

100 0 100 200 400 600

Boon AB (unexplored)
went over
got to Oakland

0 FEET
400 600

looks like capacity

THE DESIGN FLOW IN THE SAN MATEO STORM DRAIN IS 96 CFS. THE PROPOSED FLOW IN THE SAN MATEO STORM DRAIN IS 102 CFS.

INSTALLATION OF THE FACILITIES PROPOSED IN THIS REPORT WILL REDUCE FLOWS TO THE STREETS IN THE WILDFLOWER SUBDIVISION AND ALLOW FREE DISCHARGE OF ALL PROPERTIES IN THE STUDY AREA.

me

LINE X

BOLLEWARD

LAIR LANE

MILFORD

AMERICAN

ZONE AO
(DEPTH 3)

DUNE

BAY

CONDITION	B A S I N	STORM RETURN PERIOD	TREATMENT TYPE	TREATMENT AREA	EXCESS PRECIPITATION	PEAK RUNOFF	RUNOFF VOLUME	RUNOFF RATE
EXISTING	A1	year	(table 4)		(table 6)	(table 9)		
			10	A	sq. ft.	in	cu. ft.	cfs
				192800	0.19	0.58	3053	2.57
			A	192800			3053	2.57
		100	A	192800	0.06	1.87	10604	8.28
			A	192800			10604	8.28
	A2	10	A	711000	0.19	0.58	11258	9.47
			A	711000			11258	9.47
	100		A	711000	0.06	1.87	39106	30.52
			A	711000			39106	30.52
	A3	10	A	265600	0.19	0.58	4205	3.54
			A	265600			4205	3.54
	100		A	265600	0.06	1.87	14608	11.40
			A	265600			14608	11.40
	B1	10	A	320800	0.19	0.58	5079	4.27
			A	320800			5079	4.27
	100		A	320800	0.06	1.87	17644	13.77
			A	320800			17644	13.77
	C1	10	A	99700	0.19	0.58	1579	1.33
			A	99700			1579	1.33
	100		A	99700	0.06	1.87	5484	4.28
			A	99700			5484	4.28
	C2	10	A	264800	0.19	0.58	4193	3.53
			A	264800			4193	3.53
	100		A	264800	0.06	1.87	14584	11.37
			A	264800			14584	11.37
	C3	10	B	15700	0.36	1.19	471	0.43
			C	15700	0.62	2	811	0.72
			D	62860	1.5	3.39	7850	4.88
			TOTAL	94200			9132	6.04
	100		B	15700	0.92	2.6	1204	0.94
			C	15700	1.29	3.45	1688	1.24
	D		D	62860	2.36	5.02	12351	7.34
			TOTAL	94200			15242	8.46
	D1	10	C	14040	0.62	2	728	0.66
			D	60840	1.5	3.39	7805	4.73
	TOTAL			74880			8330	5.39
	100		C	14040	1.29	3.45	1509	1.11
			D	60840	2.36	5.02	11995	7.89
	TOTAL			74880			13475	8.18
	D2	10	C	4320	0.62	2	223	0.20
			D	18720	1.5	3.39	2340	1.46
	TOTAL			23040			2563	1.68
	100		C	4320	1.29	3.45	464	0.34
			D	18720	2.36	5.02	3882	2.16
	TOTAL			23040			4146	2.50

CONDITION	S A S I N	STORM RETURN PERIOD	TREATMENT TYPE	TREATMENT AREA	EXCESS PRECIPITATION	PEAK RUNOFF	VOLUME RUNOFF	INFLUENT RATE
DEVELOPED	A1	year 10	(table 4)	sq. ft.	in.	(table 5)	cu. ft.	gals.
			C	18029	0.82	2	6016	8.74
			D	84089	1.5	3.39	8016	4.06
			TOTAL	80108			8686	5.72
	100		C	18029	1.28	3.45	1722	1.57
			D	84089	2.30	5.08	12892	7.30
			TOTAL	86108			14609	8.86
	A2	10	B	54405	0.38	1.19	1035	1.40
			C	10089	0.82	2	565	0.60
			D	152336	1.5	3.39	18949	11.39
			TOTAL	217829			21238	13.94
	100		B	54405	0.82	2.6	4171	3.39
			C	10890	1.28	3.45	1176	0.90
			D	152336	2.30	5.08	28982	17.98
			TOTAL	217829			35369	21.68
	A3	10	B	25780	0.38	1.19	773	0.70
			C	5158	0.82	2	280	0.24
			D	72190	1.5	3.39	9034	5.82
			TOTAL	103125			10008	6.94
	100		B	25780	0.82	2.6	1976	1.54
			C	5190	1.28	3.45	664	0.41
			D	72190	2.30	5.08	14187	9.32
			TOTAL	103128			16727	10.27
	A4	10	B	81900	0.38	1.19	2487	2.24
			C	16380	0.82	2	540	0.70
			D	228520	1.5	3.39	29988	17.48
			TOTAL	337600			31495	20.64
	100		B	81900	0.82	2.6	6374	4.90
			C	16380	1.28	3.45	1701	1.30
			D	228520	2.30	5.08	49108	28.48
			TOTAL	337700			59136	36.61
	B1	10	C	18080	0.82	2	628	0.63
			D	72000	1.5	3.39	9888	5.89
			TOTAL	90080			9936	6.48
	100		C	18000	1.28	3.45	1828	1.43
			D	72000	2.30	5.08	14188	8.38
			TOTAL	90000			16016	9.72
	B2	10	B	84425	0.38	1.19	2548	2.22
			C	16980	0.82	2	677	0.78
			D	227914	1.5	3.39	29688	18.48
			TOTAL	336309			33116	21.46
	100		B	84425	0.82	2.6	6925	5.50
			C	16980	1.28	3.45	1634	1.34
			D	227910	2.30	5.08	46710	27.37
			TOTAL	336900			56627	33.78
	B3	10	B	84425	0.38	1.19	2548	2.22
			C	16980	0.82	2	677	0.78
			D	227910	1.5	3.39	29688	18.48
			TOTAL	336300			33110	21.98
	100		B	84425	0.82	2.6	6925	5.50
			C	16980	1.28	3.45	1634	1.34
			D	227910	2.30	5.08	46710	27.37
			TOTAL	336300			56627	33.78

CONDITION	B A B C D E F G H I J K L M N O P Q R S T U V W X Y Z	STORM RETURN PERIOD	TREATMENT TYPE	TREATMENT AREA	DESIGN PRECIPITATION	PEAK RUNOFF	PEAK VOLUME	RUNOFF RATE
			(acres-ft)	(sq. ft.)	(in/hr)	(cfs)	(cu ft.)	(cfs)
G1	10	B	15708	1708	0.28	471	643	0.43
		C	9420	1020	0.62	2	462	0.43
		D	98080	10608	1.5	3.39	8636	0.58
		TOTAL	94200	10200			8698	0.58
	10B	B	15708	1708	0.82	2.6	1294	0.84
		C	9420	1020	1.28	3.48	1019	0.78
		D	98080	10608	3.38	5.02	15868	7.96
		TOTAL	94200	10200			15868	8.84
G2	10	C	18000	1920	0.82	2	930	0.83
		D	72000	7680	1.5	3.38	9080	5.95
		TOTAL	90000	9600			9920	6.78
	10B	C	18000	1920	3.38	6.46	1936	1.48
		D	72000	7680	2.38	5.02	14160	8.33
		TOTAL	90000	9600			16096	9.72
D1	10	C	10896	1162	0.82	2	877	0.78
		D	23710	25475	1.5	3.38	3080	18.28
		TOTAL	25475				3080	18.28
	10B	C	10896	1162	3.38	6.46	1824	1.34
		D	23710	25475	2.38	5.02	4670	27.31
		TOTAL	25475				46804	28.72
G3	10	C	16808	1808	0.82	2	877	0.78
		D	23710	25475	1.5	3.38	3080	18.44
		TOTAL	25475				3080	18.28
	10B	C	16808	1808	3.38	6.46	1824	1.34
		D	23710	25475	2.38	5.02	4670	27.31
		TOTAL	25475				46804	28.72

STORM DRAIN SYSTEM ASSUMPTIONS

1. BASIN A IS ROUTED TO CULVERTS NORTH OF OAKLAND.
2. BASIN B IS ROUTED TO SAN MATEO TOWN DRAIN.
3. BASIN C IS ROUTED TO SOUTH LA CUEVA CHANNEL.
4. BASIN D1 IS ROUTED TO SAN MATEO STORM DRAIN.
5. BASIN D2 IS ROUTED TO SOUTH LA CUEVA CHANNEL.
6. FINAL CONSTRUCTION OF SAN MATEO SAVING WILL BLOCK OFFSITE FLOWS FROM ALAMEDA BLVD.

BASIN A

from DPM Plate 22.3 D.2 w/ Q = 61.4 cfs, S = 1.85%
D = 0.58 ft

from DPM Plate 22.3 D.5 w/ D = 0.58 ft, S = 1.85%
Q = 10.1 cfs

from DPM Plate 22.3 D.2 w/ Q = 41.2 cfs, S = 1.85%
D = 0.53 ft

from DPM Plate 22.3 D.6 w/ D = 0.53 ft, S = 1.85%
Q = 9.5 cfs

from DPM Plate 22.3 D.2 w/ Q = 22.2 cfs, S = 1.85%
D = 0.42 ft

from DPM Plate 22.3 D.6 w/ D = 0.42 ft, S = 1.85%
Q = 8.0 cfs

street flow is very near the street capacity.

	FEMA FLOODPLAIN BOUNDARY
	DRAINAGE BASIN BOUNDARY
	EROSION SETBACK LINE
	EXISTING CONTOUR
	PROPOSED CONTOUR
XX.XX	EXISTING SPOT ELEVATION
XX.XX	PROPOSED SPOT ELEVATION
XX.XX	RECORD SPOT ELEVATION

[illegible]