

GRAPHIC SCALE

(IN FEET)

المستهمين ويستداء الرازي والمناهية والمسهوات المادات والماسا

 $1'' = 20 \, \text{FT}$ 

**CURB RADIUS DATA** LEGEND R1 = 1'-6"NEW 16' TALL POLE LIGHT W/ 50 WATT CERAMIC R2 = 2'-0"METAL HALIDE LAMPING R3 = 3'-0"(FULL CUT-OFF, SHOE R5 = 5'-0"BOX TYPE.) R8 = 8'-0"R10 = 10'-0''EXISTING FIRE HYDRANT R15 = 15'-0"R20 = 20'-0"R25 = 25'-0"R50 = 50'-0''RADIUS MEASURED TO OUTSIDE FACE OF CURB

### SITE CALCULATIONS

USE: OFFICE

PROPERTY AREA: 54,073 SF (1.2413 AC) GROSS BLDG AREA: 13,704 SF (25%) NET LEASABLE AREA: 9,736 SF LANDSCAPE AREA: 8,623 SF (16%) R.O.W. LANDSCAPING: 553 SF PAVING & SIDEWALK AREA: 31,746 SF (59%)

GROSS PARKING SPACES REQUIRED: 13,704/200 = 69 (LESS 5% BUS ROUTE CREDIT) = 3 TOTAL PARKING SPACES REQUIRED = 66

PARKING SPACES PROVIDED: 62 + 4 HC (2 VAN ACCESSIBLE) = 66 BIKE RACK SPACES PROVIDED: 3

ADDRESS: 8500 JEFFERSON ST., NE ALBUQUERQUE, NM 87113

LEGAL DESCRIPTION:
LOT 14-A-2-A OF UNIT V, LOOP INDUSTRIAL DISTRICT, ALBUQUERQUE, NEW MEXICO, AS THE SAME IS SHOW
AND DESIGNATED ON THE PLAT THEREOF, FILED IN THE OFFICE OF THE COUNTY CLERK OF BERNALILLO COUNTY, NEW MEXICO ON JANUARY 3, 1997, IN PLAT BOOK 97C, FOLIO 2

ZONING SU-2 FOR M-1

LEGAL NOTES: 1. CITY OF ALBUQUERQUE UPC NO. 1-017-064-367-234-40256

2. SUBJECT PROPERTY IS LOCATED WITHIN FLOOD ZONE X, DESIGNATING AREAS DETERMINED TO BE OUTSIDE THE 500-YEAR FLOODPLAIN ACCORDING TO THE FLOOD INSURANCE RATE MAP, BERNALILLO COUNTY, NEW MEXICO AND INCORPORATED AREAS PER MAP NO. 35001C02137F, EFFECTIVE DATE.

GENERAL NOTES [C1.1] ALL STANDARD PARKING SPACES SHALL BE 8-6W X 20-0'D

[C1.2] ALL HANDICAP PARKING SPACES SHALL BE 8'-O'W X 20'-O'D WITH ADJACENT 5W STRIPED ACCESS AISLE ( 1 VAN ACCESSIBLE SPACE PER PROPERTY SHALL HAVE AN 8 WIDE ACCESS AISLE). ALL SPACES SHALL HAVE POLE SIGN AND HANDICAP SYMBOL PAVEMENT MARKINGS.

[C1.3] ALL PARKING SPACES, HANDICAP SYMBOLS AND CROSS HATCHED ACCESS AISLES SHALL BE MARKE ON PAVEMENT WITH WHITE ALKYD STRIPING PAINT, TYP.

IC1.4] ALL PARKING SPACES ABUTTING A SIDEWALK SHALL BE PROVIDED WITH A PRECAST CONCRETE PAKING BUMPER LOCATED 2'-0" OFF THE SIDEWALK

KEYED NOTES
[1] ASPHALT PAVED SURFACE - SEE DETAIL 1/C1.1

[2] CONCRETE CURB & GUTTER, - SEE DETAILS 2/C1.1

(3) CONCRETE SIDEWALK - SEE DETAIL 4/C1.1 - TYPICAL SIDEWALK WIDTH SHALL BE 6'-0' UNLESS NOTED OTHERWISE.

[4] SIDEWALK RAMP - SEE DETAIL 3/C1.1

[5] SIDEWALK RAMP W/ FLAIRS - SEE DETAIL 6/C1.1

[6] PUBLIC SIDEWALK PER CITY OF ALBUQUERQUE STANDARDS DRAWING 2430 "STPEWALL" DI

[7] PUBLIC SIDEWALK ADA ACCESS RAMP PER CITY OF ALBUQUEROUE STANDARD DRAWNG 2441 [8] CAST IN PLACE CONCRETE DUMPSTER ENCLOSURE W/ GATES - SEE DETAIL 128/13/C1.1

[9] PRECAST CONCRETE BIKE RACK SET IN SIDEWALK - SEE DETAIL 10/C1 1 [10] HANDICAP PARKING SPACE SIGN - ONE SIGN PER HANDICAP PARKING SPACE, TYP. - SEE DETAIL 8/C1.

[11] EXISTING CONCRETE BOLL CURB TO BEMAIN

[12] 16 TALL POLE LIGHT WITH FULL CUT-OFF SHOE BOX TYPE CANOPY [13] CONCRETE STAIR WITH HAND RAILS - SEE DETAIL 7/C1 1

[14] TRANSFORMER ON CONCRETE PAD PER PNM REQUIREMENTS

[15] CONCRETE ELEC. METER/TRANFORMER SCREEN WALL - SEE DETAIL 9/C1.1 (SMOOTH CONCRETE FINE ON METER MOUNTING FACE OF WALL)

[16] CONCRETE ROLL CURB - SEE DETAIL 5/C1.1

[17] PRECAST CONCRETE PARKING BUMPERS - SET 2-0" OFF FACE OF SIDEWALK

[18] MONUMENT SIGN - SEE DETAIL 16/C1.1

**VICINITY MAP/AERIAL** 

STANDARD DRAWING 2415A "CURB [19] NEW CURB CUT PER CITY OF ALBUQUERQUE SP GUTTER AND CUPB CUT (20) EXISTING CURB CUT TO REMAIN - 24 0 LIDE

1004326 PROJECT NUMBER:

APPLICATION NUMBER: 050PB-01147

IS AND INFRASTRUCTURE LIST REQUIRED? ( ) YES ( ) NO. IF YES, THEN A SET OF APPROVED DRC PLANS WITH A WORK ORDER IS REQUIRED FOR ANY CONSTRUCTION WITHIN PUBLIC RIGHT-OF-WAY OR FOR CONSTRUCTION OF PUBLIC IMPROVEMENTS

DRB SITE DEVELOPMENT PLAN APPROVAL:

7-27.05 DATE GINEERING TRANSPORTATION DIVISION 72-27-05 7/27/05 DATE 7/27/05 **ENVIRONMENTAL HEALTH DEPARTMENT (conditional)** Michael Holton SOLID WASTE MANAGEMENT

7/27/05 DATE 7/27/05

JUL 1 0 2006

HYDROLOGY SECTION

INSITE: WORKS

KNIGHT L

SEAVEY

ALBUQUERQUE, NM 87122 888.781.0154 WEBSITE | insiteworks.com EMAIL knightfäinsiteworks.com

PG. C-17 1"= 100

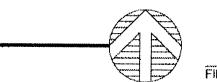
THIS DRAWING IS THE PROPERTY OF INSITE WORKS AND SHALL NOT BE REPRODUCED OR USED IN ANY WAY WITHOUT EXPRESSED WRITTEN CONSENT

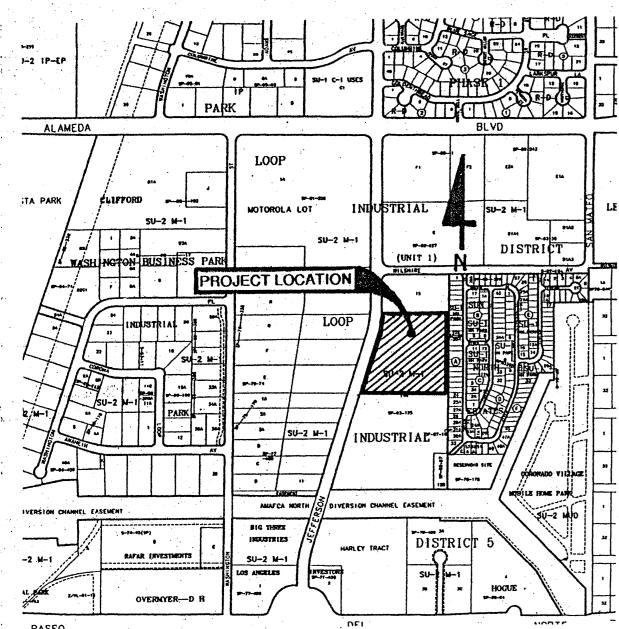
> Lot 14-A-2-A **Loop Industrial District**

PROJECTIO JLM JLM Investments 8500 Jefferson St. NE

C1.0DRE

SITE PLAN SCALE: 1"==20"





LEGAL DESCRIPTION TRACT A-14-2 LOOP INDUSTRIAL TRACT U', TO

# BENCH MARKS:

ACS BRASS CAP-"LOOP INDUSTRIAL DISTRICT UNIT IV" JEFFERSON/WILSHIRE FIFVATION = 5131.89

AMAFCA BRASS CAP "NDC 7-1B2" ELEVATION = 5064.40 PLANNED DEVELOPMENT

Development planned for Tract 14-A-2, Unit 5, Loop Industrial Tract consists of subdividing the existing 9.4 +/- acre parcel into lots and constructing an industrial park. The property is zoned SU-2/M1. A private access road is planned which provides six lots access to Jefferson Street: The remaining three lots access Jefferson Street via private turnouts. This Drainage and Grading Plan for subdivision recommends drainage management and infrastructure improvements necessary to support the planned development.

The project is located on Jefferson Street between Paseo Del Norte and Wilshire Avenue, in northeast Albuquerque, New Mexico. Existing terrain consists predominately of mild slopes, 1%-3%, with minimal vegetation. The property generally slopes from east to west. The property is not located in a F.E.M.A. flood plain.

#### EXISTING HYDROLOGIC CONDITIONS

The site is currently undeveloped. The site receives off-site flows from a portion of the mobile home park (1:9 acres) adjacent to its east property line. The remaining runoff originating at the mobile home park is diverted by Brook Street and drained southward to the North Diversion Channel. Flows generated by the site, including off-site flows, drain into Jefferson Street (west), where they are directed south to the AMAFCA North Diversion Channel. A curb drop inlet, approximately 100' south of the site's south property line, accepts flows from Jefferson Street and discharges them to the North Diversion Channel via a 24"/30" storm drain. Excess flow, above the capacity of the curb drop inlet, drains south on Jefferson Street until the AMAFCA North Diversion Channel is reached 550' south of the curb drop inlet. At the site's north property line, Jefferson Street reaches a high point that provides a water block from runoff originating north of the site. Properties to the west drain westerly. The stretch of Jefferson Street between the sites north property line and the AMAFCA North Diversion Channel receives flow from the subject site, including its off-site basin, and 12.8 +/- acres just south of the site. A curb drop inlet connected to a 30" storm sewer is in place at the southwest corner (along Jefferson Street) of the 12.8 acre basin.

PURPOSE OF DRAINAGE AND GRADING PLAN FOR SUBDIVISION This plan presents necessary drainage and grading improvements required to support subdivision into parcels and the subsequent planned development. In addition, the plan accommodates a phased implementation process for development. As lots are purchased and developed, each lot will be required to submit a detailed grading plan that is intended to function as prescribed by this Drainage and Grading Plan. Submittal of detailed grading plans to the City Hydrology Department for grading plan review and approval, will be required. The grading plans will be stand alone construction documents that include detailed drainage and grading elements, proposed building foot print, foundation

elevations, parking areas, landscape areas, roof drains, drainage swales, sidewalk culverts, etc.

Future plans will not be required to address hydrologic analysis except for designing and sizing minor drainage structures such as swales, rundowns, and sidewalk culverts. Pro-rating flow rates established by this plan based on basin area will be an acceptable method for determining these flow rates. Lots X X and X must incorporate a pro-ration of off-site flows based on the percentage of frontage each lot shares with the mobile home park to the east. B. E & H

On-site hydrologic analysis is provided in order to determine flow rates conveyed by interior streets, swales, rundowns, and curb drains. Under existing, undeveloped conditions the site is 100% land treatment C, yielding 29.5 and 16.1 cfs for the 100 year and 10 year storm events, respectively. Under proposed conditions the site consists of 30% land treatment C and 70% land treatment yielding 39.8 cfs and 25.5 cfs for the 100 year and 10 year-storm events, respectively. Lots X and xaccept off-site flows from the a portion of the mobile home park (1.9 ac.) to the east. Under both existing, undeveloped and developed conditions the off-site basin is 40% land treatment B and 60% land treatment D. yielding 7.1 and 4.3 cfs for the 100 year and 10 year storm events, respectively.

### DEVELOPMENT IMPLEMENTATION AND PHASING

It is planned to build the private access road in conjunction with the first lot constructed. The private access road is available to convey flows generated by lots XXX and X At this time it is unknown which lot will be constructed first. The private access road will be located in a feat. Private Access and Drainage Easement.

Lot Xmay either discharge runoff to the private access road or directly to Jefferson Street via sidewalk culverts. Lots X and Xwill discharge to the private access road. Lot Xmay discharge to Jefferson Street via sidewalk culverts or to the drainage easement along its north property line. Lot Xwill discharge to the 10' private drainage easement crossing lots X and X Lot 6 will discharge directly to Jefferson Street via sidewalk oulverts. Lot may discharge to Jefferson Street via sidewalk culverts or to the drainage easement along its south property line. Lot & G discharges to the 10' private drainage easement crossing the south side of lot XA sidewalk culvert will be required at the outlets of the 10' drainage easements. All sidewalk culverts must be sized and designed accordingly along with the site specific plan.

provisions of the North I-25 Sector Development require minimum 6' landscape buffers along all side and rear property lines. Flow in private drainage easements located in these landscape buffers shall be contained within a concrete rundown or an appropriately sized landscaped wale. (See Hydraulic Calculations.)

It is planted to grade the site in a phased manner. Areas that are disturbed during construction but do not receive a permanent surface treatment will be required to install erosion control berms, or silt fences and shall be required to revegetate disturbed areas. These measures will be shown as the lot specific grading plans and shall be an integral part of the Top Soil Disturbance Permit. Revegetation will be of a permanent type designed to City of Albuquerque Minimum Specifications for Public Works Construction.

## COMPUTATIONS

HYDROLOGY Analysis per COA DPM Chapter 22.2, HYMO Peak Discharge Method, zone 2. Design Storm 100 year - 6 hour event Applied Rainfall is 2.35 inches (table 2)

10 year - 6 hour event Applied Rainfall is 2.35 inches x 0.67 = 1.57 inches (table 3) Runoff/Acre

100 year: B Treatment = 2.28 cfs/ac., C Treatment = 3.14 cfs/ac., D Treatment =, 4.70 cfs/ac. 10 year: B Treatment = 0.95 cfs/ac., C Treatment = 1.71 cfs/ac., D Treatment = 3.14 cfs/ac.

### Basin A (Subject Site - 9.4 acres zoned light industrial) Land Treatments

**Existing Conditions** 100.0% Treatment C Proposed Conditions

30% Treatment C and 70% Treatment D Peak Discharge

**Existing Conditions** 100 year = 9.4 acres x (1.00x 3.14 cfs/ac.) = 29.5 cfs10 year = 9.4 acres x (1.00x 1.71 cfs/ac.) = 16.1 cfs

100 year =  $9.4 \text{ acres } x (0.30x \ 3.14 \ \text{cfs/ac.} + 0.70x4.70 \ \text{cfs/ac.}) = 39.8 \ \text{cfs}$ 10 year = 9.4 acres x (0.30x 1.71 cfs/ac. + 0.70x3.14 cfs/ac.) = 25.5 cfs

## Basin 8 (Off-site Basin Site - 1.9 acre mobile home park east of site)

Existing and Proposed Conditions 40% Treatment B and 60% Treatment D

Teak Discharge **Existing and Proposed Condition** 

100 year = 1.9 acres x (0.40x 2.28 cfs/ac. + 0.60x4.70 cfs/ac.) = 7.1 cfs10 year = 1.9 acres x (0.40x 0.95 cfs/ac. + 0.60x3.14 cfs/ac.) = 4.3 cfs

Basin C (Off-site Basin Site - 0.7 acres of Jefferson Street - south of the subject site's north property line 16 100' south of the site's southern property line-approximate location of a curb drop inlet.)

Eisting and Proposed Conditions 32.6% Treatment B and 67.4% Treatment D Peak Discharge

## Existing and Proposed Conditions

100 year = 0.7 acres x (0.326x 2.28 cfs/ac. + 0.674x4.70 cfs/ac.) = 2.6 cfs 10 year = 0.7 acres x  $(0.326 \times 0.95 \text{ cfs/ac.} + 0.674 \times 3.14 \text{ cfs/ac.}) = 1.8 \text{ cfs}$ 

Basin D (Site South of Subject Site - 12.8 acres includes 0.7 acres of mobile home park and 2.5 acres of future reservoir site, the remaining will be developed as light industrial)

#### Land Treatments Existing Conditions

2% Treatment B, 95% Treatment C, 3% Treatment D

2% Treatment B, 42% Treatment C, 56% Treatment D Peak Discharge

100 year = 12.8 acres x (0.02x 2.28 cfs/ac. + 0.95x3.14 cfs/ac. + 0.03x 4.70) = 40.5 cfsExisting Conditions 10 year = 12.8 acres x (0.02x 0.95 cfs/ac. + 0.95x1.71 cfs/ac. + 0.03x 3.14) = 22.8 cfs

100 year = 12.8 acres x (0.02x 2.28 cfs/ac. + 0.42x3.14 cfs/ac. + 0.56x 4.70) = <math>51.1 cfs10 year = 12.8 acres x  $(0.02x \ 0.95 \ cfs/ac. + 0.42x1.71 \ cfs/ac. + 0.56x \ 3.14) = 31.9 \ cfs$ 

Basin E (Off-site Basin Site - 0.6 acres of Jefferson Street - 100' south of the subject site's southern property lineto the North Diversion Channel approximate location of a curb drop inlet.)

#### Land Treatments Existing and Proposed Conditions 32.6% Treatment B and 67.4% Treatment D

Peak Discharge Existing and Proposed Condition

10 year = 0.6 acres x  $(0.326x \ 0.95 \ cfs/ac. + <math>0.674x3.14 \ cfs/ac.) = 1.5 \ cfs$ 

100 year = 0.6 acres x (0.326x 2.28 cfs/ac. + 0.674x4.70 cfs/ac.) = 2.2 cfs

STREET HYDRAULICS Runoff Capacity of Jefferson Street

Street flow depths during peak flow were calculated using Manning's equation. Conjugate depths were calculated for flows in the super-critical state, should conditions be conducive to the formation a hydraulic jump

1) only the two torth-bound lanes could be used due to the median, 2) n = 0.017 for the roadway surface, 3) road cross slope = 2.00%, 4) curb to curb distance = 25', 5) outside curb to inside driving lane = 13 ft, 6) eight inch curbs.

To establish DPM criteria flows the following parameters were used: 10 year-storm: one lane dry, max. flow depth = 0.5'

100 year-storm: max. flow depth = 0.87'

The relevant stretch of Jefferson Street has two slope regions: a flatter region fronting the subject site with an average slope 0.85%, and a steeper region with an average slope of 1.60% south of the subject property. Two curb drop inlets service Jefferson Street between the subject site and the North Diversion Channel; at point A and point B, 100 ft and 550 ft south of the subject site, respectively. Analyses were performed to determine peak flow and the resulting flow height within Jefferson Street both immediately before and after interception of flow at each curb drop inlet site. It was assumed 100% of the runoff from basins A, B, and C drain to the curb drop inlet at point A. Inlet capacity was computed to determine the pro-ration of flows intercepted by the curb drop inlet. Basin D was assumed to form two sub-basins; one (1/3 of basin D) discharging upstream of the curb drop inlet at analysis point B and the other (the remaining 2/3 of basin D) discharging immediately downstream of the curb drop inlet at point B. The analysis at point B assumed that the carry-over from the curb drop inlet at point A, the entire basin E, and the upper 1/3 of basin D comprised the peak discharge immediately upstream of the curb drop inlet. The carry-over from the curb drop inlet at point B and the runoff from the remaining 2/3 of basin D comprise the peak flow immediately below point B. The table below summarizes the results of these analyses:

Point of Analysis	Storm Event/Condition	Max. Depth in Street * (ft.)	Peak Street Flow (cfs)	Peak Storm Sewer Flow (cfs)
Point A	10 year storm-DPM criteria	0.26	3.4	
Jefferson St. 100' south of subject site-	-existing conditions	0.52	22.2	
prior to curb drop inlet	-proposed conditions	0.61	31.6	
(street slope = 0.0085 ft/ft)	100 year storm-DPM criteria	0.87	58.8	
	-existing conditions	0.70	39.6	****
	-proposed conditions	0.80	49.5	
Point A	10 year storm-DPM criteria	0.26	3.4	11.65
Jefferson St. 100' south of subject site-	-existing conditions	0.40	10.5	15.19
after curb drop inlet	proposed conditions	0.52	21.7	****
(street slope = 0.0085 ft/ft)	100 year storm-DPM criteria	0.87	58.8	17.92
	-existing conditions	0.47	16.4	21.05
	proposed conditions	0.58	28.5	~~~
Point B	10 year storm-DPM criteria	0.26	4.6	11.65
Jefferson St. 550' north of subject site-	-existing conditions	0.45 (0.46)	19.6	15.19
prior to curb drop inlet	proposed conditions	0.55 (0.59)	33.8	
(street slope = 0.0160 ft/ft)	100 year storm-DPM criteria	0.87	78.1	17.92
	existing conditions	0.58 (0.62)	37.5	21.05
The state of the s	proposed conditions	0.65 (0.69)	47.7	21.03
Point B	10 year storm-DPM criteria	0.26	4.6	21.00
Jefferson St. 550' south of subject site-	-existing conditions	0.55 (0.59)	33.1	29.96
after curb drop inlet	proposed conditions	0.61 (0.65)	41.4	29.90
(street slope = 0.0160 ft/ft)	100 year storm-DPM criteria	0.87	78.1	31.69
CONTRACTOR OF THE STATE OF THE	existing conditions	0.67 (0.69)	49.8	38.53
	-proposed conditions	0.79	64.5	30.33

Normal depths presented are sub-critical, unless the max. flow depth is followed by parenthesis; in which case, the normal depth is supercritical. Numbers in parenthesis denote the depth at sub-critical flow in the event of a hydraulic jump.

Analyses indicates that under existing undeveloped conditions Jefferson Street has insufficient capacity to meet the 10 year minimum design criteria of one dry lane, each direction. Both the 10 year and the 100 year storms, under existing and proposed conditions are contained within the right of way prism. Because the DPM's 10 year-storm criteria could not be met under existing conditions and the effects due to the proposed development produce negligible change in flow depth, it is requested that a variance to this criteria be allowed for the proposed

Please note that the hydraulic analysis of Jefferson Street presented above is somewhat conservative. Several median breaks and median drainage culverts along Jefferson Street exist as shown on this plan. With the properties to the west of Jefferson Street draining entirely to the west, the entire capacity of Jefferson's south-bound lanes is available. All flow depths shown above are based on a curbed median. All flows greater than 6" deep in the areas without curb median, noted above, will actually spill over into the south-bound lanes.

A hydraulic grade line analysis was performed on the storm sewer paralleling Jefferson Street. The storm sewer was determined to have a capacity of 28 cfs in the 24" reach between the curb drop inlets at points A and B. South of point B, the pipe size increases to a 30" diameter

PRIVATE ACCESS/DRAINAGE EASEMENT HYDRAULICS

This analysis is provided to verify the capacity of the access road to convey flows off-site to Jefferson Street while maintaining depths under the Assume the access road conveys 100% of the runoff from lots \* \* and \* and the runoff from the off-site basin (1.98 of mobile home park)

Peak Discharge

Proposed Conditions 100 year = 39.8 cfs x (1.24ac. + 1.21ac. +1.21ac. +1.40ac.)/9.4ac. + 7.1cfs= 28.5 cfs 10 year = 25.5cfs x (1.24ac. + 1.21ac. +1.21ac. +1.40ac.)/9.4ac. + 4.3 cfs=18.0 cfs

Street flow depths during peak flow were calculated using Manning's equation. Conjugate depths were calculated for flows in the super-critical state, should conditions be conducive to the formation a hydraulic jump. 1) use mild slope region, S = 0.0075 ft/ft 2) n = 0.017 for the roadway surface, 3) road cross slope = 1.5%,

4) curb to curb distance = 25', 5) outside curb to inside driving lane = 13 ft, 6) six inch curbs.

The 100 year and 10 year storm peak flow depths are 0.35 ft and 0.26 ft, respectively. These depths are contained within the roadway prism and well below the DPM's maximum allowable depths.

## PRIVATE DRAINAGE EASEMENT HYDRAULICS

The following analyses were provided as guidelines for the development and utilization of the private drainage easements

## Peak Flows:

10' Drainage Easement Crossing Lots X and X

Assume lots X & X drain 50% and 100%, respectively, of runoff to easement Peak Flow =  $(0.65ac \times 0.5 + 0.65ac)/9.4ac. \times 39.8 cfs = 7.2 cfs$ 

F&G > F
10' Drainage Easement crossing lot ×

Assume lots X& X drain 50% and 100%, respectively, of runoff to easement Peak Flow = (1.22ac. + 0.5 x 0.93ac)/9.4ac. x 39.8 cfs = 24 cfs

For the purpose of this drainage plant the following two options were evaluated for the 10' drainage easements with peak flows of X2 cfs

Concrete Rundown Option

using n = 0.013, slope = 2.0%, a rectangular channel with a width of 7 ft has a normal depth of 0.20 ft and a velocity of 5.3 fps. The resulting energy head is 0.64 ft. Use a rectangular channel with a depth of 0.67 ft and a width of 7.0 ft. Weir Equation (King and Brater) for entrance channel Ocapacity=C \* L \* (H\*\*3/2)

C=Weir Factor =2.6 L=Weir Length=7ft H=Depth of Water Qcapacity=2.6 \* 7.0 ft \* (.67 ft \* 3/2) = 9.8 cfs > 22 [ok]

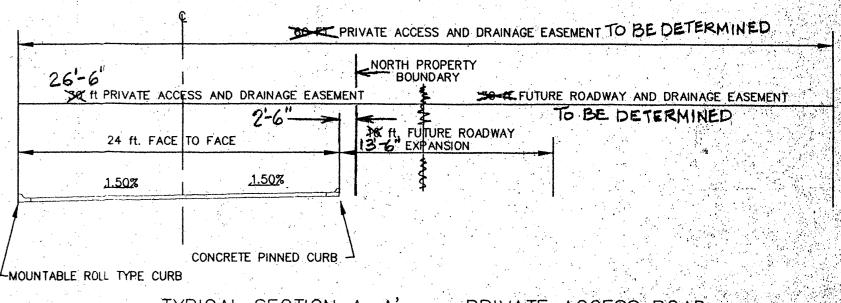
Landscaped Swale Option (assume a triangular cross section with 3:1 side slopes and grass surface) using n = 0.025, slope = 2.0%, a normal depth of 0.75 ft and a velocity of 4.23 fps.

The resulting energy head is 1.02 ft Use a triangular channel with a depth of 1.5 ft, side slopes of 3:1 and a width of 9.0 ft. Weir Equation (King and Brater) for entrance channel Qcapacity=C\*L\*(H\*\*3/2)

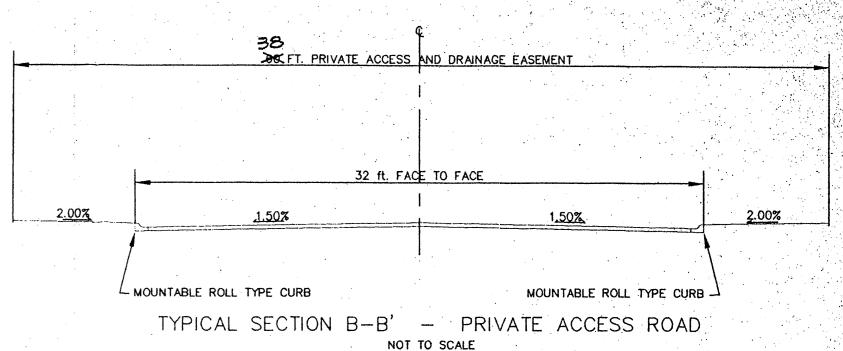
C=Weir Factor =2.6 L=Weir Length=9ft H=Depth of Water, use average depth Qcapacity=26 \* 9.0ft \* (0.75 ft\*\*3/2)=15.2 cfs > 3/2 [ok]

CONCLUSIONS AND RECOMMENDATIONS

The analysis presented in this drainage plan demonstrate that under existing conditions, flows entering Jefferson Street are such that the DPM 10 year criteria is exceeded. Further, the planned development will not significantly alter the flow conditions in Jefferson over the existing conditions. Under both existing and developed flow conditions storm water is contained within the right of way. Depths shown in the table are actually conservative due to the fact that the flows are allowed to pass to the south-bound side of Jefferson where median curb does not exist. Additionally, it is likely that development of the property to the south will utilize the existing stub at the second inlet (analysis point B) and realize the full benefit of the existing of the existing storm sewer system, further decreasing the flows in the roadway assumed under this plan. Lastly, it should be noted that this project is an in-fill project with existing infrastructure designed and constructed under old criteria. In consideration of the information presented under this drainage plan, a variance from the DPM 10 year criteria is requested.



TYPICAL SECTION A-A' - PRIVATE ACCESS ROAD





GRADING AND DRAINAGE CERTIFICATION

I, CARLOS G. PADILLA, A PROFESSINAL ENGINEER DULY REGISTERED IN THE STATE OF NEW MEXICO, HAVING CONDUCTED A SITE INSPECTION AND HAVING DIRECTED THE COLLECTION OF AS-BUILT SURVEY INFORMATION BY PRECISION SURVEYS, INC. (NEW MEXICO PROFESSIONAL SURVEYOR #11993, AGENT FOR THE OWNER), CERTIFY THAT THE SITE GRADING AND DRAINAGE IMPROVEMENTS. ARE COMPLETE AND SUBSTANTIALY COMPLY WITH THE APPROVED DRAINAGE REPORT AND CONSTRUCTION PLANS.



TRACT 14-A-2 DRAINAGE AND GRADING PLAN PLATE 1

