



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

March 24, 1999

Dennis A. Lorenz
Brasher & Lorenz, Inc.
2201 San Pedro NE
Bldg.1 Suite 210
Albuquerque, New Mexico 87110

RE: ENGINEER'S CERTIFICATION FOR ALEXIS PARK (C-18/D30) ENGINEER'S
CERTIFICATION STATEMENT DATED 3/15/99.

Dear Mr. Lorenz:

Based on the information provided on your March 16, 1999 submittal, Engineer's Certification
for the above referenced site is approved.

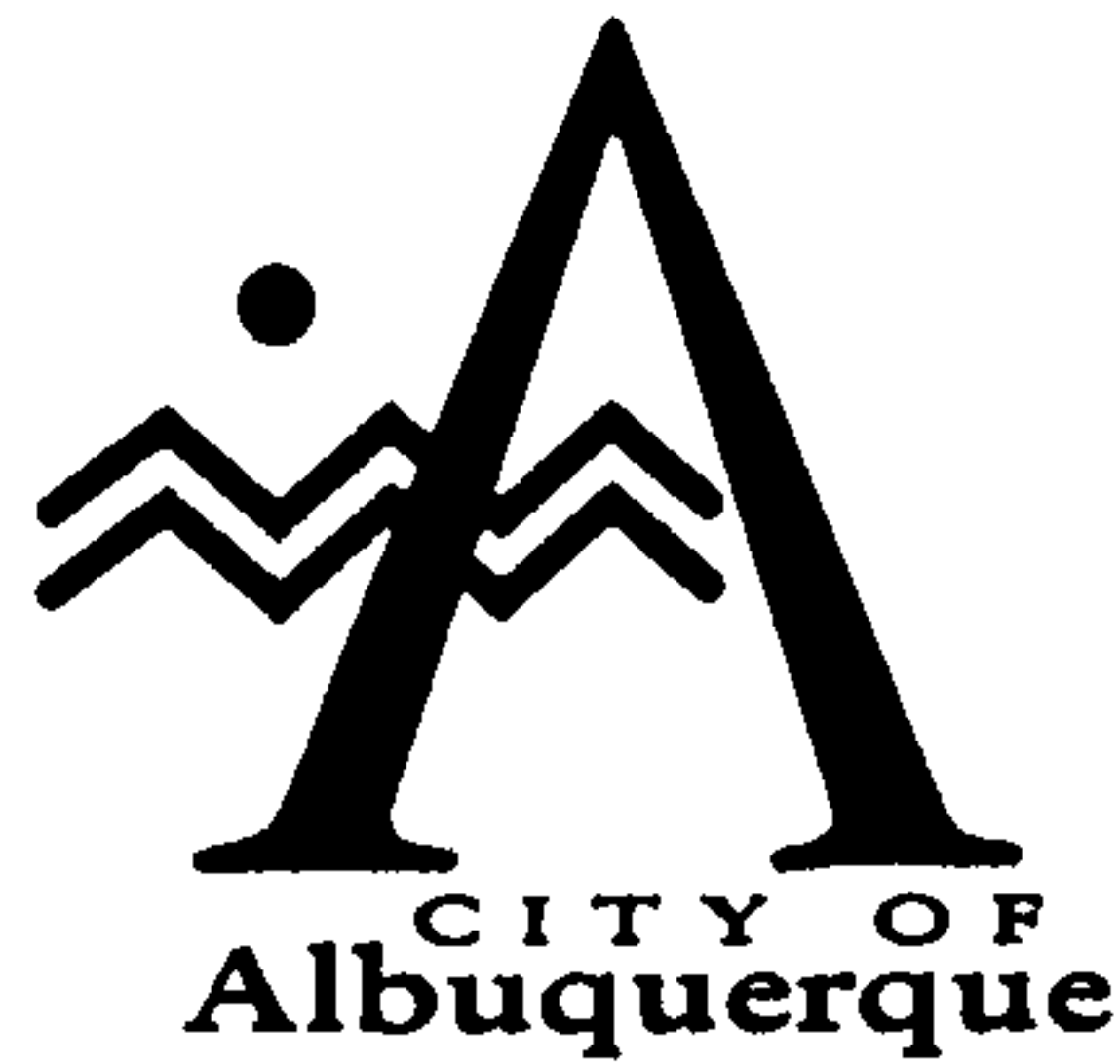
If I can be of any further assistance, please feel free to contact me at 924-3330.

Sincerely,

Andrew Garcia
Drainage Inspector

c: file

821-0439



July 28, 1998

Dennis A. Lorenz, P.E.
Brasher & Lorenz, Inc.
2201 San Pedro NE, Bldg. 1, Suite 210
Albuquerque, New Mexico 87110

***RE: Revised Drainage Plan for Alexis Park, Lots 9 & 10, Tract A, Unit B, NAA (C18/D30)
Submitted for Building Permit Approval, Engineer's Stamp Dated 7/28/98.***

Dear Mr. Lorenz:

Based on the information provided in the submittals of July 13, 1998 and July 28, 1998, the above referenced plan is approved for Building Permit release.

As you are aware, the Engineer's Certification must be submitted to and approved by this office prior to release of the Certificate of Occupancy.

If you have any questions, or if I may be of further assistance to you, please call me at 924-3982.

Sincerely,

Susan M. Calongne, P.E.
City/County Floodplain Administrator

c: File

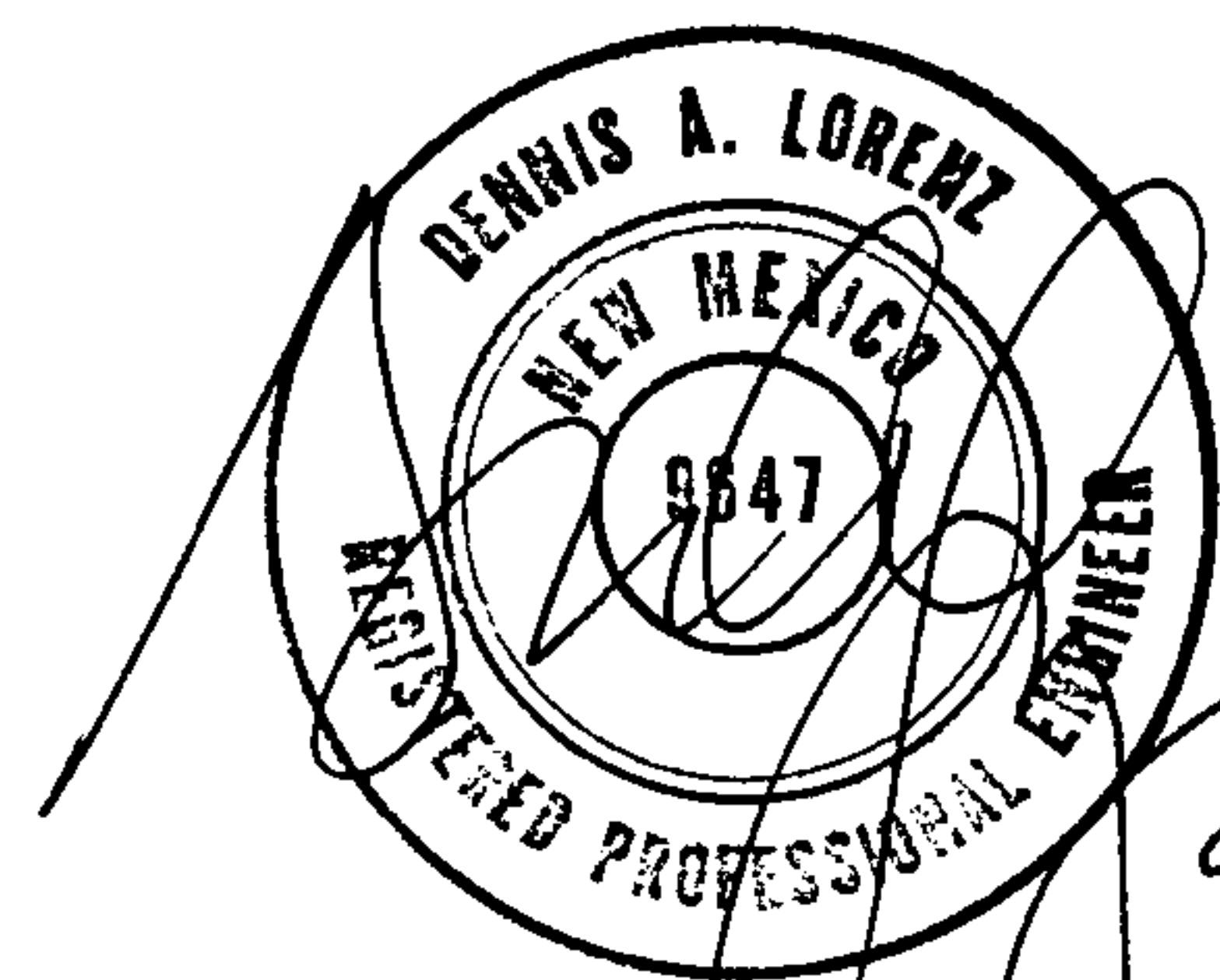
Good for You, Albuquerque!



SUPPLEMENTAL CALCULATIONS

FOR

ALEXIS PARK



9-25-96

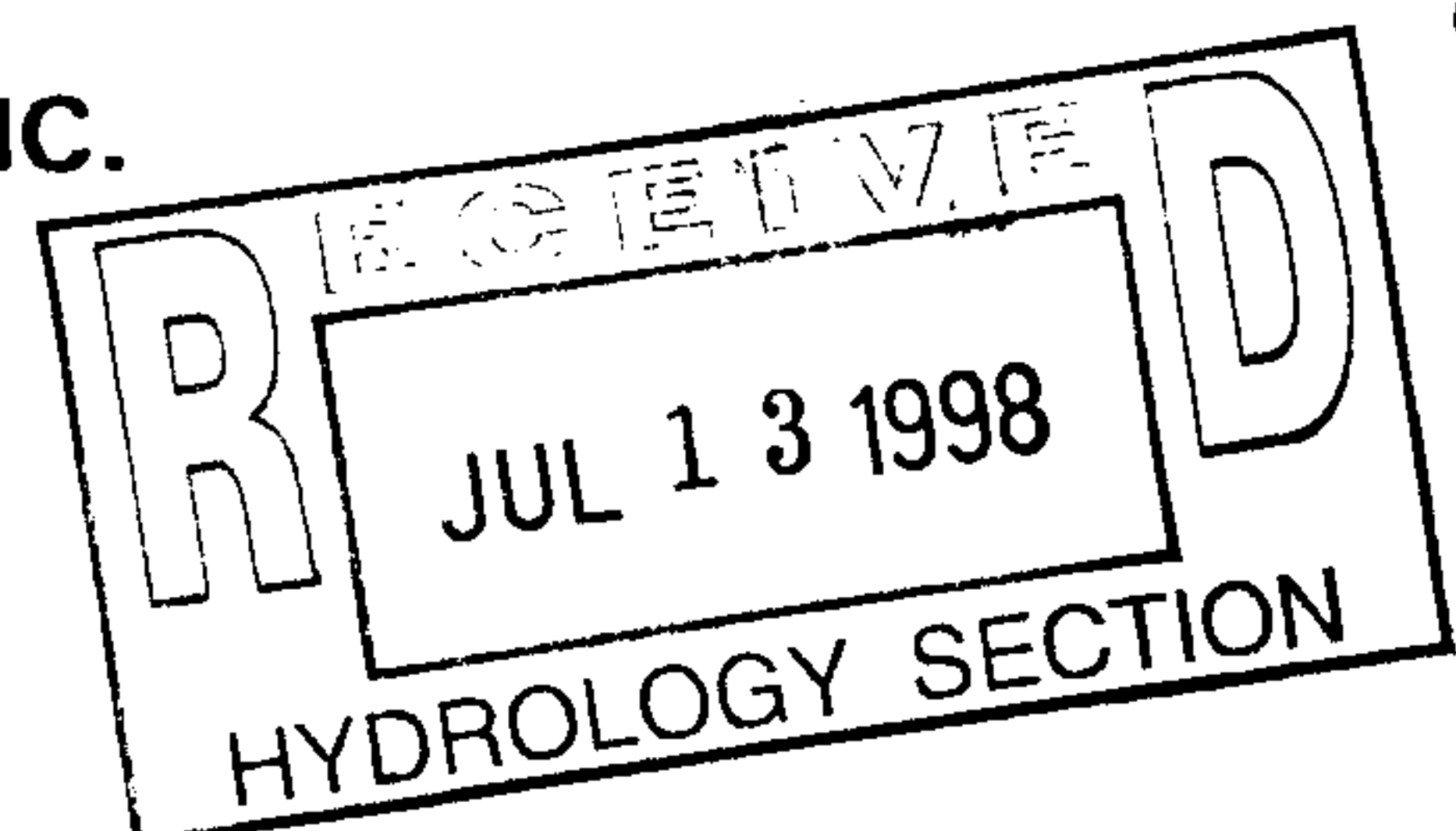
11-1-96

7-28-98

BRASHER & LORENZ, INC.

Consulting Engineers

September 1996



PROJECT NAME ALEXIS PARK JOB NO. 6044
SUBJECT POND ROUTING
BY _____ CHECKED BY _____ DATE 9.25.96 PAGE 1 OF 3

AS ESTABLISHED BY THE DRAINAGE REPORT
FOR MOTEL 6 (CIB-D27). MAX DISCHARGE IS
LIMITED TO HISTORIC.

PER AH4MO: $Q_{UNDEV} = 2.4 \text{ CFS}$

1. SIZE OUTLET FOR 2.4 CFS

BY ORIFICE EQN:

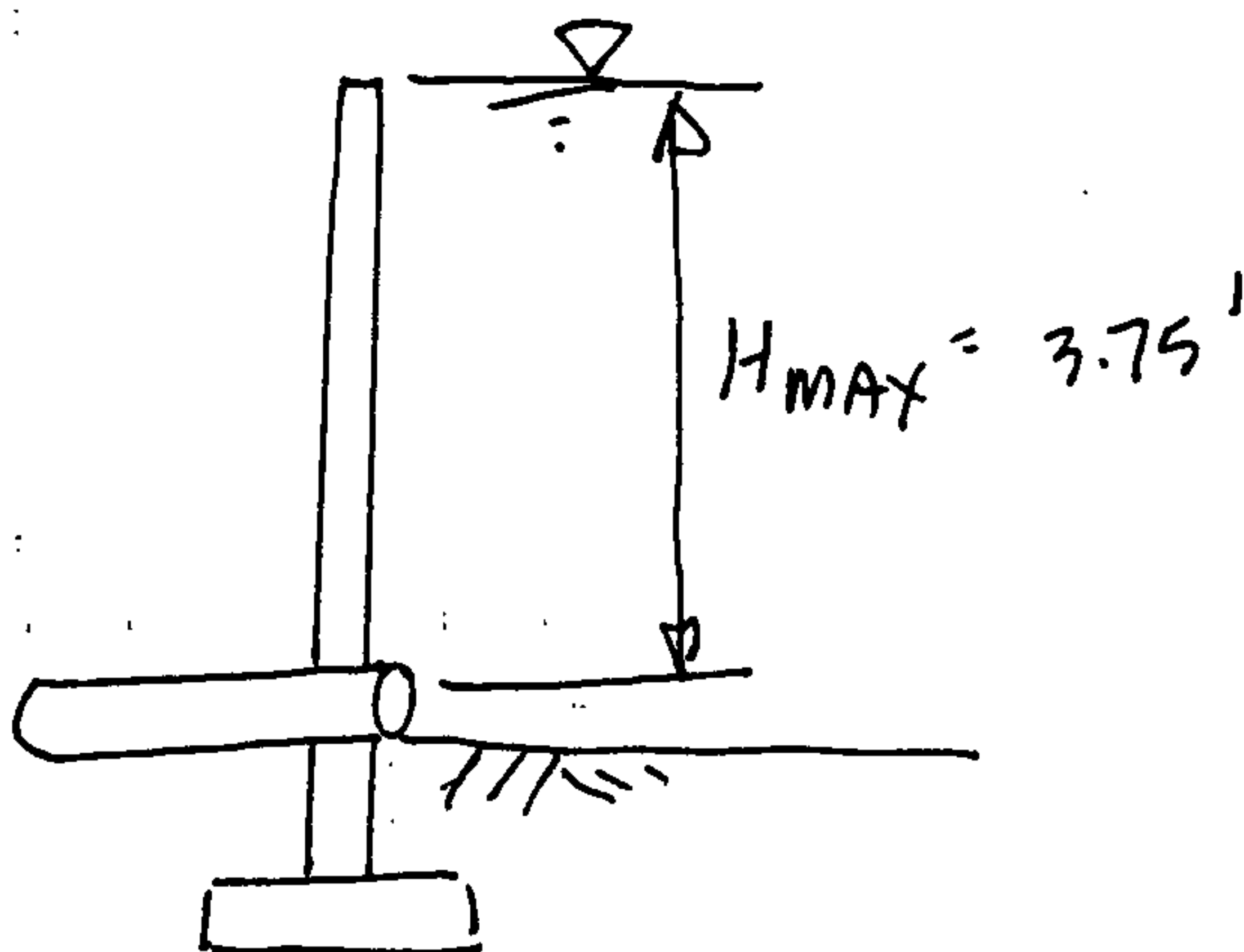
$$Q = CA\sqrt{2gh}$$

$$Q = Q_{OUT} = 2.4 \text{ CFS}$$

$$C = 0.6$$

$$g = 32.2 \text{ F/s}^2$$

$$h = 3.75'$$



SOLVING FOR A: $A = 0.25 \text{ SF}$

$\Rightarrow A(6" \text{ PIPE}) = 0.20 \text{ SF}$

PROJECT NAME ALEXIS PARK JOB NO. 6044

SUBJECT POND ROUTING

BY _____ CHECKED BY _____ DATE 9-25-96 PAGE 2 OF 3

ROUT RES TABLE

ELEV	H.	Q _{OUT}	VOL
97.5	0	0	0
98.5	0.75'	0.83	1350 CF
99.5	1.75	1.27	2700
100.5	2.75	1.60	4050
101.5	3.75	1.86	5400

PER HYMO OUTPUT:

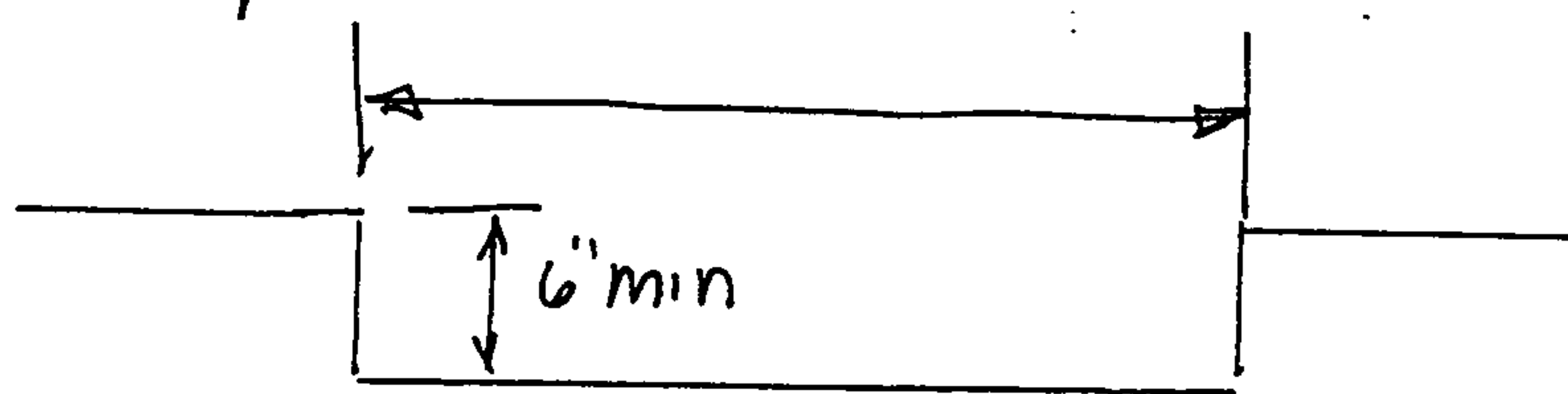
Q_{OUT} PEAK = 1.75 CFS
VOLUME = 0.1114 AF
= 4853 CF
MAX WSE = 5101.09

PROJECT NAME ALEXIS PARK JOB NO. 6044
 SUBJECT POND RUNDOWN + SPILLWAY
 BY _____ CHECKED BY _____ DATE 9-25-96 PAGE 3 OF 3

SIZE RUNDOWN FROM PARKING LOT AND
 POND OVERFLOW SPILLWAY.

$Q_{100} = 6.1 \text{ CFS}$

RUNDOWN + SPILLWAY WILL HAVE SAME
 GEOMETRY.



SECTION

NTS

WEIRS

Enter up to 10 weirs.
 Enter <Return> only for flowrate and length to end.

FLOWRATE (CFS)	LENGTH (FT)	COEFF (-)	HEAD (FT)
6.10	6.9	2.500	0.50

7' PROVIDED.

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994
INPUT FILE = 6044P.DAT

RUN DATE (MON/DAY/YR) =09/23/1996
USER NO.= BRASHERE.I01

[illegible]

OFF-SITE ANALYSIS

PURPOSE

The purpose of this off-site analysis is to determine the storm drainage improvement requirements for Wilshire Avenue, between San Pedro Drive NE and the I-25 East Frontage Road. This analysis studies the existing and future developed drainage basins contributing to the roadway, and recommends improvements to safely convey excess runoff to improved drainage facilities.

EXISTING CONDITIONS

Presently the contributing off-site basin is partially developed. The basin consists of developed land along Wilshire Avenue between San Pedro and the East Frontage Road, and undeveloped land east of San Pedro. The existing peak flow rate is estimated at 56.3 cfs. Runoff is conveyed by Wilshire Avenue, which consists of a temporary pavement section from San Pedro to the East Frontage Road. A short permanent section exists along the Imaging Concepts frontage. The basin presently outfalls to a private detention pond located within the I-25 right-of-way, just west of Imaging Concepts. This pond has a storage capacity of approximately 31,000 cubic feet and drains by a 30 inch storm drain.

The Drainage Report for Imaging Concepts, prepared by D. Mark Goodwin & Associates, 1994, anticipated a peak developed flowrate in the Wilshire north curb of 25.7 cfs (see appendix).

DEVELOPED CONDITIONS

Under fully developed conditions the contributing off-site basin will be truncated at San Pedro, due to City drainage criteria which prohibits surface drainage from crossing collector streets. It is anticipated that a storm drain will be constructed in San Pedro to collect upstream flows from Signal and Wilshire. The storm drain will likely connect to a storm drain proposed in Corona. The resulting developed surface flow in Wilshire Avenue at the Frontage Road is estimated at 57.5 cfs. Since Imaging Concepts anticipated only 25.7 cfs the excess flow will be routed south along the Frontage Road to the Corona culverts, which have excess capacity. Alexis Park will provide a drainage structure at the Wilshire/Frontage Road intersection to drain 31.8 cfs south into the I-25 right-of-way. Runoff will be conveyed in a roadside swale to 2-24 inch culverts located at the Motel 6 access drive, then on to the 8-48 inch culverts located at Corona.

FINDINGS

This off-site analysis makes the following findings:

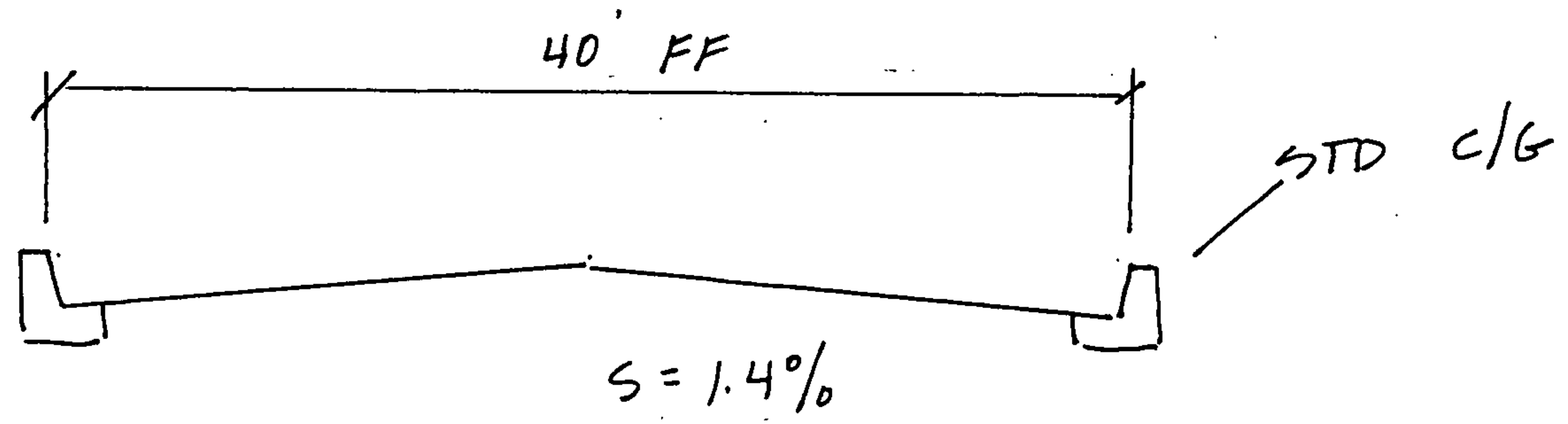
1. Developed conditions result in a peak flowrate of 57.5 cfs.
2. Wilshire Avenue has sufficient capacity to carry developed flows to the East Frontage Road.
3. Imaging Concepts anticipated 25.7 cfs in the Wilshire north curb, which drains to an existing private detention pond located within the I-25 right-of-way.
4. Alexis Park will construct the south one-half of Wilshire along the project frontage.
5. A drainage structure will be constructed to drain the difference between future developed flowrate of 57.5 cfs and the Imaging Concepts flowrate of 25.7 cfs (31.8 cfs) south to the Corona culverts.
6. Two 24 inch culverts will be provided at the Motel 6 access drive to drain future developed flows along the Frontage Road to the Corona culverts.
7. The Corona culverts have capacity to drain the excess runoff from Wilshire Avenue.

PROJECT NAME ALEXIS PARK JOB NO. 6044
SUBJECT STREET DEPTH
BY _____ CHECKED BY _____ DATE 11-1-96 PAGE 1 OF 5

WILSHIRE STREET DEPTH:

Q₁₀₀ EXIST = 56.3 CFS BASIN (A) HYD 101
Q₁₀₀ DEV = 57.5 CFS BASIN (B) HYD 103

TEST FOR DEV CONDITION @ Q = 57.5 CFS



VARIABLES LIST:
Y - FLOW ELEVATION Q - FLOWRATE S - CHANNEL SLOPE

VARIABLE TO BE SOLVED (Y, Q OR S) ? Y Enter up to 20 cross-section points.
Enter <Return> only for distance to end.

Q (CFS) ? 57.5
S (FT/FT) ? .014

CROSS-SECTION POINTS					
DIST	ELEV	COEFF	DIST	ELEV	COEFF
0	100.67.017				
0	100.00.017				
20	100.40.017				
40	100.00.017				
40	100.67.017				

RESULTS
=====

Y=	100.51 FT
A=	12.24 SF
P=	41.02 FT
V=	4.70 FPS
F=	1.50 SUPER-CRITICAL FLOW

PROJECT NAME ALEXIS PARK JOB NO. 6044
SUBJECT _____
BY _____ CHECKED BY _____ DATE 11-1-96 PAGE 2 OF 5

WILSHIRE DOWNSTREAM CAPACITY:

PER APPROVED REPORT FOR IMAGING CONCEPTS
DESIGN FLOW FOR NORTH CURB = 25.7 CFS.

COMPUTED DESIGN FLOW FOR WILSHIRE
(BASIN 'A') = 57.5 CFS. EXCESS RUNOFF
NOT ANTICIPATED BY IMAGING CONCEPTS
WILL BE DRAINED FROM THE SOUTH
CURB AND CONVEYED TO THE EXISTING
CULVERTS LOCATED AT CORONA, WHERE
EXCESS CAPACITY EXISTS.

$$\text{DIVERTED } Q = 57.5 - 25.7 = \underline{\underline{31.8}} \text{ CFS.}$$

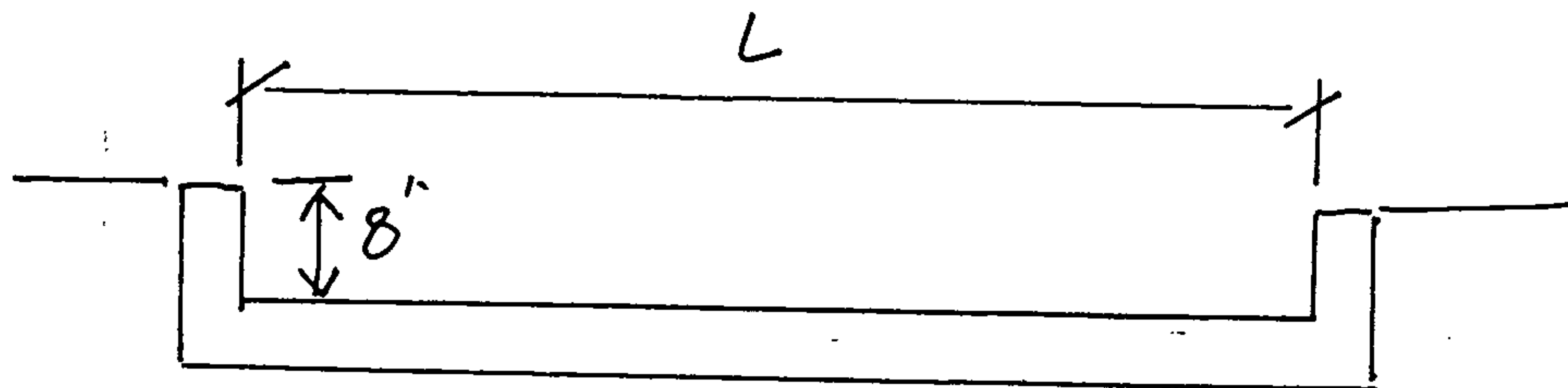
STREET DESIGN FOR WILSHIRE (SOUTH SIDE)
TO PROVIDE RUNDOWN WITH 31.8 CFS
CAPACITY.

PROJECT NAME ALEXIS PARK JOB NO. 6044

SUBJECT RUNDOWN.

BY _____ CHECKED BY _____ DATE 11-1-96 PAGE 3 OF 5

PROVIDE RUNDOWN AT WILSHIRE
SOUTH CURB:



SECTION

NTS

BY WEIR EQN:

$$Q = CLH^{3/2}$$

$$H = 0.67 \text{ (CURB HT)}$$

$$C = 2.70$$

$$Q = 31.8 \text{ CFS}$$

Enter up to 10 weirs.

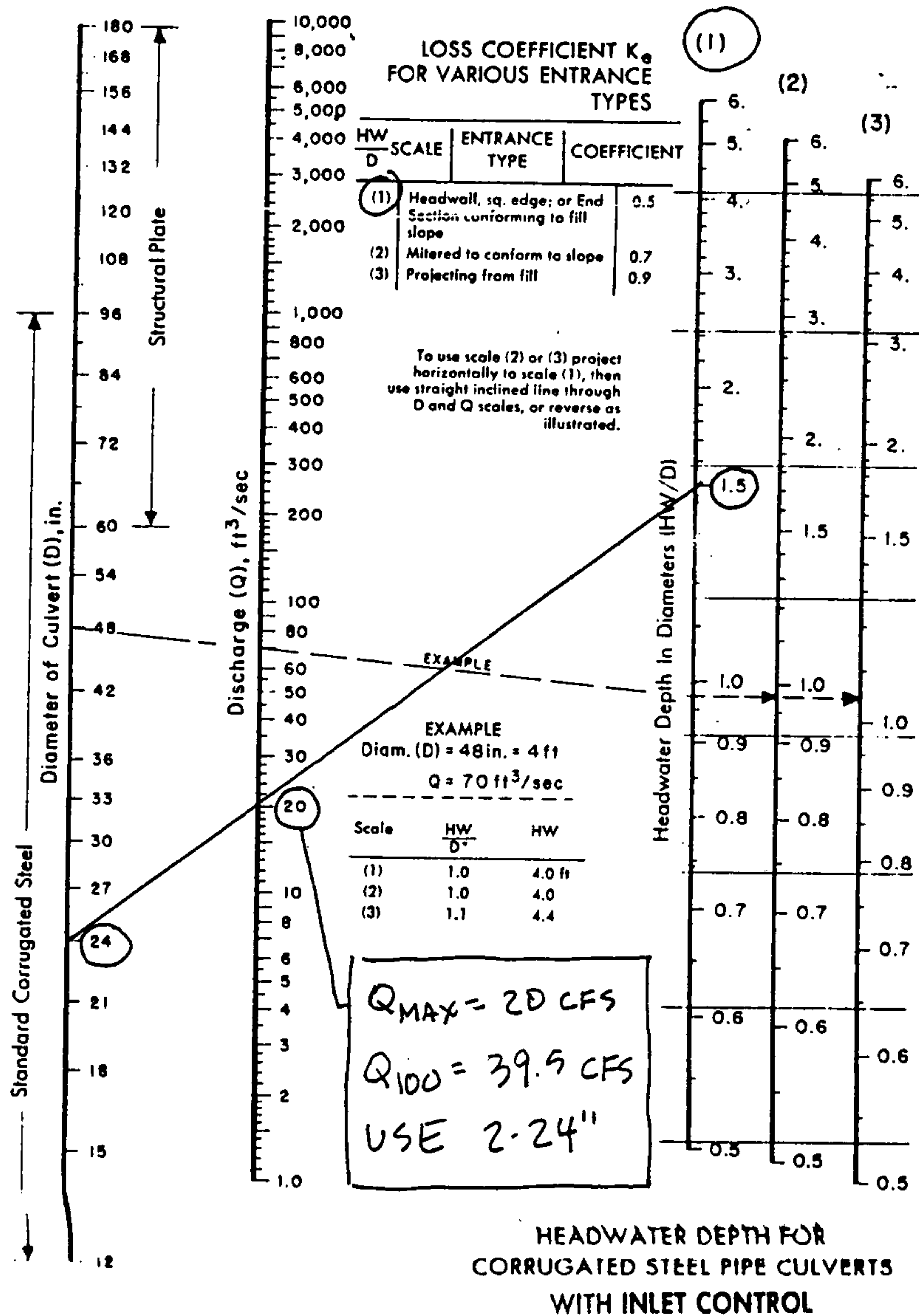
Enter <Return> only for flowrate and length to end.

FLOWRATE (CFS)	LENGTH (FT)	COEFF (-)	HEAD (FT)
32.00	21.6	2.700	0.67

USE 22'

PROJECT NAME ALEXIS PARK JOB NO. 6044
 SUBJECT CULVERT DESIGN @ MOTEL 6
 BY _____ CHECKED BY _____ DATE 9-25-96 PAGE 4 OF 5

CAPACITY @ 24" CMPS PROVIDED BY MOTEL 6



FHWA HEC 5

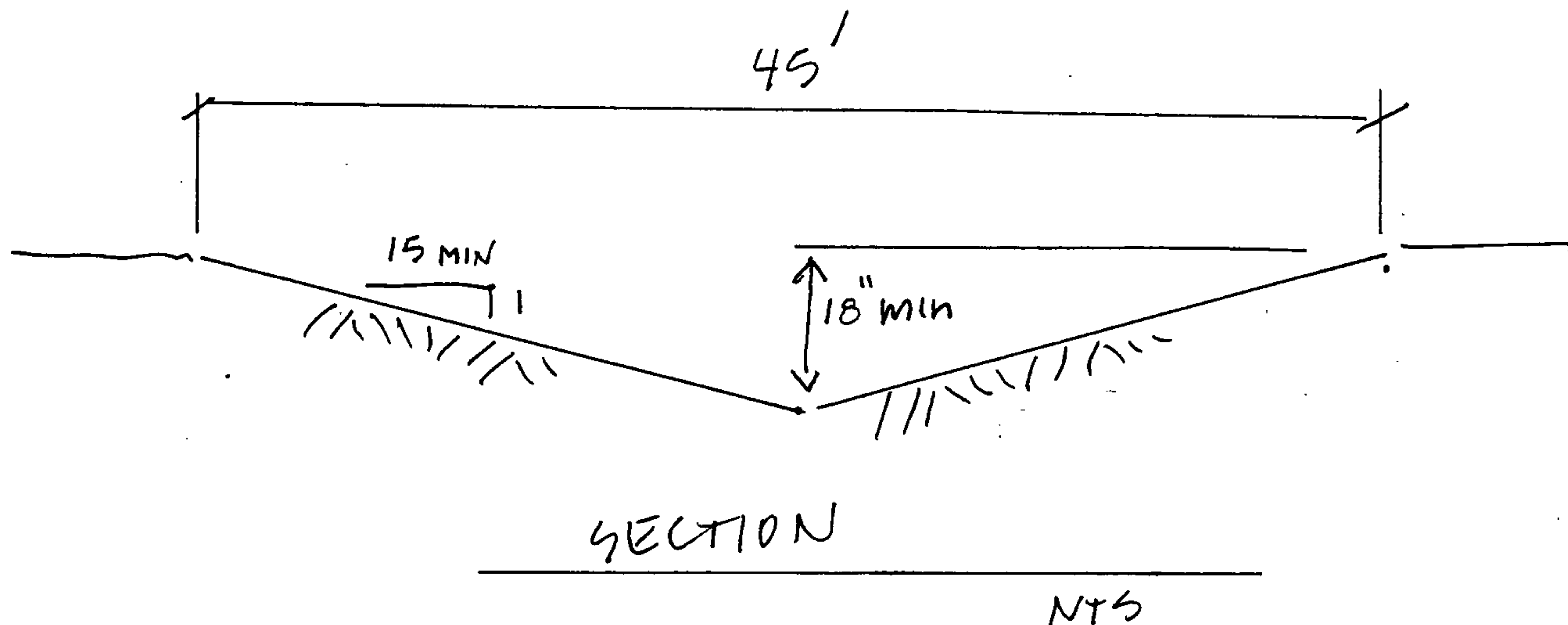
Figure 4-28 Inlet control nomograph for corrugated steel pipe culverts. The manufacturers recommended keeping HWID to a maximum of 1.5 and preferably to no more than 1.0.

PROJECT NAME ALEXIS PARK JOB NO. 6044

SUBJECT _____

BY _____ CHECKED BY _____ DATE 11-1-96 PAGE 5 OF 5

SWALE SECTION W/IN ± 25 R/W:



VARIABLES LIST:

Y - FLOW DEPTH

B - CHANNEL BOTTOM WIDTH

S - CHANNEL SLOPE

Q - FLOWRATE

M - CHANNEL SIDE SLOPE

N - CHANNEL ROUGHNESS

VARIABLE TO BE SOLVED (Y, Q, B, M, S OR N) ? Y

Q (CFS) ? 40
B (FT) ? 0
M (FT/FT) ? 15
S (FT/FT) ? .01
N (FT^{1/6}) ? .025

RESULTS

=====

Y=	0.88 FT
A=	11.64 SF
P=	26.49 FT
V=	3.44 FPS
F=	0.91

SUB-CRITICAL FLOW

NON-EROSIVE. PROVIDE EROSION CONTROL AT
END OF RUNDOWN, POND OUTLET + 24" CMP
INLETS PER DETAIL C/6.

North and South Domingo Baca Arroyos and Paseo del Norte Corridor Drainage Management Plan

SUBMITTED TO:

Albuquerque Metropolitan Arroyo
Flood Control Authority
Albuquerque, New Mexico



Resource Technology, Inc.

ENGINEERS & ENVIRONMENTAL SCIENTISTS

2129 OSUNA NE - SUITE 200, ALBUQUERQUE, NEW MEXICO 87113

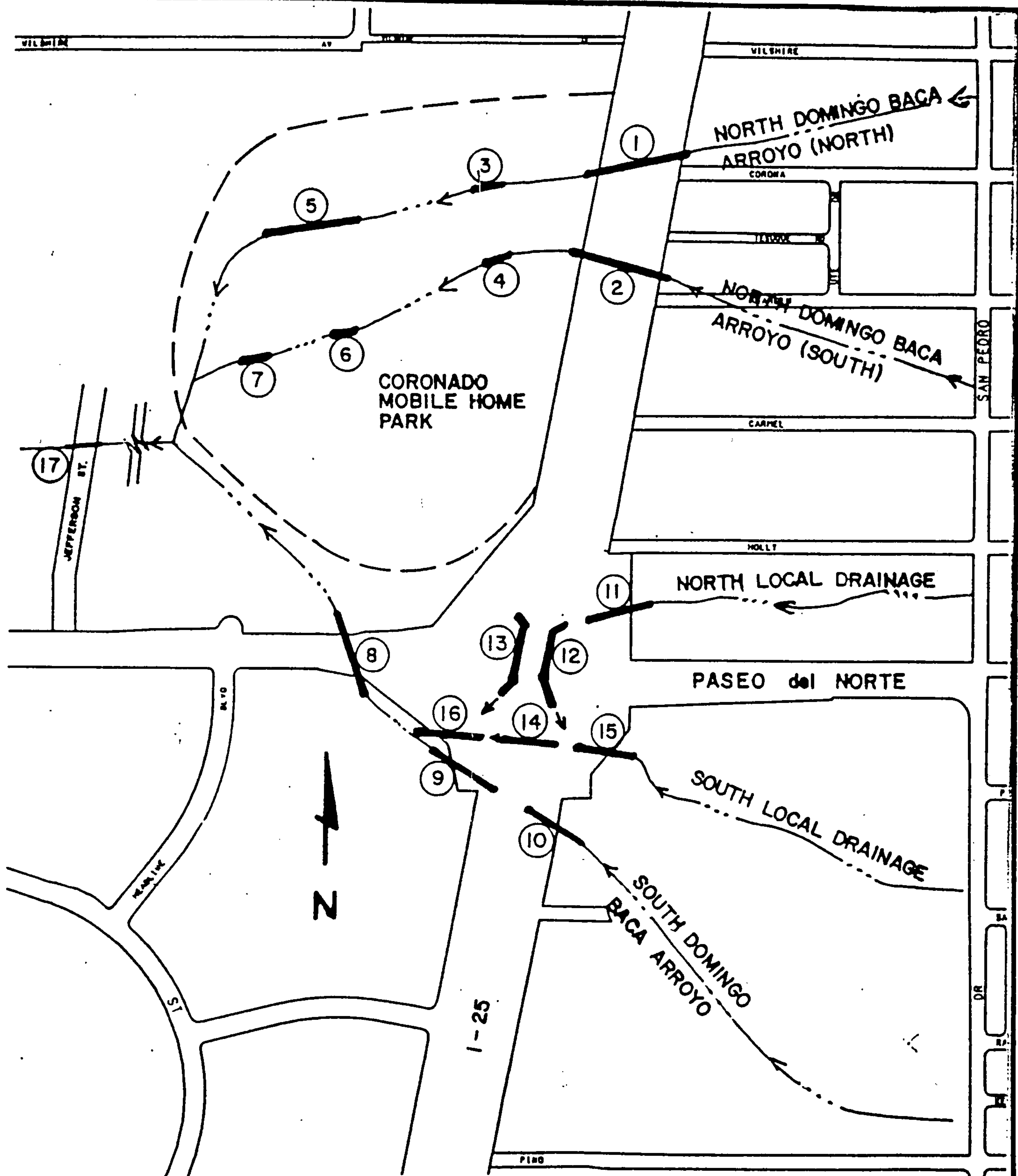
TELEPHONE - (505) 345 - 3115

in association with

Holmes & Narver Inc.

RTI PROJECT NO. 90 - 090

DECEMBER 1991



SUMMARY OF I-25, PASEO DEL NORTE AND CORONADO MOBILE HOME PARK CULVERTS

TABLE

SUMMARY OF 1-25, PASEO DEL NORTE AND CORONADO MOBILE HOME PARK CULVERTS
ASSUMING CULVERT FLOW

STRUCTURE NUMBER	QUANTITY AND DESCRIPTION	MAXIMUM FLOW DEPTH NO SEDIMENT (ft)	EXISTING AVAILABLE FLOW DEPTH		EXISTING MAXIMUM CAPACITY Assuming Culvert Flow (cfs) (a)	CAPACITY AT LOW CHORD OR SOFFIT Assuming Uniform Flow (cfs)	100-YR HYDROLOGIC RESULTS		
			INLET (ft)	OUTLET (ft)			EXISTING CONDITION (cfs)	FUTURE CONDITION OPTION H6-1 (cfs) (b)	FUTURE CONDITION OPTION G2/J (cfs) (c)
1	8 - CMP'S 4'	4.00	4.00	4.00	600		630	650	420
2	4 - CBC'S 4'H X 9'W	4.00	4.00	4.00	1250		390	90	360
3	1 - CMP 5.67'H X 8.5'W	5.67	5.67	5.50	360		630	680	(e)
4	2 - CMP'S 5.67'H X 8'W	5.67	5.67	5.67	500		390	90	780(f)
5	1 - CMP 5.5'H X 8'W	5.50	5.00	1.70	200		630	670	(e)
6	2 - CMP'S 5.5'H X 8'W	5.50	3.70	3.70	300		390	90	900(f)
7	1 - CMP 5'H X 13'W	5.00	4.70	4.70	450		390	90	900(f)
8	4 - CBC'S 8'H X 10'W	8.00	5.97	6.50	3500	10450	3340	8690	5980
9	4 - CBC'S 8'H X 10'W	8.00	7.57	8.00	3600		2840	8150	5440
10	4 - CBC'S 8'H X 10'W	8.00	6.29	8.00*	3500	10850	2840	8150	5450
11	4 - CMP'S 4'	4.00	4.00	4.00	450		240	330	330
12	2 - CMP'S 4'	4.00	4.00	4.00	120		310	400	400
13	1 - CMP 4'	4.00	4.00	4.00	140		NC	NC	NC
14	2 - RCP'S 5'	5.00	5.00	5.00	350		490	620	620
15	2 - CMP/RCP' 5'	5.00	5.00	5.00	300		160	170	170
16	2 - RCP'S 5'	5.00	5.00	5.00	300		490	620	620
17	4 - CBC's 8'H X 10'W	8.00	4.00	5.50	3500	10450	4360	9760	7080

NC Not Computed.

(a) Computed based on culvert hydraulics - assuming open culvert.

(b) Diversions from North Domingo Baca Basin at Ventura, Wyoming and San Pedro to Paseo del Norte Channel, outfall to South Domingo Baca Arroyo west of San Pedro.

(c) Based on Option G2/J - Paseo del Norte Diversion to South Domingo Baca Arroyo west of San Pedro and a detention dam near Louisiana on the North Domingo Baca Arroyo.

(e) Recommend that these culverts be abandoned in future. Divert runoff from outfall of structure 1 to outfall of structure 2 in a concrete channel (recommended).

(f) Culverts must be replaced.

* Not surveyed.

C:\MAIN\WRITE\DOMINGO\REPORT\CULHYD.SUM

RESOURCE TECHNOLOGY, INC.
ENGINEERS & ENVIRONMENTAL SCIENTISTS

2129 Osuna Road, NE Suite 200

Albuquerque, NM 87113

Phone: (505) 345-3115

Fax: (505) 345-4132

PROJECT NO.

SHEET

BY

ER

DATE 08/03/98

DESCRIPTION OF CULVERT STRUCTURES

Structure No.	Quantity	Opening Size (a)	Description	Inlet Invert Elev. (b)	Outlet Invert Elev. (b)	Existing available flow depth (ft)	
						Inlet	Outlet
①	8	4 ft dia (L = 350 ft)	RCP @ Inlet CMP @ Outlet	5194.80	5185.90	4	4
2	4	4 ft (H) x 9 ft (W) (L = 300 ft)	Concrete Box Culverts	5193.42	5188.42	3.58	3.58
3	1	5.8 ft (R) x 7.5 ft (S) (L = 30 ft)	CMP Arch (Structural Plate)	5130.20	5130.20	5.8	5.8
4	2	5.6 ft (R) x 9.0 ft (S) (L = 30 ft)	CMP Arch (Struct. Plate)	5183.30	5182.50	5.6	5.6
5	1	5.9 ft (R) x 8.5 ft (S) (L = 400 ft)	CMP Arch (Struct. Plate)	5138.29	5155.80	5.9	5.9
6	2	4.3 ft (R) x 9.5 ft (S) (L = 30 ft)	CMP Arch (Struct. Plate)	5157.10	5156.20	4.3	4.3
7	1	4.0 ft (R) x 12.4 ft (S) (L = 35 ft)	CMP Arch (Struct. Plate)	5153.10	5152.90	4.0	3.50

(a) The given sizes are "actual size" available for flow.

(b) These inlet and outlet invert elevations represent elevations of tops of sediment deposition in culverts. If there was no sediment deposition in culvert, these elevations represent true invert elevations. If the rise or height in "Opening Size" column is equal to existing available flow depth, it means that there is no sediment in it (for the particular structure).

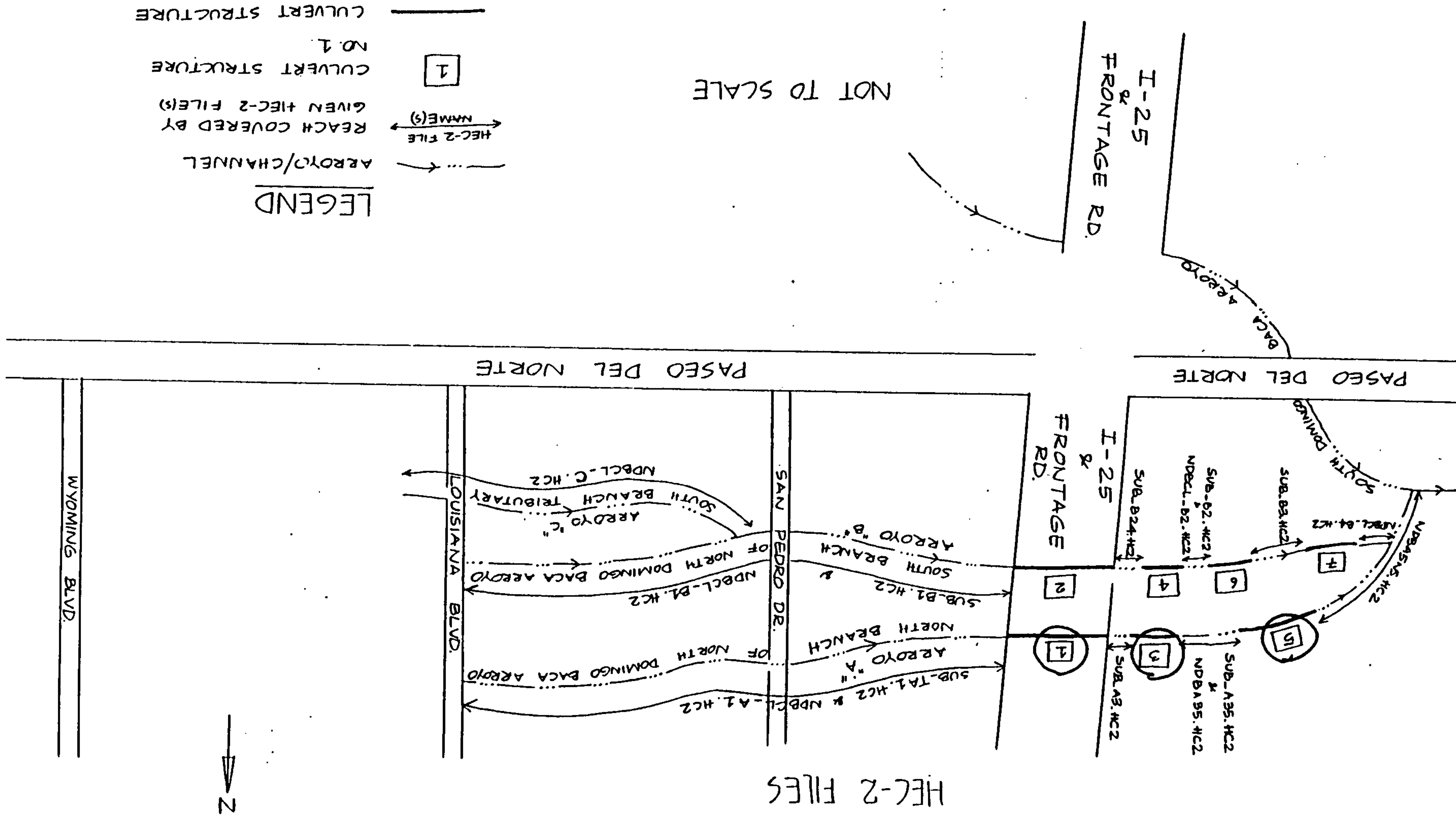
$$\text{Top elev. of opening} = 5193.42 + 3.58 = 5197.0$$

for str # ②

Note: There was no sediment deposition in culverts structures nos ①, ③, ④ & ⑤.

RESOURCE TECHNOLOGY, INC.
 FLOMR FOR NORTH DOMINGO BACA ARROYOS
 RTI PROJECT NO. 94-200-1-3

SCHEMATIC DIAGRAM ILLUSTRATING CULVERT STRUCTURES AND
 REACHES COVERED BY
 HEC-2 FILES



NOT TO SCALE



D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT Imaging Concepts
SUBJECT Drainage
BY JNM DATE 7/5/94
CHECKED _____ DATE _____
SHEET _____ OF _____

Grading and Drainage for Site Plan Approval

Pre-Design Conference Findings:

1. An approved drainage plan is required
2. Downstream capacity needs to be addressed based upon the developed condition of the contributing basin.
3. Existing capacity and ownership of the flow path for the 30" storm drain west of I-25 needs to be addressed.
4. The storm drainage capacity of Wilshire and Signal needs to be addressed.
5. Coordination and permits are required from the Highway Department.

Solutions Approach:

SA) 2. We will restrict the developed flows from our site to the historical rate. That means the contributing basin will remain as is: the existing developed condition (see attached off-site basin map) and all flows from this basin will be aimed into the 30" storm drain that passes beneath I-25.



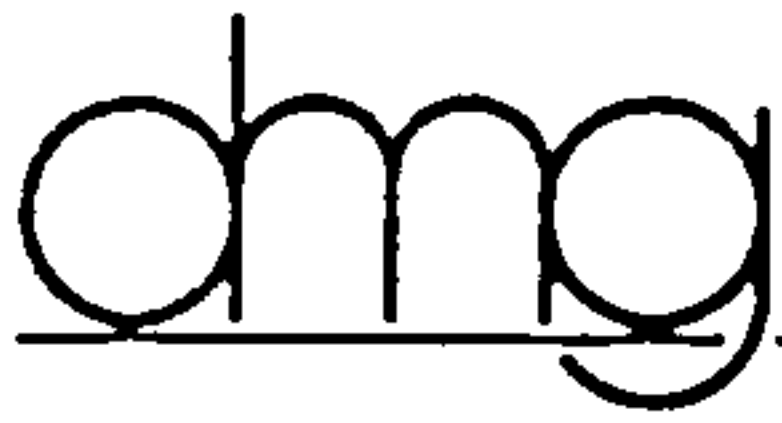
D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT Imaging Concepts
SUBJECT Drainage
BY JMM DATE 7/5/94
CHECKED _____ DATE _____
SHEET _____ OF _____

- SA) 3. The capacity of the 30" SD system is controlled by its inlet just east of the I-25 frontage road (see attached orifice-controlled backwater calculation). For our development, the peak flow through this system will not change.

There is evidence that suggests this outfall west of I-25 is directed north toward the Alameda interchange and then west in the Alameda Blvd storm drain. The Highway Department has received a plan to verify this outfall.

- SA) 4. Eventually, Wilshire and Signal will consist of new standard curb and gutter with 40' of Face to Face permanent pavement. These streets will be required to contain and convey all developed flow. From the attached AHYMO, the upstream off-site basin collects runoff from the area east of our site and discharges into the 1/2 street section (shown as $Q_{roadside} = 21.2 \text{ cfs}$ for Signal and $Q_{roadside} = 25.7 \text{ cfs}$ for Wilshire on our plan). From the attached street capacity chart, it can be shown that one half of the street conveys approximately 50 cfs. therefore, we contend that the proposed surface features will be sufficiently sized to carry the anticipated roadside flows.



D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT Imaging Concepts
SUBJECT Drainage
BY JMM DATE 7/5/94
CHECKED _____ DATE _____
SHEET _____ OF _____

SA) 4. (cont.)

Once flows reach the west ends of the respective streets, they will be directed into 6' concrete channels to be built along the Frontage road. This width should provide sufficient access to perform maintenance.

SA) 5. The Highway Department will be receiving a copy of this plan for review and comment.



D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT Landfill
SUBJECT Drainage
BY JMM DATE 7/29/21
CHECKED _____ DATE _____
SHEET _____ OF _____

PROPOSED PONDING AREA

To design the proposed ponding area, the existing conditions must be evaluated. The existing ponding capacity was determined as follows:

<u>Elevation</u>	<u>Area (ft²)</u>	<u>Depth (ft)</u>	<u>Avg Area (ft²)</u>	<u>Cumm. Volume (ft³)</u>
96.0	480	1.0	1120	
97.0	1760	1.0	2880	4000 (0.092 Ac.F)
98.0	4000	1.0	7450	
99.0	10900	1.0	19250	30700 (0.705 Ac.F)
100.0	27600			

At elevation 98.0, the pipe opening acts as a weir

$$Q = 2.9 L H^{3/2} = 2.9 (3.93) (1.25)^{3/2} = 15.9 \text{ cfs}$$

At elevation 100.0, the pipe opening acts as an orifice

$$Q = CA \sqrt{2gH} = 0.65 (4.91) \sqrt{2(32.2)(1.9)} = 35.3 \text{ cfs}$$



D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT Imaging Concepts
SUBJECT Drainage
BY GMM DATE 7/29/94
CHECKED _____ DATE _____
SHEET _____ OF _____

Placing these parameters in the AILYMO route
reservoir routine revealed the following:

Peak discharge of 31.61 cfs occurs @ 1 hour and
40 minutes into the storm

The maximum water surface is 99.62

According to a letter issued by Ms. Raymunda Van Hoven
of the State Highway Department on July 20, 1994, she
suggests that a detention pond equivalent to
a volume equal to approximately one-third of
the basin's total volume, or 0.71 Ac.Ft. (30934 ft^3),
would be adequate. She also suggests placing
the bottom of the pond at 12 inches below the
invert of the discharge pipe. Our proposed pond,
as identified on the plan, will have a bottom
at 94.90 and a top at 99.0. The average area
of this pond between the top and bottom elevation is:

Elevation	Area	Depth	Avg Area	Volume
95.	4658 ft^2	4 ft.	7757 ft	31028 ft^3
99.0	10857 ft^2			

-371

OMPANY

5A

25

24

23

10

22

12

16

SU-1 FOR AUTO SALES SERV RE

SU-2

SU-2 IP

17

NORTH

SU-2

SIGNAL

SP-80-352

OFF-SITE
BASIN A

OFF-SITE
BASIN C

3

15

16

13

OFF-SITE BASIN B

WILSHIRE

SU-2 IP

2

16

14

SU-2 IP

17

1

32

1

32B

32A

1

A

32

S

SAN PEDRO BLVD

SP-80-424

A

NEW MEXICO STATE HIGHWAY
AND TRANSPORTATION DEPARTMENT
DISTRICT THREE

P.O. BOX 91750
ALBUQUERQUE, NEW MEXICO 87199-1750
TELEPHONE (505) 841-2700
Fax (505) 841-2790

Telecopier (Fax) Transmittal Instructions

Date August 8, 1994

Attachments No. 2
(Incl. this sheet)

FAX TO: 827-5345

To: G. O. x District No. 3 Other

DRAINAGE SECTION Room 217

Attn: RAYMUNDA A. VAN HOVEN, DRAINAGE ENGINEER

Subject: Imaging Concepts Conceptual Grading and Drainage Plan
Review; IDC dated 08/03/94

Remarks: THE OWNER SHOULD MAINTAIN THE POND FOR WEEDS, DEBRIS,
AND LITER. WE CAN MOW THE SHOULDERS DURING ROUTINE MOWING
OPERATIONS. THE OWNER WILL NEED TO CONSTRUCT SHOULDERS WITH A
MINIMUM SLOPE OF 6:1 FROM THE ROADWAY TO THE FLOOR OF THE POND.

From: STEVEN P. HARRIS
DISTRICT MAINTENANCE ENGINEER

New Mexico State
Highway & Transportation Department

I N T R A - D E P A R T M E N T A L C O R R E S P O N D E N C E
=====

SUBJECT: Comments for Imaging Concepts Conceptual
Grading and Drainage Plan Review.

Date: 8-8-94

TO: Raymunda A. Van Hoven
Drainage Engineer

File Reference:
R/W General

FROM: Robert Lopez, Supervisor
Property Management

Attention of:

Your request for comments regarding the subject drainage project has been reviewed by the Property Management Unit and the Railroad and Utilities Section of the Right of Way Bureau. Since this project requires a drainage structure within right of way, District #3 will have to coordinate with Imaging Concepts through permit or agreement, however the District wants to handle it, approval of the project within the right of way.

If you have questions or need more information please contact me at 5349, ext. 218.

xc: J. Ruiz
T. Gallegos

I N T R A - D E P A R T M E N T A L C O R R E S P O N D E N C E

Date: 10/12/94

File Ref:

Attention of:

IMAGING CONCEPT

I concur with Mr. John Curtin's comments on his letter to Mr. John McKenzie dated 9/19/94 (copy attached), and should be addressed prior to issuance of the permit. It is determined from Mr. John McKenzie's calculation that the water will not overtop the Frontage Road as well as the Interstate at 100 year-6 hour rainfall.

An agreement between the developer and the Department should be prepared for the developers's maintenance of the detention pond. I have no further comments.

ALAMEDA DEVELOPMENT

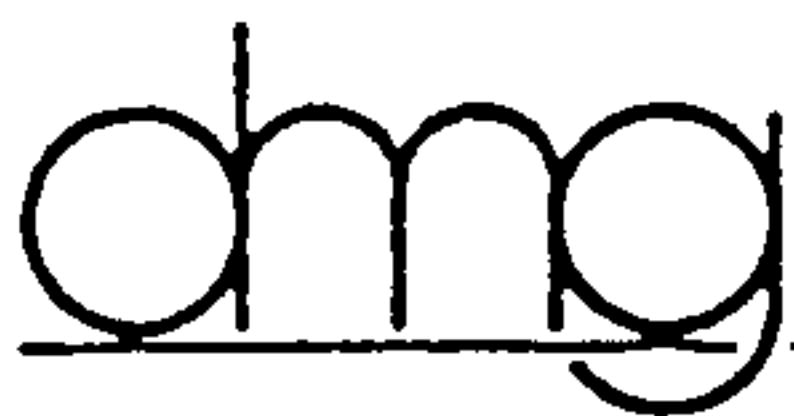
The revised system is anticipated not to impact the roadway, however, since the pipe will be connected directly into the existing storm sewer system, it is advisable to regulate the discharge into the existing system.

I recommend to change the 12" outlet pipe from detention pond "B" to 8" outlet pipe. Otherwise, the drainage recommendations are reasonable.

If I can be of further assistance, please let me know.

/ RVH

xc: Bill Moore
✓ John McKenzie, DMG & Assoc.



D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT Imaging Concepts
SUBJECT Drainage
BY JMM DATE 9/13/94
CHECKED _____ DATE _____
SHEET _____ OF _____

Design of features to be constructed at this site consist of the outlets for the ponding area in the north parking lot and for the ponding area in the south parking lot. On-site ponding for this site will consist of detention of developed flows with discharge into the Alameda Blvd. storm drain system at the historic rate of 3.81 cfs (see AHYMO run). 75% of the discharge (based upon basin area) of on-site developed flow, in addition to the off-site flow that is being passed through, will be controlled from the north parking lot while the remaining 25% will be controlled discharge from the south parking lot.

A previously submitted AHYMO reservoir routing output was provided with a previous submittal and is again being included herewith. The anticipated maximum water surface was identified as 5199.41. With our design, this water surface elevation will not change.



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Frontage Road Channel

Channel North of CMP Culvert (from Signal Ave.)

$$Q = \text{Off-site Basin "C" (previous submittal)} = 21.2 \text{ cfs}$$

$$\text{Length of Opening w/ 8" curb} = L = \frac{21.2}{2.9(.67)^{1.5}} = 13.3'$$

Maximum flow for this channel occurs where the 11.6 cfs joins the off-site flow of 21.2 cfs

Channel Dimensions: 6' x 8" WP = 7.34' Area = 4 ft²

$$Q = \frac{1.49}{.015} (4)(0.55)^{.67} (.016)^{.5}$$

$$\text{min slope} = 1.6\%$$

$$r_H = 0.55$$

$$Q = 33.74 \text{ cfs} \quad \text{capacity required} = 32.7 \text{ cfs} \quad V = \frac{Q}{A} = 8.4 \text{ fps}$$

Channel South of CMP Culvert (from Wilshire Ave.)

$$Q = \text{Offsite Basin "B" (previous submittal)} = 25.7 \text{ cfs}$$

$$L = \text{Length of opening w/ 8" curb} = \frac{25.7}{2.9(.67)^{1.5}} = 16'-2"$$

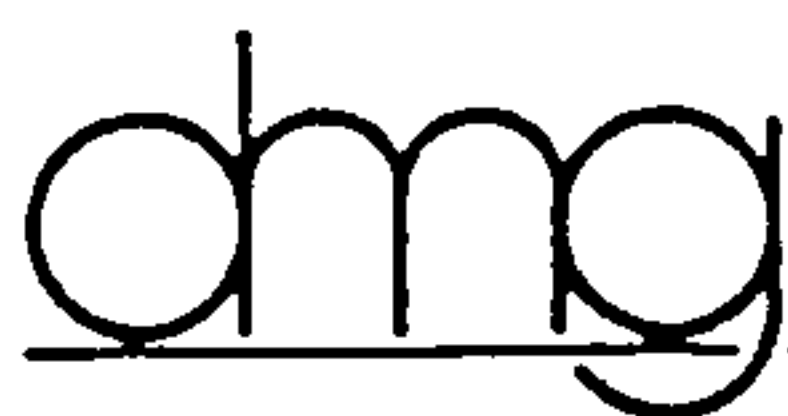
Maximum flow for south portion is 25.7 + 2.2 = 27.9 cfs

Capacity of this channel at 1.1% slope is

$$Q = \frac{1.49}{.015} (4.0)(.55)^{.67} (.011) = 27.92 \text{ cfs}$$

South of the channel junction the capacity is:

$$Q = \frac{1.49}{.015} (4.0)(0.55)^{.67} (.0093)^{.5} = 25.7 \text{ cfs} \quad V = 6.4 \text{ fps}$$



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North Ponding Area Outlet Structure & Spillway

Developed flow = $(.75)(\text{on-site developed}) = 6.44 \text{ cfs}$

Off-site "Passed Through Flow" = 5.20 cfs

Historic On-Site = $(.75)(\text{on site historic}) = 2.86 \text{ cfs}$

The control device will restrict discharge
to 8.06 cfs . Height of pond curbing is $18"$.

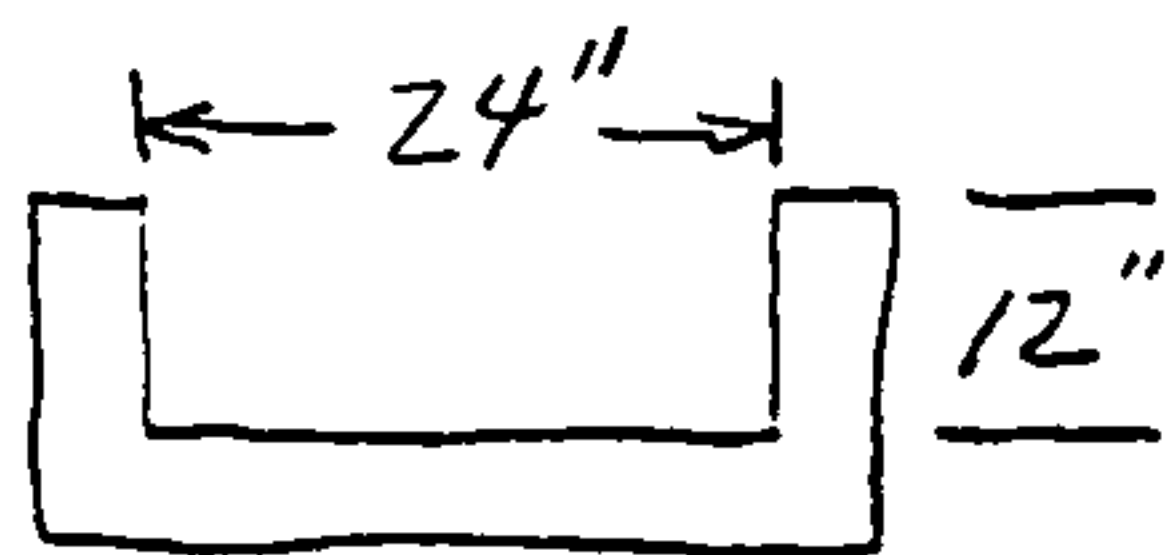
$$L = \frac{Q}{2.9(H)^{1.5}} = \frac{8.06}{2.9(1.5)^{1.5}} = 1.51' \text{ use } 18" \text{ wide opening}$$

The spillway opening must be able to exclusively
discharge the above rate and 75% of the developed
flow from this area.

$$Q = 75\% (\text{developed flow}) + \text{off-site "pass through"} \\ 6.44 \text{ cfs} + 5.20 \text{ cfs} = 11.64 \text{ cfs}$$

$$L = \frac{11.64}{2.9(.67)^{1.5}} = 7.32 \text{ use } 7' - 4"$$

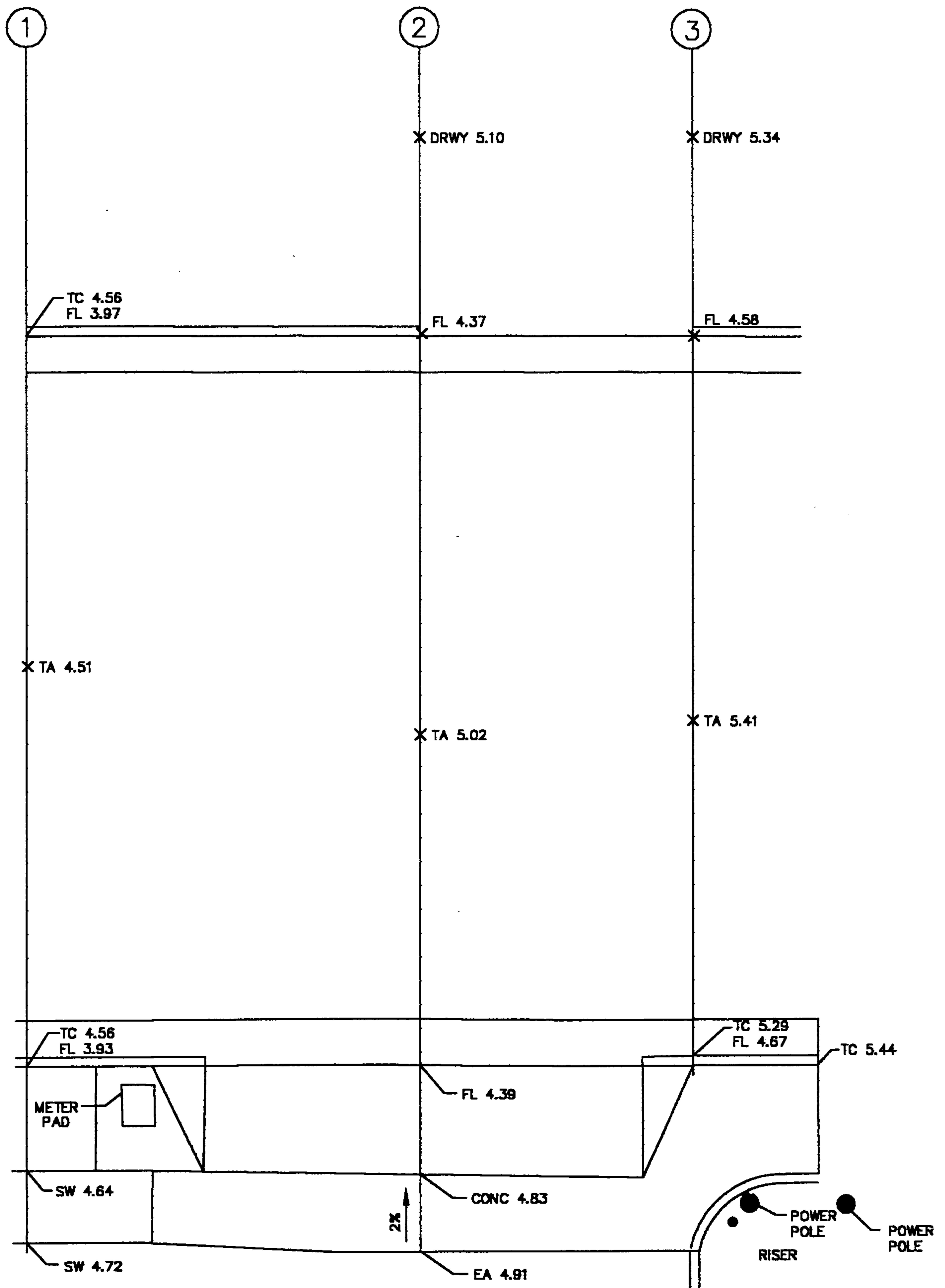
Channel Below Spillway



WP = 3 Area = 2

$r_H = 0.67$ slope = 0.6%

$$Q = \frac{1.49}{.015} (2(.67)^{.67} (.006)^{.5}) = 11.72 \text{ cfs}$$



SCALE: 1 INCH = 10 FT

Plan: Plan 01 River: Wilshire Reach:1 Riv Sta: 1 Profile: PF#1

W.S. Elev (ft)	4.45	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.62	Wt. n-Val.		0.017	
E.G. Elev (ft)	5.07	Reach Len. (ft)			
Crit W.S. (ft)	4.62	Flow Area (sq ft)		9.09	
E.G. Slope (ft/ft)	0.033856	Area (sq ft)		9.09	
Q Total (cfs)	57.50	Flow (cfs)		57.50	
Top Width (ft)	36.40	Top Width (ft)		36.40	
Vel Total (ft/s)	6.32	Avg. Vel. (ft/s)		6.32	
Max Chl Dpth (ft)	0.52	Hydr. Depth (ft)		0.25	
Conv. Total (cfs)	312.5	Conv. (cfs)		312.5	
Length Wtd. (ft)		Wetted Per. (ft)		36.89	
Min Ch El (ft)	3.93	Shear (lb/sq ft)		0.52	
Alpha	1.00	Stream Power (lb/ft s)		3.29	
Frctn Loss (ft)	0.43	Cum Volume (acre-ft)			
C & E Loss (ft)	0.03	Cum SA (acres)			

Plan: Plan 01 River: Wilshire Reach:1 Riv Sta: 4 Profile: PF#1

W.S. Elev (ft)	5.50	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.20	Wt. n-Val.		0.017	
E.G. Elev (ft)	5.71	Reach Len. (ft)	0.00	0.00	0.00
Crit W.S. (ft)	5.50	Flow Area (sq ft)		16.01	
E.G. Slope (ft/ft)	0.006040	Area (sq ft)		16.01	
Q Total (cfs)	57.50	Flow (cfs)		57.50	
Top Width (ft)	40.75	Top Width (ft)		40.75	
Vel Total (ft/s)	3.59	Avg. Vel. (ft/s)		3.59	
Max Chl Dpth (ft)	0.82	Hydr. Depth (ft)		0.39	
Conv. Total (cfs)	739.8	Conv. (cfs)		739.8	
Length Wtd. (ft)	0.00	Wetted Per. (ft)		41.67	
Min Ch El (ft)	4.68	Shear (lb/sq ft)		0.14	
Alpha	1.00	Stream Power (lb/ft s)		0.52	
Frctn Loss (ft)	0.00	Cum Volume (acre-ft)		0.00	
C & E Loss (ft)	0.01	Cum SA (acres)		0.02	

Plan: Plan 01 River: Wilshire Reach:1 Riv Sta: 3 Profile: PF#1

W.S. Elev (ft)	5.27	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.41	Wt. n-Val.		0.017	
E.G. Elev (ft)	5.67	Reach Len. (ft)	11.00	6.50	6.50
Crit W.S. (ft)	5.40	Flow Area (sq ft)		11.23	
E.G. Slope (ft/ft)	0.018668	Area (sq ft)		11.23	
Q Total (cfs)	57.50	Flow (cfs)		57.50	
Top Width (ft)	39.88	Top Width (ft)		39.88	
Vel Total (ft/s)	5.12	Avg. Vel. (ft/s)		5.12	
Max Chl Dpth (ft)	0.69	Hydr. Depth (ft)		0.28	
Conv. Total (cfs)	420.8	Conv. (cfs)		420.8	
Length Wtd. (ft)	6.50	Wetted Per. (ft)		40.01	
Min Ch El (ft)	4.58	Shear (lb/sq ft)		0.33	
Alpha	1.00	Stream Power (lb/ft s)		1.68	
Frctn Loss (ft)	0.00	Cum Volume (acre-ft)		0.00	
C & E Loss (ft)	0.02	Cum SA (acres)		0.02	

Plan: Plan 01 River: Wilshire Reach:1 Riv Sta: 2 Profile: PF#1

W.S. Elev (ft)	4.81	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.70	Wt. n-Val.		0.017	
E.G. Elev (ft)	5.51	Reach Len. (ft)	11.00	11.00	19.00
Crit W.S. (ft)	5.00	Flow Area (sq ft)		8.56	
E.G. Slope (ft/ft)	0.045547	Area (sq ft)		8.56	
Q Total (cfs)	57.50	Flow (cfs)		57.50	
Top Width (ft)	39.59	Top Width (ft)		39.59	
Vel Total (ft/s)	6.72	Avg. Vel. (ft/s)		6.72	
Max Chl Dpth (ft)	0.44	Hydr. Depth (ft)		0.22	
Conv. Total (cfs)	269.4	Conv. (cfs)		269.4	
Length Wtd. (ft)	11.00	Wetted Per. (ft)		39.64	
Min Ch El (ft)	4.37	Shear (lb/sq ft)		0.61	
Alpha	1.00	Stream Power (lb/ft s)		4.12	
Frctn Loss (ft)	0.18	Cum Volume (acre-ft)		0.00	
C & E Loss (ft)	0.03	Cum SA (acres)		0.01	