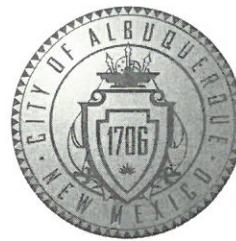


# CITY OF ALBUQUERQUE



September 29, 2016

Richard J. Berry, Mayor

David Soule, P.E.  
Rio Grande Engineering  
P.O. Box 93924  
Albuquerque, NM 87199

**RE: Legacy NAA Apartments  
Grading and Drainage Plan & Report  
Engineer's Stamp Date 9-15-2016 (File: C18D064B)**

Dear Mr. Soule:

Based upon the information provided in your submittal received 9-19-2016, the above-referenced plan is approved for Preliminary Plat Approval (#1009881). It is approved for ESC Building Permit (and ESC Grading Permit) with the following conditions:

PO Box 1293

1. Ensure that the Contractor receives the modified grate detail (Std Drawing #2220) to use on this project.
2. Ensure that the Contractor receives a legible version of the detail sheet.
3. The placement of the inline drains which was referenced in our previous review letter will be reviewed at CO.

Albuquerque

New Mexico 87103

[www.cabq.gov](http://www.cabq.gov)

Please attach a copy of this approved plan in the construction sets when submitting for a building permit. Prior to Certificate of Occupancy release, Engineer Certification per the DPM checklist will be required.

If you have any questions, you can contact me at 924-3986.

Sincerely,

A handwritten signature in black ink, appearing to read "Abiel Carrillo".

Abiel Carrillo, P.E.  
Principal Engineer, Planning Dept.  
Development Review Services

Orig: Drainage file



# City of Albuquerque

Planning Department

Development & Building Services Division

## DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV 02/2013)

Project Title: \_\_\_\_\_ Building Permit #: \_\_\_\_\_ City Drainage #: \_\_\_\_\_

DRB#: \_\_\_\_\_ EPC#: \_\_\_\_\_ Work Order#: \_\_\_\_\_

Legal Description: \_\_\_\_\_

City Address: \_\_\_\_\_

**Engineering Firm:** \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

**Owner:** \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

**Architect:** \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

**Surveyor:** \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

**Contractor:** \_\_\_\_\_ Contact: \_\_\_\_\_

Address: \_\_\_\_\_

Phone#: \_\_\_\_\_ Fax#: \_\_\_\_\_ E-mail: \_\_\_\_\_

### TYPE OF SUBMITTAL:

- DRAINAGE REPORT
- DRAINAGE PLAN 1st SUBMITTAL
- DRAINAGE PLAN RESUBMITTAL
- CONCEPTUAL G & D PLAN
- GRADING PLAN
- EROSION & SEDIMENT CONTROL PLAN (ESC)
- ENGINEER'S CERT (HYDROLOGY)
- CLOMR/LOMR
- TRAFFIC CIRCULATION LAYOUT (TCL)
- ENGINEER'S CERT (TCL)
- ENGINEER'S CERT (DRB SITE PLAN)
- ENGINEER'S CERT (ESC)
- SO-19
- OTHER (SPECIFY) \_\_\_\_\_

### CHECK TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

- SIA/FINANCIAL GUARANTEE RELEASE
- PRELIMINARY PLAT APPROVAL
- S. DEV. PLAN FOR SUB'D APPROVAL
- S. DEV. FOR BLDG. PERMIT APPROVAL
- SECTOR PLAN APPROVAL
- FINAL PLAT APPROVAL
- CERTIFICATE OF OCCUPANCY (PERM)
- CERTIFICATE OF OCCUPANCY (TCL TEMP)
- FOUNDATION PERMIT APPROVAL
- BUILDING PERMIT APPROVAL
- GRADING PERMIT APPROVAL       SO-19 APPROVAL
- PAVING PERMIT APPROVAL       ESC PERMIT APPROVAL
- WORK ORDER APPROVAL       ESC CERT. ACCEPTANCE
- GRADING CERTIFICATION       OTHER (SPECIFY) \_\_\_\_\_

WAS A PRE-DESIGN CONFERENCE ATTENDED:       Yes       No       Copy Provided

DATE SUBMITTED: \_\_\_\_\_ By: \_\_\_\_\_

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location, and scope to the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

1. **Conceptual Grading and Drainage Plan:** Required for approval of Site Development Plans greater than five (5) acres and Sector Plans
2. **Drainage Plans:** Required for building permits, grading permits, paving permits and site plans less than five (5) acres
3. **Drainage Report:** Required for subdivision containing more than ten (10) lots or constituting five (5) acres or more
4. **Erosion and Sediment Control Plan:** Required for any new development and redevelopment site with 1-acre or more of land disturbing area, including project less than 1-acre than are part of a larger common plan of development

UPDATED  
DRAINAGE REPORT

For

**LEGACY NAA APARTMENTS**

**Albuquerque, New Mexico**

Prepared by

Rio Grande Engineering  
PO Box 93924  
Albuquerque, New Mexico 87199

SEPTEMBER 2016



David Soule P.E. No. 14522

## TABLE OF CONTENTS

Purpose .....	3
Introduction.....	3
Existing Conditions.....	3
Exhibit A-Vicinity Map .....	4
Proposed Conditions .....	5
Summary .....	6

### Appendix

NAAMDP, San Pedro Storm drain and Eagle rock Diversion map .....	A
Site Hydrology .....	B
Hydraulic calculations.....	C
Hydraulic Modeling.....	D

### Map

Site Grading and Drainage Plan

**PURPOSE**

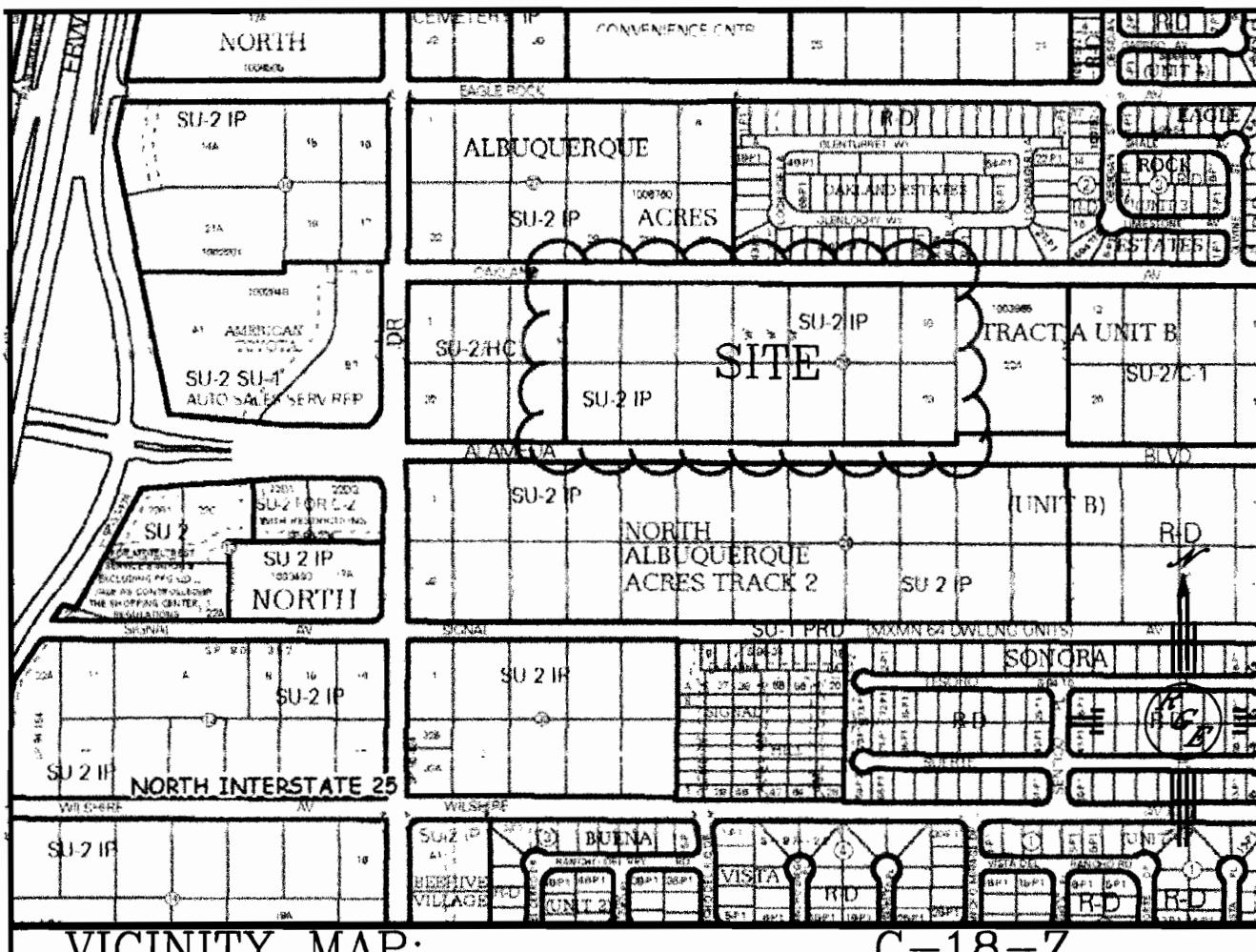
The purpose of this report is to provide the Drainage Management Plan for the development of a 12.41 acre multi family project located on Alameda Boulevard between San Pedro and Louisiana NE. This plan was prepared in accordance with the City of Albuquerque design regulations, utilizing the City of Albuquerque's Development Process Manual drainage guidelines, and HYDROCAD. This report will demonstrate that the grading does not adversely affect the surrounding properties, nor the upstream or downstream facilities.

**INTRODUCTION**

The subject of this report, as shown on the Exhibit A, is a 12.41-acre parcel of land located on the south side of Oakland Avenue and the north side of Alameda Boulevard between San Pedro and Louisiana. The legal description of this site is Lots 4-10 and 23-29, block 28, tract A, unit B, North Albuquerque Acres. As shown on FIRM map35013C0137H, the majority of the entire site is located within Flood Zone X, a recent LOMR was approved removing a previous flood zone AE-1 foot. The site has had significant grading activities upon it over the past 10 years. The site is not in native condition. Due to the upstream construction, the site is not affected by any upland flow. The site free discharges to the west. The development of the site will require the site to discharge at a rate equal to or less than the fully developed conditions assumed for this site in the governing North Albuquerque Acres Master Drainage Plan (NAAMDP), which relevant excerpts can be found in appendix A.

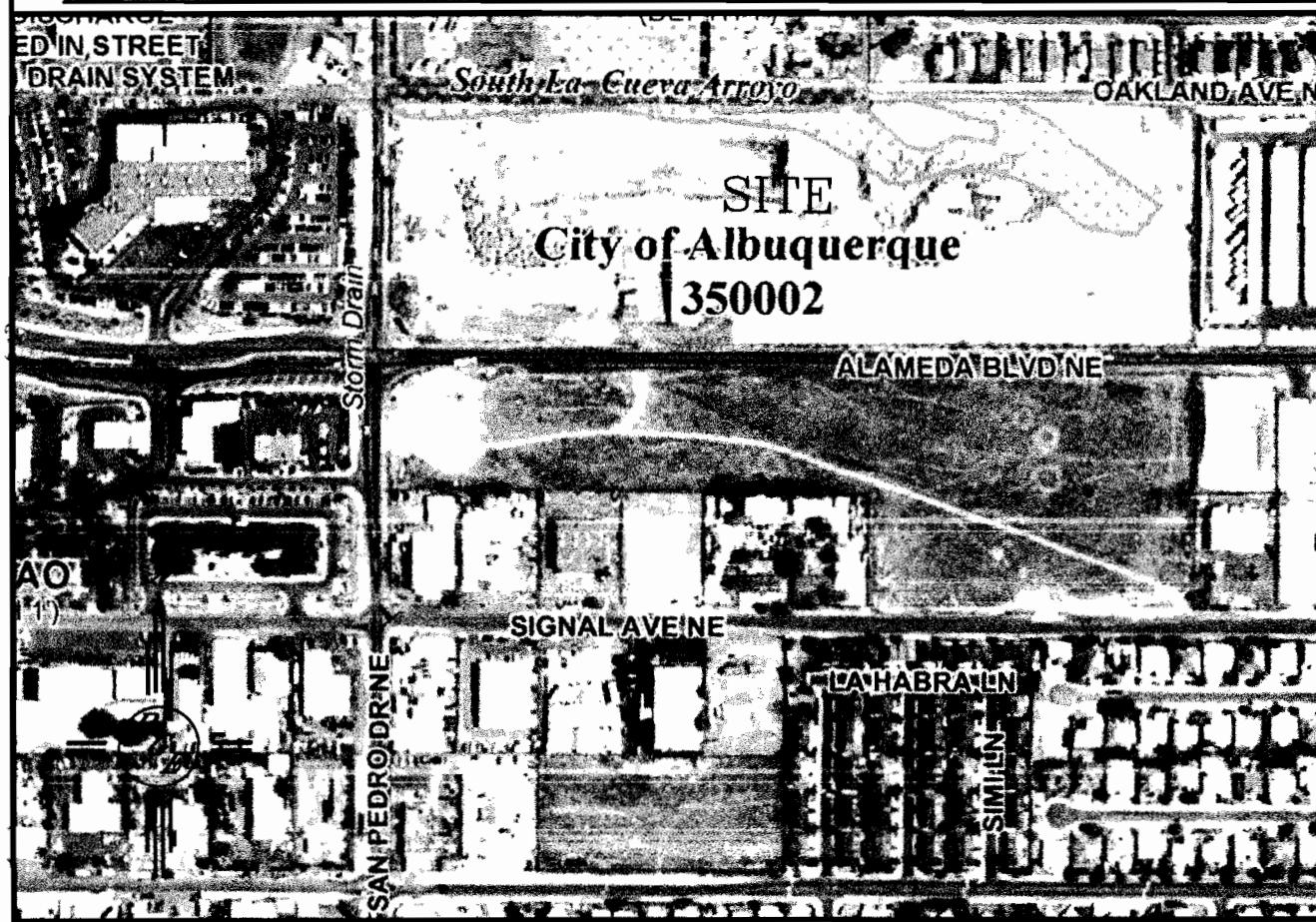
**EXISTING CONDITIONS**

The site currently does have structures on it and has been impacted by human development over the years. The site was most recently an auto salvage and parts yard. The site is not impacted by any upland flows. The site currently discharges all of its flow to the North West



VICINITY MAP:

C-18-Z



FIRM MAP:

35001C0137H

ECAT DESCRIPTION.

Corner of the site. The site is located within basins 117.2 and 117.3 of the NAAMDP. The NAAMDP design analysis has been modified by the Eagle Rock drainage plan. The diversion of the upper 57% of basin 117.2 was designed with the construction of Oakland estates Subdivision. The upland properties have been designed to drain to the storm drain provided within Oakland and Alameda. The recently constructed San Pedro and Alameda storm drain were designed to convey the developed flow from this site. Excerpts of these plan are located in appendix A

### **PROPOSED CONDITIONS**

The proposed improvements consist of a new multi family apartment complex with associated open space and paved parking areas. The drainage is conveyed to three separate discharge point. The site grading was designed utilizing a several onsite water quality ponds that fill and then 'spill' into either the onsite storm drain or into the parking lot. An onsite drainage basin map is located in appendix B. The basins have been color coded to better differentiate them. A spreadsheet calculating the hydrology is located in appendix B. An onsite storm drain map with drainage labels is also located within appendix B. The slopes for each reach have been labeled and the capacities for the pipes are confirmed in appendix C. The site generates flow that exceeds the allowable discharge rates specified within the NAA master drainage plan. To reduce the peak flow to less than allowable several of the ponds have been sized to retain the entire 100-year, 10-day volume generated, therefore removing that basin from contributing flow. The remaining peak exceedence is reduced by the introduction of orifice plates in the two western most inlets. The parking lots have been designed to act as detention basins. The stage storage calculation is located within appendix D. The detention basin was modeled utilizing AHYMO. As shown from the model in appendix D the detention basins reduce the developed site discharge to less than allowed.

As shown on the storm drain map, and site hydrology calculations, the allowable discharge to Oakland upstream of the diversion to eagle rock is 12.23 cfs. We propose to discharge 9.83 cfs. The allowable discharge to Oakland below the diversion, which drains to the san Pedro storm drain, is allowed to be 12.23 cfs. Out site will discharge 13.44 cfs, while this is 1.11 cfs higher than allowed, it enters into the san Pedro storm drain at lower down stream point that anticipated. The allowable discharge to Alameda is 24.46. This site will discharge 23.27 cfs, which is less than allowed. The discharge rates include the roadway frontage captured by the new inlets. The combined discharge to alameda and Oakland that contribute to the san Pedro storm drain is less than allowed. The existing double D inlets on Alameda are removed and replaced with double A inlets. .

The site is required to retain on site 9,413 cubic feet of water for the first flush. This site will retain onsite 15,562 cubic feet of water, which is 6149 cubic feet greater.

#### **SUMMARY AND RECOMMENDATIONS**

This project is a development of a multi family complex with the North Albuquerque Acres Master Drainage plan. The development is consistent with the land use assumptions of the plan. The surrounding development altered the upland and onsite basin by the creation of a diversion from Oakland to Eagle rock. Our plan conforms to this diversion. Our discharge will enter the downstream storm drain where it was generally anticipated. The inlets, pipes and roadways have been shown to provide the required capacity. The onsite flows are reduced to allowable by ponding certain areas and throttling the flow by creating a parking lot detention pond utilizing orifice plate to govern the discharge. The site has been designed in accordance with City of Albuquerque Drainage ordinance. This drainage plan and report conforms to the governing drainage regulations of the City. Since the effected area site encompasses more than 1 acre, a NPDES permit will be required prior to any construction activity.

**APPENDIX A**

**North Albuquerque Acres Master Drainage Plan**

**And**

**Excerpts of Oakland diversion map**

**And**

**San Pedro Storm drain design excerpts**

**FINAL  
NORTH ALBUQUERQUE ACRES  
MASTER DRAINAGE PLAN**

**Prepared For:**



**City of Albuquerque**

**Prepared By:**



**ENGINEERS AND ENVIRONMENTAL SCIENTISTS  
1720-B Randolph Road SE, Albuquerque, NM 87106  
Telephone (505) 243-7300  
Fax (505) 243-7400  
rte@raza.com**



- Commercial/Industrial (C/I): The area west of Louisiana Boulevard, north of Modesto Avenue and east of I-25 would develop as high density commercial and industrial. Also used for Paseo del Norte Corridor
- Medium Density Industrial (MI): Campus type commercial/office facilities and APS schools sites.
- Sandia Tribal Lands (ST): Sandia tribal lands south of Tramway Road and north of the Sandia Pueblo Grant Boundary were allocated land treatments consistent with moderate levels of development even though there are no current plans to develop this area.

The relative weight of each type of Land Treatment is shown in Table 2.

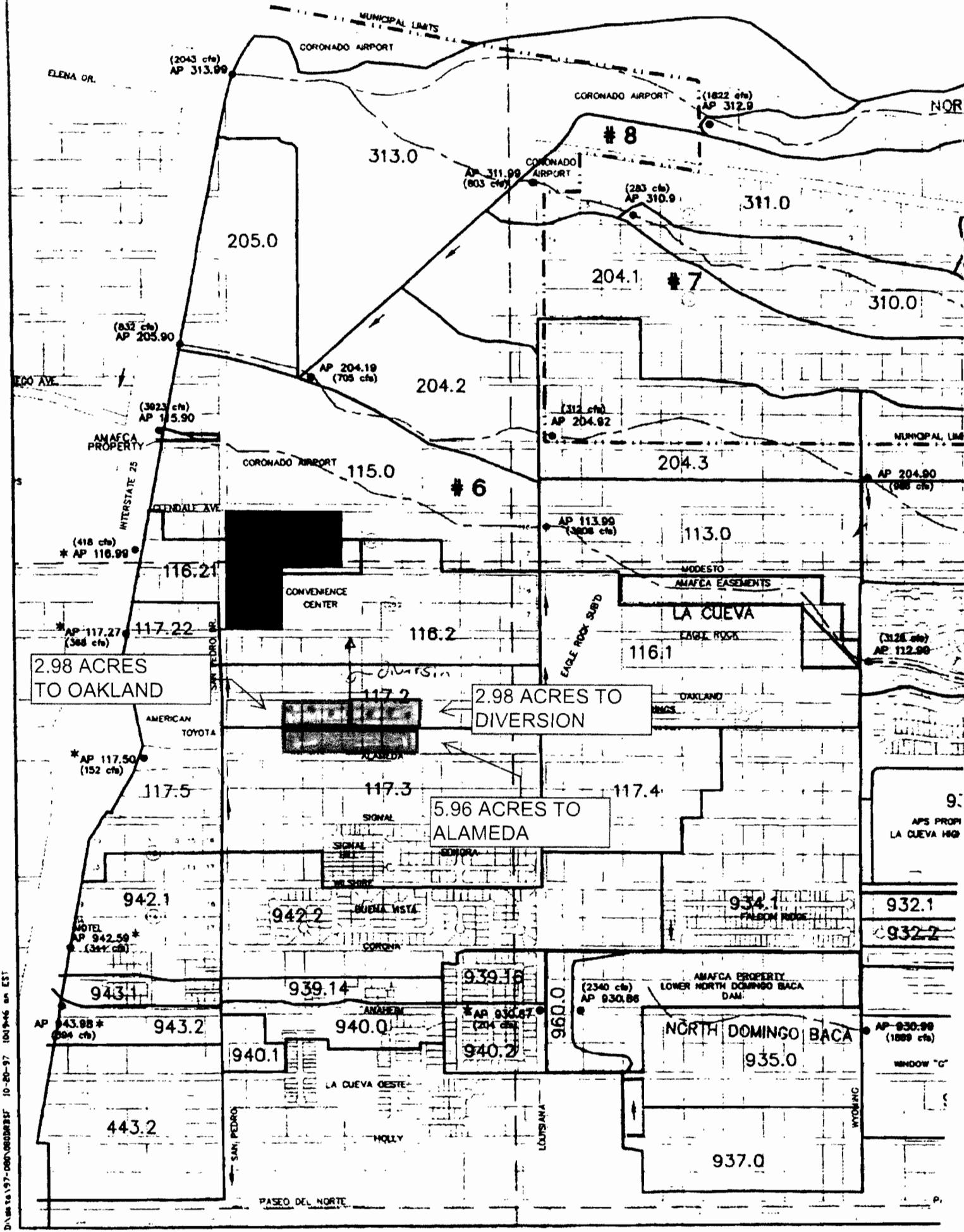
**TABLE 2**  
**FUTURE FULL DEVELOPMENT HYDROLOGIC  
CONDITION ASSUMPTIONS**

	Land Treatments (%)			
	A	B	C	D
Sandia Heights/Tramway (SH/TB)	20	40	5	35
North Albuquerque Acres (NAA)	22	23	38	17
Low Density Residential (LR)	20	20	34	26
Residential (R)	0	34	16	50
High Density Residential (HR)	0	25	15	60
Commercial/Industrial (C/I)	0	20	10	70
Medium Density Industrial (MI)	0	20	30	50
Sandia Tribal Lands (ST)	20	20	40	20
Primrose Pointe (PP)	0	40	20	40

Basin ID	Hydrologic Condition	Basin Area (mi <sup>2</sup> )	Land Treatment (%)				TP (hrs)
			A	B	C	D	
113*	Existing	.1136	80	0	15	5	.133
	Future	.1000	0	25	15	60	.133
115*	Existing	.1337	80	0	15	5	.133
	Future	.1202	0	26	12	62	.133
116*	Existing	.1309	80	0	5	15	.133
116.1	Future	.1000	0	25	15	50	.133
116.2	Future	.0719	0	25	15	50	.133
116.21	Future	.0344	0	40	20	40	.133
117.2	Existing	.1391	73	0	7	20	.22
	Future	.0500	0	34	16	50	.133
117.21*	Existing	.0234	0	34	16	50	.133
117.22*	Future	.0156	0	20	10	70	.133
117.3*	Existing	.0863	65	5	15	15	.133
	Future	.1172	0	34	16	50	.133
117.31*	Existing	.0250	0	34	16	50	.133
117.32*	Existing	.0090	0	34	16	50	.133
117.4*	Existing	.0750	85	0	5	10	.133
	Future	.0512	0	25	15	60	.133
117.5*	Existing	.0550	0	10	20	70	.133
	Future	.0550	0	10	20	70	.133
118	Existing	.0649	0	20	10	70	.133
	Future	.0649	0	20	10	70	.133
118.1	Existing	.0306	75	5	10	10	.133
	Future	.0306	0	20	30	50	.133
119	Existing	.0549	0	20	10	70	.133
	Future	.0549	0	20	10	70	.133
120	Existing	.0268	50	0	0	50	.133
	Future	.0268	0	20	10	70	.133
121	Existing	.0489	80	0	15	5	.133
	Future	.0489	0	20	10	70	.133

\*Modified for COA NAA MDP 9/97

\* W/CDMASTER PLN



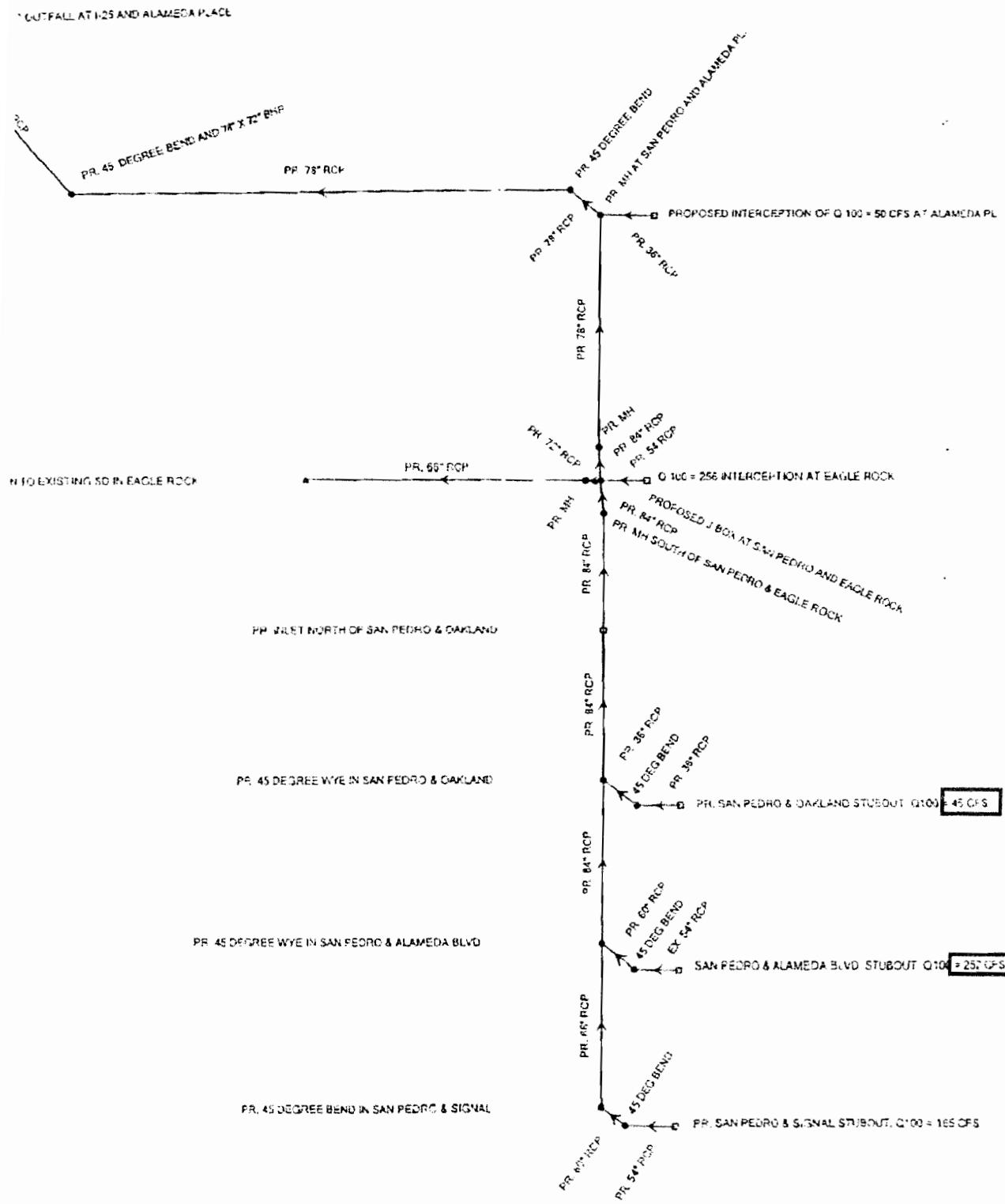
**DESIGN ANALYSIS REPORT**  
**FOR**  
**SAN PEDRO STORM DRAIN PROJECT**  
**CITY PROJECT NO. 5304.91**

**Prepared by:**  
Thompson Engineering Consultants, Inc.  
P.O. Box 65760  
Albuquerque, NM 87193

**January 2010**

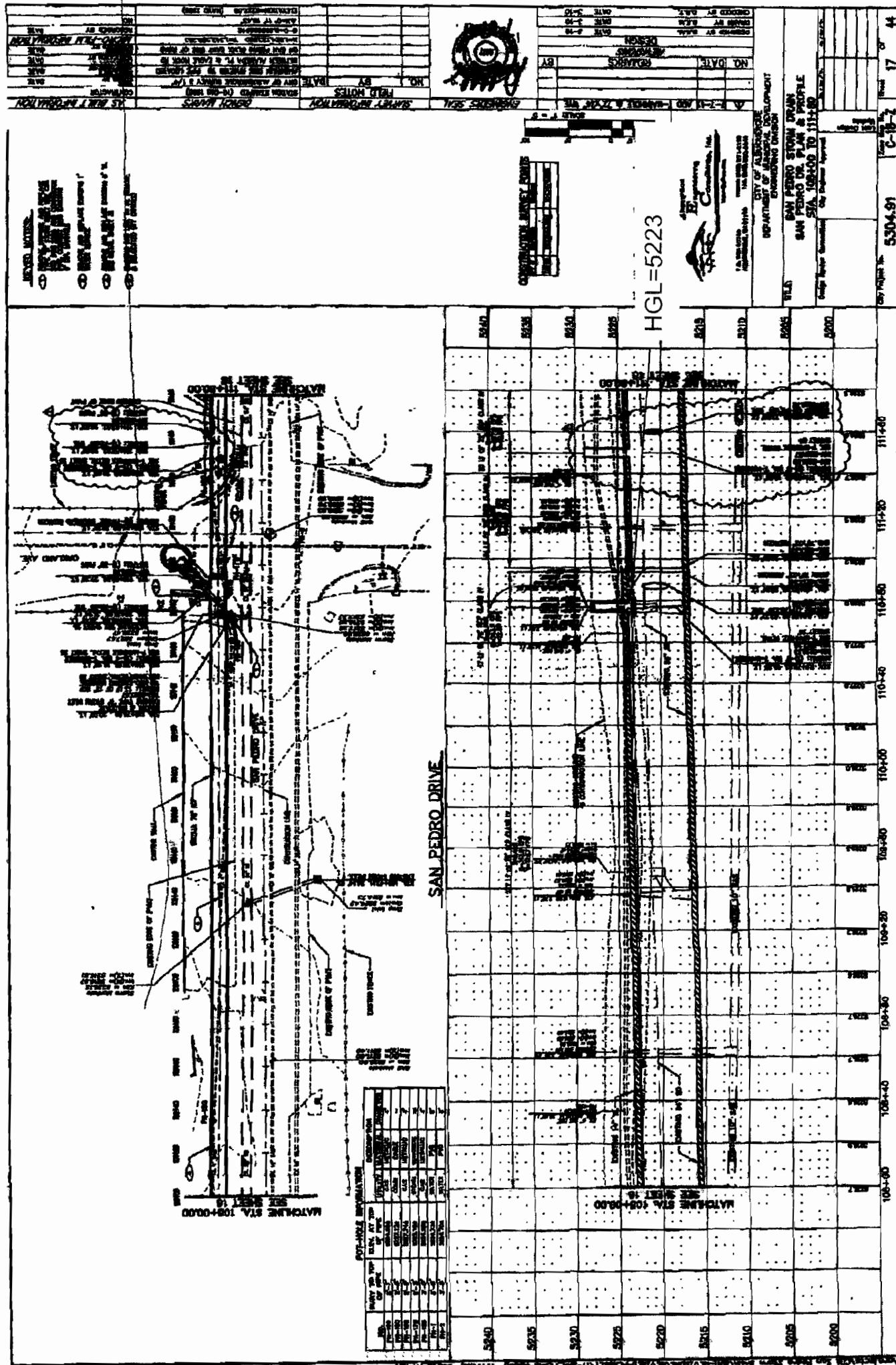
# San Pedro Storm Drain

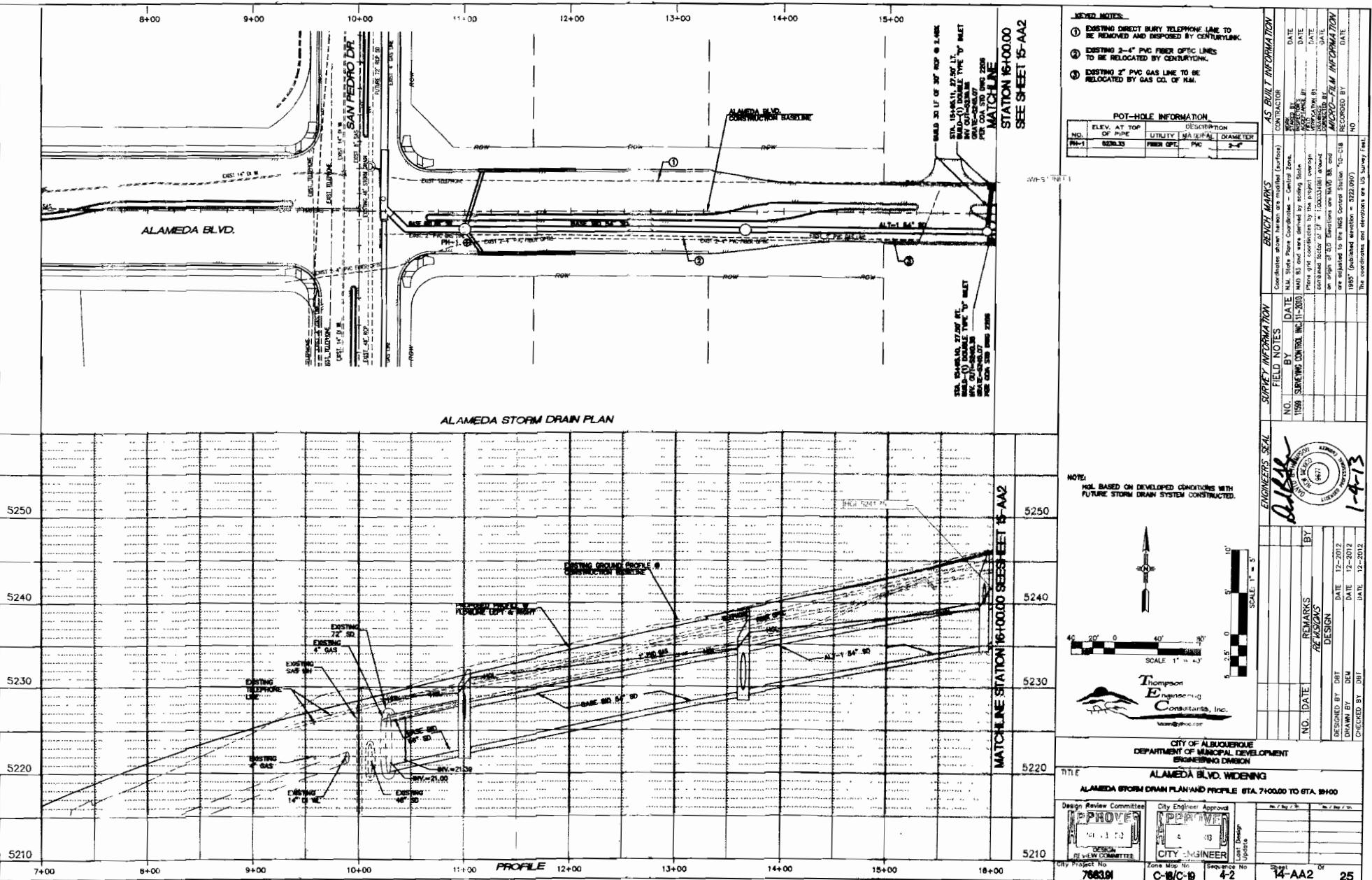
## Proposed Single Pipe System



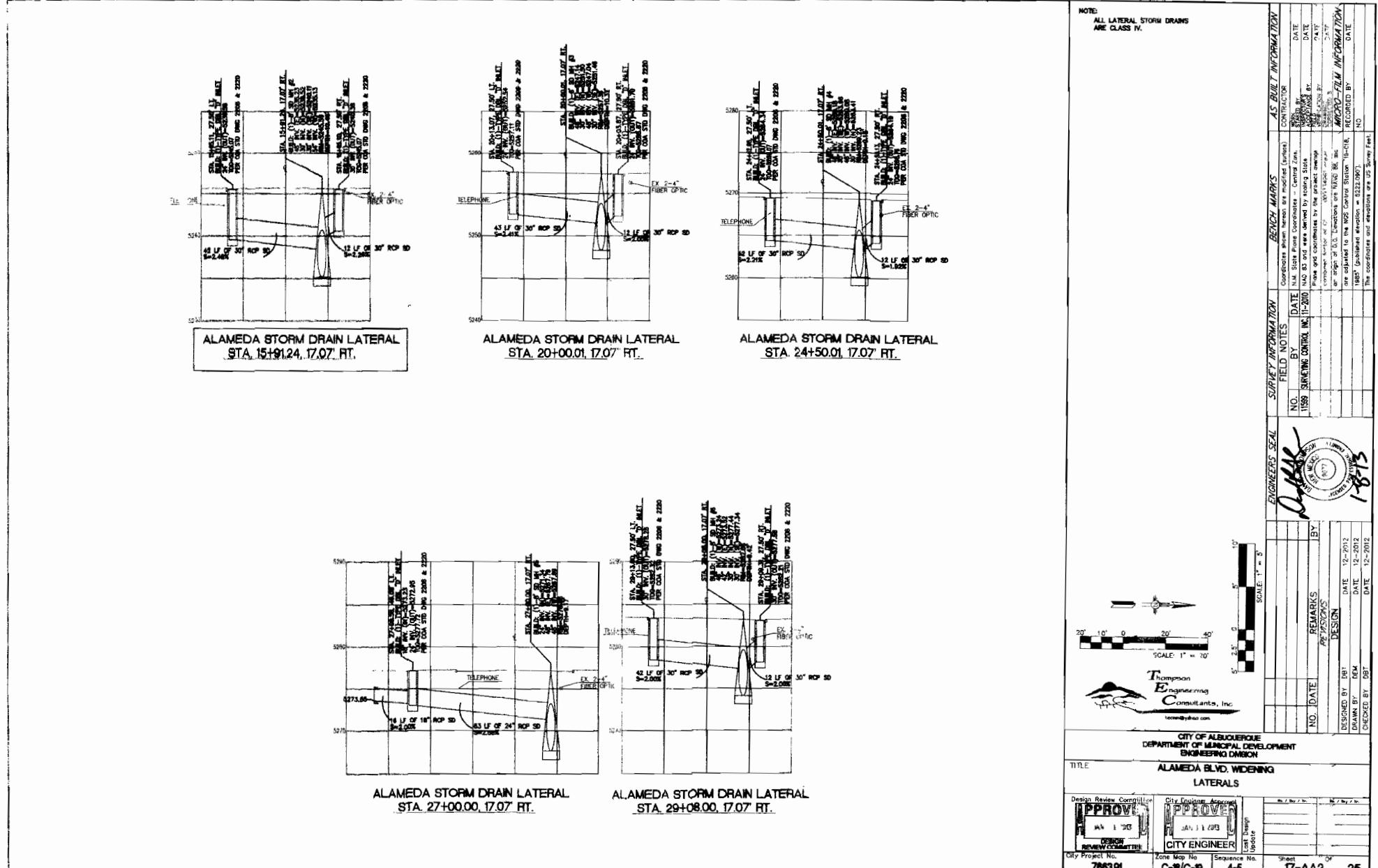
**DOT Report (San Pedro SD - Final Single Pipe System with changes from coa.stc)**

Label	Node Upstream	Node Downstream	Conduit Description	Slope (Calculated)	Length (ft)	Manning's n (0/1)	Flow (ft³/s)	Velocity (Average) (ft/s)	Ground- Upstream (ft)	-Invert- Upstream (ft)	HGL- Upstream (ft)	Ground- Downstream (ft)	-Invert- Downstream (ft)	HGL- Downstream (ft)
PR_66" RCP	PR_45 DEGREE BEND IN SAN PEDRO & SIGNAL	Circular Pipe - 66.0 in	0.006	532	0.013	165	6.94	5230.42	5222.97	5228.42	5228.13	5228.13	5228.13	5228.13
PR_84" RCP	PR_45 DEGREE WYE IN SAN PEDRO & ALAMEDA BLVD	Circular Pipe - 84.0 in	0.005	525	0.013	417	12.96	5229.65	5219.8	5228.13	5228.13	5225.46	5219.8	5225.46
PR_84" RCP	PR_45 DEGREE WYE IN SAN PEDRO & OAKLAND	Circular Pipe - 84.0 in	0.005	139	0.013	462	13.62	5229	5217.29	5223.93	5223.93	5223.93	5217.29	5223.93
PR_84" RCP	PR_INLET NORTH OF SAN PEDRO & OAKLAND	Circular Pipe - 84.0 in	0.005	335	0.013	462	13.38	5226.12	5216.57	5217.29	5223.93	5223.93	5216.57	5223.93
PR_84" RCP	PR_INLET NORTH OF SAN PEDRO & OAKLAND	Circular Pipe - 84.0 in	0.005	335	0.013	462	13.38	5226.12	5216.57	5217.29	5223.93	5223.93	5216.57	5223.93
PR_84" RCP	PR_MM SOUTH OF SAN PEDRO & EAGLE ROCK	Circular Pipe - 84.0 in	0.006	31	0.013	462	15.09	5224.23	5214.89	5220.83	5220.83	5220.83	5214.89	5220.83
PR_84" RCP	PR_MM SOUTH OF SAN PEDRO & EAGLE ROCK	Circular Pipe - 84.0 in	0.006	31	0.013	462	15.09	5224.23	5214.89	5220.83	5220.83	5220.83	5214.89	5220.83
PR_84" RCP	PROPOSED J-BOX AT SAN PEDRO AND EAGLE ROCK	Circular Pipe - 84.0 in	0.009	32	0.013	393	16.57	5224.03	5210.5	5210.5	5210.5	5210.5	5210.5	5210.5
PR_84" RCP	PROPOSED J-BOX AT SAN PEDRO AND EAGLE ROCK	Circular Pipe - 84.0 in	0.009	32	0.013	393	16.57	5224.03	5210.5	5210.5	5210.5	5210.5	5210.5	5210.5
PR_78" RCP	PR_MM	Circular Pipe - 78.0 in	0.01	505	0.013	393	17.57	5223.95	5210.22	5215.94	5215.94	5215.94	5210.22	5215.94
PR_78" RCP	PR_MM	Circular Pipe - 78.0 in	0.01	505	0.013	393	17.57	5223.95	5210.22	5215.52	5215.52	5215.52	5210.22	5215.52
PR_72" RCP	PR_MM AT SAN PEDRO AND ALAMEDA PL	Circular Pipe - 72.0 in	0.012	257	0.013	443	15.67	5221.4	5205	5212.68	5212.68	5212.68	5205	5212.68
PR_72" RCP	PR_45 DEGREE BEND AND 78" X 72" BHR	Circular Pipe - 72.0 in	0.012	257	0.013	443	15.67	5208.9	5199.5	5205.55	5205.55	5205.55	5199.5	5205.55
PR_54" RCP	SAN PEDRO SD OUTFALL AT I-25 AND ALAMEDA PLACE	Circular Pipe - 54.0 in	0.026	50	0.013	165	10.37	5230.5	5196.43	5202.74	5202.74	5202.74	5196.43	5202.74
PR_54" RCP	PR_SAN PEDRO & SIGNAL STUBOUT: Q100 = 165 CFS	Circular Pipe - 54.0 in	0.026	50	0.013	165	10.37	5233.2	5223.75	5230.9	5230.9	5230.9	5223.75	5230.9
PR_60" RCP	45 DEG BEND	Circular Pipe - 60.0 in	0.026	50	0.013	165	8.4	5231.8	5224.36	5230.25	5230.25	5230.25	5224.36	5230.25
PR_60" RCP	45 DEG BEND	Circular Pipe - 60.0 in	0.026	50	0.013	165	8.4	5231.8	5224.36	5229.89	5229.89	5229.89	5224.36	5229.89
EX_54" RCP	PR_45 DEGREE BEND IN SAN PEDRO & SIGNAL	Circular Pipe - 54.0 in	0.034	50	0.013	252	15.84	5230.42	5222.97	5229.67	5229.67	5229.67	5222.97	5229.67
EX_54" RCP	SAN PEDRO & ALAMEDA BLVD. STUBOUT: Q100 = 252 CFS	Circular Pipe - 54.0 in	0.034	50	0.013	252	15.84	5232.3	5223.36	5230.29	5230.29	5230.29	5223.36	5230.29
PR_60" RCP	45 DEG BEND	Circular Pipe - 60.0 in	0.034	50	0.013	252	12.83	5230.1	5221.58	5224.37	5224.37	5224.37	5221.58	5224.37
PR_60" RCP	45 DEG BEND	Circular Pipe - 60.0 in	0.034	50	0.013	252	12.83	5230.1	5221.58	5229.89	5229.89	5229.89	5221.58	5229.89
PR_36" RCP	PR_45 DEGREE BEND IN SAN PEDRO & ALAMEDA BLVD	Circular Pipe - 36.0 in	0.026	50	0.013	45	6.37	5230.6	5220.05	5224.6	5224.6	5224.6	5220.05	5224.6
PR_36" RCP	PR_SAN PEDRO & OAKLAND STUBOUT: Q100 = 45 CFS	Circular Pipe - 36.0 in	0.026	50	0.013	45	6.37	5229.3	5210.67	5224.37	5224.37	5224.37	5210.67	5224.37
PR_36" RCP	45 DEG BEND	Circular Pipe - 36.0 in	0.026	50	0.013	45	6.37	5229.3	5218.67	5221.15	5221.15	5221.15	5218.67	5221.15
PR_72" RCP	PR_45 DEGREE WYE IN SAN PEDRO & OAKLAND	Circular Pipe - 72.0 in	0.02	5	0.013	325	(N/A)	5224.03	5210.5	(N/A)	(N/A)	(N/A)	5210.5	5223.93
PR_72" RCP	PROPOSED J-BOX AT SAN PEDRO AND EAGLE ROCK	Circular Pipe - 72.0 in	0.02	5	0.013	325	(N/A)	5224.03	5210.5	(N/A)	(N/A)	(N/A)	5210.5	5223.93
PR_54" RCP	PR_MM	Circular Pipe - 66.0 in	0.019	334	0.013	325	20.9	5224	5210.4	5215.31	5215.31	5215.31	5210.4	5215.31
PR_78" RCP	CONNECTION TO EXISTING SD IN EAGLE ROCK	Circular Pipe - 78.0 in	0.017	30	0.013	443	13.35	5221.4	5205	5211.75	5211.75	5211.75	5205	5211.75
PR_78" RCP	PR_MM AT SAN PEDRO AND ALAMEDA PL.	Circular Pipe - 78.0 in	0.017	30	0.013	443	13.35	5221.4	5205	5204.5	5211.54	5211.54	5205	5211.54
PR_78" RCP	PR_45 DEGREE BEND	Circular Pipe - 78.0 in	0.01	496.7	0.013	443	17.77	5220	5204.5	5210.07	5210.07	5210.07	5204.5	5210.07
PR_36" RCP	PR_45 DEGREE BEND AND 78" X 72" BHR	Circular Pipe - 42.0 in	0.01	50	0.013	50	10.44	5222	5199.5	5206.85	5206.85	5206.85	5199.5	5206.85
PR_36" RCP	PROPOSED INTERCEPTION OF Q100 = 50 CFS AT ALAMEDA PL.	Circular Pipe - 42.0 in	0.01	50	0.013	50	10.44	5222	5211.5	5213.71	5213.71	5213.71	5211.5	5213.71
PR_54" RCP	PR_MM AT SAN PEDRO AND ALAMEDA PL.	Circular Pipe - 54.0 in	0.02	50	0.013	256	16.1	5226	5205	5212.85	5212.85	5212.85	5205	5212.85
PR_54" RCP	Q100 = 256 INTERCEPTION AT EAGLE ROCK	Circular Pipe - 54.0 in	0.02	50	0.013	256	16.1	5226	5216	5220.62	5220.62	5220.62	5216	5220.62
PR_54" RCP	PROPOSED J-BOX AT SAN PEDRO AND EAGLE ROCK	Circular Pipe - 54.0 in	0.02	50	0.013	256	16.1	5224.03	5210.5	5219.77	5219.77	5219.77	5210.5	5219.77









**APPENDIX B**

**SITE HYDROLOGY**

## **Weighted E Method**

Existing Developed Basins												100-Year, 6-hr.			10-day			
	Basin	Area (sf)	Area (acres)	Treatment A		Treatment B		Treatment C		Treatment D		Weighted E (ac-ft)	Volume (ac-ft)	Flow cfs	Volume (ac-ft)			
				%	(acres)	%	(acres)	%	(acres)	%	(acres)							
drains to oakland div	B1	61044	1.401	0%	0	10.0%	0.140	22.0%	0.3083	68%	0.953	1.981	0.231	6.21	0.358	0 000	15609.968	0.0%
	B2	4230	0.097	0%	0	10.0%	0.010	40.0%	0.03884	50%	0.049	1.788	0.014	0.40	0.021	0 000	912.27	0.0%
	B3	13645	0.313	0%	0	20.0%	0.063	24.0%	0.07518	56%	0.175	1.815	0.047	1.30	0.071	1565 000	3082.8603	50.8%
drains to oakland	G1	38271	0.879	0%	0	10.0%	0.088	22.0%	0.19329	68%	0.597	1.981	0.145	3.89	0.225	302 000	9786.5326	3.1%
	G2	3581	0.082	0%	0	30.0%	0.025	24.0%	0.01973	46%	0.038	1.671	0.011	0.32	0.016	252 000	718.3486	35.1%
	G3	3122	0.072	0%	0	40.0%	0.029	25.0%	0.01792	34%	0.024	1.493	0.009	0.26	0.012	530 000	529.93348	100.0%
	G4	5992	0.138	0%	0	15.0%	0.021	36.0%	0.04952	49%	0.067	1.759	0.020	0.56	0.029	0 000	1269.7048	0.0%
	G4A	3244	0.074	0%	0	25.0%	0.019	28.0%	0.02085	36%	0.027	1.441	0.009	0.25	0.013	252 000	545.20827	46.2%
	G5	2258	0.052	0%	0	48.0%	0.025	30.0%	0.01555	22%	0.011	1.348	0.006	0.18	0.007	537 000	319.8457	167.9%
	G6	18458	0.424	0%	0	26.0%	0.110	26.0%	0.11017	48%	0.203	1.707	0.060	1.69	0.087	2098 000	3807.5778	55.1%
	G7	8236	0.189	0%	0	10.0%	0.019	21.0%	0.03971	69%	0.130	1.991	0.031	0.84	0.049	0 000	2124.4076	0.0%
	G8	14425	0.331	0%	0	21.0%	0.070	25.0%	0.08279	54%	0.179	1.790	0.049	1.36	0.073	678 000	3190.4494	21.3%
	G8E	26480	0.608	0%	0	21.0%	0.128	25.0%	0.15197	54%	0.328	1.790	0.091	2.50	0.134	221 000	5856.714	3.8%
	O1W	5843	0.134	0%	0	18.0%	0.024	44.0%	0.05902	38%	0.051	1.630	0.018	0.52	0.025	100 000	1089.7195	9.2%
	O1E	9652	0.222	0%	0	14.0%	0.031	32.0%	0.07091	54%	0.120	1.816	0.034	0.93	0.049	100 000	2155.6133	4.6%
drains to alameda	R1	5710	0.131	0%	0	23.0%	0.030	24.0%	0.03146	53%	0.069	1.772	0.019	0.54	0.029	459 000	1246.6833	36.8%
	R2	12780	0.293	0%	0	23.0%	0.067	26.0%	0.07628	51%	0.150	1.751	0.043	1.19	0.063	841 000	2733.429	23.5%
	R3	4983	0.114	0%	0	10.0%	0.011	16.0%	0.0183	74%	0.085	2.045	0.019	0.52	0.031	0 000	1340.7592	0.0%
	R4	6059	0.139	0%	0	30.0%	0.042	22.0%	0.0306	48%	0.067	1.693	0.020	0.55	0.029	1250 000	1242.398	100.6%
	M1	767	0.018	0%	0	60.0%	0.011	40.0%	0.00704	0%	0.000	1.068	0.002	0.05	0.002	196 000	68.263	287.1%
	M2	1503	0.035	0%	0	40.0%	0.014	40.0%	0.0138	20%	0.007	1.356	0.004	0.12	0.005	210 000	209.919	100.0%
	M3E	58541	1.344	0%	0	13.0%	0.175	23.0%	0.3091	64%	0.860	1.927	0.216	5.84	0.330	543 000	14394.744	3.8%
	M3W	116701	2.679	0%	0	19.0%	0.509	16.0%	0.42865	65%	1.741	1.915	0.428	11.54	0.660	2501 000	28739.566	8.7%
	M4	5047	0.116	0%	0	58.0%	0.067	30.0%	0.03476	28%	0.032	1.581	0.015	0.46	0.020	1635 000	853.53182	191.6%
	M5	30725	0.705	0%	0	20.0%	0.141	24.0%	0.16928	56%	0.395	1.815	0.107	2.93	0.159	1492 000	6941.8017	21.5%
DRAIN TO OAKLAND DIV		78919	1.812	0%	0	11.7%	0.212497	23.3%	0.42233	65%	1.1769082	1.942	0.293	7.92	0.450	1565	19605.099	8.0%
DRAIN TO OAKLAND		139562	3.204	0%	0	18.3%	0.5867674	26.0%	0.83142	55%	1.7768021	1.812	0.484	13.31	0.721	5070	31394.055	16.1%
DRAIN TO ALAMEDA		242816	5.574	0%	0	19.1%	1.067168	20.1%	1.11929	61%	3.4063703	1.877	0.872	23.74	1.326	8927	57771.095	15.5%
FLOW IN DEDICATED ALAMEDA		39422	0.905	0%	0	10.0%	0.091	20.0%	0.181	70%	0.634	2.002	0.151	4.04	0.235	0 000	0	0.0%
FLOW IN DEDICATED OAKLAND		39422	0.905	0%	0	10.0%	0.091	20.0%	0.181	70%	0.634	2.002	0.151	4.04	0.235	0 000	0	0.0%
TOTAL FLOW		540141	12.400	0	16.5%	2.047	22.1%	2.735	62%	7.627	1.888	1.951	53.05					
ALLOWED PER NAADMP		540141	12.400	0	34.0%	4.2159766	16.0%	1.98399	50%	6.1999656	1.699	1.756	48.93					

### Equations:

$$\text{Weighted E} = E_a \cdot A_a + E_b \cdot A_b + E_c \cdot A_c + E_d \cdot A_d / (\text{Total Area})$$

Volume = Weighted D \* Total Area

$$Flow = Q_a \cdot A_a + Q_b \cdot A_b + Q_c \cdot A_c + Q_d \cdot A_d$$

Where for 100-year, 6-hour storm (zone 3)

$$\begin{array}{ll} \text{Ea} = 0.66 & \text{Qa} = 1.87 \\ \text{Eb} = 0.92 & \text{Qb} = 2.6 \\ \text{Ec} = 1.29 & \text{Qc} = 3.45 \\ \text{Fd} = 2.36 & \text{Qd} = 5.02 \end{array}$$

PONDING PROVIDED  
FIRST FLUSH REQUIREMENT  
FLOW RATE EXCEEDANCE  
REDUCTION FOR ROUTING AND PONDS

11.87

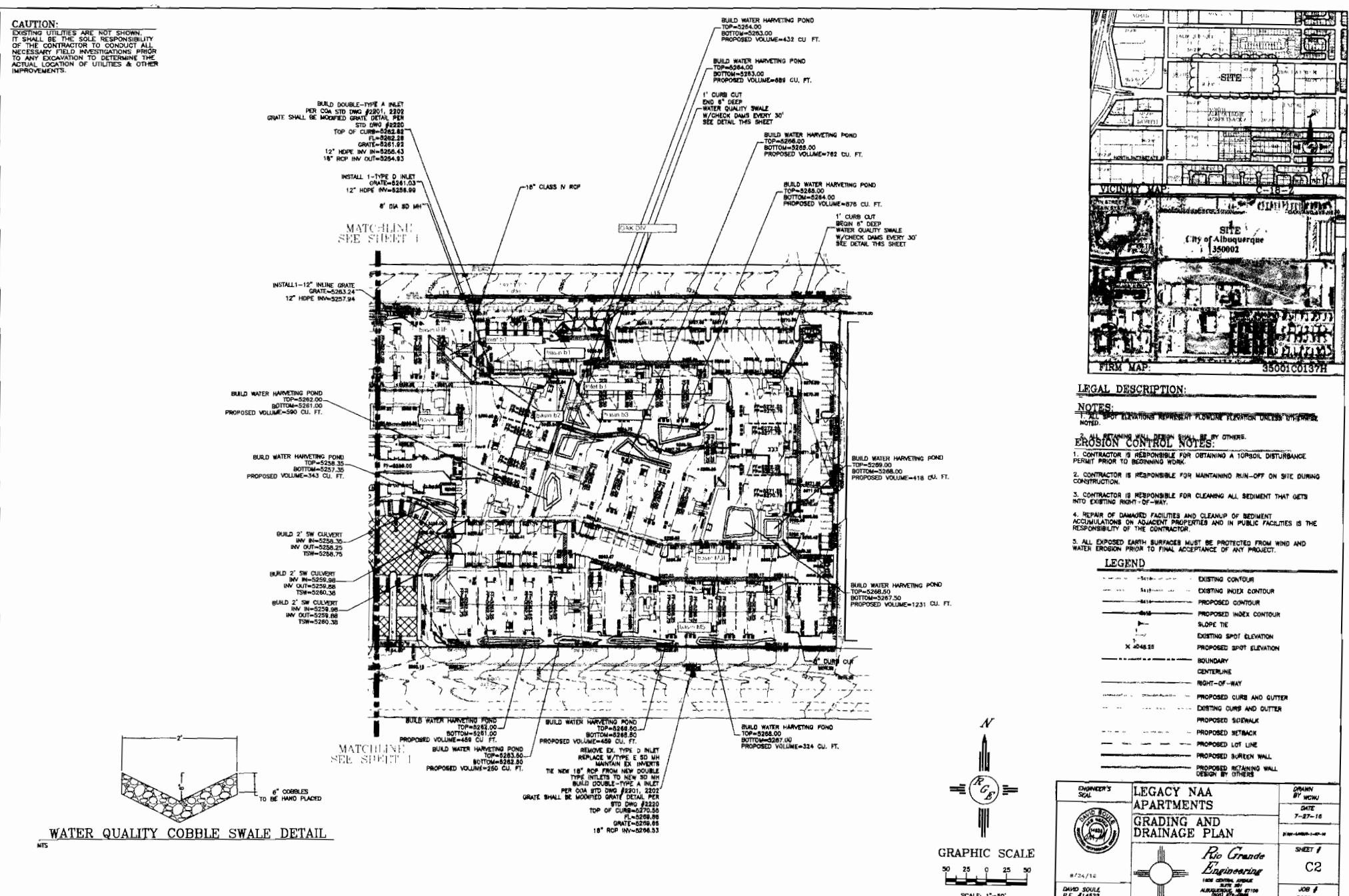
**FLOW SUMMARY**  
**FLOW TO OAKLAND DIRVERSION**  
**FLOW TO OAKLAND**  
**FLOW TO ALAMEDA**

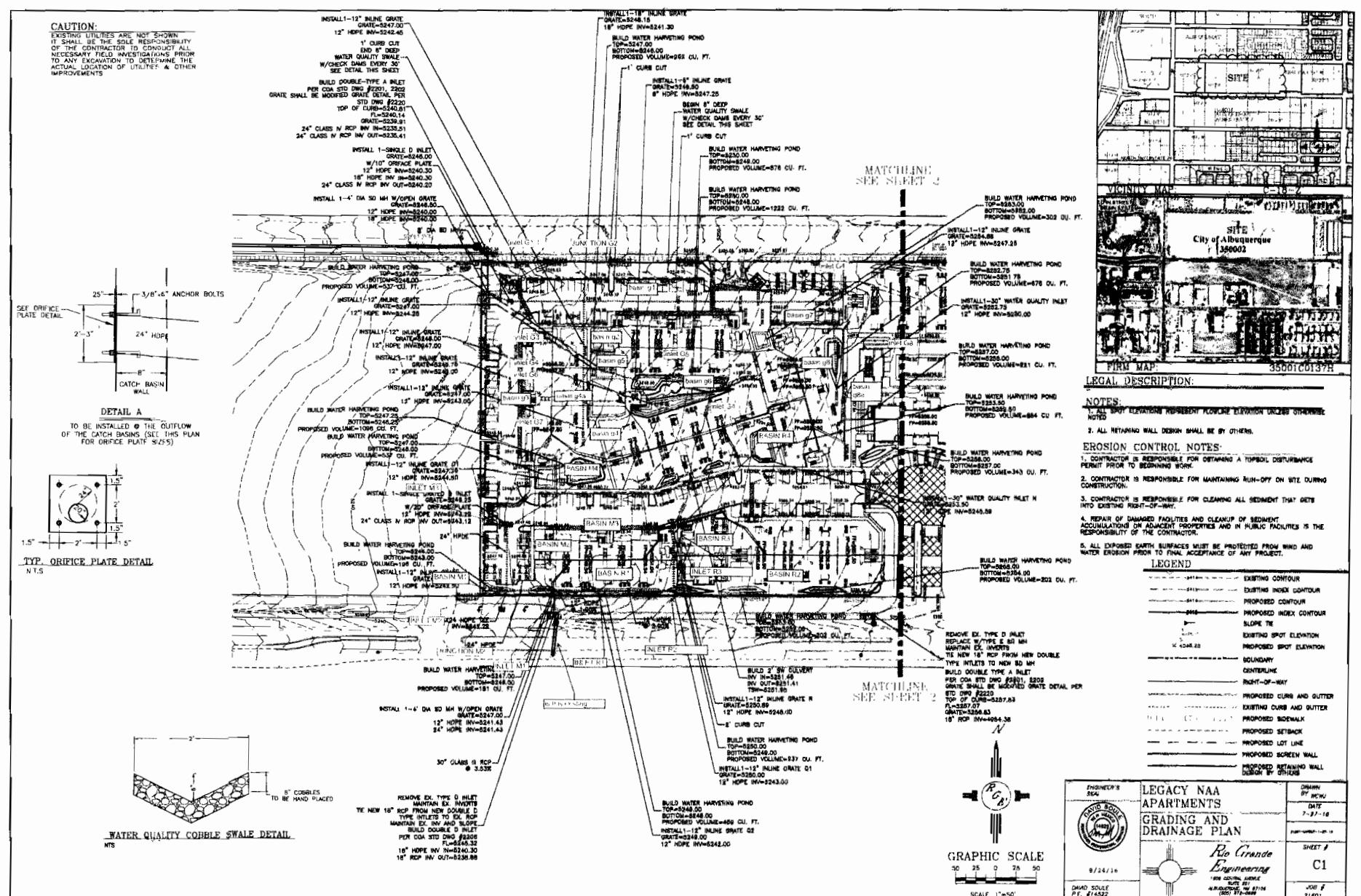
ROAD FLOWS AT INLET	
EAST ALAMEDA*	3.40 CFS
MIDDLE ALAMEDA	3.4 CFS
WEST ALAMEDA	3.4 CFS
EAST OAKLAND	2.02 CFS
WEST OAKLAND	0.62 CFS

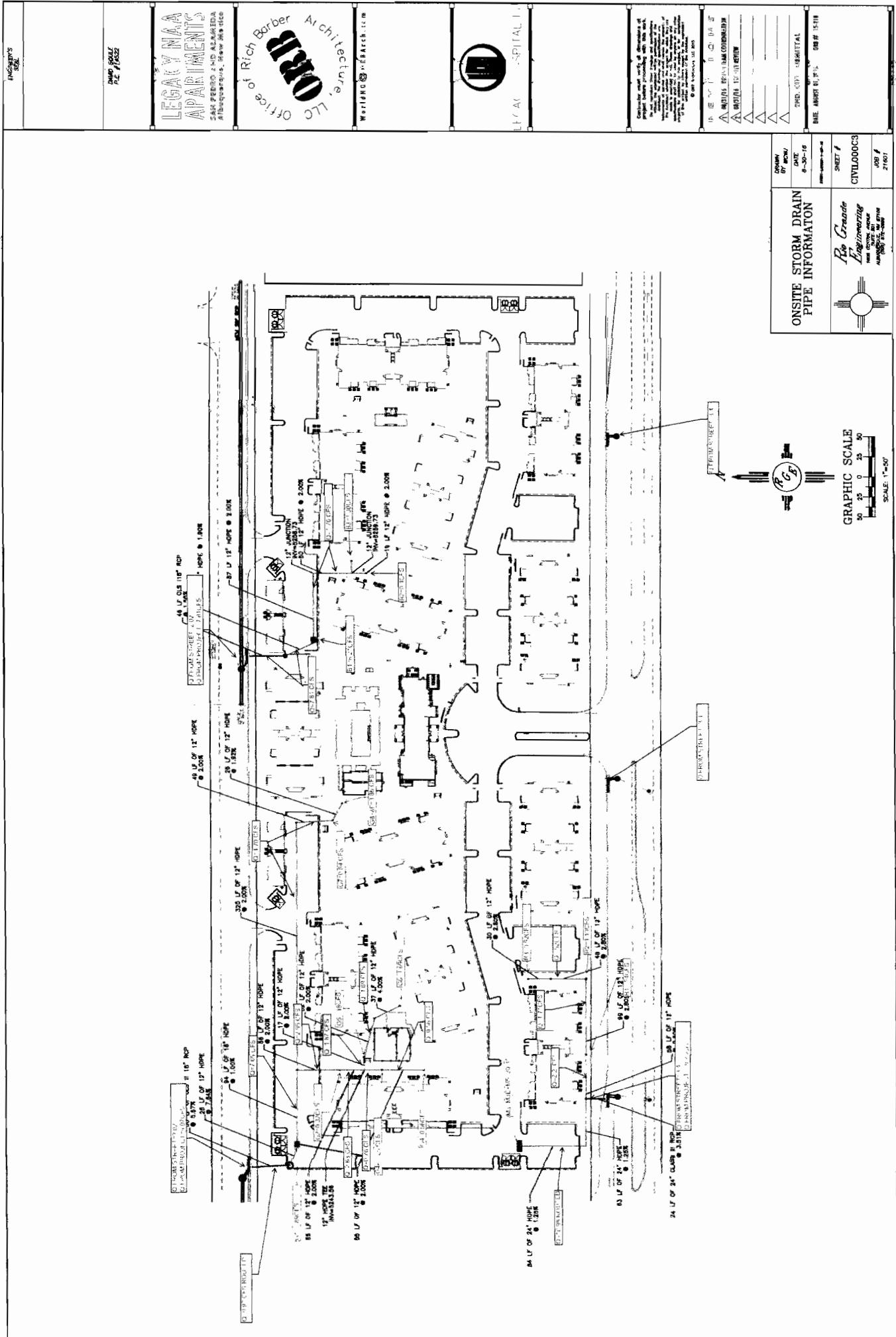
PROPOSED FROM SITE	FROM ROADWAY
7.81	2.02
11.42	2.02
19.23	4.04

BASINS THAT RETAIN ALL FLOWS	
G3	0.26 CFS
G5	0.18 CFS
R4	0.55 CFS
M1	0.05 CFS
M2	0.12
M4	0.46 CFS
TOTAL	1.62 CFS

\* STREET FLOWS IN ALAMEDA ARE BASED UPON FLOWS GENERATED BY OUR 10' LANE AND ASPHALT MULTIPLIED BY 2.5 TO ACCOUNT FOR 20' OF EX ASPHALT







**APPENDIX C**

**HYDRAULIC CALCULATIONS**

## **DROP INLET CALCULATIONS**

INLET	TYPE OF INLET	AREA (SF)	Q (CFS)	H (FT)	H ALLOW (FT)
north	SINGLE	3.84	7.78	0.1771	1.75
south	DOUBLE	7.68	40.62	1.2066	1.75
east	SINGLE	3.84	12.42	0.4512	0.67

### ORIFICE EQUATION

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$g = 32.2$$

FLOW RATES ARE DOUBLED

Pipe Capacity  
for all onsite pipes

D (in)	Slope (%)	Area (ft^2)	R	Q Provided (cfs)	Q Required (cfs)	Velocity (ft/s)
18	5.57	1.77	0.375	24.86	9.97	5.64
12	7.66	0.79	0.25	9.89	9.97	12.69
18	1	1.77	0.375	10.53	7.65	4.33
12	2	0.79	0.25	5.05	4.70	5.98
24	1.25	3.14	0.5	25.36	16.98	5.40
12	2.8	0.79	0.25	5.98	0.54	0.69
18	1.56	1.77	0.375	13.16	7.81	4.42
30	1	4.91	0.625	41.13	19.23	3.92

Manning's Equation:

$$Q = 1.49/n * A * R^{(2/3)} * S^{(1/2)}$$

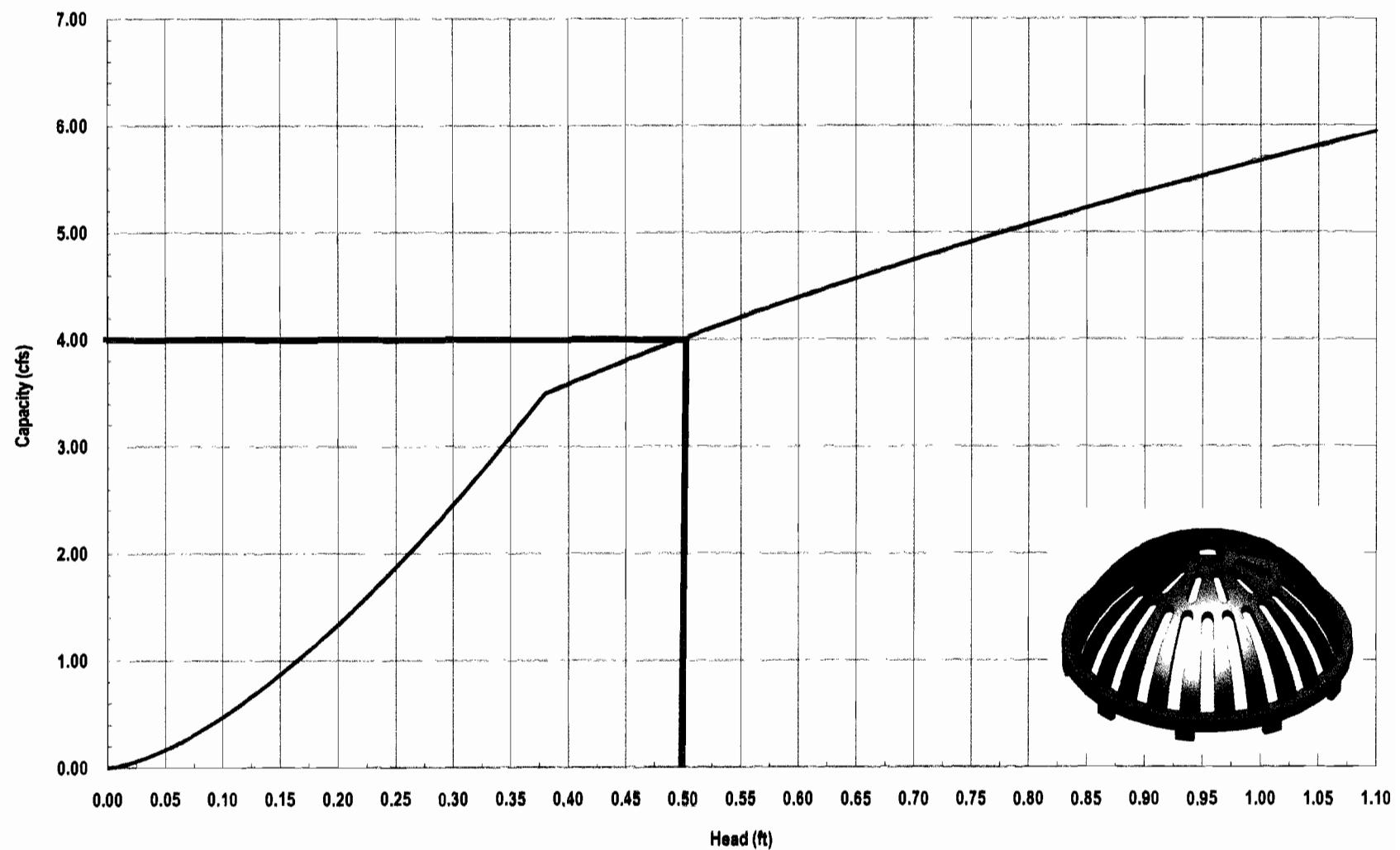
A = Area

R = D/4

S = Slope

n = 0.013

Nyloplast 18" Dome Grate Inlet Capacity Chart



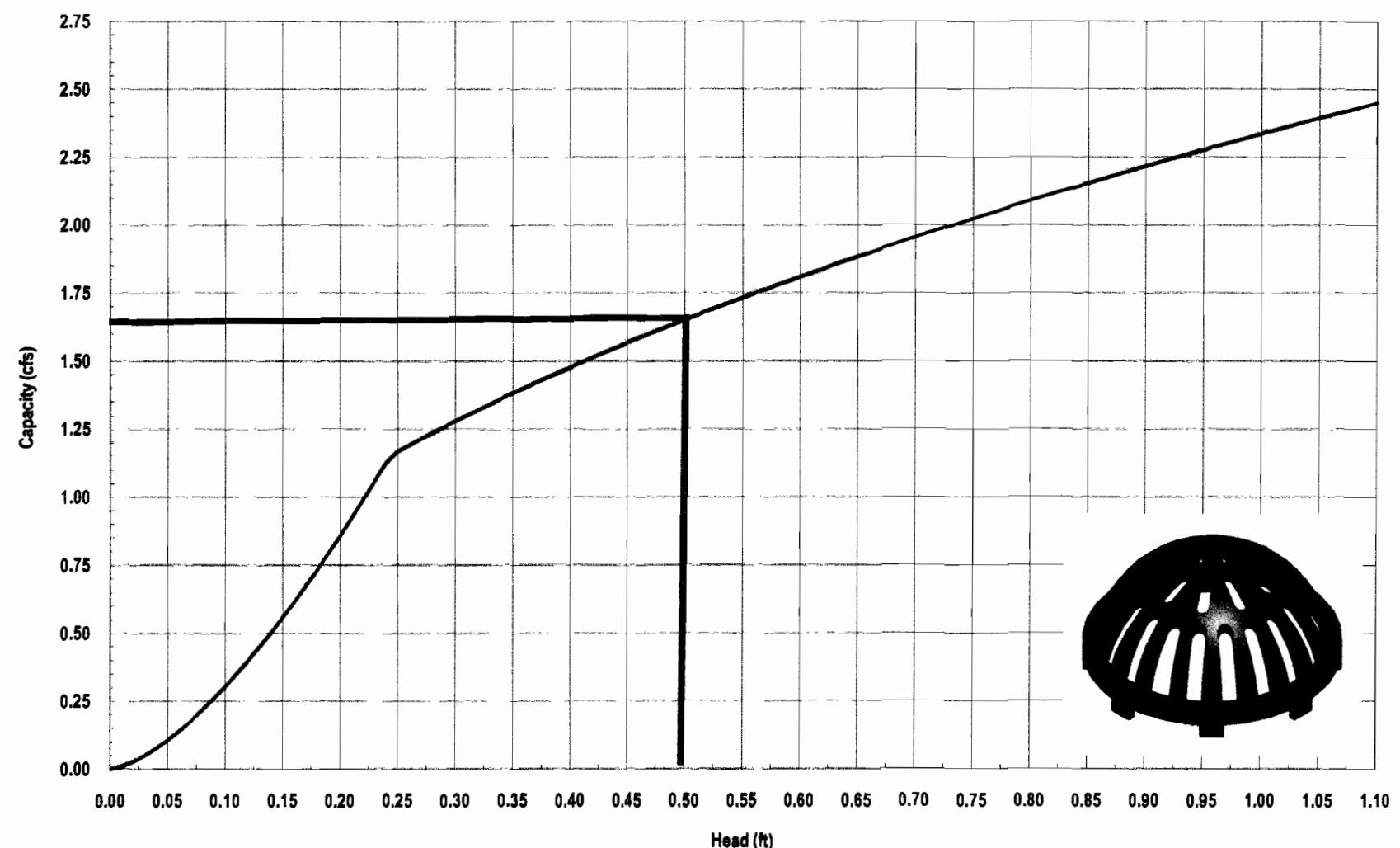
np  
**Nyloplast®**

3130 Verona Avenue • Buford, GA 30518

(866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490

© Nyloplast Inlet Capacity Charts June 2012

Nyloplast 12" Dome Grate Inlet Capacity Chart



  
**Nyloplast®**  
3130 Verona Avenue • Buford, GA 30518  
(866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490  
© Nyloplast Inlet Capacity Charts June 2012

**APPENDIX D**

**HYDRAULIC MODEL**

Npondrout0909 16.txt

\*S AHYMO - NORTH INLET  
\*S POND ROUTING

START TIME=0.0 PUNCH CODE=0

RAINFALL

TYPE=2  
QUARTER=0.0 ONE= 2.14 IN  
SIX= 2.60 IN DAY= 3.10 IN DT = 0.05 HR

COMPUTE NM HYD

ID=1 HYD NO=101 DA= .004297 SQ MI  
PER A=0 PER B=17.50 PER C=24.5 PER D=58  
TP=-.145 MASSRAIN=-1

PRINT HYD

ID=1 CODE=3

\* ROUTE THE TOTAL FLOW THROUGH THE PROPOSED RESERVOIR.

ROUTE RESERVOIR	ID=2 HYD NO=102 INFLOW=1 CODE=3	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)
		5.24	0.000	42.00
		7.63	0.001	44.00
		8.83	0.001	45.00
		9.88	0.016	46.00
		10.83	0.072	47.00

FINISH

## NORTH POND OUTLET AHYMO.OUT

AHYMO PROGRAM (AHYMO-S4) - Version: S4.01a - Rel: 01a  
 RUN DATE (MON/DAY/YR) = 09/11/2016  
 START TIME (HR:MIN:SEC) = 19:45:15 USER NO.=  
 RioGrandeSingleA41963517  
 INPUT FILE = \Owner\Desktop\2015 JOBS\15120-alameda  
 apartments\RAINAGE\Npondrout0909 16.txt

\*S AHYMO - NORTH INLET  
 \*S POND ROUTING

START TIME=0.0 PUNCH CODE=0

RAINFALL TYPE=2  
 QUARTER=0.0 ONE= 2.14 IN  
 SIX= 2.60 IN DAY= 3.10 IN DT = 0.05 HR

AREAS (NM & AZ) - D1 24-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE

DT	0.050000 HOURS	END TIME	= 24.000002 HOURS
0.0000	0.0031	0.0062	0.0096 0.0133 0.0171 0.0214
0.0274	0.0368	0.0470	0.0575 0.0690 0.0807 0.0927
0.1052	0.1178	0.1320	0.1467 0.1627 0.1887 0.2196
0.2611	0.3081	0.3661	0.4435 0.5307 0.6811 0.9149
1.3155	1.5971	1.8192	1.9308 2.0287 2.0989 2.1549
2.2036	2.2393	2.2720	2.2991 2.3181 2.3331 2.3464
2.3590	2.3700	2.3804	2.3905 2.4002 2.4083 2.4129
2.4175	2.4219	2.4261	2.4303 2.4343 2.4383 2.4422
2.4459	2.4495	2.4531	2.4566 2.4601 2.4634 2.4667
2.4699	2.4731	2.4762	2.4792 2.4822 2.4851 2.4880
2.4909	2.4937	2.4965	2.4992 2.5019 2.5046 2.5072
2.5098	2.5124	2.5149	2.5175 2.5200 2.5224 2.5249
2.5273	2.5296	2.5320	2.5343 2.5366 2.5389 2.5412
2.5434	2.5456	2.5478	2.5500 2.5521 2.5542 2.5564
2.5584	2.5605	2.5626	2.5646 2.5666 2.5686 2.5706
2.5725	2.5745	2.5764	2.5783 2.5802 2.5821 2.5839
2.5858	2.5876	2.5894	2.5912 2.5930 2.5948 2.5965
2.5983	2.6000	2.6017	2.6035 2.6052 2.6069 2.6086
2.6104	2.6121	2.6138	2.6155 2.6172 2.6190 2.6207
2.6224	2.6241	2.6258	2.6275 2.6292 2.6309 2.6326
2.6343	2.6360	2.6377	2.6394 2.6411 2.6428 2.6445
2.6461	2.6478	2.6495	2.6512 2.6529 2.6545 2.6562
2.6579	2.6595	2.6612	2.6629 2.6645 2.6662 2.6679
2.6695	2.6712	2.6728	2.6745 2.6761 2.6778 2.6794
2.6811	2.6827	2.6844	2.6860 2.6876 2.6893 2.6909
2.6925	2.6942	2.6958	2.6974 2.6990 2.7007 2.7023
2.7039	2.7055	2.7071	2.7087 2.7104 2.7120 2.7136
2.7152	2.7168	2.7184	2.7200 2.7216 2.7232 2.7248
2.7264	2.7279	2.7295	2.7311 2.7327 2.7343 2.7359
2.7374	2.7390	2.7406	2.7422 2.7437 2.7453 2.7469
2.7484	2.7500	2.7516	2.7531 2.7547 2.7562 2.7578
2.7593	2.7609	2.7624	2.7640 2.7655 2.7671 2.7686
2.7701	2.7717	2.7732	2.7747 2.7763 2.7778 2.7793
2.7808	2.7824	2.7839	2.7854 2.7869 2.7884 2.7899
2.7915	2.7930	2.7945	2.7960 2.7975 2.7990 2.8005
2.8020	2.8035	2.8050	2.8065 2.8079 2.8094 2.8109
2.8124	2.8139	2.8154	2.8168 2.8183 2.8198 2.8213

	NORTH POND	OUTLET	AHYMO.	OUT		
2.8227	2.8242	2.8257	2.8271	2.8286	2.8301	2.8315
2.8330	2.8344	2.8359	2.8373	2.8388	2.8402	2.8417
2.8431	2.8446	2.8460	2.8474	2.8489	2.8503	2.8517
2.8532	2.8546	2.8560	2.8574	2.8589	2.8603	2.8617
2.8631	2.8645	2.8659	2.8674	2.8688	2.8702	2.8716
2.8730	2.8744	2.8758	2.8772	2.8786	2.8800	2.8813
2.8827	2.8841	2.8855	2.8869	2.8883	2.8897	2.8910
2.8924	2.8938	2.8952	2.8965	2.8979	2.8993	2.9006
2.9020	2.9033	2.9047	2.9061	2.9074	2.9088	2.9101
2.9115	2.9128	2.9141	2.9155	2.9168	2.9182	2.9195
2.9208	2.9222	2.9235	2.9248	2.9262	2.9275	2.9288
2.9301	2.9314	2.9328	2.9341	2.9354	2.9367	2.9380
2.9393	2.9406	2.9419	2.9432	2.9445	2.9458	2.9471
2.9484	2.9497	2.9510	2.9523	2.9536	2.9549	2.9561
2.9574	2.9587	2.9600	2.9612	2.9625	2.9638	2.9651
2.9663	2.9676	2.9689	2.9701	2.9714	2.9726	2.9739
2.9751	2.9764	2.9776	2.9789	2.9801	2.9814	2.9826
2.9839	2.9851	2.9863	2.9876	2.9888	2.9900	2.9912
2.9925	2.9937	2.9949	2.9961	2.9974	2.9986	2.9998
3.0010	3.0022	3.0034	3.0046	3.0058	3.0070	3.0082
3.0094	3.0106	3.0118	3.0130	3.0142	3.0154	3.0166
3.0178	3.0189	3.0201	3.0213	3.0225	3.0237	3.0248
3.0260	3.0272	3.0283	3.0295	3.0307	3.0318	3.0330
3.0341	3.0353	3.0364	3.0376	3.0387	3.0399	3.0410
3.0422	3.0433	3.0445	3.0456	3.0467	3.0479	3.0490
3.0501	3.0513	3.0524	3.0535	3.0546	3.0558	3.0569
3.0580	3.0591	3.0602	3.0613	3.0624	3.0635	3.0646
3.0658	3.0669	3.0680	3.0690	3.0701	3.0712	3.0723
3.0734	3.0745	3.0756	3.0767	3.0777	3.0788	3.0799
3.0810	3.0821	3.0831	3.0842	3.0853	3.0863	3.0874
3.0885	3.0895	3.0906	3.0916	3.0927	3.0937	3.0948
3.0958	3.0969	3.0979	3.0990	3.1000		

COMPUTE NM HYD ID=1 HYD NO=101 DA=.004297 SQ MI  
PER A=0 PER B=17.50 PER C=24.5 PER D=58  
TP=-.145 MASSRAIN=-1

K = 0.079025HR TP = 0.145000HR K/TP RATIO = 0.545000 SHAPE  
 CONSTANT, N = 7.106428  
 UNIT PEAK = 9.0456 CFS UNIT VOLUME = 0.9989 B = 526.28  
 P60 = 2.1400  
 AREA = 0.002492 SQ MI IA = 0.10000 INCHES INF = 0.04000  
 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =  
 0.050000

K = 0.129687HR TP = 0.145000HR K/TP RATIO = 0.894390 SHAPE  
 CONSTANT, N = 3.964006  
 UNIT PEAK = 4.3907 CFS UNIT VOLUME = 0.9979 B = 352.77  
 P60 = 2.1400 AREA = 0.001805 SQ MI IA = 0.41250 INCHES INF = 1.00500  
 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT =  
 0.050000

PRINT HYD ID=1 CODE=3

**PARTIAL HYDROGRAPH**

TIME FLOW TIME FLOW TIME FLOW  
Page 2

TIME HRS	FLOW CFS	NORTH POND OUTLET AHYMO.OUT					
		TIME HRS	FLOW CFS	TIME HRS	FLOW CFS	HRS	CFS
14.850	0.000	0.0	19.800	4.950	0.0	9.900	0.1
	0.0			0.0			
15.000	0.150	0.0	19.950	5.100	0.0	10.050	0.1
	0.0			0.0			
15.150	0.300	0.0	20.100	5.250	0.0	10.200	0.1
	0.0			0.0			
15.300	0.450	0.0	20.250	5.400	0.0	10.350	0.1
	0.0			0.0			
15.450	0.600	0.0	20.400	5.550	0.0	10.500	0.1
	0.0			0.0			
15.600	0.750	0.0	20.550	5.700	0.1	10.650	0.1
	0.0			0.0			
15.750	0.900	0.3	20.700	5.850	0.1	10.800	0.1
	0.0			0.0			
15.900	1.050	0.6	20.850	6.000	0.1	10.950	0.0
	0.0			0.0			
16.050	1.200	1.3	21.000	6.150	0.1	11.100	0.0
	0.0			0.0			
16.200	1.350	3.5	21.150	6.300	0.1	11.250	0.0
	0.0			0.0			
16.350	1.500	11.4	21.300	6.450	0.1	11.400	0.0
	0.0			0.0			
16.500	1.650	7.8	21.450	6.600	0.1	11.550	0.0
	0.0			0.0			
16.650	1.800	3.7	21.600	6.750	0.1	11.700	0.0
	0.0			0.0			
16.800	1.950	2.0	21.750	6.900	0.1	11.850	0.0
	0.0			0.0			
16.950	2.100	1.2	21.900	7.050	0.1	12.000	0.0
	0.0			0.0			
17.100	2.250	0.7	22.050	7.200	0.1	12.150	0.0
	0.0			0.0			
17.250	2.400	0.5	22.200	7.350	0.1	12.300	0.0
	0.0			0.0			
17.400	2.550	0.3	22.350	7.500	0.1	12.450	0.0
	0.0			0.0			
17.550	2.700	0.2	22.500	7.650	0.1	12.600	0.0
	0.0			0.0			
17.700	2.850	0.1	22.650	7.800	0.1	12.750	0.0
	0.0			0.0			
17.850	3.000	0.1	22.800	7.950	0.1	12.900	0.0
	0.0			0.0			
18.000	3.150	0.1	22.950	8.100	0.1	13.050	0.0
	0.0			0.0			
18.150	3.300	0.1	23.100	8.250	0.1	13.200	0.0
	0.0			0.0			
18.300	3.450	0.0	23.250	8.400	0.1	13.350	0.0
	0.0			0.0			
18.450	3.600	0.0	23.400	8.550	0.1	13.500	0.0
	0.0			0.0			
18.600	3.750	0.0	23.550	8.700	0.1	13.650	0.0
	0.0			0.0			
18.750	3.900	0.0	23.700	8.850	0.1	13.800	0.0
	0.0			0.0			
18.900	4.050	0.0	23.850	9.000	0.1	13.950	0.0
	0.0			0.0			
19.050	4.200	0.0	24.000	9.150	0.1	14.100	0.0
	0.0			0.0			
19.200	4.350	0.0	24.150	9.300	0.1	14.250	0.0
	0.0			0.0			

			NORTH POND	OUTLET	AHYMO.OUT		
19.350	4.500	0.0	24.300	9.450	0.1	14.400	0.0
19.500	4.650	0.0	24.450	9.600	0.1	14.550	0.0
19.650	4.800	0.0	24.600	9.750	0.1	14.700	0.0
			RUNOFF VOLUME =	2.16519 INCHES	=	0.4962 ACRE-FEET	
			PEAK DISCHARGE RATE =	11.53 CFS	AT	1.550 HOURS	BASIN AREA =
0.0043 SQ. MI.							

\* ROUTE THE TOTAL FLOW THROUGH THE PROPOSED RESERVOIR  
ROUTE RESERVOIR ID=2 HYD NO=102 INFLOW=1 CODE=3  
OUTFLOW(CFS) STORAGE(AC-FT) ELEV(FT)  
5.24 0.000 42.00  
7.63 0.001 44.00  
8.83 0.001 45.00  
9.88 0.016 46.00  
10.83 0.072 47.00

*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)															
0.00	0.00	37.62	-0.002	0.00															
0.15	0.00	42.00	0.000	5.24															
0.30	0.00	42.00	0.000	5.24															
0.45	0.00	42.00	0.000	5.24															
0.60	0.00	42.00	0.000	5.24															
0.75	0.04	42.00	0.000	5.24															
0.90	0.28	42.00	0.000	5.24															
1.05	0.59	42.00	0.000	5.24															
1.20	1.25	42.00	0.000	5.24															
1.35	3.52	42.00	0.000	5.24															
1.50	11.45	45.64	0.011	9.51															
1.65	7.83	46.01	0.017	9.89															
1.80	3.68	42.00	0.000	5.24															
1.95	2.01	42.00	0.000	5.24															
2.10	1.16	42.00	0.000	5.24															
2.25	0.74	42.00	0.000	5.24															
2.40	0.51	42.00	0.000	5.24															
2.55	0.29	42.00	0.000	5.24															
2.70	0.19	42.00	0.000	5.24															
2.85	0.13	42.00	0.000	5.24															
3.00	0.09	42.00	0.000	5.24															
3.15	0.07	42.00	0.000	5.24															
3.30	0.06	42.00	0.000	5.24															
3.45	0.04	42.00	0.000	5.24															
3.60	0.04	42.00	0.000	5.24															
3.75	0.04	42.00	0.000	5.24															

		NORTH	POND	OUTLET	AHYMO	OUT
3.90	0.04	42.00	0.000		5.24	
4.05	0.04	42.00	0.000		5.24	
4.20	0.04	42.00	0.000		5.24	
4.35	0.04	42.00	0.000		5.24	
4.50	0.04	42.00	0.000		5.24	
4.65	0.04	42.00	0.000		5.24	
4.80	0.04	42.00	0.000		5.24	
4.95	0.04	42.00	0.000		5.24	
5.10	0.05	42.00	0.000		5.24	
5.25	0.05	42.00	0.000		5.24	
5.40	0.05	42.00	0.000		5.24	
5.55	0.05	42.00	0.000		5.24	
5.70	0.05	42.00	0.000		5.24	
5.85	0.05	42.00	0.000		5.24	
6.00	0.05	42.00	0.000		5.24	
6.15	0.06	42.00	0.000		5.24	
6.30	0.05	42.00	0.000		5.24	
6.45	0.06	42.00	0.000		5.24	
6.60	0.06	42.00	0.000		5.24	
6.75	0.06	42.00	0.000		5.24	
6.90	0.05	42.00	0.000		5.24	
7.05	0.05	42.00	0.000		5.24	
7.20	0.05	42.00	0.000		5.24	
7.35	0.05	42.00	0.000		5.24	
7.50	0.05	42.00	0.000		5.24	
7.65	0.05	42.00	0.000		5.24	
7.80	0.05	42.00	0.000		5.24	
7.95	0.05	42.00	0.000		5.24	
8.10	0.05	42.00	0.000		5.24	
8.25	0.05	42.00	0.000		5.24	

PEAK DISCHARGE = 9.968 CFS - PEAK OCCURS AT HOUR 1.60  
 MAXIMUM WATER SURFACE ELEVATION = 46.093  
 MAXIMUM STORAGE = 0.0212 AC-FT INCREMENTAL TIME= 0.050000HRS

FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 19:45:15

Spondrout0909 16.txt

```
*S      AHYMO - SOUTH INLET  
*S      POND ROUTING  
START          TIME=0.0  PUNCH CODE=0  
  
RAINFALL      TYPE=2  
QUARTER=0.0    ONE= 2.14 IN  
SIX= 2.60 IN   DAY= 3.10 IN   DT = 0.05 HR  
  
COMPUTE NM HYD      ID=1  HYD NO=101  DA= .0073875 SQ MI  
PER A=0  PER B=17.4 PER C=19.2 PER D=63.4  
TP=-.142  MASSRAIN=-1  
  
PRINT HYD      ID=1  CODE=3  
  
* ROUTE THE TOTAL FLOW THROUGH THE PROPOSED RESERVOIR  
ROUTE RESERVOIR      ID=2  HYD NO=102  INFLOW=1  CODE=3  
OUTFLOW(CFS)      STORAGE(AC-FT)      ELEV(FT)  
    7.37            0.000            44.00  
   11.26            0.001            45.00  
   14.11            0.001            46.25  
  16.48            0.014            46.50  
  17.54            0.062            47.00
```

FINISH

## SOUTH POND AHYMO.OUT

AHYMO PROGRAM (AHYMO-S4) - Version: S4.01a - Rel: 01a  
 RUN DATE (MON/DAY/YR) = 09/11/2016  
 START TIME (HR:MIN:SEC) = 20:09:09  
 USER NO.=  
 RioGrandeSingleA41963517  
 INPUT FILE = \Owner\Desktop\2015 JOBS\15120-alameda  
 appartments\RAINAGE\Spondrout0909 16.txt

\*S AHYMO - SOUTH INLET  
 \*S POND ROUTING

START TIME=0.0 PUNCH CODE=0

RAINFALL TYPE=2  
 QUARTER=0.0 ONE= 2.14 IN  
 SIX= 2.60 IN DAY= 3.10 IN DT = 0.05 HR

AREAS (NM & AZ) - D1 24-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE

DT	0.050000 HOURS	END TIME	= 24.000002 HOURS
0.0000	0.0031	0.0062	0.0096 0.0133 0.0171 0.0214
0.0274	0.0368	0.0470	0.0575 0.0690 0.0807 0.0927
0.1052	0.1178	0.1320	0.1467 0.1627 0.1887 0.2196
0.2611	0.3081	0.3661	0.4435 0.5307 0.6811 0.9149
1.3155	1.5971	1.8192	1.9308 2.0287 2.0989 2.1549
2.2036	2.2393	2.2720	2.2991 2.3181 2.3331 2.3464
2.3590	2.3700	2.3804	2.3905 2.4002 2.4083 2.4129
2.4175	2.4219	2.4261	2.4303 2.4343 2.4383 2.4422
2.4459	2.4495	2.4531	2.4566 2.4601 2.4634 2.4667
2.4699	2.4731	2.4762	2.4792 2.4822 2.4851 2.4880
2.4909	2.4937	2.4965	2.4992 2.5019 2.5046 2.5072
2.5098	2.5124	2.5149	2.5175 2.5200 2.5224 2.5249
2.5273	2.5296	2.5320	2.5343 2.5366 2.5389 2.5412
2.5434	2.5456	2.5478	2.5500 2.5521 2.5542 2.5564
2.5584	2.5605	2.5626	2.5646 2.5666 2.5686 2.5706
2.5725	2.5745	2.5764	2.5783 2.5802 2.5821 2.5839
2.5858	2.5876	2.5894	2.5912 2.5930 2.5948 2.5965
2.5983	2.6000	2.6017	2.6035 2.6052 2.6069 2.6086
2.6104	2.6121	2.6138	2.6155 2.6172 2.6190 2.6207
2.6224	2.6241	2.6258	2.6275 2.6292 2.6309 2.6326
2.6343	2.6360	2.6377	2.6394 2.6411 2.6428 2.6445
2.6461	2.6478	2.6495	2.6512 2.6529 2.6545 2.6562
2.6579	2.6595	2.6612	2.6629 2.6645 2.6662 2.6679
2.6695	2.6712	2.6728	2.6745 2.6761 2.6778 2.6794
2.6811	2.6827	2.6844	2.6860 2.6876 2.6893 2.6909
2.6925	2.6942	2.6958	2.6974 2.6990 2.7007 2.7023
2.7039	2.7055	2.7071	2.7087 2.7104 2.7120 2.7136
2.7152	2.7168	2.7184	2.7200 2.7216 2.7232 2.7248
2.7264	2.7279	2.7295	2.7311 2.7327 2.7343 2.7359
2.7374	2.7390	2.7406	2.7422 2.7437 2.7453 2.7469
2.7484	2.7500	2.7516	2.7531 2.7547 2.7562 2.7578
2.7593	2.7609	2.7624	2.7640 2.7655 2.7671 2.7686
2.7701	2.7717	2.7732	2.7747 2.7763 2.7778 2.7793
2.7808	2.7824	2.7839	2.7854 2.7869 2.7884 2.7899
2.7915	2.7930	2.7945	2.7960 2.7975 2.7990 2.8005
2.8020	2.8035	2.8050	2.8065 2.8079 2.8094 2.8109
2.8124	2.8139	2.8154	2.8168 2.8183 2.8198 2.8213

SOUTH POND AHYMO.OUT

2.8227	2.8242	2.8257	2.8271	2.8286	2.8301	2.8315
2.8330	2.8344	2.8359	2.8373	2.8388	2.8402	2.8417
2.8431	2.8446	2.8460	2.8474	2.8489	2.8503	2.8517
2.8532	2.8546	2.8560	2.8574	2.8589	2.8603	2.8617
2.8631	2.8645	2.8659	2.8674	2.8688	2.8702	2.8716
2.8730	2.8744	2.8758	2.8772	2.8786	2.8800	2.8813
2.8827	2.8841	2.8855	2.8869	2.8883	2.8897	2.8910
2.8924	2.8938	2.8952	2.8965	2.8979	2.8993	2.9006
2.9020	2.9033	2.9047	2.9061	2.9074	2.9088	2.9101
2.9115	2.9128	2.9141	2.9155	2.9168	2.9182	2.9195
2.9208	2.9222	2.9235	2.9248	2.9262	2.9275	2.9288
2.9301	2.9314	2.9328	2.9341	2.9354	2.9367	2.9380
2.9393	2.9406	2.9419	2.9432	2.9445	2.9458	2.9471
2.9484	2.9497	2.9510	2.9523	2.9536	2.9549	2.9561
2.9574	2.9587	2.9600	2.9612	2.9625	2.9638	2.9651
2.9663	2.9676	2.9689	2.9701	2.9714	2.9726	2.9739
2.9751	2.9764	2.9776	2.9789	2.9801	2.9814	2.9826
2.9839	2.9851	2.9863	2.9876	2.9888	2.9900	2.9912
2.9925	2.9937	2.9949	2.9961	2.9974	2.9986	2.9998
3.0010	3.0022	3.0034	3.0046	3.0058	3.0070	3.0082
3.0094	3.0106	3.0118	3.0130	3.0142	3.0154	3.0166
3.0178	3.0189	3.0201	3.0213	3.0225	3.0237	3.0248
3.0260	3.0272	3.0283	3.0295	3.0307	3.0318	3.0330
3.0341	3.0353	3.0364	3.0376	3.0387	3.0399	3.0410
3.0422	3.0433	3.0445	3.0456	3.0467	3.0479	3.0490
3.0501	3.0513	3.0524	3.0535	3.0546	3.0558	3.0569
3.0580	3.0591	3.0602	3.0613	3.0624	3.0635	3.0646
3.0658	3.0669	3.0680	3.0690	3.0701	3.0712	3.0723
3.0734	3.0745	3.0756	3.0767	3.0777	3.0788	3.0799
3.0810	3.0821	3.0831	3.0842	3.0853	3.0863	3.0874
3.0885	3.0895	3.0906	3.0916	3.0927	3.0937	3.0948
3.0958	3.0969	3.0979	3.0990	3.1000		

COMPUTE NM HYD      ID=1 HYD NO=101 DA=.0073875 SQ MI  
 PER A=0 PER B=17.4 PER C=19.2 PER D=63.4  
 TP=-.142 MASSRAIN=-1

K = 0.077390HR      TP = 0.142000HR      K/TP RATIO = 0.545000      SHAPE  
 CONSTANT, N = 7.106428  
 UNIT PEAK = 17.358      CFS      UNIT VOLUME = 0.9985      B = 526.28  
 P60 = 2.1400  
 AREA = 0.004684 SQ MI      IA = 0.10000 INCHES      INF = 0.04000  
 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.128552HR      TP = 0.142000HR      K/TP RATIO = 0.905294      SHAPE  
 CONSTANT, N = 3.913266  
 UNIT PEAK = 6.6520      CFS      UNIT VOLUME = 0.9992      B = 349.35  
 P60 = 2.1400  
 AREA = 0.002704 SQ MI      IA = 0.42131 INCHES      INF = 1.02967  
 INCHES PER HOUR  
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD      ID=1 CODE=3  
 PARTIAL HYDROGRAPH 101.00  
 TIME      FLOW      TIME      FLOW      TIME      FLOW  
 Page 2

TIME		FLOW		TIME		FLOW		SOUTH POND AHYMO.OUT	
HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS	HRS	CFS
	0.000		0.0		20.400		5.100		0.1
15.300	0.1						0.1		10.200
	0.150		0.0		20.550		5.250		0.1
15.450	0.1						0.1		10.350
	0.300		0.0		20.700		5.400		0.1
15.600	0.1						0.1		10.500
	0.450		0.0		20.850		5.550		0.1
15.750	0.1						0.1		10.650
	0.600		0.0		21.000		5.700		0.1
15.900	0.1						0.1		10.800
	0.750		0.1		21.150		5.850		0.1
16.050	0.1						0.1		10.950
	0.900		0.5		21.300		6.000		0.1
16.200	0.1						0.1		11.100
	1.050		1.1		21.450		6.150		0.1
16.350	0.1						0.1		11.250
	1.200		2.4		21.600		6.300		0.1
16.500	0.1						0.1		11.400
	1.350		6.4		21.750		6.450		0.1
16.650	0.1						0.1		11.550
	1.500		20.3				6.600		0.1
16.800	0.1				21.900		6.750		0.1
	1.650		13.4				0.1		11.850
16.950	0.1				22.050		6.900		0.1
	1.800		6.4				0.1		12.000
17.100	0.1				22.200		7.050		0.1
	1.950		3.5				0.1		12.150
17.250	0.1				22.350		7.200		0.1
	2.100		2.0				0.1		12.300
17.400	0.1				22.500		7.350		0.1
	2.250		1.3				0.1		12.450
17.550	0.1				22.650		7.500		0.1
	2.400		0.9				0.1		12.600
17.700	0.1				22.800		7.650		0.1
	2.550		0.5				0.1		12.750
17.850	0.1				22.950		7.800		0.1
	2.700		0.3				0.1		12.900
18.000	0.1				23.100		7.950		0.1
	2.850		0.2				0.1		13.050
18.150	0.1				23.250		8.100		0.1
	3.000		0.2				0.1		13.200
18.300	0.1				23.400		8.250		0.1
	3.150		0.1				0.1		13.350
18.450	0.1				23.550		8.400		0.1
	3.300		0.1				0.1		13.500
18.600	0.1				23.700		8.550		0.1
	3.450		0.1				0.1		13.650
18.750	0.1				23.850		8.700		0.1
	3.600		0.1				0.1		13.800
18.900	0.1				24.000		8.850		0.1
	3.750		0.1				0.1		13.950
19.050	0.1				24.150		9.000		0.1
	3.900		0.1				0.1		14.100
19.200	0.1				24.300		9.150		0.1
	4.050		0.1				0.1		14.250
19.350	0.1				24.450		9.300		0.1
	4.200		0.1				0.1		14.400
19.500	0.1				24.600		9.450		0.1
	4.350		0.1				0.1		14.550
19.650	0.1				24.750		0.0		0.1

			SOUTH POND AHYMO.OUT			
19.800	4.500	0.1	9.600	0.1	14.700	0.1
19.950	4.650	0.1	9.750	0.1	14.850	0.1
20.100	4.800	0.1	9.900	0.1	15.000	0.1
20.250	4.950	0.1	10.050	0.1	15.150	0.1
	0.1					

RUNOFF VOLUME = 2.24744 INCHES = 0.8855 ACRE-FEET  
 PEAK DISCHARGE RATE = 20.34 CFS AT 1.500 HOURS BASIN AREA =  
 0.0074 SQ. MI.

\* ROUTE THE TOTAL FLOW THROUGH THE PROPOSED RESERVOIR  
 ROUTE RESERVOIR ID=2 HYD NO=102 INFLOW=1 CODE=3  
 OUTFLOW(CFS) STORAGE(AC-FT) ELEV(FT)

7.37	0.000	44.00
11.26	0.001	45.00
14.11	0.001	46.25
16.48	0.014	46.50
17.54	0.062	47.00

\* \* \* \* \*

TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)
0.00	0.00	42.11	-0.002	0.00
0.15	0.00	44.00	0.000	7.37
0.30	0.00	44.00	0.000	7.37
0.45	0.00	44.00	0.000	7.37
0.60	0.00	44.00	0.000	7.37
0.75	0.07	44.00	0.000	7.37
0.90	0.54	44.00	0.000	7.37
1.05	1.14	44.00	0.000	7.37
1.20	2.38	44.00	0.000	7.37
1.35	6.42	44.00	0.000	7.37
1.50	20.34	46.50	0.014	16.48
1.65	13.45	46.66	0.030	16.83
1.80	6.37	44.00	0.000	7.37
1.95	3.55	44.00	0.000	7.37
2.10	2.03	44.00	0.000	7.37
2.25	1.29	44.00	0.000	7.37
2.40	0.88	44.00	0.000	7.37
2.55	0.49	44.00	0.000	7.37
2.70	0.32	44.00	0.000	7.37
2.85	0.23	44.00	0.000	7.37
3.00	0.16	44.00	0.000	7.37
3.15	0.13	44.00	0.000	7.37
3.30	0.11	44.00	0.000	7.37
3.45	0.09	44.00	0.000	7.37

		SOUTH POND	AHYMO.OUT
3.60	0.08	44.00	0.000 7.37
3.75	0.07	44.00	0.000 7.37
3.90	0.07	44.00	0.000 7.37
4.05	0.07	44.00	0.000 7.37
4.20	0.07	44.00	0.000 7.37
4.35	0.07	44.00	0.000 7.37
4.50	0.08	44.00	0.000 7.37
4.65	0.08	44.00	0.000 7.37
4.80	0.08	44.00	0.000 7.37
4.95	0.08	44.00	0.000 7.37
5.10	0.09	44.00	0.000 7.37
5.25	0.09	44.00	0.000 7.37
5.40	0.09	44.00	0.000 7.37
5.55	0.09	44.00	0.000 7.37
5.70	0.10	44.00	0.000 7.37
5.85	0.10	44.00	0.000 7.37
6.00	0.10	44.00	0.000 7.37
6.15	0.10	44.00	0.000 7.37
6.30	0.10	44.00	0.000 7.37
6.45	0.10	44.00	0.000 7.37
6.60	0.10	44.00	0.000 7.37
6.75	0.10	44.00	0.000 7.37
6.90	0.10	44.00	0.000 7.37
7.05	0.10	44.00	0.000 7.37
7.20	0.10	44.00	0.000 7.37
7.35	0.10	44.00	0.000 7.37
7.50	0.10	44.00	0.000 7.37
7.65	0.10	44.00	0.000 7.37
7.80	0.10	44.00	0.000 7.37
7.95	0.10	44.00	0.000 7.37
8.10	0.10	44.00	0.000 7.37
8.25	0.10	44.00	0.000 7.37

PEAK DISCHARGE = 16.976 CFS - PEAK OCCURS AT HOUR 1.60  
 MAXIMUM WATER SURFACE ELEVATION = 46.734  
 MAXIMUM STORAGE = 0.0364 AC-FT INCREMENTAL TIME= 0.050000HRS

FINISH

NORMAL PROGRAM FINISH

END TIME (HR:MIN:SEC) = 20:09:09

## VOLUME CALCULATIONS

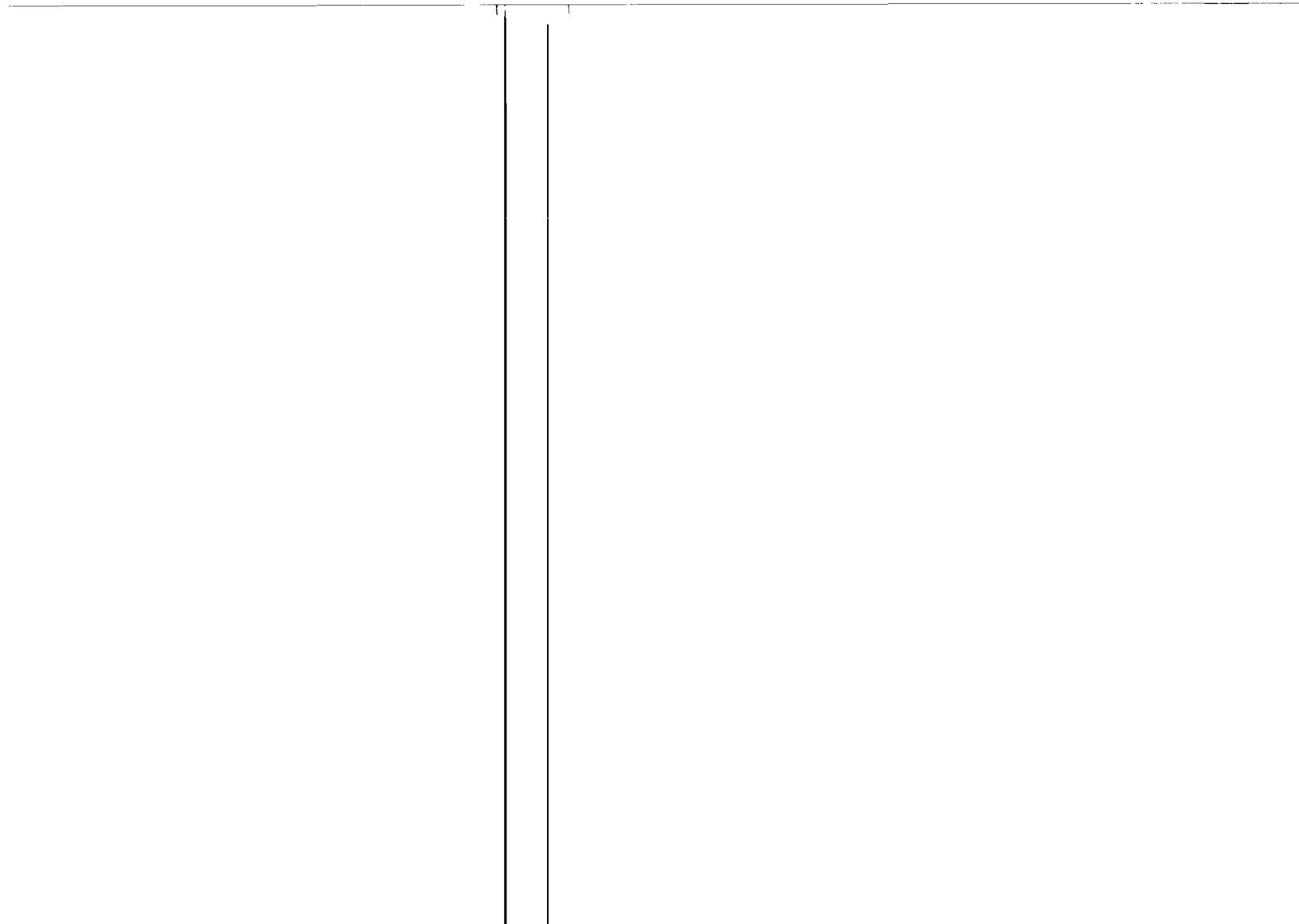
SOUTH INLET

OUTLET	inlet bottom POND OUTLET	ACTUAL ELEV.	DEPTH (FT)	AREA SF	VOLUME PER UNIT	VOLUME CUMULATIVI	VOLUME AC-FT	Q (CFS)
		43.33	0.00	12.00	0	1	0.000	
		43.50	0.00	12.0000	2.04	3.04	0.000	
		44.00	0.50	12.0000	6.0000	9.04	0.000	5.07
		45.00	1.50	12.0000	12.0000	21.04	0.000	7.37
		46.00	2.50	12.0000	12.0000	33.04	0.001	11.26
		46.25	3.50	12.0000	12.0000	45.04	0.001	14.11
		46.50	4.50	2275.0000	571.7500	616.79	0.014	16.48
		47.00	5.00	6054.0000	2082.2500	2699.04	0.062	17.54

Orifice Equation

$$Q = CA \sqrt{2gH}$$

C = 0.6  
 Diameter (in) 18  
 Area (ft^2)= 1.767145868  
 g = 32.2  
 H (Ft) = Depth of water above center of orifice  
 Q (CFS) = Flow



# VOLUME CALCULATIONS

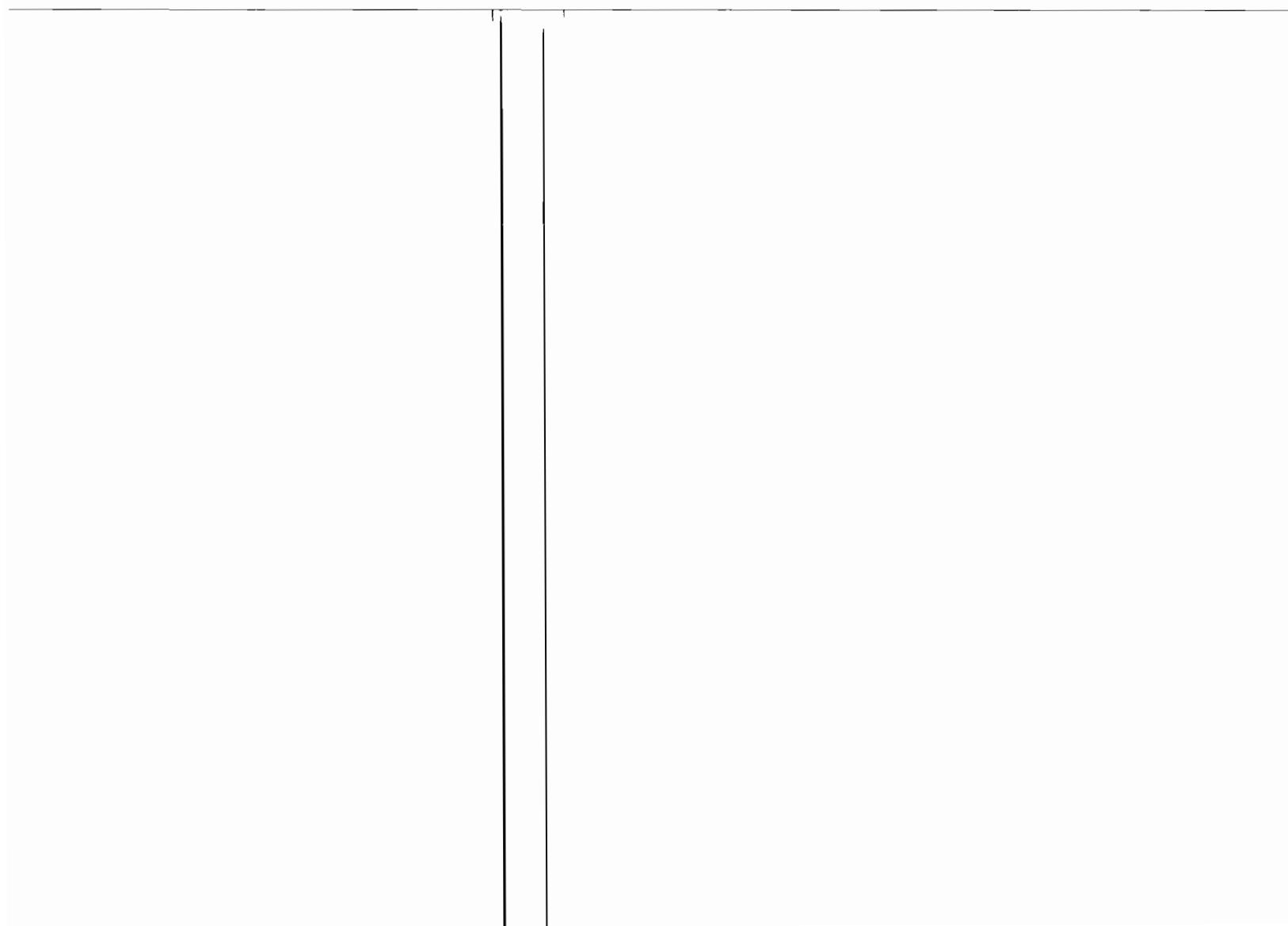
NORTH INLET

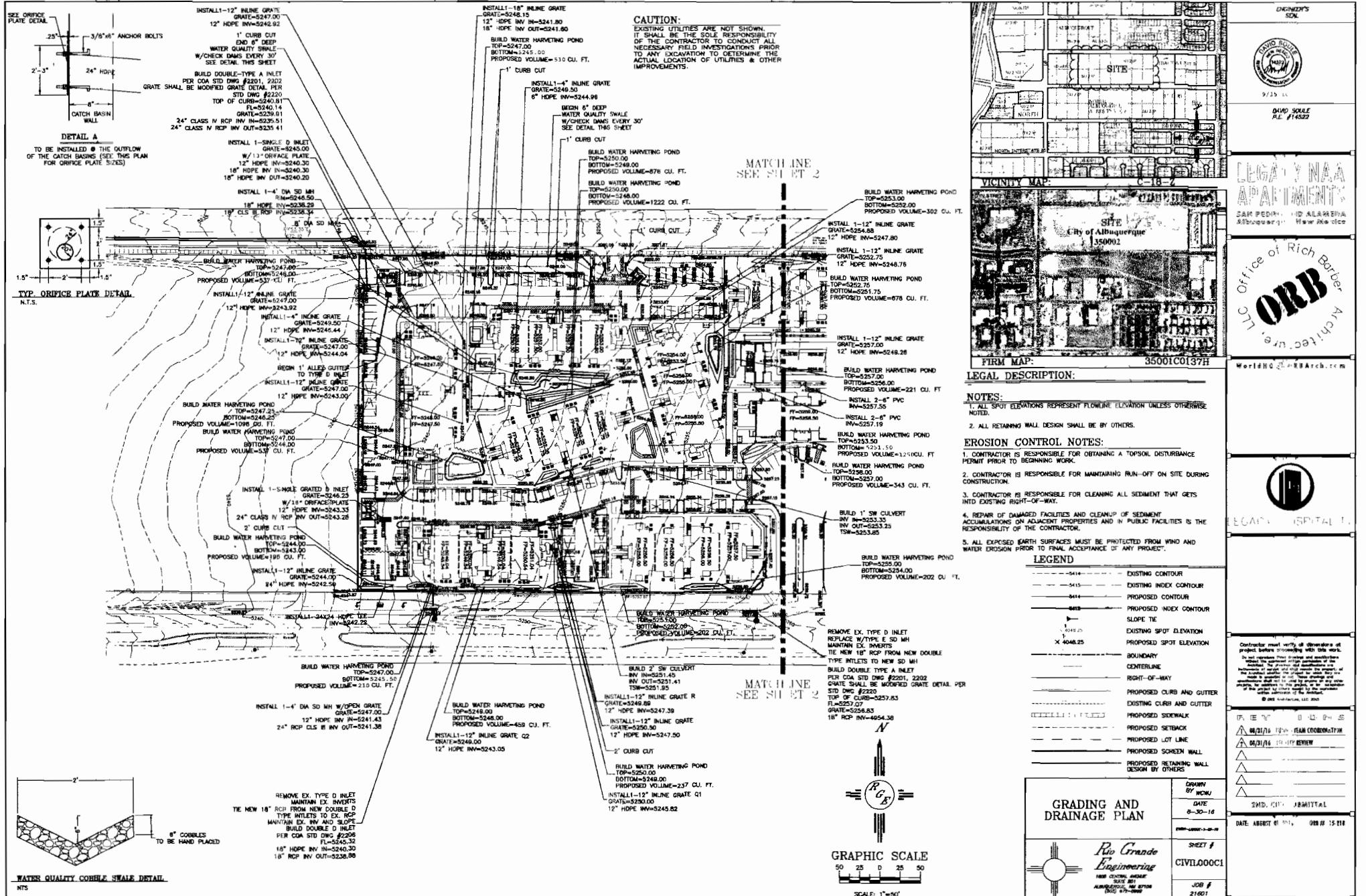
OUTLET	inlet bottom POND OUTLET	ACTUAL ELEV.	DEPTH (FT)	AREA SF	VOLUME PER UNIT	VOLUME CUMULATIVI	VOLUME AC-FT	Q (CFS)
		40.20	0.00	12.00	0	1	0.000	
		40.50	0.00	12.0000	2.04	3.04	0.000	
		42.00	1.50	12.0000	6.0000	9.04	0.000	5.24
		43.00	2.50	12.0000	12.0000	21.04	0.000	6.21
		44.00	3.50	12.0000	12.0000	33.04	0.001	7.63
		45.00	4.50	12.0000	12.0000	45.04	0.001	8.83
		46.00	5.50	2565.0000	644.2500	689.29	0.016	9.88
		47.00	6.50	7285.0000	2462.5000	3151.79	0.072	10.83

Orifice Equation

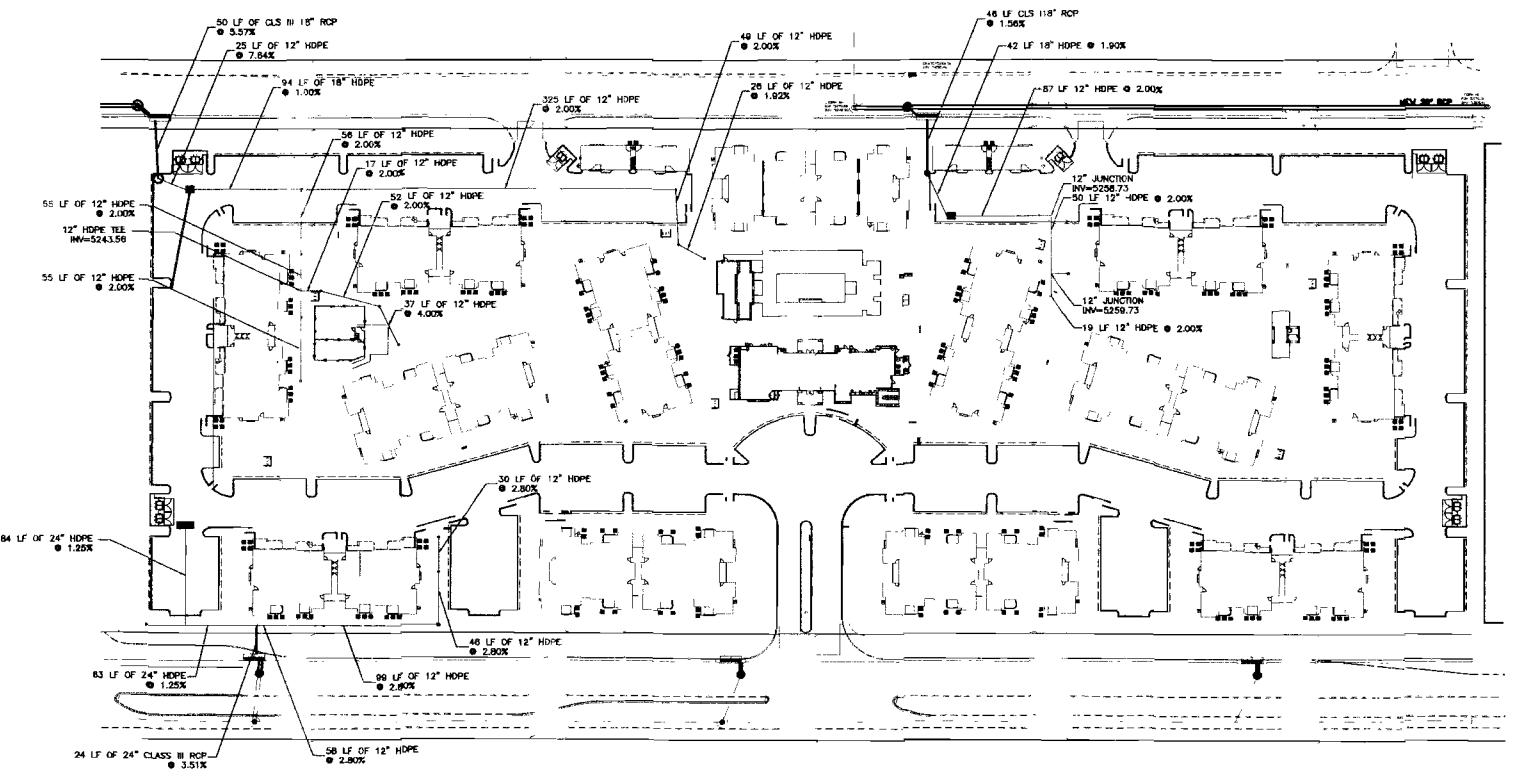
$$Q = CA \sqrt{2gH}$$

C = 0.6  
 Diameter (in) 13  
 Area (ft^2)= 0.921752011



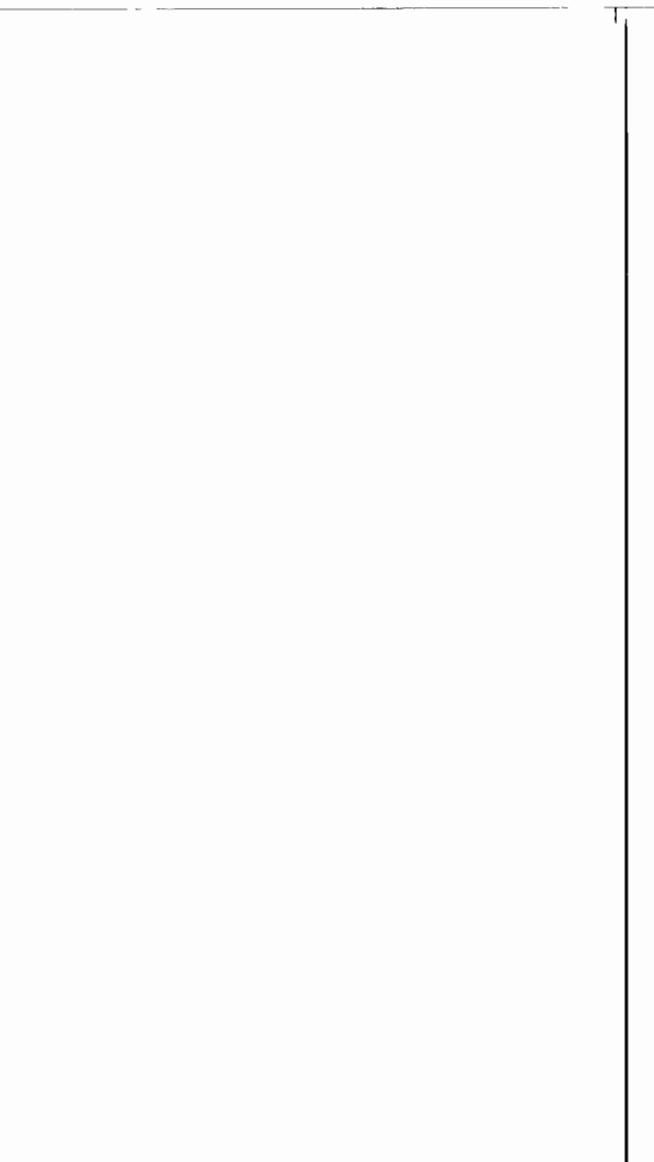
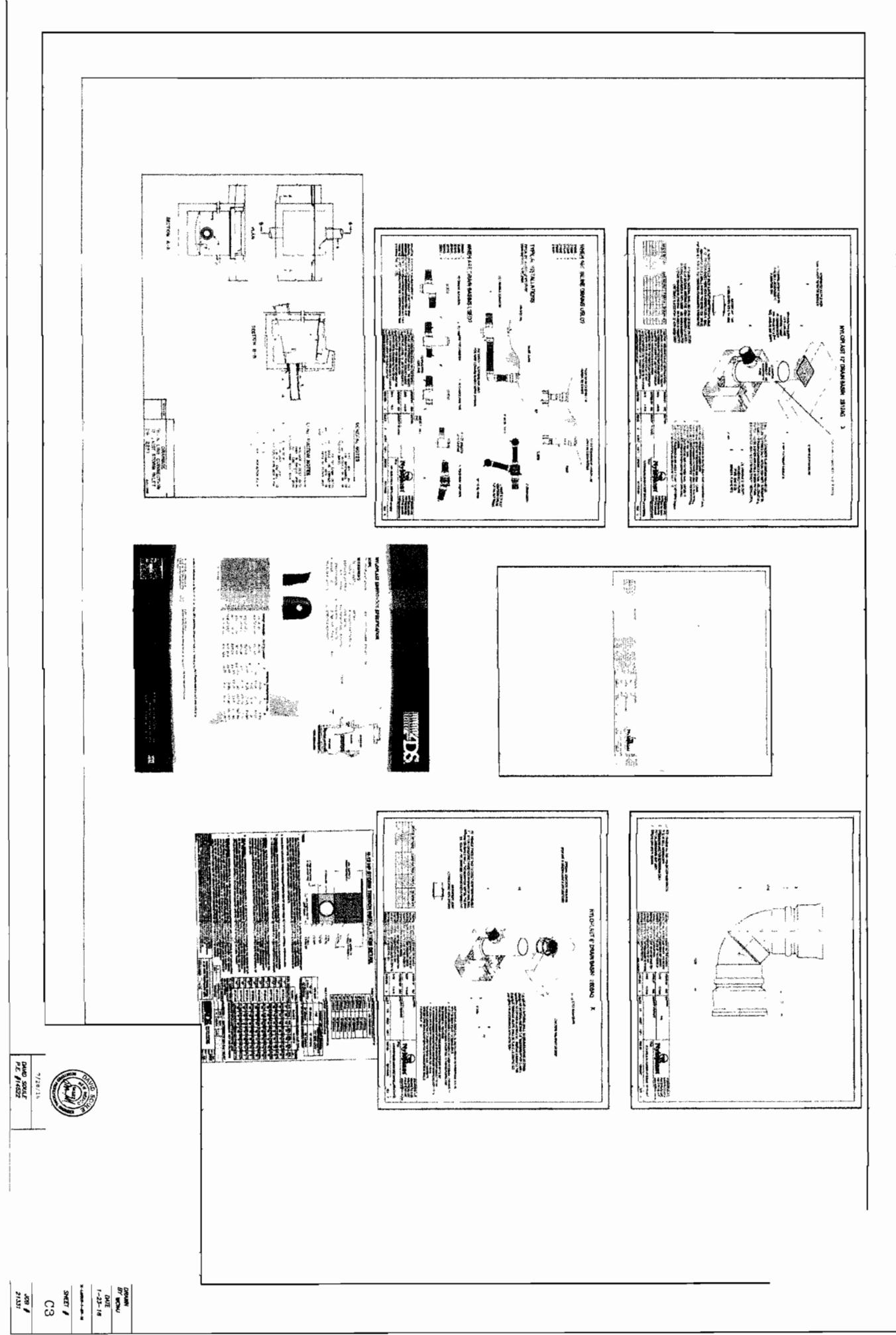






	<i>Rio Grande</i> <b>Engineering</b> 1005 CENTRAL AVENUE ALBUQUERQUE, NM 87108 (505) 265-0860	DRAWN BY RHW  DATE 6-30-16  <small>PRINT NUMBER 40-16</small>	 24H. CR
		SHEET # <b>CIVIL000C3</b>	DATE: AUGUST 01,
		JOB # <b>21801</b>	

ENCODER'S SEAL	
DATE: 08/15/16	
DAVID SOULE P.E. #14322	
<b>LEGA V NAA APARTMENT</b> CLASS PERMIT - ID: 40-40-40-000 & 40-40-40-000 - New Structure	
 <b>WORK</b>	
DATE: 08/15/16 - EXPIRES: 08/15/16	
I - A(1) - 53-12-1:	
<p>Contractor and verify all dimensions at project before commencing work.</p> <p>Do not reproduce these drawings and specifications without the expressed written permission of the architect or engineer.</p> <p>The architect or engineer reserves the right to withdraw his services if the contractor or any other person engaged in the construction of the project violates any of the terms of the agreement.</p> <p style="text-align: center;">© ULC Architectural LLC 2015</p>	
<p>Contractor and verify all dimensions at project before commencing work.</p> <p>Do not reproduce these drawings and specifications without the expressed written permission of the architect or engineer.</p> <p>The architect or engineer reserves the right to withdraw his services if the contractor or any other person engaged in the construction of the project violates any of the terms of the agreement.</p> <p style="text-align: center;">© ULC Architectural LLC 2015</p>	
<p>RECEIVED [initials] DATE: 08/15/16</p> <p>▲ 08/21/16 REISSUE 1 YEAR CERTIFICATION</p> <p>▲ 08/21/16 11-MT REVIEW</p> <p>▲ ▲ ▲ ▲</p> <p style="text-align: right;">SMB, GCF 1000FTAL</p>	
DATE: AUGUST 01, 2016      OEM # 15-118	





**CAUTION:**

EXISTING UTILITIES ARE NOT SHOWN.  
IT SHALL BE THE SOLE RESPONSIBILITY  
OF THE CONTRACTOR TO CONDUCT ALL  
NECESSARY FIELD INVESTIGATIONS PRIOR  
TO ANY EXCAVATION TO DETERMINE THE  
ACTUAL LOCATION OF UTILITIES & OTHER  
IMPROVEMENTS.

 ENGINEER'S  
SEAL

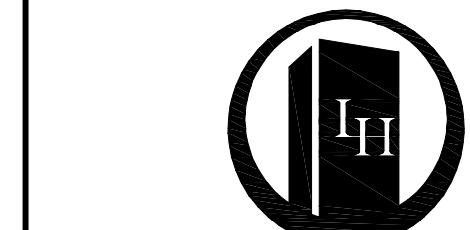
 9/15/16  
DAVID SOULE  
P.E. #14522

**LEGACY NAA  
APARTMENTS**

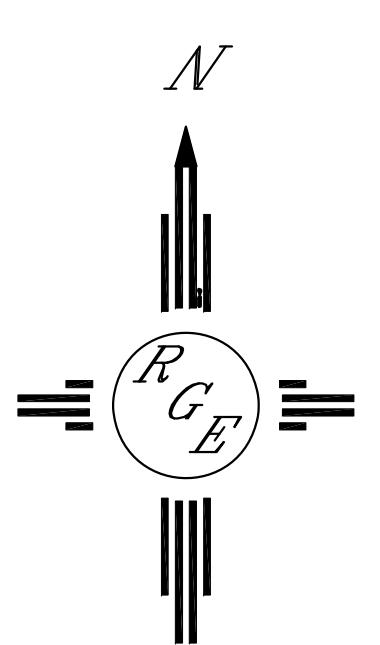
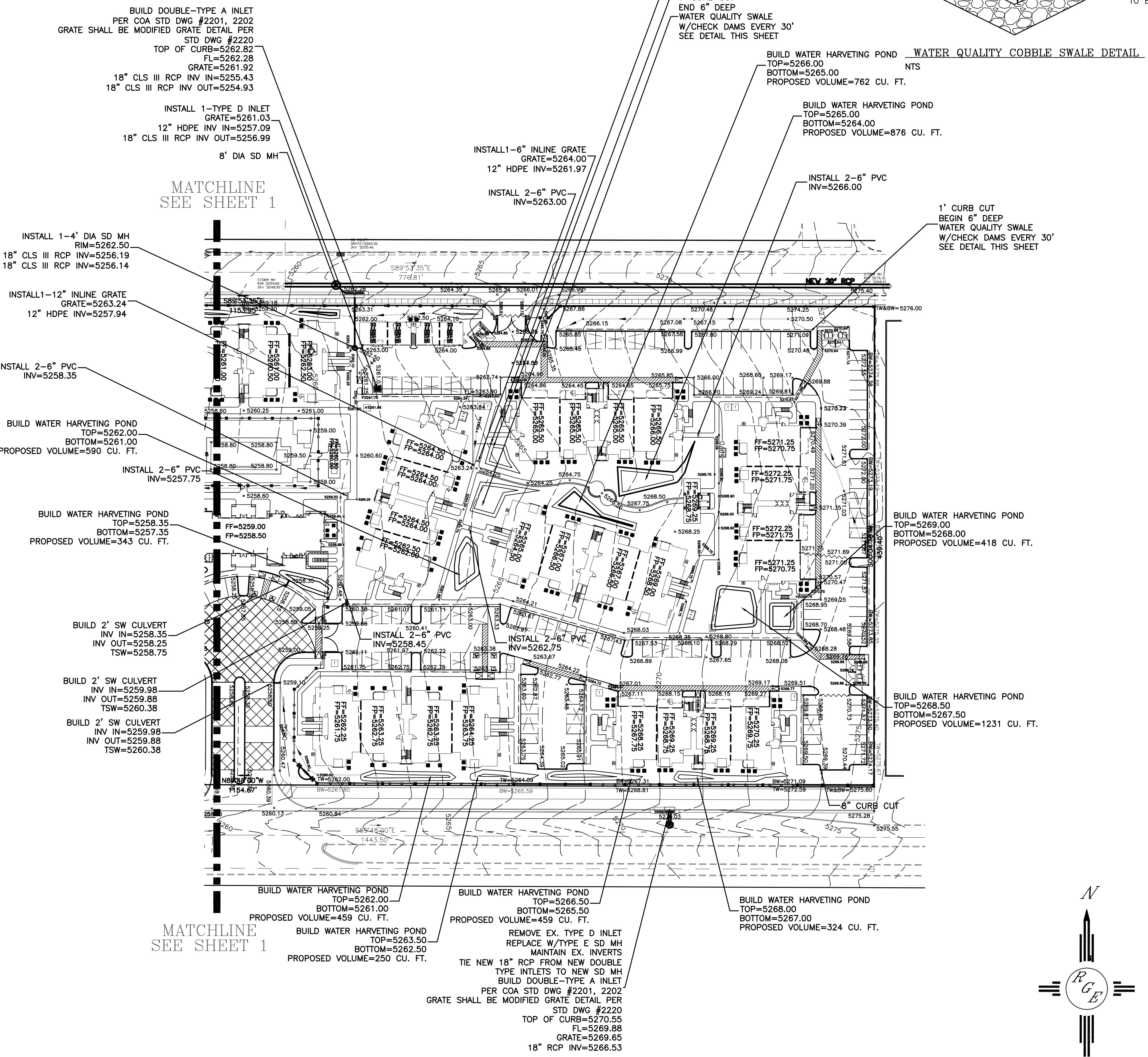
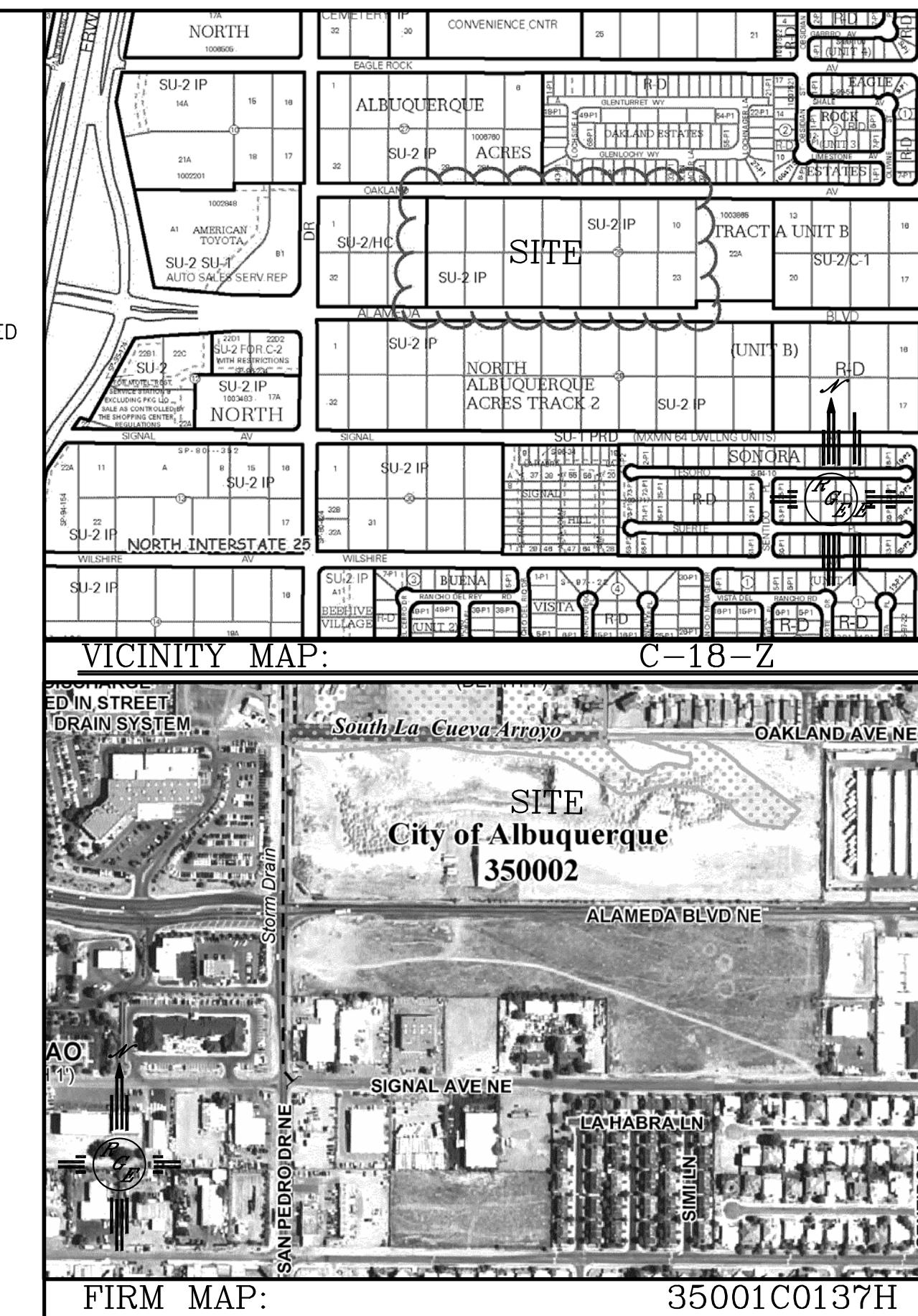
 SAN PEDRO AND ALAMEDA  
Albuquerque, New Mexico

 Office of Rich Barber  
Architect  
**ORB**

WorldHQ@ORBarb.com



LEGACY HOSPITALITY



<b>GRADING AND DRAINAGE PLAN</b>	DRAWN BY	WCWJ
	DATE	8-30-16
	21601-LAYOUT-1-07-16	
	SHEET #	CIVILO00C2
Rio Grande Engineering	JOB #	21601
1606 CENTRAL AVENUE SUITE 201 ALBUQUERQUE, NM 87106 (505) 872-0999		

△ 08/31/16 DESIGN TEAM COORDINATION
△ 08/31/16 1ST CITY REVIEW
△ 08/31/16 2ND. CITY SUBMITTAL
DATE: AUGUST 01, 2016 ORB # 15-218

Contractor must verify all dimensions at project before proceeding with work.  
Do not reproduce these drawings and specifications without written permission from the Architect. The drawings and specifications are instruments of service only and remain the property of the Architect. They are to be returned to the Architect when they are made or executed or not. These drawings and specifications are not to be copied by anyone or other projects, for addition to this project or for completion of this project by others except by the expressed written consent of the Architect.

© ORB Architecture, LLC 2015



9/15/16

DAVID SOULE  
P.E. #14522

# LEGACY NAA APARTMENTS

SAN PEDRO AND ALAMEDA  
Albuquerque, New Mexico

Office of Rich Barber  
Architect  
ORB

WorldHQ@ORBArch.com



LEGACY HOSPITALITY

Contractor must verify all dimensions at project before proceeding with this work.  
Do not reproduce these drawings and specifications without written permission from the Architect. The drawings and specifications are instruments of service and shall remain the property of the Architect. They are to be used only while they are made or executed or not. These drawings and specifications may not be copied by anyone and other projects for addition to this project or for completion of this project by others except by the expressed written consent of the Architect.

© ORB Architecture, LLC 2015

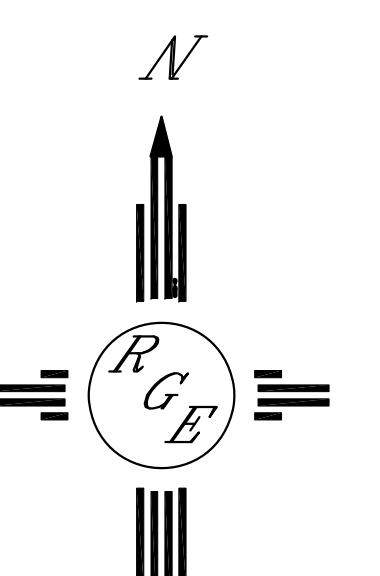
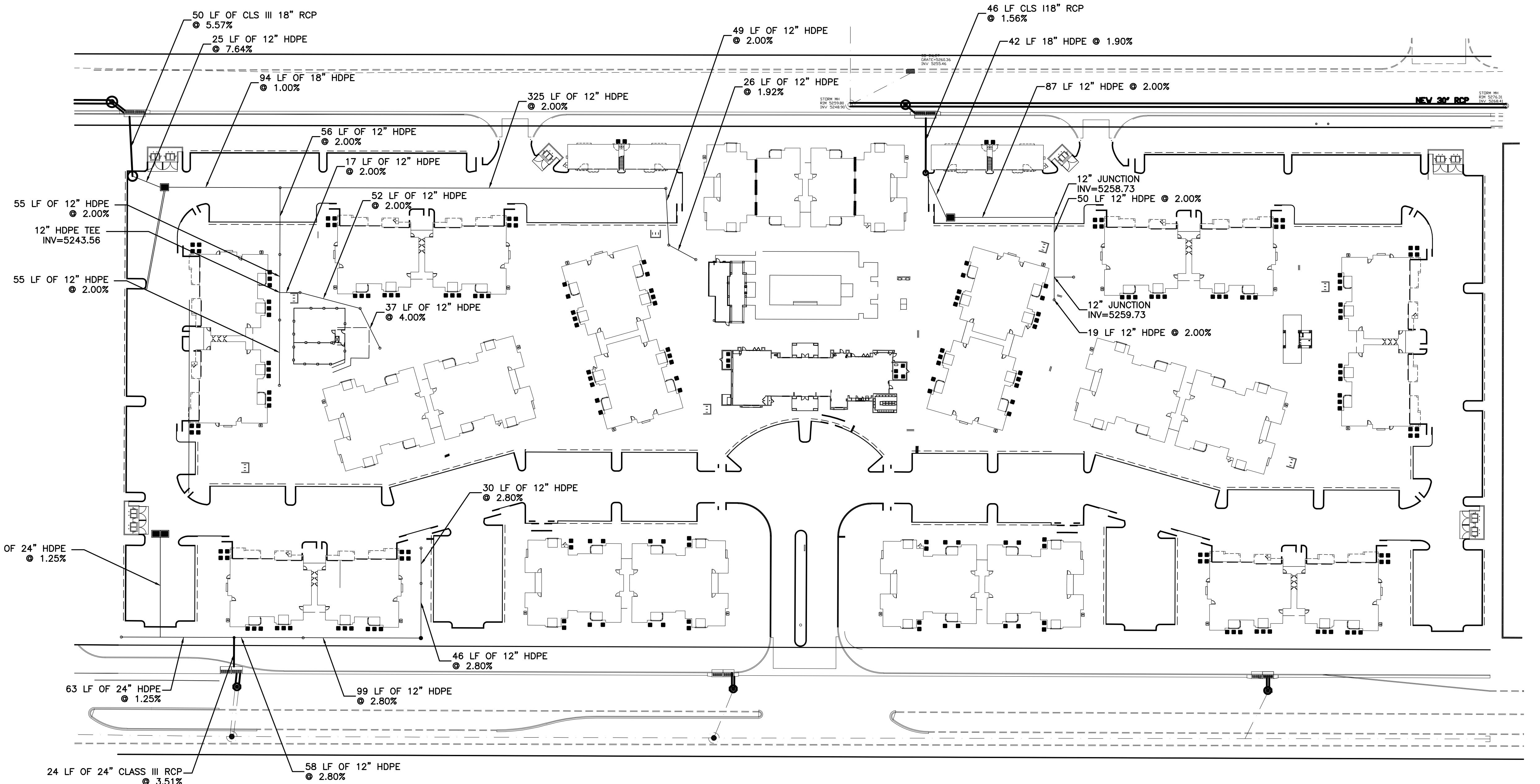
## REVIZIONS

08/31/16 DESIGN TEAM COORDINATION

08/31/16 1ST CITY REVIEW

2ND. CITY SUBMITTAL

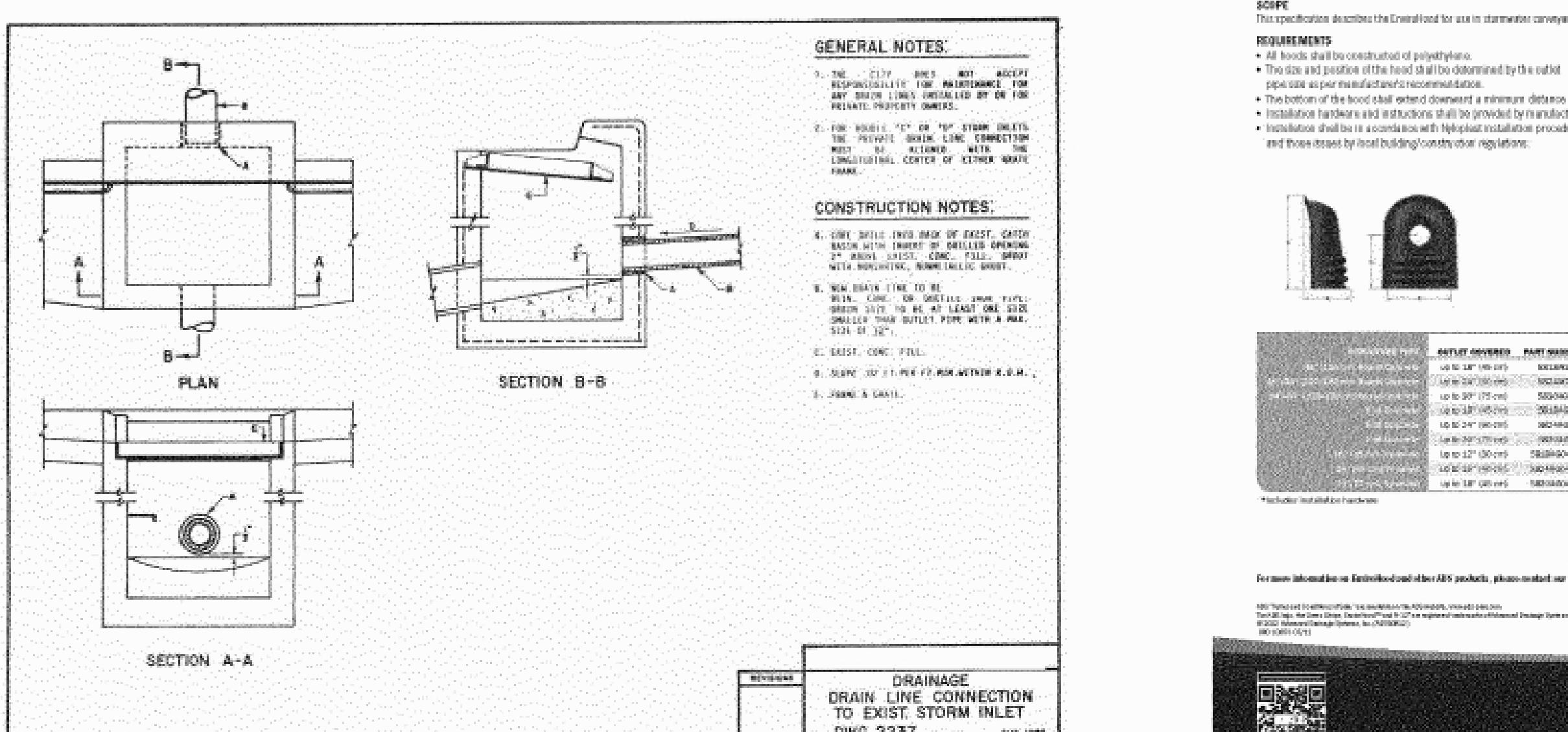
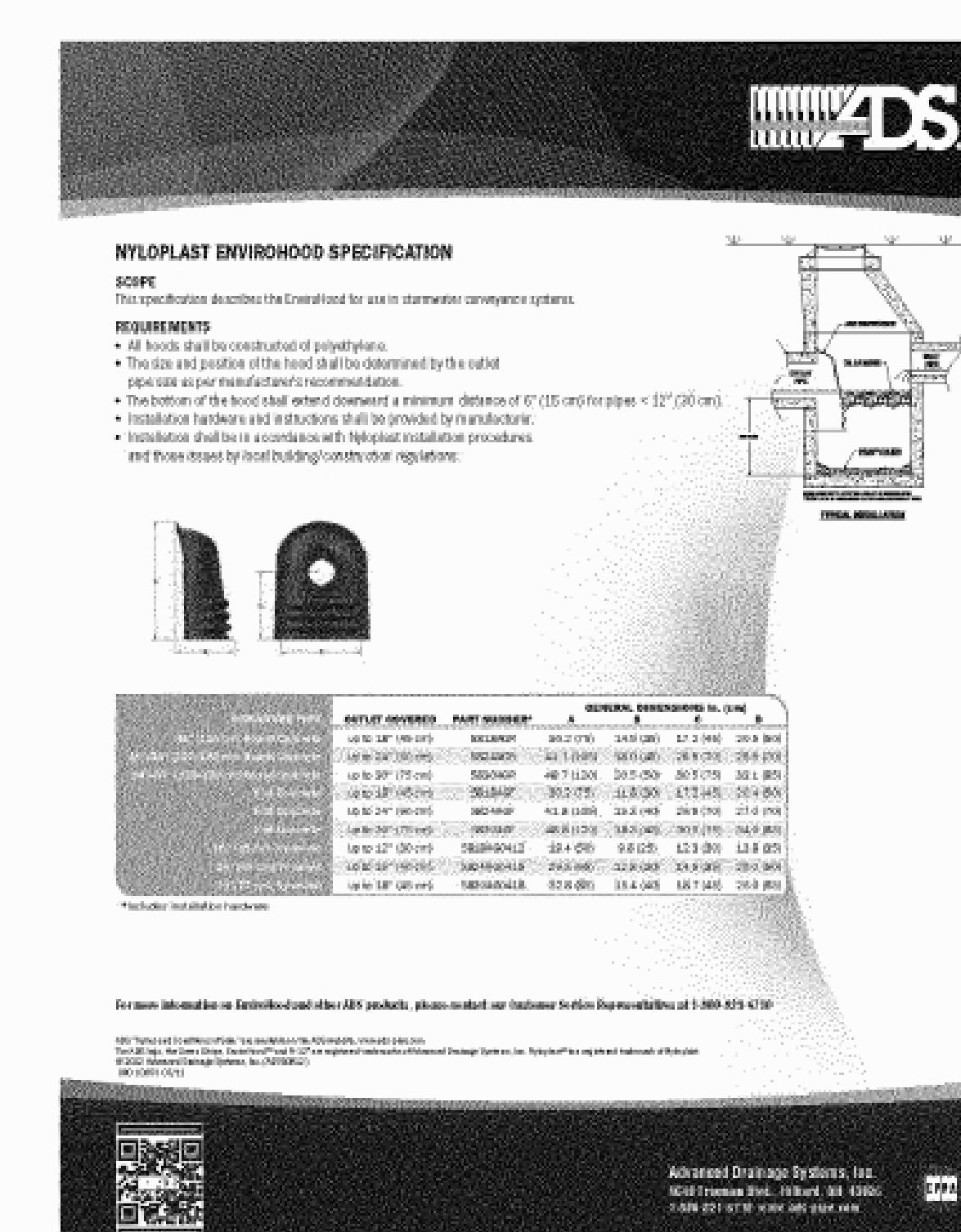
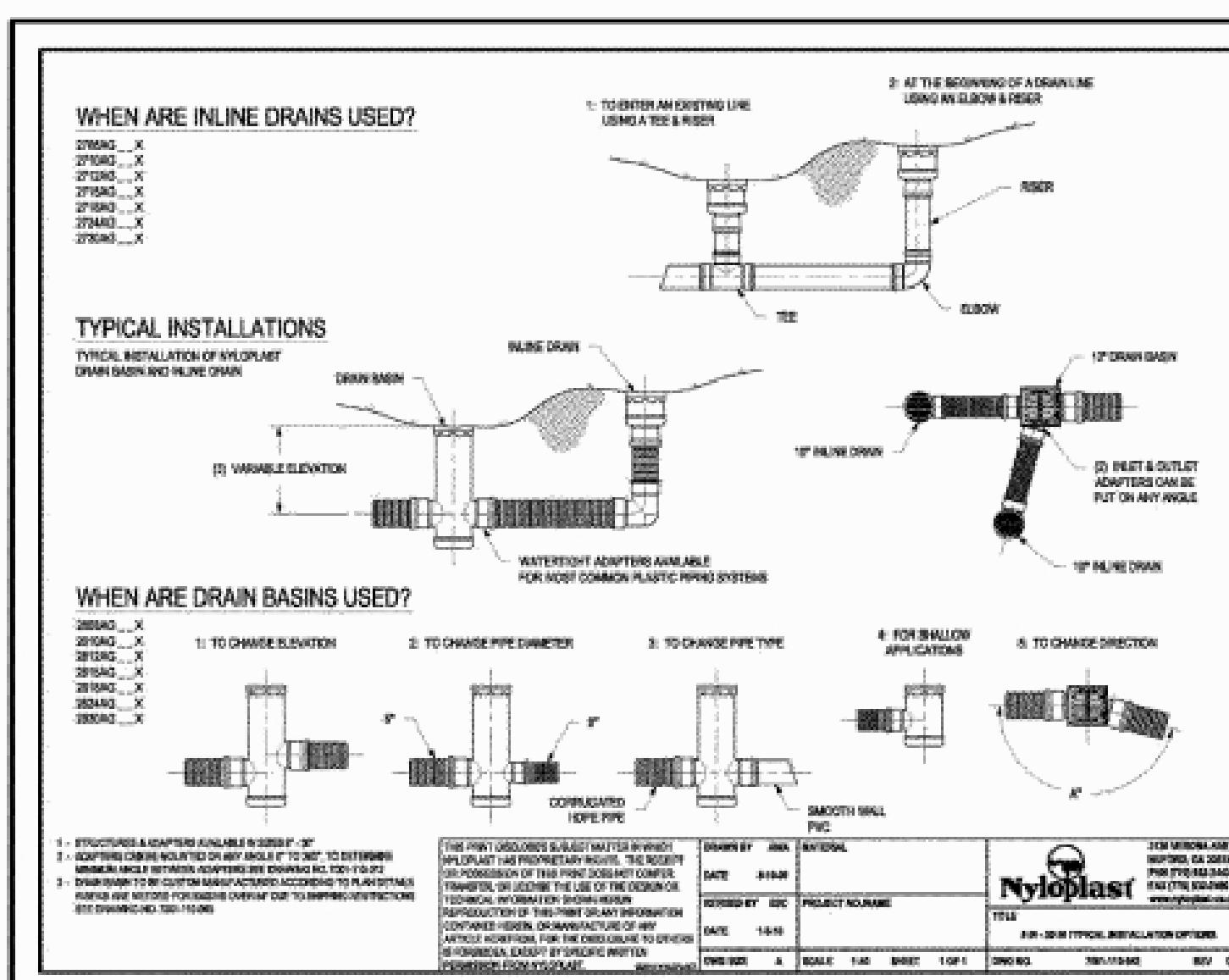
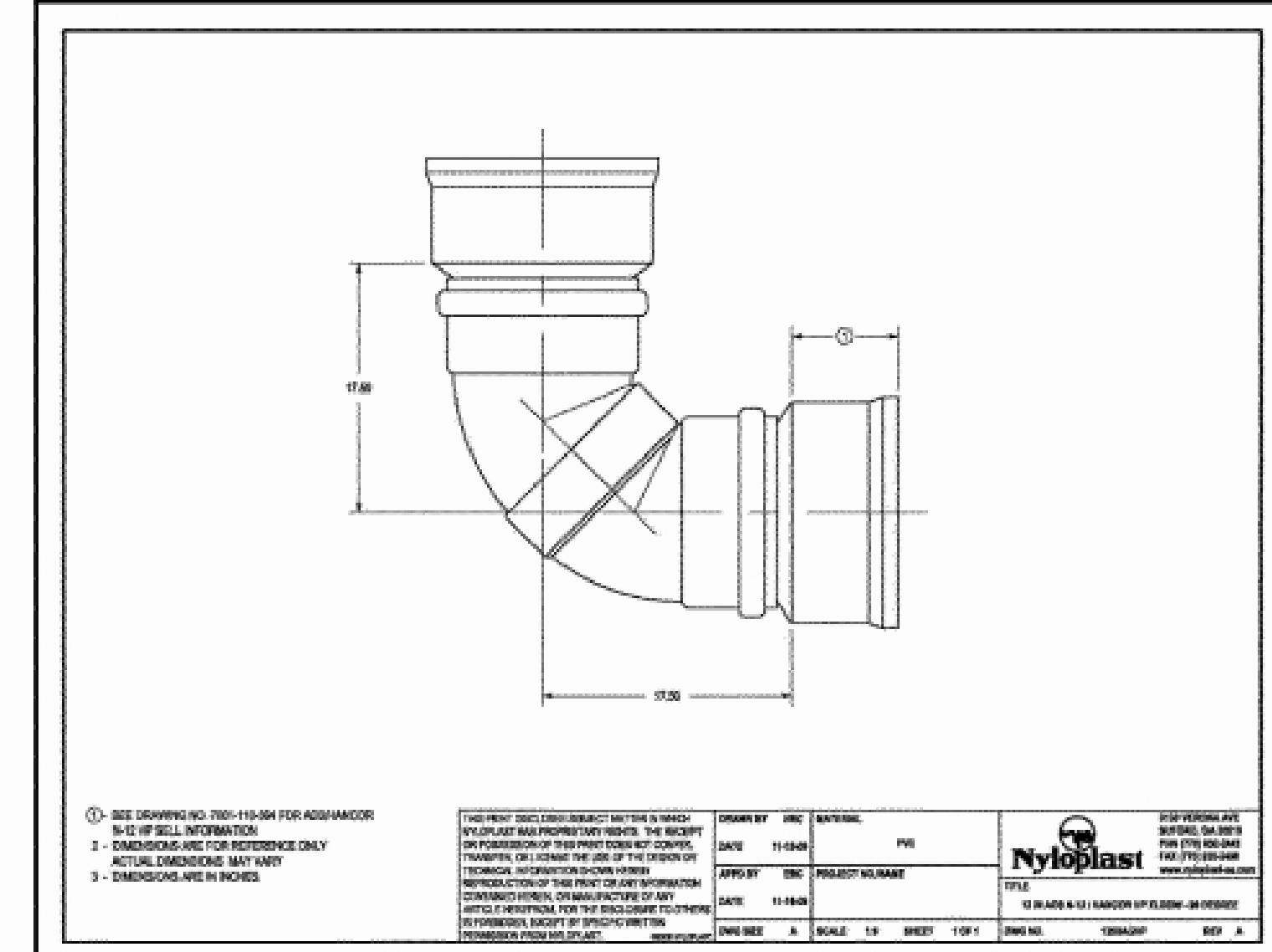
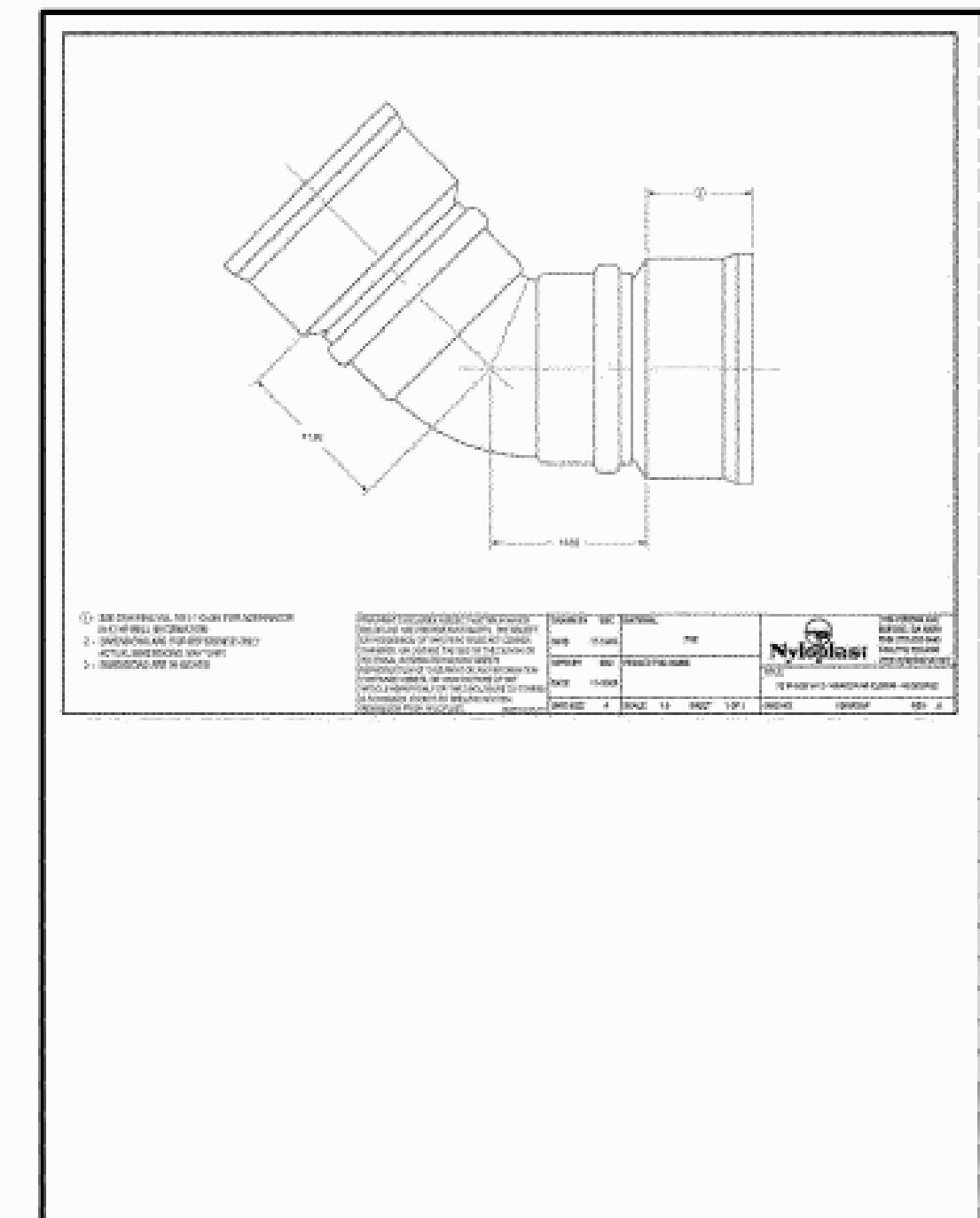
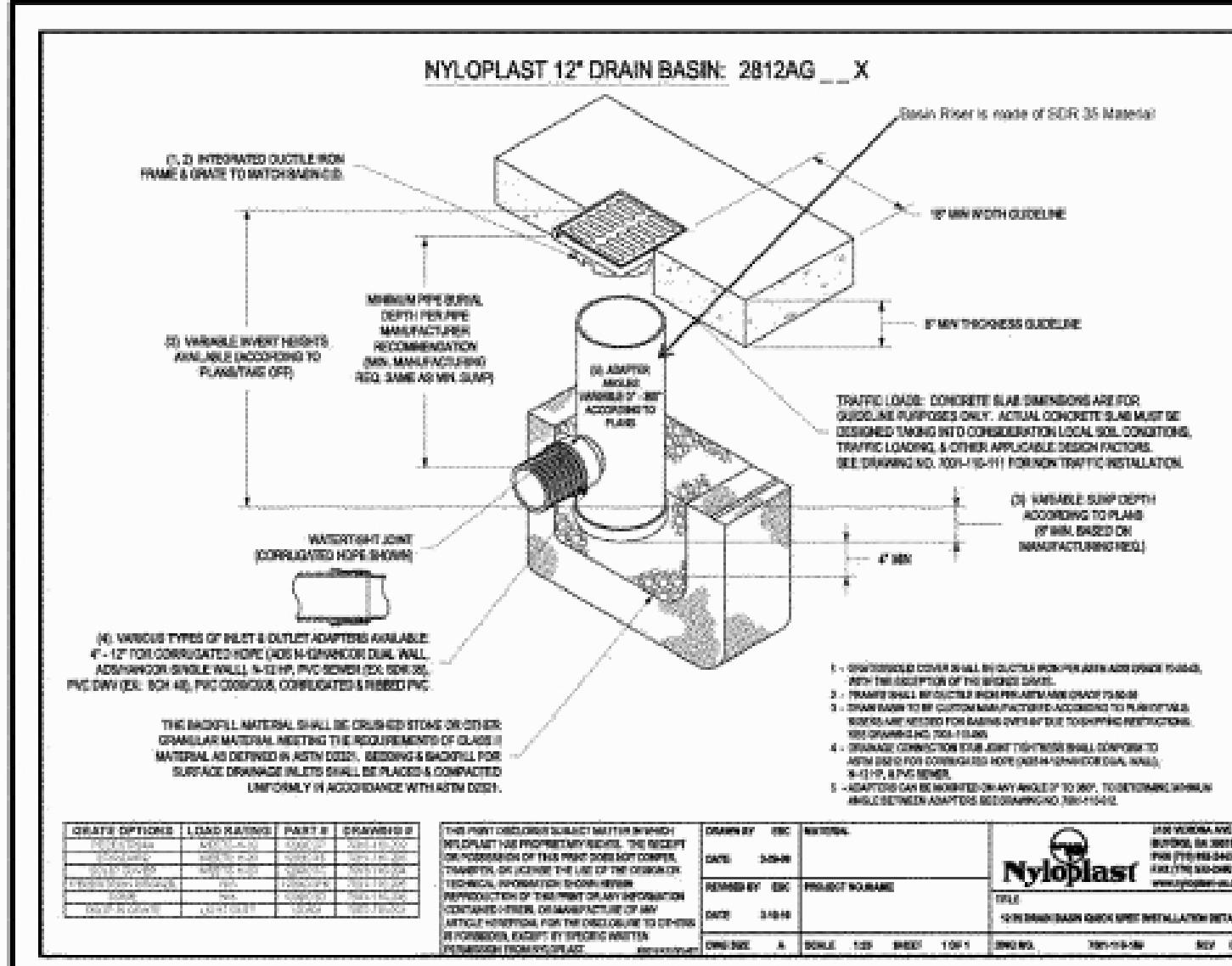
DATE: AUGUST 01, 2016 ORB # 15-218



GRAPHIC SCALE  
50 25 0 25 50  
SCALE: 1"=50'

ONSITE STORM DRAIN PIPE INFORMATION	DRAWN BY WCWJ
	DATE 8-30-16
	21601-LAYOUT-1-07-16
	SHEET #
	CIVILO00C3
	JOB # 21601

Rio Grande  
Engineering  
1606 CENTRAL AVENUE  
SUITE 201  
ALBUQUERQUE, NM 87106  
(505) 872-0999



DRAWN BY WCWJ  
DATE 1-23-16  
SHEET # C3  
JOB # 21-LAYOUT-1-07-16  
DRAWN BY WCWJ  
DATE 1-23-16  
SHEET # C3  
JOB # 21-LAYOUT-1-07-16  
7/28/16  
DAVID SOUZE  
P.E. #14522