

City of Albuquerque

Planning Department

Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV 02/2013)

Project Title:	Building Permit #:	City Drainage #:
DRB#: EPC#:		Work Order#:
Legal Description:		
City Address:		
Engineering Firm:		Contact:
Address:		
Phone#: Fax#:		E-mail:
Owner:		Contact:
Address:		
Phone#: Fax#:		E-mail:
Architect:		Contact:
Address:		
Phone#: Fax#:		E-mail:
Surveyor:		Contact:
Address:		
Phone#: Fax#:		E-mail:
Contractor:		Contact:
Address:		
Phone#: Fax#:		E-mail:
TYPE OF SUBMITTAL:	CHECK TYPE OF APPROV	AL/ACCEPTANCE SOUGHT:
DRAINAGE REPORT	SIA/FINANCIAL GUARAN	TEE RELEASE
DRAINAGE PLAN 1st SUBMITTAL	PRELIMINARY PLAT APPI	ROVAL
DRAINAGE PLAN RESUBMITTAL	S. DEV. PLAN FOR SUB'D	APPROVAL
CONCEPTUAL G & D PLAN	S. DEV. FOR BLDG. PERMI	IT APPROVAL
GRADING PLAN	SECTOR PLAN APPROVAL	_
EROSION & SEDIMENT CONTROL PLAN (ESC)	FINAL PLAT APPROVAL	
ENGINEER'S CERT (HYDROLOGY)	CERTIFICATE OF OCCUPA	ANCY (PERM)
CLOMR/LOMR	CERTIFICATE OF OCCUPA	ANCY (TCL TEMP)
TRAFFIC CIRCULATION LAYOUT (TCL)	FOUNDATION PERMIT AP	PROVAL
ENGINEER'S CERT (TCL)	BUILDING PERMIT APPRO	DVAL
ENGINEER'S CERT (DRB SITE PLAN)	GRADING PERMIT APPRO	VAL SO-19 APPROVAL
ENGINEER'S CERT (ESC)	PAVING PERMIT APPROV	AL ESC PERMIT APPROVAL
SO-19	WORK ORDER APPROVAL	ESC CERT. ACCEPTANCE
OTHER (SPECIFY)	GRADING CERTIFICATION	N OTHER (SPECIFY)
WAS A PRE-DESIGN CONFERENCE ATTENDED:	Yes No Co	ppy Provided
DATE SUBMITTED:	By:	

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location, and scope to the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following

1. Conceptual Grading and Drainage Plan: Required for approval of Site Development Plans greater than five (5) acres and Sector Plans

2. Drainage Plans: Required for building permits, grading permits, paving permits and site plans less than five (5) acres

3. **Drainage Report**: Required for subdivision containing more than ten (10) lots or constituting five (5) acres or more

4. Erosion and Sediment Control Plan: Required for any new development and redevelopment site with 1-acre or more of land disturbing area, including project less than 1-acre than are part of a larger common plan of development

February 3, 2015

Ms. Amy Niese Senior Engineer Hydrology Department Public Works Department City of Albuquerque

RE: Revised Grading Plan (C-18D012) American Toyota Albuquerque, New Mexico

Dear Ms. Niese:

The purpose of this letter is to accompany the enclosed revised grading plan. The plan has been revised to accommodate your written comments dated 12/23/14. The following is a summary of your comment and the narrative as to how we addressed

1. Flood zone AE should be AO.

I have corrected this in the report

- First flush should be .34 inches multiplied by impervious area.
 We have added this calculation the calculation sheet. The retained volumes to reduce the flow to less than allowed is greater than the 'first-flush' amount
- 3. What are the flows identified in the DMP.

We have included excerpts of the NAADMP.

- Indicate on the existing basin map where the existing discharges are the flow and pipe sizes
 We have added this information on the basin map
- 5. On the proposed basin map, show the allowable and proposed area, flow and volume for each basin. For each Stormtech system, show the flow and volume in and out. show proposed flow and volume being discharged off site. Show allowable and volume at each location. label basins and roads.

We have added more detail onto the proposed basin map. In addition we have shown existing flow for each discharge point and a comparison of allowed flow to existing and proposed.

- Retention volumes should be based uopn100-year 10-day not 6 hour
 In calculating the resultant discharge based upon the captured volume. We utilize the 10- day volumes as requested
- Include calculation for the design of the stormtech systems
 We have included details and calculations for each system,
- Provide a detail sheet for storm tech system specific to this site
 We have included the details from the manufacturer.
- 9. How will the storm tech manifold system be done. Provide detail of how to be built We have included details of system and layout.

10. In south west corner what is the size of outlet pipe

We have added the size on grading plan

11. In the southwest corner what is size of outlet pip and how will flow go into stormtech and into alameda system

We have added the size of the outlet pipe. The existing pipe will be maintained. A 4' manhole is proposed down stream with a baffle that will force the water into the chambers until they are full then they will discharge to the existing storm drain.

- 12. for south two systems how do excess flows discharge One of the systems has been removed. This portion is designed to fill to capacity and overflow within the pavement. This basin will discharge thru a 6' rundown and discharge from the site at the historical location within the driveway..
- 13. In northwest corner what are sizes of pips connection to the system

We have added the sizes of the pipes

- 14. For north basin will the site no longer utilize existing concrete channelWe will continue to use the concrete channel
- 15. is there enough capacity in alameda and eagle rock to accept flows

There are no as-builts for this system. The proposed discharge is consistent with the North Albuquerque Master Drainage Plan and less than existing conditions.

16. determine ownership of alameda and eagle rock system

The City Department of Municipal Development does not maintain these, therefore we have submitted this same report to the NMDOT for approval

17. Show more spot elevations on the wall

We have added additional spots

18. provide electronic copy of report and drawings

We have submitted pdf with this resubmittal

Should you have any questions regarding this matter, please do not hesitate to call me.

Sincerely,

David Soule, PE RIO GRANDE ENGINEERING PO Box 93924 ALBUQUERQUE, NM 87199 321-9099 REVISED DRAINAGE REPORT

For

AMERICAN TOYOTA EXPANSION

Albuquerque, New Mexico

Prepared by

Rio Grande Engineering PO Box 93924 Albuquerque, New Mexico 87199

FEBRUARY 2015



David Soule P.E. No. 14522

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Excerpt from original drainage report	Α
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PROPOSED BASIN MAP	C.
Site Hydrology	D
Stormtech Details	E

<u>Map</u> Site Grading and Drainage Plan

PURPOSE

The purpose of this report is to provide the Drainage Management Plan for the development of a 10acre parcel located at 5995 alameda. This plan was prepared in accordance with the City of Albuquerque design regulations, utilizing the City of Albuquerque's Development Process Manual drainage guidelines. This report will demonstrate that the grading does not adversely affect the surrounding properties, nor the upstream or downstream facilities.

INTRODUCTION

The subject of this report, as shown on the Exhibit A, is a 10-acre parcel of land located on the west side of San Pedro between Alameda and Eagle rock. The legal description of this site is Lots A and B land of American Toyota and lots 15-18, tract A, unit B North Albuquerque Aces. As shown on FIRM map35013C0137H, the majority of the site is located within Flood Zone X; a portion of the site is impacted by flood zone AO-1 foot. The site has had significant grading activities upon it over the past 10 years. The site is not in native condition and is currently developed. Due to the upstream construction of san Pedro, the site is not affected by any upland flow. The site free discharges to the west. The development of the site will require the site to discharge at a rate equal to or less than the fully developed conditions assumed for this site in the governing North Albuquerque Acres Master Drainage Plan (NAAMDP), which relevant excerpts can be found in appendix B.

EXISTING CONDITIONS

The site currently does have structures on it and has been impacted by human development over the years. The site is currently used as a car dealership and sales lot. The site was developed utilizing he approved drainage report in file C18d12, of which excerpts are found in appendix A. The file is old and significant portions were not found. The site is not impacted by any upland flows. As shown in appendix C, The site currently contains 4 basins. The three southern basins discharge to the existing storm drain in Alameda. As shown in appendix A, the storm drain was not a NMDOT facility but the City of Albuquerque DMD claims they do not maintain so permission from NMDOT to continue to drain at the same rate will be required. Basin Alameda B discharge 11.39 cfs to the Alameda roadway via surface flow thru the driveway. Basin Alameda A-1 discharges 7.78 cfs to the alameda storm drain via a 12" RCP conduit, and Alameda A-2 discharges 13.87 cfs to an 24" storm drain that runs within the frontage road connecting to the Alameda storm drain. The north portion of the site currently drains 13.20 cfs to a series of inlets which are connected to the Eagle rock storm drain. The adjacent site shows the inlets are designed for free discharge of the entire basin, which are significantly reduced due to the completion of San Mateo.



PROPOSED CONDITIONS

The proposed improvements consist of demolishing the existing building and constructing a new 75,000 building. The general drainage patterns will remain, and increases will be captured and harvested in accordance with new city policy. The amount of storage required to reduce the flow was calculated by comparing the volume of water generated from the basin in the allowed conditions of the NAA Drainage master plan and the water generated with the proposed land treatments. The calculation concept is to determine the how much land area the storage volume is equal to. The theory is the initial discharge is captured and once the collection basins are full the remaining site will discharge in accordance with what the down stream would experience according to the remaining area that is not capture. This increase in volume is captured by a series of underground infiltration chambers. The layout and volume calculation is located in appendix E.

The existing discharge points to the Alameda storm drain and the Eagle rock storm drain will be utilized. No offsite improvements will be constructed. The discharge point for existing basin Alameda B will contain new basins A, B and D. The proposed discharge rate of 10.11 from basins A and B will combine with basin D for a discharge rate of 12.68 cfs, the existing discharge rate is 11.39 cfs. The infiltrator system #4 will captured 6,058 cubic feet. The discharge point for basin Alameda will contain basin E, the proposed discharge rate of 6.66 cfs will leave the site within the existing 12" rcp pipe and 4000 cf will be captured by infiltrator system #3. The existing discharge rate is 7.78 cfs. The discharge point for basin Alameda B2 via frontage road contains basin F, with a proposed discharge rate of 11.25 will leave the site via the existing 24" rcp, 4000 cf will be captured by system #2, the existing discharge rate is 13.87. The flow from existing basin Eagle will contain basin C, it will discharge 6.65 cfs to the existing concrete channel and inlets. 10,100 cf will be captured by system#1. The existing discharge rate is 13.22 cfs

The portion of the site that discharges to eagle rock conforms to NAADMP basin 117.22,

the allowed discharge rate of 6.69 cfs is not exceeded. The portion of the site that drains to Alameda conforms to NAADMP basin 117.5. The allowed discharge rate of 36.93 is not exceeded. The site will discharge 6.65 cfs to Eagle Rock and 37.74 cfs to alameda. This is less than existing and less than allowed. We will utilize existing storm drain connection onsite. No off site infrastructure will be constructed. The proposed discharge rates and locations are less than historical and less than allowed in the North Albuquerque Acres master drainage plan.

SUMMARY AND RECOMMENDATIONS

This project is a redevelopment of an existing site. The development discharge will be consistent with the land use assumptions of the North Albuquerque Acres Master drainage plan. The use of underground infiltration will be used to collect the excess discharge and the water quality volume required. The site has been designed in accordance with City of Albuquerque Drainage ordinance. This drainage plan and report conforms to the governing drainage regulations of the City. Since the effected area site encompasses more than 1 acre, a NPDES permit will be required prior to any construction activity. A letter of Map revision (LOMR) has been submitted to remove the floodplain. In addition a LOMR will be required to be submitted prior to release of financial guarantee.

APPENDIX A

Excerpts of Original drainage report

0000 0000 1795

AMERICAN TOYOTA TRACT B

GRADING AND DRAINAGE PLAN

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Prepared by:

Bruther Engineering, Inc. 4425 Juan Tabo N. E. Sain 202 Albuquerque, New Mexico 87112

September, 1994



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AMERICAN TOYOTA TRACT B

GRADING AND DRAINAGE FLAN

PURPOSE AND SCOPE

The purpose of dis Conting and Distingt. Has is to devote the hydrology for the subject graphing, and to contast the site for use as a vehicle parties, and storage facility.

The scope of this separt is no analysis of dealarge conditions for Track P, originally analyzed in 1996, using current hydrologic criterin. This plan describes the solutions conditions, recent dealarge sonlyzer periodsing to the site, and the proposed sitesized of managing stormwater remail.

SITE LOCATION AND DESCRIPTION

The project site is American Toyoto Start B., Homester of 2.00 acrossements to the City at the notification connect of Almosth and San Pedro, in Map C-18. It is branded on the most by Outburd, on figstant by San Pedro, on the work by an example plan dedicating facility, and on the could by Afoneshi. Outburd in a Month Almoneshy more for any start and file of the work. Almost to 24 fort in width, with an existing 54° storm done flowing more in the out allow of the work. Almost to 24 fort in width, with an existing 54° storm done flowing more in the out allow of the work. Almost to 24 fort in width, with an existing 54° storm done flowing more in the out allow of the work. Almost is perceited personantly to bell-width on most of the teerthicking with calls and getter (allow if a first the last of the carbon in a point of the teerthicking work in the out all the distribution is perceited and carbon with The size and a picture of the start flow of the start of a first teer to be in 1906, together with The size and application in the out allow all all the provides in participant the facts of the carbon in the start applicate from the date of the start allow the participant is the start and the carbon in 1906 for both teers. It was made all I teers and destarding understard anne. The destarting place in 1906 for both teers. It are start of Theorem and destarding under teers around and destarge place in 1906 for both teers. It are all teers and Theorem and Caldwell is a start with percent and destarge cancers to block connects by reversion on the out of the start. It is accert, all approx is the start is a descent on the place of the and the me cannot te the place is and it is through the teel.

The site is presently manufacted, but much could , and is use for specage of new vehicles, and some couplingers parting, all related to the ante destroking operation (~ Thest A. The site shorts generally despress to meet at approximately 45. It mer arighted y parted in confirmment with coloring propagingly without excessive casing or filling. As shown by PEMA PRICE Place 300002 6010C, dis sho does not be within a 100 year floodplich.

Chashe nells consist mainty of Parliado Tijens complex, and Epidenia, which we chashing by the Soil Concernation Service as hydrologic group 'B' solls. SCS describes them as follows:

Bub - Subado gravelly fine undy loans: 0-55 vinges. These are gravelly doin, well desired soils formed as allowing derived from decomposed, course gravel gravitic suchs. They enable mediate twent characteristics with madesite excess.

BC - Enducto - Idents complex, fine starty lows, 0.9% slopet. This tage access in distangenergy and depression, and de Tjerner will is an few edges in conversion definition. Second to stations, and employ is inclusive.

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EXISTING DRAINAGE CONDITIONS

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The 1985 designs the antipart decomposes and downstream basis for both Teacts A and B. It was descentized that all flows generated can of San Fedro should be intercepted at or restream. San Police by the 54⁴ due in San Police. This designs plan should be intercepted at or restream. San Intercepted to accomplish due for anti-veloped conditions updates. It should find the inter and developed flows could be appropriately by solidional drop inter-constructed at the interactions with Alameda and Ockland. This original plan independent from both Tracts A and B interactions with Alameda and Ockland. This original plan independent from both Tracts A and B index developed determined that it lead dis capacity to convey, interactive from both Tracts A and B index developed conditions, based upon crimets is effect at that line.

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Tract B was graded to drate to the west to the private drainage and access essential on the east side of Tract A, then south as Alamada. A small position of Tract B was also planned to discharge to Outland where, downsteens to the cal-do-acc, a drop left was constructed with a sumform to the 1-25 footings root. This grading and includes plan does not purpose to the these original conditioned

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At the time of addition, Tract A rest carametered with public and private infestivations Traportaneous. All these implemented where continuented. The impresentation opportunity is Tract B a related and by infestivative listing, but were granted a bulk land variance and therefore deferred. The listing are furth the reprivative for private in Califord, San Police, and Alexanda, and variables. In San Token. The paring improvements in Alexandr will be considered and refressed. The San Token. 가지 집을 et deferred.

PROPOSED CONDITIONS

The ship was graded and has been used contamily since 1985 for paring and vehicle storage. The only change to this confidence is due the site will be pared. In compliance with the Maith 3.25 Sector Plan, a backgoing lattice will be conversed at the side of very face of the relation 3.25 sector Plan, a backgoing lattice are 15" while on Plans and Alameda, and 10° on Onlined. The sector of the parine sector and desimple constants, and a moreor sub of the north cut of the side will desire to the private scenar and desimple constants, and a moreor sub of the north cut of the side will desire to Caldenil. Refere paring, the text grading will be reflared. The infinite-scene lights manorements for Track 8 will be constructed by separate City work only. The infinite-scene fields the stored grades to be constructed by due work only and by City Project 2007 in Alameda.

The original grading and drainings plan consequences in improvious site for Tract B, and incorporated & improvements under former ordering consequences she did at estimately improvements is forward, the sequences under fordering consequences by a considers the did at estimately improvement, for some small theorem and volumes are compared. This plan generates present presents and consequences in 1996, and the generated water presents and consequences. This plan generates are consequent in the plan generates are consequent. This plan generates are consequent for the difference present standardinary generates are consequent. This plan generates water present standardinary, the size was constituted as generating 12.3 plat water 100-year constitues. By mained presenting a second generate are generated are will now generates 14.2 cfs - as increase of 1.4 cfs at a second of days, of a state dividence of the present scale will now generates 14.2 cfs - as increase of 1.4 cfs at a second of days, of a state dividence of the second generate for the distribution provides the second generate of the second generate to describe provides for the distribution of a second generate 14.2 cfs - at increase of 1.4 cfs at a second of the generate of the distribution provides for the distribution of a second generate of the second generate for the second generate of the second generate of the second generate of the second generate of the second generate for the distribution provides of the second generate for the second generate of the second generate of the second generate of the second generate of the second generate for the second generate of the second generate for the second generate for the second generate of the second generate of the second generate for the second generate of the second generate of the second generate of the second generate of th γ.

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P.O. Spr. 200, stample Building and sports and Boundary 10, 1986

TO MININE IT MAY COMPENN:

The store court system in anistance on San Pages Drive is the vicinity of Alamada Drive, as woll as the store search system constructed to pass store matter under 1-25 at the Alamada Intercharge are not the property of for material and by the State Righnay Separatempt.

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D. C. ARP District Highery Engineer



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APPENDIX D

PROPOSED HYDROLOGY

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Weighted E Method AMERICAN TOYOTA

PROPOSED Developed Basins

											100-Year, 6-t	nr		10-day
Basin	Area	Area	Treatment	A	Treatment	B	Treatm	ent C	Treatmen	t D	Weighted E	Volume	Flow	Volume
	(sf)	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(ac-ft)	(ac-ft)	cfs	(ac-ft)
BASIN A	39648	0.910	0%	0	4.0%	0.036	6.0%	0.05461	90%	0.819	2.238	0.170	4.40	0.279
BASIN B	74514	1.711	0%	0	4.0%	0.068	6.0%	0.10264	90%	1.540	2.238	0.319	8.26	0.524
BASIN C	95977	2.203	0%	0	4.0%	0.088	6.0%	0.1322	90%	1.983	2.238	0.411	10.64	0.675
BASIN D	27176	0.624	0%	0	10.0%	0.062	42.0%	0.26203	48%	0.299	1.767	0.092	2.57	0.132
BASIN E	73535	1.688	0%	0	4.0%	0.068	6.0%	0.10129	90%	1.519	2.238	0.315	8.15	0.517
BASIN F	116842	2.682	0%	0	4.0%	0.107	6.0%	0.16094	90%	2.414	2.238	0.500	12.95	0.822
BASIN G	6395	0.147	0%	0	15.0%	0.022	85.0%	0.12479	0%	0.000	1.235	0.015	0.49	0.015
WATER QUALITY	427692	9.8184573											·· <u></u>	

Equations:

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Weighted E = Ea*Aa + Eb*Ab + Ec*Ac + Ed*Ad / (Total Area)

Volume = Weighted D * Total Area

Flow = Qa * Aa + Qb * Ab + Qc * Ac + Qd * Ad

Where for 100-year, 6-hour storm (zone 3)

Ea= 0.66	Qa= 1.87
Eb= 0.92	Qb= 2.6
Ec= 1.29	Qc= 3.45
Ed= 2.36	Qd= 5.02

FLOW SUMMARY

	PROPOS	SED			
DISCHARGE TO INLET A	4.40	CFS			
DISCHARGE TO INLETB	8.26	CFS			
DISCHARGE TO INLET C	10.64	CFS			
DISCHARGE TO INLET E	8.15	CFS			
DISCHARGE TO INLET F	12.95	CFS			
			EXISTING	FIRST FLUSH	RETAINED
DISHCHARGE TO FALL 1	10.11	CFS	11.390 CFS	2911	6000
DISCHARGE TO OUTFALL 2	6.66	CFS	7.780 CFS	1875	3500
DISCHARGE TO OUTFALL 3	11.25	CFS	13.870 CFS	2980	4000
DISCHARGE TO OUTFALL4	6.65	CFS	13.220 CFS	2448	10000
COMPARISION					
	EXISTIN	G	PROPOSED	ALLOWED	
EAGLE ROCK	1:	3.2	6.66	6.69	
ALAMEDA	33.	.04	31.08	36.93	
TOTALS	46.	.24	37.74	43.62	

Weighted E Method AMERICAN TOYOTA OUTFALL #1

PROPOSED Developed Basins														
											100-Year, 6-h	n <u>r. </u>		24-hour
Basin	Area	Area	Treatment	Ā	Treatment	В	Treatm	ent C	Treatment	t D	Weighted E	Volume	Flow	Volume
	<u>(sf)</u>	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(ac-ft)	(ac-ft)	<u>cfs</u>	(ac-ft)
BASIN A	39648	0.910	0%	0	4.0%	0.036	6.0%	0.05461	90%	0.819	2.238	0.170	4.40	0.235
BASIN B	74514	1.711	0%	0	4.0%	0.068	6.0%	0.10264	90%	1.540	2.238	0.319	8.26	0.442
AREA CAPTURED	23000	0.528	0%	0	4.0%	0.021	6.0%	0.03168	90%	0.475	2.238	0.098	2.55	0.136
WATER QUALITY Equations: Weighted E = Ea*Aa + Eb*Ab + Volume = Weighted D * Total Au Flow = Qa * Aa + Qb * Ab + Qc Where for 100-year, 6-hour stor	2911.131 Ec*Ac + Ed*Ad rea * Ac + Qd * Ad m (zone 3) Ea= Eb= Ec= Ed=	0.66 0.92 1.29 2.36	a)	Qa= Qb= Qc= Qd=	1.87 2.6 3.45 5.02				STORAG	Ξ	RESULTANT EXISTING 6000 CF	DISCHARGE 0.137741047	10.11 11.39	CFS CFS

Weighted E Method AMERICAN TOYOTA OUTFALL#2

PROPOSED Developed Basins

												100-Year, 6-h	nr		10-day
	Basin	Area	Area	Treatment	A	Treatment	B	Treatm	nent C	Treatment	D	Weighted E	Volume	Flow	Volume
		(<u>s</u> f)	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(ac-ft)	(ac-ft)	cfs	(ac-ft)
	BASINE	73535	1.688	0%	0	4.0%	0.068	6.0%	0.10129	90%	1.519	2.238	0.315	8.15	0.436
	CAPTURED	13500	0.310	0%	0	4.0%	0.012	6.0%	0.0186	90%	0.279	2.238	0.058	1.50	0.080
••	WATER QUALITY	1875.1425											H		2)

Equations:

Weighted E = Ea*Aa + Eb*Ab + Ec*Ac + Ed*Ad / (Total Area)

Volume = Weighted D * Total Area

Flow = Qa * Aa + Qb * Ab + Qc * Ac + Qd * Ad

Where for 100-year, 6-hour storm (zone 3)

STORAGE

3500 0.08034894

EXISTING

RESULTANT DISCHARGE

6.66 CFS

7.78 CFS

	0 4.07
Ea= 0.00	Qa= 1.87
Eb= 0.92	Qb= 2.6
Ec= 1.29	Qc= 3.45
Ed= 2.36	Qd= 5.02

Weighted E Method AMERICAN TOYOTA OUTFALL 3

PROPOSED Developed Basins

								_			100-Year, 6-	hr.		10-day
Basin	Area	Area	Treatment	A	Treatment	в	Treatm	nent C	Treatmen	it D	Weighted E	Volume	Flow	Volume
L	(sf)	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(ac-ft)	(ac-ft)	cfs	(ac-ft)
BASIN F	116842	2.682	0%	C	4.0%	0.107	6.0%	0.16094	90%	2.414	2.238	0.500	12.95	0.822
AREA CAPTURED	15400	0.354	0%	Q	4.0%	0.014	6.0%	0.02121	90%	0.318	2.238	0.066	1.71	0.091
WATER QUALITY	2979.471										•			
Equations:											RESULTAN	DISCHARGE	11.25	CFS
											EXISTING		13.87	CFS
Weighted E = Ea*Aa + Eb*Ab -	+ Ec*Ac + Ed*/	Ad / (Total A	rea)											
Volume = Weighted D * Total A	rea													
Elow = Qa * Aa + Qb * Ab + Qc	* hc + Od * A	d												
									STORAG	E	4000 CF	0.091827365		
Where for 100-year, 6-hour sto	rm (zone 3)									—				
•	Èa=	0.66		Qa=	: 1.87									
	Eb=	0.92		Qb=	2.6									
	Ec=	1.29		Qc=	3.45									
	Ed=	2.36		Qd=	5.02									

Weighted E Method AMERICAN TOYOTA OUTFALL 4

PROPOSED Developed Basins

											100-Year, 6-I	nr		10-day
Basin	Area	Area	Treatment.	Ā	Treatment	B	Treatm	ent C	Treatmen	tD	Weighted E	Volume	Flow	Volume
	<u>(sf)</u>	(acres)	%	(acres)	_%	(acres)	%	(acres)	%	(acres)	(ac-ft)	(ac-ft)	cfs	(ac-ft)
BASIN C	95977	2.203	0%	0	4.0%	0.088	6.0%	0.1322	90%	1.983	2.238	0.411	<u>10.</u> 64	0.675
" AREA CAPTURED	36000	0.826	0%	0	4.0%	0.033	6.0%	0.04959	90%	0.744	2.238	0.154	3.99	0.214
WATER QUALITY	2447.4135	2.2033287									·			
Equations:											RESULTAN	DISCHARGE	6.65	CFS
											EXISTING		13.22	CFS
Weighted E = Ea*Aa + Eb*Ab +	Ec*Ac + Ed*/	Ad / (Total A	rea)										6.69	
Volume = Weighted D * Total A	vrea													
Flow = Qa * Aa + Qb * Ab + Qo	;*Ac+Qd*A	d												
									STORAG	E	10000CF	0.229568411		
Where for 100-year, 6-hour sto	rm (zone 3)													
	Ea=	0.66		Qa=	1.87									
	Eb=	0.92		Qb=	2.6									
	Ec=	1.29		Qc=	3.45									

Qd= 5.02

Ed= 2.36

APPENDIX B

NAADMP EXCERPTS



Weighted E Method AMERICAN TOYOTA

NAAMDP Developed Basins

						_		-			100-Year, 6-t	ـــــــــــــــــــــــــــــــــــــ		10-day
Basin	Area	Area	Treatment	Α	Treatment	B	Treatm	ent C	Treatmen	t D	Weighted E	Volume	Flow	Volume
	(sf)	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(ac-ft)	(ac-ft)	cfs	(ac-ft)
EAGLEROCK	66508	1.527	0%	0	20.0%	0.305	10.0%	0.15268	70%	1.069	1.965	0.250	6.69	0.393
ALAMEDA	367341	8.433	0%	0	20.0%	1.687	10.0%	0.8433	70%	5.903	1.965	1.381	36.93	2.168

,

Equations:

Weighted E = Ea*Aa + Eb*Ab + Ec*Ac + Ed*Ad / (Total Area)

Volume = Weighted D * Total Area

Flow = Qa * Aa + Qb * Ab + Qc * Ac + Qd * Ad

Where for 100-year, 6-hour storm (zone 3)

Ea= 0.66	Qa= 1.87
Eb= 0.92	Qb= 2.6
Ec= 1.29	Qc= 3.45
Ed= 2.36	Qd= 5.02



		TABLE A-2 (con	t.)				
	LA CUEVA ARROY	YO SUB-BASIN	CHARA	CTER	ISTIC	5	
Basin D	Basin ID Hydrologic Basin Area Land Treatment (%)						TP
	Condition	(mi ²)	A	B	С	D	(hrs)
113*	Existing Future	.1136	8 0 0	0 25	15 15	5 60	.133 .133
115*	Existing Future	.1337 .1202	80 0	0 26	15 12	5 62	.133
116*	Existing	.1309	80	0	5	15	.133
116.1	Future	.1000	0	25	15	50	.133
116.2	Future	.0719	0	25	15	60 50	.133
116.21	Future	.0344	0	40	20	40	.133
117.2*	Existing Future	.1391 .0500	73 0	0 34	7 16	20 50	.22 .133
117.21*	Existing	.0234	0	34	16	50	.133
117.22*	Future	.0156	0	20	10	70	.133
117.3*	117.3* Existing Future		65 0	· 5 34	15 16	15. 50	.133 .133
117.31*	Existing	.0250	0	34	16	50	.133
117.32*	Existing	.0090	0	34	16	50	.133
117.4*	Existing Future	.0750 .0512	85 0	0 25	5 15	10 60	.133 .133
117.5*	Existing Future	.0550 .0550	0 0	10 10	20 20	70 70	.133 .133
118	Existing Future	.0649 .0649	0	20 20	10 10	70 70	.133 .133
118.1	Existing Future	.0306 .0306	75 0	5 20	10 30	10 50	.133 .133
119	Existing Future	.0549 .0549	00	20 20	10 [.] 10	70 70	.133 .133
120	Existing Future	.0268 .0268	50 0	0 20	0 10	50 70	.133 .133
121	Existing Future	.0489 .0489	80 0	0 20	15 10	5 70	.133 .133

*Modified for COA NAA MDP 9/97

A:197-080MASTER.PLN

APPENDIX C

EXISTING HYDROLOGY

.



APPENDIX E

STORMTECH DETAILS AND CALCULATIONS

.

ADS SALES REP:	PETER NICHOLS 505-301-5604 PETER.NICHOLS@ADS-PIPE.COM
PROJECT NO:	82394 REV1



AMERICAN TOYOTA

ALBUQUERQUE, NM

2.

STORMWATER CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH MC-4500 OR APPROVED EQUAL. 1
- 2. CHAMBERS SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS.
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT 3. WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS. THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS. SECTION 12.12. ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418. "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED 5 WALL STORMWATER COLLECTION CHAMBERS".
- 6 CHAMBERS SHALL BE DESIGNED AND ALLOWABLE LOADS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 7. ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
 - A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD. THE MINIMUM REQUIRED BY ASTM F2787 AND BY AASHTO FOR THERMOPLASTIC PIPE.
 - A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET. THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
 - C. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED.
- 8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

IMPORTANT - NOTES FOR THE BID

- 1 STORMTECH MC-4500 CHAMBERS SHALL NO **PRE-CONSTRUCTION MEETING WITH THE INS**
- 2 STORMTECH MC-4500 CHAMBERS SHALL BE
- CHAMBERS ARE NOT TO BE BACKFILLED WIT 3.

STORMTECH RECOMMENDS 3 BACKFILL MET

- STONESHOOTER LOCATED OFF THE
- BACKFILL AS ROWS ARE BUILT USING
- BACKFILL FROM OUTSIDE THE EXCAV
- THE FOUNDATION STONE SHALL BE LEVELED 4
- JOINTS BETWEEN CHAMBERS SHALL BE PRO 5.
- 6. MAINTAIN MINIMUM - 9" (230 mm) SPACING BE
- 7. INLET AND OUTLET MANIFOLDS MUST BE INS
- 8. EMBEDMENT STONE SURROUNDING CHAMB DESIGNATION OF #3 OR #4.
- STONE SHALL BE BROUGHT UP EVENLY ARO 9 DIFFER BY MORE THAN 12" (300 mm) BETWEE
- STONE MUST BE PLACED ON THE TOP CENTI 10.
- ADS RECOMMENDS THE USE OF "FLEXSTOR 11 STORMWATER MANAGEMENT SYSTEM FROM

NOTES FOR CONSTRUCTION EQU

- STORMTECH MC-4500 CHAMBERS SHALL BE 1
 - THE USE OF EQUIPMENT OVER MC-4500 CHA
 - NO EQUIPMENT IS ALLOWED ON BARI
 - NO RUBBER TIRED LOADER. DUMP TR
 - WITH THE "STORMTECH MC-3500/MC-
 - WEIGHT LIMITS FOR CONSRUCTION E



PROPOSED ELEVATIONS (SYSTEM #1)

MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	5218.75
MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):	5214.25
MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):	5213.75
MINIMUM ALLOWABLE GRADE (TOP OF RIGID CONCRETE PAVEMENT):	5213.75
TOP OF STONE:	5212.75
TOP OF CHAMBER:	5211.75
24" TOP MANIFOLD INVERT:	5208.67
24" ISOLATOR ROW INVERT:	5206.94
BOTTOM OF CHAMBER:	5206.75
BOTTOM OF STONE:	5206.00



PROPOSED ELEVATIONS (SYSTEM #2)

MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	5214.25
MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):	5209.75
MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):	5209.25
MINIMUM ALLOWABLE GRADE (TOP OF RIGID CONCRETE PAVEMENT):	5209.25
TOP OF STONE:	5208.25
TOP OF CHAMBER:	5207.25
24" TOP MANIFOLD INVERT:	5204.17
24" ISOLATOR ROW INVERT:	5202.44
BOTTOM OF CHAMBER:	5202.25
BOTTOM OF STONE:	5201.50





MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	5214.25
MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):	5209.75
MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):	5209.25
MINIMUM ALLOWABLE GRADE (TOP OF RIGID CONCRETE PAVEMENT):	5209.25
TOP OF STONE:	5208.25
TOP OF CHAMBER:	5207.25
24" ISOLATOR ROW INVERT:	5202.44
BOTTOM OF CHAMBER:	5202.25
BOTTOM OF STONE:	5201.50



PROPOSED ELEVATIONS (SYSTEM #5)

MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	5231.75
MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):	5227.25
MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):	5226.75
MINIMUM ALLOWABLE GRADE (TOP OF RIGID CONCRETE PAVEMENT):	5226.75
TOP OF STONE:	5225.75
TOP OF CHAMBER:	5224.75
24" ISOLATOR ROW INVERT:	5219.94
BOTTOM OF CHAMBER:	5219.75
BOTTOM OF STONE:	5219.00



D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	P I N
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	M
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 4	
A	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 4	

PLEASE NOTE:

1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 ST ANGULAR NO. 4 (AASHTO M43) STONE".

2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVE

 WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.



NOTES:

- 1. MC-4500 CHAMBERS SHALL CONFORM TO THE REQUIREMENTS OF ASTM F2418 "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS
- 2. MC-4500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION

3. "ACCEPTABLE FILL MATERIALS" TABLE ABOVE PROVIDES MATERIAL LOCATIONS, DESCRIPTIONS, GRADATIONS, AND COMPACTION REQUIREMENTS FOR FOUNDATION, EMBEDMENT, AND FILL MATE

- 4. THE "SITE DESIGN ENGINEER" REFERS TO THE ENGINEER RESPONSIBLE FOR THE DESIGN AND LAYOUT OF THE STORMTECH CHAMBERS FOR THIS PROJECT.
- 5. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WI CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.



1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.

2 CONDUCT INTTING AND VACTORING ANNHALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY



*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION AND BETWEEN CHAMBERS, 12" (305 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY.

STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B" STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T"

PART #	STUB	B	С
MC4500REPE06T	611 (1E0 mm)	42.54" (1.081 m)	
MC4500REPE06B	o" (150 mm)		0.86" (22 mm)
MC4500REPE08T	9" (200 mm)	40.50" (1.029 m)	
MC4500REPE08B	6 (200 mm)		1.01" (26 mm)
MC4500REPE10T	10" (250 mm)	38.37" (975 mm)	
MC4500REPE10B	10 (250 mm)		1.33" (34 mm)
MC4500REPE12T	40% (200)	35.69" (907 mm)	
MC4500REPE12B	12 (300 mm)		1.55" (39 mm)
MC4500REPE15T	4Ell (975 mm)	32.72" (831 mm)	
MC4500REPE15B	15" (375 mm)		1.70" (43 mm)
MC4500REPE18TC	40% (4E0 mama)	29.36" (746 mm)	
MC4500REPE18BC	10 (450 mm)		1.97" (50 mm)
MC4500REPE24TC	 2.4% (600 mm)	23.05" (585 mm)	
MC4500REPE24BC	24 (600 mm)		2.26" (57 mm)
MC4500REPE30BC			2.95" (75 mm)
MC4500REPE36BC		-	3.25" (83 mm)
MC4500REPE42BC	42" (1050 mm)		3.55" (90 mm)







NOTES

- 1. 8-30" (200-750 mm) GRATES/SOLID COVERS SHALL BE DUCTILE IRON PER ASTM A5 GRADE 70-50-05
- 2. 12-30" (300-750 mm) FRAMES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-5
- 3. DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN DETAILS
- DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D321 FOR CORRUGATED HDPE (ADS & HANCOR DUAL WALL) & SDR 35 PVC
- 5. FOR COMPLETE DESIGN AND PRODUCT INFORMATION: WWW.NYLOPLAST-US.CO
- 6. TO ORDER CALL: 800-821-6710

Α	PART #	GRATE/SOLID COVER OPT				
8" (200 mm)	2808AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIC		
10" (250 mm)	2810AG	PEDESTRIAN LIGHT	STANDARD LIGHT DUTY	SOLID LIC		
12" (300 mm)	2812AG	PEDESTRIAN AASHTO H-10	STANDARD AASHTO H-20	SO AASH7		
15" (375 mm)	2815AG	PEDESTRIAN AASHTO H-10	STANDARD AASHTO H-20	SO AASHT		
18" (450 mm)		PEDESTRIAN	STANDARD AASHTO	SO		

82394 - System #1 - REV1

Project:	82394 - System #1 - REV1		-	4 3
Chamber Mod Units -	lei -	MC-4500 Imperial	Click Here fo	StormTech
Number of Ch Number of En Voids in the sl	ambers ~ d Caps - one (porosity) -	61 6 30	%	
Base of Stone Amount of Sto Amount of Sto Area of syster	Elevation - ne Above Chambers - ne Below Chambers - n -	5206.00 12 9 2675	ft in in sf Min. Ai	Include Perimeter Stone in Calculations rea - 2424 sf min. area

Height of	Incremental Single	Incremental	Incremental	Incremental	incremental	Incremental Ch,	Cumulative	
System	Champer	Single End Cap	Champers	End Cap	Stone	EC and Stone	System	Elevation
(Inches)				CUDIC TEEL				(1001)
01	0.00	0.00	0.00	0.00	00.00	00.00	10114.00	5212.70
70	0.00	0.00	0.00	0.00	66.98	00,00	0090.03	5212.07
78	0.00	0.00	0.00	0.00	66.89	66.89	9900.93	5212.00
70	0.00	0.00	0.00	0.00	66.88	66.88	9914.00	5212.00
76	0.00	0.00	0.00	0.00	66.88	66.88	0780 31	5212.42
76	0.00	0.00	0.00	0.00	66.89	66.98	9760.31	5212.00
73	0.00	0.00	0.00	0.00	88 33	66.88	0646 56	5212.20
73	0.00	0.00	0.00	0.00	66.88	86.88	9579.68	5212.08
70	0.00	0.00	0.00	0.00	88 88	66.88	9512.81	5212.00
71	0.00	0.00	0.00	0.00	66.88	66.88	9445 93	5211 92
70	0.00	0.00	0.00	0.00	66 88	66.88	9379.06	5211 83
69	0.04	0.00	2.50	0.00	66.13	68.62	9312.18	5211.75
68	0.12	0.01	7.08	0.06	64.73	71.87	9243.56	5211.67
67	0.16	0.03	10.05	0.16	63.81	74.02	9171.68	5211.58
66	0.21	0.05	12.73	0.29	62.97	75.99	9097.66	5211.50
65	0.27	0.07	16.37	0.41	61.84	78.62	9021.68	5211.42
64	0.45	0.09	27.62	0.53	58.43	86.58	8943.06	5211.33
63	0.67	0.11	40.58	0.68	54.50	95.76	8856.48	5211.25
62	0.80	0.14	48.74	0.85	52.00	101.59	8760.73	5211.17
61	0.91	0.17	55.40	1.01	49.95	106.36	8659.14	5211.08
60	1.00	0.19	61.18	1.15	48.18	110.50	8552.78	5211.00
59	1.09	0.22	66.33	1.29	46.59	114.21	8442.28	5210.92
58	1.16	0.24	70.97	1.45	45.15	117.57	8328.07	5210.83
57	1.23	0.27	75.27	1.62	43.81	120.70	8210.50	5210.75
56	1.30	0.30	79.28	1.79	42.56	123.62	8089.80	5210.67
55	1.36	0.32	83.02	1.94	41.39	126.35	7966.18	5210.58
54	1.42	0.35	86.54	2.09	40.29	128.91	7839.83	5210.50
53	1.47	0.37	89.87	2.23	39.25	131.34	7710.91	5210.42
52	1.53	0.39	93.03	2.36	38.26	133.65	7579.57	5210.33
51	1.57	0.42	96.04	2.50	37.31	135.86	7445.92	5210.25
50	1.62	0,44	98.90	2.64	36.41	137,96	7310.06	5210.17
49	1.67	0.46	101.64	2.78	35.55	139.97	7172.10	5210.08
48	1.71	0.48	104.26	2.90	34.73	141.89	7032.13	5210.00
4/	1.70	0.50	100.70	3.03	33.94	143.72	6746 52	5209.92
40	1./9	0.53	109,10	3.10	33.19	140.40	0740.02	5209.63 5200 75
40	1.03	0.55	112.67	3.27	32.40	147.19	6452.85	5209.75
43	1.00	0.50	115.80	3.50	31.09	150.38	6305.00	5209.58
42	1.93	0.50	117.84	3.61	30.44	151.89	6154.66	5209.50
41	1.96	0.62	119.81	3 72	29.82	153 35	6002 76	5209 42
40	2.00	0.64	121 70	3.83	29.22	154 75	5849 42	5209.33
39	2.03	0.66	123.53	3.93	28.64	156.10	5694.67	5209.25
38	2.05	0.67	125.28	4.04	28.08	157.40	5538.58	5209.17
37	2.08	0.69	126.97	4.14	27.54	158.65	5381.18	5209.08
36	2.11	0.71	128.59	4.24	27.02	159.86	5222.52	5209.00
35	2.13	0.72	130.16	4.34	26.52	161.03	5062.66	5208.92
34	2.16	0.74	131.68	4.44	26.04	162.16	4901.63	5208.83
33	2.18	0.76	133.14	4.54	25.57	163.24	4739.47	5208.75
32	2.21	0.77	134.54	4.63	25.13	164.29	4576.23	5208.67
31	2.23	0.79	135.89	4.72	24.69	165.30	4411.94	5208.58
30	2.25	0.80	137.18	4.81	24.28	166.27	4246.64	5208.50
29	2.27	0.82	138.43	4.92	23.87	167.22	4080.37	5208.42
28	2.29	0.84	139.63	5.04	23.47	168.15	3913.14	5208.33
27	2.31	0.85	140.78	5.08	23.12	168.97	3745.00	5208.25
26	2.33	0.86	141.88	5.15	22.76	169.80	3576.02	5208.17
25	2.34	0.87	142.94	5.23	22.42	170.60	3406.22	5208.08
24	2.36	0.89	143.95	5.31	22.10	171.36	3235.63	5208.00
23	2.38	0,90	144.92	5.39	21.78	172.09	3064.27	5207.92
22	2.39	0.91	145.85	5.46	21.48	172.79	2892.17	5207.83
21	2.41	0.92	146.73	5.53	21.19	173.46	2719.38	5207.75
20	2.42	0.93	147.57	5.61	20.92	174.10	2545.92	5207.67
19	2.43	0.95	148.38	5.67	20.66	174.71	2371.82	5207.58
18	2.44	0.96	149.14	5.74	20.41	175.29	2197.11	5207.50
17	2.46	0.97	149.85	5.80	20.18	175.84	2021.82	5207.42
16	2.47	0.98	150.53	5.87	19.95	176.36	1845.98	5207.33

82394 - System #2 - REV1

Project:

roject:	82394 - System #2	- REV1	_	24A
			_	StormToch
Chamber Model -		MC-4500	7	SUMMECH
Units -		Imperial	Click Here for	Metric
Number of Chamb	ers -	22		t decision of
Number of End Ca	ps -	4]	
Voids in the stone	(porosity) -	30]%	
Base of Stone Eler	vation -	5201.50]ft [
Amount of Stone A	bove Chambers -	12]in [✓] Include Perimeter Stone in Calculations
Amount of Stone E	elow Chambers -	9	in	
Area of system -		1158	sf Min. Are	a - 934 sf min. area

				-				_
Height of	Incremental Single	Incremental	Incremental	Incremental	Incremental	Incremental Ch,	Cumulative	_
System	Chamber	Single End Cap	Chambers	End Cap	Stone	EC and Stone	System	Elevation
<u>(iiicites/</u> 					29.05			(TEET)
80	0.00	0.00	0.00	0.00	20.90	20.90	4065.14	5206.20
79	0.00	0.00	0.00	0.00	28.95	28.95	4027 24	5208.08
78	0.00	0.00	0.00	0.00	28.95	28.95	3998.29	5208.00
77	0.00	0.00	0.00	0.00	28.95	28.95	3969.34	5207.92
76	0.00	0.00	0.00	0.00	28.95	28.95	3940.39	5207.83
75	0.00	0.00	0.00	0.00	28.95	28.95	3911.44	5207.75
74	0.00	0.00	0.00	0.00	28.95	28.95	3882.49	5207.67
73	0.00	0.00	0.00	0.00	28.95	28.95	3853.54	5207.58
72	0.00	0.00	0.00	0.00	28.95	28.95	3824.59	5207.50
71	0.00	0.00	0.00	0.00	28.95	28.95	3795.64	5207.42
69	0.04	0.00	0.90	0.00	28.68	20.95	3737 74	5207.33
68	0.12	0.01	2.55	0.04	28.17	30.77	3708.15	5207.17
67	0.16	0.03	3.62	0.11	27.83	31.56	3677.39	5207.08
66	0.21	0.05	4.59	0.19	27.52	32.30	3645.83	5207.00
65	0.27	0.07	5.90	0.27	27.10	33.27	3613.53	5206.92
64	0.45	0.09	9.96	0.35	25.86	36.17	3580.26	5206.83
63	0.67	0.11	14.64	0.45	24.42	39.51	3544.09	5206.75
61	0.80	0.14	17.56	0.57	23.51	41.65	3504.58	5206,67
60	1.00	0.17	22.06	0.07	22.76	43.40	3402.93	5206.50
59	1.09	0.22	23.92	0.86	21.52	46.30	3374.59	5206.42
58	1.16	0.24	25.60	0.97	20.98	47.54	3328.29	5206.33
57	1.23	0.27	27.15	1.08	20.48	48.71	3280.75	5206.25
56	1.30	0.30	28.59	1.19	20.01	49.80	3232.04	5206.17
55	1.36	0.32	29.94	1.29	19.58	50.82	3182.24	5206.08
54	1.42	0.35	31.21	1.39	19.17	51.77	3131.43	5206.00
53	1.4/	0.37	32.41	1.48	18.78	52.68	3079.65	5205.92
51	1.55	0.39	33.55	1.08	10,91	03.04 54.37	3020.98 2073 AA	5205.53
50	1.62	0.44	35.67	1.07	17 72	55 15	2919.07	5205.75
49	1.67	0.46	36.66	1.85	17.40	55.91	2863.92	5205.58
48	1.71	0.48	37.60	1.94	17.09	56.63	2808.01	5205.50
47	1.75	0.50	38.50	2.02	16.79	57.32	2751.39	5205.42
46	1.79	0.53	39.36	2.10	16.51	57.98	2694.07	5205.33
45	1.83	0.55	40.20	2.18	16.24	58.61	2636.10	5205.25
44	1.86	0.56	41.00	2.26	15.97	59.23	2577.48	5205.17
43	1.90	0.58	41,/0	2.33	15.72	59.82	2518.25	5205.08
42 41	1.95	0.60	42.50	2.41	15.40	60.39	2400.44	5205.00
40	2.00	0.64	43.89	2.55	15.02	61.46	2337 12	5204.83
39	2.03	0.66	44.55	2.62	14.80	61.97	2275,66	5204.75
38	2.05	0.67	45.18	2.69	14.59	62.46	2213.6 9	5204.67
37	2.08	0.69	45.79	2.76	14.38	62.94	2151.22	5204.58
36	2.11	0.71	46.38	2.83	14.19	63.39	2088.28	5204.50
35	2.13	0.72	46.94	2.90	14.00	63.84	2024.89	5204.42
34	2.10	0.74	47.49	2.96	13.81	04.27	1961.00	5204.33 5204.25
32	2.10	0.78	40.02	3.02	13.04	65.08	1832 11	5204.20
31	2.23	0.79	49.01	3.15	13.30	65.46	1767.03	5204.08
30	2.25	0.80	49.48	3.21	13.15	65.83	1701.57	5204.00
29	2.27	0.82	49.93	3.28	12.99	66.20	1635.75	5203.92
28	2.29	0.84	50.36	3.36	12.83	66.55	1569.55	5203.83
27	2.31	0.85	50.77	3.38	12.70	66.86	1503.00	5203.75
26	2.33	0.86	51.17	3.43	12.57	67.17	1436.14	5203.67
25	2.34	0.87	51.55	3.49	12.44	67.48	1368.96	5203.58
24	2.36	0.89	51.92	3.54	12.31	61.77 69 0E	1301.48	5203.50
23	2.30 2.20	0.90	52 60	3,64	12.19	60.00 68 32	1200./1	5203,42
21	2.00	0.92	52.92	3.69	11.97	68.58	1097.34	5203.33
20	2.42	0.93	53.22	3.74	11.86	68.82	1028.76	5203.17
19	2.43	0.95	53.51	3.78	11.76	69.06	959.94	5203.08
18	2.44	0.96	53.79	3.83	11.67	69.28	890.89	5203.00
17	2.46	0.97	54.05	3.87	11.58	69.49	821.61	5202.92
16	2.47	0.98	54.29	3.91	11.49	69.69	752.11	5202.83

82394 - System #3 - REV1

oject: 82394 - System	#3 - REV1		
Chamber Model -	MC-4500	¬ StormTec	, h
Units -	Imperial	Click Here for Metric	
Number of Chambers -	22	I derston of mutuer	DS
Number of End Caps -	4		
Voids in the stone (porosity) -	30	7%	
Base of Stone Elevation -	5201.50	ft	
Amount of Stone Above Chambers -	12	in I Include Perimeter Stone in Calculation	s
Amount of Stone Below Chambers -	9	in	
Area of system -	1116	sf Min. Area - 934 sf min. area	

Height of	Incremental Single	Incremental	Incremental	Incremental	Incremental	Incremental Ch,	Cumulative	
System	Chamber	Single End Cap	Chambers	End Cap	Stone	EC and Stone	System	Elevation
(inches)	(cubic feet)	(cubic feet)	(cubic feet)	(cubic feet)	(cubic feet)	(cubic feet)	(cubic feet)	(feet)
81	0.00	0.00	0.00	0.00	27.90	27.90	4000.09	5208.25
80 70	0.00	0.00	0.00	0.00	27.90	27.90	39/2.19	5208.17
79	0.00	0.00	0.00	0.00	27.90	27.90	3944.29	5208.08
70	0.00	0.00	0.00	0.00	27.90	27.90	3916.39	5208.00
70	0.00	0.00	0.00	0.00	27.90	27.90	3888.49	5207.92
76	0.00	0.00	0.00	0.00	27,90	27.90	3860.59	5207.83
73	0.00	0.00	0.00	0.00	27.90	27.90	3832.69	5207.75
73	0.00	0.00	0.00	0.00	27.80	27.80	3004./9	0207.07
70	0.00	0.00	0.00	0.00	27.00	27.90	3710.08	5207.50
71	0.00	0.00	0.00	0.00	27.90	27.90	3740,99	5207.00
70	0.00	0.00	0.00	0.00	27.90	27.50	3603 10	5207.42
69	0.04	0.00	0.00	0.00	27.63	28.53	3665 20	5207.33
68	0.12	0.00	2.55	0.00	27 12	20.00	3636 75	5207.20
67	0.16	0.03	3.62	0.11	26.78	30.51	3607.04	5207.08
66	0.21	0.05	4.59	0.19	26.47	31.25	3576.53	5207.00
65	0.27	0.07	5.90	0.27	26.05	32.22	3545.28	5206.92
64	0.45	0.09	9.96	0.35	24.81	35.12	3513.06	5206.83
63	0.67	0.11	14.64	0.45	23.37	38.46	3477.94	5206.75
62	0.80	0.14	17.58	0.57	22.46	40.60	3439.48	5206.67
61	0.91	0.17	19.98	0.67	21.71	42.35	3398.88	5206.58
60	1.00	0.19	22.06	0.77	21.05	43.88	3356.52	5206.50
59	1.09	0.22	23.92	0.86	20.47	45.25	3312.64	5206.42
58	1.16	0.24	25.60	0.97	19,93	46.49	3267.39	5206.33
57	1.23	0.27	27.15	1.08	19.43	47.66	3220.90	5206.25
56	1.30	0.30	28.59	1.19	18.96	48.75	3173.24	5206.17
55	1.36	0.32	29.94	1.29	18.53	49.77	3124.49	5206.08
54	1.42	0.35	31.21	1.39	18.12	50.72	3074.73	5206.00
53	1.47	0.37	32.41	1.48	17.73	51.63	3024.00	5205.92
52	1.53	0.39	33.55	1.58	17.36	52.49	2972.38	5205.83
51	1.57	0.42	34.64	1.67	17.01	53.32	2919.89	5205.75
50	1.62	0.44	35.67	1.76	16.67	54.10	2866.57	5205.67
49	1.67	0.46	36.66	1.85	16.35	54.86	2812.47	5205.58
48	1.71	0.48	37.60	1.94	16.04	55.58	2757.61	5205.50
41	1.75	0.50	38.50	2.02	15.74	56.27	2702.04	5205.42
46	1.79	0.53	39.36	2.10	15.46	56.93	2645.77	5205.33
45	1.83	0.55	40.20	2.18	15.19	57.56	2568.85	5205.25
44	1.80	0.56	41.00	2.26	14.92	58.18	2531.28	5205.17
43	1.90	0.58	41./0	2.33	14.67	56.77	2473.10	5205.00
42	1.93	0.00	42.00	2.41	14.43	09.04	2414.34	5205.00
41	1.90	0.02	43.21	2.40	14.19	39.00	2300.00	5204.92
30	2.00	0.04	43.05	2.00	13.87	60.41	2280.12	5204.03
38	2.03	0.00	44.00	2.02	13.75	61 41	22.04.71	5204.75
37	2.03	0.69	45 79	2.03	13 33	61 89	2112 37	5204.07
36	2.00	0.03	46 38	2.83	13 14	62 34	2050 48	5204.50
35	2.13	0.72	46.94	2.90	12.95	62.79	1988.14	5204.42
34	2.16	0.74	47.49	2.96	12.76	63.22	1925.35	5204.33
33	2.18	0.76	48.02	3.02	12.59	63.63	1862.14	5204.25
32	2.21	0.77	48,52	3.09	12.42	64.03	1798.51	5204.17
31	2.23	0.79	49.01	3.15	12.25	64.41	1734.48	5204.08
30	2.25	0.80	49.48	3.21	12.10	64.78	1670.07	5204.00
29	2.27	0.82	49.93	3.28	11.94	65.15	1605.30	5203.92
28	2.29	0.84	50.36	3.36	11.78	65.50	1540.15	5203.83
27	2.31	0.85	50.77	3.38	11.65	65.81	1474.65	5203.75
26	2.33	0.86	51.17	3.43	11.52	66.12	1408.84	5203.67
25	2.34	0.87	51.55	3.49	11.39	66.43	1342.71	5203.58
24	2.36	0.89	51.92	3.54	11.26	66.72	1276.28	5203.50
23	2.38	0.90	52.27	3,59	11.14	67.00	1209.56	5203.42
22	2.39	0.91	52.60	3.64	11.03	67.27	1142.56	5203.33
21	2.41	0.92	52.92	3.69	10.92	67.53	1075.29	5203.25
20	2.42	0.93	53.22	3.74	10.81	67.77	1007.76	5203.17
19	2.43	0.95	53.51	3.78	10.71	68.01	939.99	5203.08
18	2.44	0.96	53.79	3.83	10.62	68.23	871.99	5203.00
17	2.46	0.97	54.05	3.87	10.53	68.44	803.76	5202.92
16	2.47	0.98	54.29	3.91	10.44	68.64	735.31	5202.83

Project:

82394 - System #4 - REV1

Project:

oject:	62394 - System #4	- KEVI	-		
Chamber Mod	lel -	MC-4500]	StormTech	1
Units -		Imperial	Click He	eré for Metric	~
Number of Ch	ambers -	35		rand store of many	5
Number of En	d Caps -	4			
Voids in the st	tone (porosity) -	30	7%		
Base of Stone	Elevation -	5219.00	Tft .	File and the second second	٦
Amount of Sto	ne Above Chambers -	12	in	Include Perimeter Stone in Calculations	
Amount of Sto	ne Below Chambers -	9	lin		_
Area of syster	n -	1654	sf Min	n. Area - 1409 sf min. area	
		· · · · · · · · · · · · · · · · · · ·			

			-					
Height of	incremental Single	Incremental	Incremental	Incremental	Incremental	Incremental Ch,	Cumulative	
System	Chamber	Single End Cap	Chambers	End Cap	Stone	EC and Stone	System	Elevation
(Inches)				(CUDIC TEET)				(1005 75
90	0.00	0.00	0.00	0.00	41.33	41.30	0038./3	5225.75
79	0.00	0.00	0.00	0.00	41.35	41.35	5976.05	5225.07
78	0.00	0.00	0.00	0.00	41.35	41.35	5934 70	5225.50
77	0.00	0.00	0.00	0.00	41 35	41.35	5803 35	5225.00
76	0.00	0.00	0.00	0.00	41.35	41.35	5852.00	5225 33
75	0.00	0.00	0.00	0.00	41.35	41.35	5810.65	5225 25
74	0.00	0.00	0.00	0.00	41.35	41.35	5769.30	5225.17
73	0.00	0.00	0.00	0.00	41.35	41.35	5727.95	5225.08
72	0.00	0.00	0.00	0.00	41.35	41.35	5686.60	5225.00
71	0.00	0.00	0.00	0.00	41.35	41.35	5645.25	5224.92
70	0.00	0.00	0.00	0.00	41.35	41.35	5603.90	5224.83
69	0.04	0.00	1.43	0.00	40.92	42.35	5562.55	5224.75
68	0.12	0.01	4.06	0.04	40.12	44.22	5520.19	5224.67
107 68	0.16	0.03	5.77	0.11	39,59	45.46	54/5.9/	5224.58
65	0.21	0.03	0.30	0.19	39.10	40.00	5283.01	5224.00
64	0.45	0.09	15.85	0.35	36.49	52.69	5335.80	5224.42
63	0.67	0.11	23.28	0.45	34.23	57.97	5283.11	5224.25
62	0.80	0.14	27.97	0.57	32.79	61.32	5225.14	5224.17
61	0.91	0.17	31.78	0.67	31.61	64.07	5163.82	5224.08
60	1.00	0.19	35.10	0.77	30.59	66.46	5099.75	5224.00
59	1.09	0.22	38.06	0.86	29.67	68.59	5033.30	5223.92
58	1.16	0.24	40.72	0.97	28.84	70.53	4964.70	5223.83
57	1.23	0.27	43.19	1.08	28.07	72.34	4894.17	5223.75
56	1.30	0.30	45.49	1.19	27.35	74.03	4821.83	5223.67
55	1.36	0.32	47.64	1.29	26.67	75.60	4747.81	5223.58
54	1.42	0.35	49.66	1.39	26.04	77.08	46/2.21	5223.50
53	1.47	0.37	52.29	1.48	25.43	70.92	4090.12	5223.42
51	1.55	0.39	55 11	1.50	24.00	81.00	4010.04	5222,00
50	1.62	0.44	56 75	1.07	23.80	82 31	4355 73	5223 17
49	1.67	0.46	58.32	1.85	23 30	83.47	4273.42	5223 08
48	1.71	0.48	59.82	1.94	22.82	84.58	4189.95	5223.00
47	1.75	0.50	61.25	2.02	22.37	85.64	4105.37	5222.92
46	1.79	0.53	62.63	2.10	21.93	86.66	4019.73	5222.83
45	1.83	0.55	63.95	2.18	21.51	87.64	3933.07	5222.75
44	1.86	0.56	65.22	2.26	21.11	88.58	3845.43	5222.67
43	1.90	0.58	66.44	2.33	20.72	89.49	3756.85	5222.58
42	1.93	0.60	67.61	2.41	20.34	90.36	3667.35	5222.50
41	1.96	0.62	68.74	2.48	19.98	91.21	3576.99	5222.42
40	2.00	0.04	70 99	2.00	19.04	92.02	3460.78	5222.33
38	2.03	0.60	70.00	2.02	19.30	92.00	3300 97	5222.20
37	2.08	0.69	72.85	2.03	18.67	94 28	3207 42	5222.08
36	2.11	0.71	73.78	2.83	18.37	94.98	3113.14	5222.00
35	2.13	0.72	74.68	2.90	18.08	95.66	3018.16	5221.92
34	2.16	0.74	75.55	2.96	17.80	96.31	2922.50	5221.83
33	2.18	0.76	76.39	3.02	17.53	96.94	2826.19	5221.75
32	2.21	0.77	77.19	3.09	17.27	97.55	2729.25	5221.67
31	2.23	0.79	77.97	3.15	17.02	98.13	2631.71	5221.58
30	2.25	0.80	78.71	3.21	16.77	98.69	2533.58	5221.50
29	2.27	0.82	79.43	3.28	16.54	99.25	2434.88	5221.42
28	2.29	0.84	80.11	3.36	16.31	99.78	2335.64	5221.33
2/	2.31	0.85	8U.//	3.38	10.10	100.26	2235.85	0221.25 6224.47
20 25	2.35	0.80	01.47	3.43 2.40	10.90	100,74	2130.09	0221.1/ 5224 0P
20	2.04	0.07	82 80	3.48	15.70	101.20	2004.00	5221.00
23	2.38	0.90	83.15	3.59	15 33	102.07	1832.00	5220.92
22	2,39	0.91	83,68	3.64	15.15	102.48	1729.93	5220.83
21	2.41	0.92	84.19	3.69	14.99	102.87	1627.45	5220.75
20	2.42	0.93	84.67	3.74	14.83	103.24	1524.59	5220.67
19	2.43	0.95	85.13	3.78	14.68	103.59	1421.35	5220.58
18	2.44	0.96	85.57	3.83	14.53	103.93	1317.76	5220.50
17	2.46	0.97	85.98	3.87	14.39	104.25	1213.83	5220.42
16	2.47	0.98	86.37	3.91	14.26	104.55	1109.58	5220.33



		GENERAL NOTES
	1. U	SE TYPE "C" MANHOLE FOR DEPTHS OF LESS THAN 6'
	M	EASURED FROM INVERT TO RIM.
	2. C	ONTRACTOR HAS OPTION TO CONSTRUCT TYPE "C" ANHOLE IN LIEU OF TYPE "E" MANHOLE FOR DEPTHS OF
	3. D	ESIGN APPLIES TO 4' TO 6' I.D. MANHOLES.
	4. M	ANHOLE GREATER THAN 18' IN DEPTH SHALL ONLY BE
		CONSTRUCTION PRECAST CONCRETE SECTIONS.
	J. P	ENETRATIONS.
	6. 0	OMPACT ALL BACKFILL AROUND MANHOLE TO 95%.
	7. P	STITION MARNOLE OPENING OVER THE OPSILEAR SIDE
		CONSTRUCTION_NOTES
	٨. (CONCRETE PIPE SUPPORTS SHALL EXTEND OUTSIDE OF
	1	ANHOLE TO BELL OF FIRST JOINT AND SHALL CRADLE
	B. 1	THE PENETRATION INTO MANHOLE SHALL BE FLUSH TO
		" MAX., MEASURED AT SPRINGLINE OF PIPE.
	C. 1	MANHOLE MAY BE CONSTRUCTED OF CONCRETE BLOCK, CR.
		CONCRETE IF BLOCK OR BRICK PLASTER INSIDE AND OUT
	1	WITH 1/2" MORTAR. SEE DWG. 2118 FOR DETAILS.
	D. 1	PRECAST CONCRETE COVER, SEE DWG. 2107.
		STREET FOR FUTURE ADJUSTMENT OF MANHOLE FRAME TO
	1	PAVEMENT GRADE PLASTER INSIDE WITH 1/2" MORTAR.
	r. (BARS AT 6" O.C. KA. WAY FOR MANHOLE DEPTH OF 16'
		OR GREATER. NO. 4 BARS AT 12" O.C. EA. WAY FOR
		MANHOLE LESS THAN 16' IN DEPTH.
		PLANS.
	J. (5" GROUT FILLET ON UPPER HALF OF PIPE AND AROUND
		SASE. ISE A 5' X 5' CONCRETE PAD IN ALL AREAS.
	L. 1	FRAME AND COVER, SEE DWG. 2110.
	M. 1	CONCRETE, SEE SECTION 101.
	N	SLOPE 1" PER FT. FROM PIPE CROWN. SHELF TO BE 9" WIDE MIN.
	Q	APPROVED WATERSTOP TO BE COMPATIBLE WITH TYPE OF
	P	PIPE. STUDE TO BE INSTALLED AS PER SPEC. SECTION 920.
	s. 1	EMD (IN UNPAVED AREAS).
	т.	IN UNPAVED AREAS SET FRAME TO GRADE AND SLOPE TO
		×t 100.
-	REVISION	
	-14-01	SEWER
A COLORADO		MANHOLE TYPE"C"
1		DWC 2101
8		

	172. NORTH 1008505.	CEIMETERY IP 32 30	CONVENIENCE, CNTR	25	21 22 24 141	
	1 SU-2 IP 1 14A 19 1002201 21A 1002201 2/22/27	ALBUQU	P ACRES			
	MARCHART	SU-2/HC	SU-2 IP	SU-2 IP 10 23		T B 18 18 1 U-2/C-1 17 2 10 BLVD
A CONTRACTOR	2201 2202 SU2 FQR.C.2 SU-2 SU-2 SU2 FQR.C.2 WTH restrictions SU-2 IP SU-2 IP SU-2 IP SU-2 IP SU-2 IP 1003833 17A NORTH ULLENDE ISUAL AV	1 SU-2	P NORTH ALBUQUERQ ACRES TRAC	UE K. 2 SU-2.1 - 1 PRU (MXMN 64 D	(UNIT B)	
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				ALAMEDA'BI	LVD NE	
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LEGAL DESCRIPTION:

NOTES:

1. ALL SPOT ELEVATIONS REPRESENT FLOWLINE ELEVATION UNLESS OTHERWISE NOTED.

2. ALL CURB AND GUTTER TO 6" HEADER UNLESS OTHERWISE NOTED.

3. ALL RETAINING WALL DESIGN SHALL BE BY OTHERS.

LEGEND

		5414————— EXI	STING CONTOUR	
		5415 EXI	STING INDEX CONTOUR	
		5414 PR	DPOSED CONTOUR	
		5415 PR	DPOSED INDEX CONTOUR	
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	1 × 40 1•	048.25 EXI	STING SPOT ELEVATION	
	× 40	48.25 PR	DPOSED SPOT ELEVATION	
	·	во	JNDARY	
		CE	ITERLINE	
		RIG	HT-OF-WAY	
		PR	DPOSED CURB AND GUTTER	
		EXI	STING CURB AND GUTTER	
		PR	DPOSED SIDEWALK	
		PR	DPOSED SETBACK	
	· ·	PR	DPOSED LOT LINE	
	*****	PR	DPOSED SCREEN WALL	
N		PR	DPOSED RETAINING WALL	
A			ITS OF FLOODPLAIN	
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	ROUGH GRAD	ING APPROVAL	DATE	
	ENGINEER'S SEAL	AMERICA	Ν ΤΟΥΟΤΑ	DRAWN ^{BY} WCWJ
	NID SO			DATE
	OF W MEXICO M			2-05-15
	REC (14522) Hand	DRAINAG	<u>E PLAN</u>	21403-LAYOUT-1-25-14
	TO PROFESSIONALE		Ria Granda	SHEET #
GRAPHIC SCALE				_
50 25 0 25 50	2/5/15			
	DAVID SOLILE	-1	IOUO CENTRAL AVENUE SE SUITE 201 ALBUOUERQUE, NM 87106	JOB #
SCALE: 1"=50'	P.E. #14522		(505) 872–0999	21403