# CITY OF ALBUQUERQUE



March 10, 2005

David Soule, PE Rio Grande Engineering 1606 Central SE, Ste 201 Albuquerque, NM 87106

Re: Paseo del Norte Sportsplex Drainage Report Engineer's Stamp dated 12-29-04

Dear Mr. Soule,

Based upon the information provided in your submittal dated 12-29-04, the above referenced report is approved for Site Development Plan. Prior to Building Permit approval, please address the following comments.

P.O. Box 1293

- Please direct the emergency spillway toward Paseo del Norte.
- How does the runoff leave the pond? Does it daylight to the existing grade?

Albuquerque

• Please check the volumes of the pond – they appear small. This will probably affect the AHYMO run.

New Mexico 87103

• Pipes 7 and 8 are undersized. Also, please check your weir calculation.

• Please include exhibit from the previous report (C17-D19) showing allowable discharge to the property to the west.

www.cabq.gov

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE

Principal Engineer, Planning Dept. Development and Building Services

C: file

#### DRAINAGE REPORT

for

# Paseo Del Norte Sportsplex Albuquerque, New Mexico

Prepared by
Rio Grande Engineering
1606 Central Ave. SE, Suite 201
Albuquerque, New Mexico 87106

December 2004



DEC S. G. 2004
HYDROLOGY SECTION

David Soule P.E. No. 14522

#### **PURPOSE**

The purpose of this report is to provide the Drainage Management Plan for the development of indoor/ outdoor sports complex. The proposed development will consist of an approximately 56,000 square foot building, 11outdoor volley-ball courts, a miniature baseball field and their associated parking lot. The site contains 9.48 acres. This plan will identify the upstream and downstream hydraulic constraints affecting the subject property. This plan was prepared in accordance with the City of Albuquerque's Development Process Manual Drainage Criterion. This report will demonstrate that the proposed improvements do not adversely affect the surrounding properties, nor the upstream or downstream facilities.

#### INTRODUCTION

The subject of this report, as shown on the Exhibit A - vicinity map, is a 9.48-acre parcel of land located on the north side of Paseo Del Norte Avenue west of Washington Avenue NE. The site is currently undeveloped. The legal description of the parcel is tracts 1 & 2 Loop Industrial Park. The site is bounded by an inlet to the North AMAFCA Diversion Channel on the North, the Paseo Del Norte Frontage Road on the south, a railroad spur to the east and a partially developed parcel to the west. Due to the surrounding improvements, this site is not impacted by any significant offsite flow. The site currently discharges 21.16 cfs directly to the adjacent tract of land to the west of the site. A drainage plan (C17-D19) was completed for the adjacent tract which allows for 16.01cfs to leave enter this site from the subject site. Due to the existing drainage facilities and the fact the site is significantly lower than the adjacent AMAFCA channel and Paseo Del Norte, the existing patterns will be maintained and the development of this site shall be in conformance to the approved plan for the adjacent tract.

#### **EXISTING CONDITIONS**

This site is currently undeveloped. It appears this site has never been developed. The site is covered by native grasses and indigenous plants. The site drains from northeast to the southwest with general grades between 2-3 %. As shown in appendix A, the site currently discharges 21.16 cfs upon the adjacent westerly tract at the southwest corner of the site. This site and the adjacent site to the west are significantly lower than the adjacent roadway. Once the flow enters the adjacent tract, it combines with the developed flows and enters the North Diversion channel just west of the adjacent tract. Due to the existing grades, the adjacent site was designed to accommodate 16.01 cfs from this site. This report was prepared by BHI with a stamp date of April 22, 1998 and is located in C17-D19. This report defines this site as offsite basin B-1 and accounts for 16.01 cfs to discharge at the southern boundary. There no visual evidence that the existing drainage patterns have any negative impacts onsite or offsite.

#### PROPOSED CONDITIONS

As shown in Map Pocket A, the site contains a 15 drainage basin. Each basin drains to an underground storm drainage system. As shown in Appendix A, the weighted E method was used to quantify the peak rates generated within each basin. The underground drainage system drains to a detention pond located at the historical low point of the site. As shown in Appendix B, the inlets and drainage conduit are adequately sized. The proposed detention pond discharge 16.295 cfs via a 24" outfall pipe with a 16.5" orifice plate. This pond was modeled using AHYMO and the pond routing function. The input and output files of the model are included within Appendix C. As shown from the hydraulic pond model, the peak discharge leaving the site is throttled to 16.3 cfs during a 100-year, six hour storm event. A 24' wide emergency overflow has been included should the outlet become plugged. The proposed discharge rate leaving the site is

slightly greater than the rate of 16.01 cfs accounted for within the drainage plan for the westerly site. This increase of less than 0.3 cfs is insignificant and will be not have any adverse impact on the adjacent tract.

#### **SUMMARY AND RECOMMENDATIONS**

This project consists of the development of an undeveloped site. The site is surrounded by streets that are fully developed. No significant offsite flows impact the site. The site currently discharges 21.16 cfs to the adjacent tract during a 100-year, 6-hour storm event. This flow passes through the adjacent site where it is captured by an permanent drainage structure and conveyed to the North Diversion Channel. The proposed development will discharge a peak rate of 16.3 cfs, while maintaining the existing drainage patterns. The adjacent tract was designed and approved to accept the flow from this site. The grading plan and drainage report was prepared in conformance with the City of Albuquerque Development Process Manual's drainage criteria. The existing and proposed storm discharge rates have been calculated using the City of Albuquerque's Weighted E method as prescribed in the DPM. The pond function was modeled using AHYMO 97. Since the proposed redevelopment of an existing site as shown within this plan do not adversely affects the upstream or downstream facilities, we recommend approval of the site-grading plan. Since this site encompasses more than 1 acre, a NPDES permit will be required prior to any construction activity.

# Weighted E Method

Existing Basins

IOU-Teal	olume Flow	(ac-ft) cfs	0.680 21.18	0.680 21.18
	Weighted E \	(ac-ft)	0.861	
	reatment D	(acres)	1.422	1.422
	Treatr	%	15%	
	reatment C	(acres)	0.5688	0.5688
	Treat	%	%9	
	reatment B	(acres)	1.422	1.422
	Treat	%	15%	
	reatment A	(acres)	6.0672	6.0672
	Treatr	%	64%	
	Area	(acres)	9.48	9.48
	Area	(st)	412805.05	412805.05
	Basin		ONSITE	Total

Proposed Developed Basins

											100-Year, 6-hr.		10-day
Basin	Area	Area	Treatme	ment A	Treat	Treatment B	Treatment C		reatment D	Weighted E	Volume	Flow	Volume
	(st)	(acres)	%	(acres)	%	(acres)	% (acres)	% (s	(acres)	(ac-ft)	(ac-ft)	cfs	(ac-ft)
4	35518.82	0.815	%9	0.04077	10%	0.082	5% 0.0407	42 80%	6 0.652	1.859	0.126	3.44	0.213
В	15424.60	0.354	2%	0.007082	3%	0.011	5% 0.0177	71 90%	0.319	1.999	0.059	1.59	0.101
O	25234.31	0.579	2%	0.011586	2%	0.029	6% 0.03476	%28 92%	0.504	1.962	0.095	2.56	0.162
	7623.00	0.175	2%	0.0035	<b>%9</b>	0.011	8% 0.014	14 84%	6 0.147	1.929	0.028	0.76	0.048
ш	36024.12	0.827	10%	0.0827	20%	0.165	20% 0.1654	54 50%	0.414	1.498	0.103	2.97	0.158
L	7104.64	0.163	%8	0.013048	12%	0.020	20% 0.03262	62 60%	960.0	1.636	0.022	0.63	0.035
9	19514.88	0.448	1%	0.00448	4%	0.018	5% 0.0224	24 90%	6 0.403	2.001	0.075	2.01	0.128
6-1	30823.06	0.708	30%	0.21228	30%	0.212	20% 0.14152	52 20%	0.142	1.052	0.062	1.92	0.081
(FUTURE)	95919.12	2.202	2%	0.1101	10%	0.220	10% 0.2202	.02 75%	1.652	1.809	0.332	9.13	0.552
_	15472.51	0.355	30%	0.10656	20%	0.071	10% 0.03552	52 40%	6 0.142	1.285	0.038	1.11	0.057
5	66337.52	1.523	20%	0.30458	30%	0.457	25% 0.38073	73 25%	0.381	1.159	0.147	4.50	0.198
1-1	16282.73	0.374	%0	0	2%	0.019	5% 0.01869	%06 69	0.336	2.004	0.062	1.68	0.107
소	16674.77	0.383	%0	0	2%	0.019	5% 0.01914	14 90%	6 0.345	2.004	0.064	1.72	0.110
_	8842.68	0.203	8%	0.01624	18%	0.037	16% 0.03248	48 58%	6 0.118	1.596	0.027	92'0	0.043
Z	16030.08	0.368	%0	0	2%	0.018	5% 0.0184	84 90%	6 0.331	2.004	0.061	1.66	0.106
Total	412826.83	9.48		0.91		1.39	1.	1.19	5.98		1.30	36.45	2.10

# Equations:

Weighted E = Ea\*Aa + Eb\*Ab + Ec\*Ac + Ed\*Ad / (Total Area)

Volume = Weighted D \* Total Area

Flow = Qa \* Aa + Qb \* Ab + Qc \* Ac + Qd \* Ad

Where for 100-year, 6-hour storm
Ea= 0.56
Eb= 0.78
Ec= 1.13
Ed= 2.12

Qa= 1.56 Qb= 2.28 Qc= 3.14 Qd= 4.7

# **VOLUME CALCULATIONS**

#### **DETENTION POND**

Ab - Bottom Of The Pond Surface Area

At - Top Of The Pond Surface Area

D - Water Depth

Dt - Total Pond Depth

C - Change In Surface Area / Water Depth

Volume = 
$$Ab * D + 0.5 * C * D^2$$
  
C =  $(At - Ab) / Dt$ 

Ab = 2,080.00

At = 5,269.00 Dt = 6.25

C = 510.24

ACTUAL	DEPTH	VOLUME	Q
ELEV.	(FT)	(AC-FT)	(CFS)
68.75	0	0	0.000
70.00	1.25	0.0597	3.997
70.75	2.00	0.0988	7.370
71.25	2.50	0.1285	8.937
71.75	3.00	0.1612	10.268
72.25	3.50	0.1968	11.445
72.75	4.00	0.2353	12.512
73.25	4.50	0.2767	13.495
73.75	5.00	0.3211	14.411
74.25	5.50	0.3684	15.272
74.75	6.00	0.4186	16.087
75.00	6.25	0.4449	16.479

CHECK NOTUNE

CALCS

0.5272 16.863

#### Orifice Equation

Q = CA SQRT(2gH)

C =

Diameter (in) 16.5

Area (ft $^2$ )= 1.4848934

g = 32.2

H(Ft) = Depth of water above center of orifice

0.6

Q(CFS)= Flow

	21.18 cfs
Existing Condition	Discharge to adjacent tract

	CALCULATED Q	27.33	22.01	5.10	1.66	1.66	2.35	1.59	14.34	1.92	11.79	8.67	8.67	4.17	1.72	9.13	36.45
		2.97	2.56	3.44		1.66	0.76	1.59	0.63	1.92	3.12		4.50	2.45	1.72	9.13	
	CONTRIBUTING	ш	ပ	∢		Σ	Q	B	UL.	6-1	j'e		7	J1,L	¥	I	
21.18 cfs	CONTRIBUTING	13,1A	2,3	10	14		12		4,6		7	∞	6	7			
Discharge to adjacent tract	- 1010		14	2	10	4	13	12	က	4	9	7	ω	တ	7	က	TOTAL FLOW TO POND
Discharge to	Pour productions	Developed Conditions PIPE	BIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	PIPE	TOTAL FLC

# Pipe Capacity

Pipe	D	Slope	Area	R	Q Provided	Q Required	Velocity
	(in)	(%)	(ft^2)		(cfs)	(cfs)	(ft/s)
1	30	0.6	4.91	0.625	31.86	27.33	5.57
1A	30	0.6	4.91	0.625	31.86	22.01	4.48
2	18	0.6	1.77	0.375	8.16	5.10	2.89
10	12	0.6	0.79	0.25	2.77	1.66	2.11
14	12	0.6	0.79	0.25	2.77	1.66	2.11
13	15	0.6	1.23	0.3125	5.02	2.35	1.91
12	12	0.6	0.79	0.25	2.77	1.59	2.02
3	24	0.6	3.14	0.5	17.57	14.34	4.56
4	12	0.6	0.79	0.25	2.77	1.92	2.44
6	24	0.6	3.14	0.5	17.57	11.79	3.75
7	18	0.6	1.77	0.375	8.16	8.67	4.91
8	18	0.6	1.77	0.375	8.16	8.67	4.91
9	15	0.6	1.23	0.3125	5.02	4.17	3.40
11	12	0.6	0.79	0.25	2.77	1.72	2.19
5	21	0.6	2.41	0.4375	12.31	9.13	3.80

<u>Manning's Equation:</u>
Q = 1.49/n \* A \* R^(2/3) \* S^(1/2)

A = Area

R = D/4 S = Slope n = 0.013

# **DROP INLET CALCULATIONS**

INLET	TYPE OF	AREA	Q	Н	H ALLOW
	INLET	(SF)	(CFS)	(FT)	(FT)
ALL	Single 'D'	5.92	4.5	0.0249	0.5

# ORIFICE EQUATION

 $Q = CA \ sqrt(2gH)$ 

C =

0.6

g =

32.2

### **Overflow Channel**

#### Weir Equation:

$$Q = CLH^{3/2}$$

Q = 36.45 cfs

 $\hat{C} = 2.95$ 

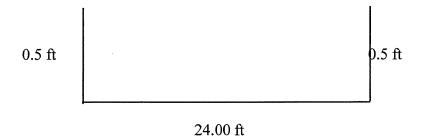
H = 0.5 ft

L = Length of weir

$$L = \frac{36.45}{2.95(0.5)^{3/2}} = 34.95'$$

L = 23.98 ft

Use 24.00 feet for length of weir



		ND.txt	
*******	******	*******	
	PASEO DEL NORTE SPORT		* ********
* 100-YEAR	, 6-HR STORM (PONDIN	NG CALCULATION	S) * *******
START *	TIME=0.0		
* ROUTE 1 *			
* OVERALL SITE*			
RAINFALL	TYPE=1 RAIN QUARTER=	=0.0 IN	
	RAIN ONE=2.01 IN RAI		
	RAIN DAY=2.75 IN DT=		
COMPUTE NM HYD	ID=1 HYD NO=101.1 AF		
	PER A=10.0 PER B=14.		PER D=64.0
± 1	TP=-0.1333 HR MASS F	RAINFALL=-1	
* BASIN 1 PONDING *			
ROUTE RESERVOIR	ID=2 HYD NO=501.1 IN		
	OUTFLOW(CFS) ST		ELEVATION(FT)
	0.0000	0.0000	68.75
	3.997	0.0597	70.00
	7.370	0.0988	70.75
	8.937 10.268	0.1285	71.25 71.75
	10.208	0.1612 0.1968	71.73
	12.512	0.1966	72.75
	13.495	0.2353	73.25
	14.411	0.3211	73.75
	15.272	0.3684	74.25
	16.087	0.4186	74.75
	16.479	0.4449	75.00
	<del>-</del>		
*			

\* \*

FINISH

- Version: 1997.02d AHYMO PROGRAM (AHYMO 97) -RUN DATE (MON/DAY/YR) = 12/28/2004START TIME (HR:MIN:SEC) = 17:27:31USER NO. = AHYMO-S-9702d2TierraW-AH INPUT FILE = C:\DOCUME~1\David\Desktop\2453\POND.txt

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* PASEO DEL NORTE SPORTS PLEX \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* 100-YEAR, 6-HR STORM (PONDING CALCULATIONS) \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* TIME=0.0

START

\* ROUTE 1

\* OVERALL SITE\*

RAINFALL

TYPE=1 RAIN QUARTER=0.0 IN RAIN ONE=2.01 IN RAIN SIX=2.35 IN RAIN DAY=2.75 IN DT=0.03333 HR

COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2

- PEAK AT 1.40 HR.

DT =	.033330 но	OURS	END T	IME =	5.9994	00 HOURS
.0000	.0016	.0033	.0049	.0066	.0084	.0102
.0120	.0139	.0158	.0178	.0199	.0219	.0241
.0263	.0286	.0309	.0333	.0358	.0384	.0411
.0439	.0467	.0497	.0529	.0561	.0596	.0631
.0669	.0709	.0751	.0807	.0866	.0930	.1066
.1371	.1840	.2514	.3434	.4644	.6186	.8106
1.0449	1.2624	1.3533	1.4300	1.4982	1.5602	1.6174
1.6704	1.7200	1.7664	1.8102	1.8514	1.8904	1.9273
1.9622	1.9953	2.0268	2.0566	2.0850	2.0915	2.0976
2.1033	2.1088	2.1140	2.1191	2.1239	2.1285	2.1329
2.1373	2.1414	2.1454	2.1494	2.1531	2.1568	2.1604
2.1639	2.1673	2.1706	2.1739	2.1771	2.1802	2.1832
2.1862	2.1891	2.1919	2.1947	2.1975	2.2002	2.2028
2.2054	2.2080	2.2105	2.2130	2.2154	2.2178	2.2202
2.2225	2.2248	2.2270	2.2293	2.2315	2.2336	2.2358
2.2379	2.2399	2.2420	2.2440	2.2460	2.2480	2.2500
2.2519	2.2538	2.2557	2.2576	2.2594	2.2612	2.2631
2.2648	2.2666	2.2684	2.2701	2.2718	2.2735	2.2752
2.2769	2.2785	2.2802	2.2818	2.2834	2.2850	2.2866
2.2881	2.2897	2.2912	2.2928	2.2943	2.2958	2.2973
2.2987	2.3002	2.3017	2.3031	2.3045	2.3060	2.3074
2.3088	2.3102	2.3115	2.3129	2.3143	2.3156	2.3169
2.3183	2.3196	2.3209	2.3222	2.3235	2.3248	2.3261
2.3273	2.3286	2.3298	2.3311	2.3323	2.3335	2.3348
2.3360	2.3372	2.3384	2.3396	2.3408	2.3419	2.3431
2.3443	2.3454	2.3466	2.3477	2.3488	2.3500	

COMPUTE NM HYD

ID=1 HYD NO=101.1 AREA=0.0148125 SQ MI PER A=10.0 PER B=14.0 PER C=12.0 PER D=64.0 TP=-0.1333 HR MASS RAINFALL=-1

K = .072649HR TP = .133300HR K/TP RATIO = .545000 SHAPE CONSTANT, N = 7.106420

UNIT PEAK = 37.428 CFS UNIT VOLUME = .9991 B =

P60 = 2.0100

AREA = .009480 SQ MI IA = .10000 INCHES INF = .04000

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033330

K = .131670HR TP = .133300HR K/TP RATIO = .987773

SHAPE CONSTANT, N = 3.574608

UNIT PEAK = 13.031 CFS UNIT VOLUME = .9993

P60 = 2.0100

AREA = .005333 SQ MI IA = .49167 INCHES INF = 1.22667

INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033330

#### \* BASIN 1 PONDING

-	~ FT M M	 0 = =	 -

ROUTE	RESERVOIR	ID=2 HYD NO=501.1	INFLOW ID=1 COD	E=24
		OUTFLOW(CFS)	STORAGE (AC-FT)	ELEVATION (FT)
	•	0.0000	0.0000	68.75
		3.997	0.0597	70.00
		7.370	0.0988	70.75
		8.937	0.1285	71.25
		10.268	0.1612	71.75
		11.445	0.1968	72.25
		12.512	0.2353	72.75
		13.495	0.2767	73.25
		14.411	0.3211	73.75
		15.272	0.3684	74.25
		16.087	0.4186	74.75
		16.479	0.4449	75.00

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
.00	.00	68.75	.000	.00
.80	.00	68.75	.000	.00
1.60	25.87	74.51	.394	15.69
2.40	1.48	70.47	.084	6.11
3.20	.29	68.89	.007	.46
4.00	.17	68.81	.003	.19
4.80	.16	68.80	.002	.16
5.60	.18	68.81	.003	.18
6.40	.02	68.77	.001	.07
7.20	.00	68.75	.000	.00

PEAK DISCHARGE = 16.295 CFS - PEAK OCCURS AT HOUR 1.70

MAXIMUM WATER SURFACE ELEVATION = 74.883

MAXIMUM STORAGE = .4325 AC-FT INCREMENTAL TIME=

.033330HRS

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 17:27:31

# MAP POCKET A DRAINAGE BASIN MAP

