

CITY OF ALBUQUERQUE



Richard J. Berry, Mayor

May 24, 2017

Diane Hoelzer, P.E.
Mark Goodwin & Associates
PO Box 90606
Albuquerque, NM, 87199

**RE: Oakland Ridge Subdivision
Grading Plan and Drainage Report
Stamp Date: 5/19/17
Hydrology File: C18D085**

Dear Ms. Hoelzer:

Based upon the information provided in your submittal received 5/19/2017, the Grading Plan and Drainage Report is **not** approved for Preliminary Plat action by the DRB. The following comments need to be addressed for approval of the above referenced project:

PO Box 1293

Albuquerque

1. More than 1 acre of disturbance is proposed, therefore an Erosion and Sediment Control Plan is required and is to be submitted to the storm water quality engineer (Curtis Cherne, PE, ccherne@cabq.gov). An approval for this must be given prior to Hydrology's approval for Grading Permit.

Drainage Repot:

New Mexico 87103

www.cabq.gov

1. Under Design Criteria and Previous Reports, please add that the NAA MDP design analysis was modified by the Eagle Rock Drainage Plan. A storm pipe and Manhole on Oakland Ave. was installed with the construction of Oakland Estates. This pipe was designed to capture the drainage of the east portion of Basin 117.2 and discharges into a storm sewer system on Eagle Rock Ave.
2. Please note that the proposed 30-in storm pipe on Oakland Ave. which will tie into the above mentioned existing manhole and storm sewer is currently at best only about 20% constructed. This has a completion date in August and accepted by the City two or three months after the completion date. Depending on the quickness of this project, a temporary retention pond may be needed until the storm sewer system is accepted by the City.
3. Under Developed Drainage Conditions, it states that the existing storm drain in Oakland Avenue with inlets will intercept the North basin's flow. As stated above, the existing storm sewer system on Oakland is currently not accepting drainage from Basin 117.2. Once the system is accepted, it will be open to the drainage.

CITY OF ALBUQUERQUE



Richard J. Berry, Mayor

Please provide the inlet capacity calculations on the existing inlet constructed by the adjacent development downstream to demonstrate that there will be downstream capacity once the Oakland storm sewer is accepted by the City.

4. Under Developed Drainage Conditions, it states that South basin will discharge 7.05 cfs which will be conveyed through a proposed storm pipe to an inlet on Alameda. However, according to the Drainage Letter Report for Alameda Boulevard San Pedro to Wyoming Project dated January 2012 by Thompson Engineering Consultants, the storm system on Alameda was designed to take 3.82 cfs/acre from Basin 117.3. For this project, The area which is part of Basin 117.3 is the two southern existing lots. The combined area of these two lots is 1.61 acres and therefore the allowable maximum discharge is 6.16 cfs. See attached report and basin exhibit. Please change the North and South drainage basis, so that the South basin will only discharge 6.16 cfs or less.

5. Please update Figure 4 as outlined above. Also please state the acreage of the North basin and the South basin.

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New Mexico 87103

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6. Please update Figure 5. This should reflect the new basins, so Lot 6 & 7 information should be moved from the South basin to the North basin. Also Lot 18 & 19 information should be moved from the South basin to the North basin.

7. Please provide inlet capacity and weir calculations for the proposed Type A inlet.

8. Please provide the calculation for the 100 year HGL through the proposed 24" storm pipe from the existing inlet to the proposed Type A inlet.

9. Please provide an exhibit showing the profile of the proposed 24" storm pipe from the existing inlet to the proposed Type A inlet. Please include the HGL.

Grading Plan:

1. Please provide the street slopes.
2. The retaining wall along the East property line appears to have a constructability problem with undermining the existing sidewalk. Please provide a cross section.
3. Please add the site floodplain information.
4. On the Typical Depressed Area Detail, Notes #4 & 5 are missing. Please correct the Detail.

CITY OF ALBUQUERQUE



Richard J. Berry, Mayor

5. On the Typical Front Yard First Flush Detail, Please show the property line that goes through the middle of the majority of the ponds. Also cross section would greatly improve the readability and show that the first flush volume is only within the 6-inch depth. Also this pond should have gravel mulch within the first flush volume.
6. Please clarify the Typical Lot Grading Scheme. It appears that the back lot drainage will just travel either to the north or south depending on the grading without being directed to the first flush ponds.
7. It appears that the first flush ponds will not collect the majority of the lot runoff as designed. Please show that each first flush basin is designed for its drainage basin. Pond location or another layout may be necessary.
8. Please show better line weight between the existing sidewalks & ramps and the proposed sidewalks & ramps.
9. Please provide the Grate elevation for the Type A inlet.

PO Box 1293

10. At the Proposed Type A inlet, is the proposed sidewalk supposed to connect to the proposed sidewalk along Alameda Blvd? If so, then please remove the retaining wall at the connection.

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New Mexico 87103

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11. Please provide proposed grade points at the southwest corner (on the proposed sidewalk), at the Type A inlet (on the proposed sidewalk), at the northeast corner (on the proposed sidewalk), at the end of the wall on Lot 1, and at the end of the curved wall on Lot 13 (on the proposed sidewalk).

12. Along the northern half of the existing retaining wall along the western property line, starting at Lot 6 the proposed grades are higher than the top of the existing retaining wall. There are considerable constructability issues here. Please clarify and provide a cross section of the existing retaining wall.

If you have any questions, please contact me at 924-3995 or rbrissette@cabq.gov.

Sincerely,

Renee C. Brissette

Reneé C. Brissette, P.E.
Senior Engineer, Hydrology
Planning Department



City of Albuquerque

Planning Department

Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 09/2015)

Project Title:	Building Permit #:	City Drainage #:
DRB#:	EPC#:	Work Order#:
Legal Description:		
City Address:		
Engineering Firm:	Contact:	
Address:		
Phone#:	Fax#:	E-mail:
Owner:	Contact:	
Address:		
Phone#:	Fax#:	E-mail:
Architect:	Contact:	
Address:		
Phone#:	Fax#:	E-mail:
Other Contact:	Contact:	
Address:		
Phone#:	Fax#:	E-mail:

Check all that Apply:

DEPARTMENT:

- HYDROLOGY/ DRAINAGE
 TRAFFIC/ TRANSPORTATION
 MS4/ EROSION & SEDIMENT CONTROL

TYPE OF SUBMITTAL:

- ENGINEER/ ARCHITECT CERTIFICATION

 CONCEPTUAL G & D PLAN
 GRADING PLAN
 DRAINAGE MASTER PLAN
 DRAINAGE REPORT
 CLOMR/LOMR

 TRAFFIC CIRCULATION LAYOUT (TCL)
 TRAFFIC IMPACT STUDY (TIS)
 EROSION & SEDIMENT CONTROL PLAN (ESC)

OTHER (SPECIFY) _____

CHECK TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

- BUILDING PERMIT APPROVAL
 CERTIFICATE OF OCCUPANCY

 PRELIMINARY PLAT APPROVAL
 SITE PLAN FOR SUB'D APPROVAL
 SITE PLAN FOR BLDG. PERMIT APPROVAL
 FINAL PLAT APPROVAL
 SIA/ RELEASE OF FINANCIAL GUARANTEE
 FOUNDATION PERMIT APPROVAL
 GRADING PERMIT APPROVAL
 SO-19 APPROVAL
 PAVING PERMIT APPROVAL
 GRADING/ PAD CERTIFICATION
 WORK ORDER APPROVAL
 CLOMR/LOMR

 PRE-DESIGN MEETING
 OTHER (SPECIFY) _____

IS THIS A RESUBMITTAL?: Yes No

DATE SUBMITTED: _____ By: _____

COA STAFF: _____ ELECTRONIC SUBMITTAL RECEIVED: _____

Oakland Ridge Subdivision

Drainage Management Plan

Prepared by
Mark Goodwin & Associates, P.A.

May 2017





City of Albuquerque

Planning Department
Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 09/2015)

Project Title:	Oakland Ridge Subdivision	Building Permit #:	City Drainage #:
DRB#:	1010793	EPC#:	Work Order#:
Legal Description: Lots 15, 16, 17, 18, Block 28, Tract A, Unit B, North Albuquerque Acres			
City Address: Oakland Ave and Olivine Ct.			
Engineering Firm:	Mark Goodwin & Associates, PA	Contact:	Diane Hoelzer, PE
Address:	PO BOX 90606, Albuquerque, NM 87199		
Phone#:	505-828-2200	Fax#:	E-mail: diane@goodwinengineers.com
Owner:	Brian Urlacher, a Single Man	Contact:	Bo Johnson, Bokay Construction
Address:	5160 San Francisco NE, Albuquerque, NM 87109		
Phone#:	505-450-4616	Fax#:	E-mail: bo@bokayconst.com
Architect:		Contact:	
Address:			
Phone#:		Fax#:	E-mail:
Other Contact:		Contact:	
Address:			
Phone#:		Fax#:	E-mail:

Check all that Apply:

DEPARTMENT:

- HYDROLOGY/ DRAINAGE
 TRAFFIC/ TRANSPORTATION
 MS4/ EROSION & SEDIMENT CONTROL

TYPE OF SUBMITTAL:

- ENGINEER/ ARCHITECT CERTIFICATION

 CONCEPTUAL G & D PLAN
 GRADING PLAN
 DRAINAGE MASTER PLAN
 DRAINAGE REPORT
 CLOMR/LOMR

 TRAFFIC CIRCULATION LAYOUT (TCL)
 TRAFFIC IMPACT STUDY (TIS)
 EROSION & SEDIMENT CONTROL PLAN (ESC)

 OTHER (SPECIFY) _____

CHECK TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

- BUILDING PERMIT APPROVAL
 CERTIFICATE OF OCCUPANCY

 PRELIMINARY PLAT APPROVAL
 SITE PLAN FOR SUB'D APPROVAL
 SITE PLAN FOR BLDG. PERMIT APPROVAL
 FINAL PLAT APPROVAL
 SIA/ RELEASE OF FINANCIAL GUARANTEE
 FOUNDATION PERMIT APPROVAL
 GRADING PERMIT APPROVAL
 SO-19 APPROVAL
 PAVING PERMIT APPROVAL
 GRADING/ PAD CERTIFICATION
 WORK ORDER APPROVAL
 CLOMR/LOMR

- PRE-DESIGN MEETING
 OTHER (SPECIFY) _____

IS THIS A RESUBMITTAL?: Yes No

DATE SUBMITTED: May 19, 2017 By: Diane Hoelzer, PE

COA STAFF: ELECTRONIC SUBMITTAL RECEIVED: _____

Oakland Ridge Subdivision

Table of Contents

- I. PROJECT DESCRIPTION
- II DESIGN CRITERIA AND PREVIOUS REPORTS
- III. EXISTING DRAINAGE CONDITIONS
- IV. DEVELOPED DRAINAGE CONDITIONS
- V. FIRST FLUSH PONDS

FIGURE 1 Vicinity Map

FIGURE 2 Aerial Google Earth Map

FIGURE 3 FIRM Panel 35001C0119G (September 26, 2008)

FIGURE 4 Sub Basin Boundary Exhibit

FIGURE 5 First Flush Ponds Calculations

FIGURE 6 Infrastructure List

Grading and Drainage Plan 11x17

Preliminary Plat 11x17

APPENDIX A

*First Flush Pond Calculations and Design
AHYMO Printouts*

POCKET 1 GRADING AND DRAINAGE PLAN
PRELIMINARY PLAT

I. PROJECT DESCRIPTION

The proposed Oakland Ridge Subdivision covers an area of approximately 2.83 acres. It is bounded by Oakland Ave. to the north, Louisiana Blvd. to the east, Alameda Blvd. to the south and a new subdivision currently under construction to the west. The subdivision will consist of 23 single family residential homes.

II. DESIGN CRITERIA AND PREVIOUS REPORTS

The design criteria used in this report was in accordance with Section 22.2 Hydrology of the Development Process Manual, Volume 2, Design Criteria, January 1993 edition. The 100-year 6-hour storm event was analyzed to determine flow to be conveyed within the roadways using $P(1\ hr)=2.10"$, $P(6\ hr)=2.50"$. The onsite Land Treatment values were determined based on Table A-5 Percent Treatment D for single family residential. First Flush volumes were calculated using 0.34 inches of precipitation over the new impervious areas (60%), which is the latest "design criteria" used by the City of Albuquerque.

There is an approved North Albuquerque Acres Master Drainage Plan (Dixon, 10-28-98). This project site lies within sub basins 117.2 and 117.3 in the NAA MDP report. Half of our site is allowed free discharge to the north in Oakland Avenue and half as allowable flows south to Alameda Blvd. In the NAA MDP report Land treatment values for future developed conditions were assumed to be Treatment A/B/C/D = 0/34/16/50. The 100 year discharge in this report used Treatment values of 0/20/20/60. A comparison was made between the allowable discharge based on the NAA MDP report and the actual discharge based on treatment values used in this project. The allowable discharge is 11.51 cfs as compared to the actual 12.21 cfs. There is a 0.7 cfs difference between these values, which for the 100 year storm event is considered an insignificant increase.

The project site is in FEMA flood zone X as shown on FIRM Panel 137 of 825, map number 35001C0137H, August 16, 2012 (Figure 3).

III. EXISTING DRAINAGE CONDITIONS

Under existing drainage conditions, onsite runoff is conveyed as overland surface flow in a westerly direction. There is a current development underway that is blocking the natural flow westward. They have constructed temporary ponds on this project site to prevent this site's runoff from flowing onto their property. Since this property is bounded by developed streets with curb and gutter on the other three sides, no offsite runoff enters this site.

IV. DEVELOPED DRAINAGE CONDITIONS

The total peak 100 year 6 hour discharge under developed conditions from this project site is 12.21 cfs. The North Sub basin will discharge 5.15 cfs into Oakland Avenue. There is an existing storm drain in Oakland Avenue with inlets that would intercept these flows. The South Sub basin will discharge 7.05 cfs into Alameda Avenue. There is an existing storm drain in Alameda with an existing inlet close enough to our project site, that an onsite inlet can connect to the existing inlet in Alameda Blvd. and convey the 7.05 cfs.

V. FIRST FLUSH PONDS

It is proposed to construct first flush ponds in the front yard areas and along the landscape strip between the curb and sidewalk as illustrated in Figure 4. These ponds should be constructed to be 6" deep (typical) with side slopes no greater than 3:1 (maximum). The grading plan shows the area required for each of the front yard ponds.

A summary of First Flush pond calculations and exhibit can be found in Figure 5 and 4, respectively. Additional first flush volume calculations can be found in Appendix A as well.

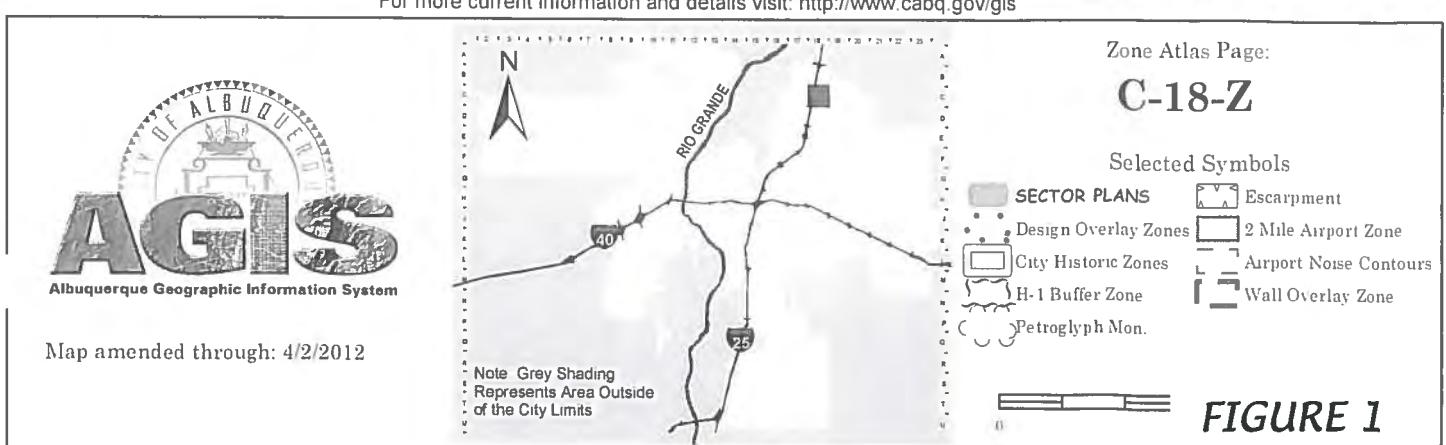
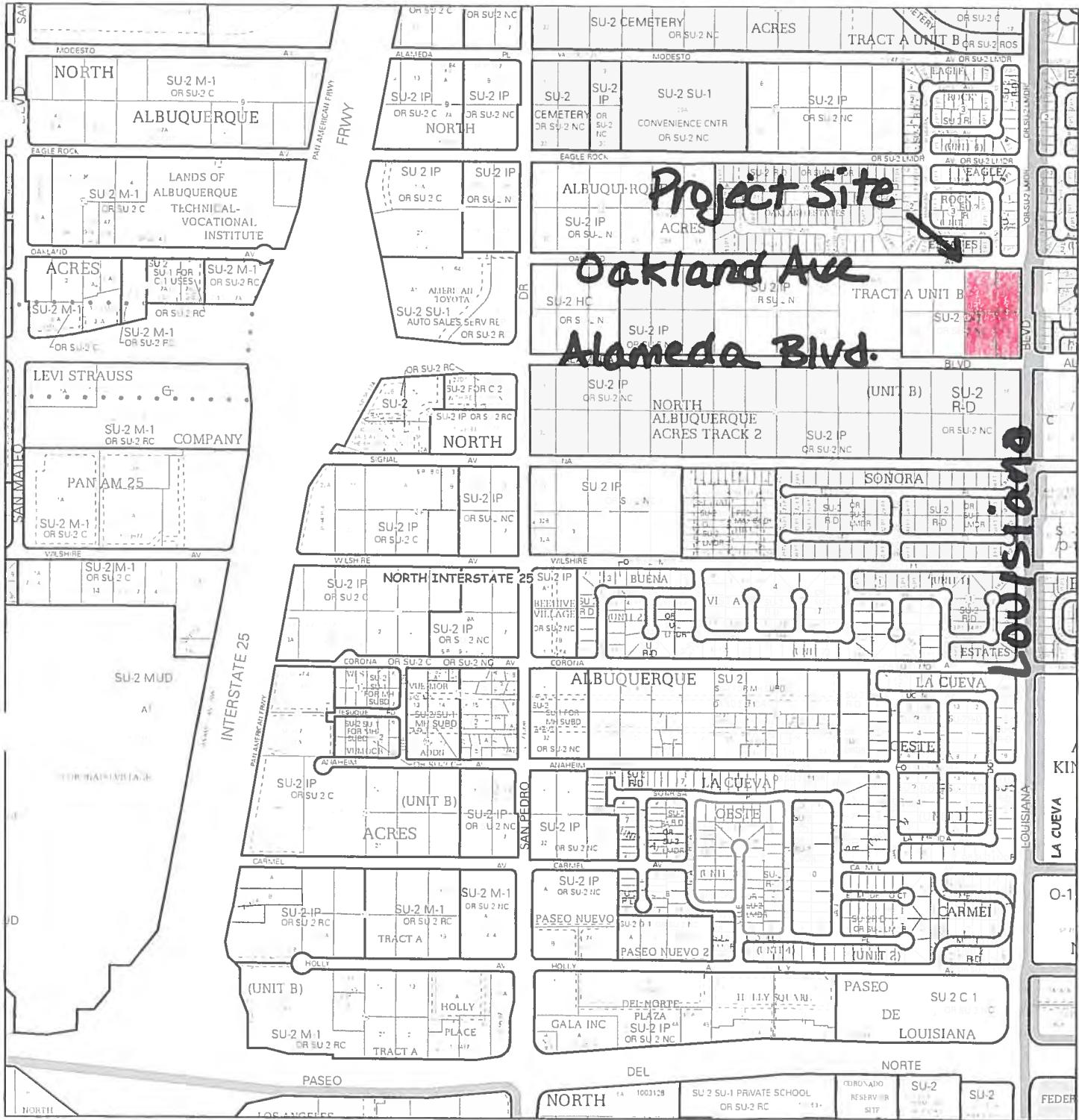
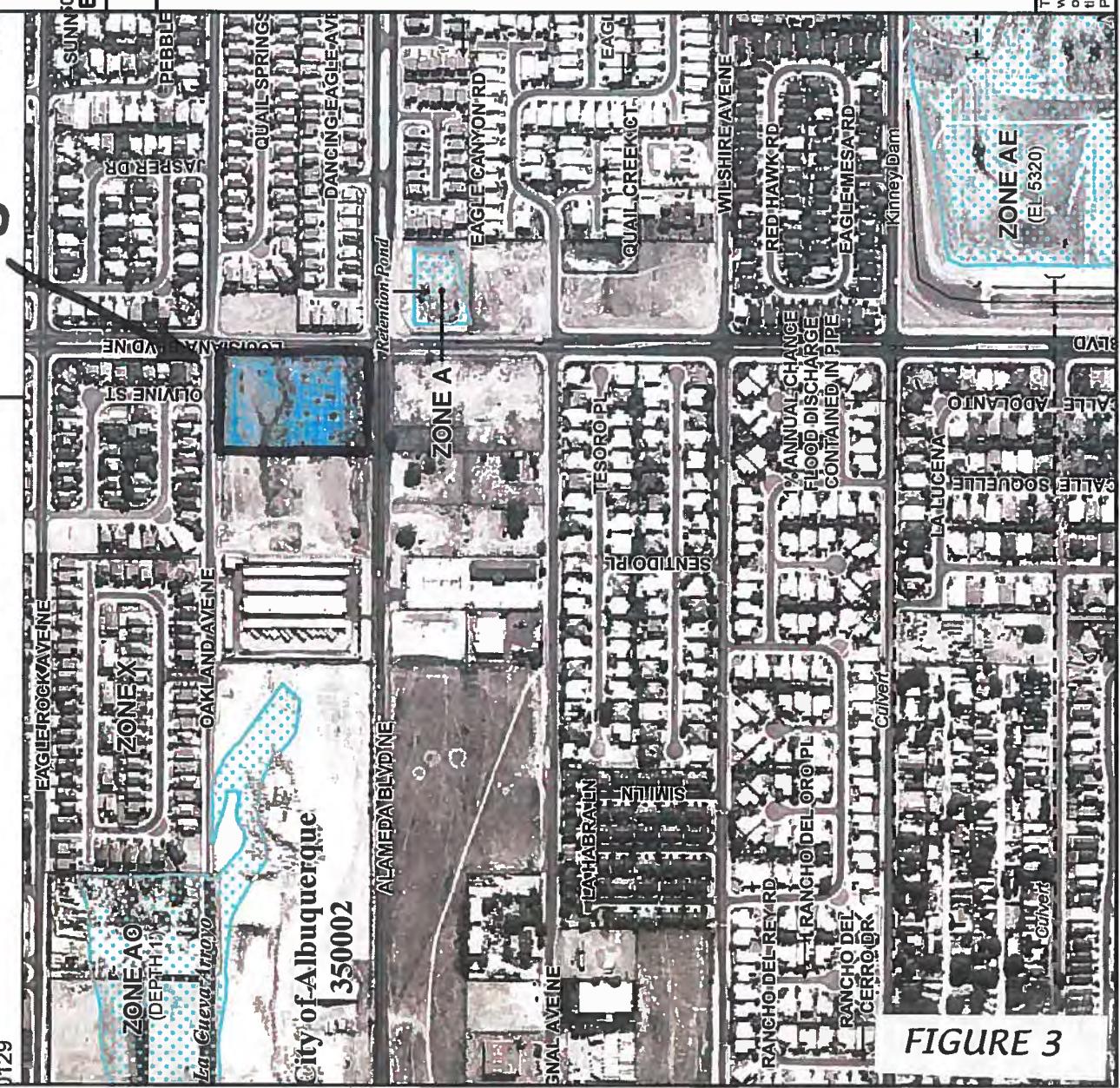




FIGURE 2

Project Site

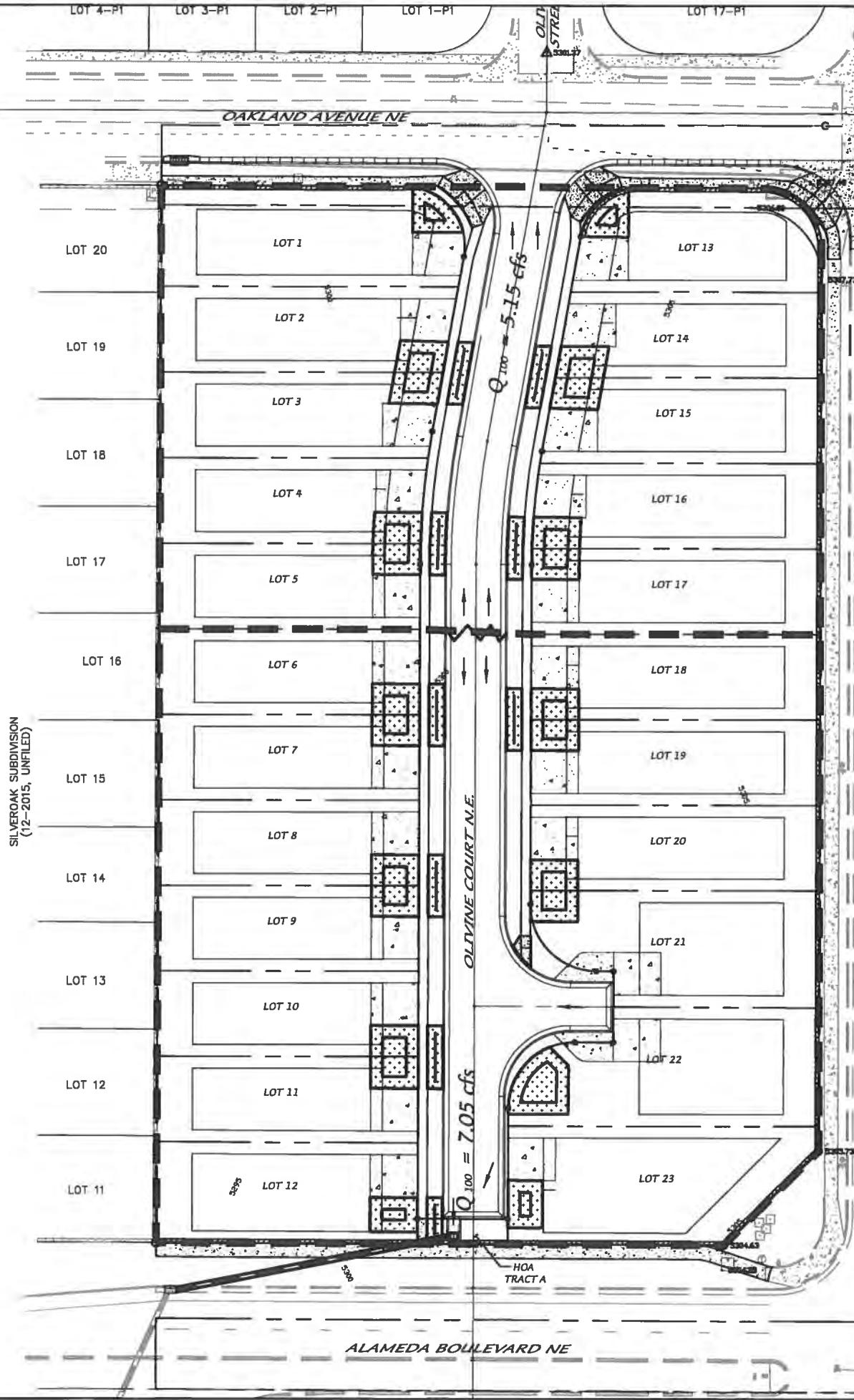
1545000 FT



This is an official copy of a portion of the above referenced flood map. It was extracted using F-MIR On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance Program flood maps, check the FEMA Flood Map Store at www.msfc.fema.gov.

FIGURE 4
OAKLAND RIDGE SUBDIVISION
SUB-BASIN BOUNDARY EXHIBIT

Louisiana Boulevard NE



OAKLAND RIDGE FIRST FLUSH POND CALCULATIONS					
NORTH BASIN			SOUTH BASIN		
LOCATION	Front Yard	Curbside	LOCATION	Front Yard	Curbside
	cu.ft.	cu.ft.		cu.ft.	cu.ft.
Lot 1	72.2				
Lot 2 & 3	166.0	30.5			
Lot 4 & 5	163.5	30.3			
			Lot 6 & 7	161.4	30.0
			Lot 8 & 9	161.4	30.0
			Lot 10 & 11	165.1	30.8
			Lot 12	74.9	20.1
Lot 13	74.5				
Lot 14 & 15	166.3	30.5			
Lot 16 & 17	162.6	30.3			
			Lot 18 & 19	161.4	30.0
			Lot 20 & 21	161.4	
			Lot 22	180.4	
			Lot 23	74.9	
	805.0	121.5		1140.9	140.9
Total provided		926.5			1281.7
Total required		885			1,211

FIGURE 5

Current DRC Project Number: _____ Date Submitted: _____ 5/19/17
 Date Site Plan Approved: _____ Date Preliminary Plat Approved: _____
 Date Preliminary Plat Expires: _____ DRB Project No.: _____ 1010793
 DRB Application No.: _____

FIGURE 12
INFRASTRUCTURE LIST

EXHIBIT "A"
TO SUBDIVISION IMPROVEMENTS AGREEMENT
DEVELOPMENT REVIEW BOARD (D.R.B.) REQUIRED INFRASTRUCTURE LIST

Oakland Ridge Subdivision

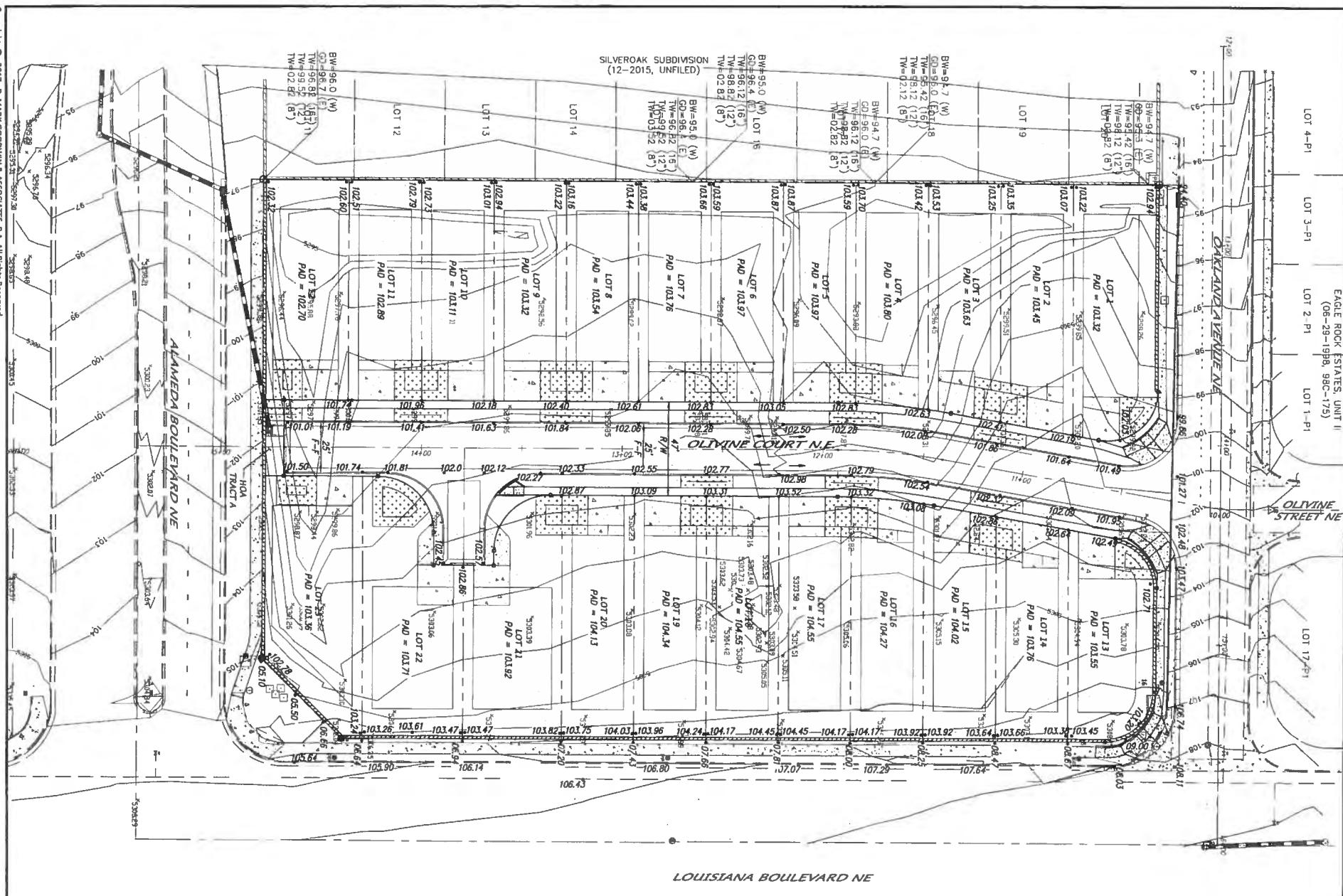
PROPOSED NAME OF PLAT AND/OR SITE DEVELOPMENT PLAN

Lots 15, 16, 17, and 18, Block 28, Tract A, Unit B, N.A.A.

EXISTING LEGAL DESCRIPTION PRIORITY TO PLATTING ACTION

Following is a summary of PUBLIC/PRIVATE Infrastructure required to be constructed or financially guaranteed for the above development. This Listing is not necessarily a complete listing. During the SIA process and/or in the review of the construction drawings, if the DRC Chair determines that appurtenant items and/or unforeseen items have not been included in the infrastructure listing, the DRC Chair may include those items in the listing and related financial guarantee. Likewise, if the DRC Chair determines that appurtenant or non-essential items can be deleted from the listing, those items may be deleted as well as the related portions of the financial guarantees. All such revisions require approval by the DRC Chair, the User Department and agent/owner. If such approvals are obtained, these revisions to the listing will be incorporated administratively. In addition, any unforeseen items which arise during construction which are necessary to complete the project and which normally are the Subdivider's responsibility will be required as a condition of project acceptance and close-out by the City.

SIA Sequence #	COA DRC Project #	Type of Improvement	Size	Location	From	To	City Inspector	City Cnst Engineer
		ON-SITE PAVING		Olivine Court	Oakland Ave	Lot 12 and 23	/	/
		Res Pavnt	25FF				/	/
		Curb & Gutter		Olivine Court	Oakland Ave	Lot 12	/	/
		Sidewalk (west side) (1)	4'	Olivine Court	Oakland Ave	Lot 21	/	/
		Sidewalk (east sides) (1)	4'				/	/
							/	/
		Res Pavnt	20 FF	Olivine Club	Olivine Court	Lot 21 & 22	/	/
		Curb & Gutter		"			/	/
		Sidewalk (south side)	4'	Oakland Ave	West P.L.	Louisiana	/	/
		Sidewalk (north side)	6'	Alameda Blvd.	West P.L.	Louisiana	/	/
							/	/
		WATER		Olivine Court	Ex WL Oakland Ave	Ex WL Alameda	/	/
		Watertine	8"				/	/
							/	/
		SANITARY SEWER		Olivine Court	Ex SAS Oakland Ave	Lot 12/23	/	/
		SAS	8"				/	/
							/	/
		PRO-RATA	\$1,293.30	WATER			/	/
		PRO-RATA	\$1,528.85	SANITARY SEWER			/	/
							/	/
		DRAINAGE		Olivine Court	South End of ROW	Ex. Inlet Alameda	/	/
		RCP	24"				/	/
							/	/

LOT 4-P1
LOT 3-P1
LOT 2-P1
LOT 1-P1EAGLE ROCK ESTATES, UNIT II
(06-29-1998, 98C-175)
ESTATES UNIT III
(05-13-1999,
99C-118)

LOT 9-P1

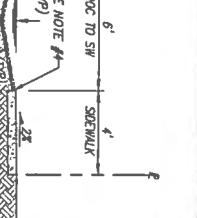
CAUTION:
NOTE THAT ALL EXISTING UTILITIES MAY NOT BE
SHOWN. ALL EXISTING SERVICE CONNECTIONS ARE
NOT SHOWN. ANY EXISTING UTILITIES THAT ARE
SHOWN ARE APPROXIMATE LOCATION ONLY.
IT SHALL BE THE SOLE RESPONSIBILITY OF THE
CONTRACTOR TO CONTACT ALL THE UTILITY
OWNERS AND TO CONDUCT ALL NECESSARY
FIELD INVESTIGATIONS PRIOR TO ANY EXCAVATIONS
AND OTHER IMPROVEMENTS.

LANDSCAPE BUFFER NOTES:
1. Surface between back of curb and sidewalk to be covered with
gravel mulch (minimum 3/4"), cobble or rip-rap. Do not fill
entire swale.

2. Landscape fabric is recommended, but not required, between
the dirt and the stone. If landscape fabric is to be used it
is to be permeable.

3. The 6" depth is measured from top of curb to top of
landscape rock material or gravel mulch.

LEGEND



GENERAL NOTES

1. CONTRACTOR MUST OBTAIN A TOPSOIL DISTURBANCE PERMIT FROM
THE ENVIRONMENTAL HEALTH DIVISION PRIOR TO CONSTRUCTION.
2. CITY OF ALBUQUERQUE STANDARD SPECIFICATIONS FOR PUBLIC
WORKS CONSTRUCTION, LATEST EDITION SHALL GOVERN ALL WORK.
3. THE CONTRACTOR SHALL CONFORM TO ALL CITY, COUNTY, STATE
AND FEDERAL DUST CONTROL MEASURES AND REQUIREMENTS AND
WILL BE RESPONSIBLE FOR PREPARING AND OBTAINING ALL
NECESSARY APPLICATIONS AND APPROVALS.

4. THE CONTRACTOR SHALL ENSURE THAT NO SOIL EROSION FROM
THE LOTS INTO PUBLIC RIGHT-OF-WAY. THIS CAN BE ACHIEVED
BY CONSTRUCTING TEMPORARY BERM AND WETTING THE SOIL TO
KEEP IT FROM BLOWING.

5. THE EARTHWORK CONTRACTOR SHALL STOCKPILE ENOUGH MATERIAL
ADJACENT TO RE-FACING WALL LOCATIONS TO BE UTILIZED FOR
WALL BACKFILL.

LEGAL DESCRIPTION

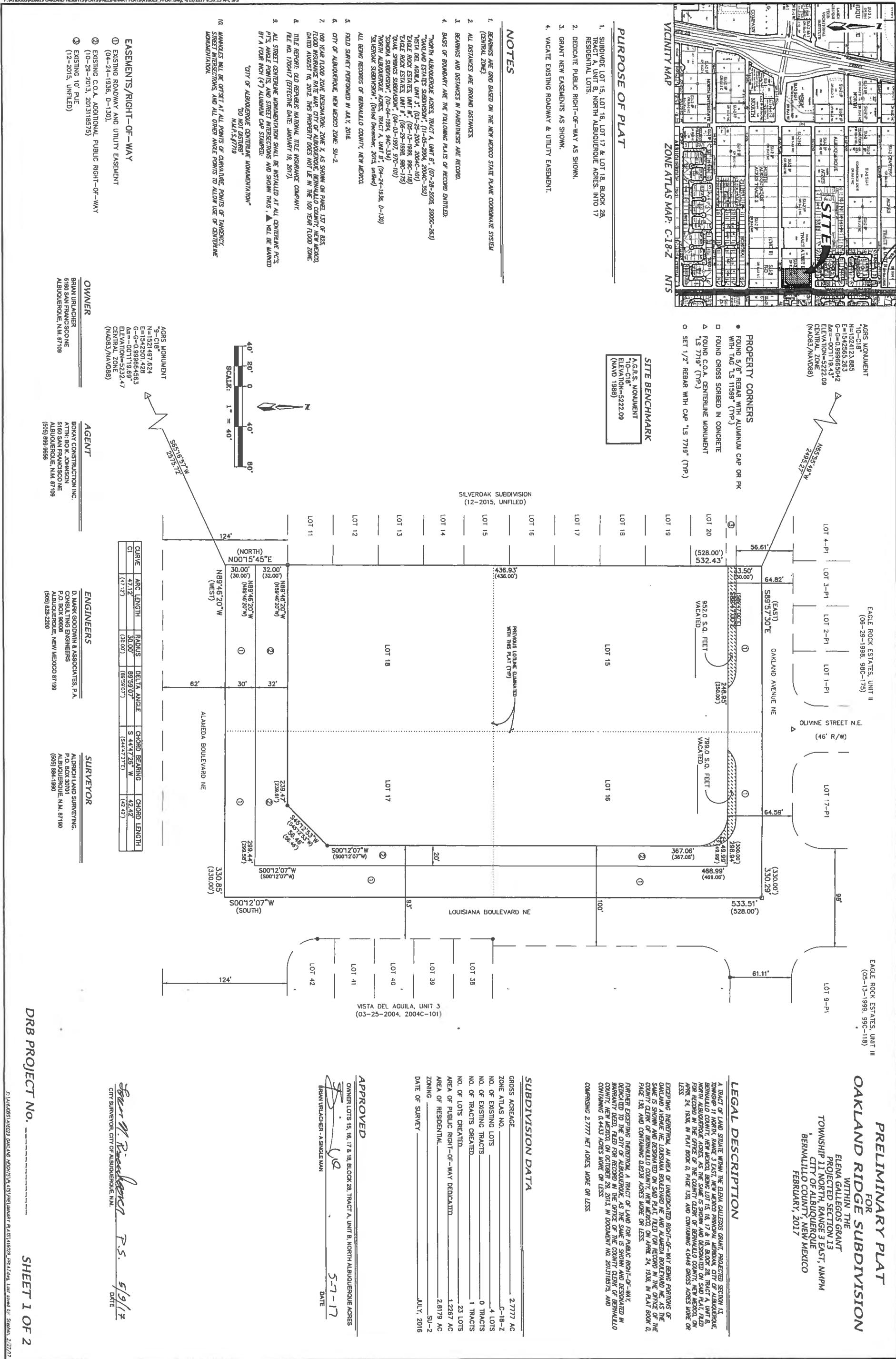
A TRACT OF LAND SITUATE WITHIN THE ELENA CALLEGOS GRANT,
MEXICO PROVINCIAL MEXICO, CITY OF ALBUQUERQUE, BERNALLO
COUNTY, NEW MEXICO, BEING LOT 15, 17 & 18, BLOCK 26, TRACT
A, LINE 3, MASTERS ALAMEDA ADDRESSES AS SAME. SAME IS SHOWN
AS REFERENCED ON PLAT, FILED FOR RECORD IN THE OFFICE
OF THE COUNTY CLERK OF BERNALLO COUNTY, NEW MEXICO, ON
APRIL 24, 1936, IN PLAT BOOK D, PAGE 130, AND CONTAINING
0.6236 ACRES MORE OR LESS.

EXCEPT THEREFROM, A TRACT OF LAND FOR PUBLIC
USE AND ALAMEDA BOULEVARD NE AS THE SAME IS SHOWN AND
DESIGNATED ON SAID PLAT, FILED FOR RECORD IN THE OFFICE OF
THE SAME AND DESIGNATED IN MARSHALL DEED, FILED
FOR RECORD IN THE OFFICE OF THE COUNTY CLERK OF BERNALLO
COUNTY, NEW MEXICO, ON OCTOBER 28, 2011, IN DOCUMENT NO.
20113783, AND CONTAINING 0.4433 ACRES MORE OR LESS.

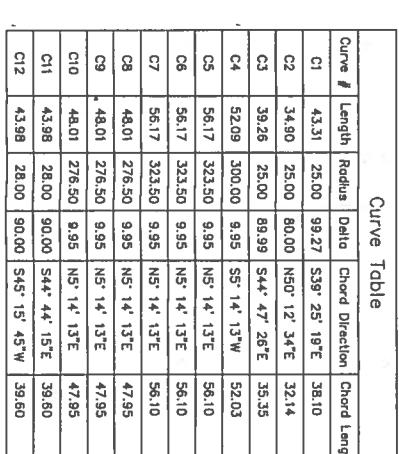
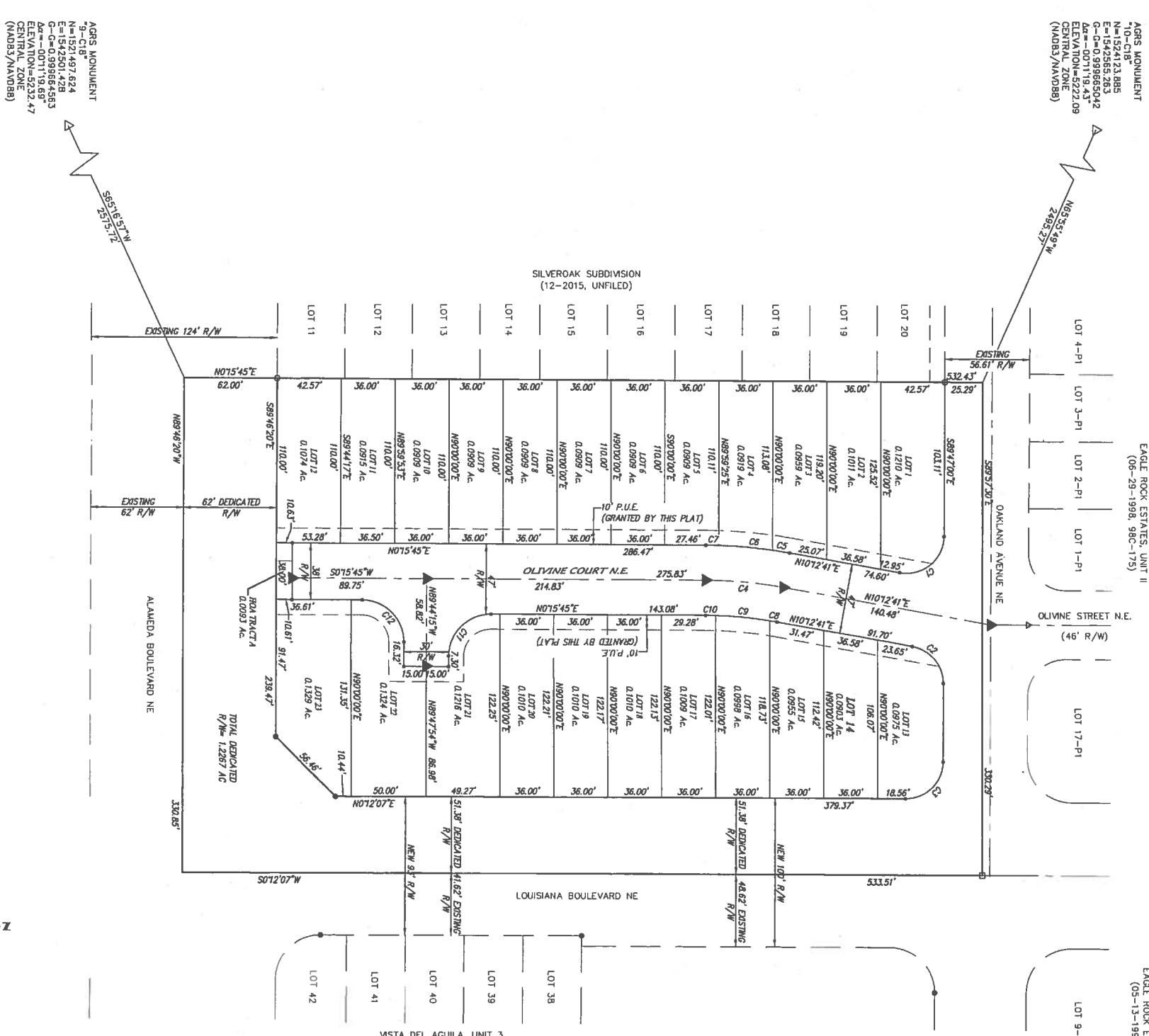
COMPRESSING 2.7777 NET ACRES, MORE OR LESS.

CROSS REFERENCES: PLAT BOOK D, PAGE 130, AND CONTAINING 0.6466
ACRES MORE OR LESS.

ACROSS ADDRESSES UNKNOWN.



F:\V16J085\A16029 OAKLAND HEIGHTS\PLATS\PRELIMINARY PLATS\A16029_PPLAT.dwg, 4/19/2017 8:40:32 AM, SPS



**PRELIMINARY PLAT
FOR
OAKLAND RIDGE SUBDIVISION
WITHIN THE**

**PROJECTED SECTION 13
TOWNSHIP 11 NORTH, RANGE 3 EAST, N.M.
CITY OF ALBUQUERQUE
BERNALILLO COUNTY, NEW MEXICO**
FEBRUARY, 2017

- FOUND 5/8" REBAR WITH ALUMINUM CAP U
WITH TAG "LS 11599" (TYP.)
 - FOUND SCRIBED IN CONCRETE
 - △ FOUND C.O.A. CENTERLINE MONUMENT
"LS 7719" (TYP.)
 - SET 1/2" REBAR WITH CAP "LS 7719" (TYP.)

EAGLE ROCK ESTATES, UNIT #1
(05-13-1999, 99C-11B)

EAGLE ROCK ESTATES, UNIT II
(06-29-1998, 98C-175)

AGRS MONUMENT
"10-C1B"
N=1524123.985
E=1542565.263
G=G-0.998650442
 $\Delta x = -001119.43^*$
ELEVATION=522.09
CENTRAL ZONE
(NADB3/NAVD88)

N=1521497.624
E=1542501.428
G-G=0.999664563
 $\Delta x = -00^{\circ}11'19.69''$
ELEVATION=5232.47
CENTRAL ZONE
(NADB3/NAVD88)

DRB PROJECT No. _____

SHEET 2 OF 2

APPENDIX A

*First Flush Calculations
AHYMO printouts
Excerpts from N.A.A. Master Drainage Plan*

OAKLAND RIDGE SUBDIVISION

First Flush Calculations:

Project Site Area = 123,350 SF

Impervious Area:

NUMBER OF LOTS = 23

N value = 23/2.83 = 8.12

Therefore Treatment D = 60 %

((123,350 SF) x (0.6)) (0.34")/(12) = **2,097 cu.ft.**

Total required treatment volume = 2,097 cubic feet

North Sub basin area = 42.22% x 2097 cu.ft. = 885 cu.ft.

South Sub basin area = 57.78% x 2097 cu.ft. = 1212 cu.ft.

FIRST FLUSH TREATMENT PONDS DESIGN DIMENSIONS

Front Yards: Dimensions as shown on the plan,

6" maximum depth with varying side slopes, with a 3:1 maximum on any one side

Curbside: Six feet wide, 6" maximum depth, with 6:1 side slopes (typical).

AHYMO PROGRAM (AHYMO-S4) - Version: S4.01a - Rel: 01a
 RUN DATE (MON/DAY/YR) = 05/17/2017
 START TIME (HR:MIN:SEC) = 09:30:51 USER NO.= M-GoodwinNMSiteA90075759
 INPUT FILE = C:\Program Files (x86)\AHYMO-S4\oakland.dat

START LOCATION
 NEW MEXICO
 State of New Mexico soil infiltration values (LAND FACTORS) used for computations.

Land Treatment	Initial Abstr. (in)	Unif. Infiltr. (in/hour)
A	0.65	1.67
B	0.50	1.25
C	0.35	0.83
D	0.10	0.04

TIME=0.0 HR PUNCH CODE=0 PRINT LINES=-6

North Basin (42.22%)
 $Q = 5.16 \text{ cfs}$

South Basin (57.78%)
 $Q = 7.05 \text{ cfs}$

 ***** FILE: OAKLAND.DAT REV: 5-16-17 DLH
 ***** ZONE ATLAS

 ***** 100 YEAR 6 HOUR STORM EVENT

 ***** TYPE=1 RAIN QUARTER=0.0
 ***** RAIN ONE=2.1 IN RAIN SIX=2.50 IN
 ***** RAIN DAY=2.85 IN DT=0.05 HRS

6-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1
 DT = 0.050000 HOURS END TIME = 6.000000 HOURS

 ***** DEVELOPED CONDITIONS
 ***** SUB BASIN 100
 ***** AREA= 2.8317 ACRES

 ***** COMPUTE NM HYD ID=1 HYD NO=100. AREA= 0.00425 SQ MI
 ***** PER A=0 PER B=20 PER C=20 PER 60
 ***** TP=-.1333 HR MASS RAIN=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
 UNIT PEAK = 10.482 CFS UNIT VOLUME = 0.9981 B = 526.28 P60 = 2.1000
 AREA = 0.002655 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
 RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=1 CODE=1 PARTIAL HYDROGRAPH 100.00

RUNOFF VOLUME = 1.81394 INCHES = 0.4281 ACRE-FEET
 PEAK DISCHARGE RATE = 12.21 CFS AT 1.5000 HOURS BASIN AREA = 0.0044 SQ. MI.
 *S***** FINISH END TIME (HR:MIN:SEC) = 09:30:51

**FINAL
NORTH ALBUQUERQUE ACRES
MASTER DRAINAGE PLAN**

Prepared For:



City of Albuquerque

Prepared By:



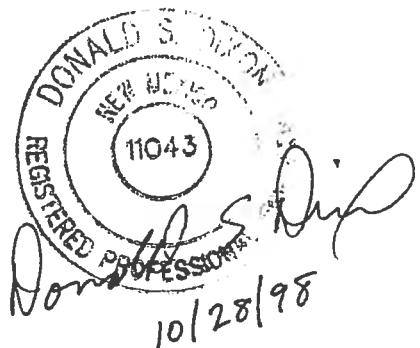
**ENGINEERS AND ENVIRONMENTAL SCIENTISTS
1720-B Randolph Road SE, Albuquerque, NM 87106**

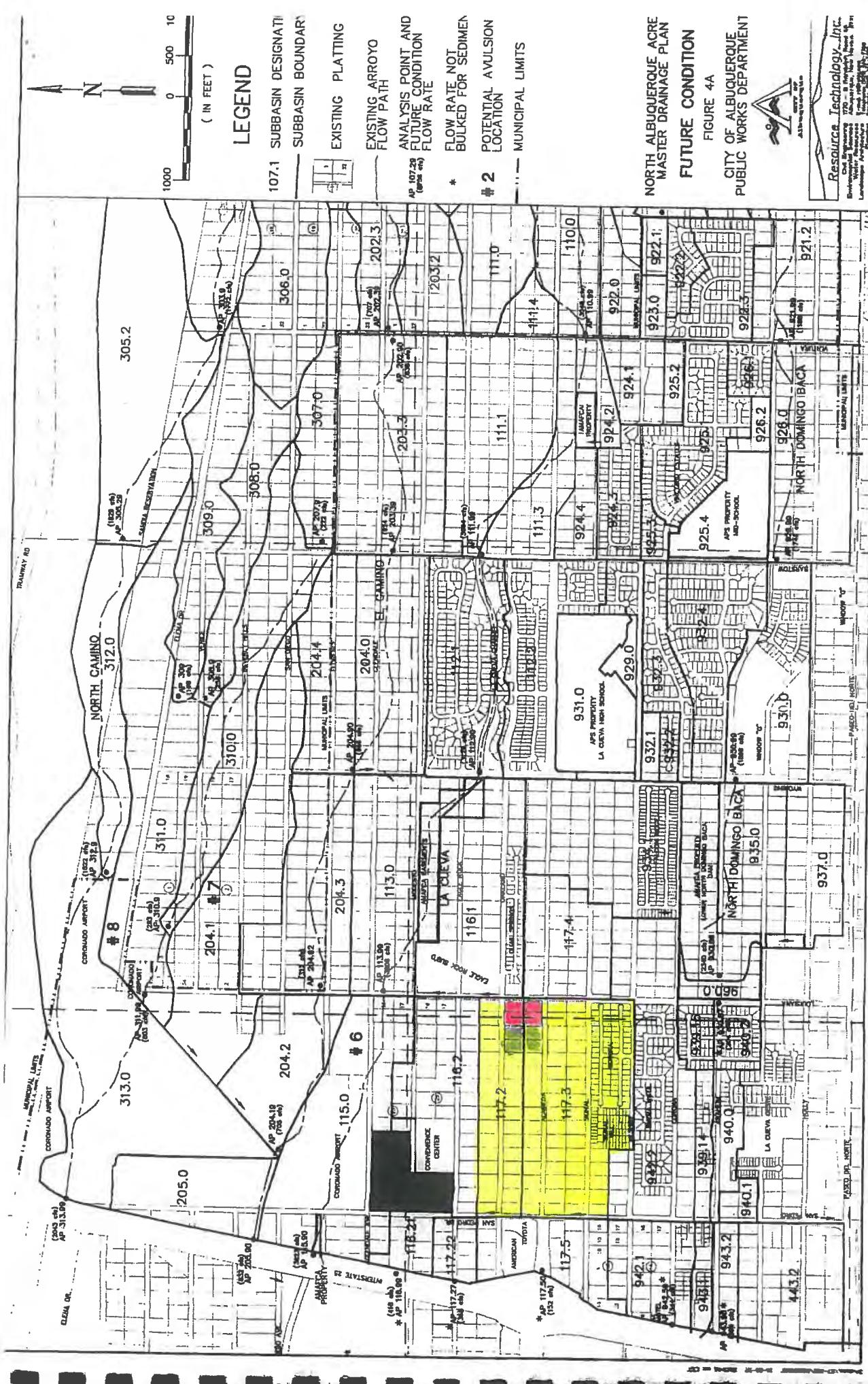
Telephone (505) 243-7300

Fax (505) 243-7400

rti@nmia.com

October 1998





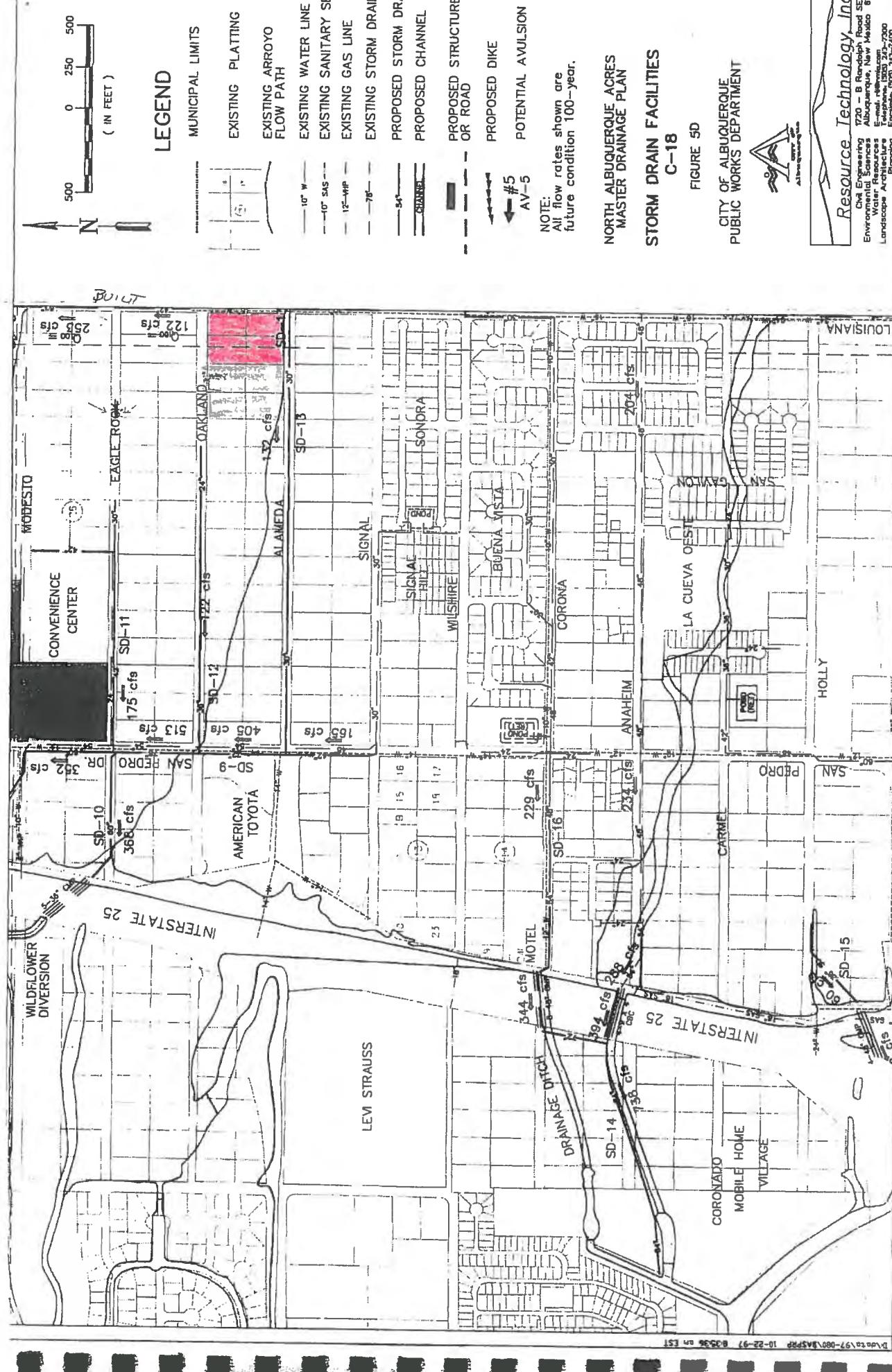




FIGURE 5E
CITY OF ALBUQUERQUE
PUBLIC WORKS DEPARTMENT

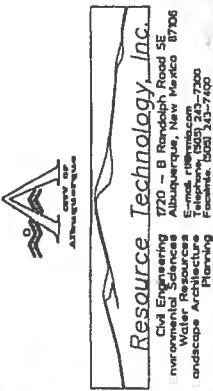
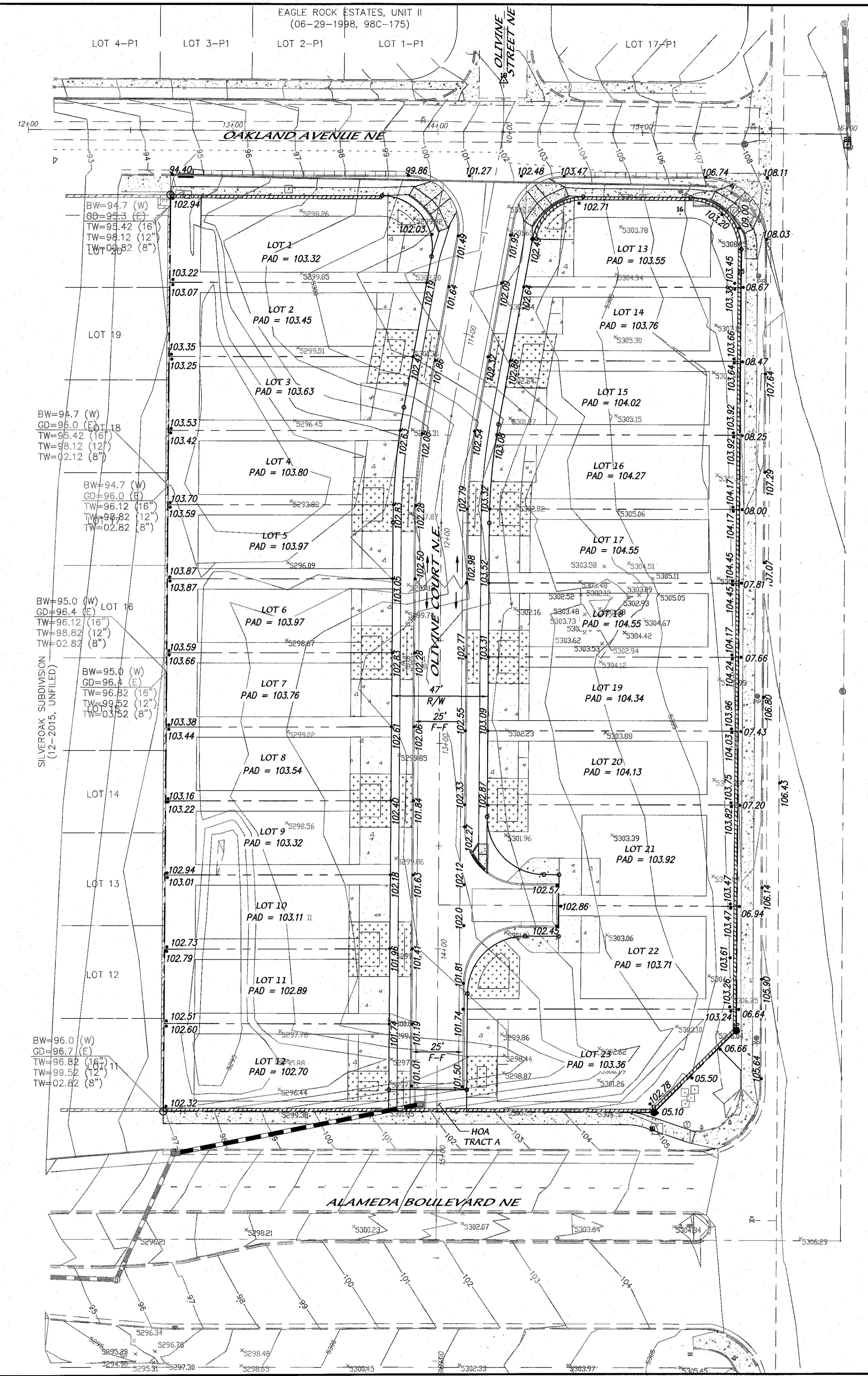


TABLE A-2 (cont.)

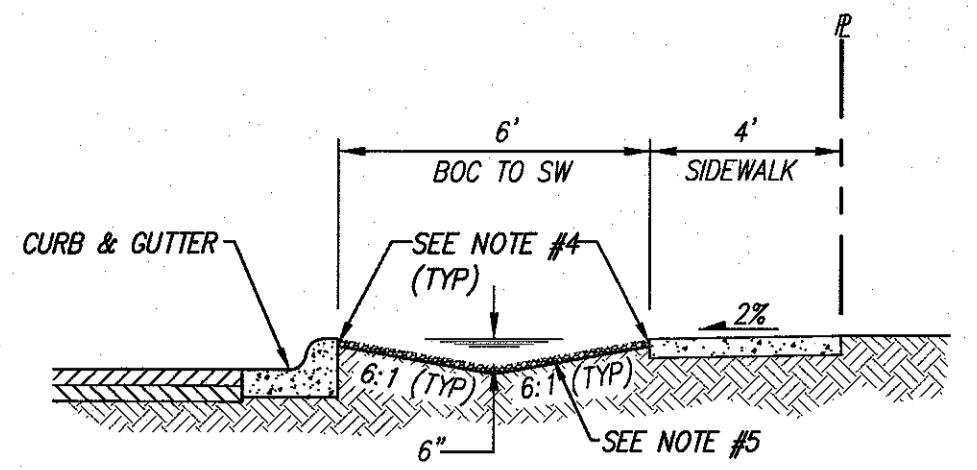
LA CUEVA ARROYO SUB-BASIN CHARACTERISTICS

Basin ID	Hydrologic Condition	Basin Area (mi ²)	Land Treatment (%)				TP (hrs)
			A	B	C	D	
113*	Existing	.1136	80	0	15	5	.133
	Future	.1000	0	25	15	60	.133
115*	Existing	.1337	80	0	15	5	.133
	Future	.1202	0	26	12	62	.133
116*	Existing	.1309	80	0	5	15	.133
116.1	Future	.1000	0	25	15	50	.133
116.2	Future	.0719	0	25	15	60 50	.133
116.21	Future	.0344	0	40	20	40	.133
117.2*	Existing	.1391	73	0	7	20	.22
	Future	.0500	0	34	16	50	.133
117.21*	Existing	.0234	0	34	16	50	.133
117.22*	Future	.0156	0	20	10	70	.133
117.3*	Existing	.0863	65	5	15	15	.133
	Future	.1172	0	34	16	50	.133
117.31*	Existing	.0250	0	34	16	50	.133
117.32*	Existing	.0090	0	34	16	50	.133
117.4*	Existing	.0750	85	0	5	10	.133
	Future	.0512	0	25	15	60	.133
117.5*	Existing	.0550	0	10	20	70	.133
	Future	.0550	0	10	20	70	.133
118	Existing	.0649	0	20	10	70	.133
	Future	.0649	0	20	10	70	.133
118.1	Existing	.0306	75	5	10	10	.133
	Future	.0306	0	20	30	50	.133
119	Existing	.0549	0	20	10	70	.133
	Future	.0549	0	20	10	70	.133
120	Existing	.0268	50	0	0	50	.133
	Future	.0268	0	20	10	70	.133
121	Existing	.0489	80	0	15	5	.133
	Future	.0489	0	20	10	70	.133

*Modified for COA NAA MDP 9/97



CAUTION:
NOTE THAT ALL EXISTING UTILITIES MAY NOT BE SHOWN. ALL EXISTING SERVICE CONNECTIONS ARE NOT SHOWN. ANY EXISTING UTILITIES THAT ARE SHOWN ARE APPROXIMATE LOCATION ONLY.
IT SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO CONTACT ALL THE UTILITY OWNERS AND TO CONDUCT ALL NECESSARY FIELD INVESTIGATIONS PRIOR TO ANY EXCAVATIONS TO DETERMINE THE ACTUAL LOCATION OF UTILITIES AND OTHER IMPROVEMENTS.



SECTION A - A
TYPICAL DEPRESSED AREA
ON-SITE BETWEEN SIDEWALK & BACK OF CURB

LANDSCAPE BUFFER NOTES:

1. Surface between back of curb and sidewalk to be covered with gravel mulch (minimum 3/4"), cobbles or rip-rap. Do not fill entire swale.
 2. Landscape fabric is recommended, but not required, between the dirt and the stone. If landscape fabric is to be used it is to be permeable.
 3. The 6" depth is measured from top of curb to top of landscape rock material or gravel mulch.

LEGEND

EXISTING CONCRETE

EXISTING BLOCK WALL

EXISTING METAL FENCE

EXISTING METAL FENCING W/BLOCK PILASTERS

EXISTING WATER VALVE

EXISTING FIRE HYDRANT

EXISTING SANITARY SEWER MANHOLE

EXISTING STORM DRAIN MANHOLE

EXISTING STORM DRAIN INLET

EXISTING UTILITY PEDESTAL

EXISTING UNDERGROUND GAS LINE

EXISTING UNDERGROUND SANITARY SEWER

EXISTING UNDERGROUND STORM DRAIN LINE

EXISTING UNDERGROUND WATER LINE

EXISTING SPOT ELEVATION

EXISTING BACK OF CURB ELEVATION

EXISTING FLOW LINE ELEVATION

EXISTING TOP ELEVATION

EXISTING TOE ELEVATION

EXISTING TOP OF CONCRETE ELEVATION

NEW STANDARD CURB & GUTTER

NEW MOUNTABLE CURB & GUTTER

NEW RIGHT-OF-WAY

NEW CENTERLINE

NEW LOT LINES

NEW EASEMENTS

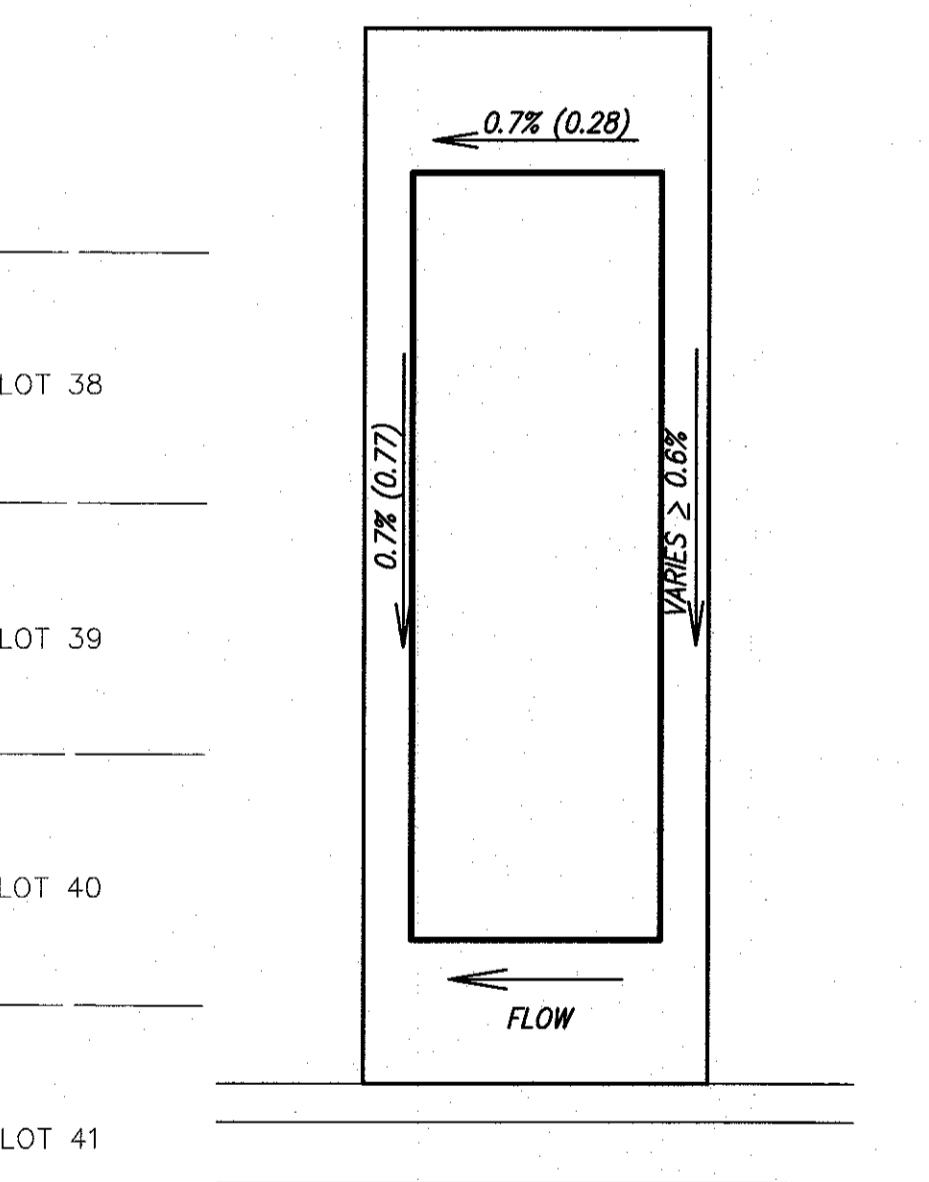
NEW TOP OF WALL ELEVATION

NEW BOTTOM OF WALL ELEVATION

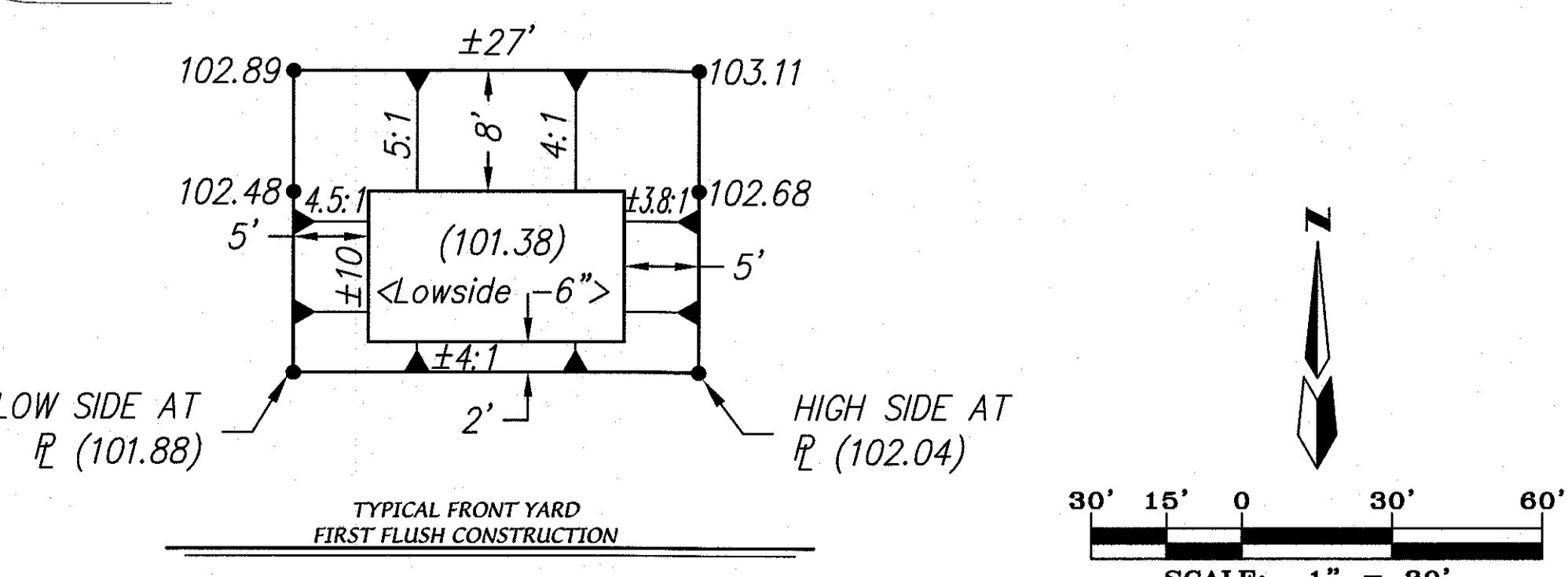
NEW SPOT ELEVATIONS

NEW FLOW DIRECTION

NEW STORM DRAIN

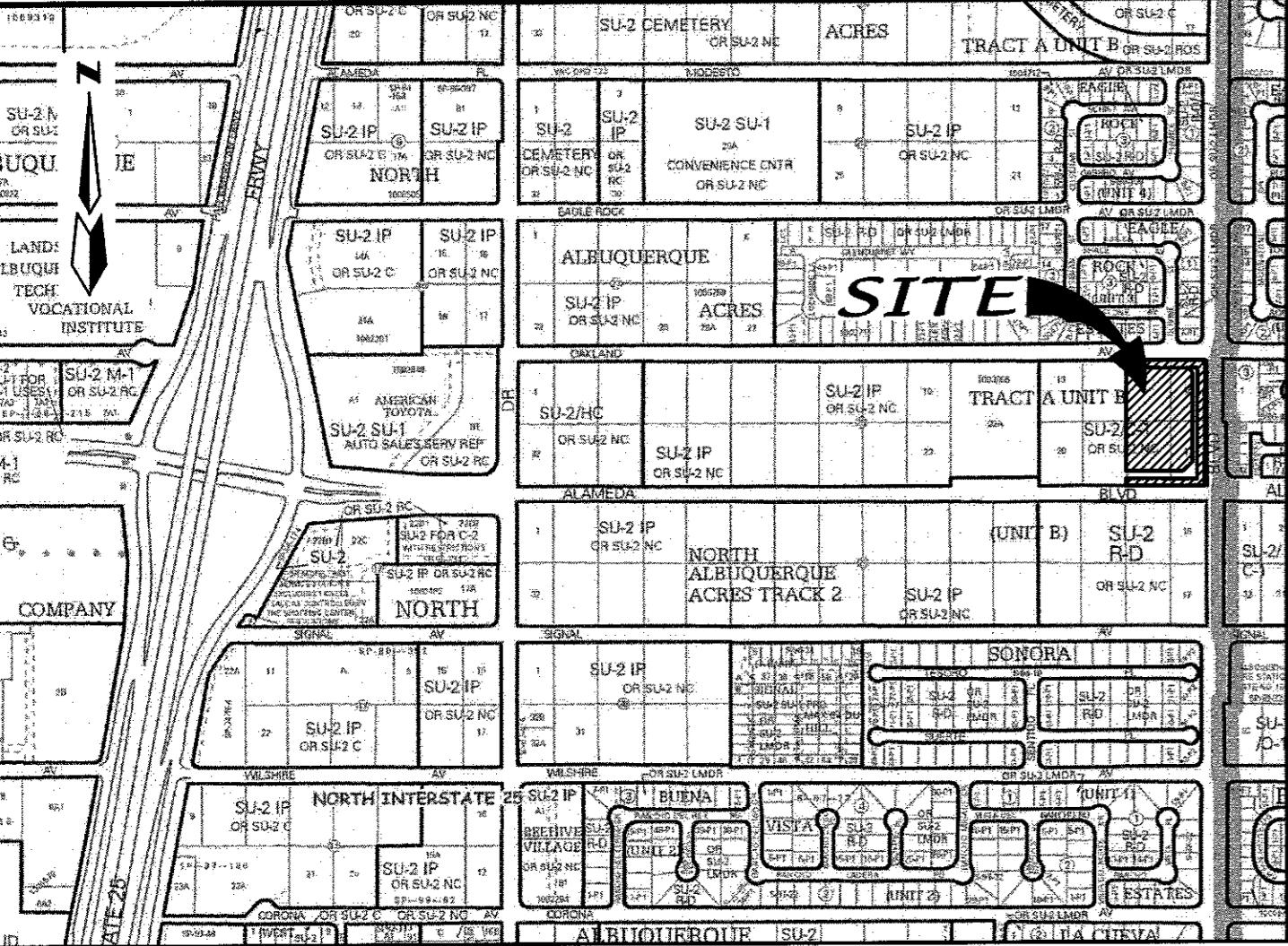


TYPICAL LOT GRADING SCHEME



F:\A16JOBS\A16029 OAKLAND HEIGHTS\GRADE & DRAIN\A16029_G&D PLAN_R.dwg, Last saved by: Stephen, 2/22/17

**PRELIMINARY PLAT
FOR
OAKLAND RIDGE SUBDIVISION**
WITHIN THE
ELENA GALLEGOS GRANT
PROJECTED SECTION 13
TOWNSHIP 11 NORTH, RANGE 3 EAST, NMPM
CITY OF ALBUQUERQUE
BERNALILLO COUNTY, NEW MEXICO
FEBRUARY, 2017



PURPOSE OF PLAT

1. SUBDIVIDE LOT 15, LOT 16, LOT 17 & LOT 18, BLOCK 28, TRACT A, UNIT B, NORTH ALBUQUERQUE ACRES. INTO 17 RESIDENTIAL LOTS.
2. DEDICATE PUBLIC RIGHT-OF-WAY AS SHOWN.
3. GRANT NEW EASEMENTS AS SHOWN.
4. VACATE EXISTING ROADWAY & UTILITY EASEMENT.

NOTES

1. BEARINGS ARE GRID BASED ON THE NEW MEXICO STATE PLANE COORDINATE SYSTEM (CENTRAL ZONE).
2. ALL DISTANCES ARE GROUND DISTANCES.
3. BEARINGS AND DISTANCES IN PARENTHESIS IN RECORD.
4. BASIS OF BOUNDARY ARE THE FOLLOWING PLATS OF RECORD ENTITLED:

 - "NORTH ALBUQUERQUE ACRES, TRACT A, UNIT B", (07-28-2005, 2005C-263)
 - "OAKLAND ESTATES SUBDIVISION", (11-05-2004, 2004C-352)
 - "VISTA DEL AGUILA, UNIT 3", (03-25-2004, 2004C-101)
 - "EAGLE ROCK ESTATES, UNIT II", (05-13-1999, 99C-118)
 - "EAGLE ROCK ESTATES, UNIT I", (06-29-1998, 98C-175)
 - "QUAIL SPRINGS SUBDIVISION", (04-03-1997, 97C-101)
 - "SONORA SUBDIVISION", (10-04-1994, 94C-334)
 - "NORTH ALBUQUERQUE ACRES, TRACT A, UNIT B", (04-24-1936, D-130)
 - "SILVEROK SUBDIVISION", (Dated December, 2015, unfiled)

ALL BEING RECORDS OF BERNALILLO COUNTY, NEW MEXICO.

5. FIELD SURVEY PERFORMED IN JULY, 2016.
6. CITY OF ALBUQUERQUE, NEW MEXICO ZONE: SU-2.
7. 100 YEAR FLOOD ZONE DESIGNATION: ZONE X, AS SHOWN ON PANEL 137 OF 825, FLOOD INSURANCE RATE MAP, CITY OF ALBUQUERQUE, BERNALILLO COUNTY, NEW MEXICO, DATED AUGUST 16, 2012. THIS PROPERTY DOES NOT LIE IN THE 100 YEAR FLOOD ZONE.
8. TITLE REPORT: OLD REPUBLIC NATIONAL TITLE INSURANCE COMPANY, FILE NO. 1700417 (EFFECTIVE DATE: JANUARY 19, 2017).
9. ALL STREET CENTERLINE MONUMENTATION SHALL BE INSTALLED AT ALL CENTERLINE PC'S, PTS, ANGLE POINTS, AND STREET INTERSECTIONS AND SHOWN THUS, ▲ WILL BE MARKED BY A FOUR INCH (4") ALUMINUM CAP STAMPED:

 - "CITY OF ALBUQUERQUE CENTERLINE MONUMENTATION"
 - "DO NOT DISTURB"
 - N.M.P.S.#719

10. MANHOLES WILL BE OFFSET AT ALL POINTS OF CURVATURE, POINTS OF TANGENCY, STREET INTERSECTIONS, AND ALL OTHER ANGLE POINTS TO ALLOW USE OF CENTERLINE MONUMENTATION.

AGRS MONUMENT
"10-C18"
N=1524123.885
E=1542565.263
G-G=0.999665042
 $\Delta\alpha=-00^{\circ}11'19.43''$
ELEVATION=5222.09
CENTRAL ZONE
(NAD83/NAVD88)

- PROPERTY CORNERS**
- FOUND 5/8" REBAR WITH ALUMINUM CAP OR PK WITH TAG "LS 11599" (TYP.)
 - FOUND CROSS SCRIBED IN CONCRETE
 - △ FOUND C.O.A. CENTERLINE MONUMENT "LS 7719" (TYP.)
 - SET 1/2" REBAR WITH CAP "LS 7719" (TYP.)

SITE BENCHMARK

A.G.R.S. MONUMENT
"10-C18"
ELEVATION=5222.09
(NAVD 1988)

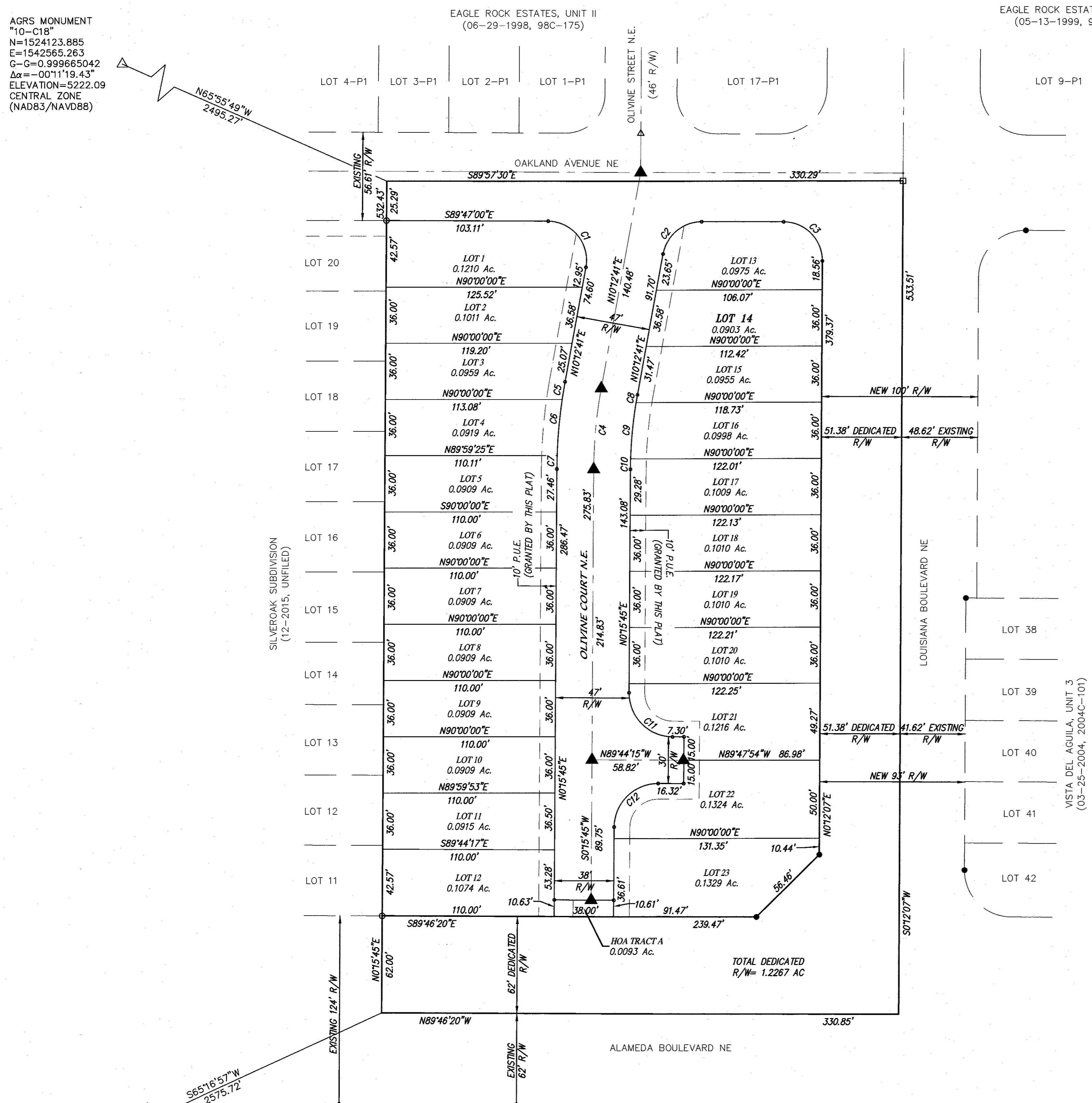
NOTES

**PRELIMINARY PLAT
FOR
OAKLAND RIDGE SUBDIVISION
WITHIN THE
ELENA GALLEGOS GRANT
PROJECTED SECTION 13
TOWNSHIP 11 NORTH, RANGE 3 EAST, NMPM
CITY OF ALBUQUERQUE
BERNALILLO COUNTY, NEW MEXICO
FEBRUARY, 2017**

AGRS MONUMENT
"10-C18"
N=1524123.885
E=1542565.263
G-G=0.999665042
 $\Delta\alpha=-00^{\circ}11'19.43''$
ELEVATION=5222.0
CENTRAL ZONE
(NAD83/NAVD88)

EAGLE ROCK ESTATES, UNIT II
(06-29-1998, 98C-175)

EAGLE ROCK ESTATES, UNIT III
(05-13-1999, 99C-118)



AGRS MONUMENT
"9-C18"
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E=1542501.428
G-G=0.999664563
 $\Delta\alpha=-00^{\circ}11'19.69''$
ELEVATION=5232.47
CENTRAL ZONE
(NAD83/NAVD88)

A map showing a survey line. The line starts at a point labeled '20' and ends at a point labeled '80'. A north arrow points downwards. Below the line, a scale bar indicates a distance of 1 inch equals 40 feet.

DRB PROJECT No. _____

SHEET 2 OF 2

- PROPERTY CORNERS**

 - FOUND 5/8" REBAR WITH ALUMINUM CAP OR PK WITH TAG "LS 11599" (TYP.)
 - FOUND CROSS SCRIBED IN CONCRETE
 - △ FOUND C.O.A. CENTERLINE MONUMENT "LS 7719" (TYP.)
 - SET 1/2" REBAR WITH CAP "LS 7719" (TYP.)

Curve Table					
Curve #	Length	Radius	Delta	Chord Direction	Chord Length
C1	43.31	25.00	99.27	S39° 25' 19"E	38.10
C2	34.90	25.00	80.00	N50° 12' 34"E	32.14
C3	39.26	25.00	89.99	S44° 47' 26"E	35.35
C4	52.09	300.00	9.95	S5° 14' 13"W	52.03
C5	56.17	323.50	9.95	N5° 14' 13"E	56.10
C6	56.17	323.50	9.95	N5° 14' 13"E	56.10
C7	56.17	323.50	9.95	N5° 14' 13"E	56.10
C8	48.01	276.50	9.95	N5° 14' 13"E	47.95
C9	48.01	276.50	9.95	N5° 14' 13"E	47.95
C10	48.01	276.50	9.95	N5° 14' 13"E	47.95
C11	43.98	28.00	90.00	S44° 44' 15"E	39.60
C12	43.98	28.00	90.00	S45° 15' 45"W	39.60

DRAINAGE LETTER REPORT
FOR
ALAMEDA BOULEVARD SAN PEDRO TO WYOMING
PROJECT
CITY PROJECT NO. 7663.91

January 2012

DRAINAGE LETTER REPORT
FOR
ALAMEDA BOULEVARD SAN PEDRO TO WYOMING
PROJECT
CITY PROJECT NO. 7663.91

Prepared by:
Thompson Engineering Consultants, Inc.
P.O. Box 65760
Albuquerque, NM 87193

January 2012

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APPENDIX A – HYDRAULIC CALCULATIONS

LIST OF EXHIBITS

EXHIBIT I – DRAINAGE BASINS

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TABLE 2 STORM INLET CAPACITIES	3
TABLE 3 STORM DRAIN NORMAL DEPTH	4
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I. INTRODUCTION AND SITE LOCATION

Part of the Alameda Boulevard Widening Project from I-25 to Wyoming includes the installation of a storm drain that will tie into a proposed 72" storm drain in San Pedro Drive on the west and tie into an existing 36" storm drain in Alameda Boulevard just east of Louisiana Boulevard. The storm drain system will also extend south in Louisiana Boulevard to Signal Avenue and then east to an existing 36" storm drain in Signal Avenue. The construction of the proposed storm drain is sized to accept the runoff from the ultimate Alameda street section and the adjacent properties and will eliminate the need for three existing retention ponds in the project area.

The Alameda storm drain discharges to the recently constructed or soon to be constructed storm drain included as part of the San Pedro Storm Drain Project. There is also an existing parallel storm drain system in San Pedro ranging from 48" to 54" diameter. The eventual outfall for both San Pedro Storm Drains are either 5-36" RCP culverts under I-25 north of Eagle Rock or the 8-36" RCP culverts under I-25 north of Alameda Place. The peak runoff for the developed condition is determined by following the basins and hydrology in the North Albuquerque Acres Master Drainage Plan (NAADMP), by Resource Technology Inc. dated October 1998 and revising the basins based on subsequent drainage reports in the drainage area.

II. METHODOLOGY

A hydrologic analysis was not performed for this report. The hydrology given in the NAADMP was used to determine the peak flows that drain to the San Pedro Storm Drain. The hydrologic analyses in the NAADMP was based on Section 22 of the City of Albuquerque Development Process Manual (DPM), entitled "Drainage, Flood Control, and Erosion Control," January, 1993.

The hydraulic analyses of the proposed storm drain system was also based on Section 22 of the DPM for determining pressure flow conditions and head losses at manholes. Microsoft Excel spreadsheet software was used to calculate the hydraulic grade line in storm drains under pressure and for determining head losses at manholes. Graphs given in Section 22 of the DPM were used to determine storm inlet capacities.

Pipe sizes, invert and rim elevations, and system geometry were taken from the record drawings provided by the COA as well as survey data taken for the project by the design team.

III. DRAINAGE ANALYSIS

A. HYDROLOGY

The scope of work identified reviewing the drainage basins in the NAADMP and revising those basins based on subsequent drainage reports that affect the basins that drain to Alameda within the project area. The NAADMP and San Pedro Storm Drain Project DAR identified basins 117.32 and 117.4 draining to Alameda Boulevard. For the developed condition, these basins have Land Treatment Type D percentages ranging from 50% to 60%.

Basins 117.32 and 117.4 were further divided based on previous drainage reports in the project area or on the proposed storm inlet locations along Alameda Boulevard. Basin 117.32 was divided into 9 sub-basins and Basin 117.4 was divided into 4 sub-basins (refer to Exhibit I). For each of the revised basins it was assumed that the Land Treatment D percentage would be the same for the similar basins in the NAADMP. Therefore, the revised basin area was multiplied by the unit peak flow (CFS/ACRE) to determine the peak flow from that basin. To be conservative, the peak flows from each basin were added instead of routed. Exhibit I shows the revised drainage basins and peak flows for each basin and at critical analysis points. Table 1 shows the peak flows for the revised drainage basins.

Table 1 Revised Drainage Basin Peak Flows

Basins	Area (acres)	Type D Land Treatment (%)	CFS/Acre	100yr Peak Flow (CFS)
117.321	0.54	50	3.82	2.06
117.322	2.44	50	3.82	9.32
117.323	2.68	50	3.82	10.24
117.324	1.37	50	3.82	5.23
117.325	1.25	50	3.82	4.77
117.326	5.96	50	3.82	22.77
117.327	4.80	50	3.82	18.34
117.328	5.34	50	3.82	20.40
117.329	6.74	50	3.82	25.75
117.41	17.75	60	4.02	71.36
117.42	14.29	60	4.02	57.45
117.43	0.85	60	4.02	3.42
117.44	0.43	60	4.02	1.33

B. STORM DRAIN HYDRAULICS

1. INTRODUCTION

The proposed storm drain system was modeled using record drawings and topographic and planimetric survey data obtained in the field. The design survey was produced in the NAVD 88 vertical datum. Two systems were modeled to determine the hydraulic grade line (HGL) of the proposed systems. The proposed storm drain system data were input to the models and flows were input at various points in the system represented by locations future flow interception points.

2. STORM INLET CAPACITIES

Storm inlet capacities were determined for the proposed storm drain to be constructed in Alameda and Louisiana. Graphs given in Section 22 of the DPM were used to determine storm inlet capacities. First, the depth of flow in the ultimate street section was determined using Plate 22.3 D-4. The proposed street slope and one-half of the street flows are inputs to the graph to obtain the depth of flow. Then the depth of flow and street slope are input to Plate 22.3 D-6 for

double grate inlets to determine the inlet capacity. It is assumed that each double grate will be 50% clogged and therefore the inlet capacity is reduced by half. Table 2 gives the inlet capacities for the proposed storm drain system.

Table 2 Storm Inlet Capacities

Inlet Station	Contributing Basins	½ Street Flow (CFS)	Street Slope (%)	Flow Depth (FT)	Inlet Capacity (CFS)	Number of Inlets	Bypass Flow (CFS)
29+00	117.325 & 117.321	3.42	2.83	0.29	1.85	2	0.00
24+50	117.326	11.39	3.11	0.41	3.40	3	1.19
20+00	117.327	10.36	2.40	0.40	3.30	3	0.46
15+50	117.328	10.66	2.61	0.40	3.35	3	0.61
11+00	117.329	13.49	3.00	0.44	4.80	3	0.00

3. STORM DRAIN HYDRAULICS

The hydraulic grade line analysis for the proposed storm drain was completed using an Excel spreadsheet that was developed using the methodology given in Section 22.3 of the DPM. The analysis showed that the downstream portion of the proposed Alameda Storm Drain System just east of San Pedro Drive is under pressure flow. The pressure flow unseals between the manholes at station 11+00 and station 15+50 and continues in gravity flow conditions.

The remainder of the storm drain system flows in gravity flow conditions. Therefore, between manholes the hydraulic grade line equals the normal depth of the storm drain. Table 3 gives the normal depths for each pipe segment under gravity flow conditions.

Table 3 Storm Drain Normal Depth

Segment Stations	Pipe Dia. (IN)	Pipe Slope (%)	Peak Flow (CFS)	Velocity (FPS)	Normal Depth (FT)
Alameda					
15+50 to 20+00	48	2.89	205.0	21.77	2.81
20+00 to 24+50	48	2.61	185.2	20.51	2.70
24+50 to 27+10	42	2.85	165.1	20.12	2.78
27+10 to 29+00	42	2.83	159.8	20.01	2.71
29+00 to 29+80	42	2.94	153.0	20.25	2.56
29+80 to 31+45	42	2.94	142.8	20.04	2.43
31+45 to 33+50	42	2.18	133.5	17.47	2.59
33+50 to 36+67	42	2.10	133.5	17.18	2.63
36+67 to 38+04	36	6.43	71.4	22.91	1.36
38+04 to 40+77	36	2.54	63.2	15.68	1.67
Louisiana					
11+10 to 12+74	36	0.80	60.9	9.61	2.52
7+54 to 11+10	36	0.65	57.5	8.53	2.72
12+74 to 13+59	24	1.42	1.33	4.45	0.30
Signal	36	1.88	57.5	13.67	1.73

The head losses through the manholes equals the heal loss due to bend losses, junction losses, and manhole losses. Table 4 shows the total head losses at each of the manholes.

Table 4 Manhole Head Losses

Station	Bend Loss (FT)	Junction Loss (FT)	Manhole Loss (FT)	Total Losses (FT)
Alameda				
20+00	0.00	1.60	0.33	1.93
24+50	0.00	1.27	0.31	1.58
27+10	0.00	0.38	0.31	0.69
29+00	0.00	0.32	0.32	0.64
29+80	0.00	0.73	0.31	1.04
31+45	0.00	1.68	0.24	1.92
33+50	0.00	0.00	0.23	0.23
36+67	0.00	2.51	0.41	2.92
38+04	0.00	2.56	0.21	2.77
Louisiana				
7+05	0.00	0.00	0.15	0.15
7+55	0.58	0.00	0.15	0.73
11+10	0.00	0.41	0.06	0.47

APPENDIX A
HYDRAULIC CALCULATIONS

STREET CAPACITY

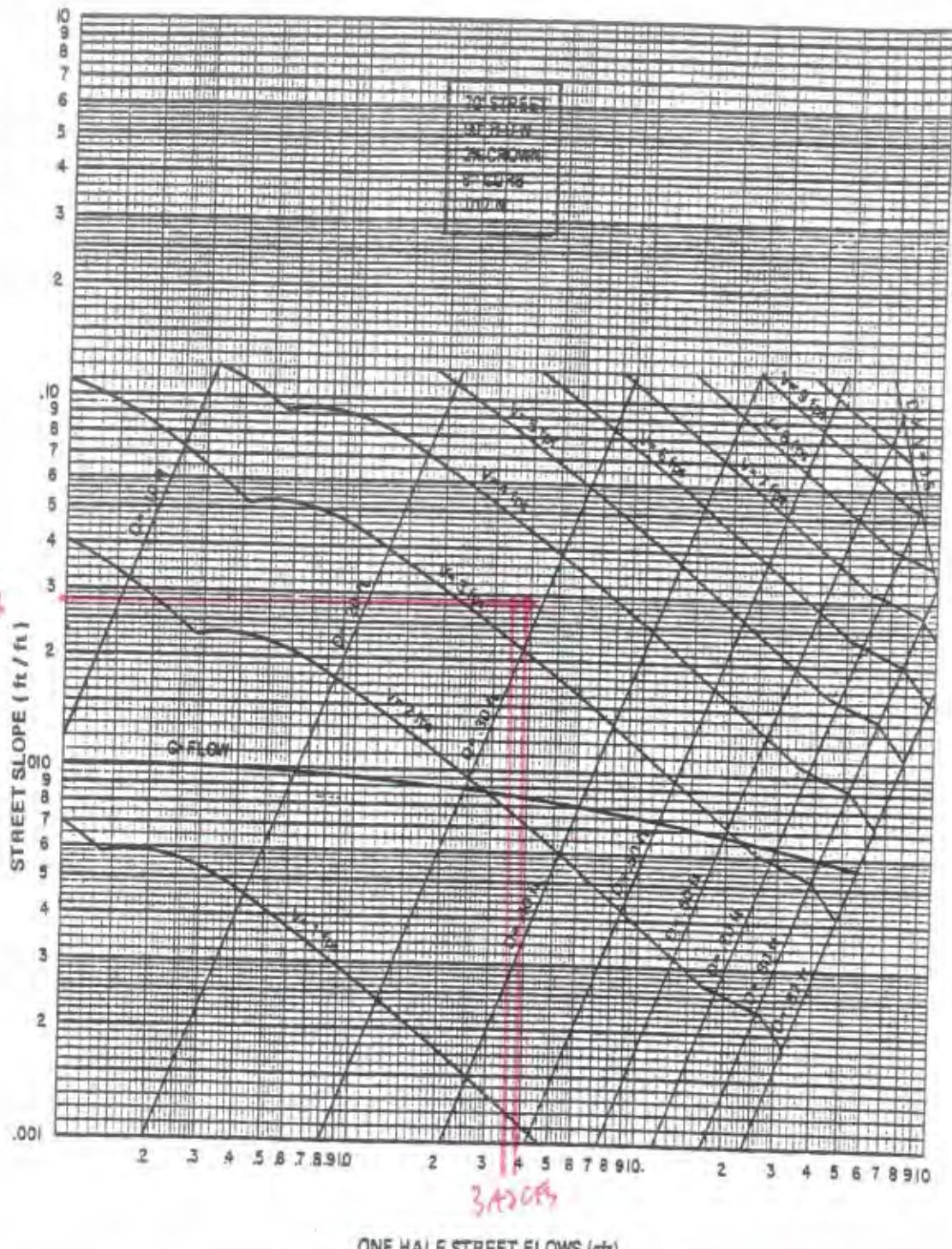


PLATE 22.3 D-4

BASIN 117.325

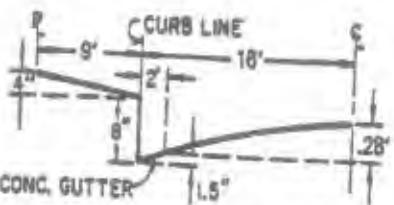
$$\frac{1}{2} = 2.39 \text{ CPS} + ((\frac{1}{2} \text{ at Basin } 117.3 \text{ ft}) 1.03 = 3.42 \text{ CPS}$$

$$S = 2.83^{\circ} \text{ N}$$

GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION
(ABOVE BASIN)

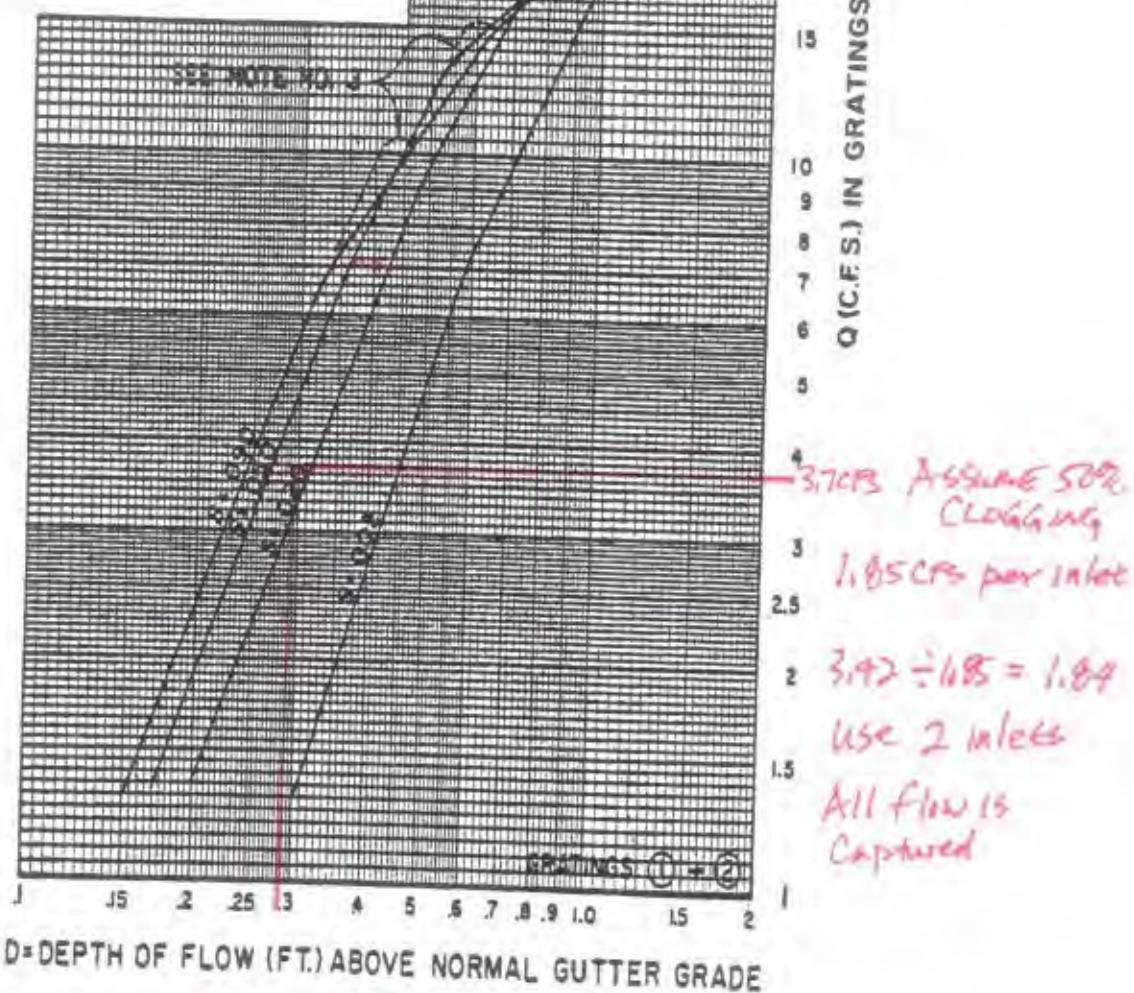


PLATE 22.3 D-6

BASIN 117,325

STREET CAPACITY

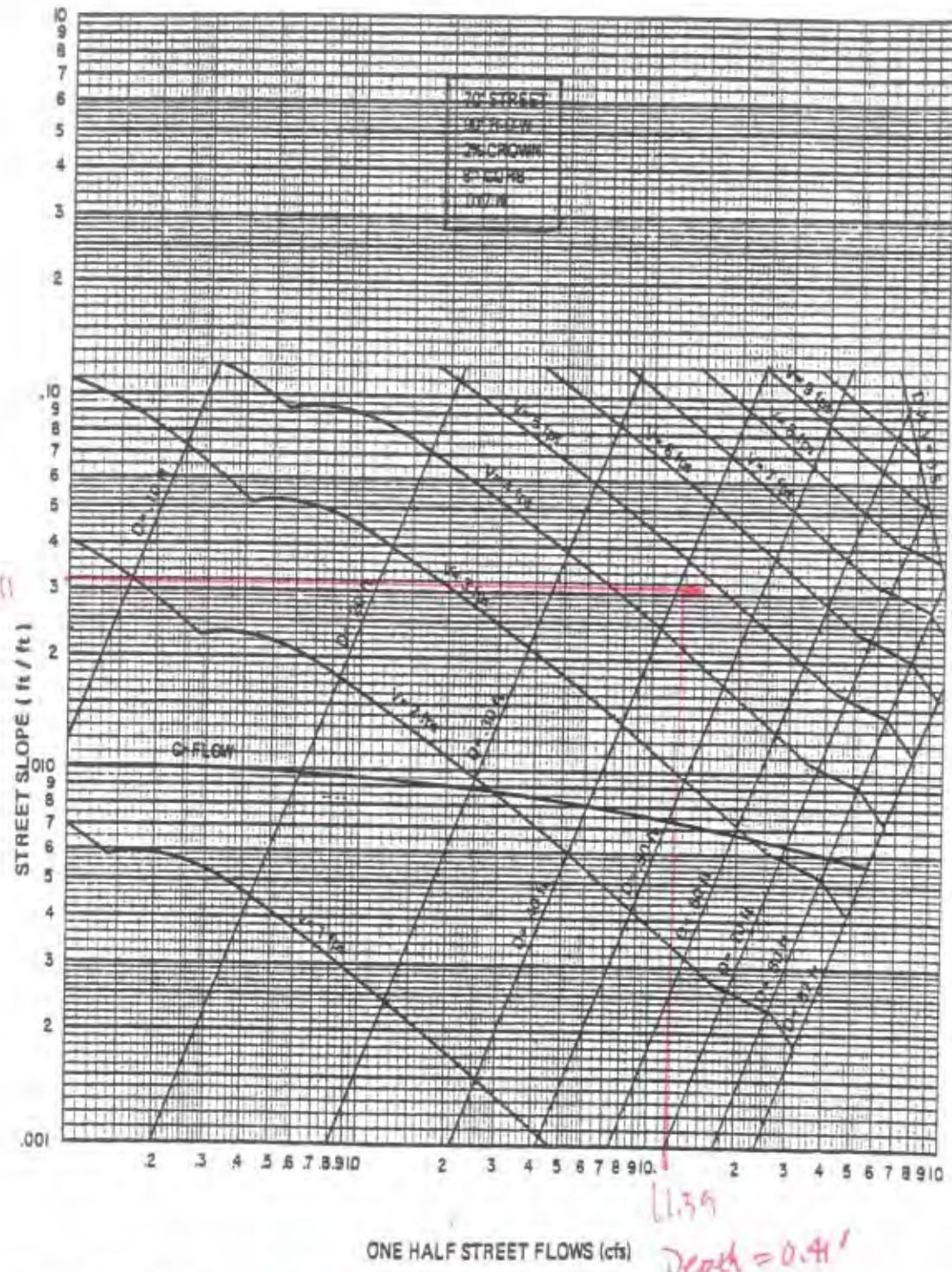


PLATE 22.3 D-4

BRAIN 117.326
 $b - \alpha = 11.39085$
 $s = 3.110$

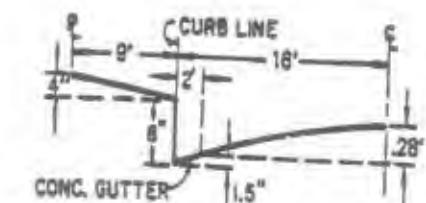
June 1997

22-142

GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION
(ABOVE BASIN)

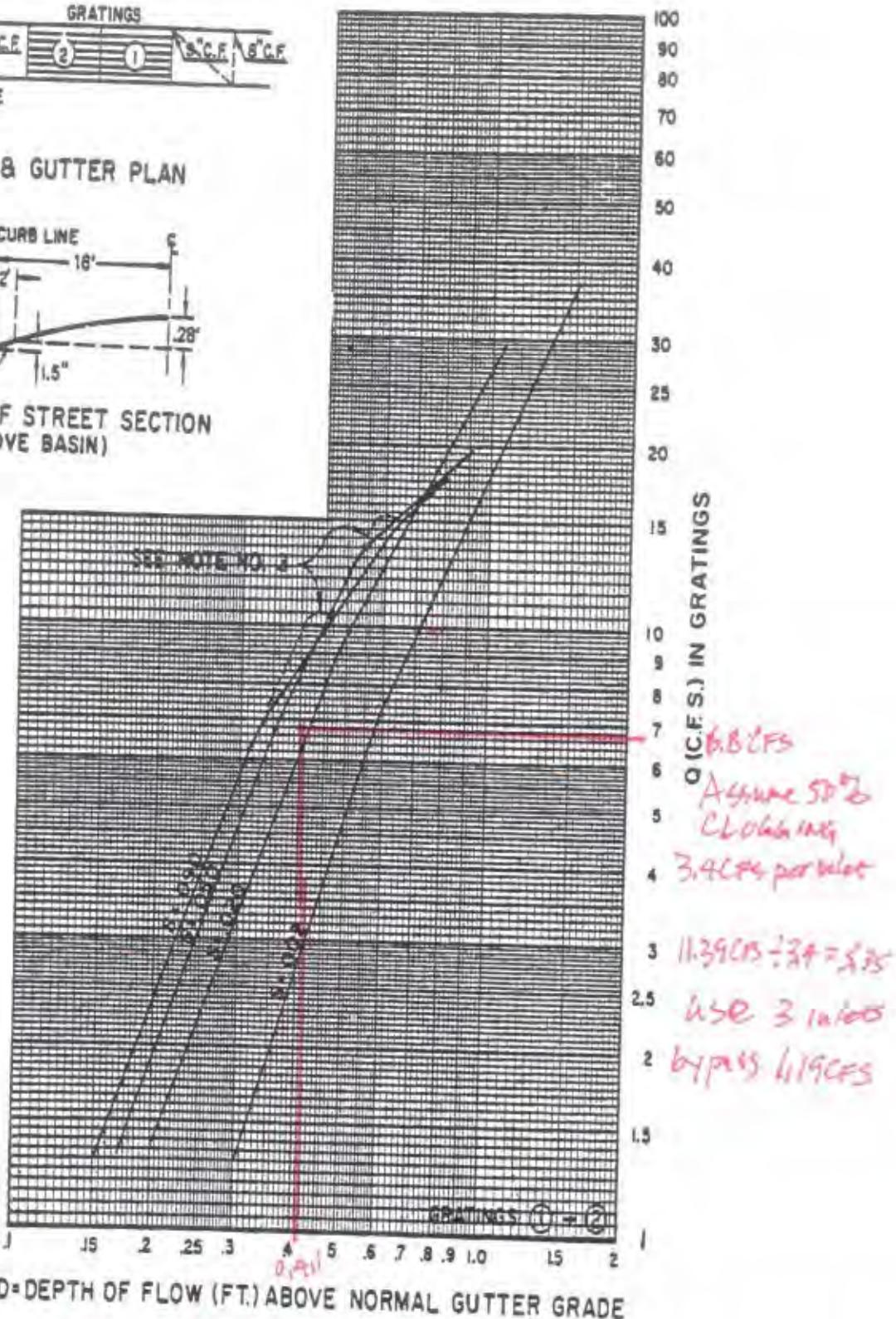


PLATE 22.3 D-6

11.39 CFS

STREET CAPACITY

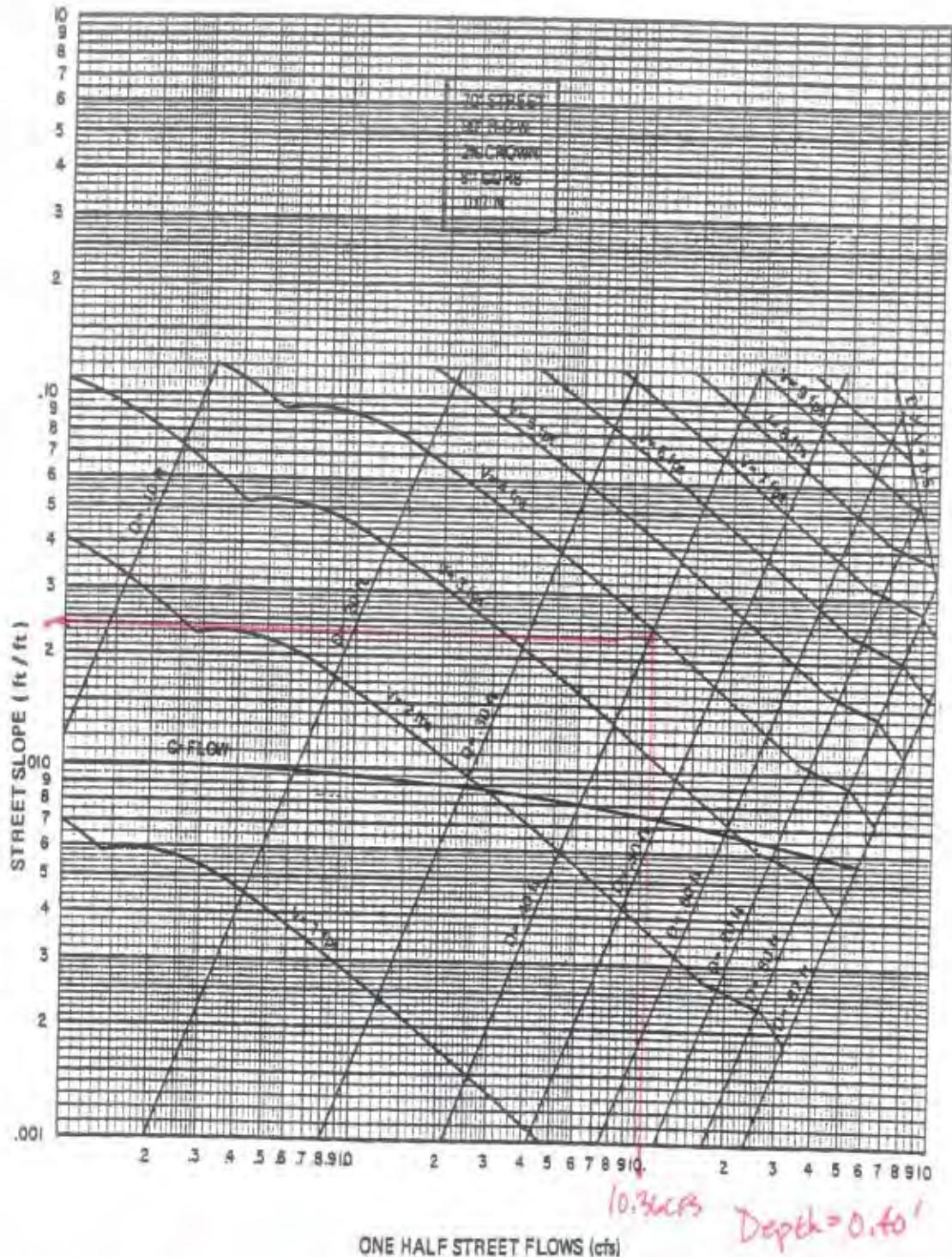


PLATE 22.3 D-4

BASIN 117,327 bypass from 117,326

$$\frac{1}{2} \alpha = 9.17 \text{ cfs} + 1.19 \text{ cfs} = 10.36 \text{ cfs}$$

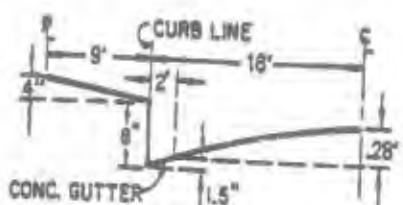
$$S = 2.40\%$$

June 1997

GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION
(ABOVE BASIN)

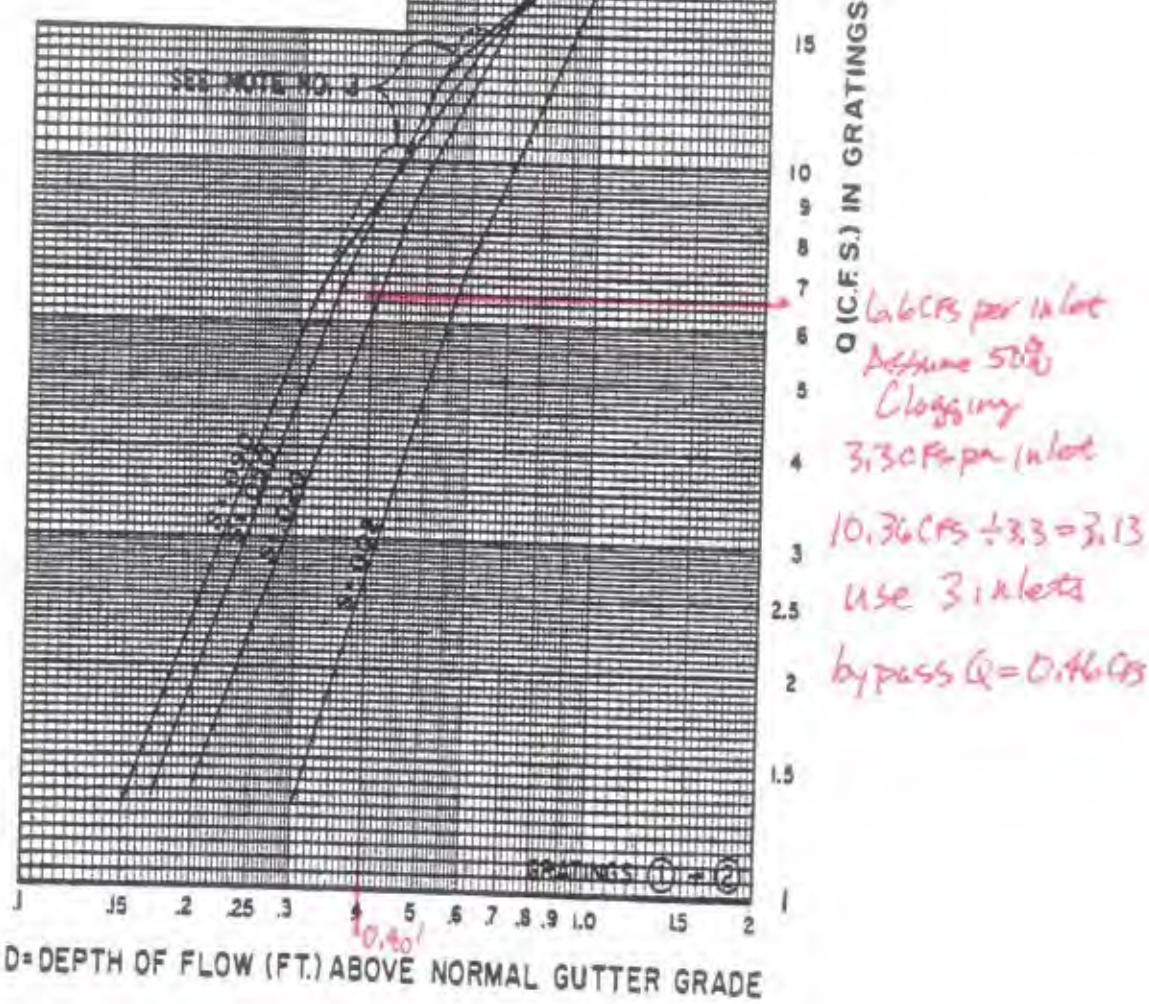


PLATE 22.3 D-6

BASIN 117.327

STREET CAPACITY

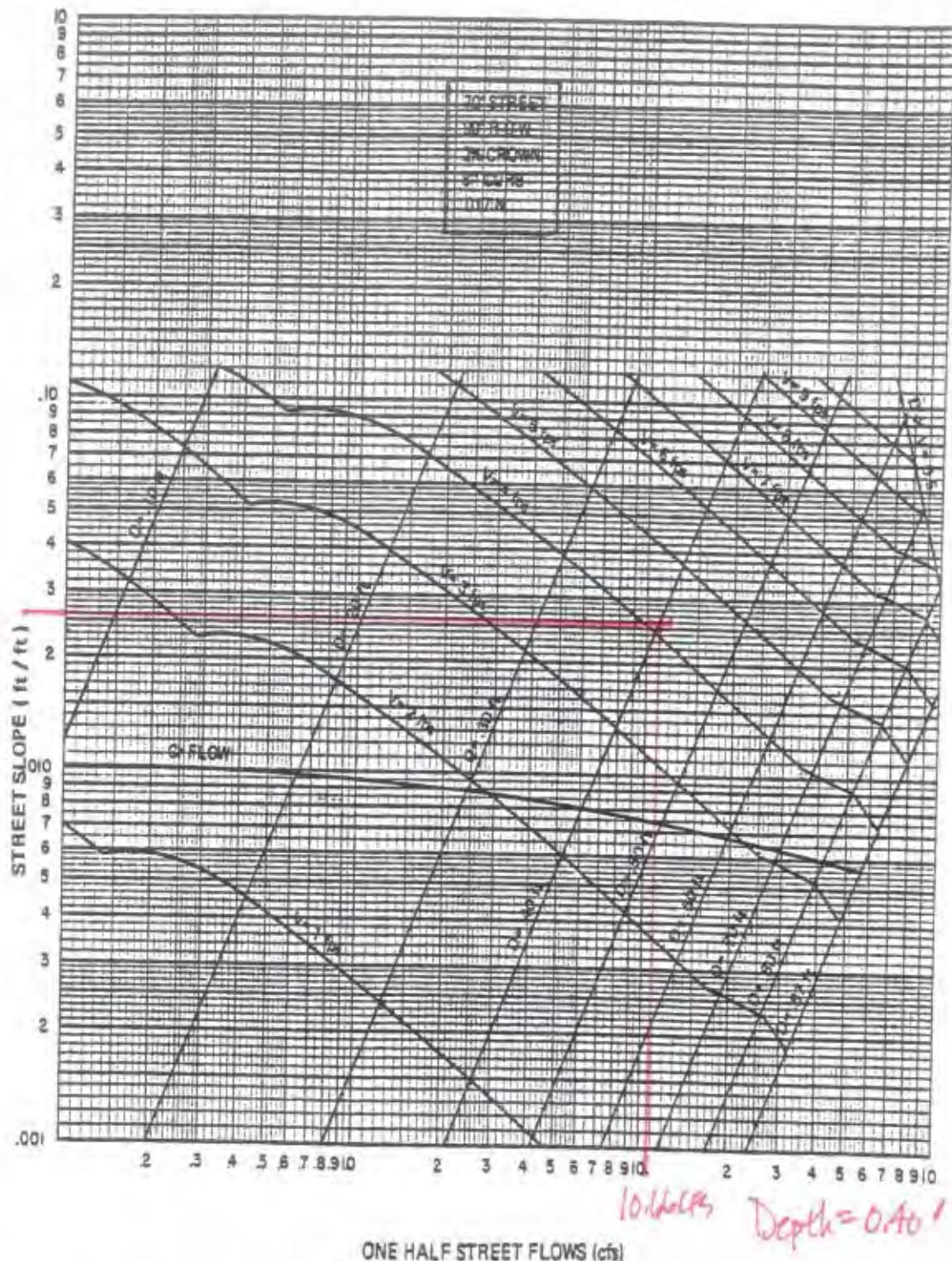


PLATE 22.3 D-4

BASIN 117,328 bypass Q from 117,327

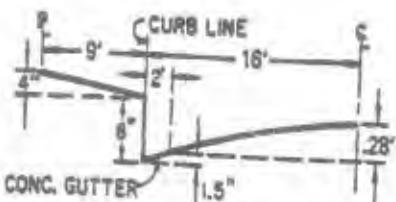
$$V = 10.20 \text{ CPS} + 0.46 \text{ CPS} = 10.66 \text{ CPS}$$

$$\epsilon = 2.61\%$$

GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION
(ABOVE BASIN)

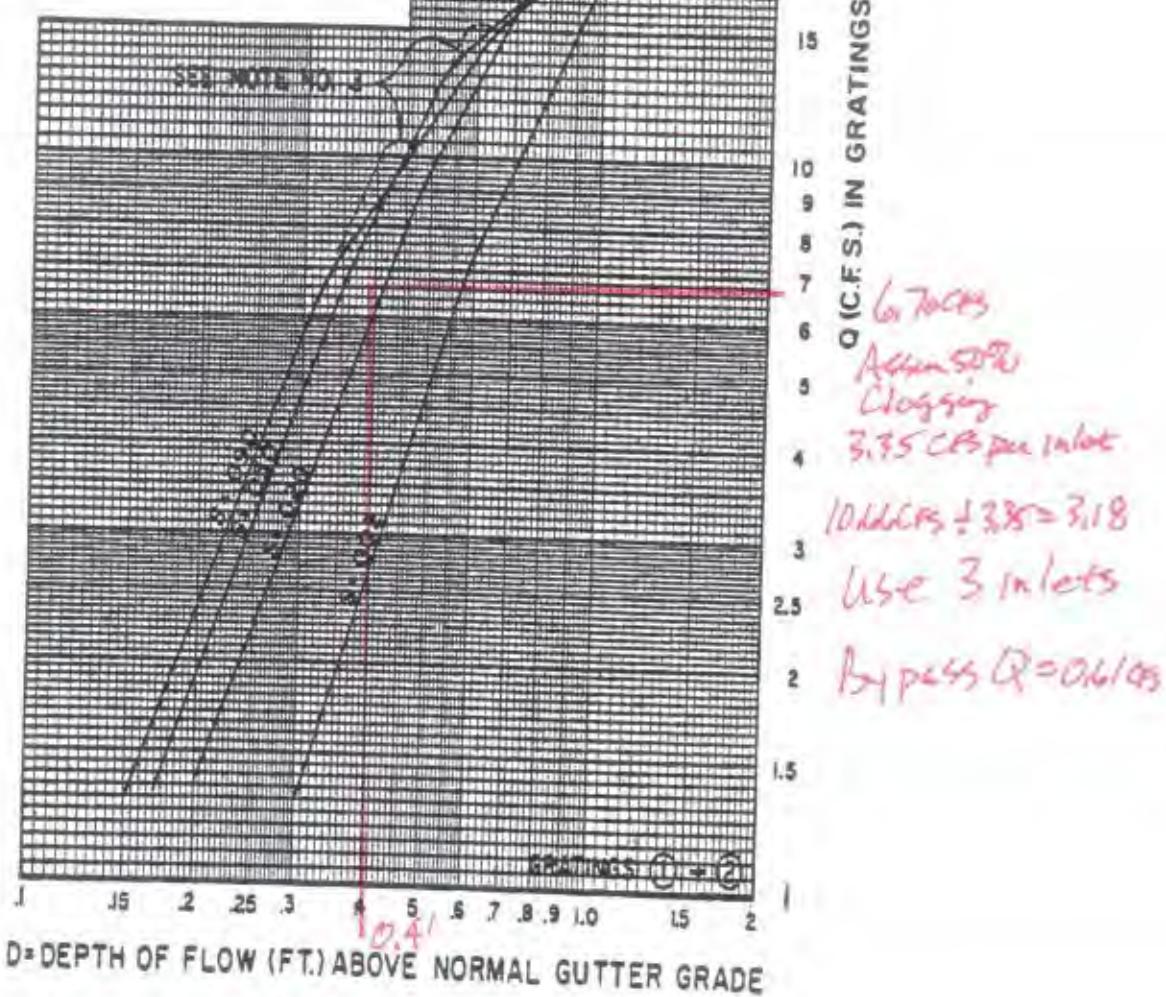


PLATE 22.3 D-6

BASIN 117.328

STREET CAPACITY

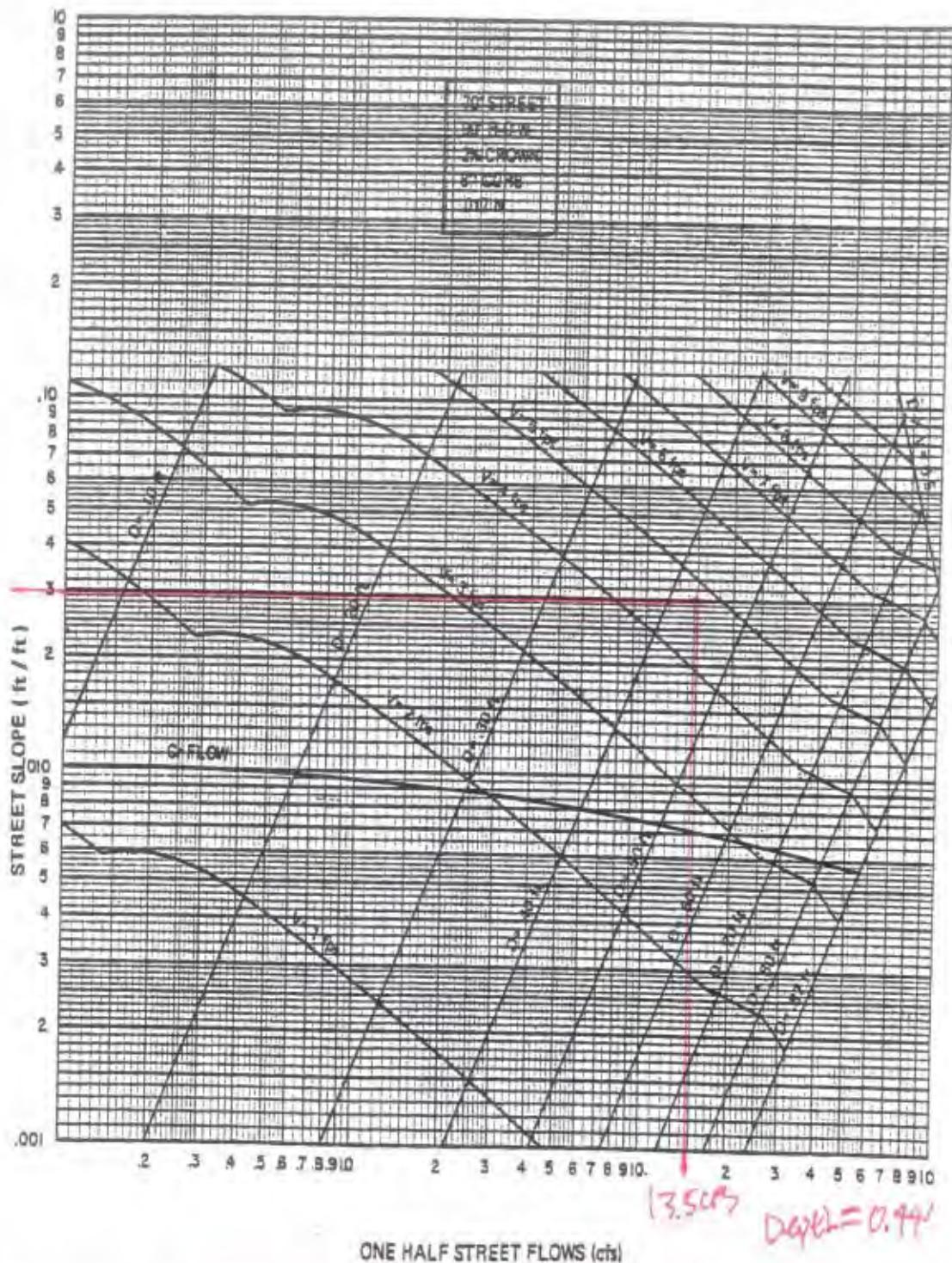


PLATE 22.3 D-4

BASIN 117.3209

bypass Q 117.328

$$\frac{1}{2}Q = 12.88 \text{ cfs} + 0.61 \text{ cfs} = 13.49 \text{ cfs}$$

$$S = 3.0\%$$

GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN

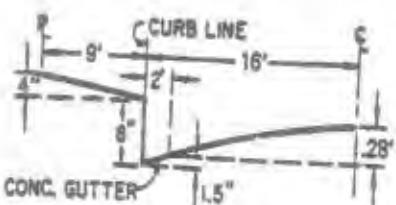
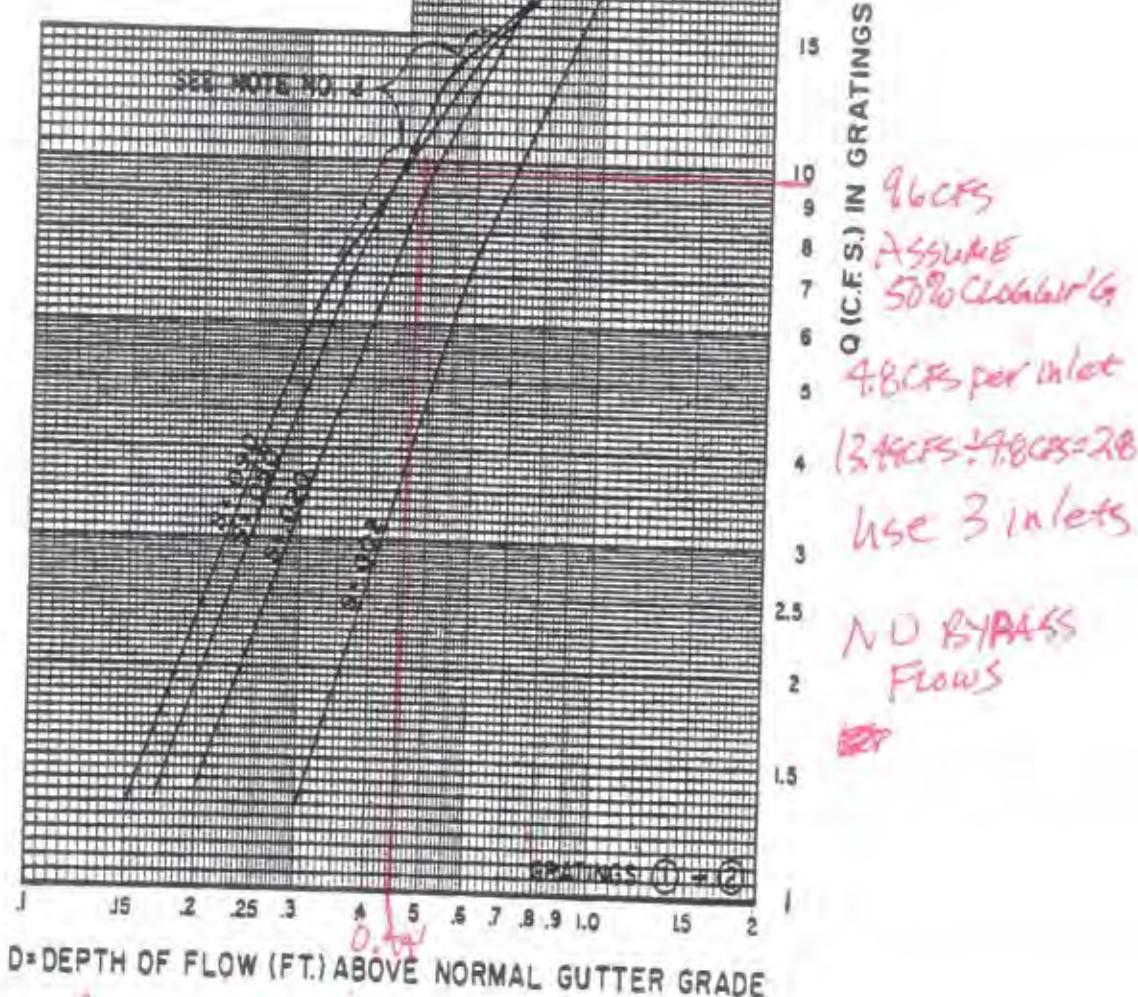
TYPICAL HALF STREET SECTION
(ABOVE BASIN)

PLATE 22.3 D-6

BASIN 117.32

SUMMARY OF HYDRAULIC CALCULATIONS																			BY:	DBT					
CLOSED CONDUIT																			DATE:	1/10/12	SHEET:	1 of 1			
PROJECT: ALAMEDA FROM SAN PEDRO TO EAST OF LOUISIANA AND LOUISIANA FROM SIGNAL TO ALAMEDA																									
100 year																									
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23			
										JUNCTION	LOSSES														
STATION	STRUCT	D	Q	A	V	K	Sf	L	DELTA	Q	D	ANGLE	hf	hb	Aavg	hj	hmh	ht	hmisc	SUM	E.G.	hv	H.G.	GROUND ELEV.	
10+23.88	WYE												0.00											5228.70	
		60	252	19.64	12.83	2606	0.0094	19					0.18											5230.00	
10+44.56	BEND									45				0.36	19.64	0.00	0.13	0.00		0.49	5231.92	2.56	5229.37		5230.00
		60	252	19.64	12.83	2606	0.0094	56					0.52											5232.45	
11+00	MH									27	24	80		0.00	17.77	0.02	0.00	0.00		0.02	5232.47	3.11	5229.36		5231.50
		54	225	15.90	14.15	1967.6	0.0131	450					5.88											5238.35	
15+50	MH													0.00	15.90	0.00	0.16	0.00		0.16	5238.51	3.11	5235.40		5244.00
		54	225	15.90	14.15	1967.6	0.0131	0					0.00												
REMARKS: BETWEEN STATION 11+00 AND 15+50 HGL BECOMES NON-PRESSURE										Manning's n: 0.013															
AND CONTINUES UNDER GRAVITY FLOW CONDITIONS																									

Circular Pipe Flow						
Diameter (ft..in)	4.00	48	Alameda Boulevard	Station 15+50 to Station 20+00		
Slope	0.0289	ft/ft				
Manning's N	0.013					
Percent full	70%					
Depth	2.81	ft				
theta	3.97					
Area	9.42	sf				
Wetted Perimeter	7.94	ft				
Surface Width	3.661	ft				
Q	205.02	cfs				
V	21.77	fps				
Depth	theta	A	T	Q	V	
0.20	0.90	0.23	1.80	1.74	1.17	4.99
0.40	1.29	0.65	2.57	2.40	5.10	7.80
0.60	1.59	1.18	3.18	2.86	11.87	10.04
0.80	1.85	1.79	3.71	3.20	21.38	11.95
1.00	2.09	2.46	4.19	3.46	33.45	13.62
1.20	2.32	3.17	4.64	3.67	47.82	15.08
1.40	2.53	3.92	5.06	3.82	64.21	16.38
1.60	2.74	4.69	5.48	3.92	82.29	17.53
1.80	2.94	5.48	5.88	3.98	101.71	18.55
2.00	3.14	6.28	6.28	4.00	122.10	19.43
2.20	3.34	7.08	6.68	3.98	143.03	20.20
2.40	3.54	7.87	7.09	3.92	164.06	20.84
2.60	3.75	8.65	7.50	3.82	184.71	21.36
2.80	3.96	9.40	7.93	3.67	204.45	21.76
3.00	4.19	10.11	8.38	3.46	222.67	22.03
3.20	4.43	10.78	8.86	3.20	238.69	22.15
3.40	4.69	11.38	9.38	2.86	251.63	22.10
3.60	5.00	11.91	9.99	2.40	260.26	21.85
3.80	5.38	12.33	10.76	1.74	262.39	21.28
4.00	6.28	12.57	12.57	0.00	244.19	19.43
						Full

Circular Pipe Flow						
Diameter (ft..in)	4.00	48	Alameda Boulevard	Station 20+00 to Station 24+50		
Slope	0.0261	ft/ft				
Manning's N	0.013					
Percent full	68%					
Depth	2.70	ft				
theta	3.86					
Area	9.03	sf				
Wetted Perimeter	7.72	ft				
Surface Width	3.746	ft				
Q	185.21	cfs				
V	20.51	fps				
Depth	theta	A	T	Q	V	
0.20	0.90	0.23	1.80	1.74	1.11	4.74
0.40	1.29	0.65	2.57	2.40	4.84	7.41
0.60	1.59	1.18	3.18	2.86	11.28	9.54
0.80	1.85	1.79	3.71	3.20	20.32	11.36
1.00	2.09	2.46	4.19	3.46	31.79	12.94
1.20	2.32	3.17	4.64	3.67	45.45	14.33
1.40	2.53	3.92	5.06	3.82	61.02	15.57
1.60	2.74	4.69	5.48	3.92	78.20	16.66
1.80	2.94	5.48	5.88	3.98	96.66	17.62
2.00	3.14	6.28	6.28	4.00	116.03	18.47
2.20	3.34	7.08	6.68	3.98	135.92	19.19
2.40	3.54	7.87	7.09	3.92	155.91	19.80
2.60	3.75	8.65	7.50	3.82	175.53	20.30
2.80	3.96	9.40	7.93	3.67	194.29	20.68
3.00	4.19	10.11	8.38	3.46	211.61	20.93
3.20	4.43	10.78	8.86	3.20	226.83	21.05
3.40	4.69	11.38	9.38	2.86	239.13	21.00
3.60	5.00	11.91	9.99	2.40	247.33	20.76
3.80	5.38	12.33	10.76	1.74	249.35	20.22
4.00	6.28	12.57	12.57	0.00	232.06	18.47 Full

Circular Pipe Flow						
Diameter (ft..in)	3.50	42	Alameda Boulevard Station 24+50 to Station 27+10			
Slope	0.0285	ft/ft				
Manning's N	0.013					
Percent full	80%					
Depth	2.78	ft				
theta	4.41					
Area	8.21	sf				
Wetted Perimeter	7.71	ft				
Surface Width	2.823	ft				
Q	165.10	cfs				
V	20.12	fps				
Depth	theta	A	T	Q	V	
0.18	0.90	0.18	1.58	1.53	0.82	4.54
0.35	1.29	0.50	2.25	2.10	3.55	7.08
0.53	1.59	0.90	2.78	2.50	8.26	9.12
0.70	1.85	1.37	3.25	2.80	14.87	10.86
0.88	2.09	1.88	3.67	3.03	23.27	12.37
1.05	2.32	2.43	4.06	3.21	33.26	13.70
1.23	2.53	3.00	4.43	3.34	44.66	14.88
1.40	2.74	3.59	4.79	3.43	57.24	15.93
1.58	2.94	4.20	5.15	3.48	70.75	16.85
1.75	3.14	4.81	5.50	3.50	84.92	17.65
1.93	3.34	5.42	5.85	3.48	99.48	18.35
2.10	3.54	6.03	6.20	3.43	114.11	18.93
2.28	3.75	6.62	6.56	3.34	128.48	19.41
2.45	3.96	7.19	6.94	3.21	142.20	19.77
2.63	4.19	7.74	7.33	3.03	154.88	20.01
2.80	4.43	8.25	7.75	2.80	166.02	20.12
2.98	4.69	8.72	8.21	2.50	175.02	20.08
3.15	5.00	9.12	8.74	2.10	181.02	19.85
3.33	5.38	9.44	9.42	1.53	182.51	19.33
3.50	6.28	9.62	11.00	0.00	169.85	17.65
						Full

Circular Pipe Flow						
Diameter (ft..in)	3.50	42	Alameda Boulevard Station 27+10 to Station 29+00			
Slope	0.0283	ft/ft				
Manning's N	0.013					
Percent full	77%					
Depth	2.71	ft				
theta	4.30					
Area	7.99	sf				
Wetted Perimeter	7.52	ft				
Surface Width	2.930	ft				
Q	159.80	cfs				
V	20.01	fps				
Depth	theta	A	T	Q	V	
0.18	0.90	0.18	1.58	1.53	0.81	4.52
0.35	1.29	0.50	2.25	2.10	3.53	7.06
0.53	1.59	0.90	2.78	2.50	8.23	9.09
0.70	1.85	1.37	3.25	2.80	14.82	10.82
0.88	2.09	1.88	3.67	3.03	23.18	12.33
1.05	2.32	2.43	4.06	3.21	33.14	13.65
1.23	2.53	3.00	4.43	3.34	44.50	14.83
1.40	2.74	3.59	4.79	3.43	57.04	15.87
1.58	2.94	4.20	5.15	3.48	70.50	16.79
1.75	3.14	4.81	5.50	3.50	84.63	17.59
1.93	3.34	5.42	5.85	3.48	99.13	18.28
2.10	3.54	6.03	6.20	3.43	113.71	18.87
2.28	3.75	6.62	6.56	3.34	128.02	19.34
2.45	3.96	7.19	6.94	3.21	141.70	19.70
2.63	4.19	7.74	7.33	3.03	154.34	19.94
2.80	4.43	8.25	7.75	2.80	165.44	20.05
2.98	4.69	8.72	8.21	2.50	174.40	20.01
3.15	5.00	9.12	8.74	2.10	180.39	19.78
3.33	5.38	9.44	9.42	1.53	181.86	19.26
3.50	6.28	9.62	11.00	0.00	169.25	17.59
						Full

Circular Pipe Flow						
Diameter (ft..in)	3.50	42	Alameda Boulevard		Station 29+00 to Station 29+80	
Slope	0.0294	ft/ft				
Manning's N	0.013					
Percent full	73%					
Depth	2.56	ft				
theta	4.11					
Area	7.55	sf				
Wetted Perimeter	7.19	ft				
Surface Width	3.098	ft				
Q	153.00	cfs				
V	20.25	fps				
Depth	theta	A	T	Q	V	
0.18	0.90	0.18	1.58	1.53	0.83	4.61
0.35	1.29	0.50	2.25	2.10	3.60	7.19
0.53	1.59	0.90	2.78	2.50	8.39	9.27
0.70	1.85	1.37	3.25	2.80	15.11	11.03
0.88	2.09	1.88	3.67	3.03	23.63	12.56
1.05	2.32	2.43	4.06	3.21	33.78	13.92
1.23	2.53	3.00	4.43	3.34	45.36	15.11
1.40	2.74	3.59	4.79	3.43	58.13	16.18
1.58	2.94	4.20	5.15	3.48	71.86	17.11
1.75	3.14	4.81	5.50	3.50	86.25	17.93
1.93	3.34	5.42	5.85	3.48	101.04	18.64
2.10	3.54	6.03	6.20	3.43	115.90	19.23
2.28	3.75	6.62	6.56	3.34	130.49	19.71
2.45	3.96	7.19	6.94	3.21	144.43	20.08
2.63	4.19	7.74	7.33	3.03	157.31	20.32
2.80	4.43	8.25	7.75	2.80	168.62	20.44
2.98	4.69	8.72	8.21	2.50	177.76	20.39
3.15	5.00	9.12	8.74	2.10	183.86	20.16
3.33	5.38	9.44	9.42	1.53	185.36	19.63
3.50	6.28	9.62	11.00	0.00	172.51	17.93
						Full

Circular Pipe Flow						
Diameter (ft..in)	3.50	42	Alameda Boulevard		Station 29+80 to Station 31+45	
Slope	0.0294	ft/ft				
Manning's N	0.013					
Percent full	69%					
Depth	2.43	ft				
theta	3.94					
Area	7.13	sf				
Wetted Perimeter	6.89	ft				
Surface Width	3.226	ft				
Q	142.81	cfs				
V	20.04	fps				
Depth	theta	A	T	Q	V	
0.18	0.90	0.18	1.58	1.53	0.83	4.61
0.35	1.29	0.50	2.25	2.10	3.60	7.19
0.53	1.59	0.90	2.78	2.50	8.39	9.27
0.70	1.85	1.37	3.25	2.80	15.11	11.03
0.88	2.09	1.88	3.67	3.03	23.63	12.56
1.05	2.32	2.43	4.06	3.21	33.78	13.92
1.23	2.53	3.00	4.43	3.34	45.36	15.11
1.40	2.74	3.59	4.79	3.43	58.13	16.18
1.58	2.94	4.20	5.15	3.48	71.86	17.11
1.75	3.14	4.81	5.50	3.50	86.25	17.93
1.93	3.34	5.42	5.85	3.48	101.04	18.64
2.10	3.54	6.03	6.20	3.43	115.90	19.23
2.28	3.75	6.62	6.56	3.34	130.49	19.71
2.45	3.96	7.19	6.94	3.21	144.43	20.08
2.63	4.19	7.74	7.33	3.03	157.31	20.32
2.80	4.43	8.25	7.75	2.80	168.62	20.44
2.98	4.69	8.72	8.21	2.50	177.76	20.39
3.15	5.00	9.12	8.74	2.10	183.86	20.16
3.33	5.38	9.44	9.42	1.53	185.36	19.63
3.50	6.28	9.62	11.00	0.00	172.51	17.93
						Full

Circular Pipe Flow						
Diameter (ft..in)	3.50	42	Alameda Boulevard	Station 31+45 to Station 33+50		
Slope	0.0218	ft/ft				
Manning's N	0.013					
Percent full	74%					
Depth	2.59	ft				
theta	4.15					
Area	7.64	sf				
Wetted Perimeter	7.26	ft				
Surface Width	3.067	ft				
Q	133.51	cfs				
V	17.47	fps				
Depth	theta	A	T	Q	V	
0.18	0.90	0.18	1.58	1.53	0.71	3.97
0.35	1.29	0.50	2.25	2.10	3.10	6.19
0.53	1.59	0.90	2.78	2.50	7.22	7.98
0.70	1.85	1.37	3.25	2.80	13.01	9.50
0.88	2.09	1.88	3.67	3.03	20.35	10.82
1.05	2.32	2.43	4.06	3.21	29.09	11.98
1.23	2.53	3.00	4.43	3.34	39.06	13.02
1.40	2.74	3.59	4.79	3.43	50.06	13.93
1.58	2.94	4.20	5.15	3.48	61.87	14.74
1.75	3.14	4.81	5.50	3.50	74.27	15.44
1.93	3.34	5.42	5.85	3.48	87.01	16.05
2.10	3.54	6.03	6.20	3.43	99.80	16.56
2.28	3.75	6.62	6.56	3.34	112.36	16.97
2.45	3.96	7.19	6.94	3.21	124.37	17.29
2.63	4.19	7.74	7.33	3.03	135.46	17.50
2.80	4.43	8.25	7.75	2.80	145.20	17.60
2.98	4.69	8.72	8.21	2.50	153.07	17.56
3.15	5.00	9.12	8.74	2.10	158.32	17.36
3.33	5.38	9.44	9.42	1.53	159.62	16.91
3.50	6.28	9.62	11.00	0.00	148.55	15.44
						Full

Circular Pipe Flow						
Diameter (ft..in)	3.50	42	Alameda Boulevard	Station 33+50 to Station 36+67		
Slope	0.0210	ft/ft				
Manning's N	0.013					
Percent full	75%					
Depth	2.63	ft				
theta	4.20					
Area	7.77	sf				
Wetted Perimeter	7.35	ft				
Surface Width	3.020	ft				
Q	133.50	cfs				
V	17.18	fps				
Depth	theta	A	T	Q	V	
0.18	0.90	0.18	1.58	1.53	0.70	3.89
0.35	1.29	0.50	2.25	2.10	3.04	6.08
0.53	1.59	0.90	2.78	2.50	7.09	7.83
0.70	1.85	1.37	3.25	2.80	12.77	9.32
0.88	2.09	1.88	3.67	3.03	19.97	10.62
1.05	2.32	2.43	4.06	3.21	28.55	11.76
1.23	2.53	3.00	4.43	3.34	38.34	12.77
1.40	2.74	3.59	4.79	3.43	49.13	13.67
1.58	2.94	4.20	5.15	3.48	60.73	14.46
1.75	3.14	4.81	5.50	3.50	72.90	15.15
1.93	3.34	5.42	5.85	3.48	85.40	15.75
2.10	3.54	6.03	6.20	3.43	97.95	16.25
2.28	3.75	6.62	6.56	3.34	110.28	16.66
2.45	3.96	7.19	6.94	3.21	122.07	16.97
2.63	4.19	7.74	7.33	3.03	132.95	17.18
2.80	4.43	8.25	7.75	2.80	142.51	17.27
2.98	4.69	8.72	8.21	2.50	150.24	17.24
3.15	5.00	9.12	8.74	2.10	155.39	17.04
3.33	5.38	9.44	9.42	1.53	156.66	16.59
3.50	6.28	9.62	11.00	0.00	145.80	15.15 Full

Circular Pipe Flow						
Diameter (ft..in)	3.00	36	Alameda Boulevard		Station 36+67 to Station 38+04	
Slope	0.0643	ft/ft				
Manning's N	0.013					
Percent full	45%					
Depth	1.36	ft				
theta	2.95					
Area	3.12	sf				
Wetted Perimeter	4.43	ft				
Surface Width	2.987	ft				
Q	71.39	cfs				
V	22.91	fps				
Depth	theta	A	T	Q	V	
0.15	0.90	0.13	1.35	1.31	0.81	6.15
0.30	1.29	0.37	1.93	1.80	3.53	9.60
0.45	1.59	0.66	2.39	2.14	8.22	12.37
0.60	1.85	1.01	2.78	2.40	14.81	14.72
0.75	2.09	1.38	3.14	2.60	23.17	16.76
0.90	2.32	1.78	3.48	2.75	33.12	18.57
1.05	2.53	2.20	3.80	2.86	44.47	20.17
1.20	2.74	2.64	4.11	2.94	56.99	21.59
1.35	2.94	3.09	4.41	2.98	70.45	22.84
1.50	3.14	3.53	4.71	3.00	84.57	23.93
1.65	3.34	3.98	5.01	2.98	99.06	24.87
1.80	3.54	4.43	5.32	2.94	113.63	25.66
1.95	3.75	4.86	5.63	2.86	127.93	26.30
2.10	3.96	5.29	5.95	2.75	141.60	26.79
2.25	4.19	5.69	6.28	2.60	154.23	27.12
2.40	4.43	6.06	6.64	2.40	165.32	27.27
2.55	4.69	6.40	7.04	2.14	174.28	27.22
2.70	5.00	6.70	7.49	1.80	180.26	26.90
2.85	5.38	6.94	8.07	1.31	181.73	26.20
3.00	6.28	7.07	9.42	0.00	169.13	23.93
						Full

Circular Pipe Flow						
Diameter (ft..in)	3.00	36	Alameda Boulevard			
Slope	0.0254	ft/ft	Station 38+10 to Station 40+77			
Manning's N	0.013					
Percent full	56%					
Depth	1.67	ft				
theta	3.36					
Area	4.03	sf				
Wetted Perimeter	5.04	ft				
Surface Width	2.982	ft				
Q	63.18	cfs				
V	15.68	fps				
Depth	theta	A	T	Q	V	
0.15	0.90	0.13	1.35	1.31	0.51	3.86
0.30	1.29	0.37	1.93	1.80	2.22	6.03
0.45	1.59	0.66	2.39	2.14	5.17	7.77
0.60	1.85	1.01	2.78	2.40	9.31	9.25
0.75	2.09	1.38	3.14	2.60	14.56	10.54
0.90	2.32	1.78	3.48	2.75	20.82	11.67
1.05	2.53	2.20	3.80	2.86	27.95	12.68
1.20	2.74	2.64	4.11	2.94	35.82	13.57
1.35	2.94	3.09	4.41	2.98	44.28	14.35
1.50	3.14	3.53	4.71	3.00	53.15	15.04
1.65	3.34	3.98	5.01	2.98	62.26	15.63
1.80	3.54	4.43	5.32	2.94	71.42	16.13
1.95	3.75	4.86	5.63	2.86	80.41	16.53
2.10	3.96	5.29	5.95	2.75	89.00	16.84
2.25	4.19	5.69	6.28	2.60	96.93	17.05
2.40	4.43	6.06	6.64	2.40	103.90	17.14
2.55	4.69	6.40	7.04	2.14	109.54	17.11
2.70	5.00	6.70	7.49	1.80	113.29	16.91
2.85	5.38	6.94	8.07	1.31	114.22	16.47
3.00	6.28	7.07	9.42	0.00	106.30	15.04 Full

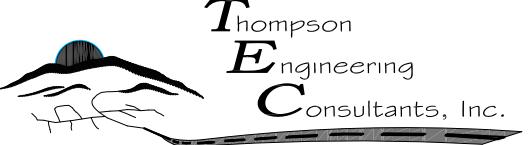
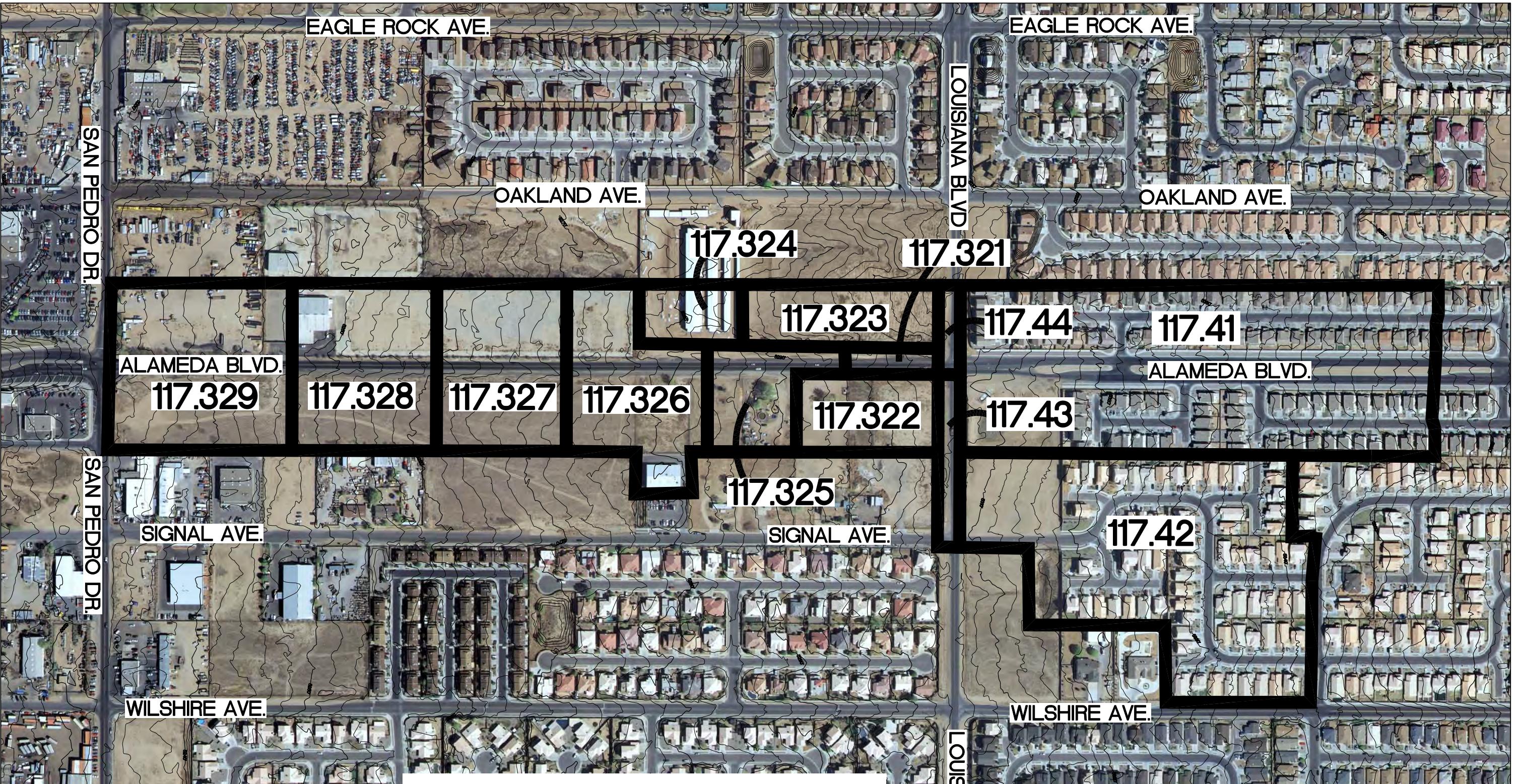
Circular Pipe Flow						
Diameter (ft..in)	3.00	36	Louisiana Boulevard	Station 11+10 to Station 12+74		
Slope	0.0080	ft/ft				
Manning's N	0.013					
Percent full	84%					
Depth	2.52	ft				
theta	4.64					
Area	6.34	sf				
Wetted Perimeter	6.95	ft				
Surface Width	2.201	ft				
Q	60.90	cfs				
V	9.61	fps				
Depth	theta	A	T	Q	V	
0.15	0.90	0.13	1.35	1.31	0.29	2.17
0.30	1.29	0.37	1.93	1.80	1.25	3.39
0.45	1.59	0.66	2.39	2.14	2.90	4.36
0.60	1.85	1.01	2.78	2.40	5.22	5.19
0.75	2.09	1.38	3.14	2.60	8.17	5.91
0.90	2.32	1.78	3.48	2.75	11.68	6.55
1.05	2.53	2.20	3.80	2.86	15.69	7.11
1.20	2.74	2.64	4.11	2.94	20.10	7.61
1.35	2.94	3.09	4.41	2.98	24.85	8.05
1.50	3.14	3.53	4.71	3.00	29.83	8.44
1.65	3.34	3.98	5.01	2.98	34.94	8.77
1.80	3.54	4.43	5.32	2.94	40.08	9.05
1.95	3.75	4.86	5.63	2.86	45.12	9.28
2.10	3.96	5.29	5.95	2.75	49.95	9.45
2.25	4.19	5.69	6.28	2.60	54.40	9.57
2.40	4.43	6.06	6.64	2.40	58.31	9.62
2.55	4.69	6.40	7.04	2.14	61.47	9.60
2.70	5.00	6.70	7.49	1.80	63.58	9.49
2.85	5.38	6.94	8.07	1.31	64.10	9.24
3.00	6.28	7.07	9.42	0.00	59.66	8.44
						Full

Circular Pipe Flow						
Diameter (ft..in)	3.00	36	Louisiana Boulevard	Station 7+54 to Station 11+10		
Slope	0.0065	ft/ft				
Manning's N	0.013					
Percent full	91%					
Depth	2.72	ft				
theta	5.05					
Area	6.74	sf				
Wetted Perimeter	7.58	ft				
Surface Width	1.734	ft				
Q	57.50	cfs				
V	8.53	fps				
Depth	theta	A	T	Q	V	
0.15	0.90	0.13	1.35	1.31	0.26	1.95
0.30	1.29	0.37	1.93	1.80	1.12	3.05
0.45	1.59	0.66	2.39	2.14	2.61	3.93
0.60	1.85	1.01	2.78	2.40	4.71	4.68
0.75	2.09	1.38	3.14	2.60	7.37	5.33
0.90	2.32	1.78	3.48	2.75	10.53	5.90
1.05	2.53	2.20	3.80	2.86	14.14	6.41
1.20	2.74	2.64	4.11	2.94	18.12	6.86
1.35	2.94	3.09	4.41	2.98	22.40	7.26
1.50	3.14	3.53	4.71	3.00	26.89	7.61
1.65	3.34	3.98	5.01	2.98	31.50	7.91
1.80	3.54	4.43	5.32	2.94	36.13	8.16
1.95	3.75	4.86	5.63	2.86	40.68	8.36
2.10	3.96	5.29	5.95	2.75	45.02	8.52
2.25	4.19	5.69	6.28	2.60	49.04	8.62
2.40	4.43	6.06	6.64	2.40	52.56	8.67
2.55	4.69	6.40	7.04	2.14	55.41	8.65
2.70	5.00	6.70	7.49	1.80	57.31	8.55
2.85	5.38	6.94	8.07	1.31	57.78	8.33
3.00	6.28	7.07	9.42	0.00	53.77	7.61 Full

Circular Pipe Flow						
Diameter (ft..in)	3.00	36	Louisiana Boulevard	Station 7+54 to Station 11+10		
Slope	0.0188	ft/ft				
Manning's N	0.013					
Percent full	58%					
Depth	1.73	ft				
theta	3.44					
Area	4.21	sf				
Wetted Perimeter	5.16	ft				
Surface Width	2.966	ft				
Q	57.51	cfs				
V	13.67	fps				
Depth	theta	A	T	Q	V	
0.15	0.90	0.13	1.35	1.31	0.44	3.32
0.30	1.29	0.37	1.93	1.80	1.91	5.19
0.45	1.59	0.66	2.39	2.14	4.45	6.69
0.60	1.85	1.01	2.78	2.40	8.01	7.96
0.75	2.09	1.38	3.14	2.60	12.53	9.07
0.90	2.32	1.78	3.48	2.75	17.91	10.04
1.05	2.53	2.20	3.80	2.86	24.05	10.91
1.20	2.74	2.64	4.11	2.94	30.82	11.67
1.35	2.94	3.09	4.41	2.98	38.09	12.35
1.50	3.14	3.53	4.71	3.00	45.73	12.94
1.65	3.34	3.98	5.01	2.98	53.56	13.45
1.80	3.54	4.43	5.32	2.94	61.44	13.87
1.95	3.75	4.86	5.63	2.86	69.18	14.22
2.10	3.96	5.29	5.95	2.75	76.57	14.49
2.25	4.19	5.69	6.28	2.60	83.39	14.66
2.40	4.43	6.06	6.64	2.40	89.39	14.75
2.55	4.69	6.40	7.04	2.14	94.24	14.72
2.70	5.00	6.70	7.49	1.80	97.47	14.55
2.85	5.38	6.94	8.07	1.31	98.27	14.17
3.00	6.28	7.07	9.42	0.00	91.45	12.94
						Full

Circular Pipe Flow						
Diameter (ft..in)	2.00	24	Louisiana Boulevard	Station 12+74 to Station 13+59		
Slope	0.0142	ft/ft				
Manning's N	0.013					
Percent full	15%					
Depth	0.30	ft				
theta	1.60					
Area	0.30	sf				
Wetted Perimeter	1.60	ft				
Surface Width	1.432	ft				
Q	1.33	cfs				
V	4.45	fps				
Depth	theta	A	T	Q	V	
0.10	0.90	0.06	0.90	0.87	0.13	2.20
0.20	1.29	0.16	1.29	1.20	0.56	3.44
0.30	1.59	0.30	1.59	1.43	1.31	4.43
0.40	1.85	0.45	1.85	1.60	2.36	5.28
0.50	2.09	0.61	2.09	1.73	3.69	6.01
0.60	2.32	0.79	2.32	1.83	5.28	6.66
0.70	2.53	0.98	2.53	1.91	7.09	7.23
0.80	2.74	1.17	2.74	1.96	9.08	7.74
0.90	2.94	1.37	2.94	1.99	11.23	8.19
1.00	3.14	1.57	3.14	2.00	13.48	8.58
1.10	3.34	1.77	3.34	1.99	15.79	8.92
1.20	3.54	1.97	3.54	1.96	18.11	9.20
1.30	3.75	2.16	3.75	1.91	20.39	9.43
1.40	3.96	2.35	3.96	1.83	22.57	9.61
1.50	4.19	2.53	4.19	1.73	24.58	9.73
1.60	4.43	2.69	4.43	1.60	26.35	9.78
1.70	4.69	2.85	4.69	1.43	27.78	9.76
1.80	5.00	2.98	5.00	1.20	28.73	9.65
1.90	5.38	3.08	5.38	0.87	28.97	9.40
2.00	6.28	3.14	6.28	0.00	26.96	8.58 Full

SUMMARY OF HYDRAULIC CALCULATIONS																	BY:						
CLOSED CONDUIT - HEAD LOSS AT MANHOLES																	DATE:						
PROJECT:	ALAMEDA FROM SAN PEDRO TO EAST OF LOUISIANA AND LOUISIANA FROM SIGNAL TO ALAMEDA																SHEET: 1 of 1						
100 year	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	21	23		
STATION	STRUCT	D	Q	A	V	K	SI	L	DELTA	Q	JUNCTION	LOSSES	hf	hb	Aavg	hj	hmh	ht	hmisc	SUM	hv	GROUND ELEV.	
15+50	MH																		0.00	0.00	7.36	5244.00	
		48	205	12.57	21.77	1437.2	0.0203	450											0.00	0.00	7.36		
20+00	MH										20	24	80		12.57	1.60	0.33	0.00	1.92	6.53	5257.00		
		48	185	12.57	20.51	1437.2	0.0166	450				20	24	80		11.09	1.27	0.31	0.00	1.58	6.29	5269.00	
24+50	MH																		0.00	0.00	6.29		
		42	165	9.62	20.12	1006.6	0.0269	260				5	24	80		9.62	0.38	0.31	0.00	0.69	6.22	5277.00	
27+10	MH																		0.00	0.00	6.22		
		42	160	9.62	20.01	1006.6	0.0253	190											0.00	0.00	6.22		
29+00	MH										7	24	80		9.62	0.32	0.32	0.00	0.64	6.37	5282.00		
		42	153	9.62	20.25	1006.6	0.0231	80											0.00	0.00	6.37		
29+80	MH										10	24	80		9.62	0.73	0.31	0.00	1.04	6.24	5284.00		
		42	143	9.62	20.04	1006.6	0.0202	165											0.00	0.00	6.24		
31+45	MH										9	24	80		9.62	1.68	0.24	0.00	1.92	4.74	5290.00		
		42	134	9.62	17.47	1006.6	0.0177	205											0.00	0.00	4.74		
33+50	MH										0				9.62	0.00	0.23	0.00	0.23	4.58	5298.00		
		42	134	9.62	17.18	1006.6	0.0177	318											0.00	0.00	4.58		
36+67	MH										63	36	90		8.34	2.51	0.41	0.00	2.92	8.15	5307.00		
		36	71	7.07	22.91	667.28	0.0113	137											0.00	0.00	8.15		
38+04	MH										8	24	90		7.07	2.56	0.21	0.00	2.77	4.27	5311.00		
		36	63	7.07	16.58	667.28	0.0089	267											0.00	0.00	4.27		
																					5307.00		
12+75	MH													0.00					0.00	0.00	1.43		
		36	60.9	7.07	9.61	667.28	0.0083	164											0.00	0.00	1.43		
11+10	MH										3.4	24	80		0.00	7.07	0.41	0.06	0.00	0.47	1.13	5306.00	
		36	57.5	7.07	8.53	667.28	0.0074	355											0.00	0.00	1.13		
7+55	MH										90	0			0.58	7.07	0.00	0.15	0.00	0.73	2.90	5309.00	
		36	57.5	7.07	13.67	667.28	0.0074	50											0.00	0.00	2.90		
7+05	MH										4.5				0.00	7.07	0.00	0.15	0.00	0.15	2.90	5310.00	
		36	53	7.07	13.67	667.28	0.0063	0											0.00	0.00	2.90		
0+00	MH										53				0.00	3.53	0.00	0.00	-0.58	-0.58	0.00		
REMARKS:													Manning's n: 0.013										



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BASIN	AREA	Q_{100}	BASIN	AREA	Q_{100}
117.321	0.54 AC	2.06 CFS	117.328	5.34 AC	20.40 CFS
117.322	2.44 AC	9.32 CFS	117.329	6.74 AC	25.75 CFS
117.323	2.68 AC	10.24 CFS	117.41	17.75 AC	71.36 CFS
117.324	1.37 AC	5.23 CFS	117.42	14.29 AC	57.45 CFS
117.325	1.25 AC	4.77 CFS	117.43	0.85 AC	3.42 CFS
117.326	5.96 AC	22.77 CFS	117.44	0.43 AC	1.33 CFS
117.327	4.80 AC	18.34 CFS			

LOUISIANA BLVD.



SCALE: 1'-300'

**ALAMEDA BLVD.
PROJECT
C.O.A. PROJECT # 7663.91
BASIN EXHIBIT**