CITY OF ALBUQUERQUE



Richard J. Berry, Mayor

March 30, 2017

Fred C. Arfman, P.E. Isaacson & Arfman, P.A. 128 Monroe St. N.E Albuquerque, NM, 87108

RE: Alameda Self Storage - Oakland Storm Drain Improvements

Grading Plan

Stamp Date: 3/2/17

Hydrology File: C18D064A

Dear Mr. Arfman:

PO Box 1293 Based upon the information provided in your submittal received 3/6/2017, the Grading

Plan and Drainage Report (Supplemental Information Onsite Pond Revisions) is approved

for Grading Permit and Paving Permit.

Renee C. Brissell

Albuquerque If you have any questions, please contact me at 924-3995 or rbrissette@cabq.gov.

Sincerely,

New Mexico 87103

www.cabq.gov Reneé C. Brissette, P.E.

Senior Engineer, Hydrology

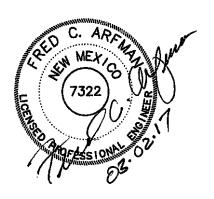
Planning Department

SUPPLEMENTAL INFORMATION

FOR

ALAMEDA SELF STORAGE BUILDING ADDITIONS

6800 Oakland Ave. NE Albuquerque, NM



PROJECT NO. 2204

BY

ISAACSON & ARFMAN, P.A.
Consulting Engineering Associates

Thomas O. Isaacson, PE(RET.) & LS(RET.) Fred C. Arfman, PE Åsa Nilsson-Weber, PE

INTRODUCTION

The Alameda Self-Storage facility was developed in 2006 with an interim drainage solution consisting of a private on-site stormwater retention facility along the west property line. The holding of developed storm waters was required due to limited downstream capacity in the rural type public roadways adjacent to the site and the absence of a storm drain extension from the public system(s) to the west.

The purpose of this report is to support the elimination of the existing on-site detention pond based on the upcoming storm drain system in Oakland Ave.

I. EXISTING CONDITIONS

The approved Grading and Drainage Plan (C18/D64A –included for information) for the Alameda Self Storage facility (Property) prepared by this office (I&A Project Number 1418 dated May 2005) consisted of a full build plan and an interim condition plan which required onsite retention ponding until proposed off-site public storm drain infrastructure was available to the site.

II. PROPOSED CONDITIONS

Per the approved 2005 plans and supplemental information, once the Oakland Avenue / Alameda Blvd. storm drain systems are installed, the interim retention pond will no longer be required.

South Basin: The recent (2015) construction of the Alameda Blvd. storm drain and paving improvements included public storm drain with a stub provided to this property. The south First Flush / detention pond was constructed in 2015/16 to release to Alameda Blvd. at the allowable rate of 5.84 cfs.

North Basin: The 1.8 acre North Basin will generate 8.5 cfs. Per the Master Plan, the allowable discharge rate, based on a land treatment ratio of A:0 B:16 C:34 D:50 is 7.0 cfs.

The area outside the perimeter walls will continue to free discharge 0.5 cfs to Oakland Ave. 1.6 acres inside the perimeter walls will drain 8.0 cfs to the proposed detention pond which will provide orifice control to reduce the discharge to 6.5 cfs to the Oakland Ave. storm drain.

Total discharge to Oakland Ave. = 0.5 cfs (exterior basin) + 6.5 (from NW pond) = 7.0 cfs. OK

Total detention will be 8.0 cfs (portion of north basin within perimeter walls) -6.5 cfs (discharge from pond to Oakland storm drain stub) = 1.5 cfs.

III. FIRST FLUSH REQUIREMENTS

Effective May of 2014, the City of Albuquerque Drainage Ordinance requires that all new development projects, where practicable, shall manage the First Flush defined as the storm water runoff during the early stages of a storm equal to or less than runoff from a 90th Percentile Storm Event (=0.34"/sf impervious area after initial abstraction).

The south pond, constructed in 2015 provides first flush retention volume of 1,800 cf.

The north pond which will be constructed by this project, has an area of 900 sf. At a depth of 1.5', the available retention volume = 900 sf x 1.5 ft = 1,350 cf. Total First Flush retention = 3.150 cf.

Based on Draina			CAL	CULATIONS: 1	NORT	H BASIN		
	age De	sign Criteria fo	r City of	Albuquerque Section		DPM, Vol 2,	dated Jar	1., 1993
AREA OF SITE	g.			ON-SIT 77220	E SF	=	1.8	
AREA OF SITE	۵.			100-year, 6-hour	эг	_	1.0	
ALLOWABLE	E DISC	CHARGE:		DEVELOPED FL	OWS:			EXCESS PRECIP:
		Treatment SF	F %			Treatment SI	F %	Precip. Zone 3
Area A	=	0	0%	Area A	=	0	0%	$E_{A} = 0.66$
Area B	=	26254.8	34%	Area B	=	3861	5%	$E_{\rm B} = 0.92$
Area C	=	12355.2	16%	Area C	=	3861	5%	$E_{\rm C} = 1.29$
Area D	=	38610	50%	Area D	=	69498	90%	$E_{\rm D} = 2.36$
Total Area	=	77220	100%	Total Area	=	77220	100%	•
On-Site Weighte	ed Exce	ess Precipitatio	n (100-Ye	ear, 6-Hour Storm)				The allowable discharge
C		Weighted E =		$E_A A_A + E_B A_B + E_C$		$E_{\mathrm{D}}\mathrm{A}_{\mathrm{D}}$		to the public storm dra
			_	$A_A + A_B + A$	$A_{\rm C} + A_{\rm D}$			in Oakland is $= 7.0 \text{ cfs}$
Historic E	=	1.7	0 in. I	Developed E	=		3 in.	The exterior of the
On-Site Volume	of Rur	noff: V360 =	I	E*A / 12				property (N2) discharg
Historic V ₃₆₀	=	1093	4 CF I	Developed V ₃₆₀	=	1437	9 CF	0.5 cfs. The interior (N
								will control release to
On-Site Peak D	ischarg	ge Rate: Qp =	$Q_{pA}A_A+Q$	$Q_{pB}A_B+Q_{pC}A_C+Q_{pI}$	$_{\rm D}A_{\rm D}/43$	3,560		7.0 - 0.5 = 6.5 cfs.
For Precipitation	7one	3						
or recipitation	i Lone							
Q _{pA}	=	1.87		Q_{pC}	=	3.45		1.6 cfs will be detained
•	=			$\begin{array}{c} Q_{pC} \\ Q_{pD} \end{array}$		3.45 5.02		1.6 cfs will be detained See Hydrograph next
Q_{pA}	=	1.87 2.60	0 CFS I			5.02	5 CFS	See Hydrograph next
$egin{aligned} Q_{pA} \ Q_{pB} \end{aligned}$	= =	1.87 2.60	0 CFS I	Q_{pD}	=	5.02	5 CFS	
$egin{aligned} Q_{pA} \ Q_{pB} \end{aligned}$	= =	1.87 2.60	0 CFS I	Q_{pD}	=	5.02	5 CFS	See Hydrograph next
Q_{pA} Q_{pB} Historic Q_p	= =	1.87 2.60	0 CFS I	Q_{pD}	=	5.02		See Hydrograph next
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716 CF

cfs

0.54

Sub-basin Weighted Excess Precipitation (see formula above)

A =

 $\mathbf{B} =$

C =

D =

LAND TREATMENT

0%

50%

50%

0%

0.2 Ac.

7772

Weighted E =

 V_{360}

 Q_{P}

SF

Sub-basin Volume of Runoff (see formula above)

Sub-basin Peak Discharge Rate: (see formula above)

The following calculations are based on Treatment areas as shown in table to the right

Area of basin flows =

CALCULATIONS: 0:0

HYDROGRAPH FOR SMALL WATERSHED DPM SECTION 22-2 * PAGE A-13/14

Base time, t_B, for a small watershed hydrograph is,

$$tB = (2.107 * E * A / Q_P) - (0.25 * A_D / A)$$

Where

Е	=	2.36	inches
A	=	1.61	acres
A_{D}	=	1.61	acres
Q_{P}	=	8.1	cfs

$$t_{\rm B} = 0.74 \ hours$$

E is the excess precipitation in inches (from DPM TABLE A-8), Q_P is the peak flow, A_D is the area (acres) of treatment D, and A_T is the total area in acres. Using the time of concentration, t_C (hours), the time to peak in hours is:

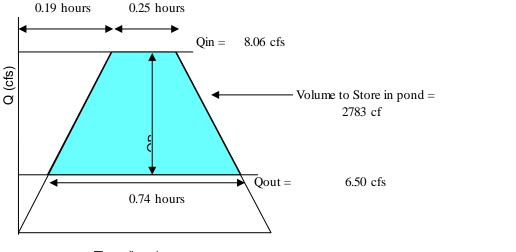
$$t_P = (0.7 * tC) + ((1.6 - (A_D / A)) / 12)$$

Where

$$t_C = 0.20 \text{ hours}$$

$$t_P = 0.19 \text{ hours}$$

Continue the peak for $0.25 * A_D / A_T$ hours. When A_D is zero, the hydrograph will be triangular. When A_D is not zero, the hyrograph will be trapezoidal. see the graph below:



Time (hour)

ORIFICE EQUATION - 13" ORIFICE IN POND WALL TO STORM DRAIN

The Orifice Equation is used to calculate the Flow at the opening of a Channel

$$Q = C*A * (2*g*h) ^0.5$$

Where 6.46 cfs Q = C = 0.6 (indicating that the opening will function at 60% capacity) A 0.85 sq.ft. = 32.2 ft/sec^{2} g = ft h 2.48 depth of flow at opening from the center of culvert =

18" outlet pipe

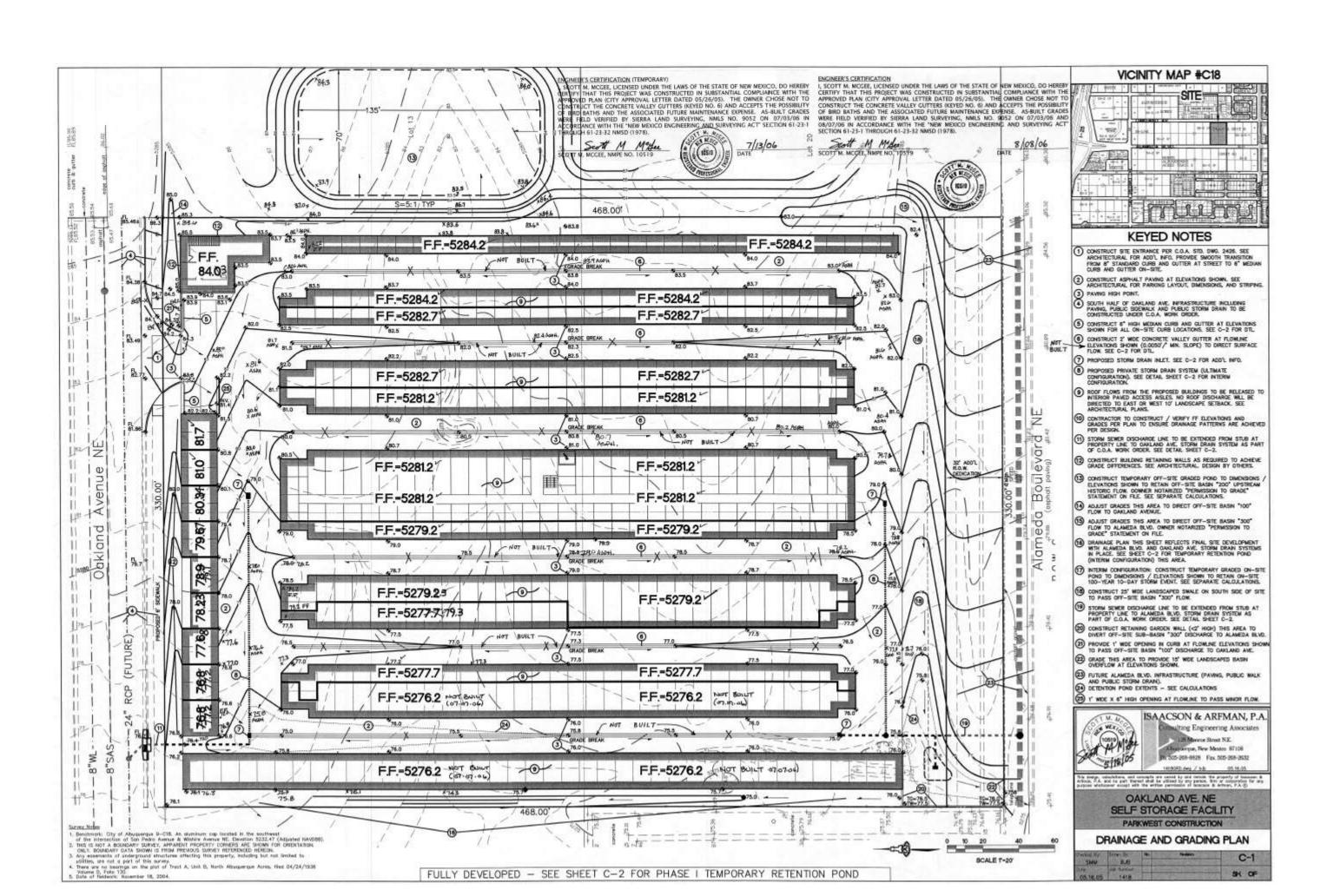
12.5" diameter hole cut orifice plate over outlet pipe

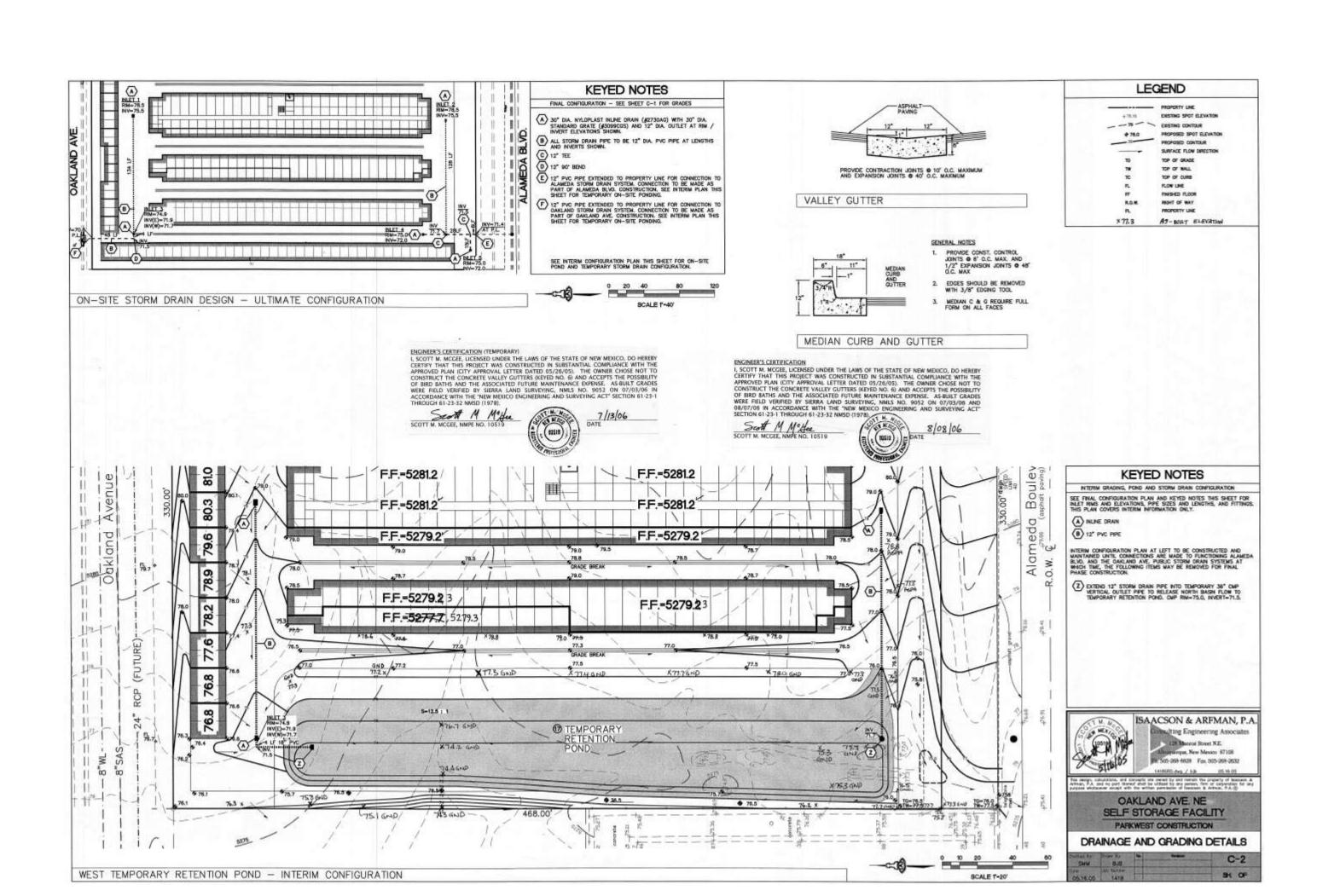
Invert of orifice opening = 73.0

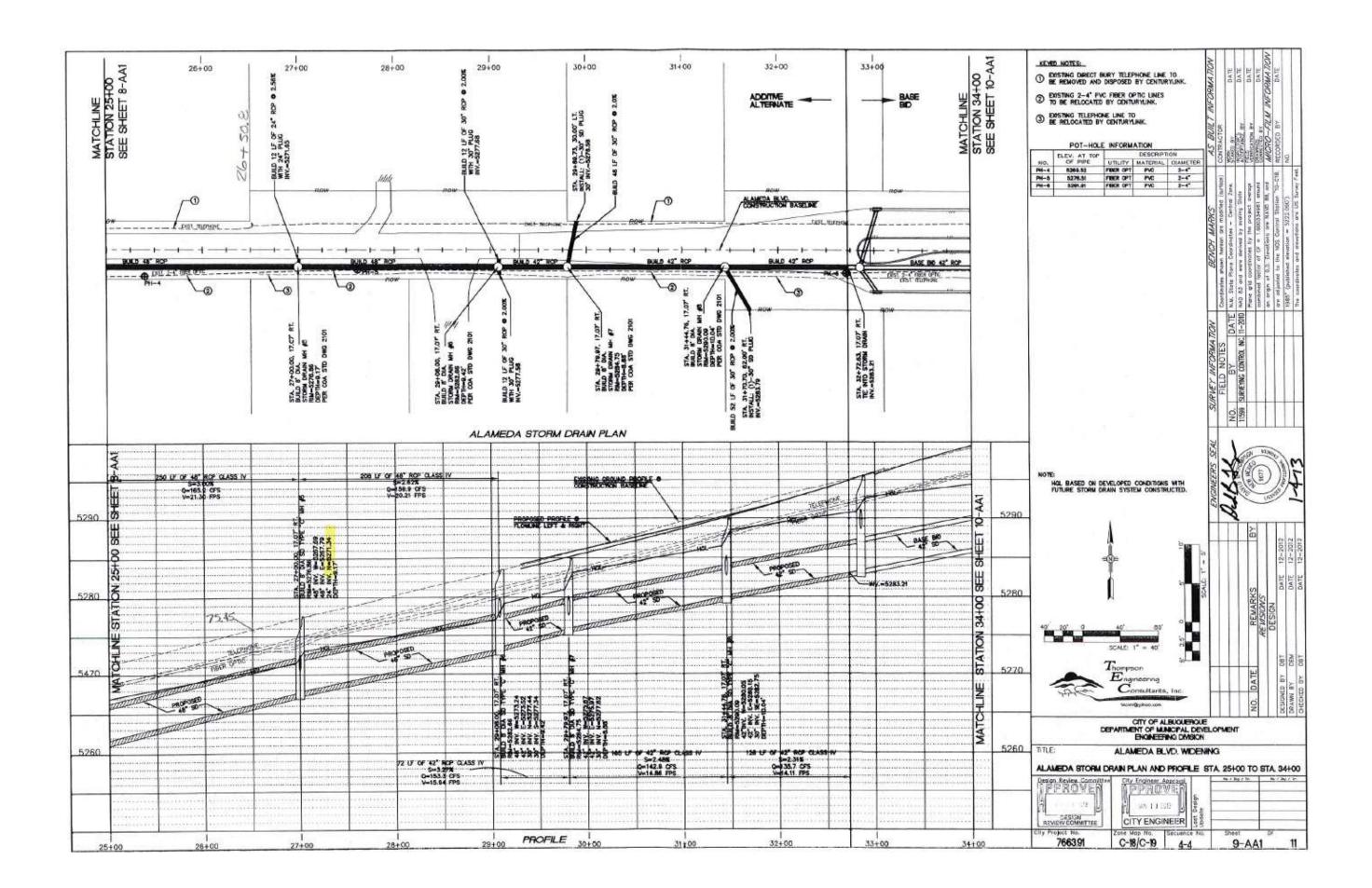
Water Surface at emergency overflow = 76.0

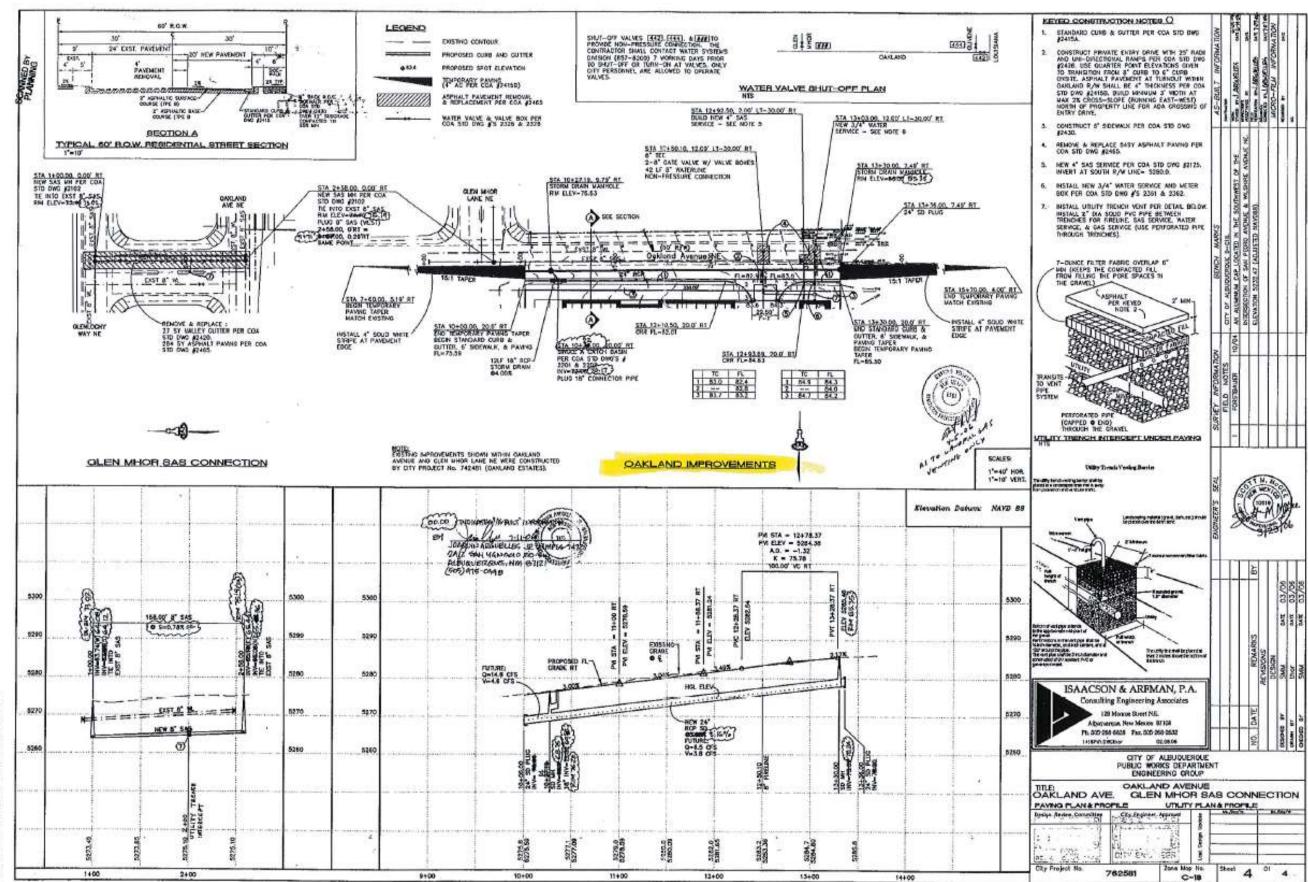
Center of orifice = 73.52

At a head of 2.48' (76.0 - 73.52) a 12.5" dia. opening will pass 6.46 cfs. < 6.5 cfs

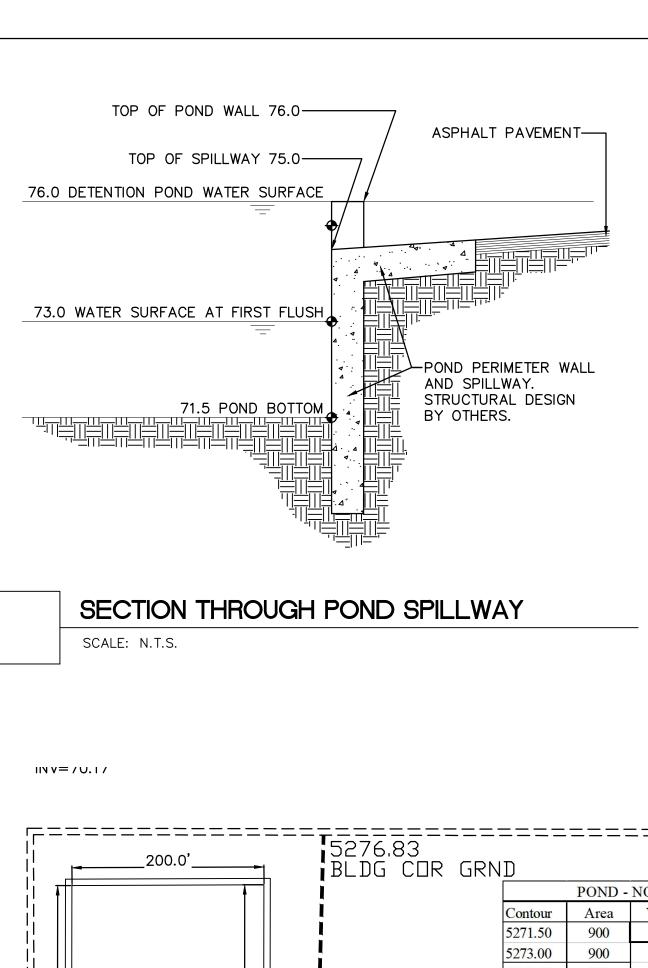


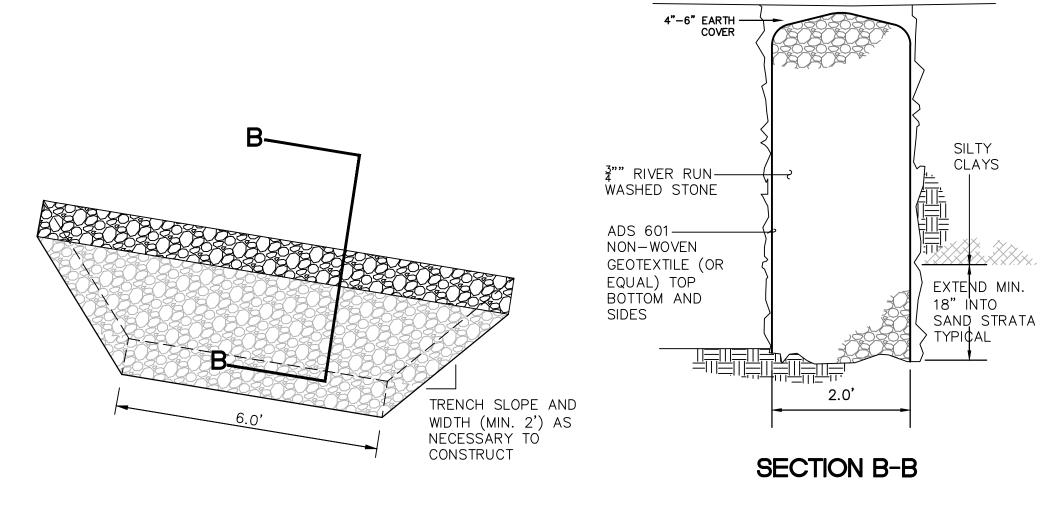






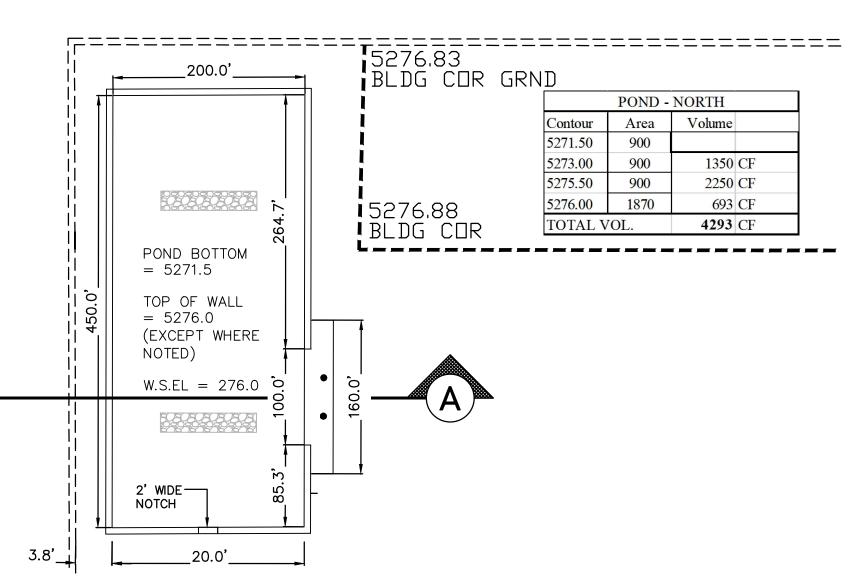
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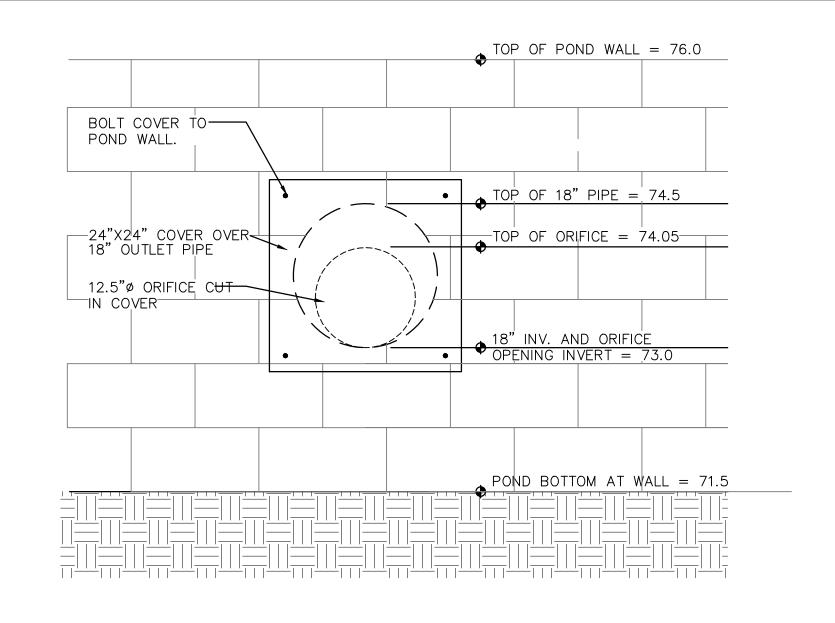




PERCOLATION TRENCH

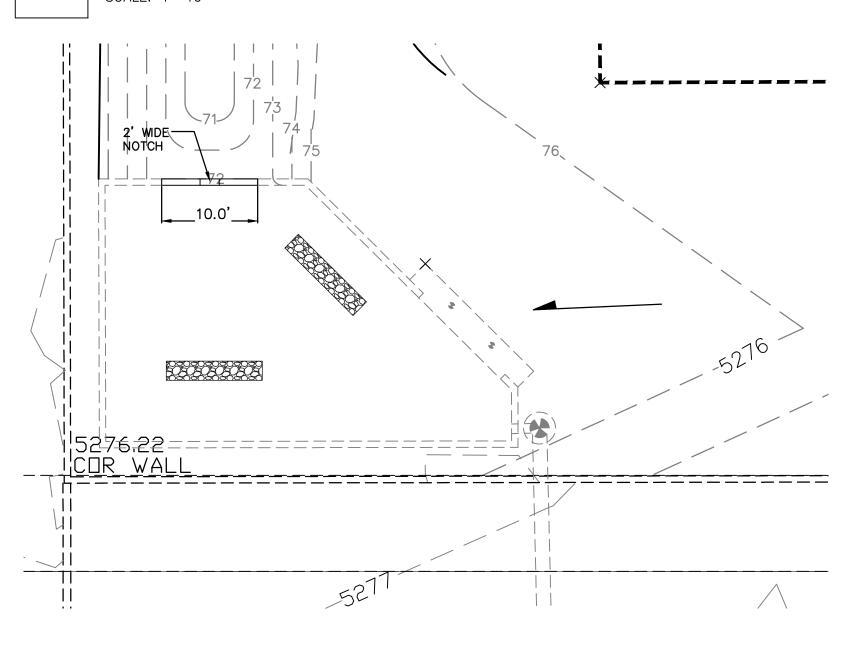
SCALE: N.T.S.





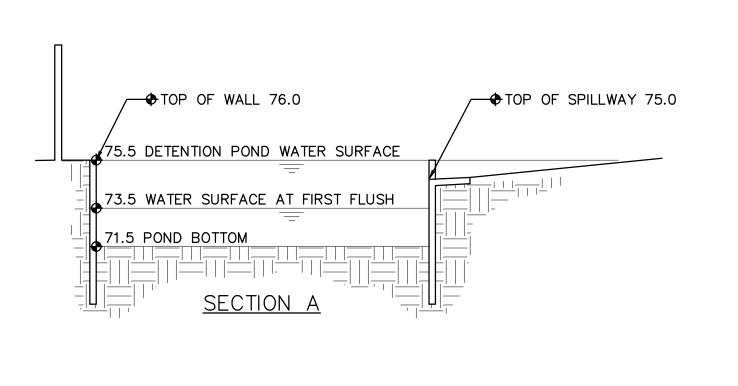
NORTH POND WALL DIMENSIONS

SCALE: 1"=10'





SCALE: 1"=10'



SOUTH POND WALL DIMENSIONS

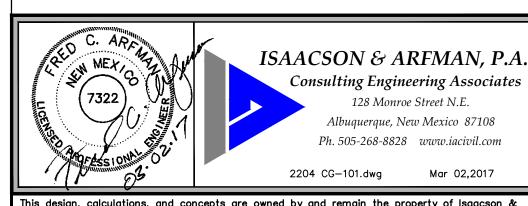
SCALE: 1"=10"

SECTION A: THROUGH NORTH POND

SCALE: 1"=10'

STORM DRAIN NOTES

- INSTALL ALL STORM DRAIN PIPE PER ADS MANUFACTURER'S SPECIFICATIONS.
- ON-SITE PIPE SHALL BE ADS N-12 (WATERTIGHT) OR ENGINEER APPROVED EQUIVALENT. PIPE SHALL BE INSTALLED PER MANUFACTURER'S RECOMMENDATIONS. CONNECTION TO OAKLAND STUB (RCP) TO BE WATERTIGHT USING ADS FITTINGS AS REQUIRED.
- STORM DRAINS SHALL BE INSTALLED AT INVERTS AND SLOPES SPECIFIED ON THE PLANS. THE PIPE SHALL DRAIN AT A CONSTANT SLOPE BETWEEN FITTINGS AND MANHOLES. THE PIPE SHALL DRAIN TOWARD THE OUTLET AT ALL LOCATIONS.
- STORM DRAIN SYSTEM WILL REQUIRE REGULAR MAINTENANCE TO ENSURE PROPER FUNCTIONING DURING STORM EVENTS. ENGINEER RECOMMENDS THAT PROPERTY OWNER PUT IN PLACE INSPECTION AND MAINTENANCE CRITERIA SCHEDULED TO OCCUR MONTHLY AND AFTER EACH STORM EVENT.
- VIBRATORY COMPACTION SHALL NOT BE USED OVER IN-PLACE UTILITIES.
- ALL BACKFILL SHALL BE COMPACTED TO A MINIMUM 95% DENSITY PER ASTM D-1557.



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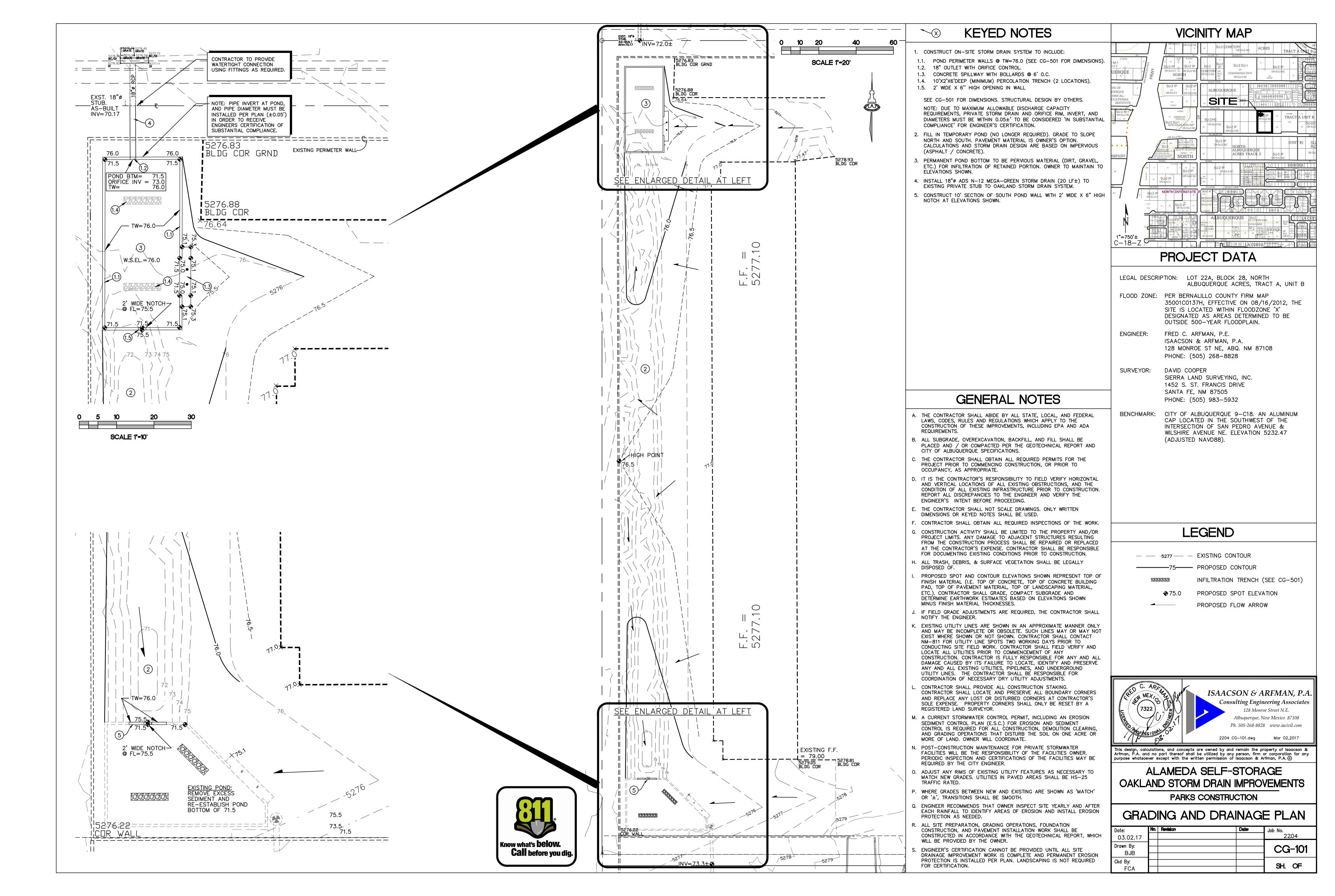
ALAMEDA SELF-STORAGE OAKLAND STORM DRAIN IMPROVEMENTS

PARKS CONSTRUCTION

GRADING AND DRAINAGE DETAILS

Date:	No.	Revision:	Date:	Job No.
03.02.17				22.04
Drawn By: BJB				GG-50
	+			
Ckd By: FCA				- SH. OF





M:PROJECTS/2200-2299/2204[DWG\2204 CG-10].dwg, 3/2/2017 8:58:15 AM, BJB, BJB