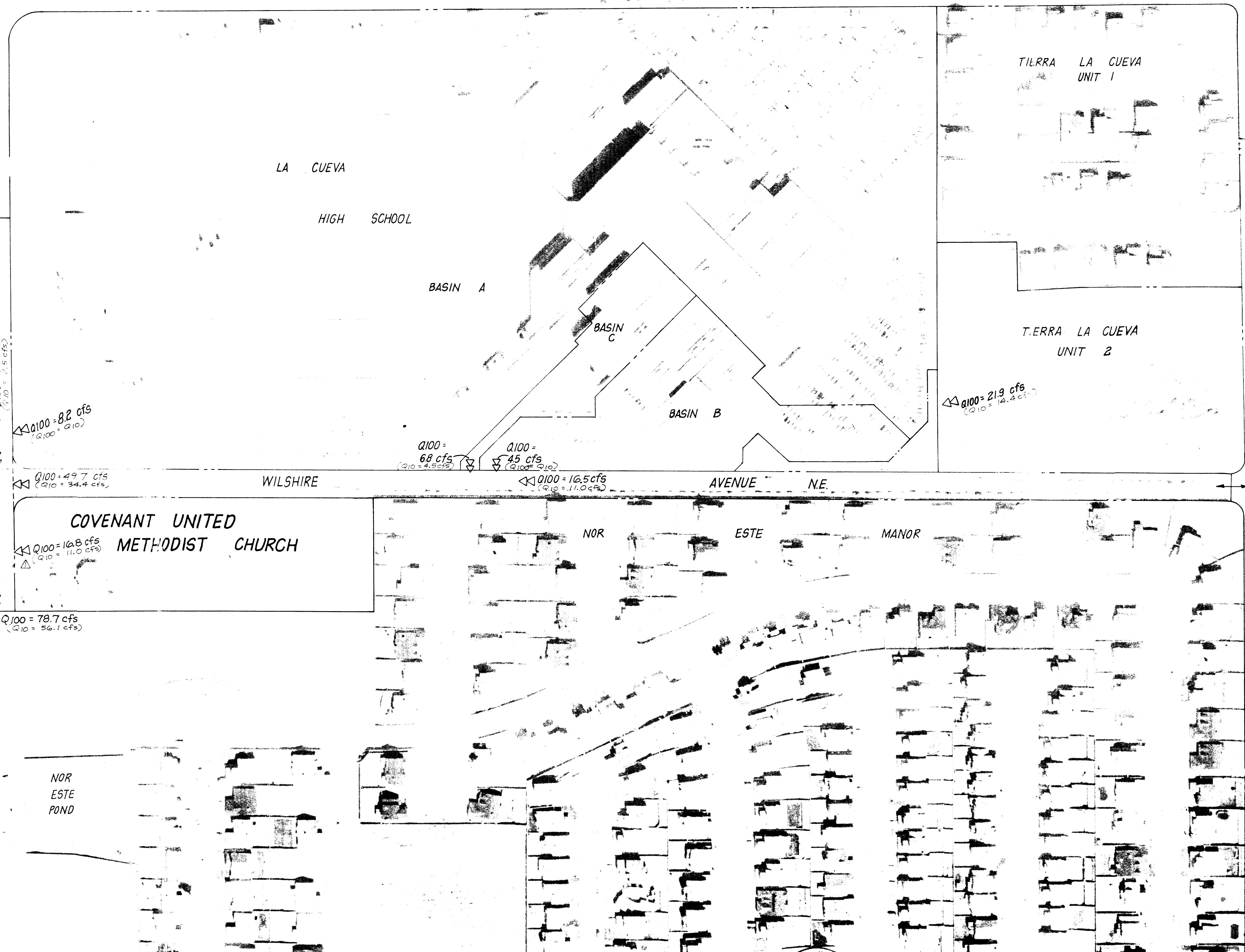


WYOMING BLVD. N.E.
Q100 = 12.2 cfs
Q100 = 4.0 cfs
Q100 = 8.2 cfs
Q100 = 61.9 cfs
Q100 = 78.7 cfs



WATERSHED MAP

COVENANT UNITED METHODIST CHURCH

Jma JEFF MORTENSEN & ASSOCIATES, INC.
6010-B MIDWAY PARK BLVD. N.E.
ALBUQUERQUE, NEW MEXICO 87109
ENGINEERS (505) 345-4250



DESIGNED BY	J.G.M.	DATE	06/93
DRAWN BY	T.P.H.	DATE	06/93
APPROVED BY	J.G.M.	DATE	06/93
PROJECT NO.		920412	
SHEET		1 OF 6	

DRAINAGE ANALYSIS

The following analysis has been prepared to determine the extent of public infrastructure required in conjunction with the development of the Covenant United Methodist Church. The required infrastructure for drainage is related to conformance with the Drainage Ordinance. Criteria as stated in the Development Process Manual are as follows:

a. "In the event of the 10-year design discharge (depth) may not exceed 0.5 feet in any collector or ARTERIAL street. One lane free of flowing or standing water in each traffic direction must be preserved on arterial streets."

b. "The product of depth times velocity (dv) shall not exceed 6.5 in any location of any street in the event of a 10-year design storm."

$$v = \text{fps}; d = \text{depth above gutter flowline.}$$

As shown on the Watershed Map, four drainage basins contribute runoff to Wilshire Avenue N.E., a local street. In addition, two drainage basins contribute runoff to Wyoming Boulevard N.E., a Principal Arterial. Because the tabulated discharge rates exceed the above referenced criteria for street flow, an underground storm drain system has been identified. As shown on the paving plan and profile sheets, street grades have been established and storm inlets located on both Wilshire Avenue N.E. and Wyoming Boulevard N.E. The storm drain will ultimately drain south to discharge to the North Arroyo de Domingo Baca. The gradient of storm drain piping has been established equal to the street gradient.

The calculations which appear hereon analyze the existing and developed conditions for the 100-year, 6-hour rainfall event. Where discharge rates and volumes have been previously identified, those values have been reprinted below. Where values did not presently exist, current calculations have been performed. Using the Procedure for 40 Acre and Smaller Basins set forth in the Revision of Section 22.2, Hydrology of the Development Process Manual, Volume 2, Design Criteria, dated August 1991, normal depth street flow has been calculated by the Manning Equation. For supercritical conditions, the sequent depth method has been used. Storm inlet grating capacities have been evaluated using the nomographs set forth in the DPM and reprinted hereon. Pipe flow capacities are calculated using the Manning Equation.

CALCULATIONS

I. HYDROLOGY

Site Characteristics

1.	Precipitation Zone	3
2.	$P_{6,100} = P_{360} =$	2.60
3.	Total Area (A_T)	
4.	Land Treatments	
a.	Tierra La Cueva - Unit 2 (refer to C19/D9A)	
b.	La Cueva High School (refer to C19/D1)	
c.	<u>Wilshire Avenue</u> ($A_T = 3.44$ Ac)	
	<u>Treatment</u>	<u>Area (sf/ac)</u>
C		32,500/0.74
D		117,500/2.70
d.	Wyoming Boulevard ($A_T = 0.98$ Ac)	
	<u>Treatment</u>	<u>Area (sf/ac)</u>
B		12,600/0.29
C		13,800/0.31
D		16,500/0.38
5.	Developed Land Treatment	
a.	Tierra La Cueva Unit 2 - No Change	
b.	La Cueva High School - No Change	
c.	<u>Wilshire Avenue</u>	
	<u>Treatment</u>	<u>Area (sf/ac)</u>
C		20,000/0.46
D		130,000/2.98
d.	Wyoming Avenue	
	<u>Treatment</u>	<u>Area (sf/ac)</u>
B		12,600/0.29
C		7,700/0.18
D		22,550/0.52

Existing Condition

A. Tierra La Cueva - Unit 2 (from C19/D9A)	
$V_{100} = 33,300$ cf	
$Q_{100} = 21.9$ cfs	
B. La Cueva High School (from C19/D1)	
1. Basin A	
$V_{100} = 166,670$ cf	
$Q_{100} = Q_{\text{release}} = 8.2$ cfs	
2. Basin B	
$V_{100} = 22,080$ cf	
$Q_{100} = Q_{\text{release}} = 4.5$ cfs	
3. Basin C	
$V_{100} = 11,750$ cf	
$Q_{100} = 6.8$ cfs	
C. Wilshire Avenue	
$E_w = [(1.29)(0.74) + (2.36)(2.70)]/3.44 = 2.13$ in	
$V_{100} = (E_w/12)A = 0.61$ ac. ft.	
$Q_{100} = 3.45(0.74) + 5.02(2.70) = 16.1$ cfs	
D. Wyoming Boulevard	
$E_w = [(0.92)(0.29) + (1.29)(0.31) + (2.36)(0.38)]/0.98 = 1.60$ in	
$V_{100} = (E_w/12)A = 0.13$ ac. ft.	
$Q_{100} = 2.60(0.29) + 3.45(0.31) + 5.02(0.38) = 3.7$ cfs	

Developed Condition

A. Tierra La Cueva - Unit 2 - No Change	
B. La Cueva High School - No Change	
C. Wilshire Avenue	
$E_w = [(1.29)(0.46) + (2.36)(2.98)]/3.44 = 2.22$ in	
$V_{100} = (2.22/12)(3.44) = 0.64$ ac.ft.	
$Q_{100} = 3.45(0.46) + 5.02(2.98) = 16.5$ cfs	
D. Wyoming Boulevard	
$E_w = [(0.92)(0.29) + (1.29)(0.18) + (2.36)(0.52)]/0.98 = 1.76$ in	
$V_{100} = (1.76/12)(0.98) = 0.14$ ac.ft.	
$Q_{100} = 2.60(0.29) + 3.45(0.18) + 5.02(0.52) = 4.0$ cfs	
E. Covenant United Methodist Church (Full Development) (From the Conceptual Plan)	
1. Basin A	
$V_{100} = 16,300$ cf	
$Q_{100} = 10.1$ cfs	
$V_{10 \text{ day}} = 30,150$ cf	
2. Basin B	
$V_{100} = 10,800$ cf	
$Q_{100} = 6.7$ cfs	
$V_{10 \text{ day}} = 20,040$ cf	

Comparison

A. Wilshire Avenue	
1. Volume	
$V_T, \text{Exist.} = 33,300 + 22,080 + 11,750 + 26,600 = 93,730$ cf	
$V_T, \text{Dev.} = 33,300 + 22,080 + 11,750 + 27,750 = 94,880$ cf	
$\Delta V_{100} = 94,880 - 93,730 = 1150$ cf (increase)	
2. Discharge	
$Q_T, \text{Exist.} = 21.9 + 4.5 + 6.8 + 16.1 = 49.3$ cfs	
$Q_T, \text{Dev.} = 21.9 + 4.5 + 6.8 + 16.5 = 49.7$ cfs	
$\Delta Q_{100} = 49.7 - 49.3 = 0.4$ cfs (increase)	
B. Wyoming Boulevard	
1. Volume	
$V_T, \text{Exist.} = 166,670 + 5,700 + 4,990 + 10,800 = 188,160$ cf	
$V_T, \text{Dev.} = 166,670 + 6,300 + 16,300 + 10,800 = 200,070$ cf	
$\Delta V_{100} = 200,070 - 188,160 = 11,910$ cf (increase)	
2. Discharge	
$Q_T, \text{Exist.} = 8.2 + 3.7 + 6.7 + 4.0 = 22.6$ cfs	
$Q_T, \text{Dev.} = 8.2 + 4.0 + 10.1 + 6.7 = 29$ cfs	
$\Delta Q_{100} = 29.0 - 22.6 = 6.4$ cfs (increase)	

II. STREET HYDRAULICS

Normal depth is calculated for both streets using Manning's Equation. The sequent depth is used for Wilshire Avenue to determine total flow depth including the hydraulic jump depth.

Input Criteria:

- Manning's $n = 0.017$
- Cross sectional geometry
- Normal depth

A. Wilshire Avenue N.E.

$A_n = 4.08$ sf
$A_g = 2.47$ sf
$P_n = 20.484$ ft
$P_g = 15.85$ ft
$R^{2/3} = (A/P)^{2/3}$
$S^{1/2} = 0.1892$ (θ 0.0358 slope)
$Q_{10} = 35$ cfs

Max Q_{capacity} of one side of road before it flows over the crown is 23.1 cfs, so the rest flows to the south side of the road (11.9 cfs)

$$Q_n = 23.1 \text{ cfs } @ d = 0.484'$$

$$Q_g = 11.3 \text{ cfs } @ d = 0.388'$$

Use Sequent Depth Method due to supercritical flow in Wilshire Avenue N.E.

$$d_{\text{seq}} = 0.5d_1[(1+8F^2)^{1/2} - 1] \quad (\text{eq. 3-21 from Open Channel Hydraulics by Ven Te Chow})$$

$$F = v / (gd_1)^{1/2}$$

$$V = Q/A;$$

$$G = 32.2 \text{ ft/sec}^2$$

$$V_n = Q_n/A_n = 23.1/4.08 = 5.66 \text{ fps}$$

$$V_g = Q_g/A_g = 11.3/2.38 = 4.75 \text{ fps}$$

$$F_n = 1.43$$

$$F_g = 1.35$$

$$d_{n, \text{seq}} = 0.77 \text{ ft} < 0.87 \text{ ft (max. allowable depth in street)}$$

$$d_{g, \text{seq}} = 0.58 \text{ ft} < 0.87 \text{ ft (max. allowable depth in street)}$$

$$dv = (d)(v)$$

$$dvn = (0.484)(5.66) = 2.74 < 6.5 \text{ max. allowable; satisfies criteria}$$

$$dvs = (0.388)(4.75) = 1.84 < 6.5 \text{ max. allowable; satisfies criteria}$$

$$d_{100} > d_{\text{crown}} \text{ then let flow be evenly distributed}$$

$$SO \text{ both sides of the road will have a } Q \text{ of } 25.3 \text{ cfs}$$

$$Q = 25.3 \text{ cfs}$$

$$A = 4.29 \text{ sf}$$

$$P = 20.495 \text{ ft}$$

$$R = (A/P)^{2/3}$$

$$S = (0.005)^{1/2}$$

$$d = 0.495 \text{ ft}$$

Use Sequent Depth Method due to supercritical flow in Wilshire Avenue N.E.

$$d_{\text{seq}} = 0.5d_1[(1+8F^2)^{1/2} - 1]$$

$$F = v / (gd_1)^{1/2}$$

$$G = 32.2 \text{ ft/sec}^2$$

$$V = Q/A;$$

$$V = 5.90 \text{ ft/sec}$$

$$F = 1.48$$

$$d_{\text{seq}} = 0.818 \text{ ft} < 0.87 \text{ ft (max. allowable depth in street)}$$

$$dv = (0.495)(5.9) = 2.92 < 6.5 \text{ max. allowable; satisfies criteria}$$

B. Wyoming Boulevard N.E.

Q that leaves one free lane (required for Q_{10})

Manning's Equation is used to calculate discharge.

$$n = 0.017$$

$$A = 5.61 \text{ sf}$$

$$R^{2/3} = (A/P)^{2/3}$$

$$P = 24.05 \text{ ft}$$

$$S = (0.005)^{1/2}$$

$$Q_{\text{allowable}} = 13.2 \text{ cfs } @ d = 0.56'$$

$$Q \text{ at maximum curb height} = 8"$$

$$n = 0.017$$

$$A = 8.54 \text{ sf}$$

$$P = 29.75 \text{ ft}$$

$$R = (A/P)^{2/3}$$

$$S = (0.005)^{1/2}$$

$$Q = 23.1 \text{ cfs } @ d = 0.67'$$

III. INLET CAPACITIES

A. Wilshire Avenue N.E.: $Q_{100} = 50.6$ cfs1. For Q_{100}

- Single 'A' Storm Inlet (1st in series)
- Double 'C' Storm Inlet (2nd in series)
- Double 'C' Storm Inlet (3rd in series)

$$Q_{\text{cap}} = 9.2 \text{ cfs (each side of street)}$$

$$Q_{\text{cap}} = 8.6 \text{ cfs (each side of street)}$$

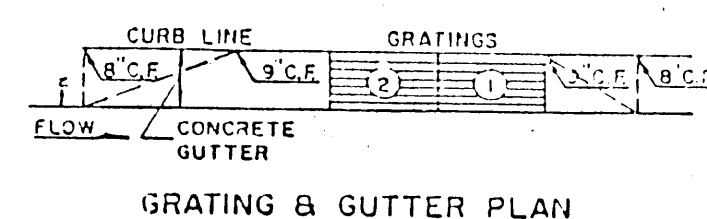
$$Q_{\text{cap}} = 5.5 \text{ cfs (each side of street)}$$

$$Q_{\text{cap}} = 3.0 \text{ cfs to Wyoming Blvd. N.E.}$$

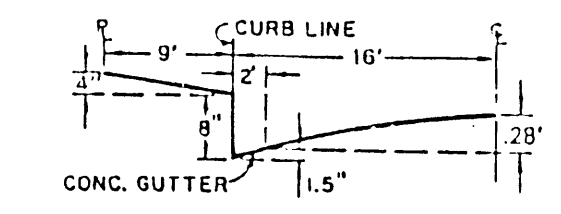
B. Wilshire Avenue N.E.: $Q_{100} = 11.3$	
1. Single 'A' Storm Inlet (1st in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
2. Double 'C' Storm Inlet (2nd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
3. Double 'C' Storm Inlet (3rd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
4. Double 'C' Storm Inlet (4th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
5. Double 'C' Storm Inlet (5th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
6. Double 'C' Storm Inlet (6th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
7. Double 'C' Storm Inlet (7th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
8. Double 'C' Storm Inlet (8th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
9. Double 'C' Storm Inlet (9th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
10. Double 'C' Storm Inlet (10th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
11. Double 'C' Storm Inlet (11th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
12. Double 'C' Storm Inlet (12th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
13. Double 'C' Storm Inlet (13th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
14. Double 'C' Storm Inlet (14th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
15. Double 'C' Storm Inlet (15th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
16. Double 'C' Storm Inlet (16th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
17. Double 'C' Storm Inlet (17th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
18. Double 'C' Storm Inlet (18th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
19. Double 'C' Storm Inlet (19th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
20. Double 'C' Storm Inlet (20th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
21. Double 'C' Storm Inlet (21st in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
22. Double 'C' Storm Inlet (22nd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
23. Double 'C' Storm Inlet (23rd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
24. Double 'C' Storm Inlet (24th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
25. Double 'C' Storm Inlet (25th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
26. Double 'C' Storm Inlet (26th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
27. Double 'C' Storm Inlet (27th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
28. Double 'C' Storm Inlet (28th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
29. Double 'C' Storm Inlet (29th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
30. Double 'C' Storm Inlet (30th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
31. Double 'C' Storm Inlet (31st in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
32. Double 'C' Storm Inlet (32nd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
33. Double 'C' Storm Inlet (33rd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
34. Double 'C' Storm Inlet (34th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
35. Double 'C' Storm Inlet (35th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
36. Double 'C' Storm Inlet (36th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
37. Double 'C' Storm Inlet (37th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
38. Double 'C' Storm Inlet (38th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
39. Double 'C' Storm Inlet (39th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
40. Double 'C' Storm Inlet (40th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
41. Double 'C' Storm Inlet (41st in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
42. Double 'C' Storm Inlet (42nd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
43. Double 'C' Storm Inlet (43rd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
44. Double 'C' Storm Inlet (44th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
45. Double 'C' Storm Inlet (45th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
46. Double 'C' Storm Inlet (46th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
47. Double 'C' Storm Inlet (47th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
48. Double 'C' Storm Inlet (48th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
49. Double 'C' Storm Inlet (49th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
50. Double 'C' Storm Inlet (50th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
51. Double 'C' Storm Inlet (51st in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
52. Double 'C' Storm Inlet (52nd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
53. Double 'C' Storm Inlet (53rd in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
54. Double 'C' Storm Inlet (54th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
55. Double 'C' Storm Inlet (55th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
56. Double 'C' Storm Inlet (56th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
57. Double 'C' Storm Inlet (57th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
58. Double 'C' Storm Inlet (58th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	
59. Double 'C' Storm Inlet (59th in series 'south side')	
$Q_{\text{cap}} = 8.6$ cfs	

WYOMING BLVD. - DOUBLE 'C'

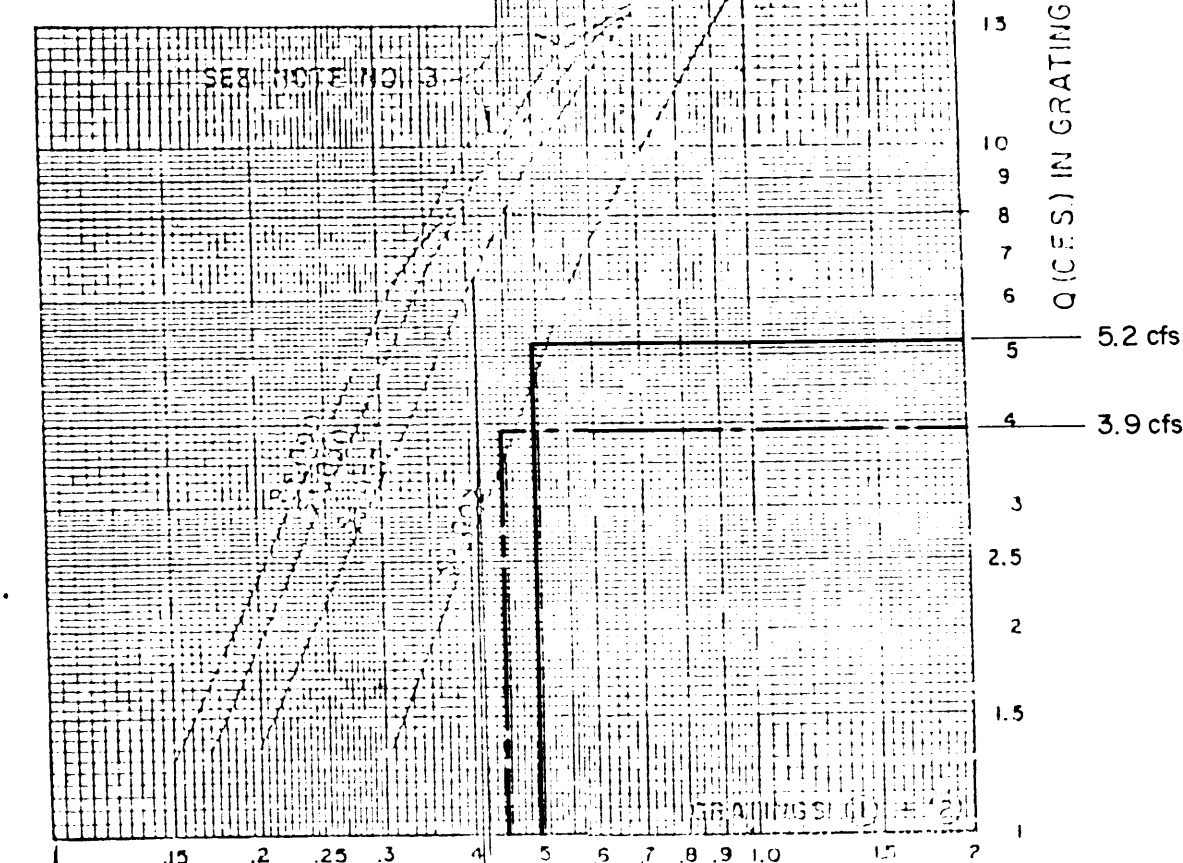
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)

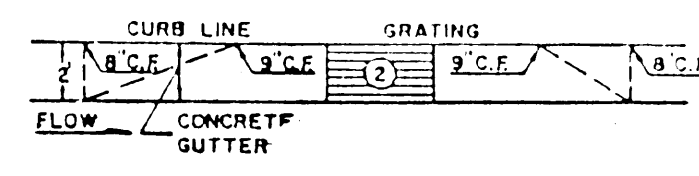


D=DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

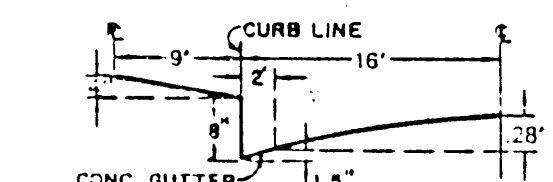
Q₁₀₀ ——— d = 0.494 FT (Q_{cap} = 5.2 cfs)Q₁₀ ——— d = 0.445 FT (Q_{cap} = 3.9 cfs)

WYOMING BLVD. - SINGLE 'A'

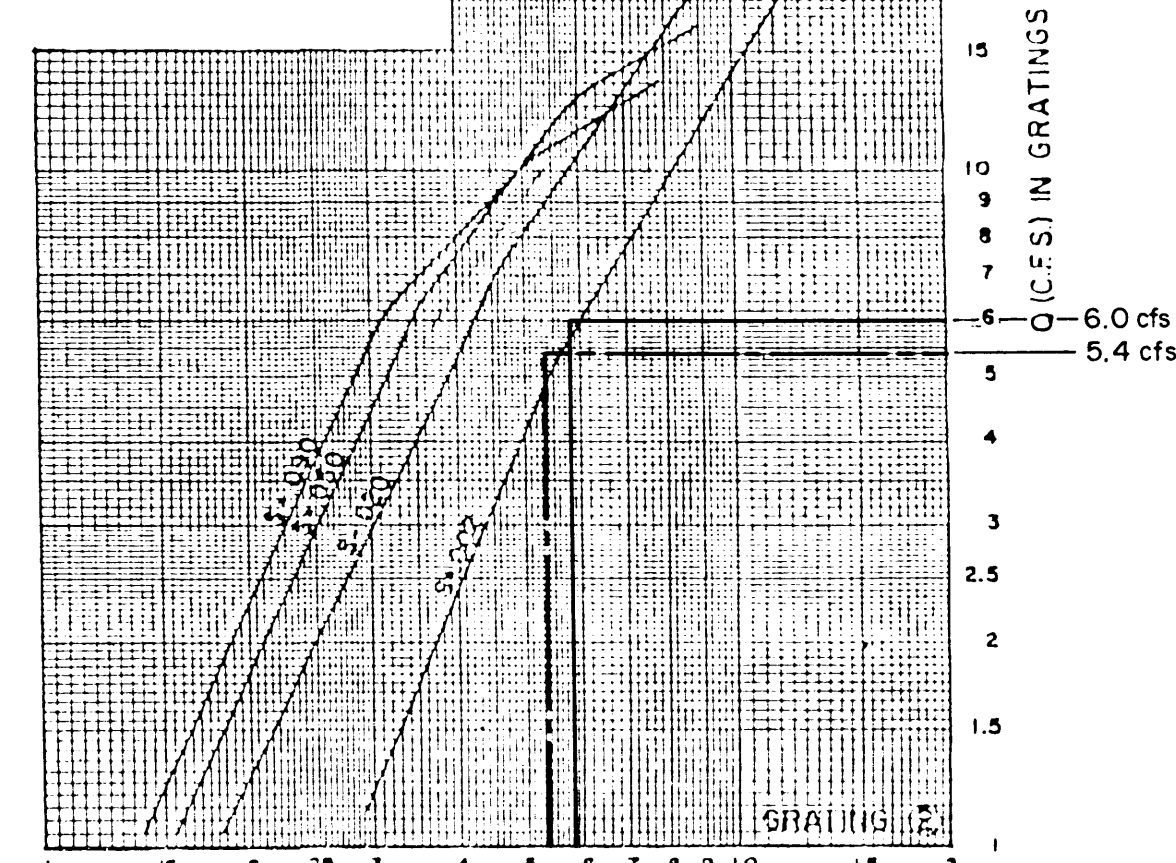
GRATING CAPACITIES FOR TYPE "A", "C" AND "D"



GRATING & GUTTER PLAN



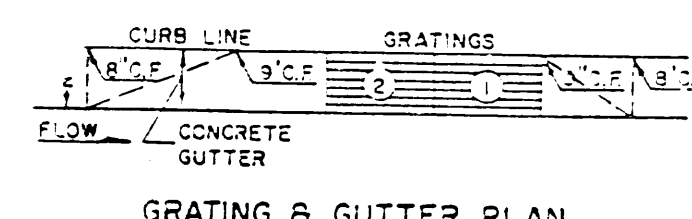
TYPICAL HALF STREET SECTION (ABOVE BASIN)



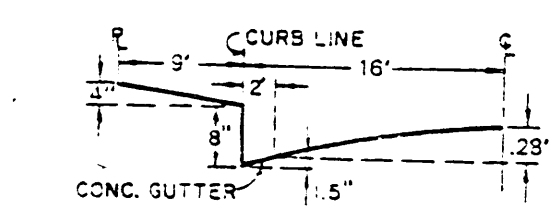
D=DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

Q₁₀₀ ——— d = 0.581 FT (Q_{cap} = 6.0 cfs)Q₁₀ ——— d = 0.538 FT (Q_{cap} = 5.4 cfs)WYOMING BLVD.-DOUBLE 'C'
AFTER Q CHURCH

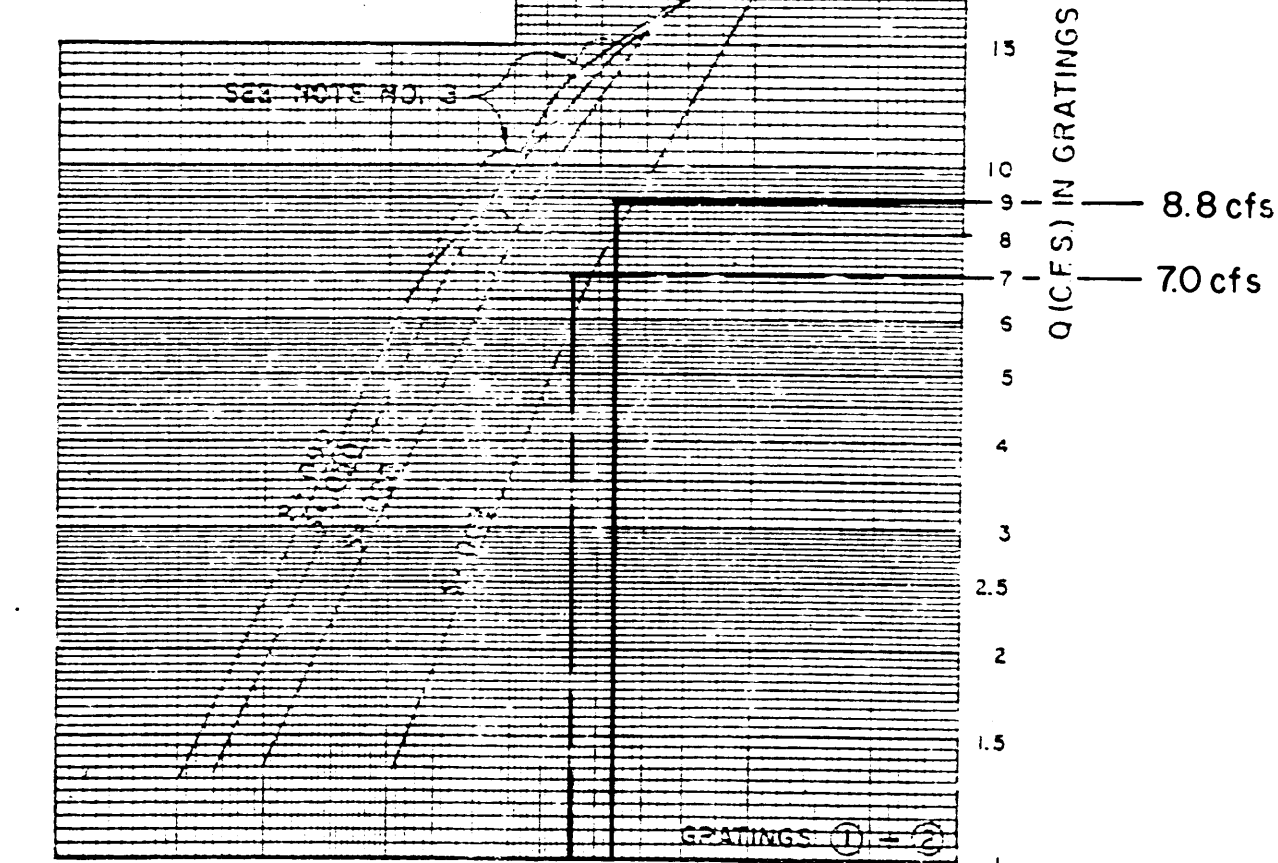
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)

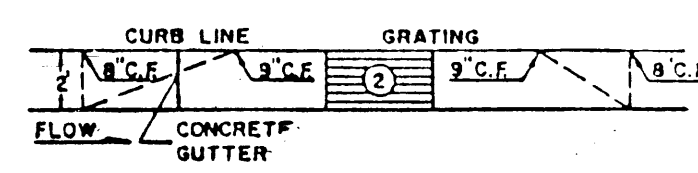


D=DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

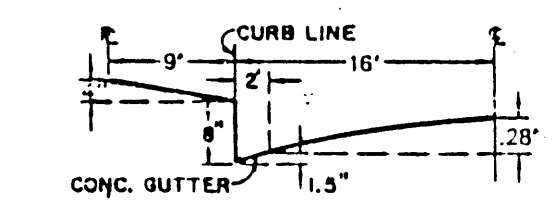
Q₁₀₀ ——— d = 0.645 FT (Q_{cap} = 8.8 cfs)Q₁₀ ——— d = 0.563 FT (Q_{cap} = 7.0 cfs)

WILSHIRE AVE. - SINGLE 'A'

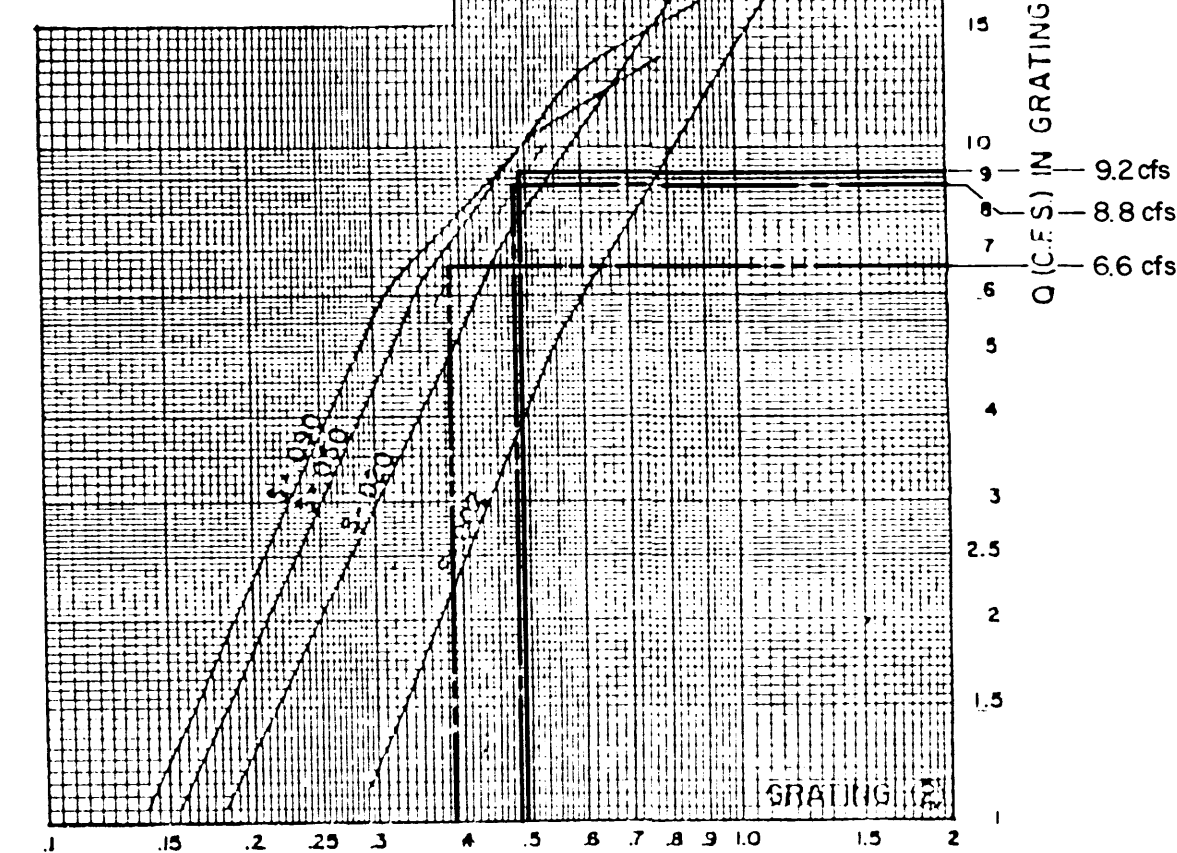
GRATING CAPACITIES FOR TYPE "A", "C" AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)

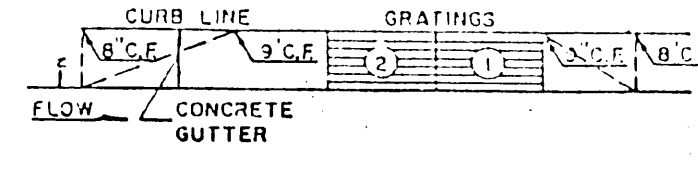


D=DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

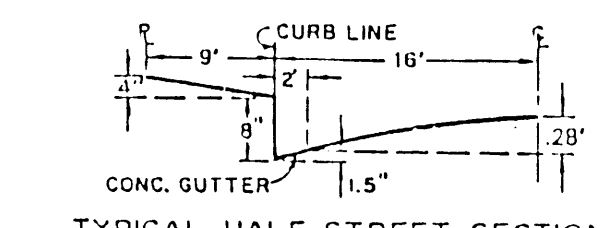
Q₁₀₀ ——— d = 0.49 FT (Q_{cap} = 9.2 cfs)Q_{10A} ——— d = 0.484 FT (Q_{cap} = 8.8 cfs)Q_{10S} ——— d = 0.388 FT (Q_{cap} = 6.6 cfs)

WILSHIRE AVE. - FIRST DOUBLE 'C'

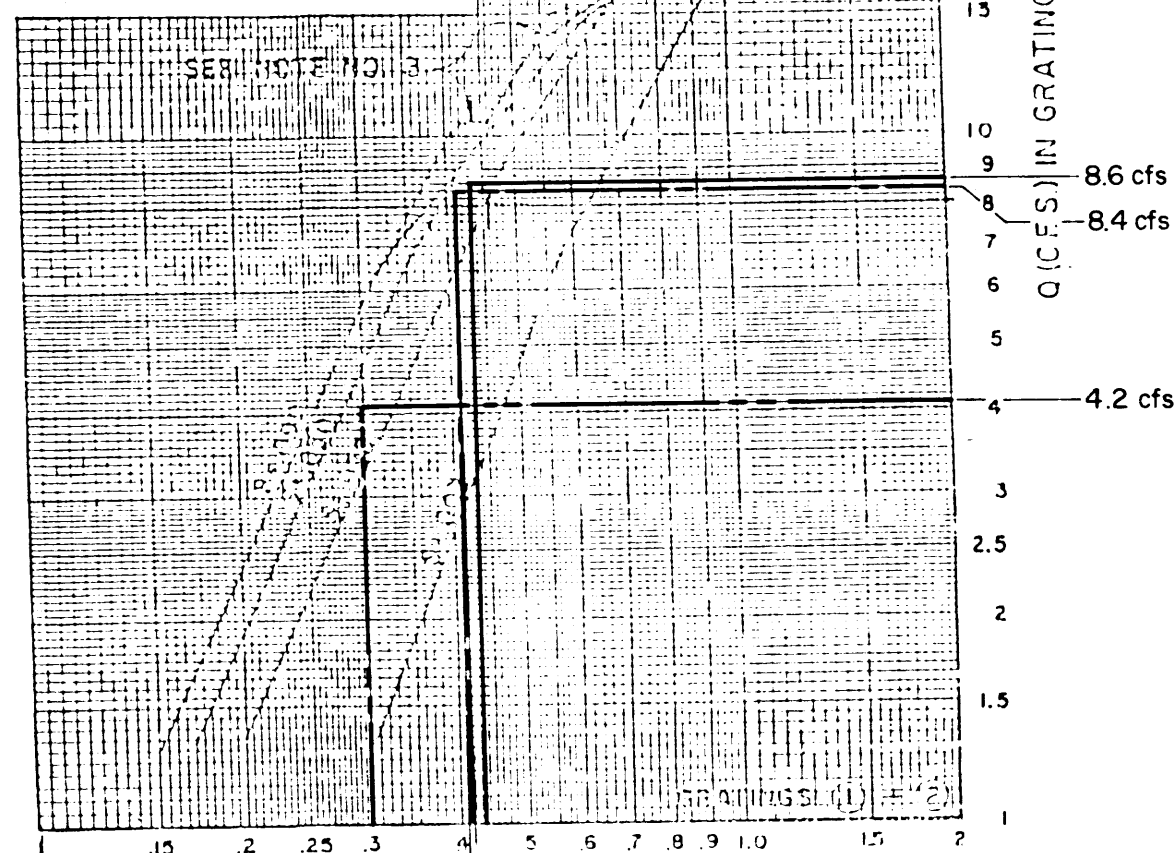
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)

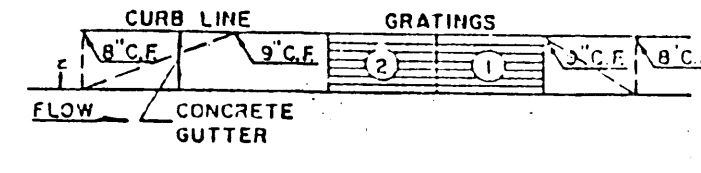


D=DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

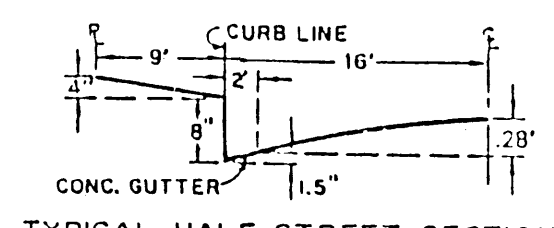
Q₁₀₀ ——— d = 0.432 FT (Q_{cap} = 8.6 cfs)Q_{10A} ——— d = 0.417 FT (Q_{cap} = 8.4 cfs)Q_{10S} ——— d = 0.298 FT (Q_{cap} = 4.2 cfs)

WILSHIRE AVE. - SECOND DOUBLE 'C'

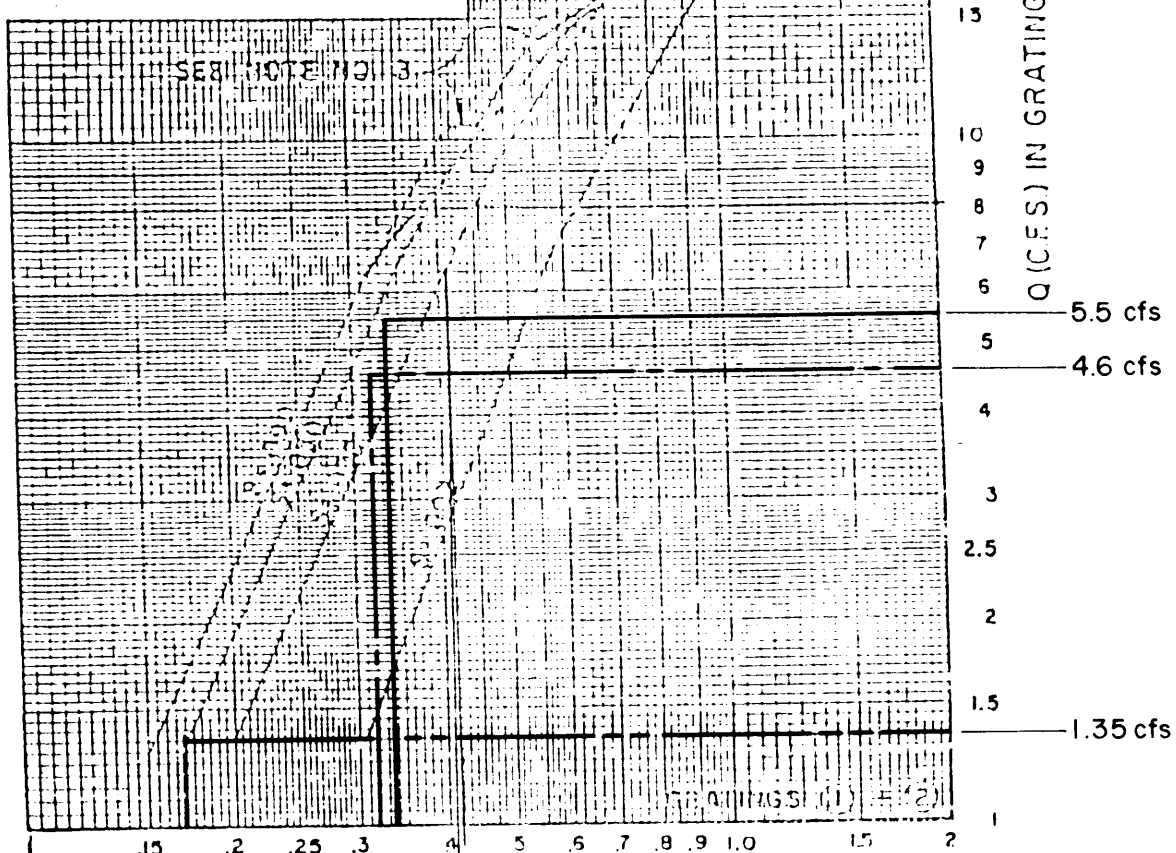
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



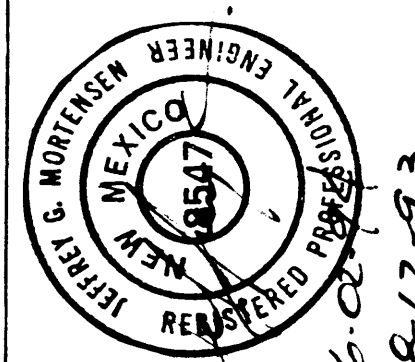
TYPICAL HALF STREET SECTION (ABOVE BASIN)



D=DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

Q₁₀₀ ——— d = 0.336 FT (Q_{cap} = 5.5 cfs)Q_{10A} ——— d = 0.319 FT (Q_{cap} = 4.6 cfs)Q_{10S} ——— d = 0.154 FT (Q_{cap} = 1.35 cfs)
(0.5 cfs NEEDED)

ENGINEER'S SEAL		SURVEY INFORMATION		BENCH MARKS		AS BUILT INFORMATION	
NO.	DATE	NO.	DATE	CONTRACTOR	DATE	CONTRACTOR	DATE
				A STANDARD A.C.S. BRASS TABLET STAMPED			
				1-C19 M.A.A. LOT 32, BLK. 10 SET IN TOP OF A			
				CONC. POST FLUSH W/ THE GROUND, LOCATED			
				@ THE INTERSECTION OF LOUISIANA BLVD. N.E. &			
				PAVED DEL NORTE, IN THE N.E. QUADRANT,			
				50' NORTH OF THE N.W. CORNER OF A			
				CHAINLINK FENCE AROUND THE F.A.A. AIR			
				TRAFFIC CONTROL CENTER			
				ELEVATION: 5318.175 FT. (M.S.L.D.)			



08-12-93

CITY OF ALBUQUERQUE
PUBLIC WORKS DEPARTMENT
ENGINEERING GROUPTITLE: COVENANT UNITED METHODIST CHURCH
PAVING & STORM DRAINAGE IMPROVEMENTS
GRATING CAPACITIES

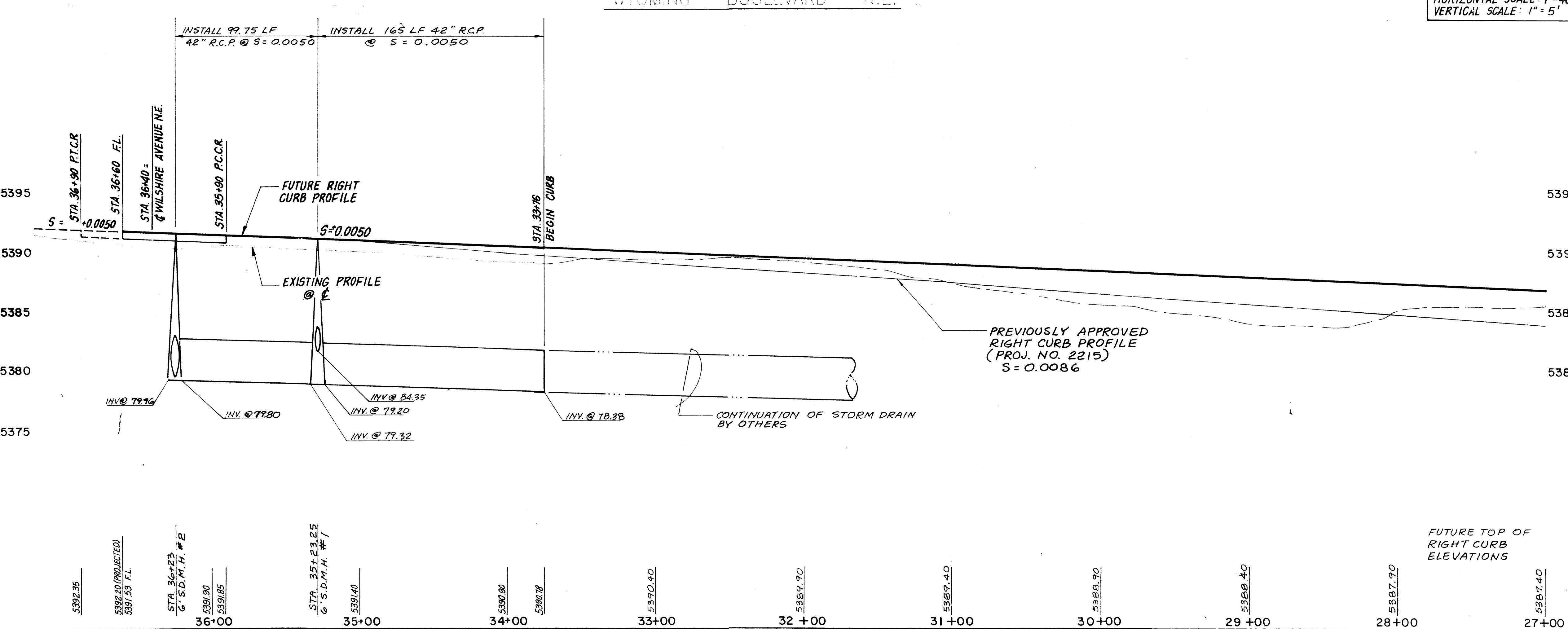
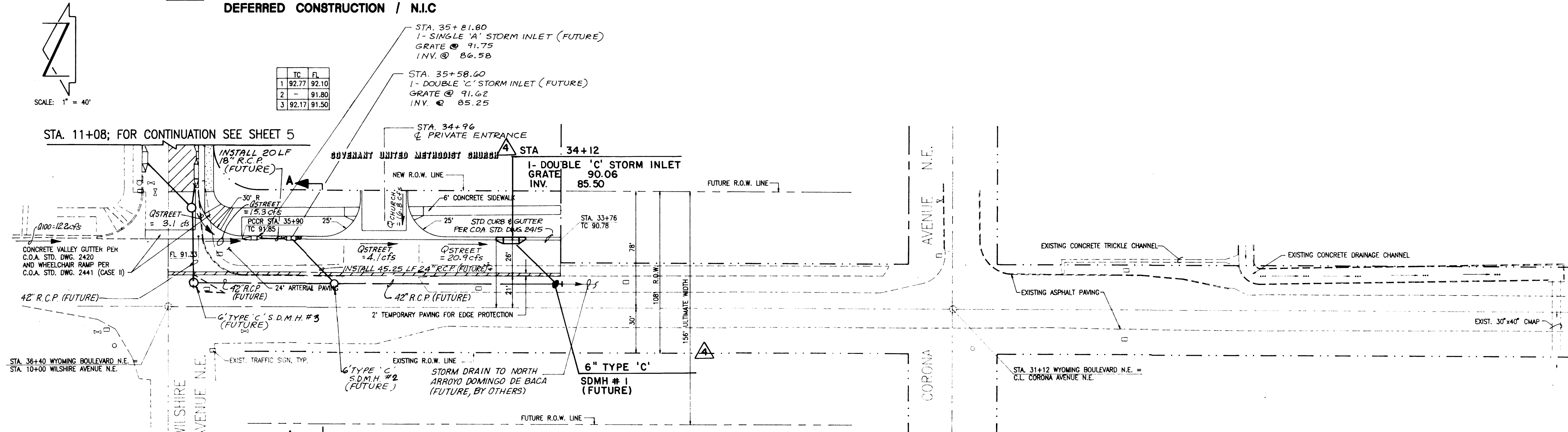
APPROVALS	ENGINEER	DATE	APPROVALS	ENGINEER	DATE
DRG CHAIRMAN			WATER		
TRANSPORTATION			WASTE WATER		
HYDROLOGY					

PROJECT NO.	MAP NO.	SHEET	OF
2-394	C-19	3	6

DESIGN ANALYSIS

The street grades presented hereon have been established at the minimum allowable street grade set forth in the Development Process Manual. The minimum slope of 0.0050 has been maintained. The previously approved street grade for this portion of Wyoming Boulevard N.E. is 0.0086 which would place the street profile lower than that which is proposed at this time. The gradient of 0.0050 has been selected due to the fact that it is a minimum slope and that it provides of the highest possible street grade at the crossing of the North Arroyo de Domingo Baca, this will provide more flexibility in discharging into that Arroyo once a crossing is designed at a future date. The storm drain shown hereon has been established at the same minimum street grade of 0.0050. The design assumption here is that the storm drain shall parallel the street. The design is based upon keeping the storm drain as shallow as possible so as to allow for future discharge into the Arroyo.

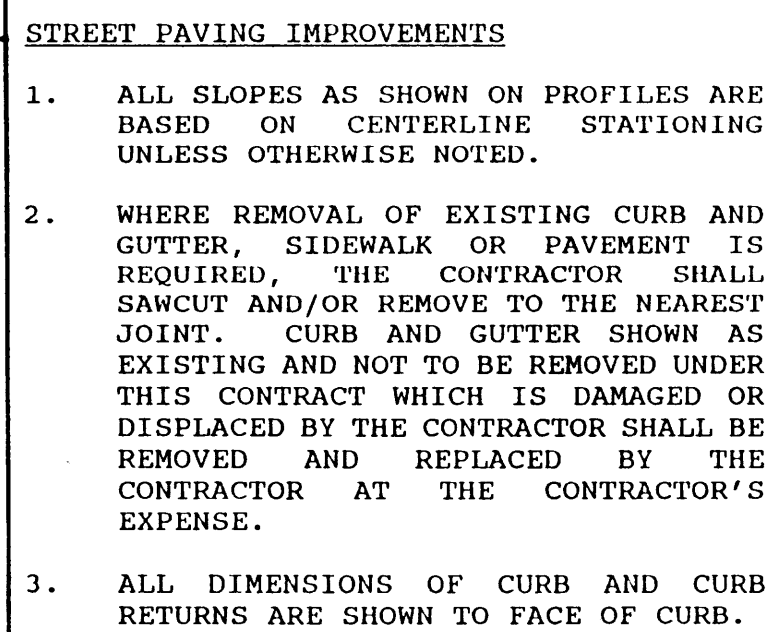
NOTE: THIS PLAN FOR INFORMATION ONLY
DEFERRED CONSTRUCTION / N.I.C



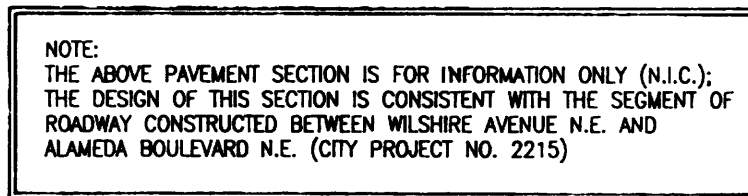
HORIZONTAL SCALE: 1"=40'
VERTICAL SCALE: 1"=5'

AS BUILT INFORMATION		BENCH MARKS		SURVEY INFORMATION		ENGINEER'S SEAL		REVISIONS		M.D.	
DATE	BY	DATE	BY	NO	NO	DATE	BY	NO	DATE	DATE	DATE
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	1	1	11-19-94	W. J. G. M.	1	1	11-19-94	11-19-94
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	2	2	11-19-94	W. J. G. M.	2	2	11-19-94	11-19-94
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	3	3	11-19-94	W. J. G. M.	3	3	11-19-94	11-19-94
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	4	4	11-19-94	W. J. G. M.	4	4	11-19-94	11-19-94
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	5	5	11-19-94	W. J. G. M.	5	5	11-19-94	11-19-94
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	6	6	11-19-94	W. J. G. M.	6	6	11-19-94	11-19-94
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	7	7	11-19-94	W. J. G. M.	7	7	11-19-94	11-19-94
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	8	8	11-19-94	W. J. G. M.	8	8	11-19-94	11-19-94
11-19-94	W. J. G. M.	11-19-94	W. J. G. M.	9	9	11-19-94	W. J. G. M.	9	9	11-19-94	11-19-94

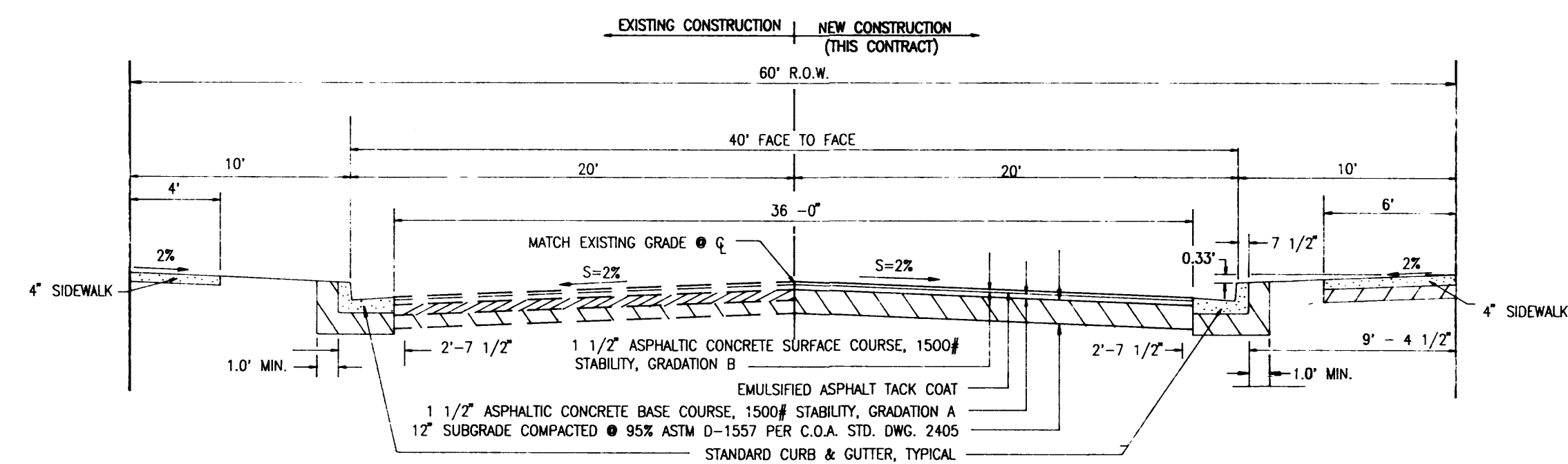
CITY OF ALBUQUERQUE PUBLIC WORKS DEPARTMENT ENGINEERING GROUP					
TITLE COVENANT UNITED METHODIST CHURCH PAVING & STORM DRAINAGE IMPROVEMENTS WYOMING BLVD. N.E. ~ STA. 31+12 TO STA. 36+40					
APPROVALS	ENGINEER	DATE	APPROVALS	ENGINEER	DATE
DRG CHAIRMAN			WATER		
TRANSPORTATION			WASTE WATER		
HYDROLOGY					
DESIGNED BY	W. J. G. M.	DATE	06/93	CHECKED BY	W. J. G. M.
DRAWN BY	S. G. H. / T. P. H.	DATE	06/93		
CHECKED BY	J. G. M.	DATE	07/93		
PROJECT NO. 920412		MAP NO. C-19		SHEET 4 OF 6	



CITY OF ALBUQUERQUE PUBLIC WORKS DEPARTMENT ENGINEERING GROUP					
TITLE: COVENANT UNITED METHODIST CHURCH PAVING & STORM DRAINAGE IMPROVEMENTS WILSHIRE AVE. N.E. ~ STA. 10+00 TO STA. 18+24.75					
APPROVALS	ENGINEER	DATE	APPROVALS	ENGINEER	DATE
DRG CHAIRMAN			WATER		
TRANSPORTATION			WASTE WATER		
HYDROLOGY					



SECTION A —



SECTION B - B

ENGINEER'S SEAL

06-02-94

08-12-95

07-02-93

TEHRAN G. MORTAZAVI
REGISTERED PROFESSIONAL ENGINEER
MEXICO
16547

TITLE: COVENANT UNITED METHODIST CHURCH
SECTIONS AND DETAILS

PROJECT NO.	2 1994	MAP NO.	C-19	SHEET	OF	6	6
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