phone#: Fax#:		E-mail:
Architect:		Contact:
Address:		
Phone#: Fax#:		E-mail:
Surveyor:		Contact:
Address:		
Phone#: Fax#:		E-mail:
Contractor:		Contact:
Address:		
Phone#: Fax#:		E-mail:
TYPE OF SUBMITTAL:	CHECK TYPE OF APPROV	AL/ACCEPTANCE SOUGHT:
DRAINAGE REPORT	SIA/FINANCIAL GUARAN	TEE RELEASE
DRAINAGE PLAN 1st SUBMITTAL	PRELIMINARY PLAT APPI	ROVAL
DRAINAGE PLAN RESUBMITTAL	S. DEV. PLAN FOR SUB'D	APPROVAL
CONCEPTUAL G & D PLAN	S. DEV. FOR BLDG. PERMI	IT APPROVAL
GRADING PLAN	SECTOR PLAN APPROVAL	_
EROSION & SEDIMENT CONTROL PLAN (ESC)	FINAL PLAT APPROVAL	
ENGINEER'S CERT (HYDROLOGY)	CERTIFICATE OF OCCUPA	ANCY (PERM)
CLOMR/LOMR	CERTIFICATE OF OCCUPA	ANCY (TCL TEMP)
TRAFFIC CIRCULATION LAYOUT (TCL)	FOUNDATION PERMIT AP	PROVAL
ENGINEER'S CERT (TCL)	BUILDING PERMIT APPRO	DVAL
ENGINEER'S CERT (DRB SITE PLAN)	GRADING PERMIT APPRO	VAL SO-19 APPROVAL
ENGINEER'S CERT (ESC)	PAVING PERMIT APPROV	AL ESC PERMIT APPROVAL
SO-19	WORK ORDER APPROVAL	ESC CERT. ACCEPTANCE
OTHER (SPECIFY)	GRADING CERTIFICATION	N OTHER (SPECIFY)
WAS A PRE-DESIGN CONFERENCE ATTENDED:	Yes No Co	ppy Provided
DATE SUBMITTED:	By:	

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location, and scope to the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following

1. Conceptual Grading and Drainage Plan: Required for approval of Site Development Plans greater than five (5) acres and Sector Plans

2. Drainage Plans: Required for building permits, grading permits, paving permits and site plans less than five (5) acres

3. **Drainage Report**: Required for subdivision containing more than ten (10) lots or constituting five (5) acres or more

4. Erosion and Sediment Control Plan: Required for any new development and redevelopment site with 1-acre or more of land disturbing area, including project less than 1-acre than are part of a larger common plan of development

Bohannan 🛦 Huston

Courtyard I 7500 Jefferson St. NE Albuquerque, NM 87109-4335

June 11, 2015

www.bhinc.com

voice: 505.823.1000 facsimile: 505.798.7988 toll free: 800.877.5332

Ms. Jeanne Wolfenbarger, PE Senior Engineer City of Albuquerque 600 2nd St NW Albuquerque, NM 87102

Re: Paseo Del Norte Sportsplex, Hydrology Re-Submittal

Dear Ms. Wolfenbarger:

Enclosed for your review is a copy of the revised grading plan and drainage management plan. The revisions are based on comments received in your letter dated June 2, 2015 and our meeting on June 8, 2015. Below is a brief description of how the comments were addressed:

- 1. The AHYMO Model has been modified to reflect approximately 10 minute increments and is cut off at 10 hours. The updated model has been provided with this submittal. The Storage Discharge Tables for both ponds have been updated and are now shown on the Drainage Management Plan (C-002).
- 2. The water surface elevations on the AHYMO Model and Drainage Management Plan now match. As mentioned above, the Storage Discharge Tables showing how outflow was determined are now shown on the Drainage Management Plan (C-002).
- 3. A few additional spot elevations have been provided on the Grading Plan for clarity. A "Top of Pond" boundary (shown as a dashed line) for Pond "A" and Pond "B" has been provided on the Drainage Management Plan (C-001).
- 4. The storm drain reach north of the building is undersized. A note explaining how the field is intended to drain is provided in a narrative on sheet C-002.
- 5. A column showing actual flows has been added to the Basin Data Table on the Drainage Management Plan (sheet C-002).
- 6. The flow produced from Basins B2-A, B2-B, B2-C, and B2-D does not include any runoff from the building. The storm drain reach on the East side of the building has more than enough capacity for the runoff produced by the baseball field.

The runoff from the building drains entirely to the South. More information showing the direction the roof drains has been provided on the Drainage Management Plan (sheet C-001).

- 7. A new detail for the large 16' concrete rundown has been provided on sheet C-102. All rundowns are now referenced by the same designation.
 - Engineering **A**
 - Spatial Data 🔺
 - Advanced Technologies **A**

Ms. Jeanne Wolfenbarger City of Albuquerque June 11, 2015 Page 2

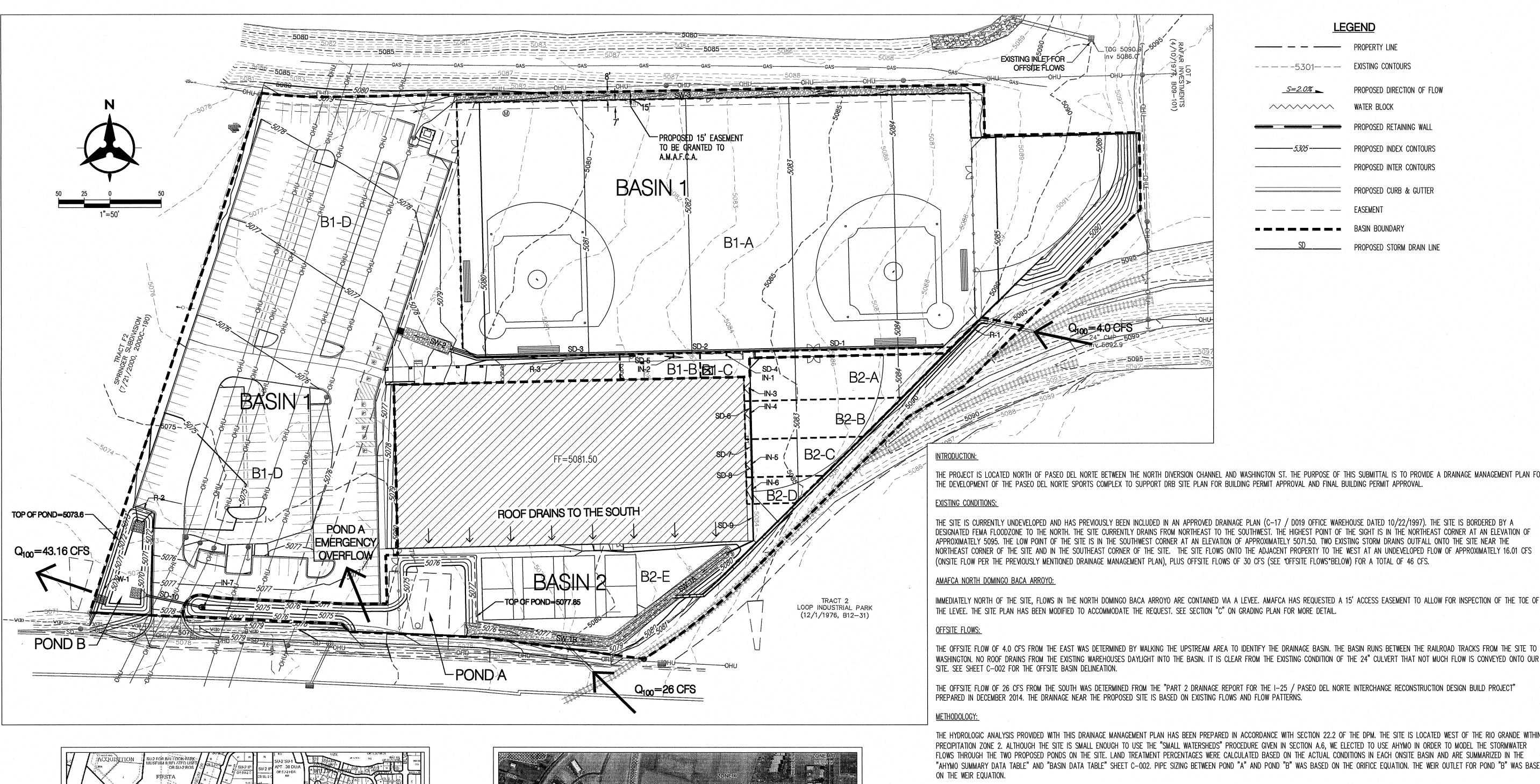
- 8. Type "VL" Angular Riprap per COA Standard Specification 109 has a mean particle size of 6". The Riprap details on sheet C-102 have been updated to reference a 12" thickness which is 2.0 times the aforementioned mean particle size of 6".
- 9. Onsite sidewalk culverts have a small capacity and are intended to convey small storms. The larger onsite storms will flow over the top of the sidewalk culverts in the direction of our intended flow path. This has been added to the drainage narrative on sheet C-002.
- 10. The Inlet capacities are based off the Nyloplast Manufacturer's Nomographs. This has been noted on the "Inlet Table" (sheet C-002). The applicable Manufacturer's Nomographs have been provided with this resubmittal.
- 11. The existing storm drain information for the offsite flows has been provided on the Grading Plans (sheets C-100, C-101, and C-102). Please note that 10 LF of the existing Eastern storm drain will be removed and disposed to properly daylight into a proposed rundown (Sheet C-102, Detail "M").
- 12. The new design of the swale north of the building (SW-2) will now include a concrete rundown. The new detail has been included on sheet C-102. All associated drainage calculations have been included on the Drainage Management Plan (sheet C-002).
- 13. A new spot elevation has been provided on the water block. See sheet C-101 for more details.
- 14. The sand volleyball courts are set at a finished grade elevation of 79.00. Additional detail has been provided to show the extents.

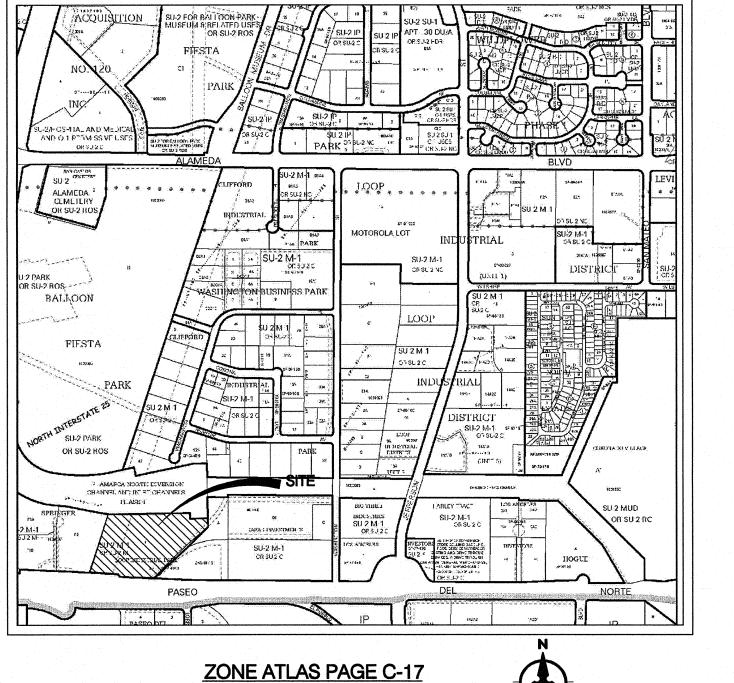
With this resubmittal, we are requesting Hydrology Building Permit Approval. If you have any questions or require further information, please feel free to contact me.

Sincerely,

Matthew Satches, El Engineer Intern Community Development & Planning

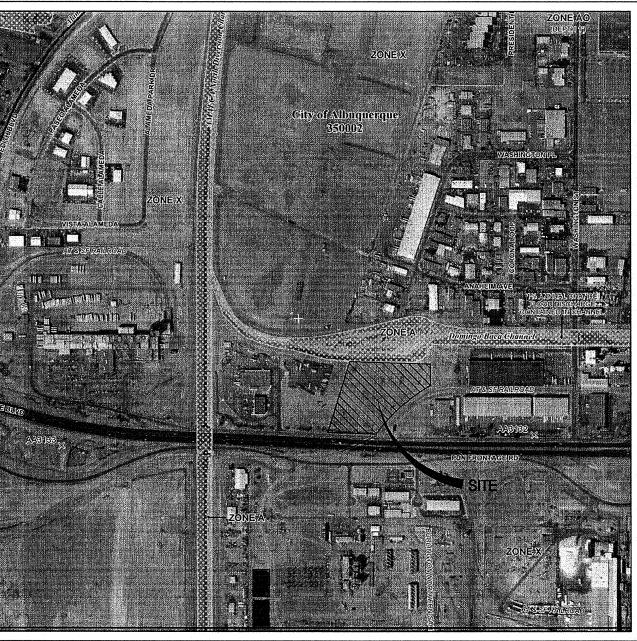
MHS/jcm Enclosures





NTS

Thu, 11-Jun-2015 - 9:22: am, Plotted by: MSATCHES P:\20150146\CDP\Plans\General\CD's\20150146_DMP01.dwg



FEMA FLOODPLAIN MAP 35001C0136G NTS



PROPOSED CONDITIONS:

IT WAS DETERMINED THAT THE MAXIMUM ALLOWABLE DISCHARGE FROM OUR SITE IS APPROXIMATELY 46.0 CFS. THIS IS DERIVED FROM EXISTING ONSITE CONDITIONS PLUS THE ADDITIONAL OFFSITE FLOWS. THE OFFSITE FLOWS WILL BE CONVEYED THROUGH OUR SITE. BASIN 2 ALONG WITH THE OFFSITE FLOWS ARE CONVEYED TO POND "A" VIA A SWALE ALONG THE SOUTHERN PORTION OF THE SITE. POND "A" ULTIMATELY OUTFALLS INTO A 24" PIPE WHERE IT IS ROUTED TO POND "B". EMERGENCY OVERFLOW FROM POND "A" IS TO THE NORTH OVER THE CURB INTO THE PAVED PARKING LOT. THE LENGTH OF OVERFLOW WEIR IS GREATER THAN 100' AND THE OVERFLOW CAPACITY FAR EXCEEDS THE PEAK INFLOW TO THE POND. POND "B" MITIGATES THE DISCHARGE FROM BASIN 1 AND POND "A". A WEIR ON THE WEST SIDE POND "B" OUTFALLS TO THE ADJACENT PROPERTY AT A MAXIMUM DISCHARGE RATE OF 43.16 CFS WHICH IS LESS THAN EXISTING CONDITIONS. THE FIRST FLUSH DEVELOPED BY THE IMPERVIOUS AREA IS RETAINED IN POND "B". THE EMERGENCY OVERFLOW CAPACITY OF THE POND "B" WEIR IS APPROXIMATELY 57.7 CFS WHICH EXCEEDS THE PEAK INFLOW. ONCE THE SITE OUTFALLS ONTO THE ADJACENT PROPERTY, IT WILL CONTINUE ON ITS HISTORIC FLOW PATH.

POND "A": BOTTOM OF POND: 5074.50 FT TOP OF POND: 5077.85 MAXIMUM WATER SURFACE ELEVATION: 5077.30 FT

<u>POND "B"</u> BOTTOM OF POND: 5070.00 FT TOP OF POND: 5073.60 MAXIMUM WATER SURFACE ELEVATION: 5072.60 FT

<u>FIRST_FLUSH</u> IMPERVIOUS AREA = 110,794 SF REQUIRED VOLUME = 4,062 CF PROVIDED VOLUME (POND "A") = 2,554 CF PROVIDED VOLUME (POND "B") = 1,849 CF. TOTAL PROVIDED VOLUME = 4,403 CF

CONCLUSION:

THE PEAK DISCHARGE FROM OUR SITE IS 43.16 CFS WHICH IS LESS THAN THE ALLOWABLE DISCHARGE OF 46.0 CFS. FURTHERMORE, THE GRADING PLAN AND THIS DRAINAGE MANAGEMENT PLAN DEMONSTRATE THAT WE ARE IN CONFORMANCE WITH THE CITY OF ALBUQUERQUE HYDROLOGY REQUIREMENTS. WE REQUEST BUILDING PERMIT APPROVAL.

<u>LE(</u>	GEND
	PROPERTY LINE
5301	EXISTING CONTOURS
<u></u>	PROPOSED DIRECTION OF FLOW WATER BLOCK
	PROPOSED RETAINING WALL
5305	PROPOSED INDEX CONTOURS
	PROPOSED INTER CONTOURS
	PROPOSED CURB & GUTTER EASEMENT
	BASIN BOUNDARY
SD	PROPOSED STORM DRAIN LINE

THE PROJECT IS LOCATED NORTH OF PASED DEL NORTE BETWEEN THE NORTH DIVERSION CHANNEL AND WASHINGTON ST. THE PURPOSE OF THIS SUBMITTAL IS TO PROVIDE A DRAINAGE MANAGEMENT PLAN FOR

THE SITE IS CURRENTLY UNDEVELOPED AND HAS PREVIOUSLY BEEN INCLUDED IN AN APPROVED DRAINAGE PLAN (C-17 / D019 OFFICE WAREHOUSE DATED 10/22/1997). THE SITE IS BORDERED BY A DESIGNATED FEMA FLOODZONE TO THE NORTH. THE SITE CURRENTLY DRAINS FROM NORTHEAST TO THE SOUTHWEST. THE HIGHEST POINT OF THE SIGHT IS IN THE NORTHEAST CORNER AT AN ELEVATION OF APPROXIMATELY 5095. THE LOW POINT OF THE SITE IS IN THE SOUTHWEST CORNER AT AN ELEVATION OF APPROXIMATELY 5071.50. TWO EXISTING STORM DRAINS OUTFALL ONTO THE SITE NEAR THE NORTHEAST CORNER OF THE SITE AND IN THE SOUTHEAST CORNER OF THE SITE. THE SITE FLOWS ONTO THE ADJACENT PROPERTY TO THE WEST AT AN UNDEVELOPED FLOW OF APPROXIMATELY 16.01 CFS

IMMEDIATELY NORTH OF THE SITE, FLOWS IN THE NORTH DOMINGO BACA ARROYO ARE CONTAINED VIA A LEVEE. AMAFCA HAS REQUESTED A 15' ACCESS EASEMENT TO ALLOW FOR INSPECTION OF THE TOE OF

THE OFFSITE FLOW OF 4.0 CFS FROM THE EAST WAS DETERMINED BY WALKING THE UPSTREAM AREA TO IDENTIFY THE DRAINAGE BASIN. THE BASIN RUNS BETWEEN THE RAILROAD TRACKS FROM THE SITE TO

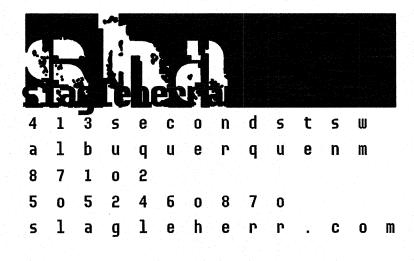
THE OFFSITE FLOW OF 26 CFS FROM THE SOUTH WAS DETERMINED FROM THE "PART 2 DRAINAGE REPORT FOR THE 1-25 / PASEO DEL NORTE INTERCHANGE RECONSTRUCTION DESIGN BUILD PROJECT" PREPARED IN DECEMBER 2014. THE DRAINAGE NEAR THE PROPOSED SITE IS BASED ON EXISTING FLOWS AND FLOW PATTERNS.

THE HYDROLOGIC ANALYSIS PROVIDED WITH THIS DRAINAGE MANAGEMENT PLAN HAS BEEN PREPARED IN ACCORDANCE WITH SECTION 22.2 OF THE DPM. THE SITE IS LOCATED WEST OF THE RIO GRANDE WITHIN PRECIPITATION ZONE 2. ALTHOUGH THE SITE IS SMALL ENOUGH TO USE THE "SMALL WATERSHEDS" PROCEDURE GIVEN IN SECTION A.6, WE ELECTED TO USE AHYMO IN ORDER TO MODEL THE STORMWATER FLOWS THROUGH THE TWO PROPOSED PONDS ON THE SITE. LAND TREATMENT PERCENTAGES WERE CALCULATED BASED ON THE ACTUAL CONDITIONS IN EACH ONSITE BASIN AND ARE SUMMARIZED IN THE "AHYMO SUMMARY DATA TABLE" AND "BASIN DATA TABLE" SHEET C-002. PIPE SIZING BETWEEN POND "A" AND POND "B" WAS BASED ON THE ORIFICE EQUATION. THE WEIR OUTLET FOR POND "B" WAS BASED



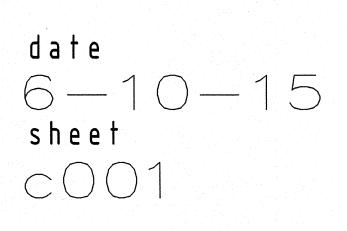
SPORTSPLEX tract A, loop industrial park

Albuquerque, New Mexico



drainage management plan





D	SEO DEI eveloped C s table is bas	condition	s Basin Da	ata Table				
Basin	Area	Area	Land	d Treatme	nt Percent	ages	Q(100yr)	Q(100yr)
ID	(SQ. FT)	(AC.)	Α	В	C	D	(cfs/ac.)	(CFS)
PROPOSED BASINS								
B1-A	146368	3.36	0.0%	0.0%	100.0%	0.0%	3.14	10.55
B1-B	1881	0.04	0.0%	0.0%	25.0%	75.0%	4.31	0.19
B1-C	2318	0.05	0.0%	0.0%	12.0%	88.0%	4.51	0.24
B1-D	131192	3.01	0.0%	0.0%	60.0%	40.0%	3.76	11.34
B2-A	7134	0.16	0.0%	0.0%	98.0%	2.0%	3.17	0.52
B2-B	4954	0.11	0.0%	0.0%	96.0%	4.0%	3.20	0.36
B2-C	3511	0.08	0.0%	0.0%	94.0%	6.0%	3.23	0.26
B2-D	1586	0.04	0.0%	0.0%	93.0%	7.0%	3.25	0.12
B2-E	98554	2.26	0.0%	0.0%	45.0%	55.0%	4.00	9.05
TOTAL	397498	9.125	-		-	-		n an tao sa an Santa ang sa ang sa ang Santa ang sa ang

BASIN & SUBBASIN DATA TABLE

Inlet	Inlet	Basin	Actual	Avail	Capacity
#	Туре		Flow	Head ft	CFS
IN1	1-10" NYLOPLAST (DOME GRT)*	B1-C	0.24	0.30	1.00
IN2	1-10" NYLOPLAST (DOME GRT)*	B1-B	0.19	0.30	1.00
IN3	1-10" NYLOPLAST (DROP IN GRT)*	B2-A	0.52	0.20	0.55
IN4	1-10" NYLOPLAST (DROP IN GRT)*	B2-B	0.36	0.20	0.55
IN5	1-10" NYLOPLAST (DROP IN GRT)*	B2-C	0.26	0.20	0.55
IN6	1-10" NYLOPLAST (DROP IN GRT)*	B2-D	0.12	0.20	0.55
IN7	1-30" NYLOPLAST (DOME GRT)*	B2-E	SEE POND "	A" STORAGE DISC	HARGE TABL

INLET TABLE

STORM DRAIN PIPE TABLE

					ACTUAL
PIPE #	INLET/SD/BASIN	Size	Slope	Capacity*	FLOW
		in.		cfs	cfs
SD1	B1-A	18	0.50%	7.43***	10.55
SD2	SD-1, SD-4	18	0.50%	7.43***	10.79
SD3	SD-2, SD-5	18	0.50%	7.43***	10.98
SD4	IN -1	10	1.50%	2.68	0.24
SD5	IN-2	10	1.50%	2.68	0.19
SD6	IN-3	10	0.50%	1.55	0.52
SD7	IN-4, SD-6	10	0.50%	1.55	0.88
SD8	IN-5, SD-7	10	0.50%	1.55	1.14
SD9	IN-6, SD-8	10	0.50%	1.55	1.26
SD10	IN-7	24	2.00%	31.99	22.9**

*Capacity Based on Manning's Eq w/ N=0.013 **See AHYMO Analysis For Peak Discharge From POND "A"

***Storm Drain Under Capacity. See Narrative (This Sheet) For Explanation.

STORM DRAIN PIPE TABLE

CONCRETE RUNDOWN TABLE											
Rundown #	Basin ID	Rundown Type	Required Flow	Weir Height ft	Weir Length ft	Weir Capacity**	Channel Width ft	Channel Height ft	Minimum Slope	Capacity* CFS	
R-1	EAST STORM DRAIN	Rectangle	4.00		N/A		2.00	0.50	1.00%	5.50	
R-2	Basin 1	Rectangle	22.31	0.67	16.00	24.00	6.00	0.50	33.00%	111.98	
R-3	EXCESS B1-A FLOW	Rectangle	3.55		N/A		2.00	0.50	1.00%	5.50	
	ed on Manning's Eq w/ N=0.0	13 - *	n di al contra di a								
Weir Eq: Q=2.	65L(h^1.5) - **										

RUNDOWN TABLE

SWALE #	Contributing Basins & Flows	Required Flow	Manning's Coefficient	Channel Slope	Stream Capacity*
SW-1A	B2-A, B2-B, B2-C, B2-D, 1/2-B2-E, OS-E	9.79	0.035	0.50%	29.29
SW-1B	B2-A, B2-B, B2-C, B2-D, B2-E, OS-E, OS-S	40.31	0.035	1.30%	47.22
SW-2	B1-A, B1-B, B1-C	10.98	0.035	0.50%	14.66
SW-3	MINIMAL OFFSITE FLOWS	1.11	0.035	1.50%	4.11
Capacity Bas	sed on Manning's Eq - *				
Neir Coeffici	ent = 2.65 - **				

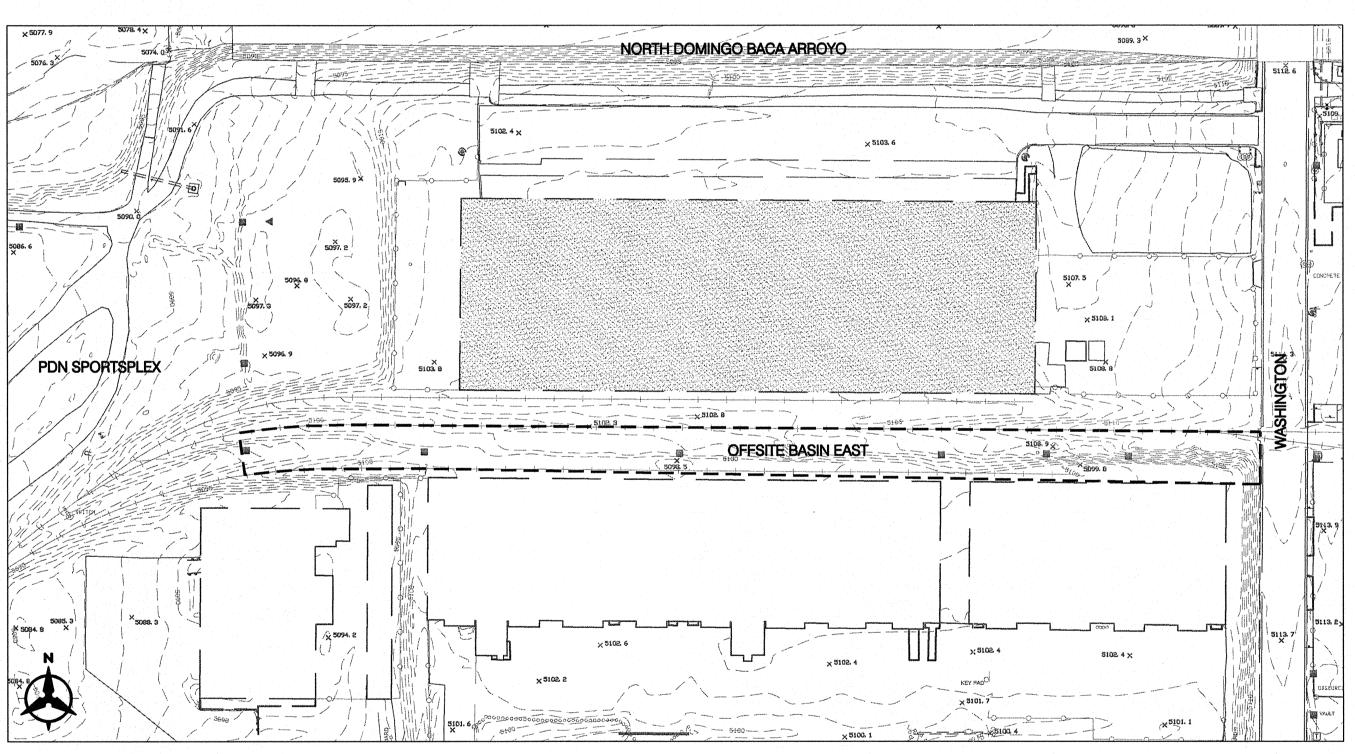
SWALE CAPACITY TABLE

WEIR CAPACITY TABL	E				
WEIR #	Contributing Basins & Flows	Required Flow	Weir Height (FT)	Weir Length (FT)	Weir Capacity*
EMERGENCY OVERFLOW	BASIN 2, OFFSITE SOUTH, OFFSITE EAST	31.60	0.40	250.0	168.00
W1	ENTIRE SITE	42.83	2.00	8.00	60.00
Weir Coefficient = 2.65 - *					

WEIR CAPACITY TABLE

AHYMO PROGRA	AM SUMMARY TABLE (AHYMO-S4)		- Ver. S4	4.01a, Rel: C	1a RUN DA	TE (MON/I	DAY/YR) =0	6/11/2015					
INPUT FILE = P:\2	20150146\CDP\HYDRC	O\Building P	ermit\100	YR-BP.HYI	Μ	USER N	O.= AHYMO	D_Temp_U	ser:2012201	.0	1			
													-	
		FROM		ТО		PEAK	RUNOFF		TIME TO	CFS	PAGE	=	1	
	HYDROGRAPH	ID		ID	AREA	DISCHARGE	VOLUME	RUNOFF	PEAK	PER				
COMMAND	IDENTIFICATION	NO.		NO.	(SQ MI)	(CFS)	(AC-FT)	(INCHES)	(HOURS)	ACRE		NOTATION	N state state	
													5.	
*S AHYMO FILE	FOR ALBUQUERQUE S	PORTS COM	PLEX - ALE	BUQUERQ	UE,NM, BH	PROJ # 20150	0146							
*S 100 YEAR - 6	HOUR STORM						-	2 ¹						
*S						· .	an a							
*S INPUT FILE	P:\20150146\CDP\HY	DRO\Buildir	ng Permit\	100YR-BP	.HYM		· · · ·							
*S OUTPUT FILE	P:\20150146\CDP\I	HYDRO\Build	ding Permi	it\100YR-E	BP.OUT									
TART	TIME=0													
OCATION	ALBUQUERQUE			er en		n for a start of the								
RAINFALL TYPE= 1														
	*****	******	*******	*****	*******	*								
S														
S* COMPUTE BAS	SIN DEVELOPED CONI	DITIONS												
S							L							
S BASIN 1														.:
OMPUTE NM HY	D	B1		1	0.01011	23.87	0.748	1.38795	1.5		3.639 PER	IMP= 19.8	0	
S BASIN 2			al de la companya de								n kan serie di Karana Arra. Arra			
OMPUTE NM HY		B2	-	2	0.00425	11.12	0.372	1.63935	1.5		4.087 PER	IMP= 47.9	0	
5***********	*****	******	*******	********	******	*		1			and the second secon			
S ADDITION OF C	FFSITE SOUTH TO BAS	SIN 2					•••••							
ADD HYD		SOUTHB2	• • ·	20	0.01284	37.19	1.316	1.92121	1.5					1. 1
S ADDITION OF C	FFSITE EAST TO BASI	N 2												
ADD HYD		EASTB2	-	21	0.01468	41.22	1.434	1.83216	1.5					
S ROUTE BASIN 2	& OFFSITE EAST & SO	UTH TO PON	ID "A". OL	TFLOW B	ASED ON 30	"NYLOPLAST	DOME GR	ATE.			· · · · · · · · · · · · · · · · · · ·			
ROUTE RESERVOII	R	PONDA	-	10	0.01468	22.91	1.404	1.79308	1.65		MAX VOLUM	E = 0.473 A	C-FT	
SADDITION OF P	OND "A" TO BASIN 1				teriteri Angeleriteri	· · · · · · · · · · · · · · · · · · ·					· · · · · · · · · · · · · · · · · · ·		a da anti- a anti-	
ADD HYD		PAB1	-	22	0.02479	44.42	2.152	1.62784	1.55					· · ·
S ROUTE BASIN 1	TO POND "B". OUTFL	OW BASED C	ON WEIR C	ALCULATI	ONS						·····			
ROUTE RESERVOII	R	PONDB	_	11	0.02479	43.16	2.125	1.60731	1.55		MAX VOLUM	E = 0.144 A	C-FT	

AHYMO SUMMARY DATA TABLE



EASTERN OFFSITE BASIN MAP

SCALE 1"=100'

torage - Outflow	<u>w Table</u>			
OND "A"				
Outflow	v Capacity based on N	Anufacturer provided N	lomographs	
Inlet T	уре:	30" Nyloplas	st Dome Inlet	
Outflow (cfs)	Storage Volume* (ft^3)	Storage Volume (Ac-ft)	Elev.	Head (ft)
0.001	0.000	0.0000	5074.50	-0.5
0.002	2554.00	0.0586	5075.00	0.0
9.250	5184.00	0.1190	5075.50	0.5
13.500	8694.00	0.1996	5076.00	1.0
17.000	12621.00	0.2897	5076.50	1.5
21.250	17010.00	0.3905	5077.00	2.0
24.000	22950.00	0.5269	5077.50	2.5
26,5000	32454.00	0.7450	5078.00	3.0

STORAGE DISCHARGE TABLE (POND "A")

Storage - Outflow Table

<u>P(</u>	<u> DND "B"</u>				·
		Ouflow Based	On Weir Equation		
	Weir Coef:	2.65		Weir Equation	
	Invert of Weir:	5071 ft		Q=2.65*L*(h^1.5)	
- 4 	Width of Weir:	8 ft			
	Outflow (cfs)	Storage Volume* (ft^3)	Storage Volume (Ac-ft)	Elev. \	NSE
	0.001	0.000	0.0000	5070.00	11 (A
	0.002	668.52	0.0153	5070.50	
e e e	0.003	1849.50	0.0425	5071.00	
	7.495	3022.92	0.0694	5071.50	
	21.200	4375.08	0.1004	5072.00	
	38.947	5914.62	0.1358	5072.50	
	59.963	7651.53	0.1757	5073.00	
	83.80	10890.00	0.2500	5073.50	1
		* AutoCAD Civil 3D Volun	nes		

STORAGE DISCHARGE TABLE (POND "B")

BASIN AND SUB-BASIN HYDROLOGIC ANALYSIS:

THE HYDROLOGIC ANALYSIS PROVIDED WITH THIS DRAINAGE MANAGEMENT PLAN HAS BEEN PREPARED IN ACCORDANCE WITH SECTION 22.2 OF THE DPM. BASIN AND SUB-BASIN BOUNDARIES ARE DELINEATED PER SHEET COO1. SUB-BASINS WERE DEFINED FOR ANALYSIS ON STORM DRAINS, INLETS, RUNDOWNS, AND SWALES. ANALYSIS OF THESE DRAINAGE STRUCTURES CAN BE FOUND ON THIS SHEET.

AHYMO ANALYSIS:

SEE NARRATIVE SHEET COO1.

INLET TABLE:

STORM DRAIN INLETS HAVE BEEN DESIGNED IN SUMP CONDITION. ALL NYLOPLAST INLET CAPACITIES ARE BASED ON NOMOGRAPHS PROVIDED BY THE MANUFACTURER SEE TABLE THIS SHEET FOR CAPACITIES AND CONTRIBUTING FLOWS.

INLET 3 IS UNDERSIZED FOR THE SUB-BASIN IT IS INTENDED TO CONTAIN. ONCE CAPACITY IS REACHED, EXCESS FLOW WILL CONTINUE SOUTH TO INLET 4 WHICH HAS ENOUGH CAPACITY TO ACCEPT THE ADDITIONAL FLOWS.

STORM DRAIN TABLE:

STORM DRAINS WERE SIZED BASED ON MANNING'S EQUATION AND GRAVITY FLOW. SIZE OF STORM DRAINS RANGE FROM 10" TO 24". SEE TABLE THIS SHEET FOR ALL STORM DRAIN REACH ANALYSIS.

THE 18" STORM DRAIN REACH NORTH OF THE BUILDING IS UNDERSIZED. A MAJORITY OF THE RUNOFF FROM THE ATHLETIC FIELD WILL CONTINUE WEST INTO THE PARKING LOT AND WON'T REACH THE PIPE. THE PORTION OF RUNOFF THAT IS UNABLE TO FLOW TO THIS PIPE WILL CONTINUE SOUTH INTO A RIPRAP SWALE THAT WAS SIZED WITH ENOUGH CAPACITY TO COMPENSATE FOR THE EXCESS RUNOFF. SEE SWALE CAPACITY TABLE THIS SHEET FOR MORE INFORMATION.

RUNDOWN TABLE:

CONCRETE RUNDOWN HAVE BEEN DESIGNED USING MANNING'S EQUATION AND THE WEIR EQUATION. RUNDOWN "R1" IS DESIGNED TO CONTAIN THE OFFSITE FLOWS FROM THE EAST. RUNDOWN "R2" IS WEIR CONTROLLED AND ULTIMATELY OUTFALLS INTO POND "B".

SWALE CAPACITY TABLE:

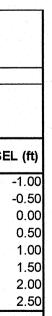
ALL RIPRAP SWALES HAVE BEEN DESIGNED USING MANNING'S EQUATION. SEE TABLE THIS SHEET FOR CAPACITIES AND CONTRIBUTING FLOWS.

WEIR CAPACITY TABLE:

ALL WEIR CAPACITIES HAVE BEEN DESIGNED USING A WEIR COEFFICIENT OF 2.65. SEE TABLE THIS SHEET FOR CAPACITIES AND CONTRIBUTING FLOWS.

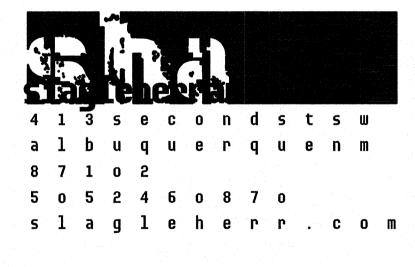
ONSITE SIDEWALK CULVERTS:

A SIDEWALK CULVERT CAPACITY TABLE HAS NOT BEEN PROVIDED. ALL ONSITE SIDEWALK CULVERTS ARE INTENDED TO CONVEY SMALL STORM EVENTS. DURING A LARGE STORM EVENT, RUNOFF WILL FLOW OVER THE TOP OF THE SIDEWALK CULVERTS IN THE DIRECTION OF THEIR INTENDED FLOWPATH.





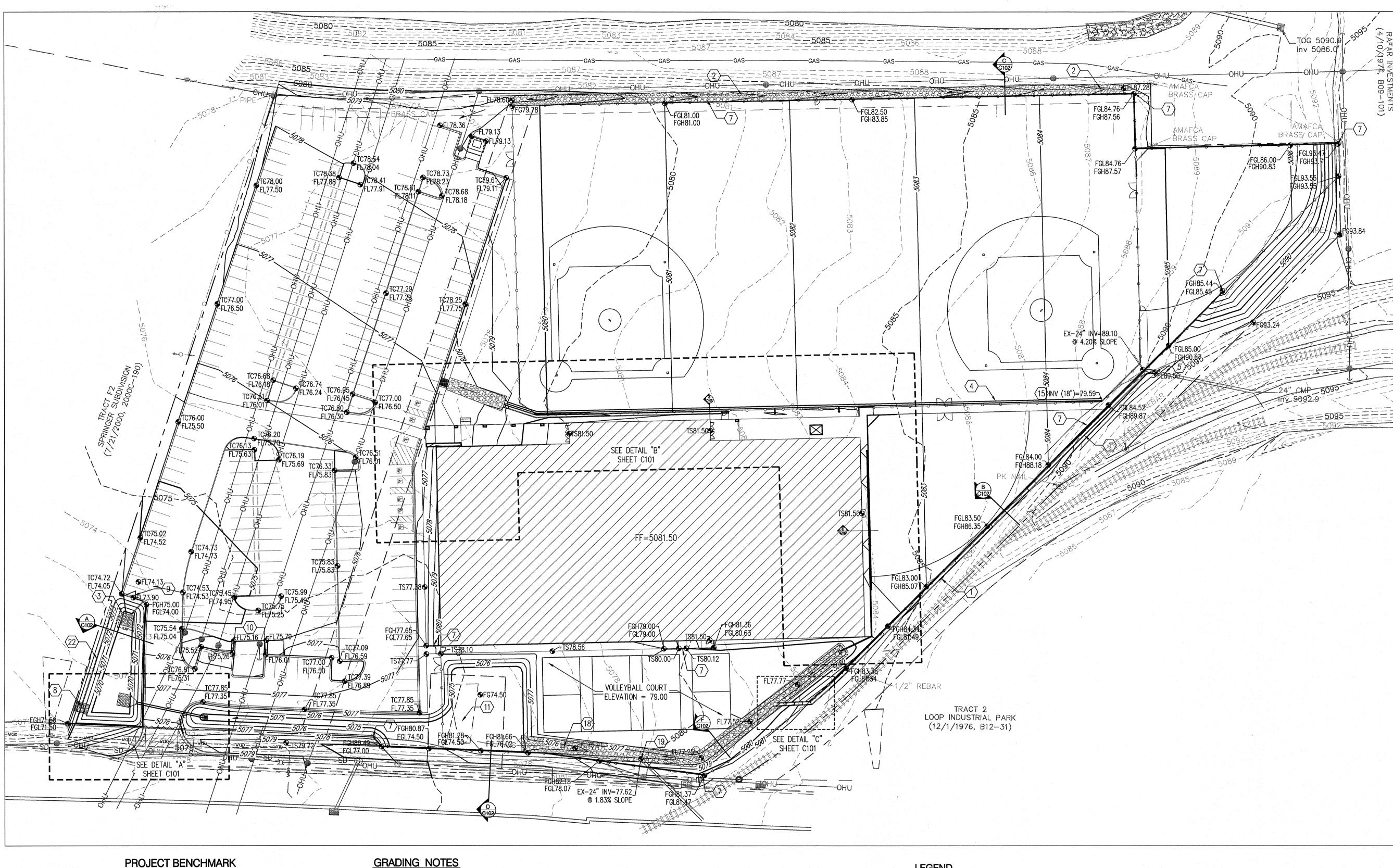
SPORTSPLEX tract A, loop industrial park Albuquerque, New Mexico



drainage management plan



date 6 - 10 - 15sheet c002



PROJECT BENCHMARK

Intersection of PDN & North Diversion Channel @ Southwest Quadrant of Bridge Abutment 3-1/4" Alum Disc ACS Monument "13_D16 NAD 1983CENTRAL ZONE X=1534181.325 Y=1518996.001 Z=5073.471 (NAVD 1988) G-G=0.999673570 Mapping Angle=-00°12'17.26"

1. EXCEPT AS PROVIDED HEREIN, GRADING SHALL BE PERFORMED AT THE ELEV ON THIS PLAN.

2. THE COST FOR REQUIRED CONSTRUCTION DUST AND EROSION CONTROL MEASURES SHALL BE INCIDENTAL TO THE PROJECT COST.

3. ALL WORK RELATIVE TO FOUNDATION CONSTRUCTION, SITE PREPARATION, AND PAVEMENT INSTALLATION, AS SHOWN ON THIS PLAN, SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE "GEOTECHNICAL INVESTIGATION". ALL OTHER WORK SHALL, UNLESS OTHERWISE STATED OR PROVIDED FOR HEREON, BE CONSTRUCTED IN ACCORDANCE WITH THE PROJECT, (FIRST PRIORITY) SPECIFICATIONS, AND/OR THE CITY OF ALBUQUERQUE (COA) STANDARD SPECIFICATIONS FOR PUBLIC WORKS (SECOND PRIORITY).

4. EARTH SLOPES SHALL NOT EXCEED 3 HORIZONTAL TO 1 VERTICAL UNLESS SHOWN OTHERWISE.

5. IT IS THE INTENT OF THESE PLANS THAT THIS CONTRACTOR SHALL NOT PERFORM ANY WORK OUTSIDE OF THE PROPERTY BOUNDARIES EXCEPT AS REQUIRED BY THIS PLAN.

6. THE CONTRACTOR IS TO ENSURE THAT NO SOIL ERODES FROM THE SITE ONTO ADJACENT PROPERTY OR PUBLIC RIGHT-OF-WAY.

7. A DISPOSAL SITE FOR ANY & ALL EXCESS EXCAVATION MATERIAL, AND UNSUITABLE MATERIAL AND/OR A BORROW SITE CONTAINING ACCEPTABLE FILL MATERIAL SHALL BE OBTAINED BY THE CONTRACTOR IN COMPLIANCE WITH APPLICABLE ENVIRONMENTAL REGULATIONS AND APPROVED BY THE OBSERVER. ALL COSTS INCURRED IN OBTAINING A DISPOSAL OR BORROW SITE AND HAUL TO OR FROM SHALL BE CONSIDERED INCIDENTAL TO THE PROJECT AND NO SEPARATE MEASUREMENT OR PAYMENT SHALL BE MADE.

8. PAVING AND ROADWAY GRADES SHALL BE +/- 0.1' FROM PLAN ELEVATIONS. PAD ELEVATION SHALL BE +/- 0.05' FROM BUILDING PLAN ELEVATION.

9. ALL PROPOSED CONTOURS REFLECT TOP OF PAVEMENT ELEVATIONS IN THE PARKING AREA AND MUST BE ADJUSTED FOR MEDIANS AND ISLANDS.

10. VERIFY ALL ELEVATIONS SHOWN ON PLAN FROM BASIS OF ELEVATION CONTROL STATION PRIOR TO BEGINNING CONSTRUCTION.

VATIONS	AND	IN	ACCORDANCE	WITH	THE	DETAILS	SHOWN

LEGEND

	PROPERTY LINE
5301	EXISTING CONTOURS
● 65.23	PROPOSED SPOT ELEVATION TC=TOP OF CURB, FL=FLOW LINE FGH=FINISHED GRADE HIGH, FGL=FINISHED GRADE LOW EX=EXISTING, TG=TOP OF GRATE FG=FINISHED GRADE
S=2.0%	PROPOSED DIRECTION OF FLOW
~~~~~~	WATER BLOCK
	PROPOSED RETAINING WALL
5305	PROPOSED INDEX CONTOURS
	PROPOSED INTER CONTOURS
	PROPOSED CURB & GUTTER
	EASEMENT
SD	PROPOSED STORM DRAIN LINE

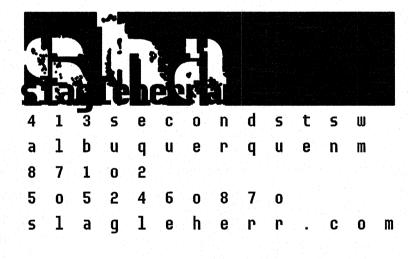
## **GRADING KEYED NOTES**

- 1. INSTALL NEW CONCRETE RIBBON CHANNEL PER DETAIL "I" SHEET C102.
- 2. INSTALL NEW RIP RAP SWALE PER DETAIL "J" SHEET C102.
- 3. INSTALL NEW RIP RAP BLANKET PER DETAIL "L" SHEET C102.
- 4. INSTALL NEW STORM DRAIN. SEE PLAN FOR SIZE. TIE FIELD SUBDRAINS TO STORM DRAIN PER SUBDRAIN MANUFACTURER'S RECOMMENDATIONS
- 5. DAYLIGHT EXISTING CULVERT INTO NEW CONCRETE RIBBON CHANNEL. SEE DETAIL "M" SHEET C102.
- 6. INSTALL CMP STORM DRAIN END SECTION SEE PLAN FOR SIZE.
- 7. INSTALL RETAINING WALL, SEE STRUCTURAL SHEETS FOR DETAILS.
- 8. INSTALL NEW POND WEIR PER DETAIL "H" SHEET C102.
- 9. INSTALL NEW 16' WIDE CONCRETE RUNDOWN PER DETAIL "N" SHEET C102 ..
- 10. INSTALL CURB OPENING PER DETAIL "K" SHEET C102.
- 11. EXISTING BILLBOARD TO REMAIN. MATCH EXISTING GRADE WITHIN 5' OF BILLBOARD FOUNDATION. SEE DETAIL "D" SHEET C102.
- 12. INSTALL NEW 10" NYLOPLAST DOME INLET OR APPROVED EQUAL
- 13. INSTALL NEW 10" NYLOPLAST DROP-IN INLET OR APPROVED EQUAL.
- 14. INSTALL NEW 30" NYLOPLAST DOME INLET OR APPROVED EQUAL 15. INSTALL STORM DRAIN CAP.
- 16. INSTALL PRE-FABRICATED STORM DRAIN FITTING WITH WATER-TIGHT GASKET, SEE PLAN FOR SIZE.
- 17. CONSTRUCT NEW 24" SIDEWALK CULVERT PER COA STD DWG. 2236.
- 18. INSTALL NEW RIP RAP SWALE PER DETAIL "F" SHEET C102.
- 19. DAYLIGHT EXISTING STORM DRAIN INTO SWALE.
- 20. INSTALL PRE-FABRICATED STORM DRAIN BEND. SEE PLAN FOR SIZE.
- 21. CONSTRUCT NEW DOUBLE 24" SIDEWALK CULVERT PER COA STD DWG. 2236.
- 22. INSTALL CONCRETE HEADER CURB PER COA STD DWG. 2415.
- * NOT ALL KEYED NOTES USED ON THIS SHEET

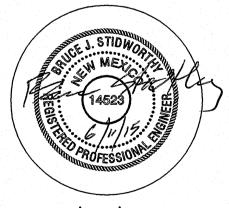
** FOR TYPICAL CROSS-SECTIONS SEE SHEET C102



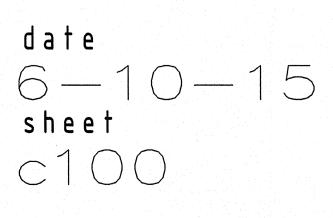
Albuquerque, New Mexico

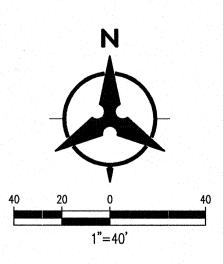


# grading and drainage plan

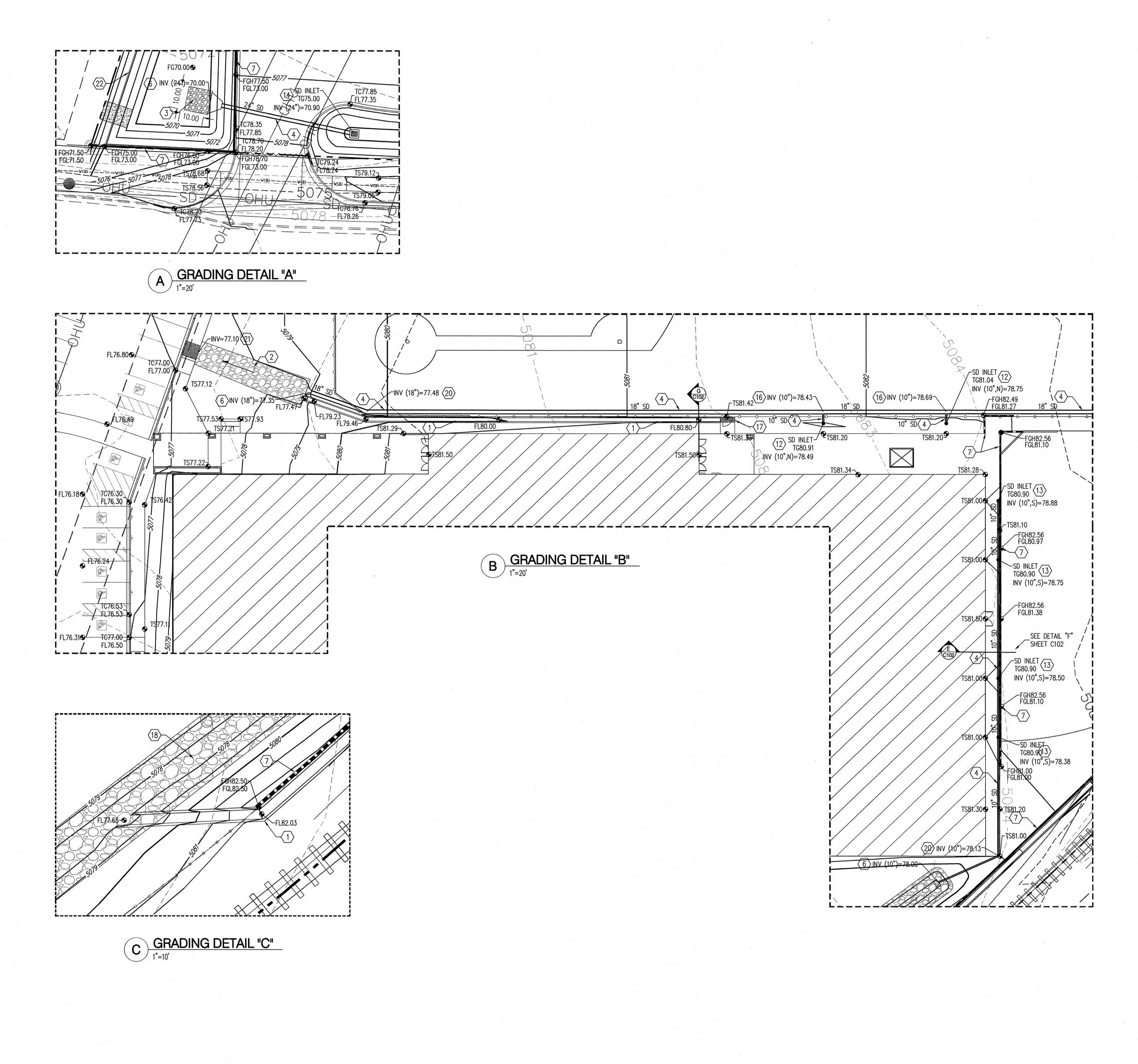


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- 1. INSTALL NEW CONCRETE RIBBON CHANNEL PER DETAIL "I" SHEET C102.
- 2. INSTALL NEW RIP RAP SWALE PER DETAIL "J" SHEET C102.
- 3. INSTALL NEW RIP RAP BLANKET PER DETAIL "L" SHEET C102.
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- 22. INSTALL CONCRETE HEADER CURB PER COA STD DWG. 2415.
- * NOT ALL KEYED NOTES USED ON THIS SHEET

** FOR TYPICAL CROSS-SECTIONS SEE SHEET C102



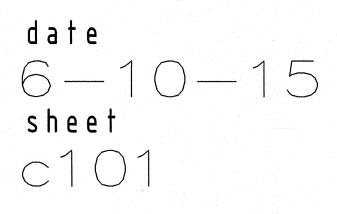
Albuquerque, New Mexico



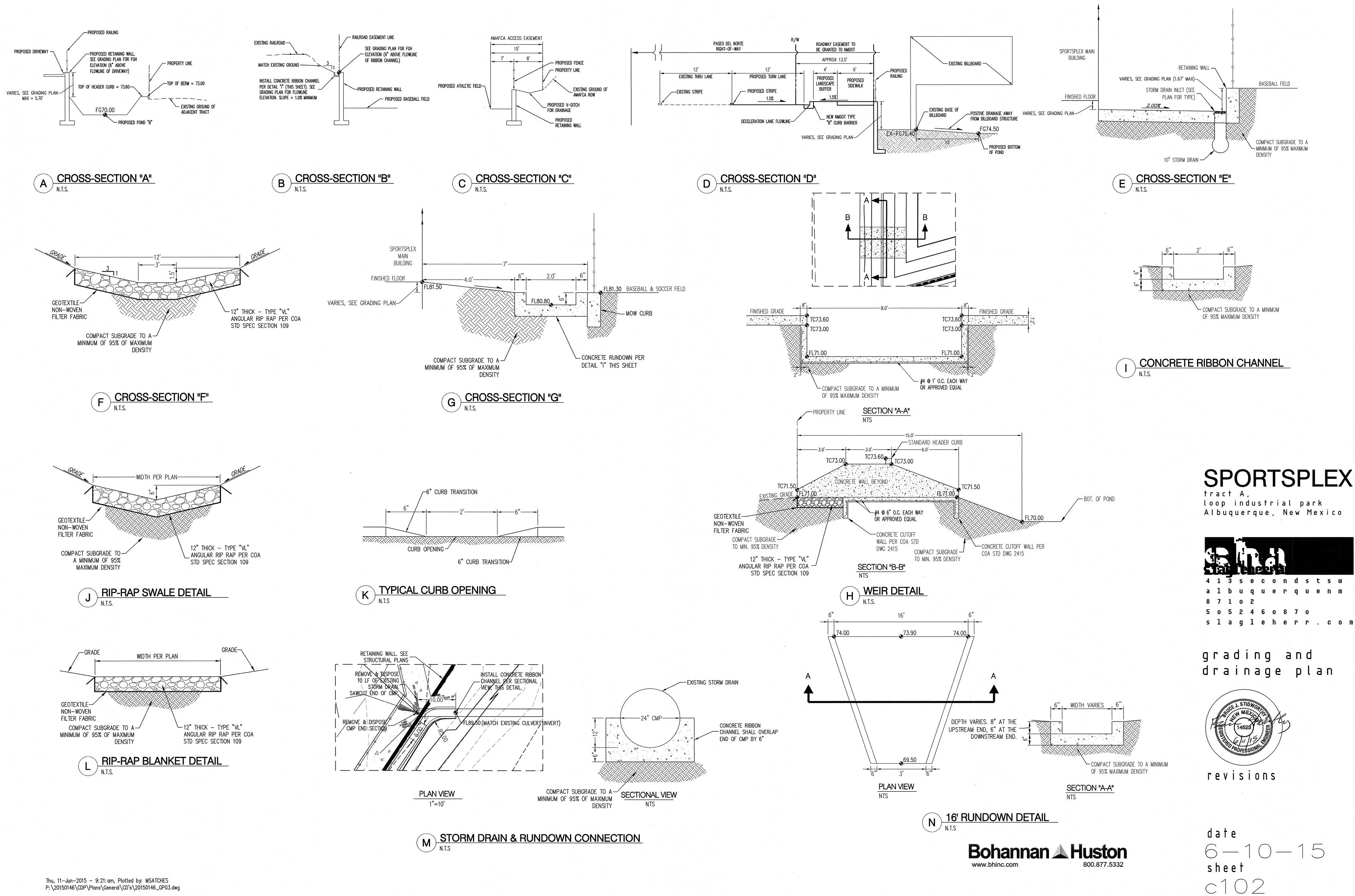
# grading and drainage plan

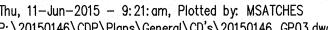


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100YR-BP.HYM *S AHYMO FILE FOR ALBUQUERQUE SPORTS COMPLEX - ALBUQUERQUE, NM , BH PROJ # 20150146 *S 100 YEAR - 6 HOUR STORM *5 *S INPUT FILE -- P:\20150146\CDP\HYDRO\AHYMO\100YR-BP-SUB.HYM * *S OUTPUT FILE -- P:\20150146\CDP\HYDRO\AHYMO\100YR-BP-SUB.OUT * *AHYMO FOR PROPOSED AND RESERVOIR ROUTING CONDITION. * * START TIME=0.0 HR PUNCH CODE=0 ******** LOCATION ALBUQUERQUE, NEW MEXICO *********************** * * 6 HR RAINFALL TABLE * *100 YEAR - 6 HOUR RAINFALL TYPE=1 RAIN QUARTER=0.0 RAIN ONE=2.01 IN RAIN SIX=2.35 IN RAIN DAY=2.75 IN DT=0.05 HRS *S * * *S -----*S -----*S* COMPUTE BASIN DEVELOPED CONDITIONS *S ------*S ------_____ *S *S BASIN 1 * COMPUTE NM HYD ID=1 HYD=B1 AREA=.01011SQ MI PER A=0 PER B=0 PER C=80.2 PER D=19.8 TP=0.1333 HR MASS RAIN=-1 PRINT HYD CODE=20 ID=1 * *S BASIN 2 * * COMPUTE NM HYD ID=2 HYD=B2 AREA=.00425SQ MI PER A=0 PER B=0 PER C=52.1 PER D=47.9 TP=0.1333 HR MASS RAIN=-1 CODE=20 ID=2 PRINT HYD * ***S OFFSITE SOUTH** ID=3 HYD=B3 AREA=.00859SQ MI COMPUTE NM HYD PER A=0 PER B=0 PER C=5 PER D=95 TP=0.1333 HR MASS RAIN=-1 PRINT HYD ID=3 CODE=20* *S OFFSITE EAST * ID=4 HYD=B4 AREA=.00184SQ MI COMPUTE NM HYD

Page 1

100YR-BP.HYM PER A=0 PER B=0 PER C=100 PER D=0 TP=0.1333 HR MASS RAIN=-1 PRINT HYD ID=4 CODE=20* * * * *S ADDITION OF OFFSITE SOUTH TO BASIN 2 ID=20 HYD=SOUTHB2 ID I=3 ID II=2 CODE=20 ADD HYD PRINT HYD ID=20 CODE=20 * *S ADDITION OF OFFSITE EAST TO BASIN 2 ADD HYD ID=21 HYD=EASTB2 ID I=4 ID II=20 CODE=20 PRINT HYD ID=21 CODE=20  $\frac{1}{2}$ * *S ROUTE BASIN 2 & OFFSITE EAST & SOUTH TO POND "A". OUTFLOW BASED ON 30" NYLOPLAST DOME GRATE. ID=10 HYD=PONDA INFLOW ID=21 CODE=3 ROUTE RESERVOIR OUTFLOW (CFS) STORAGE(AC-FT) ELEV (FT) 0.001 0.0000 5074.50 5075.00 0.002 0.0586 5075.50 9.250 0.1190 13.500 0.1996 5076.00 0.2897 5076.50 17.000 0.3905 0.5269  $5077.00 \\ 5077.50$ 21.250 24.000 5078.00 26.500 0.7450 * * *S ADDITION OF POND "A" TO BASIN 1. ID=22 HYD=PAB1 ID I=1 ID II=10 CODE=20 ADD HYD ID=22 CODE=20 PRINT HYD * *S ROUTE BASIN 1 TO POND "B". OUTFLOW BASED ON WEIR CALCULATIONS. ID=11 HYD=PONDB INFLOW ID=22 CODE=3 ROUTE RESERVOIR ELEV (FT) OUTFLOW (CFS) STORAGE(AC-FT) 0.0000 5070.00 0.001 0.002 0.0154 5070.50 0.003 0.0425 5071.00 0.0694 5071.50 7.495 5072.00 21.200 0.1004 5072.50 5073.00 38.947 0.1358 59.963 0.1757 * * ****** FINISH

100YR-BP.OUT

AHYMO PROGRAM (AHYMO-S4) - Version: S4.01a - Rel: 01a RUN DATE (MON/DAY/YR) = 06/10/2015START TIME (HR:MIN:SEC) = 14:40:42USER NO.= AHYMO_Temp_User:20122010 INPUT FILE = P:\20150146\CDP\Hydro\Building Permit\10 Minute Increment\100YR-BP.HYM AHYMO FILE FOR ALBUQUERQUE SPORTS COMPLEX - ALBUQUERQUE, NM , BH PROJ # 2015 *S *S 100 YEAR - 6 HOUR STORM *S *S INPUT FILE -- P:\20150146\CDP\HYDRO\AHYMO\100YR-BP-SUB.HYM * *S OUTPUT FILE -- P:\20150146\CDP\HYDRO\AHYMO\100YR-BP-SUB.OUT *AHYMO FOR PROPOSED AND RESERVOIR ROUTING CONDITION. 20 * START TIME=0.0 HR PUNCH CODE=0 **** LOCATION ALBUQUERQUE, NEW MEXICO City of Albuquerque soil infiltration values (LAND FACTORS) used for computations. Unif. Infilt.(in/hour) Land Treatment Initial Abstr.(in) 1.67 0.65 А 1.25 В 0.50 0.35 0.83 С D 0.10 0.04 * ****** * * 6 HR RAINFALL TABLE * ********** *100 YEAR - 6 HOUR RAINFALL TYPE=1 RAIN QUARTER=0.0 RAIN ONE=2.01 IN RAIN SIX=2.35 IN RAIN DAY=2.75 IN DT=0.05 HRS 6-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1 DT = 0.050000 HOURS END TIME = 6.000000 HOURS 0.0000 0.0023 0.0046 0.0071 0.0099 0.0127 0.0159 0.0595 0.0424 0.0509 0.0203 0.0272 0.0347 0.0684 0.0870 0.1084 0.0776 0.0974 0.1204 0.1437 0.1728 0.4649 0.2117 0.2559 0.3104 0.3831 0.6062 0.8258 1.8719 1.9379 1.2021 1.4666 1.6752 1.7800 1.9905 2.0362 2.0697 2.1005 2.1259 2.1418 2.1530 2.1629 2.1803 2.1879 2.1953 2.2025 2.2084 2.2118 2.1722 2.2152 2.2186 2.2217 2.2247 2.2278 2.2307 2.2336 2.2391 2.2417 2,2363 2.2443 2.2469 2.2494 2.2518 2.2542 2.2565 2.2588 2.2611 2.2633 2.2654 2.2676 2.2798 2.2697 2.2717 2.2738 2.2758 2.2778 2.2817 2.2911 2.2856 2.2874 2.2893 2.2930 2.2837 2.2948 2.3034 2.3000 2.3017 2.2965 2.2983 2.3051 2.3068 2.3117 2.3133 2.3084 2.3100 2.3148 2.3164 2.3180 2.3195 2.3210 2.3240 2.3255 2.3269 2.3284 2.3225 2.3313 2.3355 2.3298 2.3327 2.3341 2.3368 2.3382 2.3409 2.3422 2.3396 2.3436 2.3449 2.3462 2.3474 2.3487 2.3500

100YR-BP.OUT

*S * * *S ------*S -----*S* COMPUTE BASIN DEVELOPED CONDITIONS *S -----*S -----*S *S BASIN 1 ID=1 HYD=B1 AREA=.01011SQ MI COMPUTE NM HYD PER A=0 PER B=0 PER C=80.2 PER D=19.8 TP=0.1333 HR MASS RAIN=-1 K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428UNIT PEAK = 7.9031 CFS UNIT VOLUME = 0.9978 B = 526.28 P60 = 2.01000.002002 SQ MI IA = 0.10000 INCHESINF = 0.04000AREA =INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.107446HR TP = 0.133300HR K/TP RATIO = 0.806046 SHAPE CONSTANT, N = 4.440407UNIT PEAK = 23.329 CFS UNIT VOLUME = 1.001 B = 383.54P60 = 2.0100AREA = 0.008108 SQ MI IA = 0.35000 INCHES INF = 0.83000INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=1 CODE=20

HYDROGRAPH FROM AREA B1

TIME	TIME FLOW	FLOW TI	TIME ME FLOW	FLOW	TIME	FLOW
	HRS	CFS	HRS	CFS	HRS	CFS
HRS	CFS	HR	S CFS			
	0.000	0.0	2.000	2.4	4.000	0.0
6.000	0.0					
	1.000	0.3	3.000	0.1	5.000	0.0
	RUNGEE VO	IIME -	1 38795 TNCHES	_	0 7484 ACRE-	FFFT

 $\begin{array}{rcl} \mbox{RUNOFF VOLUME} = & 1.38795 \mbox{ Inches} = & 0.7484 \mbox{ Acre-feet} \\ \mbox{PEAK DISCHARGE RATE} = & 23.87 \mbox{ CFS} \mbox{ AT} & 1.500 \mbox{ Hours} & \mbox{BASIN AREA} = \\ \mbox{0.0101 SQ. MI.} \end{array}$ 

* * *S BASIN 2 100YR-BP.OUT

COMPUTE NM HYD

*

ID=2 HYD=B2 AREA=.00425SQ MI

PER A=0 PER B=0 PER C=52.1 PER D=47.9 TP=0.1333 HR MASS RAIN=-1

 $\begin{array}{rcl} & \mathsf{K} = & 0.072649 \mathsf{HR} & \mathsf{TP} = & 0.133300 \mathsf{HR} & \mathsf{K}/\mathsf{TP} \; \mathsf{RATIO} = & 0.545000 & \mathsf{SHAPE} \\ \mathsf{CONSTANT}, \; \mathsf{N} = & 7.106428 & & \\ & \mathsf{UNIT} \; \mathsf{PEAK} = & 8.0372 & \mathsf{CFS} \; \mathsf{UNIT} \; \mathsf{VOLUME} = & 0.9978 & \mathsf{B} = & 526.28 \\ \mathsf{P60} = & 2.0100 & & \\ & \mathsf{AREA} = & 0.002036 \; \mathsf{SQ} \; \mathsf{MI} & \mathsf{IA} = & 0.10000 \; \mathsf{INCHES} & \mathsf{INF} = & 0.04000 \\ \mathsf{INCHES} \; \mathsf{PER} \; \mathsf{HOUR} & & \\ & \mathsf{RUNOFF} \; \mathsf{COMPUTED} \; \mathsf{BY} \; \mathsf{INITIAL} \; \mathsf{ABSTRACTION}/\mathsf{INFILTRATION} \; \mathsf{NUMBER} \; \mathsf{METHOD} \; \mathsf{-DT} = \\ 0.050000 & & \end{array}$ 

 $\begin{array}{rcl} & \mathsf{K} = & 0.107446\mathsf{HR} & \mathsf{TP} = & 0.133300\mathsf{HR} & \mathsf{K}/\mathsf{TP} \; \mathsf{RATIO} = & 0.806046 & \mathsf{SHAPE} \\ & \mathsf{CONSTANT}, \; \mathsf{N} = & 4.440407 & \\ & \mathsf{UNIT} \; \mathsf{PEAK} = & 6.3710 & \mathsf{CFS} \; \mathsf{UNIT} \; \mathsf{VOLUME} = & 0.9998 & \mathsf{B} = & 383.54 \\ & \mathsf{P60} = & 2.0100 & \\ & \mathsf{AREA} = & 0.002214 \; \mathsf{SQ} \; \mathsf{MI} & \mathsf{IA} = & 0.35000 \; \mathsf{INCHES} \; \; \mathsf{INF} = & 0.83000 \\ & \mathsf{INCHES} \; \mathsf{PER} \; \mathsf{HOUR} & \\ & \mathsf{RUNOFF} \; \mathsf{COMPUTED} \; \mathsf{BY} \; \mathsf{INITIAL} \; \mathsf{ABSTRACTION}/\mathsf{INFILTRATION} \; \mathsf{NUMBER} \; \mathsf{METHOD} \; \mathsf{-} \; \mathsf{DT} = \\ & 0.050000 \end{array}$ 

PRINT HYD ID=2 CODE=20

HYDROGRAPH FROM AREA B2

TIME	TIME FLOW	FLOW TIME	TIME FLOW	FLOW	TIME	FLOW
	HRS	CFS	HRS	CFS	HRS	CFS
HRS	CFS 0.000	HRS 0.0	CFS 2.000	1.3	4.000	0.0
6.000	$\begin{array}{c} 0.0 \\ 1.000 \end{array}$	0.3	3.000	0.0	5.000	0.0

RUNOFF VOLUME = 1.63935 INCHES = 0.3716 ACRE-FEET PEAK DISCHARGE RATE = 11.12 CFS AT 1.500 HOURS BASIN AREA = 0.0043 SQ. MI.

* *S OFFSITE SOUTH * COMPUTE NM HYD

*

ID=3 HYD=B3 AREA=.00859SQ MI

PER A=0 PER B=0 PER C=5 PER D=95

TP=0.1333 HR MASS RAIN=-1

100YR-BP.OUT AREA = 0.008161 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

 $\begin{array}{rcl} \mathsf{K} = & 0.107446\mathsf{HR} & \mathsf{TP} = & 0.133300\mathsf{HR} & \mathsf{K}/\mathsf{TP} \; \mathsf{RATIO} = & 0.806046 & \mathsf{SHAPE} \\ \mathsf{CONSTANT}, \; \mathsf{N} = & 4.440407 & & \\ & \mathsf{UNIT} \; \mathsf{PEAK} = & 1.2358 & \mathsf{CFS} \; \; \mathsf{UNIT} \; \mathsf{VOLUME} = & 0.9924 & \mathsf{B} = & 383.54 \\ \mathsf{P60} = & 2.0100 & & \\ & \mathsf{AREA} = & 0.000430 \; \mathsf{SQ} \; \mathsf{MI} & \mathsf{IA} = & 0.35000 \; \mathsf{INCHES} \; \; \mathsf{INF} = & 0.83000 \\ \mathsf{INCHES} \; \mathsf{PER} \; \mathsf{HOUR} & & \\ & \mathsf{RUNOFF} \; \mathsf{COMPUTED} \; \mathsf{BY} \; \mathsf{INITIAL} \; \mathsf{ABSTRACTION}/\mathsf{INFILTRATION} \; \mathsf{NUMBER} \; \mathsf{METHOD} \; \mathsf{-DT} = \\ 0.050000 & & \end{array}$ 

PRINT HYD ID=3 CODE=20

HYDROGRAPH FROM AREA B3

ТІМЕ	TIME FLOW	FLOW TIME	TIME FLOW	FLOW	TIME	FLOW
	HRS	CFS	HRS	CFS	HRS	CFS
HRS	CFS 0.000	HRS 0.0	CFS 2.000	3.7	4.000	0.1
6.000	$\begin{smallmatrix}&0.1\\1.000\end{smallmatrix}$	1.1	3.000	0.1	5.000	0.1

 $\begin{array}{rcl} \text{RUNOFF VOLUME =} & 2.06074 \text{ INCHES} &= & 0.9441 \text{ ACRE-FEET} \\ \text{PEAK DISCHARGE RATE =} & 26.08 \text{ CFS} \text{ AT} & 1.500 \text{ HOURS} & \text{BASIN AREA} = \\ 0.0086 \text{ SQ. MI.} \end{array}$ 

* *S OFFSITE EAST * COMPUTE NM HYD

ID=4 HYD=B4 AREA=.00184SQ MI PER A=0 PER B=0 PER C=100 PER D=0

TP=0.1333 HR MASS RAIN=-1

 $\begin{array}{rcl} & \mathsf{K} = & 0.107446\mathsf{HR} & \mathsf{TP} = & 0.133300\mathsf{HR} & \mathsf{K}/\mathsf{TP} \; \mathsf{RATIO} = & 0.806046 & \mathsf{SHAPE} \\ \mathsf{CONSTANT}, \; \mathsf{N} = & 4.440407 & & \\ & \mathsf{UNIT} \; \mathsf{PEAK} = & 5.2941 & \mathsf{CFS} \; \mathsf{UNIT} \; \mathsf{VOLUME} = & 0.9995 & \mathsf{B} = & 383.54 \\ \mathsf{P60} = & 2.0100 & & \\ & \mathsf{AREA} = & 0.001840 \; \mathsf{SQ} \; \mathsf{MI} & \mathsf{IA} = & 0.35000 \; \mathsf{INCHES} \; \; \mathsf{INF} = & 0.83000 \\ \mathsf{INCHES} \; \mathsf{PER} \; \mathsf{HOUR} & & \\ & \mathsf{RUNOFF} \; \mathsf{COMPUTED} \; \mathsf{BY} \; \mathsf{INITIAL} \; \mathsf{ABSTRACTION}/\mathsf{INFILTRATION} \; \mathsf{NUMBER} \; \mathsf{METHOD} \; \mathsf{-} \; \mathsf{DT} = \\ 0.050000 \end{array}$ 

PRINT HYD ID=4 CODE=20

HYDROGRAPH FROM AREA B4

TIME	FLOW	TIME	FLOW	TIME	FLOW
		Pag	e 4		

100YR-BP.OUT FLOW TIME TIME FLOW CFS HRS HRS HRS CFS CFS HRS CFS HRS CFS 0.0 0.000 1.000 0.0 2.000 0.3 3.000 0.0 RUNOFF VOLUME = 1.21081 INCHES = PEAK DISCHARGE RATE = 4.02 CFS AT 0.1188 ACRE-FEET 1.500 HOURS BASIN AREA = 0.0018 SQ. MI. * * * * *S ADDITION OF OFFSITE SOUTH TO BASIN 2 ID=20 HYD=SOUTHB2 ID I=3 ID II=2 CODE=20 ADD HYD ID=20 CODE=20 PRINT HYD HYDROGRAPH FROM AREA SOUTHB2 FLOW FLOW TIME TIME TIME FLOW TIME FLOW TIME FLOW CFS HRS HRS CFS HRS CFS HRS CFS HRS CFS 0.000 0.0 2.000 5.1 4.000 0.1 0.2 6.000 1.000 1.3 3.000 0.1 5.000 0.1 RUNOFF VOLUME = 1.92121 INCHES 1.3156 ACRE-FEET = PEAK DISCHARGE RATE = 37.19 CFS AT 1.500 HOURS BASIN AREA = 0.0128 SQ. MI. * * *S ADDITION OF OFFSITE EAST TO BASIN 2 ADD HYD ID=21 HYD=EASTB2 ID I=4 ID II=20 CODE=20 ID=21 CODE=20 PRINT HYD HYDROGRAPH FROM AREA EASTB2 TIME FLOW TIME FLOW TIME FLOW TIME FLOW TIME FLOW CFS CFS CFS HRS HRS HRS HRS HRS CFS CFS 0.000 0.0 2.000 5.4 4.000 0.1 6.000 0.2 0.2 1.000 1.3 3.000 5.000 0.1 1.83216 INCHES 1.4344 ACRE-FEET RUNOFF VOLUME = = PEAK DISCHARGE RATE = 41.22 CFS AT 1.500 HOURS BASIN AREA = 0.0147 SQ. MI.

Page 5

*

100yr-bp.out

NYLOPL

*

*S ROUTE BASIN ROUTE RESERVO	[R		HYD=PONDA I	NFLOW ID=	OUTFLOW BASED 21 CODE=3 ELEV (FT)	on 30"
	0.0	001	0.0000		5074.50	
	0.0	002	0.0586		5075.00	
	9.2	250	0.1190		5075.50	
	13	. 500	0.1996		5076.00	
	17	.000	0.2897		5076.50	
	21	.250	0.3905		5077.00	
	24	.000	0.5269		5077.50	
	26	.500	0.7450		5078.00	
* * * *	* * *	* * *	* * * *	* * *		
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)		
0.00 0.15 0.30 0.45 0.60 0.75 0.90 1.05 1.20 1.35 1.50 1.65 1.80 1.95 2.10 2.25 2.40 2.55 2.70 2.85 3.00 3.15 3.30 3.45 3.60 3.75 3.90 4.05 4.20 4.35 4.50 5.10 5.25	$\begin{array}{c} 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.27\\ 2.17\\ 5.01\\ 13.71\\ 41.22\\ 24.76\\ 11.89\\ 6.63\\ 3.42\\ 2.01\\ 1.30\\ 0.66\\ 0.39\\ 0.25\\ 0.16\\ 0.39\\ 0.25\\ 0.16\\ 0.07\\ 0.06\\ 0.07\\ 0.06\\ 0.07\\ 0.06\\ 0.07\\ 0.08\\ 0.09\\ 0.09\\ 0.11\\ 0.11\\ 0.11\\ 0.12\end{array}$	5074.00 5074.50 5074.50 5074.50 5074.50 5074.50 5074.51 5074.62 5074.62 5075.44 5075.44 5075.46 5075.79 5075.79 5075.07 5075.01 5075.01 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00 5075.00	$\begin{array}{c} -0.059\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.000\\ 0.001\\ 0.014\\ 0.058\\ 0.112\\ 0.305\\ 0.473\\ 0.410\\ 0.282\\ 0.165\\ 0.091\\ 0.072\\ 0.065\\ 0.062\\ 0.061\\ 0.060\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0.059\\ 0$	$\begin{array}{c} 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 8.14\\ 17.65\\ 22.91\\ 21.64\\ 16.69\\ 11.69\\ 4.96\\ 2.02\\ 1.02\\ 0.55\\ 0.33\\ 0.21\\ 0.13\\ 0.09\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.07\\ 0.011\\ 0.12\\ \end{array}$		

5.40 5.55 5.70 5.85 6.00 6.15 6.30 6.45 6.60 6.75 PEAK DISCHARC MAXIMUM WATER MAXIMUM STORA	R SURFACE	5075.01 5075.01 5075.01 5075.01 5075.01 5075.00 5075.00 5075.00 5075.00 5075.00 22.915 C ELEVATION	0.059 0.059 0.059 0.059 0.059 FS - PEAK_00	0.12 0.13 0.14 0.15 0.16 0.12 0.04 0.02 0.01 0.00 CCURS AT HOUR .303		
* * *S ADDITION OF ADD HYD PRINT HYD	= POND "A			I=1 ID II=10 C	CODE=20	

### HYDROGRAPH FROM AREA PAB1

	TIME	FLOW		TIME	FLOW	TIME	FLOW
TIME	FLOW HRS	CFS	TIME	FLOW HRS	CFS	HRS	CFS
HRS	CFS 0.000	0.0	HRS	CFS 40.000	0.0	80.000	0.0
120.000	0.0	0.3	160.000	0.0	0.0	81.000	0.0
121.000	0.0		161.000	0.0			
122.000	2.000 0.0	17.5	162.000	42.000	0.0	82.000	0.0
	3.000	0.3		43.000	0.0	83.000	0.0
123.000	0.0 4.000	0.1	163.000	0.0 44.000	0.0	84.000	0.0
124.000	0.0 5.000	0.1	164.000	0.0	0.0	85.000	0.0
125.000	0.0		165.000	0.0			
126.000	6.000 0.0	0.2	166.000	46.000		86.000	0.0
127.000	7.000 0.0	0.0	167.000	47.000	0.0	87.000	0.0
	8.000	0.0		48.000	0.0	88.000	0.0
128.000	0.0 9.000	0.0	168.000	0.0 49.000	0.0	89.000	0.0
129.000	0.0 10.000	0.0	169.000	0.0 50.000	0.0	90.000	0.0
130.000	0.0		170.000	0.0			
131.000	11.000 0.0	0.0	171.000	51.000 0.0	0.0	91.000	0.0
132.000	12.000 0.0	0.0	172.000	52.000 0.0	0.0	92.000	0.0
	13.000	0.0		53.000	0.0	93.000	0.0
133.000	0.0 14.000	0.0	173.000	0.0 54.000	0.0	94.000	0.0
134.000	0.0 15.000	0.0	174.000	0.0 55.000	0.0	95.000	0.0
135.000	0.0		175.000	0.0	1		
136.000	16.000 0.0	0.0	176.000	56.000 0.0		96.000	0.0
	17.000	0.0		57.000 Pag	0.0 e 7	97.000	0.0
				, ag			

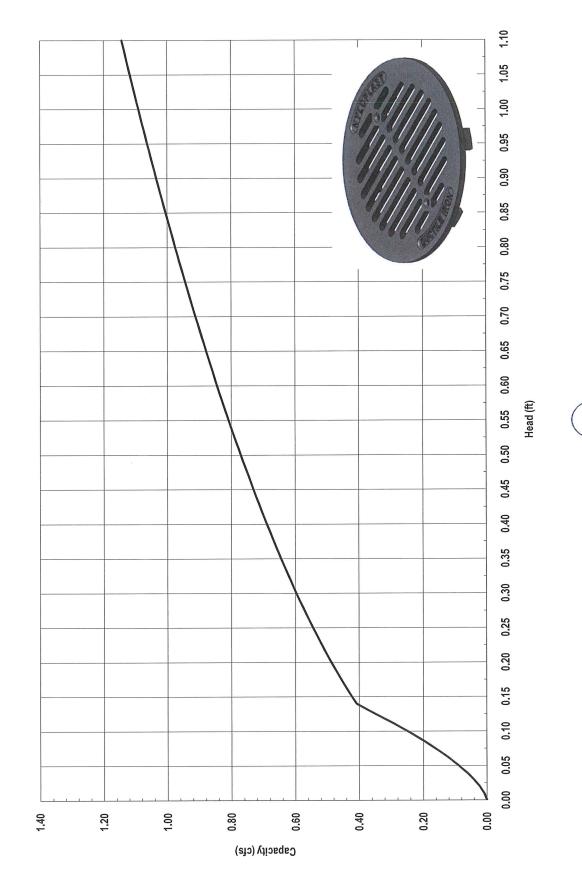
	100YR-BP.	ουτ		
137.000 0.0 18.000	177.000 0.0 0.0 58.000	0.0	98.000	0.0
138.000   0.0   19.000	178.000 0.0 0.0 59.000	0.0	99.000	0.0
139.000 0.0 20.000	179.000 0.0 0.0 60.000	0.0	100.000	0.0
140.000 0.0	180.000 0.0			
$\begin{array}{c} 21.000\\141.000 \\ 0.0 \end{array}$	$\begin{array}{cccc} 0.0 & & 61.000 \\ & 181.000 & & 0.0 \end{array}$	0.0	101.000	0.0
22.000 142.000 0.0	$ \begin{array}{cccc} 0.0 & 62.000 \\ 182.000 & 0.0 \end{array} $	0.0	102.000	0.0
23.000 143.000 0.0	$\begin{array}{ccc} 0.0 & 63.000 \\ 183.000 & 0.0 \end{array}$	0.0	103.000	0.0
24.000 144.000 0.0	$\begin{array}{ccc} 0.0 & 64.000 \\ 184.000 & 0.0 \end{array}$	0.0	104.000	0.0
25.000	0.0 65.000	0.0	105.000	0.0
145.000 0.0 26.000	185.000 0.0 0.0 66.000	0.0	106.000	0.0
146.000 0.0 27.000	186.000   0.0   0.0   0.0   0.0	0.0	107.000	0.0
147.000 0.0 28.000	187.000  0.0  0.0  0.0  0.0	0.0	108.000	0.0
148.000 0.0 29.000	$\begin{array}{ccc} 188.000 & 0.0 \\ 0.0 & 69.000 \end{array}$	0.0	109.000	0.0
149.000 0.0 30.000	189.000 0.0 0.0 70.000	0.0	110.000	0.0
150.000 0.0	190.000 0.0			
31.000 151.000 0.0	$\begin{array}{cccc} 0.0 & & 71.000 \\ & 191.000 & & 0.0 \end{array}$	0.0	111.000	0.0
32.000 152.000 0.0	$\begin{array}{cccc} 0.0 & 72.000 \\ 192.000 & 0.0 \end{array}$	0.0	112.000	0.0
33.000 153.000 0.0	$\begin{array}{cccc} 0.0 & 73.000 \\ 193.000 & 0.0 \end{array}$	0.0	113.000	0.0
34.000 154.000 0.0	0.0 74.000 194.000 0.0	0.0	114.000	0.0
35.000	0.0 75.000	0.0	115.000	0.0
155.000 0.0 36.000	$\begin{array}{cccc} 195.000 & 0.0 \\ 0.0 & 76.000 \end{array}$	0.0	116.000	0.0
156.000 0.0 37.000	$\begin{array}{ccc} 196.000 & 0.0 \\ 0.0 & 77.000 \end{array}$	0.0	117.000	0.0
157.000 0.0 38.000	197.000   0.0   0.0   0.0   78.000	0.0	118.000	0.0
158.000 0.0 39.000	198.000 0.0	0.0	119.000	0.0
159.000 0.0	$\begin{array}{ccc} 0.0 & & 79.000 \\ & 199.000 & & 0.0 \end{array}$	010	1101000	010
RUNOFF VOLU	ME = 1.62784 INCHES RGE RATE = 44.42 CFS	.=	2.1522 ACRE-FEE	T
PEAK DISCHA 0.0248 SQ. MI.	KGE KAIE = 44.42 CFS	AI	1.330 HOURS BASIN	AREA =

	100	)YR-BP.OU	г		
7.4	195	0.0694		5071.50	
21	. 200	0.1004		5072.00	
38	.947	0.1358		5072.50	
59	.963	0.1757		5073.00	
* * * * * * *	* * * *	* * *	* * *		
TIME INFLOW (HRS) (CFS)		/OLUME (AC-FT)	OUTFLOW (CFS)		
0.00 0.00 0.15 0.00 0.30 0.00 0.45 0.00 0.60 0.00 0.75 0.00 0.90 0.05 1.05 0.43 1.20 1.07 1.35 14.77 1.50 41.52 1.65 37.71 1.80 27.69 1.95 19.61 2.10 13.32 2.25 5.96 2.40 2.65 2.55 1.39 2.70 0.77 2.85 0.47 3.00 0.30 3.15 0.19 3.30 0.13 3.45 0.10 3.60 0.08 3.75 0.08 3.90 0.08 4.05 0.08 4.20 0.09 4.35 0.09 4.50 0.10 4.65 0.11 4.80 0.11 4.80 0.11 4.95 0.12 5.10 0.13 5.25 0.14 5.40 0.15 5.55 0.16 5.70 0.17 5.85 0.18 6.00 0.01 6.75 0.00 PEAK DISCHARGE =	5069.50 5070.00 5070.00 5070.00 5070.00 5070.00 5070.09 5070.38 5071.57 5072.47 5072.51 5072.22 5071.99 5071.76 5071.50 5071.22 5071.11 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 5071.01 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MAXIMUM STORAGE =	100YR-BP.OU 0.1438 AC-FT	T INCREMENTAL TIME=	0.050000HRS
* * ****** FINISH			
NORMAL PROGRAM FINISH	END TIME	(HR:MIN:SEC) = 14:4	0:42

**Nyloplast** Inlet Capacity Charts June 2012 © Nyloplast Inlet Capacity Charts June 2012

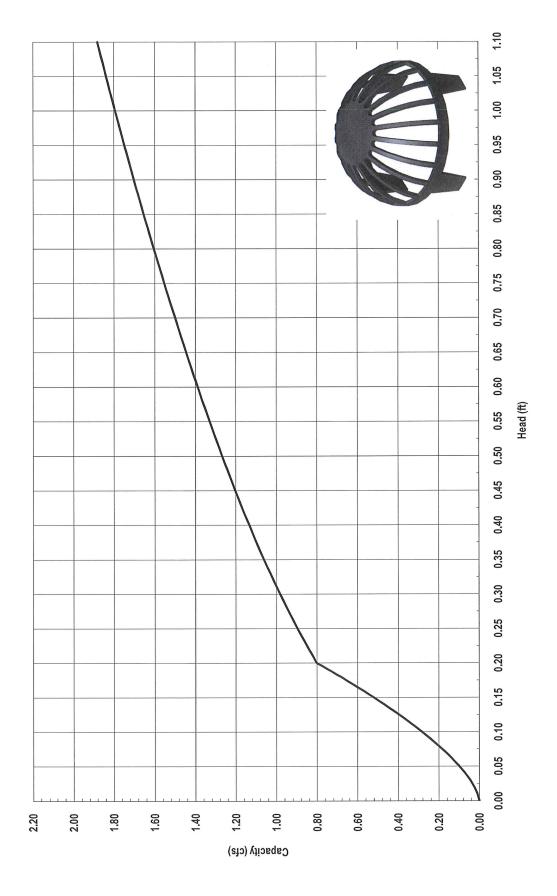
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Nyloplast 10" Drop In Grate Inlet Capacity Chart

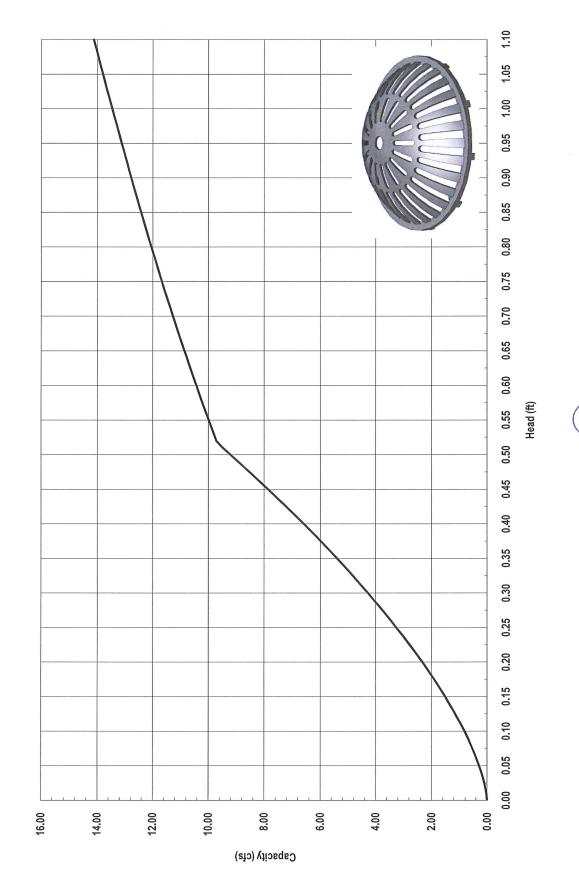
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3130 Verona Avenue • Buford, GA 30518 (866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490 © Nyloplast Inlet Capacity Charts June 2012



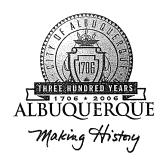
Nyloplast 10" Dome Grate Inlet Capacity Chart





Nyloplast 30" Dome Grate Inlet Capacity Chart

# CITY OF ALBUQUERQUE



March 10, 2005

David Soule, PE Rio Grande Engineering 1606 Central SE, Ste 201 Albuquerque, NM 87106

### Re: Paseo del Norte Sportsplex Drainage Report Engineer's Stamp dated 12-29-04

Dear Mr. Soule,

Based upon the information provided in your submittal dated 12-29-04, the above referenced report is approved for Site Development Plan. Prior to Building Permit approval, please address the following comments.

P.O. Box 1293

Albuquerque

New Mexico 87103

www.cabq.gov

- Please direct the emergency spillway toward Paseo del Norte.
- How does the runoff leave the pond? Does it daylight to the existing grade?
- Please check the volumes of the pond they appear small. This will probably affect the AHYMO run.
- Pipes 7 and 8 are undersized. Also, please check your weir calculation.
- Please include exhibit from the previous report (C17-D19) showing allowable discharge to the property to the west.

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE Principal Engineer, Planning Dept. Development and Building Services

C: file

### DRAINAGE REPORT

for

# Paseo Del Norte Sportsplex Albuquerque, New Mexico

Prepared by Rio Grande Engineering 1606 Central Ave. SE, Suite 201 Albuquerque, New Mexico 87106

December 2004



2. 3 2004

David Soule P.E. No. 14522

### PURPOSE

The purpose of this report is to provide the Drainage Management Plan for the development of indoor/ outdoor sports complex. The proposed development will consist of an approximately 56,000 square foot building, 11outdoor volley-ball courts, a miniature baseball field and their associated parking lot. The site contains 9.48 acres. This plan will identify the upstream and downstream hydraulic constraints affecting the subject property. This plan was prepared in accordance with the City of Albuquerque's Development Process Manual Drainage Criterion. This report will demonstrate that the proposed improvements do not adversely affect the surrounding properties, nor the upstream or downstream facilities.

### INTRODUCTION

The subject of this report, as shown on the Exhibit A - vicinity map, is a 9.48-acre parcel of land located on the north side of Paseo Del Norte Avenue west of Washington Avenue NE. The site is currently undeveloped. The legal description of the parcel is tracts 1 & 2 Loop Industrial Park. The site is bounded by an inlet to the North AMAFCA Diversion Channel on the North, the Paseo Del Norte Frontage Road on the south, a railroad spur to the east and a partially developed parcel to the west. Due to the surrounding improvements, this site is not impacted by any significant offsite flow. The site currently discharges 21.16 cfs directly to the adjacent tract of land to the west of the site. A drainage plan (C17-D19) was completed for the adjacent tract which allows for 16.01cfs to leave enter this site from the subject site. Due to the existing drainage facilities and the fact the site is significantly lower than the adjacent AMAFCA channel and Paseo Del Norte, the existing patterns will be maintained and the development of this site shall be in conformance to the approved plan for the adjacent tract.

### **EXISTING CONDITIONS**

This site is currently undeveloped. It appears this site has never been developed. The site is covered by native grasses and indigenous plants. The site drains from northeast to the southwest with general grades between 2-3 %. As shown in appendix A, the site currently discharges 21.16 cfs upon the adjacent westerly tract at the southwest corner of the site. This site and the adjacent site to the west are significantly lower than the adjacent roadway. Once the flow enters the adjacent tract, it combines with the developed flows and enters the North Diversion channel just west of the adjacent tract. Due to the existing grades, the adjacent site was designed to accommodate 16.01 cfs from this site. This report was prepared by BHI with a stamp date of April 22, 1998 and is located in C17-D19. This report defines this site as offsite basin B-1 and accounts for 16.01 cfs to discharge at the southern boundary. There no visual evidence that the existing drainage patterns have any negative impacts onsite or offsite.

### **PROPOSED CONDITIONS**

As shown in Map Pocket A, the site contains a 15 drainage basin. Each basin drains to an underground storm drainage system. As shown in Appendix A, the weighted E method was used to quantify the peak rates generated within each basin. The underground drainage system drains to a detention pond located at the historical low point of the site. As shown in Appendix B, the inlets and drainage conduit are adequately sized. The proposed detention pond discharge 16.295 cfs via a 24" outfall pipe with a 16.5" orifice plate. This pond was modeled using AHYMO and the pond routing function. The input and output files of the model are included within Appendix C. As shown from the hydraulic pond model, the peak discharge leaving the site is throttled to 16.3 cfs during a 100-year, six hour storm event. A 24' wide emergency overflow has been included should the outlet become plugged. The proposed discharge rate leaving the site is

slightly greater than the rate of 16.01 cfs accounted for within the drainage plan for the westerly site. This increase of less than 0.3 cfs is insignificant and will be not have any adverse impact on the adjacent tract.

### SUMMARY AND RECOMMENDATIONS

This project consists of the development of an undeveloped site. The site is surrounded by streets that are fully developed. No significant offsite flows impact the site. The site currently discharges 21.16 cfs to the adjacent tract during a 100-year, 6-hour storm event. This flow passes through the adjacent site where it is captured by an permanent drainage structure and conveyed to the North Diversion Channel. The proposed development will discharge a peak rate of 16.3 cfs, while maintaining the existing drainage patterns. The adjacent tract was designed and approved to accept the flow from this site. The grading plan and drainage report was prepared in conformance with the City of Albuquerque Development Process Manual's drainage criteria. The existing and proposed storm discharge rates have been calculated using the City of Albuquerque's Weighted E method as prescribed in the DPM. The pond function was modeled using AHYMO 97. Since the proposed redevelopment of an existing site as shown within this plan do not adversely affects the upstream or downstream facilities, we recommend approval of the site-grading plan. Since this site encompasses more than 1 acre, a NPDES permit will be required prior to any construction activity.

Weighted E Method

Existing Basins

-Year	Flow	cfs	0 21.18	0 21.18
100-Y	Volume	(ac-ft)	0.680	0.680
	Weighted E	(ac-ft)	0.861	
	Freatment D	(acres)	1.422	1.422
	Treat	%	15%	
	Freatment C	(acres)	0.5688	0.5688
	Treat	%	6%	
	Treatment B	(acres)	1.422	1.422
	Trea	%	15%	
	reatment A	(acres)	6.0672	6.0672
	Treatn	%	64%	_
	Area	(acres)	9.48	9.48
	Area	(sf)	412805.05	412805.05
	Basin		ONSITE	Total

											1	100-Year, 6-hr.		10-day
Basin	Area	Area	Treatm	nent A	Treat	Treatment B	Treat	Treatment C	Treat	Treatment D	Weighted E	Volume	Flow	Volume
	(sf)	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(ac-ft)	(ac-ft)	cfs	(ac-ft)
A	35518.82	0.815	5%	0.04077	10%	0.082	2%	0.04077	80%	0.652	1.859	0.126	3.44	0.213
в	15424.60	0.354	2%	0.007082	3%	0.011	5%	0.01771	%06	0.319	1.999	0.059	1.59	0.101
ပ ပ	25234.31	0.579	2%	0.011586	5%	0.029	%9	0.03476	87%	0.504	1.962	0.095	2.56	0.162
0	7623.00	0.175	2%	0.0035	6%	0.011	8%	0.014	84%	0.147	1.929	0.028	0.76	0.048
ш	36024.12	0.827	10%	0.0827	20%	0.165	20%	0.1654	50%	0.414	1.498	0.103	2.97	0.158
  L_	7104.64	0.163	8%	0.013048	12%	0.020	20%	0.03262	80%	0.098	1.636	0.022	0.63	0.035
U	19514.88	0.448	1%	0.00448	4%	0.018	5%	0.0224	%06	0.403	2.001	0.075	2.01	0.128
6-1	30823.06	0.708	30%	0.21228	30%	0.212	20%	0.14152	20%	0.142	1.052	0.062	1.92	0.081
H(FUTURE)	95919.12	2.202	5%	0.1101	10%	0.220	10%	0.2202	75%	1.652	1.809	0.332	9.13	0.552
_	15472.51	0.355	30%	0.10656	20%	0.071	10%	0.03552	40%	0.142	1.285	0.038	1.11	0.057
_ ر	66337.52	1.523	20%	0.30458	30%	0.457	25%	0.38073	25%	0.381	1.159	0.147	4.50	0.198
J-1	16282.73	0.374	%0	0	5%	0.019	5%	0.01869	%06	0.336	2.004	0.062	1.68	0.107
×	16674.77	0.383	%0	0	5%	0.019	5%	0.01914	%06	0.345	2.004	0.064	1.72	0.110
	8842.68	0.203	8%	0.01624	18%	0.037	16%	0.03248	58%	0.118	1.596	0.027	0.76	0.043
M	16030.08	0.368	%0	0	5%	0.018	2%	0.0184	90%	0.331	2.004	0.061	1.66	0.106
Total	412826.83	9.48		0.91		1.39		1.19		5.98		1.30	36.45	2.10

# Equations:

Weighted E = Ea*Aa + Eb*Ab + Ec*Ac + Ed*Ad / (Total Area)

Volume = Weighted D * Total Area

Flow = Qa * Aa + Qb * Ab + Qc * Ac + Qd * Ad

Where for 100-year, 6-hour storm

Qa= 1.56	Qb= 2.28	Qc= 3.14	Qd= 4.7
Ea= 0.56	Eb= 0.78	Ec= 1.13	Ed= 2.12

# **VOLUME CALCULATIONS**

DETENTION POND

- Ab Bottom Of The Pond Surface Area
- At Top Of The Pond Surface Area
- D Water Depth
- Dt Total Pond Depth
- C Change In Surface Area / Water Depth

Volume =  $Ab * D + 0.5 * C * D^2$ C = (At - Ab) / Dt Ab = 2,080.00 At = 5,269.00 Dt = 6.25C = 510.24

ACTUAL	DEPTH	VOLUME	Q
ELEV.	(FT)	(AC-FT)	(CFS)
68.75	0	0	0.000
70.00	1.25	0.0597	3.997
70.75	2.00	0.0988	7.370
71.25	2.50	0.1285	8.937
71.75	3.00	0.1612	10.268
72.25	3.50	0.1968	11.445
72.75	4.00	0.2353	12.512
73.25	4.50	0.2767	13.495
73.75	5.00	0.3211	14.411
74.25	5.50	0.3684	15.272
74.75	6.00	0.4186	16.087
75.00	6.25	0.4449	16.479

Orifice Equation

Q = CA SQRT(2gH)

C =	0.6
Diameter (in	16.5
Area (ft^2)=	1.4848934
g =	32.2
H (Ft) =	Depth of water above center of orifice
Q (CFS)=	Flow

	CALCULATED Q	27.33	22.01	5.10	1.66	1.66	2.35	1.59	14.34	1.92	11.79	8.67	8.67	4.17	1.72	9.13	36.45
		2.97	2.56	3.44		1.66	0.76	1.59	0.63	1.92	3.12		4.50	2.45	1.72	9.13	
	CONTRIBUTING BASINS	ш	U	A		M	D	в	Ŀ	G-1	I,G		~	J1,L	¥	т	
21.18 cfs	CONTRIBUTING PIPES	13,1A	2,3	10	14		12		4,6		7	ω	6	11			
dition Discharge to adjacent tract	PIPE		1A	2	10	14	13	12	m	4	9	7	8	6	11	ъ	TOTAL FLOW TO POND
Existing Condition Discharge to	Developed Conditons	PIPE	BIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	TOTAL FLC

## Pipe Capacity

Pipe	D	Slope	Area	R	Q Provided	Q Required	Velocity
	(in)	(%)	(ft^2)		(cfs)	(cfs)	(ft/s)
1	30	0.6	4.91	0.625	31.86	27.33	5.57
1A	30	0.6	4.91	0.625	31.86	22.01	4.48
2	18	0.6	1.77	0.375	8.16	5.10	2.89
10	12	0.6	0.79	0.25	2.77	1.66	2.11
14	12	0.6	0.79	0.25	2.77	1.66	2.11
13	15	0.6	1.23	0.3125	5.02	2.35	1.91
12	12	0.6	0.79	0.25	2.77	1.59	2.02
3	24	0.6	3.14	0.5	17.57	14.34	4.56
4	12	0.6	0.79	0.25	2.77	1.92	2.44
6	24	0.6	3.14	0.5	17.57	11.79	3.75
7	18	0.6	1.77	0.375	8.16	8.67	4.91
8	18	0.6	1.77	0.375	8.16	8.67	4.91
9	15	0.6	1.23	0.3125	5.02	4.17	3.40
11	12	0.6	0.79	0.25	2.77	1.72	2.19
5	21	0.6	2.41	0.4375	12.31	9.13	3.80

<u>Manning's Equation:</u> Q = 1.49/n * A * R^(2/3) * S^(1/2)

A = Area

R = D/4S = Slope n = 0.013

LUNDER SIZED

# DROP INLET CALCULATIONS

INLET	TYPE OF	AREA	Q	Н	H ALLOW
	INLET	(SF)	(CFS)	(FT)	(FT)
ALL	Single 'D'	5.92	4.5	0.0249	0.5

**ORIFICE EQUATION** 

Q = CA  sqrt(2gH)	
C =	0.6
g =	32.2

### **Overflow Channel**

Weir Equation:

$$Q = CLH^{3/2}$$

Q= 36.45 cfsC = 2.95 H = 0.5 ft L = Length of weir

$$L = \frac{36.45}{2.95(0.5)^{3/2}} = 34.95'$$

L = 23.98 ft Use 24.00 feet for length of weir



24.00 ft

*****	*****	POND.txt	*****
	PASEO DEL NORTE SPO	ORTS PLEX	*
* 100-YEAR ******	, 6-HR STORM (PONI	DING CALCULATIONS	5)
START *	TIME=0.0		
* ROUTE 1 *			
* OVERALL SITE*			
RAINFALL	TYPE=1 RAIN QUARTE RAIN ONE=2.01 IN E RAIN DAY=2.75 IN E	RAIN SIX=2.35 IN	
COMPUTE NM HYD	ID=1 HYD NO=101.1 PER A=10.0 PER B=3 TP=-0.1333 HR MASS	L4.0 PER C=12.0 F	
* BASIN 1 PONDING *			
ROUTE RESERVOIR	ID=2 HYD NO=501.1 OUTFLOW(CFS) 0.0000 3.997 7.370 8.937 10.268 11.445 12.512 13.495 14.411 15.272 16.087 16.479	INFLOW ID=1 CODE STORAGE(AC-FT) 0.0000 0.0597 0.0988 0.1285 0.1612 0.1968 0.2353 0.2767 0.3211 0.3684 0.4186 0.4449	

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FINISH

- Version: 1997.02d AHYMO PROGRAM (AHYMO 97) -RUN DATE (MON/DAY/YR) = 12/28/2004START TIME (HR:MIN:SEC) = 17:27:31USER NO. = AHYMO-S-9702d2TierraW-AH INPUT FILE = C:\DOCUME~1\David\Desktop\2453\POND.txt PASEO DEL NORTE SPORTS PLEX 100-YEAR, 6-HR STORM (PONDING CALCULATIONS) TIME=0.0START * ROUTE 1 * OVERALL SITE* TYPE=1 RAIN OUARTER=0.0 IN RAINFALL RAIN ONE=2.01 IN RAIN SIX=2.35 IN RAIN DAY=2.75 IN DT=0.03333 HR COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR. 5.999400 HOURS .033330 HOURS END TIME = DT =.0084 .0000 .0016 .0033 .0049 .0066 .0102 .0199 .0219 .0241 .0139 .0158 .0178 .0120 .0286 .0309 .0333 .0358 .0384 .0411 .0263 .0529 .0561 .0596 .0467 .0497 .0631 .0439 .0866 .0669 .0709 .0751 .0807 .0930 .1066 .4644 .1371 .1840 .2514 .3434 .6186 .8106 1.0449 1.2624 1.3533 1.4300 1.4982 1.5602 1.6174 1.6704 1.7200 1.7664 1.8102 1.8514 1.8904 1.9273 1.9622 1.9953 2.0268 2.0566 2.0850 2.0915 2.0976 2.1033 2.1088 2.1140 2.1191 2.1239 2.1285 2.1329 2.1531 2.1568 2.1604 2.1373 2.1414 2.1454 2.1494 2.1832 2.1639 2.1673 2.1706 2.1739 2.1771 2.1802 2.1862 2.1891 2.1919 2.1947 2.1975 2.2002 2.2028 2.2054 2.2080 2.2105 2.2130 2.2154 2.2178 2.2202 2.2225 2.2248 2.2270 2.2293 2.2315 2.2336 2.2358 2.2379 2.2399 2.2420 2.2440 2.2460 2.2480 2.2500 2.2519 2.2538 2.2557 2.2576 2.2594 2.2612 2.2631 2.2648 2.2666 2.2684 2.2701 2.2718 2.2735 2.2752 2.2769 2.2785 2.2802 2.2818 2.2834 2.2850 2.2866 2.2881 2.2897 2.2912 2.2928 2.2943 2.2958 2.2973 2.2987 2.3002 2.3017 2.3031 2.3045 2.3060 2.3074 2.3088 2.3102 2.3115 2.3129 2.3143 2.3156 2.3169 2.3183 2.3196 2.3209 2.3222 2.3235 2.3248 2.3261 2.3323 2.3335 2.3273 2.3286 2.3298 2.3311 2.3348 2.3360 2.3372 2.3384 2.3396 2.3408 2.3419 2.3431 2.3443 2.3454 2.3466 2.3477 2.3488 2.3500 COMPUTE NM HYD

E NM HYD ID=1 HYD NO=101.1 AREA=0.0148125 SQ MI PER A=10.0 PER B=14.0 PER C=12.0 PER D=64.0 TP=-0.1333 HR MASS RAINFALL=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420

UNIT PEAK = 37.428 CFS UNIT VOLUME = .9991 B = 526.28 P60 = 2.0100AREA = .009480 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT - .033330

K = .131670HR TP = .133300HR K/TP RATIO = .987773 SHAPE CONSTANT, N = 3.574608UNIT PEAK = 13.031 CFS UNIT VOLUME = .9993 B = 325.73 P60 = 2.0100AREA = .005333 SQ MI IA = .49167 INCHES INF = 1.22667 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT

- .033330

* BASIN 1 PONDING

ROUTE RESERVOIR ID=2 HYD NO=501.1 INFLOW ID=1 CODE=24

ID=2 HID NO-501.1	THETOM ID-I COD	6-24
OUTFLOW (CFS)	STORAGE (AC-FT)	ELEVATION(FT)
0.0000	0.0000	68.75
3.997	0.0597	70.00
7.370	0.0988	70.75
8.937	0.1285	71.25
10.268	0.1612	71.75
11.445	0.1968	72.25
12.512	0.2353	72.75
13.495	0.2767	73.25
14.411	0.3211	73.75
15.272	0.3684	74.25
16.087	0.4186	74.75
16.479	0.4449	75.00

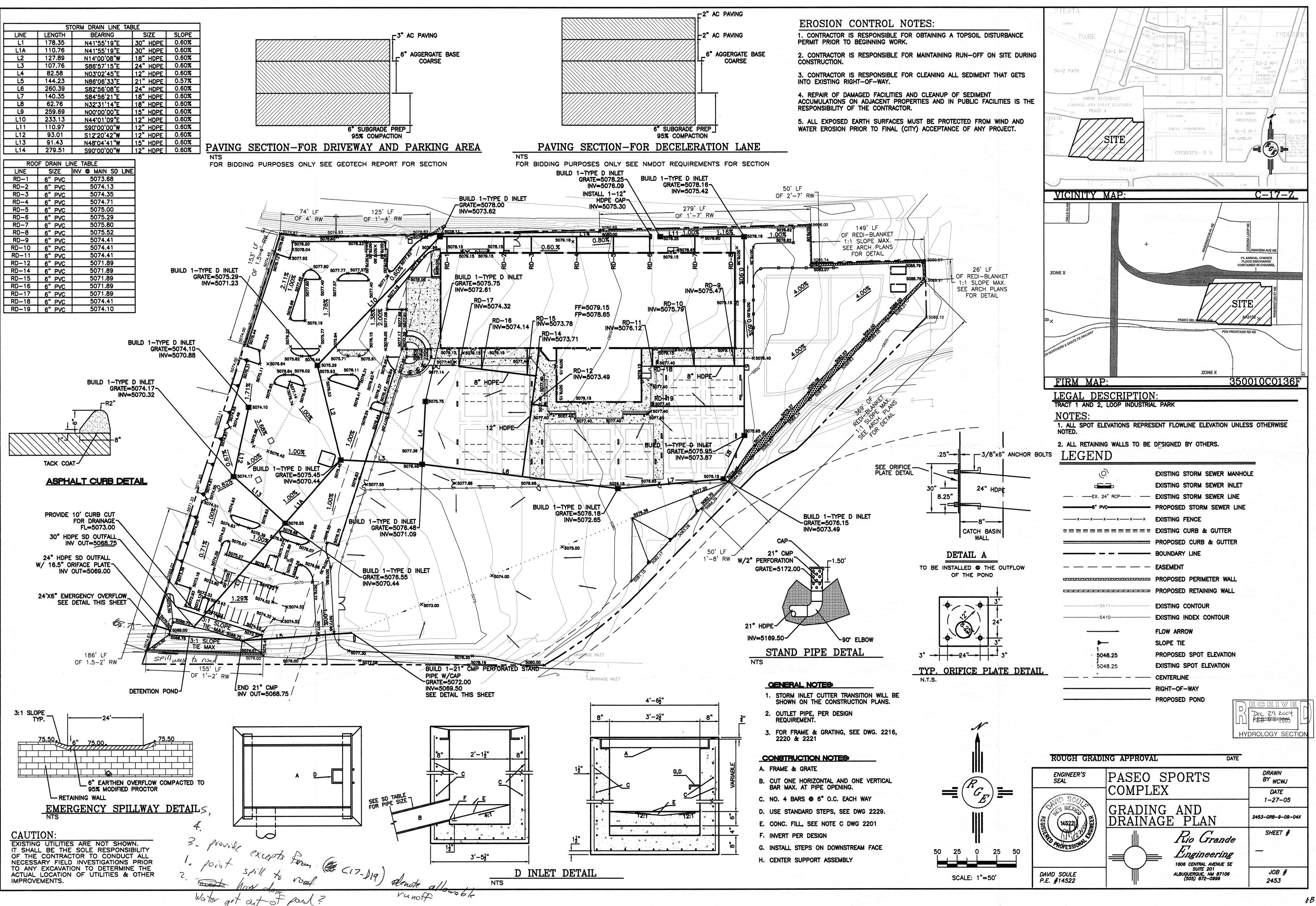
* * * *	* * *	* * * *	* * *	* * *	
TIME	INFLOW	ELEV	/OLUME	OUTFLOW	
(HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)	
.00	.00	68.75	.000	.00	
.80	.00	68.75	.000	.00	
1.60	25.87	74.51	.394	15.69	
2.40	1.48	70.47	.084	6.11	
3.20	.29	68.89	.007	.46	
4.00	.17	68.81	.003	.19	
4.80	.16	68.80	.002	.16	
5.60	.18	68.81	.003	.18	
6.40	.02	68.77	.001	.07	
7.20	.00	68.75	.000	.00	
PEAK DISCHAR	GE =	16.295 CFS	- PEAK O	CCURS AT HOUR	1.70
MAXIMUM WATER	R SURFACE	ELEVATION =	74	.883	
MAXIMUM STOR	AGE =	.4325 AG	C-FT	INCREMENTAL	TIME=
.033330HRS					

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### MAP POCKET A

## DRAINAGE BASIN MAP



1B