



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

February 15, 2002

Larry Read, P.E.
Larry Read & Assoc.
4800 Juan Tabo NE Suite C
Albuquerque, New Mexico 87111

RE: FIRE STATION NO. 20 (C-19/D23)
~~(8300 Wyoming Blvd NE)~~ (7520 CORONA NE)
ENGINEERS CERTIFICATION FOR CERTIFICATE OF OCCUPANCY
ENGINEERS STAMP DATED 12/22/1999 Rev. 2/22/2000
ENGINEERS CERTIFICATION DATED 2/14/2002

Dear Mr. Read:

Based upon the information provided in your Engineers Certification submittal dated 2/1/2002, the above referenced site is approved for Permanent Certificate of Occupancy.

If I can be of further assistance, please contact me at 924-3981.

Sincerely,

Teresa A. Martin
Hydrology Plan Checker
Public Works Department
BUB

C: Vickie Chavez, COA
approval file
✓ drainage file

DRAINAGE AND TRANSPORTATION INFORMATION SHEET

(REV. 1/11/2002)

PROJECT TITLE: CDA FIRE STATION #20 ZONE MAP/DRG. FILE #: C19/D23
DRB #: _____ EPC#: _____ WORK ORDER#: 6042.21

LEGAL DESCRIPTION: LOTS 14-19, BLOCK 6, UNIT 3, TRACT 2 WAA
CITY ADDRESS: 8300 WYOMING BLVD NE

ENGINEERING FIRM: LARRY READ & ASSOC. INC. CONTACT: LARRY READ
ADDRESS: 4800 JUAN TABO NE SUITE C PHONE: 237-1842
CITY, STATE: ALBUQUERQUE, NM 87111 ZIP CODE: 87111

OWNER: CITY OF ALBUQUERQUE FIRE & POLICE CONTACT: _____
ADDRESS: _____ PHONE: _____
CITY, STATE: _____ ZIP CODE: _____

ARCHITECT: RHODE MAY KELLER MCNAMANA CONTACT: DON MAY
ADDRESS: 400 GOLD SW SUITE 1100 PHONE: 243-5454
CITY, STATE: ALBUQUERQUE NM 87103 ZIP CODE: 87103

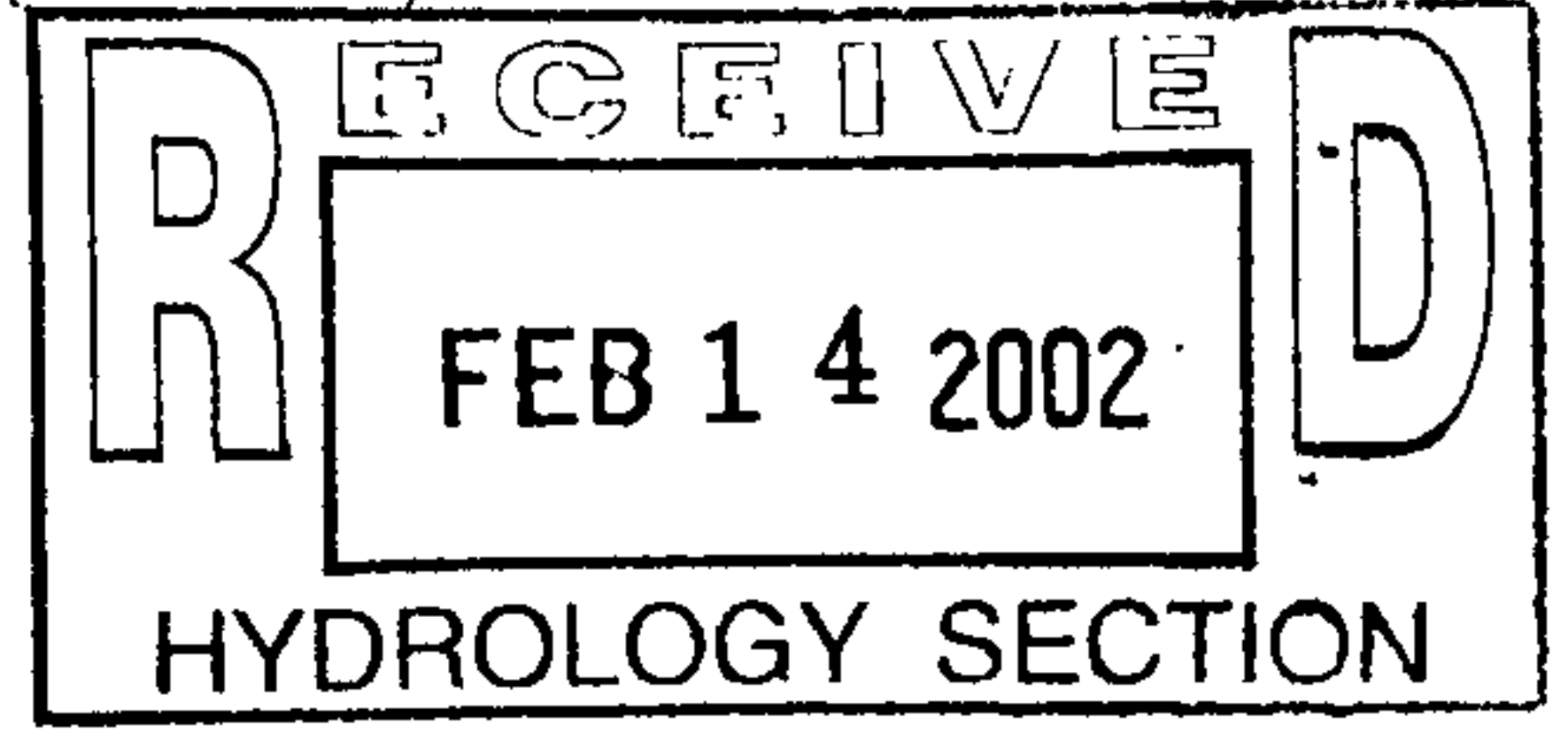
SURVEYOR: _____ CONTACT: _____
ADDRESS: _____ PHONE: _____
CITY, STATE: _____ ZIP CODE: _____

CONTRACTOR: _____ CONTACT: _____
ADDRESS: _____ PHONE: _____
CITY, STATE: _____ ZIP CODE: _____

- CHECK TYPE OF SUBMITTAL:
- DRAINAGE REPORT
 - DRAINAGE PLAN
 - CONCEPTUAL GRADING & DRAINAGE PLAN
 - GRADING PLAN
 - EROSION CONTROL PLAN
 - ENGINEER'S CERTIFICATION (HYDROLOGY)
 - CLOMR/LOMR
 - TRAFFIC CIRCULATION LAYOUT (TCL)
 - ENGINEERS CERTIFICATION (TCL)
 - ENGINEERS CERTIFICATION (DRB APPR. SITE PLAN)
 - OTHER

- CHECK TYPE OF APPROVAL SOUGHT:
- SIA / FINANCIAL GUARANTEE RELEASE
 - PRELIMINARY PLAT APPROVAL
 - S. DEV. PLAN FOR SUB'D. APPROVAL
 - S. DEV. PLAN FOR BLDG. PERMIT APPROVAL
 - SECTOR PLAN APPROVAL
 - FINAL PLAT APPROVAL
 - FOUNDATION PERMIT APPROVAL
 - BUILDING PERMIT APPROVAL
 - CERTIFICATE OF OCCUPANCY (PERM.)
 - CERTIFICATE OF OCCUPANCY (TEMP.)
 - GRADING PERMIT APPROVAL
 - PAVING PERMIT APPROVAL
 - WORK ORDER APPROVAL
 - OTHER (SPECIFY)

WAS A PRE-DESIGN CONFERENCE ATTENDED:
 YES
 NO
 COPY PROVIDED



DATE SUBMITTED: 2-14-2002 BY: [Signature]

Requests for approvals of Site Development Plans and/or Subdivision Plans shall be accompanied by a drainage submittal. The particular nature, location and scope of the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

1. **Conceptual Grading and Drainage Plan:** Required for approval of Site Development Plans greater than five
2. **Drainage Plans:** Required for building permits, grading permits, paving permits and site plans less than five (5)
3. **Drainage Report:** Required for subdivisions containing more than ten (10) lots or constituting five (5) acres or



City of Albuquerque

March 8, 2000

Larry Read, P.E.
Larry Read & Associates
Post Office Box 90233
Albuquerque, New Mexico 87199

RE: Grading and Drainage Plan for Fire Station # 20, Lots 14 - 19, Block 6, Unit 3, NAA, (C19/D23), Engineer's Stamp Dated 2/28/00.

Dear Mr. Read:

Based on the information provided, the above referenced Grading and Drainage plan dated February 28, 2000 is approved for Building Permit release.

Please attach a copy of this approved plan to the set of construction drawings for Building Permit sign-off.

As you are aware, the Engineer's Certification is required prior to release of the Certificate of Occupancy for this site.

If you have any questions, or if I may be of further assistance to you, please call me at 924-3982.

Sincerely,

Susan M. Calongne, P.E.
City/County Floodplain Administrator

c: Whitney Reiersen, City Hydrology
File



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

January 28, 2000

Larry Read, P.E.
Larry Read & Associates
Post Office Box 90233
Albuquerque, New Mexico 87199

RE: *Grading and Drainage Plan for Fire Station # 20, Lots 14 - 19, Block 6, Unit 3, NAA, (C19/D23), Engineer's Stamp Dated 12/22/99.*

Dear Mr. Read:

It is not clear what approval you were seeking with your submittal of January 3, 2000. As previously stated in my letter of November 22, 1999, the plans for the Fire Station cannot be approved for Building Permit release until my previous comments are addressed. The street grades for both Wyoming and Corona must be designated **on the plan** by the top of curb elevations and/or flow line elevations. Without this information, these plans are not approved.

If you have any questions, please call me at 924-3982.

Sincerely,

Susan M. Calongne, P.E.
City/County Floodplain Administrator

c: Whitney Reiersen, City Hydrology
File



City of Albuquerque

November 22, 1999

Larry Read, P.E.
Larry Read & Associates
Post Office Box 90233
Albuquerque, New Mexico 87199

RE: Grading and Drainage Plan for Fire Station # 20, Lots 14 - 19, Block 6, Unit 3, NAA, (C19/D23) Submitted for Building Permit Approval, Engineer's Stamp Dated 10/25/99.

Dear Mr. Read:

The above referenced submittal of October 27, 1999 did not address my previous comments. Prior to approval for Building Permit release, please address the following:

1. It was my understanding that an AMAFCA easement was required for the portion of the site that is within the FEMA floodplain. Please show the limits of the AMAFCA easement on the plan. This easement must be in place prior to Building Permit release. AMAFCA approval is also required for any construction within this easement. The existing fence must be moved out of the FEMA floodplain, unless it is allowed by AMAFCA.
2. Prior to Building Permit release, the proposed street grades for both Wyoming and Corona must be designated **on the plan** by top of curb elevations and/or flow line elevations. The plan must also show a water block at the Corona entrance.

It is unclear why the entire drainage report was resubmitted. This is not necessary unless the drainage concepts and calculations have changed. If you have any questions, please call me at 924-3982.

Sincerely,

Susan M. Calongne, P.E.
City/County Floodplain Administrator

c: Lisa Manwill, Albuquerque Metropolitan Arroyo Flood Control Authority
Whitney Reiersen, City Hydrology
File



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

June 8, 1999

Larry Read, P.E.
Larry Read & Associates
Post Office Box 90233
Albuquerque, New Mexico 87199

RE: *Conceptual Drainage Report and Grading and Drainage Plan for Fire Station # 20, Lots 14 - 19, Block 6, Unit 3, NAA, (C19/D23) Submitted for Site Development Plan Approval, Engineer's Stamp Dated 4/26/99.*

Dear Mr. Read:

Based on the information provided in the submittals of April 27, 1999 and June 7, 1999, the above referenced plan is approved for Site Development Plan approval by the DRB.

An AMAFCA easement is required for the portion of the site that is within the existing FEMA floodplain. Please show the limits of the AMAFCA easement on the plan. This easement must be in place prior to Building Permit release, or Final Plat sign-off. AMAFCA approval is also required for any construction within this easement.

Prior to Building Permit release, the proposed street grades for both Wyoming and Corona must be designated on the plan by either top of curb or flow line elevations. The plan must also show a water block at the Corona entrance, since it appears that Basin B will drain onto Corona without this water block.

As you stated in your letter, the required road improvements must be complete prior to issuance of the Certificate of Occupancy for this site.

If you have any questions, or if I may be of further assistance to you, please call me at 924-3982.

Sincerely,

Susan M. Calongne, P.E.
City/County Floodplain Administrator

c: Fred Aguirre, DRB-99-39
File

DRAINAGE REPORT

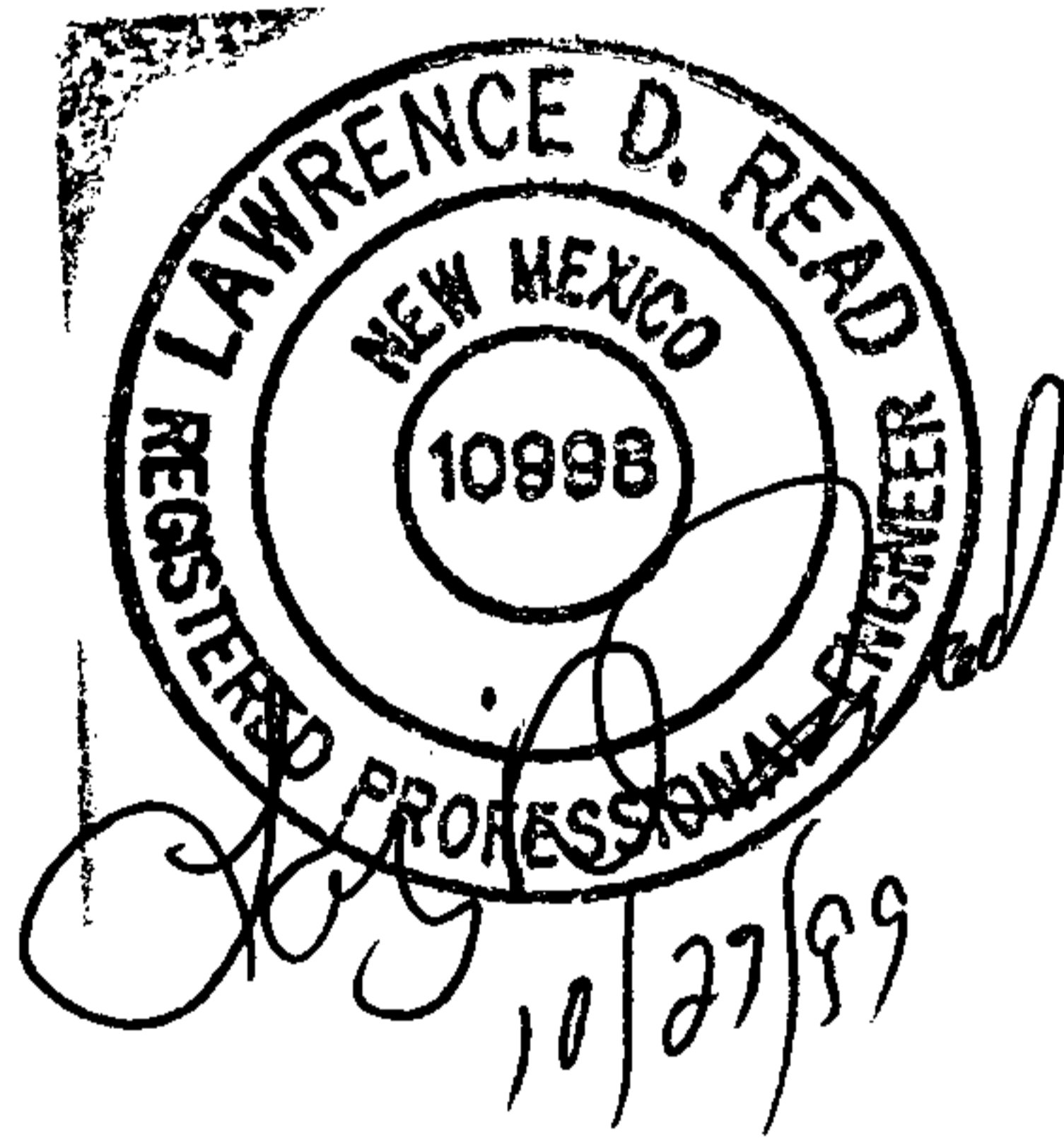
for

FIRE STATION NUMBER 20

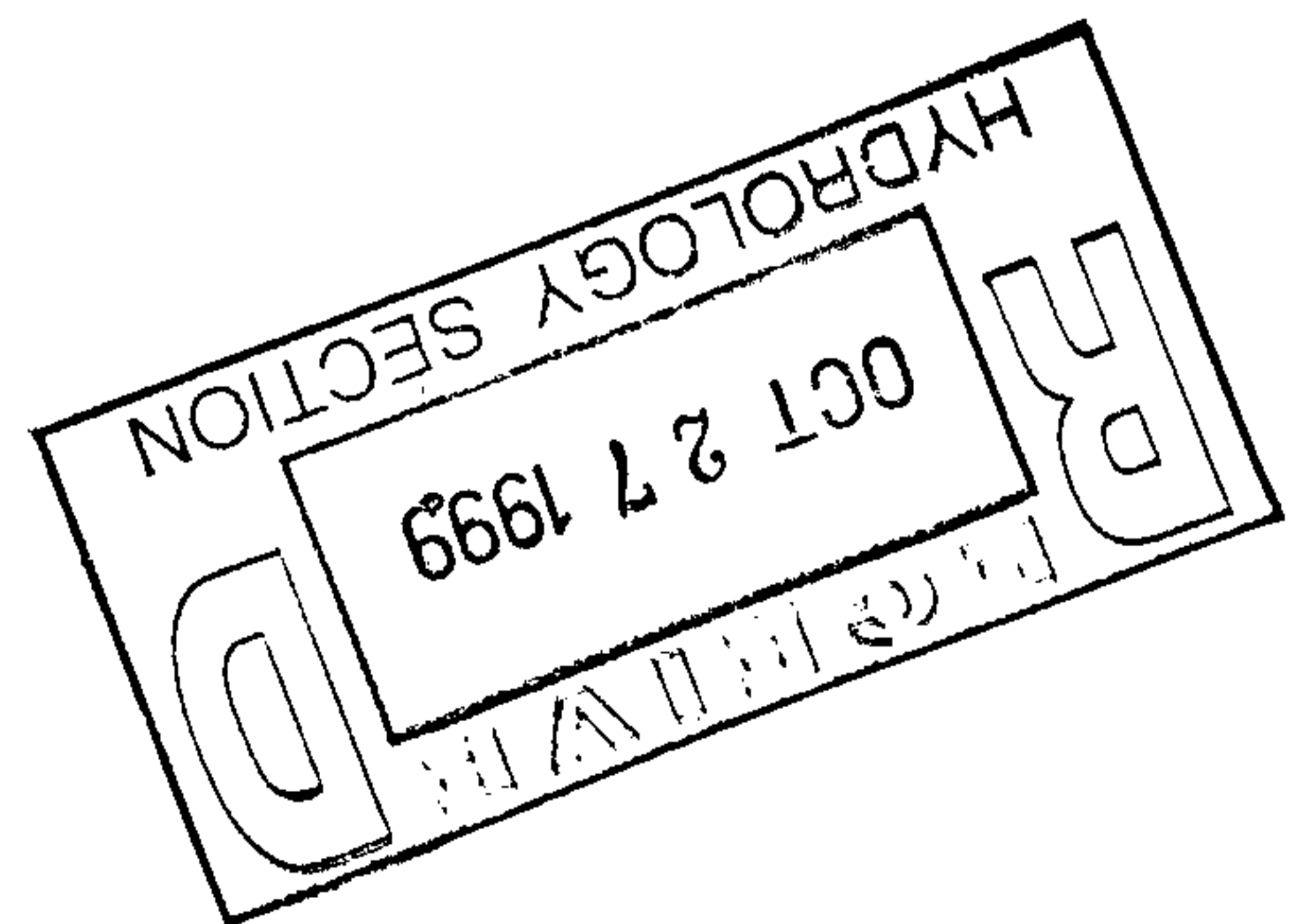
Wyoming Blvd. NE and Corona Ave. NE

Albuquerque, New Mexico

October 18, 1999



PREPARED BY
LARRY D. READ, PE
12836 Lomas Blvd., NE Suite B
ALBUQUERQUE, NEW MEXICO 87112
(505) 237-8421



DRAINAGE REPORT

for

FIRE STATION NUMBER 20

Wyoming Blvd. NE and Corona Ave. NE

Albuquerque, New Mexico

October 18, 1999

LOCATION & DESCRIPTION

This facility is proposed to be sited on the southwest corner of Wyoming Blvd. NE and Corona Ave. NE in the Domingo Baca Park. The site and the park are currently undeveloped. The City of Albuquerque Fire Department and City of Albuquerque Police Department are proposing to construct a 14,000 square foot facility to be used as Fire Station #20 and Police District 4 Substation. In addition to the building, this 4.8 acres site will include almost 37,500 square feet of paved parking to serve both departments and to provide public parking for the park when it is developed..

EXISTING DRAINAGE CONDITIONS

The existing site is vegetated with high desert type grasses and weeds and slopes toward the west at approximately 3.5%. The existing drainage from onsite runoff is a combination of shallow sheet flow with the beginning of minor channels that convey the runoff west into the end of the unimproved North Domingo Baca Arroyo and the Lower Domingo Baca Dam just east of Louisiana Blvd. between Carmel Ave. and Corona Ave.. In addition to the on-site runoff, the North Wyoming Storm Drain System outlets into the center of this site via a 60" RCP Storm Drain. The North Wyoming Storm Drain System collects all runoff from the developed areas north and east of the site. Along the southern edge of the site is the North Domingo Baca Arroyo. The Window G channel that collects runoff from the developed subdivisions east of Wyoming is soil cement lined east of Wyoming Blvd. and for a distance of about 120 feet west of Wyoming. The channel ends at the North Domingo Baca Arroyo that spreads and meanders across the park land south of this project site west toward the Lower Domingo Baca Dam.

OFFSITE DRAINAGE

As discussed above, this project site will not be affected by runoff from the developed land to the north and east due to the relocation of the outfall from the North Wyoming Storm Drain System. This site is also protected from runoff from the developed land east southeast of the site by the existing Window G Channel. Although this channel ends into the North Domingo Baca Arroyo on the west side of Wyoming (which is not improved along the south boundary of this site) the runoff is sufficiently channelized that there is only a small portion of the southeast corner of the site impacted by floodplain as shown on the Floodplain Map - Figure 2. Note that this figure is a copy of the Floodplain Map revised via LOMR dated April 24, 1999. In addition to the copy of the floodplain map, AGIS has provided an electronic copy of the floodplain overlain on the Zone Atlas Map and included as Figure 3. Note that the revised Floodplain Map was digitized and integrated into Figure 3 to reflect current conditions.

Offsite drainage basins have been delineated on the Offsite Drainage Basin Map included in Appendix B. The basins used for this analysis are those down stream of existing inlets and are the lower end of the drainage basins delineated in the North Albuquerque Acres Drainage Master Plan, December 1998 (copy in Appendix B). The land treatments and percentages used are consistent with a fully constructed six lane arterial roadway per the City of Albuquerque DPM. The land treatments used in the NAA Master Plan are consistent with large developed residential development. This report assumes that the existing storm drainage facilities were properly designed and near total interception has been achieved.

MASTER PLAN

In addition to the design analyses/master plan prepared for the design of the North Wyoming Storm Drain System, a drainage master plan has been prepared for the La Cueva Neighborhood Sector Development Plan. This report is in Draft form as of December 1998. Section 9 of the report detailing Facility Planning for Drainage has been included in Appendix D of this report for reference. This document covers several hundred acres of the North Albuquerque Area and is general in nature but does include a summary of planned improvements. There are no planned improvements affecting this site indicated in the Sector Development Plan.

PARK PROPOSED ACTIONS

This project is a portion of the proposed development of the Domingo Baca Park Master plan. The park development is proposing to replat and rezone the entire block into one parcel. As part of the replat, the existing right-of-way for Anaheim Ave. between Wyoming Blvd. and Louisiana Blvd. will be vacated. Additionally, the combined parcel will be rezoned as appropriate to Park and City facility usage. A bubble diagram of the proposed development plan has been included in Appendix D for reference. As indicated on the Preliminary Park Development Plan in Appendix D, the North Domingo Baca

Arroyo will be improved from the existing soil cement Window G Channel at the east side of this site, west to the beginning of the existing sediment and detention facilities for the Lower Domingo Baca Dam.

PROPOSED CONDITIONS

Preparation of this site for construction will require considerable earthwork and several drainage patterns will be affected as follows:

- The undeveloped site sheet flows west into the Lower Domingo Baca Dam. The development of this facility (onsite Drainage Basin B) will divert a portion of the developed flows north into Corona Avenue. This diversion is necessary to comply with the Fire Department's slope requirements for their large equipment.
- Developed runoff from all Onsite Basins will be intercepted in various onsite inlets, shown on the Grading Plan, and routed south in a storm drain to discharge into the main channel portion of the Domingo Baca Arroyo. Note that this discharge and the discharge from the rerouted North Wyoming Storm Drain System are considered temporary until the Domingo Baca Arroyo is channelized and stabilized as part of the Domingo Baca Park Construction. The proposed 24" storm drain will discharge just west of the rerouted 60" North Wyoming Storm Drain and will be provided with a separated riprap lined plunge pool.
- The existing 60" RCP discharge from the North Wyoming Storm Drain System will be rerouted south along Wyoming Blvd. from the northeast corner of the site and discharged into the North Domingo Baca Arroyo west of the end of the improved soil cement channel. The North Wyoming Storm Drain relocation has been designed by Easterling and Associates (COA Project No. 6201.91) and is in the process of being constructed by PWD on-call contractors.

Wyoming Blvd., along its frontage with this site, will be improved as part of this project. Runoff has been calculated for all offsite basins affecting this site. The offsite drainage map is included in Appendix B along with the calculations of runoff peak flow rates, depth calculations in the street, and storm inlet interception rates. The offsite basins reflected in the map in Appendix B represent only the portion of the offsite drainage basin below existing storm inlets. This report assumes that the existing inlets were sized to intercept the majority of the developed flows reaching the inlets. The proposed land treatments used in this report are in accordance with Section 22.2 of the City of Albuquerque Development Process Manual for fully developed conditions. Percentage of each land treatment used in this report is representative of a fully developed, six land arterial roadway section. Preliminary plan and profile sheets, included in Appendix E show the preliminary proposed curb profiles and inlet locations. Note that the 100-year flow depth in Wyoming from both north and south are less than 0.5 feet deep and runoff

does not cross the median or crown. Therefore, the only new storm inlets proposed for construction with this project are at the southwest corner of Wyoming and Corona. Since the 24' proposed pavement (in accordance with the City of Albuquerque DMP) construction will not connect to the existing pavement on Wyoming, it is proposed that the east edge of the new pavement will be curbed with extruded curb. The runoff from the west side of the existing pavement section will continue to flow west, over the new extruded curb, into the new pavement section, and into the two proposed new inlets at the southwest corner of Wyoming and Corona (ie. the construction of this portion of Wyoming will not block runoff from the west half of the existing roadway section) Runoff from the east half of the existing roadway section will continue to follow the east curb and gutter north to the existing inlet at the southeast corner of Wyoming and Corona. Typical roadway sections for Wyoming are included in Appendix E for reference.

The north half of Corona Ave has been constructed along the entire frontage of this site. Preliminary plan and profile sheets of the proposed south curb line have been included in Appendix E. This project will construct the south half of Corona along the site's frontage. The proposed construction of the south side of Corona will match the existing north side in both profile grade and section. Runoff calculations and offsite drainage basin map are included in Appendix B. Connection of the new south curb and gutter to the existing extruded curb at the west end of the site is proposed to be made with an extruded curb taper. Due to the slope of Corona, the runoff will follow the taper curb and continue west in inside the remaining extruded curb to the existing storm inlet approximately 1500 feet west of Wyoming on the south side of Corona (ie. no temporary drainage facilities are required to connect the full roadway section constructed by this project to the existing temporary section west of this site).

FLOOD PLAIN STATUS

FIRM Panel 350001C0137D and 141D were revised per the Letter of Map Revision approved by the Federal Emergency Management Agency via letter dated April 24, 1998. A copy of this letter and revised map have been included in Appendix G for reference. As shown on the revised FIRM Panel 350001C0141 D and 141D, effective April 24, 1998, no portion of the proposed building or parking areas are included in a 100-year floodplain. The proposed building site is included in a Zone X. A small portion of the south portion of the site is included in a Zone AO (Depth 1). This floodplain is not within the proposed development area.

METHODOLOGY

The hydrology for this project was analyzed using the January 1993 revision of the City of Albuquerque Development Process Manual, Section 22.2 as follows:

The specific values used for this analysis are as follows:

-Precipitation Zone 3

-Design Storm 100-year, 6-hour duration
i = 2.60 inches ($t_c = 0.2$ hours)

The AHYMO computer model of the runoff volumes and peak flow rates are included in the Appendix B for reference.

FIRM FLOOD INSURANCE RATE MAP

BERNALILLO COUNTY, NEW MEXICO AND INCORPORATED AREAS

PANEL 141 OF 825
SEE MAP INDEX FOR PANELS NOT PRINTED

CONTAINS COMMUNITY NUMBER PANEL SUFFIX
REVISED TO

REFLECT LOMR

DATED APR 24 1998

MAP NUMBER
35001C0141 D

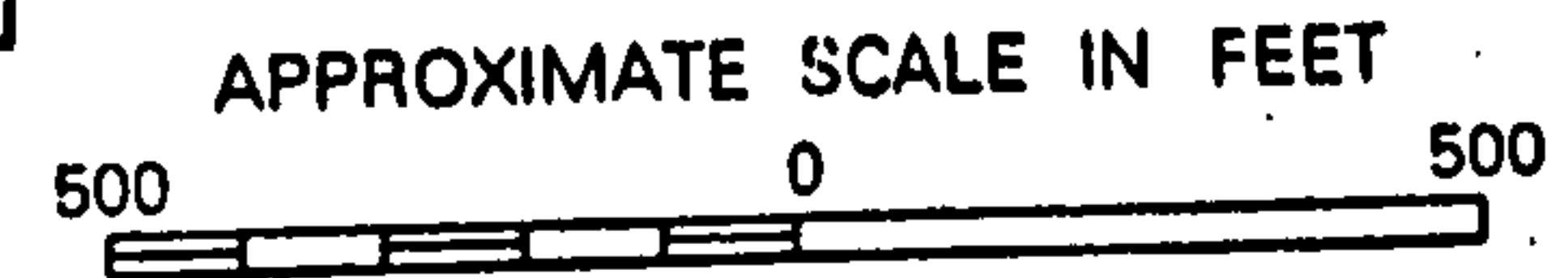
EFFECTIVE DATE:
SEPTEMBER 20, 1996



Federal Emergency Management Agency

MAP LEGEND

Revised 100-Year Floodplain



THIS AREA WAS REVISED BY LOMR DATED MARCH 25, 1998

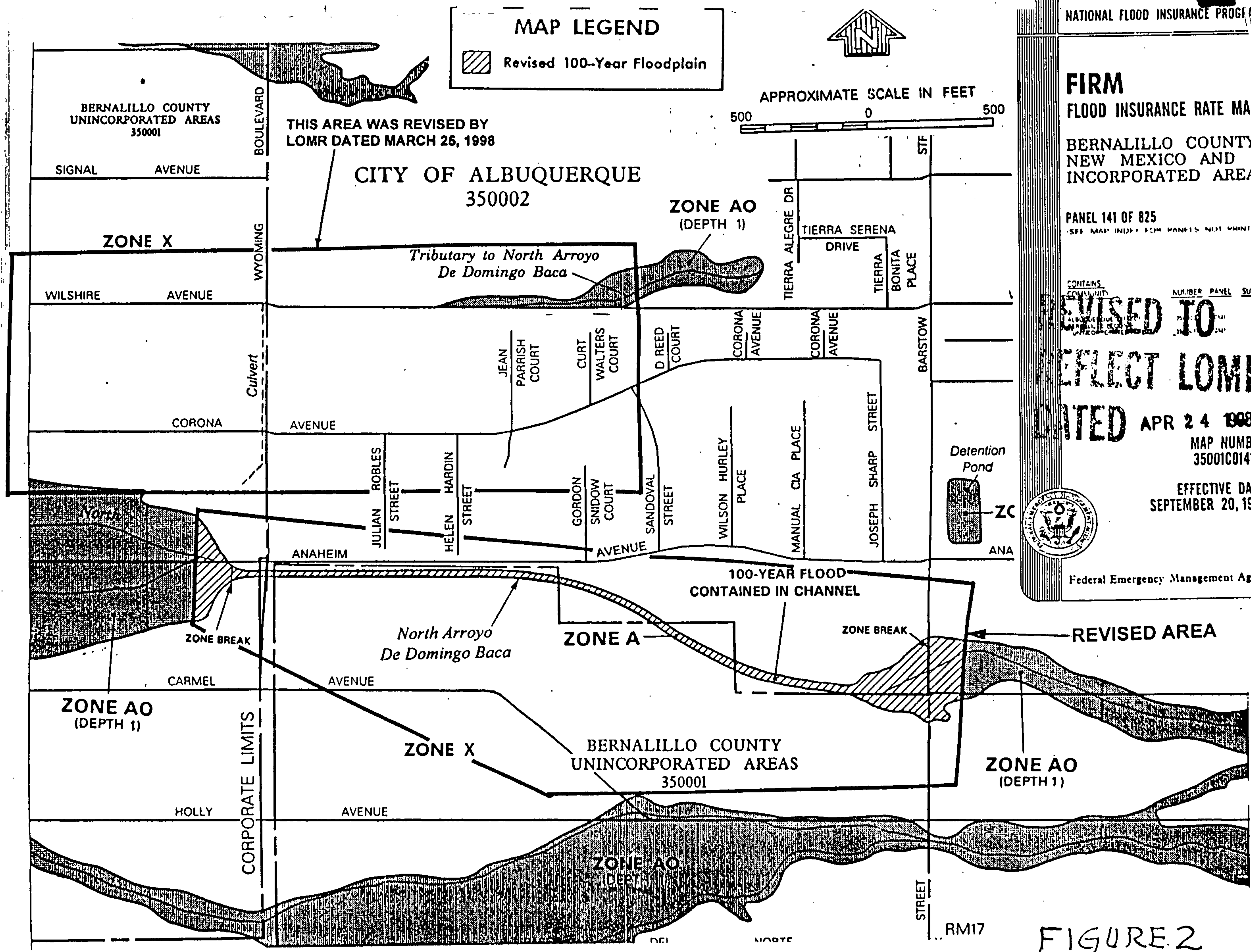
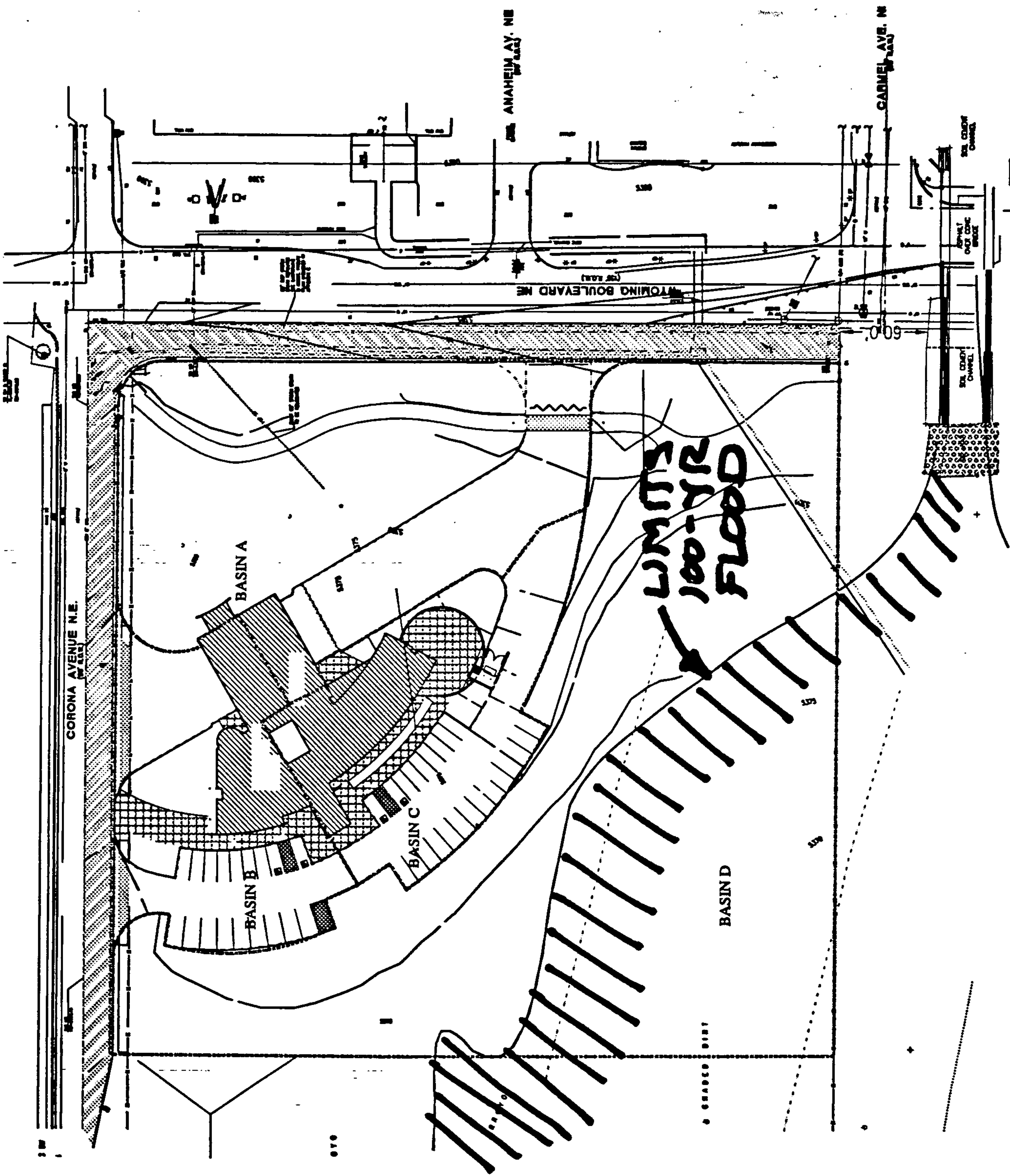
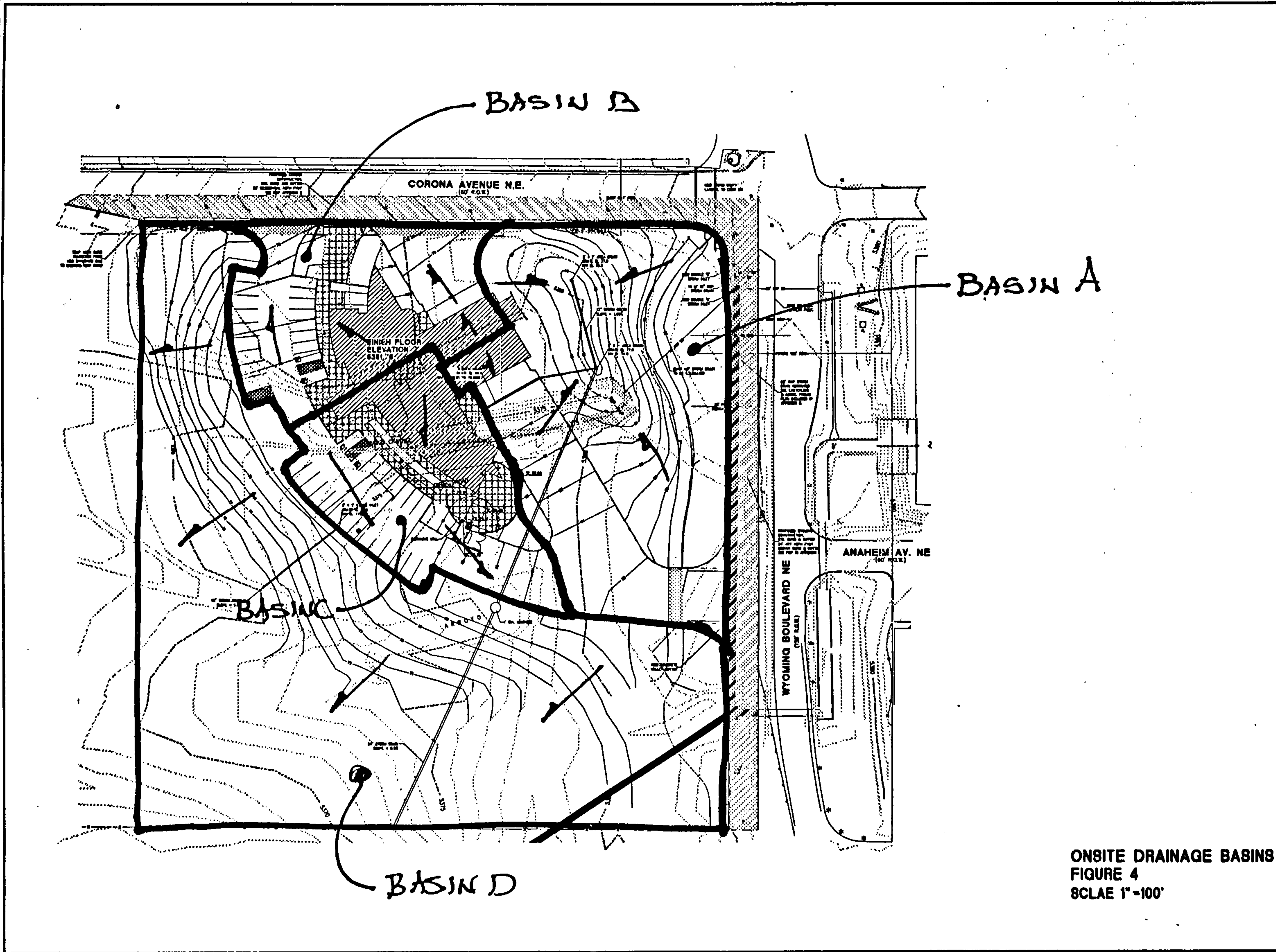


FIGURE 2



**100-YR FLOODPLAIN
FIGURE 3
1" = 100'**



ON-SITE DRAINAGE CALCULATIONS

ZONE 3 (SECTION 22.1, FIGURE A-1)

TOTAL AREA - EXISTING CONDITIONS

$$A = 4.802 \text{ acres}$$

$$Q_{100} = 4.802 * 1.87 \text{ cfs/acre} = 8.98 \text{ cfs}$$

FROM SHEET FLOWS WEST INTO THE WINDOW CHANNEL

$$Q_{10} = .66 * 8.98 = 5.93 \text{ cfs}$$

$$V_{100} = 4.802 * 0.64 \left(\frac{43560}{12} \right) = 11,505 \text{ cF}$$

$$V_{10} = .66 * 11,505 = 7,662 \text{ cF}$$

DEVELOPED CONDITIONS

BASIN A

$$\text{TOTAL AREA} = 56,160 \text{ SF} \Rightarrow 1.29 \text{ ac}$$

$$A_D = 14,105 \text{ SF} \Rightarrow 0.3238 \text{ ac}$$

$$A_C = 42,055 \text{ SF} \Rightarrow 0.9655 \text{ ac}$$

$$Q_{100} = 0.3238 * 5.02 + 0.9655 * 3.45 = 4.96 \text{ cfs}$$

$$Q_{10} = .66 * 4.96 = 3.27 \text{ cfs}$$

$$V_{100} = (0.3238 * 2.36 + 0.9655 * 1.29) \frac{43560}{12}$$

$$= 7295 \text{ cF}$$

$$V_{10} = .66 * 7295 = 4815 \text{ cF}$$

$$Q_{\text{OUTFALL CAP}} = 32 \text{ cfs} \rightarrow Q_{100} = 4.96 \text{ cfs OK}$$

BASIN B

$$\text{TOTAL AREA} = 25,200 \text{ sf} \Rightarrow 0.5785 \text{ ac}$$

$$A_D = 24,120 \text{ sf} \Rightarrow 0.5537 \text{ ac}$$

$$A_C = 1080 \text{ sf} \Rightarrow 0.025 \text{ ac}$$

$$Q_{100} = 0.5785 * 5.02 + 0.025 * 3.45 = 2.99 \text{ cfs}$$

$$Q_{10} = .66 * 2.99 = 1.97 \text{ cfs}$$

$$V_{100} = (.5785 * 2.36 + .025 * 1.29) \frac{43560}{12}$$

$$= 5073 \text{ cf}$$

$$V_{10} = .66 * 5073 = 3348 \text{ cf}$$

BASIN C

$$\text{TOTAL AREA} = 34,080 \text{ sf} \Rightarrow 0.7824 \text{ ac}$$

CONSIDER ALL TYPE D SOIL

$$Q_{100} = .7824 * 5.02 = 3.93 \text{ cfs}$$

$$Q_{10} = .66 * 3.93 = 2.59 \text{ cfs}$$

$$V_{100} = .7824 * 1.29 * \frac{43560}{12} = 3664 \text{ cf}$$

$$V_{10} = .66 * 3664 = 2418 \text{ cf}$$

BASIN D

TOTAL AREA - 93,735 sf \Rightarrow 2.15 ac

CONSIDER ALL TYPE B SINCE IT WILL HAVE BEEN GRADED.

$Q_{100} = 2.15 * 5.02 = 10.79 \text{ cfs}$

$Q_{10} = 10.79 * .66 = 7.12 \text{ cfs}$

$V_{100} = 2.15 * 2.36 * \frac{43560}{12} = 18,419 \text{ cf}$

$V_{10} = 18,419 * .66 = 12,156 \text{ cf}$

TOTAL INCREASE DUE TO DEVELOPMENT ON-SITE

EXISTING $Q_{100} = 8.98 \text{ cfs}$ $V_{100} = 11,505 \text{ cf}$

DEVELOPED

BASIN A 4.96 cfs 7295 cf

BASIN B 2.99 cfs 5073 cf

BASIN C 3.93 cfs 3664 cf

BASIN D 10.79 cfs $18,419 \text{ cf}$

INCREASE 13.69 cfs $22,996 \text{ cf}$

BASIN B OUTFALL - FROM INLET TO BASIN C
Worksheet for Circular Channel

Project Description	
Project File	c:\haestad\fmw\firesta2.fm2
Worksheet	Main Outfall from Bowl
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Capacity

Input Data	
Mannings Coefficient	0.013
Channel Slope	0.006000 ft/ft
Diameter	12.00 in

Results	
Depth	1.00 ft
Discharge	2.76 cfs
Flow Area	0.79 ft ²
Wetted Perimeter	3.14 ft
Top Width	0.00 ft
Critical Depth	0.71 ft
Percent Full	100.00
Critical Slope	0.008184 ft/ft
Velocity	3.51 ft/s
Velocity Head	0.19 ft
Specific Energy	FULL ft
Froude Number	FULL
Maximum Discharge	2.97 cfs
Full Flow Capacity	2.76 cfs
Full Flow Slope	0.006000 ft/ft

BASIN OUTFALL - FROM INLET TO MANHOLE
Worksheet for Circular Channel

Project Description	
Project File	c:\haestad\fmw\firesta2.fm2
Worksheet	Main Outfall from Bowl
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Capacity

Input Data	
Mannings Coefficient	0.013
Channel Slope	0.005000 ft/ft
Diameter	18.00 in

Results		
Depth	1.50	ft
Discharge	7.43	cfs
Flow Area	1.77	ft ²
Wetted Perimeter	4.71	ft
Top Width	0.00	ft
Critical Depth	1.06	ft
Percent Full	100.00	
Critical Slope	0.007032	ft/ft
Velocity	4.20	ft/s
Velocity Head	0.27	ft
Specific Energy	FULL	ft
Froude Number	FULL	
Maximum Discharge	7.99	cfs
Full Flow Capacity	7.43	cfs
Full Flow Slope	0.005000	ft/ft

OUTFALL FROM MANHOLE TO ARROYO
Worksheet for Circular Channel

Project Description	
Project File	c:\haestad\fmw\firesta2.fm2
Worksheet	Main Outfall from Bowl
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Capacity

Input Data	
Mannings Coefficient	0.013
Channel Slope	0.005000 ft/ft
Diameter	24.00 in

Results		
Depth	2.00	ft
Discharge	16.00	cfs
Flow Area	3.14	ft ²
Wetted Perimeter	6.28	ft
Top Width	0.00	ft
Critical Depth	1.44	ft
Percent Full	100.00	
Critical Slope	0.006612	ft/ft
Velocity	5.09	ft/s
Velocity Head	0.40	ft
Specific Energy	FULL	ft
Froude Number	FULL	
Maximum Discharge	17.21	cfs
Full Flow Capacity	16.00	cfs
Full Flow Slope	0.005000	ft/ft

TABLE A-6

NORTH DOMINGO BACA EXISTING CONDITION

Sub-basin	Area (acres)	10-yr Vol (ac-ft)	10-yr Qp (cfs)	100-yr Vol (ac-ft)	100-yr Qp (cfs)
922	.0210	0.665	16.25	1.398	32.59
922.1	.0070	0.180	4.91	.394	11.18
922.2	.0148	0.781	21.04	1.396	35.69
922.3	.0415	2.190	58.97	3.913	100.3
923.0	.0070	0.158	4.92	.370	11.32
924.1	.0190	0.233	7.75	.733	24.11
924.2	.0070	0.136	3.99	.335	10.16
924.3	.0270	1.593	41.20	2.753	68.50
924.4	.0172	0.358	10.81	.862	26.21
925.1	.0640	3.766	96.60	6.547	162.20
925.2	.0140	0.169	5.62	.536	17.65
925.3	.0105	0.614	15.82	1.063	26.43
925.4	.0370	2.246	58.52	3.887	96.45
926.0	.0375	1.326	36.64	2.624	72.25
926.1	.0120	0.408	12.54	.836	24.21
929.0	.0240	1.658	41.00	2.752	65.77
930.0	.0850	4.874	125.30	8.468	211.88
931.0	.0605	3.619	62.04	6.185	104.39
932.1	.0073	0.450	11.58	.766	19.08
932.2	.0073	0.450	11.46	.766	18.89
932.3	.0313	1.928	49.09	3.284	80.93
932.4	.0574	3.605	91.59	6.135	150.03
934.1	.0468	2.303	61.41	4.148	107.84

TABLE A-6 (cont.)

NORTH DOMINGO BACA EXISTING CONDITION

Sub-basin	Area (acres)	10-yr Vol (ac-ft)	10-yr Qp (cfs)	100-yr Vol (ac-ft)	100-yr Qp (cfs)
935.0	.1100	1.668	53.54	4.640	151.68
937.0	.0352	0.680	20.09	1.680	51.06
939.14	.0112	0.714	18.32	1.203	29.58
939.16	.0128	0.700	18.24	1.219	30.89
940.0	.0141	0.771	20.09	1.343	34.02
940.1	.0070	0.479	11.73	.791	18.82
940.2	.0156	0.853	22.23	1.486	37.64
942.1	.0469	2.362	62.18	4.197	108.16
942.2	.1031	5.193	121.03	9.227	212.49
943.1	.0120	0.793	19.85	1.322	31.97
943.2	.0130	0.230	6.74	.582	17.86
960.0	.0075	0.418	11.02	.727	18.46

AMAFCA Sediment and Erosion Design Guide, (RCE 11/94)

Assumptions: 1. Wide rectangular channel 2. Uniform Flow 3. Manning's n=0.035 4. width/depth ratio, F=(W/D)=40	Flow Characteristics:	
	input →	Q100= 1869 cfs
	input →	S= 0.032 ft/ft
		Dominant Discharge, Qd = 374 cfs

Critical slope, Sc – Equation 3.80:
 $Sc = 0.037 Qd^{-0.133} = 0.017$

Dominant channel width, Wd.

<i>Supercritical flow</i>	$Wd = 4.6 Qd^{0.4} =$	49.18 feet
<i>Subcritical flow</i>	$Wd = 2.46 Qd^{(0.375)S^{(-0.188)}}$	43.32 feet
		<i>use→</i> 49.18 feet

Meander wave length and unconstrained bend length – Equation 3.74:

<i>for Qd < 200 cfs</i>	$fee/Wd = 10$	10 feet
<i>for 200 < Qd < 2000 cfs</i>	$fee/Wd = 0.8 + 4 \cdot \log Qp =$	11.09 feet
<i>for Qd > 2000 cfs</i>	$fee/Wd = 14$	14 feet
		<i>use→</i> 11.09 feet

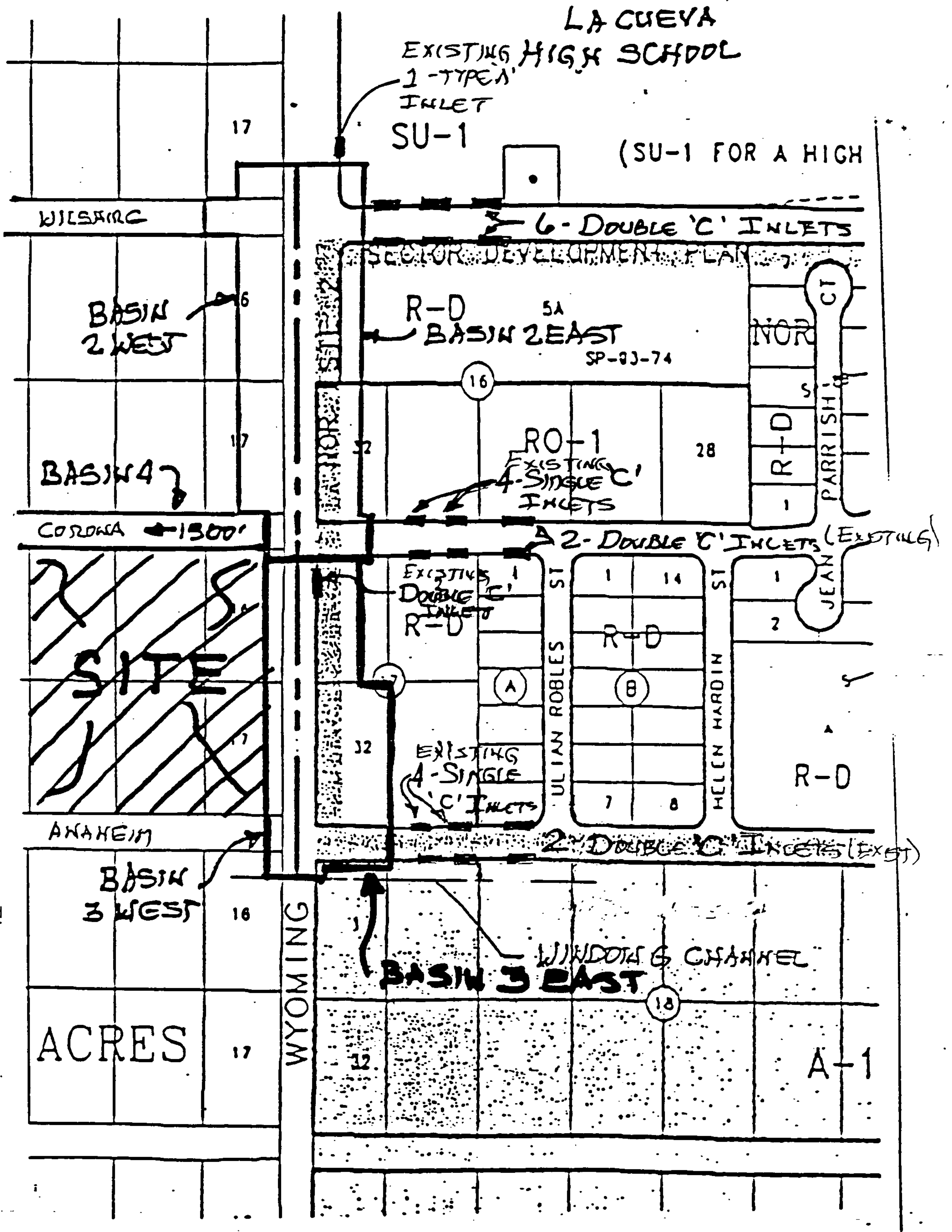
Maximum deviation of a channel from a straight line – Equation 3.75

<i>for Qd < 200 cfs</i>	$\Delta max = 2.5 Wd$	122.96 feet
<i>for 200 < Qd < 2000 cfs</i>	$\Delta max = [0.2 + \log(Qd)]Wd$	136.37 feet
<i>for Qd > 2000 cfs</i>	$\Delta max = 3.5 Wd$	172.14 feet
		<i>use→</i> 136.37 feet

Maximum deviation of a channel from a straight line – Equation 3.81

<i>for Qd < 200 cfs</i>	$\Delta max = (11.5 Qd^{0.4})$	122.96 feet
<i>for 200 < Qd < 2000 cfs</i>	$\Delta max = [0.92 + 4.6 \log(Qd)]Qd^{0.4}$	136.37 feet
<i>for Qd > 2000 cfs</i>	$\Delta max = 16.1 Qd^{0.4}$	172.14 feet
		<i>use→</i> 136.37 feet

Delta max represents the bankline setback (BSB),
 The centerline setback is $BSB + 1/2 Wd$ Centerline Setback → 160.96 feet



OFFSITE DRAINAGE BASINS
SCALE 1=200"

OFFSITE RUNOFF

ASSUMPTIONS:

1. ALL EXISTING STORM INLET SYSTEMS ARE DESIGNED FOR 100% INTERCEPTION.

2. WYOMING SECTION (FUTURE)

- Full Future ROW = 136'
6' SW + 3-12' Lanes + 28' MEDIAN + 3-12' LANES + 6' SW

$$D = 6 + 36 = 42'$$

$$C = 28/2 = 14' \text{ (NOW-PAVED MEDIAN)}$$

CALCULATIONS:

BASIN 2 WEST

$$A = 0.57 \text{ ac}$$

$$A_D = 42' * 455' + 40' * 40' = 0.48 \text{ ac}$$

(WYOMING) (WILSON)

$$A_C = 0.57 - 0.48 = 0.09 \text{ ac}$$

ZONE B (PER DPM SECTION 22.2 - FIGURE A-1)

$$Q_{100}(D) = 0.48 * (5.02 \text{ cfs/acre}) = 2.41 \text{ cfs}$$

$$Q_{100}(C) = 0.09 * (3.45 \text{ cfs/acre}) = 0.31 \text{ cfs}$$

$$\text{TOTAL } Q_{100} = 2.72 \text{ cfs}$$

$$D = 0.20' \text{ (SEE RATING TABLE NEXT PAGE)}$$

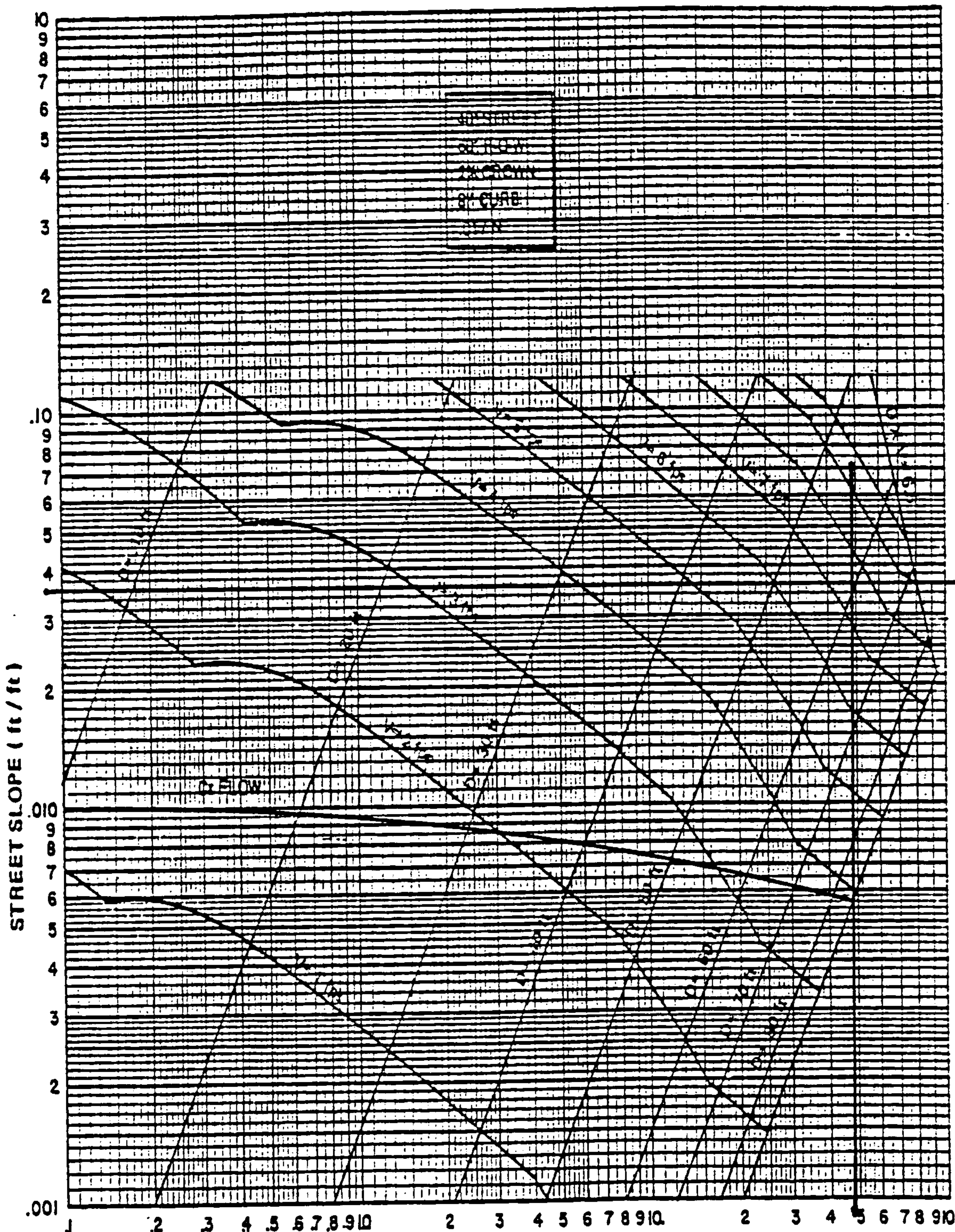
FLOW DEPTH IN WYOMING FROM BASIN 2WEST
Worksheet for Irregular Channel

Project Description	
Project File	a:\fire sta.fm2
Worksheet	WYOMING CAPACITY - NORTH OF CORONA
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data					
Channel Slope	0.020342 ft/ft				
Elevation range: 98.77 ft to 100.00 ft.					
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness	
0.00	100.00	0.00	52.63	0.017	
28.00	99.44				
28.63	98.77				
52.63	99.25				
Discharge	2.72	cfs			

Results		
Wtd. Mannings Coefficient	0.017	
Water Surface Elevation	98.97	ft
Flow Area	1.02	ft ²
Wetted Perimeter	10.28	ft
Top Width	10.19	ft
Height	0.20	ft
Critical Depth	99.00	ft
Critical Slope	0.008705	ft/ft
Velocity	2.67	ft/s
Velocity Head	0.11	ft
Specific Energy	99.08	ft
Froude Number	1.49	
Flow is supercritical.		

STREET CAPACITY



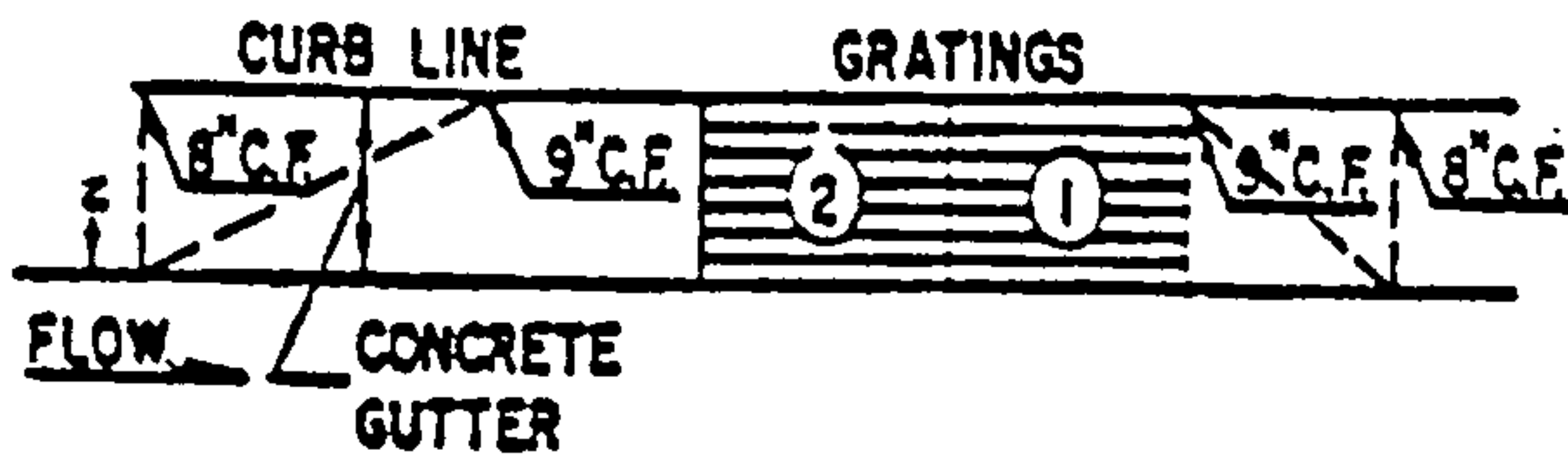
3.690

ONE HALF STREET FLOWS (cfs)

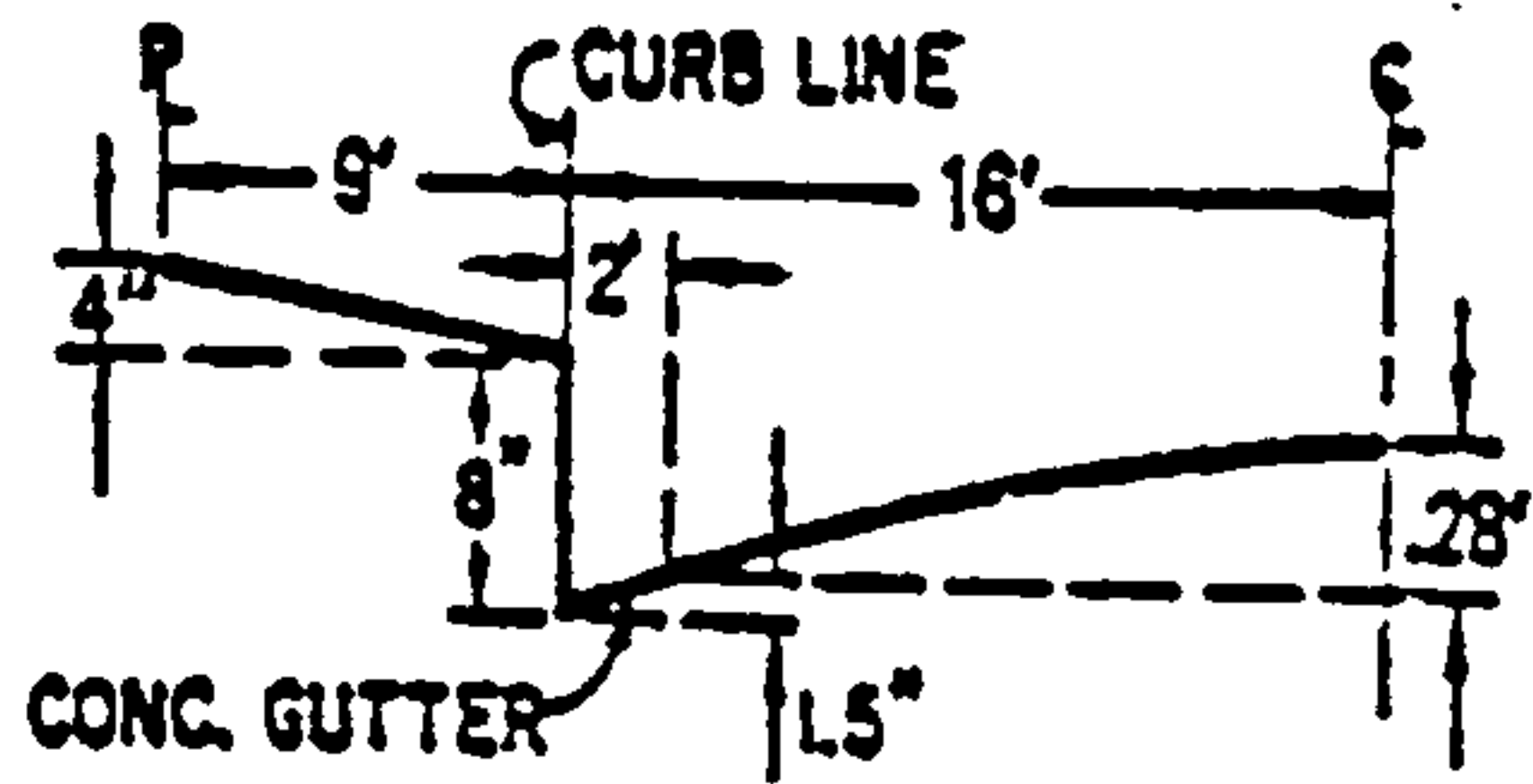
$Q_{100} = 4.9 \text{ cfs}$
 $d = 0.54' < 0.87 \text{ of}$

PLATE 22.3 D-3

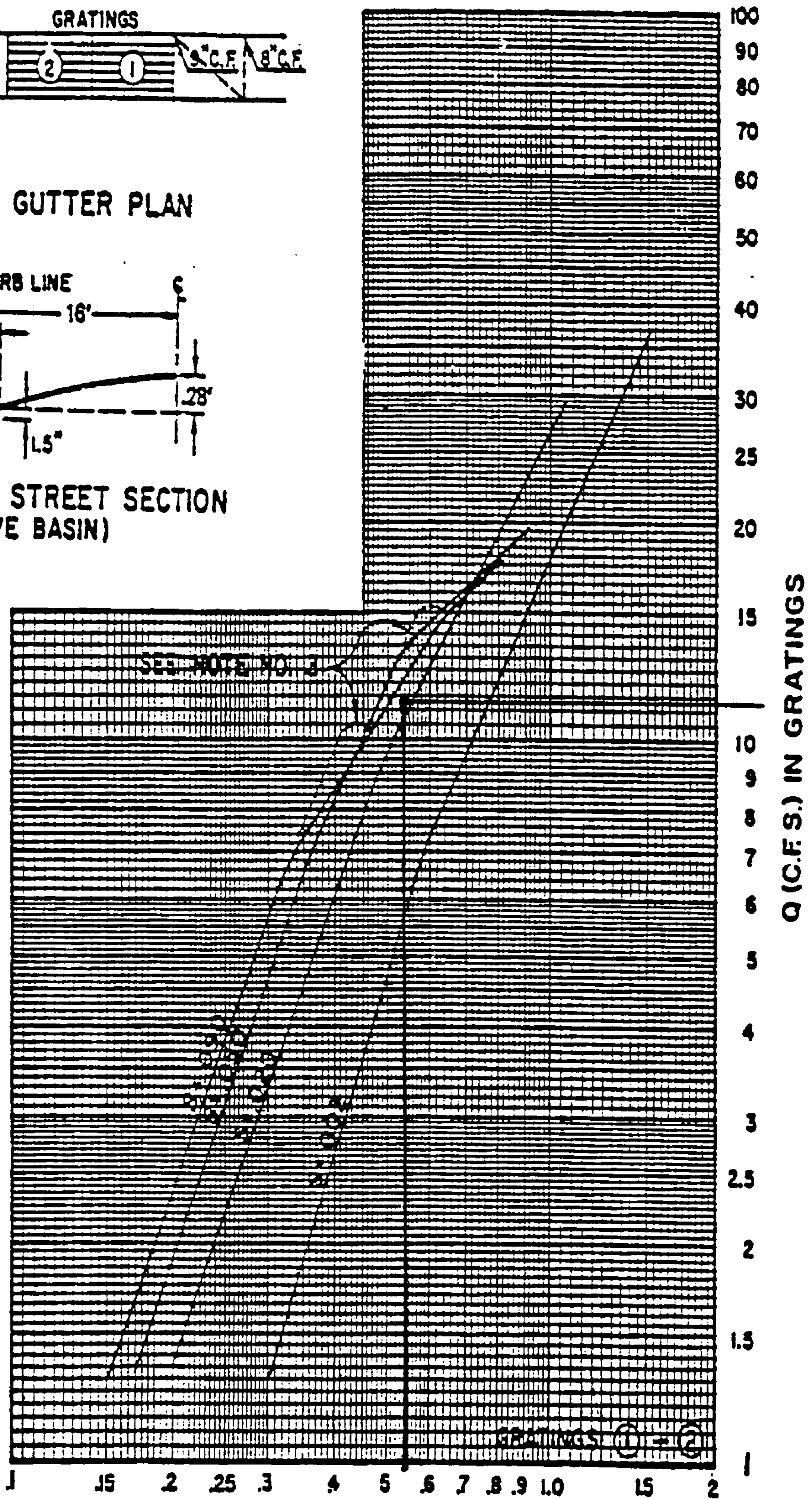
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)



D = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

$S = 3.6\%$

$d = 0.54'$

$Q_i = 11 \text{ cfs} \quad Q_{100} = 4.9 \text{ cfs} \quad \text{OK}$

CORONA AVENUE

EXISTING CAPACITY - WITHOUT FS-20

$$S = 3.6\%$$

$$D = 1473'$$

WYOMING TO EXISTING INLET - SOUTH SIDE
OF CORONA @ MURRELET DRIVE (FALCON
RIDGE SUBDIVISION)

$$W(\text{NORTH}) - \text{STREET} - 20' \quad D = \frac{26}{30} = .87$$

$$\text{SIDEWALK} - 6' \quad C = .13$$

$$\text{DIRT} - 4'$$

$$W(\text{SOUTH}) - \text{STREET} - 4' \quad D = 1.0$$

SIDEWALK - NONE

DIRT - NONE - LAND SLOPES SOUTH AWAY FROM
STREET

$$Q_{100}(\text{NORTH}) = 5.02 * 1.014 * (.87) + 3.45 * 1.014 * (.13) = 4.9c$$

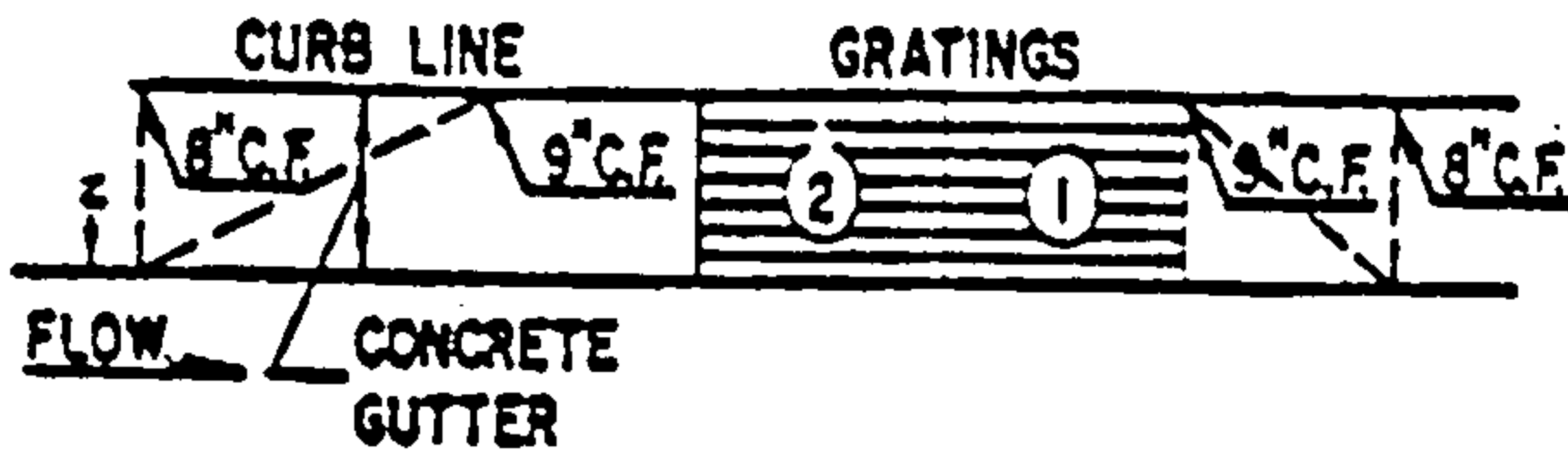
$$A = 1473 * 30 = 44,190 \text{ (1.014 ac)}$$

$$Q_{100}(\text{SOUTH}) = 5.02 * 0.135 * 1 = 0.68 cfs$$

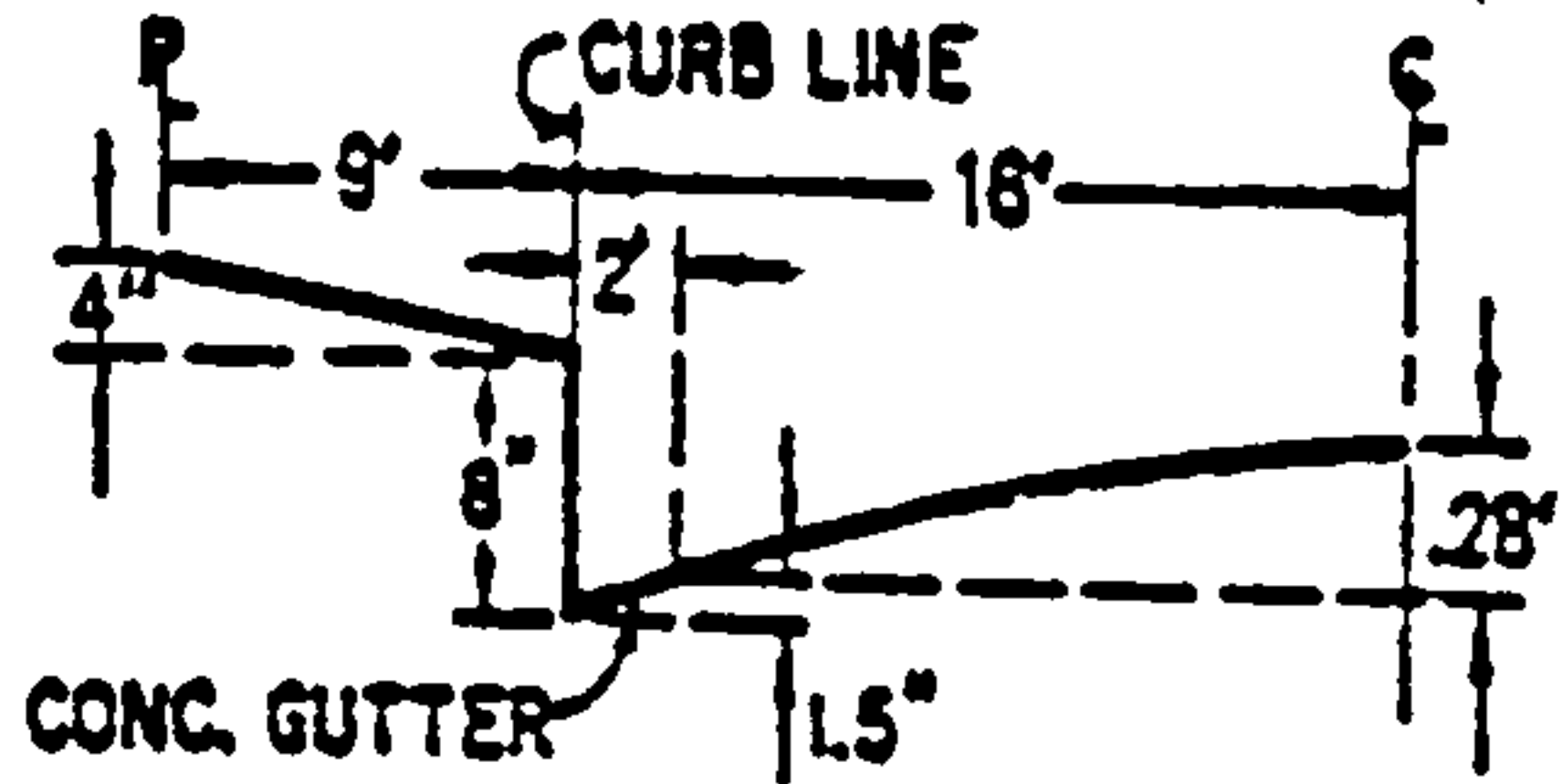
$$A = 1473 * 4 = 5892 \text{ (0.135 ac)}$$

NOTE: $Q_{100}(\text{SOUTH}) = Q_{100}(\text{NORTH}) = 4.9cfs$ for
FULLY CONSTRUCTED SECTION.

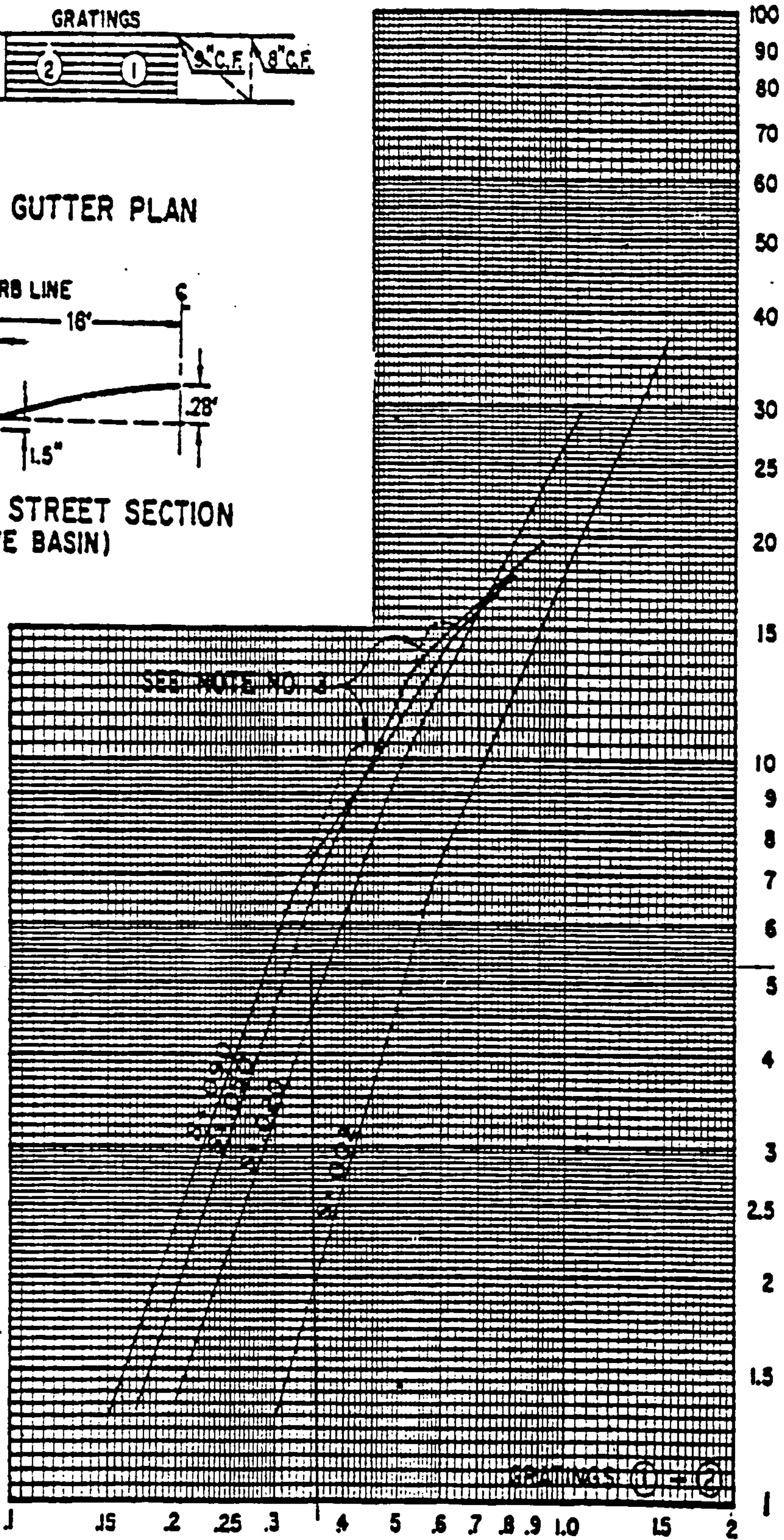
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)



$D = 99.45 - 99.13$
 $= 0.28'$

$S = 3.6\%$

$Q_i = 5.3 \text{ cfs}$

$Q_{BY} = 8.26 - 5.3$
 $= 2.96 \text{ cfs}$

No Good

D = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

CORONA TEMP SECTION W/4' TEMP PVMT
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	CORONA - EXISTING SECTION W/4' TEMP PVMT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data	
Channel Slope	0.036000 ft/ft
Elevation range: 99.13 ft to 100.12 ft.	
Station (ft)	Elevation (ft)
66.00	100.12
66.01	99.45
70.00	99.53
90.00	99.13
90.01	99.80
100.00	100.00
Discharge	8.57 cfs

Flow in South CURB = 0.35 cfs
Flow in North CURB =
8.57 - 0.35 = 8.22 cfs

Results	
Wtd. Mannings Coefficient	0.017
Water Surface Elevation	99.41 ft
Flow Area	1.95 ft ²
Wetted Perimeter	14.23 ft
Top Width	13.95 ft
Height	0.28 ft
Critical Depth	99.51 ft
Critical Slope	0.007834 ft/ft
Velocity	4.40 ft/s
Velocity Head	0.30 ft
Specific Energy	99.71 ft
Froude Number	2.08
Flow is supercritical.	

CORONA FULL SECTION W/BASIN B
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	CORONA AVE FULL SECTION
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data				
Channel Slope	0.036000 ft/ft			
Elevation range: 99.13 ft to 100.00 ft.				
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness
40.00	100.00	40.00	100.00	0.017
50.00	99.80			
50.01	99.13			
70.00	99.53			
90.00	99.13			
90.01	99.80			
100.00	100.00			
Discharge	12.79	cfs		

$Q_{100} = 4.9 + 4.9 + 2.99 \text{ (BASIN B)}$
 $= 12.79 \text{ cfs}$
 $\text{MAX DEPTH} = 99.38 - 99.13 = 0.25'$
 $< .87 \text{ OK}$

Results		
Wtd. Mannings Coefficient	0.017	
Water Surface Elevation	99.38	ft
Flow Area	3.13	ft ²
Wetted Perimeter	25.50	ft
Top Width	25.00	ft
Height	0.25	ft
Critical Depth	99.46	ft
Critical Slope	0.007863	ft/ft
Velocity	4.09	ft/s
Velocity Head	0.26	ft
Specific Energy	99.64	ft
Froude Number	2.04	
Flow is supercritical.		
Flow is divided.		

\leftarrow CROWN DEPTH FLOW NOT
 EVENLY SPLIT.

EXIST CORONA SOUTH - TEMP SECTION
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	CORONA SOUTH - EXIST
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data				
Channel Slope	0.036000 ft/ft			
Water Surface Elevation	99.41 ft			
Elevation range: 99.33 ft to 100.00 ft.				
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness
4.00	100.00	4.00	8.01	0.017
4.01	99.33			
8.01	99.41			

Results	
Wtd. Mannings Coefficient	0.017
Discharge	0.31 cfs
Flow Area	0.16 ft ²
Wetted Perimeter	4.08 ft
Top Width	4.00 ft
Height	0.08 ft
Critical Depth	99.43 ft
Critical Slope	0.011376 ft/ft
Velocity	1.91 ft/s
Velocity Head	0.06 ft
Specific Energy	99.47 ft
Froude Number	1.69
Flow is supercritical.	

$Q_{100} = 0.68 \text{ cfs}$
 $.68 - .31 = 0.37$ spills to north
 w/o FS-20
 (BASIN B)
 $Q_{100} = 0.68 + 2.99 = 3.67 \text{ cfs}$
 with FS-20 BASIN B
 $3.67 - .31 = 3.36 \text{ cfs}$ spills
 to NORTH.

100-YR FLOW DEPTH - CORONA NORTH
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	HALF CORONA AVE SECTION
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data					
Channel Slope	0.035000 ft/ft				
Elevation range: 99.13 ft to 100.00 ft.					
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness	
70.00	100.00	70.00	100.00	0.017	
80.00	99.80				
80.01	99.13				
100.00	99.53				
Discharge	4.90	cfs			

Results					
Wtd. Mannings Coefficient	0.017				
Water Surface Elevation	99.36	ft	— SINCE CROWN ELEV 99.53		
Flow Area	1.29	ft ²	THERE IS NO SPILL TO SOUTH		
Wetted Perimeter	11.60	ft			
Top Width	11.37	ft			
Height	0.23	ft			
Critical Depth	99.43	ft			
Critical Slope	0.008147	ft/ft			
Velocity	3.79	ft/s			
Velocity Head	0.22	ft			
Specific Energy	99.58	ft			
Froude Number	1.98				
Flow is supercritical.					

EXIST CORONA SOUTH - TEMP SECTION
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	CORONA SOUTH - EXIST
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

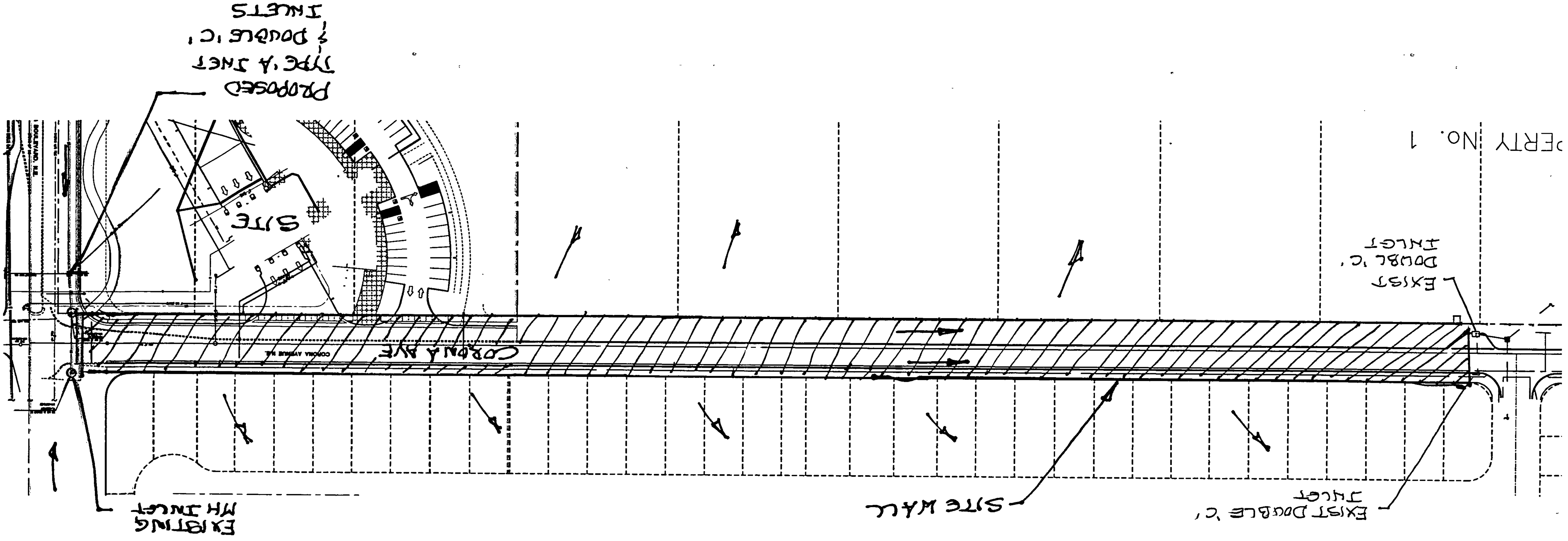
Input Data				
Channel Slope	0.036000 ft/ft			
Elevation range: 99.33 ft to 100.00 ft.				
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness
4.00	100.00	4.00	8.01	0.017
4.01	99.33			
8.01	99.41			
Discharge	0.68	cfs		

Results	
Wtd. Mannings Coefficient	0.017
Water Surface Elevation	99.43 ft
Flow Area	0.26 ft ²
Wetted Perimeter	4.13 ft
Top Width	4.00 ft
Height	0.10 ft
Critical Depth	99.47 ft
Critical Slope	0.009772 ft/ft
Velocity	2.62 ft/s
Velocity Head	0.11 ft
Specific Energy	99.54 ft
Froude Number	1.81
Flow is supercritical.	
<u>Water elevation exceeds lowest end station by 0.02 ft.</u>	

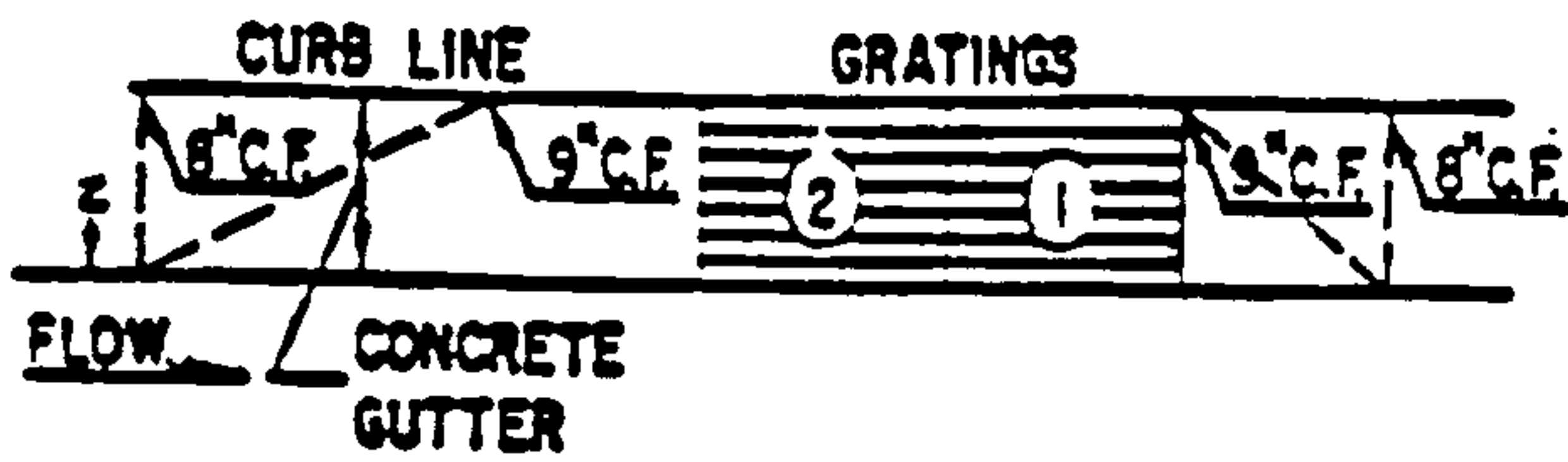
*SPILL TO NORTH
CROWN @ 99.41*

SUPPLEMENTAL ANALYSIS
BASIN 4 (OFFSITE)

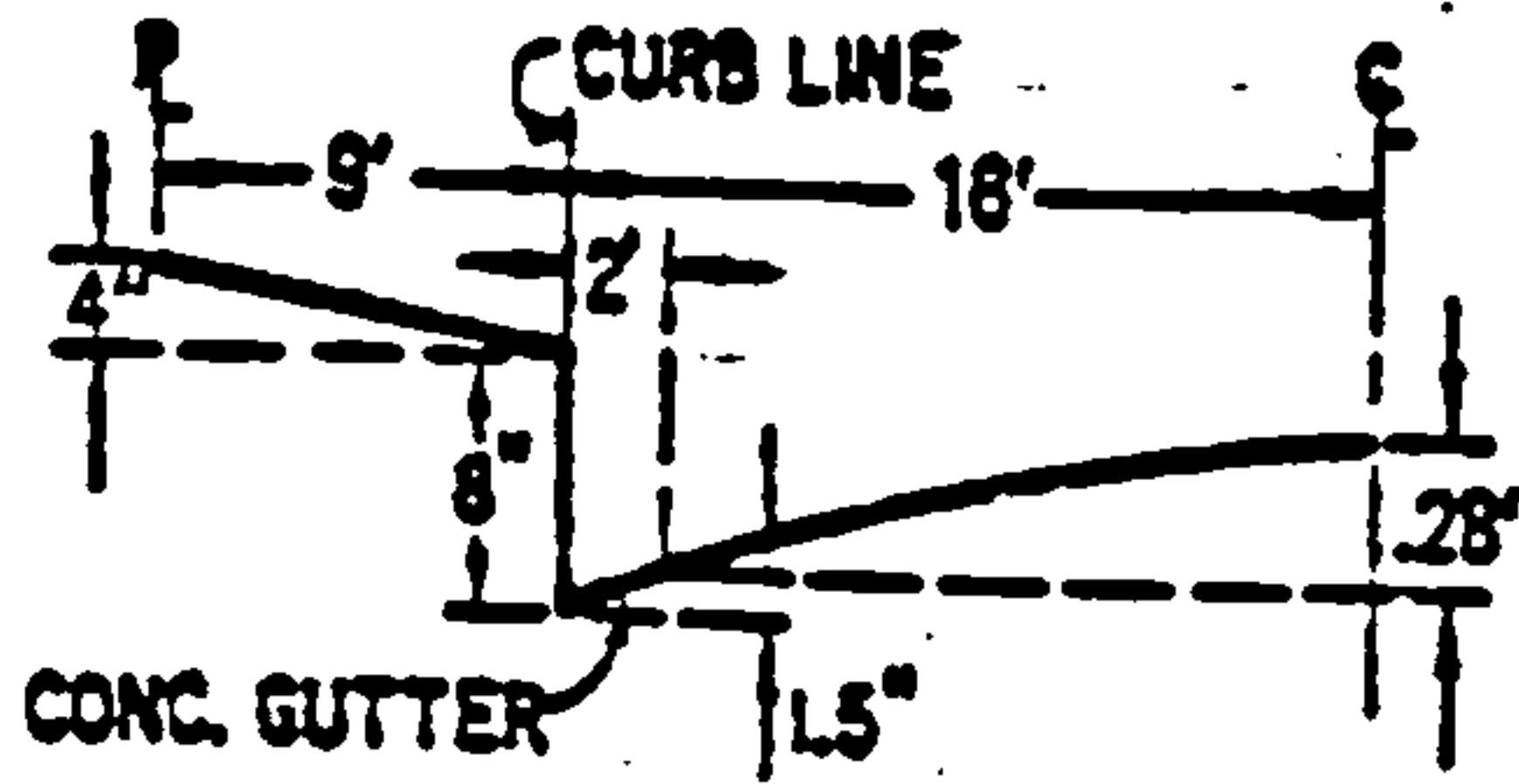
SCALE 1"=100'



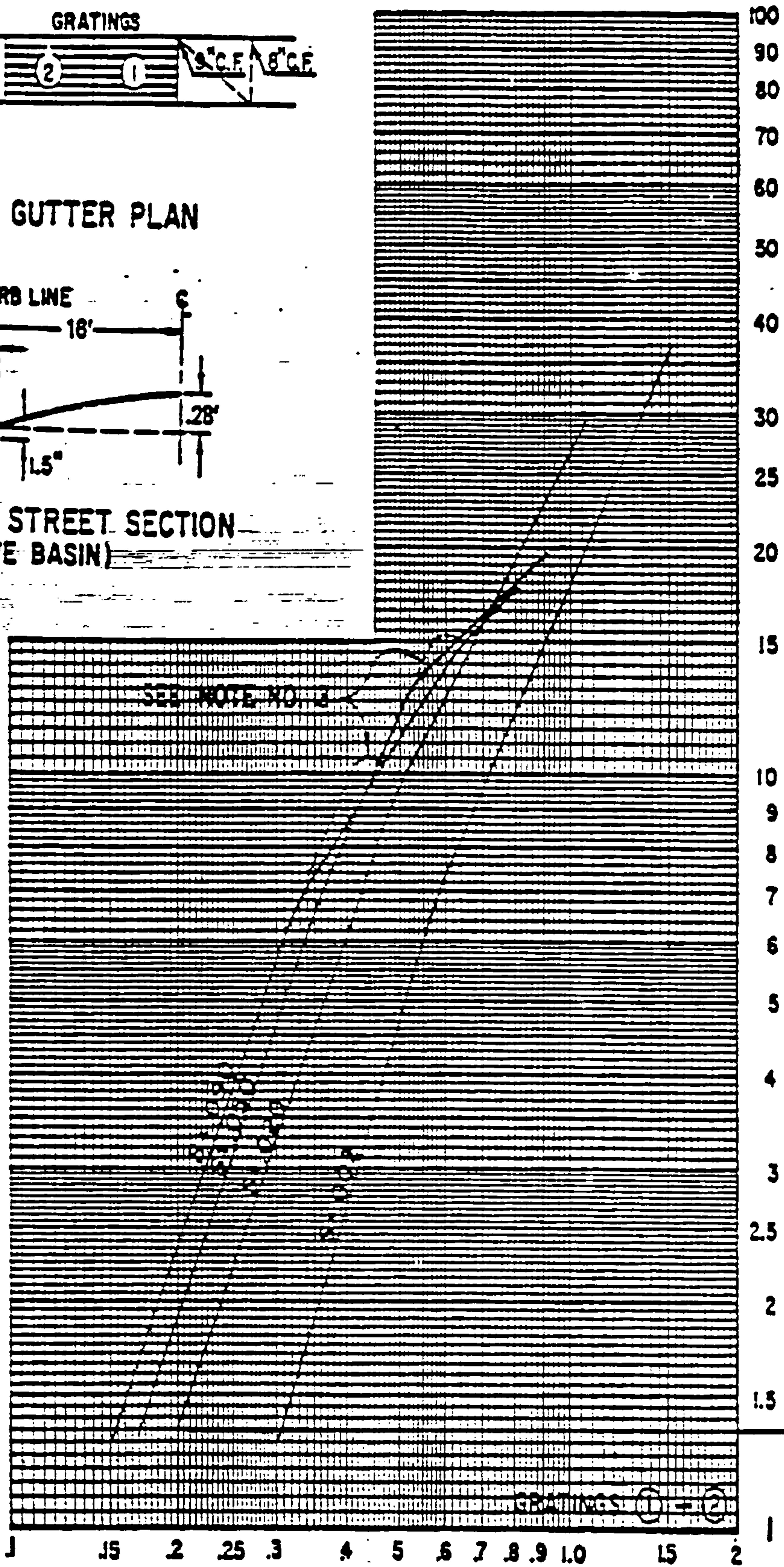
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)



$J = 0.20'$
 $S = 2.03\%$
 $Q_i = 1.4 \text{ cfs}$
 $Q_{100} = 2.7 \text{ cfs}$
 Use 2 - Double 'C'
 INLETS

$Q_i = 1.4 \text{ cfs}$

D = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

PLATE 22.3 D-6

BASIN 2 WEST

BASIN 2 EAST

$$A = 0.85 \text{ ac}$$

$$A_0 = 42' * 455' + 40' * 40' + 40' * 35' = 0.51 \text{ ac}$$

(WYOMING) (WISCONSIN) (COLORADO)

$$A_c = 0.85 - 0.51 = 0.34 \text{ ac}$$

$$Q_{100}(D) = 0.51 * 5.02 = 2.56 \text{ cfs}$$

$$Q_{100}(C) = 0.34 * 3.45 = 1.17 \text{ cfs}$$

$$\text{TOTAL } Q_{100} = 3.73 \text{ ac}$$

$$D = 0.29' \text{ (SEE WORKSHEET NEXT PAGE)}$$

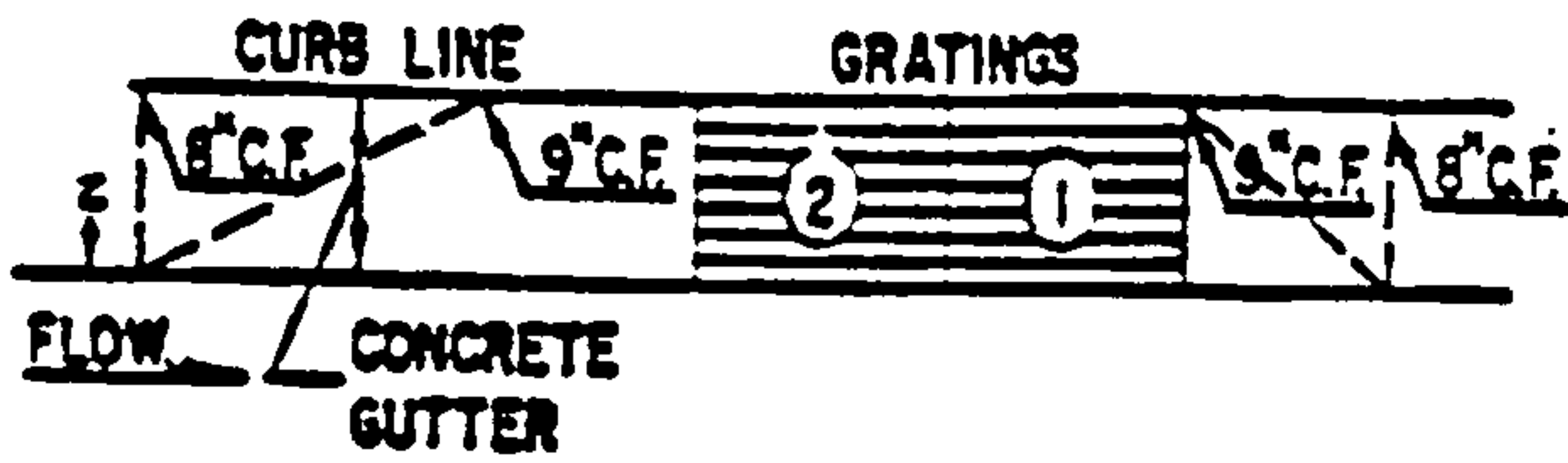
FLOW DEPTH IN WYOMING FROM BASIN 2EAST
Worksheet for Irregular Channel

Project Description	
Project File	a:\fire sta.fm2
Worksheet	WYOMING CAPACITY - NORTH OF CORONA
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

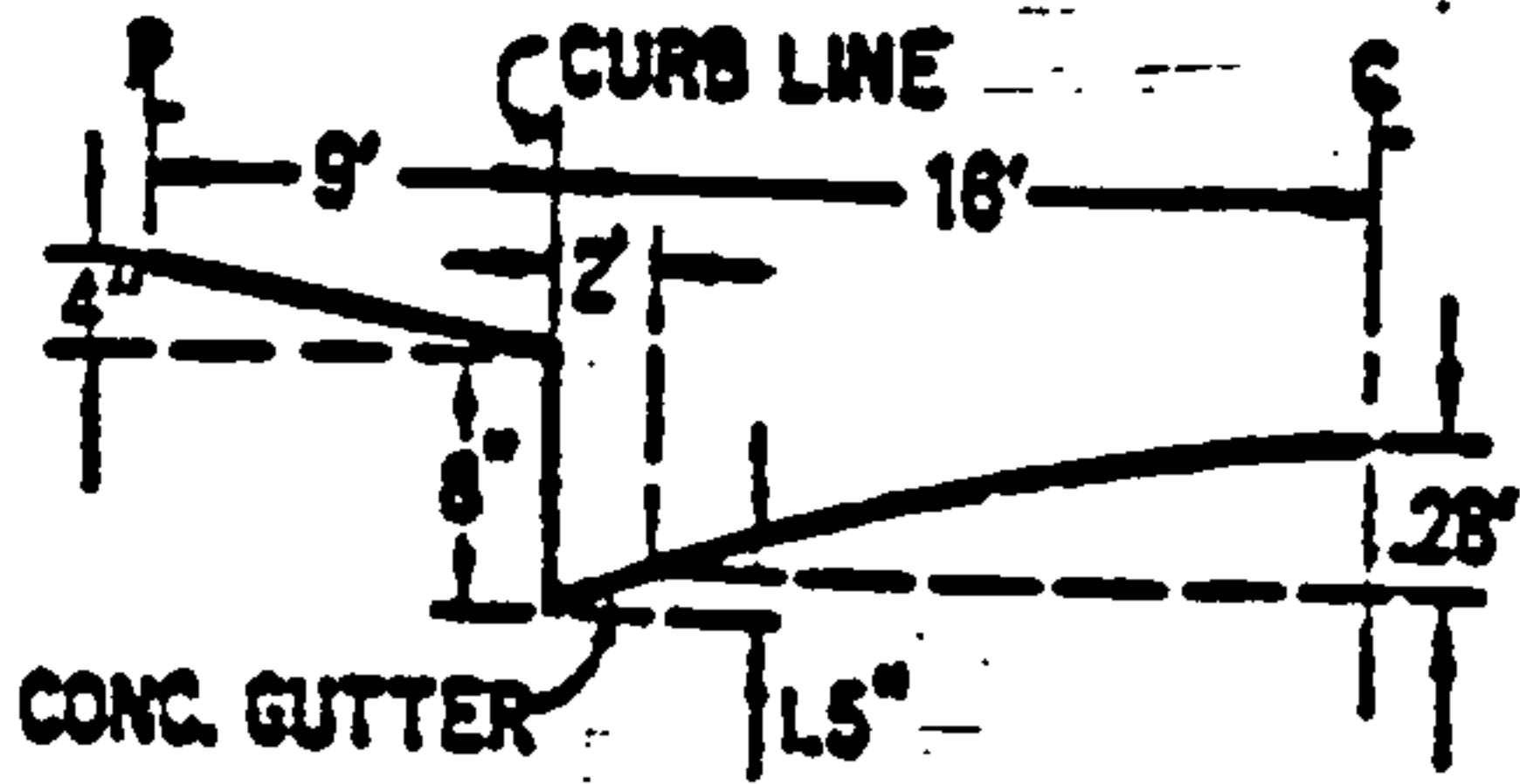
Input Data					
Channel Slope	0.020342 ft/ft				
Elevation range: 98.77 ft to 100.00 ft.					
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness	
0.00	100.00	0.00	52.63	0.017	
28.00	99.44				
28.63	98.77				
52.63	99.25				
Discharge	3.73	cfs			

Results		
Wtd. Mannings Coefficient	0.017	
Water Surface Elevation	99.00	ft
Flow Area	1.29	ft ²
Wetted Perimeter	11.57	ft
Top Width	11.47	ft
Height	0.23	ft
Critical Depth	99.04	ft
Critical Slope	0.008345	ft/ft
Velocity	2.89	ft/s
Velocity Head	0.13	ft
Specific Energy	99.12	ft
Froude Number	1.52	
Flow is supercritical.		

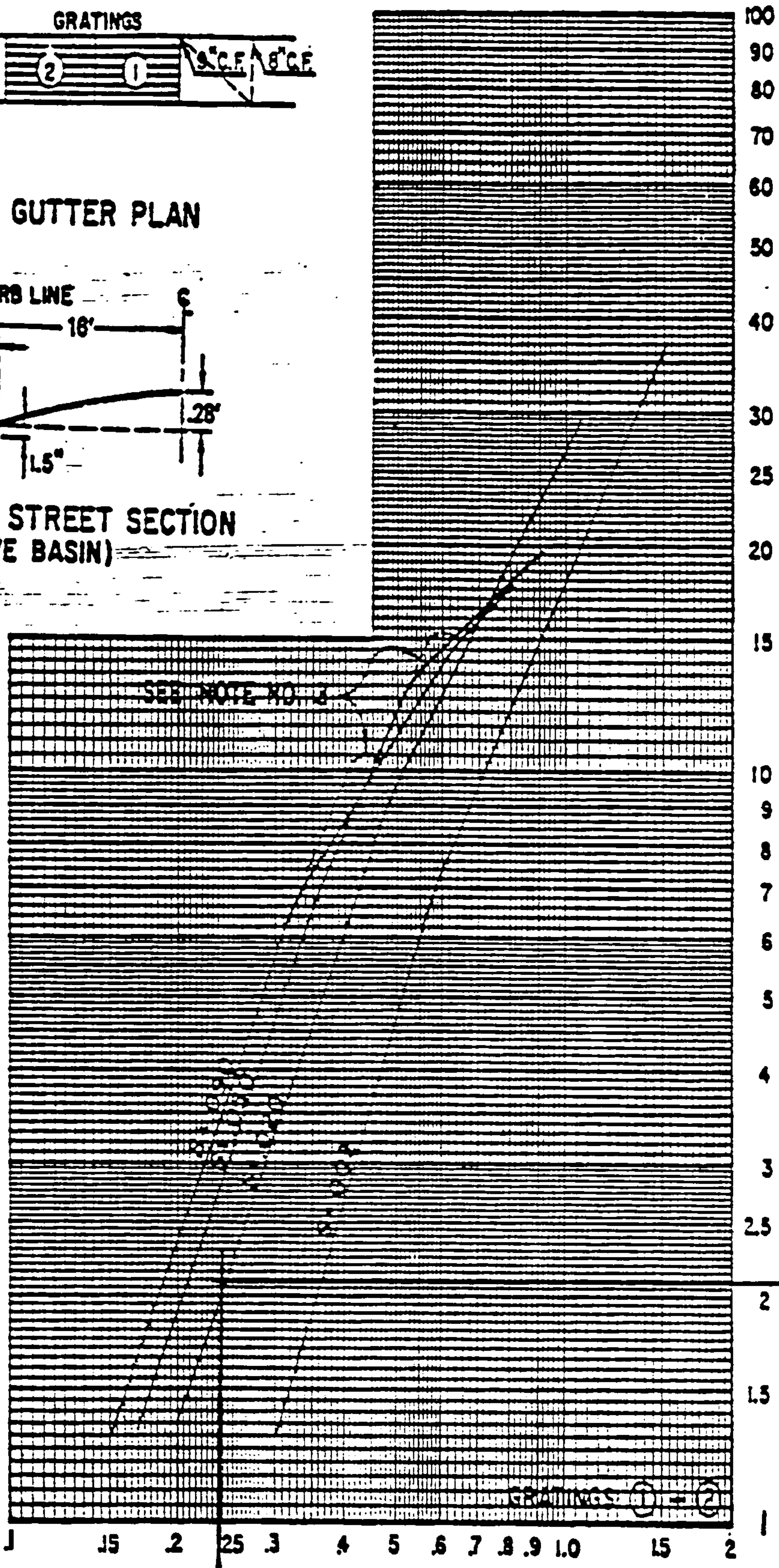
GRATING CAPACITIES FOR TYPE DOUBLE 'C,' AND 'D'



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)



$d = 0.23'$
 $s = 2.034\%$
 $Q_i = 2.1 \text{ cfs}$
 $Q_{100} = 3.73 \text{ cfs}$
 Use 2 - Double C
 INLETS

$Q_i = 2.1 \text{ cfs}$

D = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

BASIN 3 WEST

$$A = 0.34 \text{ ac}$$

$$A_D = 24 * 365 + 6 * 365 + 40 * 30 = 0.28 \text{ ac}$$

(SYPONG) (WY-SW) (ANAHERR)

$$A_C = 0.34 - 0.28 = 0.06 \text{ ac}$$

$$Q_{100}(D) = 0.28 * 5.02 = 1.41 \text{ cfs}$$

$$Q_{100}(C) = 0.06 * 3.45 = 0.21 \text{ cfs}$$

$$\text{TOTAL } Q_{100} = 1.62 \text{ cfs}$$

$$D = 0.29' \text{ SEE WORKSHEET NEXT PAGE}$$

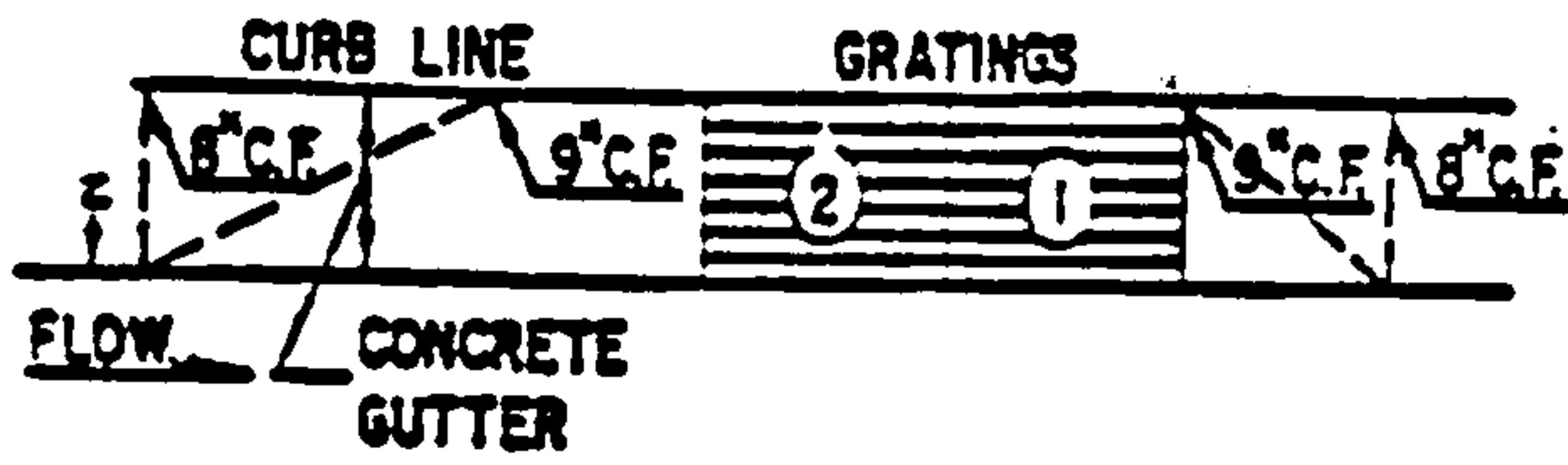
FLOW DEPTH IN WYOMING FROM BASIN 3WEST
Worksheet for Irregular Channel

Project Description	
Project File	a:\fire sta.fm2
Worksheet	WYOMING CAPACITY - NORTH OF CORONA
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

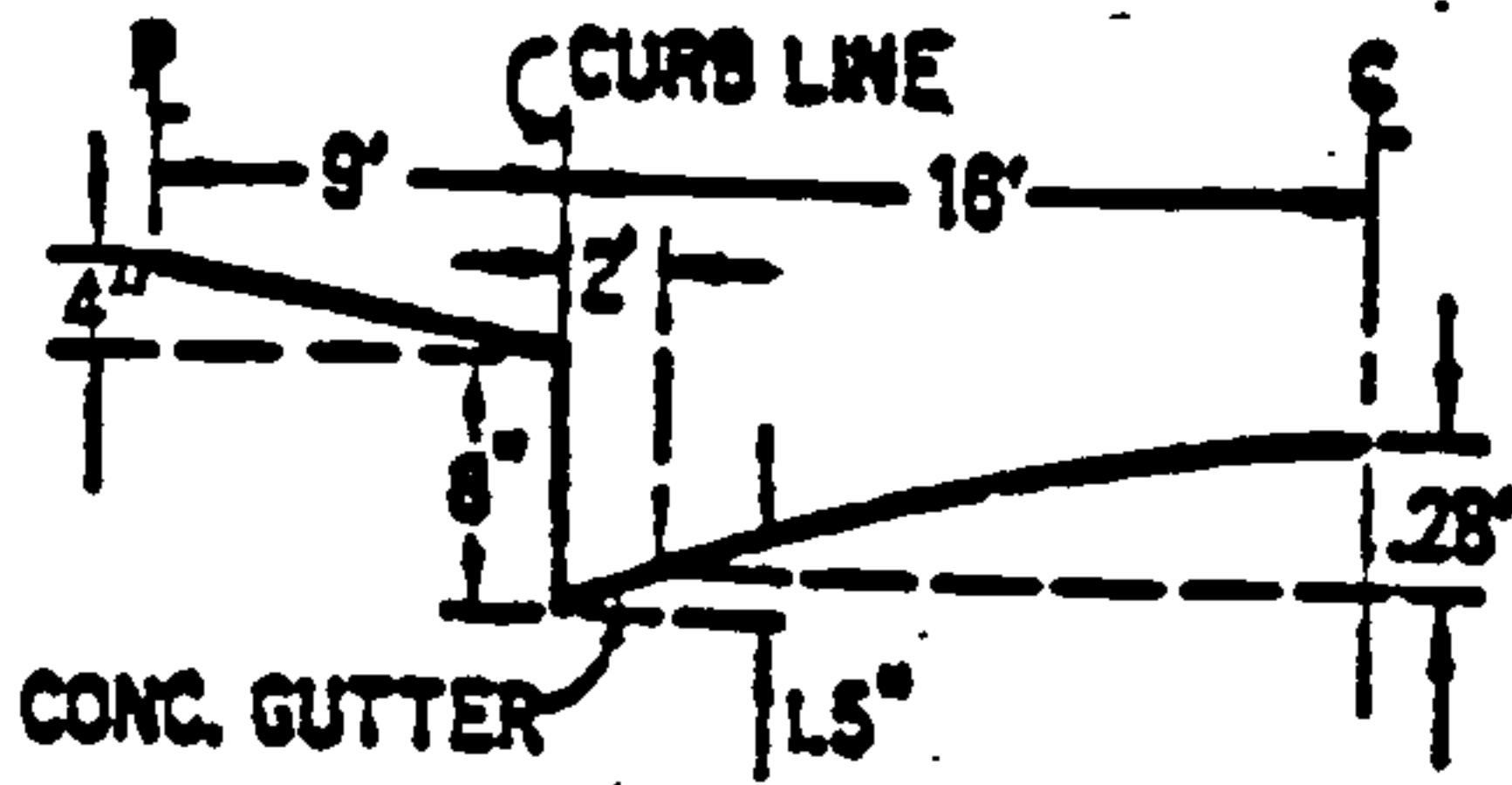
Input Data					
Channel Slope	0.008580 ft/ft				
Elevation range: 98.77 ft to 100.00 ft.					
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness	
0.00	100.00	0.00	52.63	0.017	
28.00	99.44				
28.63	98.77				
52.63	99.25				
Discharge	1.62	cfs			

Results		
Wtd. Mannings Coefficient	0.017	
Water Surface Elevation	98.96	ft
Flow Area	0.95	ft ²
Wetted Perimeter	9.95	ft
Top Width	9.86	ft
Height	0.19	ft
Critical Depth	98.96	ft
Critical Slope	0.009327	ft/ft
Velocity	1.70	ft/s
Velocity Head	0.04	ft
Specific Energy	99.01	ft
Froude Number	0.96	
Flow is subcritical.		

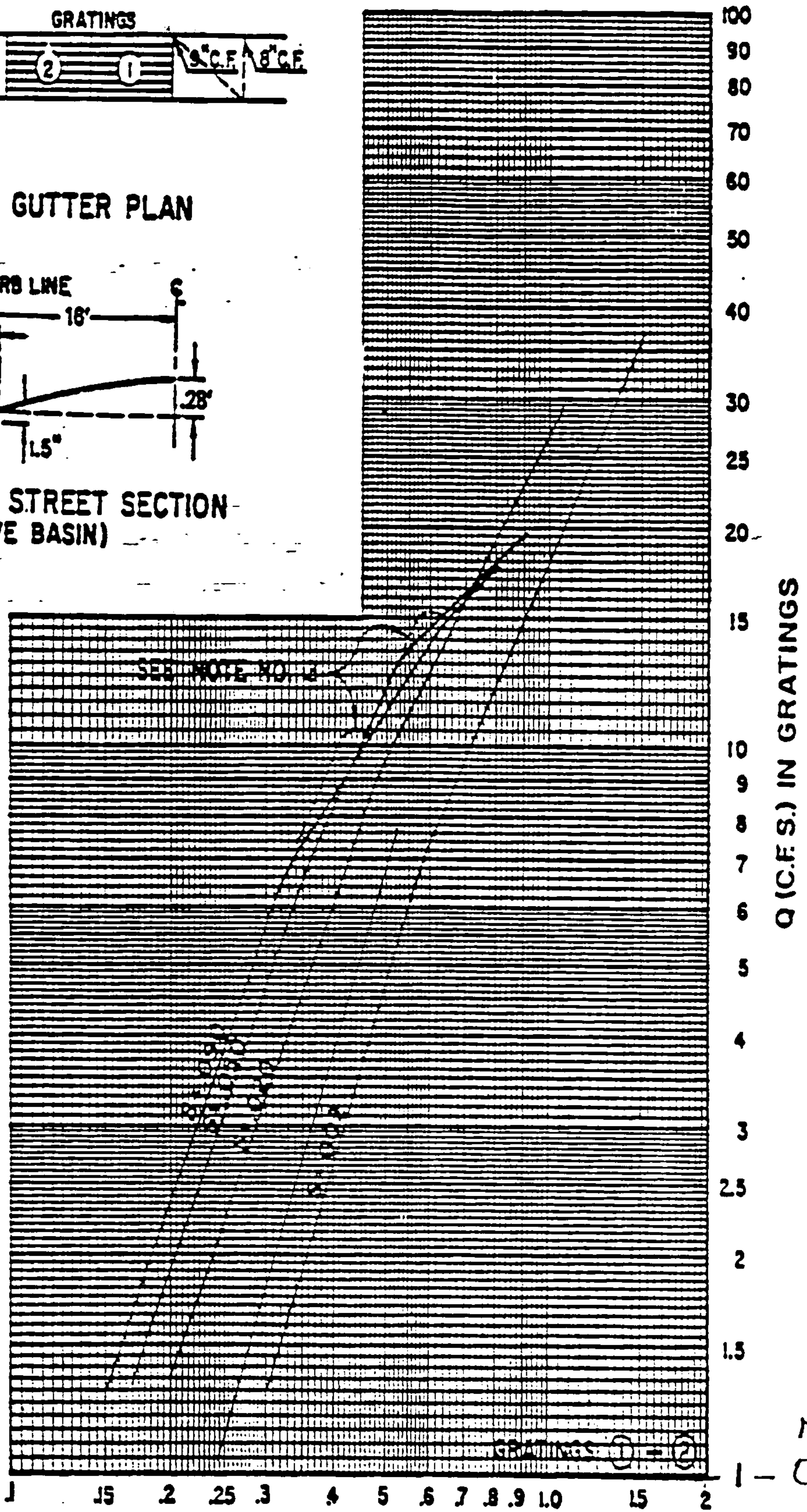
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)



$d = 0.19'$
 $s = 0.85890$
 $Q_i = 1.0 \text{ cfs}$
 $Q_{100} = 1.62 \text{ cfs}$
 Use 2-Double C
 Inlets

MIN
 $Q_i = 1 \text{ cfs}$

D = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

BASIN 3 EAST

$$A = 1.18 \text{ ac}$$

$$A_D = 24 \times 365 + 6 \times 365 + 40 \times 330 + 40 \times 30 = 0.58 \text{ ac}$$

(WYOMING) (WY-SW) (ANAFREN) (JULIAN)

$$A_C = 1.18 - 0.58 = 0.60 \text{ ac}$$

$$Q_{100}(D) = 0.58 \times 5.02 = 2.91 \text{ cfs}$$

$$Q_{100}(C) = 0.60 \times 3.45 = \underline{2.07 \text{ cfs}}$$

$$\text{TOTAL } Q_{100} = 4.98 \text{ cfs}$$

$$D = 0.29' \text{ (SEE WORK SHEET NEXT PAGE)}$$

FLOW DEPTH IN WYOMING FROM BASIN 3EAST
Worksheet for Irregular Channel

Project Description	
Project File	a:\fire sta.fm2
Worksheet	WYOMING CAPACITY - NORTH OF CORONA
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

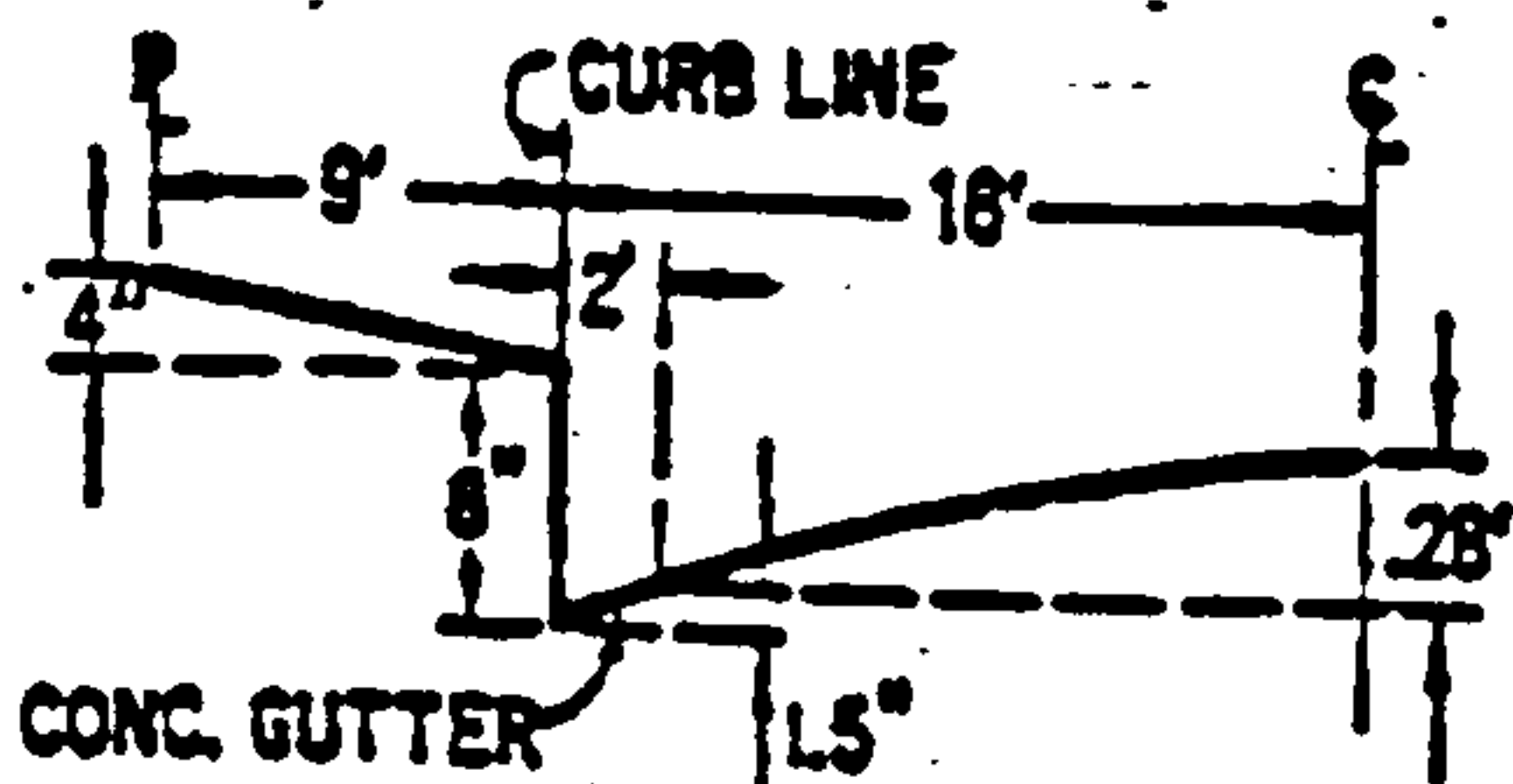
Input Data					
Channel Slope	0.008580 ft/ft				
Elevation range: 98.77 ft to 100.00 ft.					
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness	
0.00	100.00	0.00	52.63	0.017	
28.00	99.44				
28.63	98.77				
52.63	99.25				
Discharge	4.98	cfs			

Results		
Wtd. Mannings Coefficient	0.017	
Water Surface Elevation	99.06	ft
Flow Area	2.22	ft ²
Wetted Perimeter	15.16	ft
Top Width	15.03	ft
Height	0.29	ft
Critical Depth	99.07	ft
Critical Slope	0.008030	ft/ft
Velocity	2.25	ft/s
Velocity Head	0.08	ft
Specific Energy	99.14	ft
Froude Number	1.03	
Flow is supercritical.		

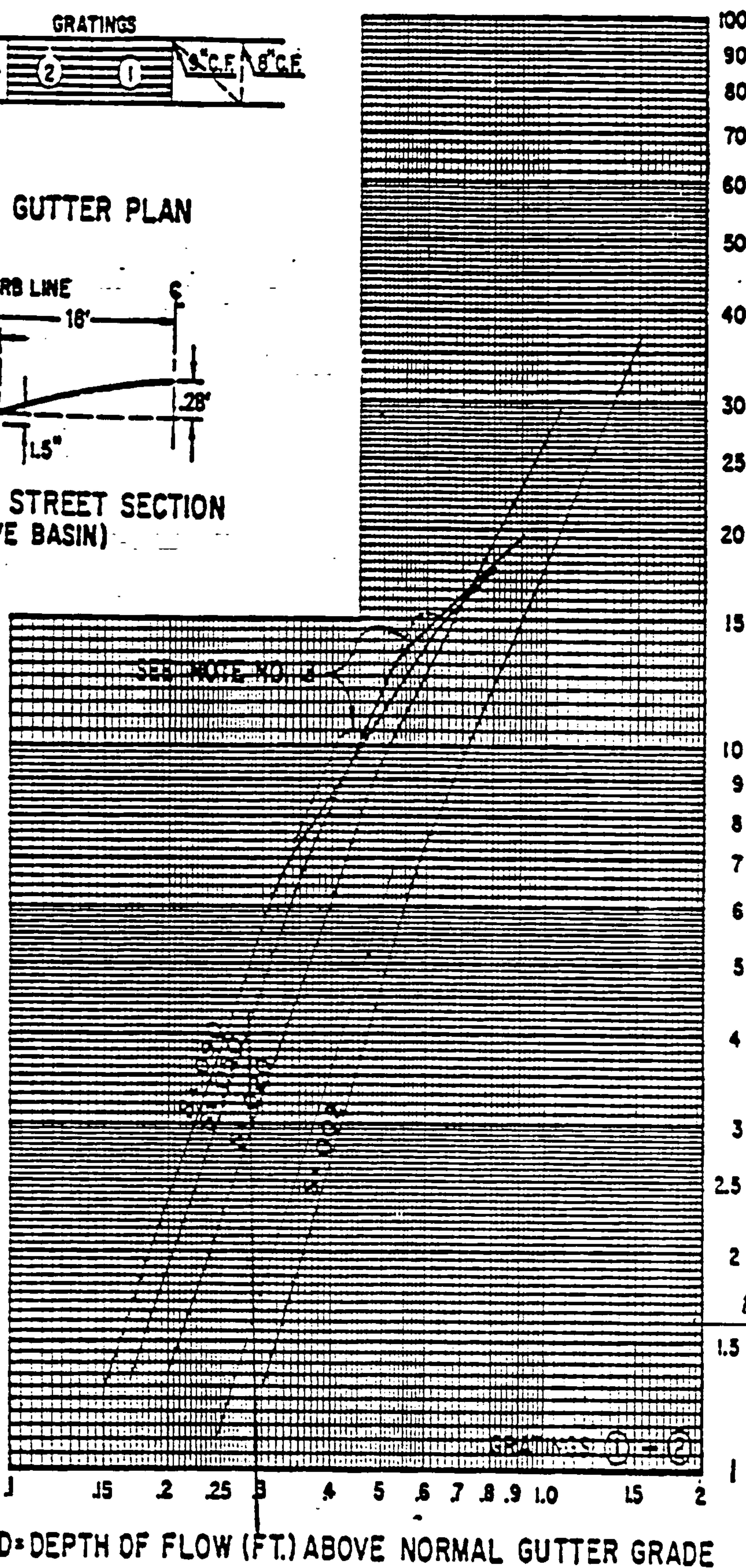
GRATING CAPACITIES FOR TYPE DOUBLE 'C,' AND 'D'



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)



$d = 0.29'$

$S = 0.858\%$

$Q_i = 1.6 \text{ cfs}$

$Q_{100} = 4.98 \text{ cfs}$

Use 3 - Double 'C' Inlets

$Q_i = 1.6 \text{ cfs}$

D = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

PLATE 22.3 D-6

BASIN 3 EAST

BASIN 4 CORONA AVE.

 $\frac{1}{2}$ STREET CALCULATIONS CONCENTRATION POINT @

EXISTING INLET

$$A = 1500 \times 30 = 1.033 \text{ ac}$$

$$A_D = 1500 \times 24 = 0.83 \text{ ac}$$

$$A_C = 1500 \times 6 = 0.21 \text{ ac}$$

$$(D) Q_{100} = 0.83 \times 5.02 = 4.2 \text{ cfs}$$

$$(C) Q_{100} = 0.21 \times 3.45 = \underline{0.72 \text{ cfs}}$$

$$Q_{100 \text{ TOTAL}} = 4.92 \text{ cfs}$$

$$d = 0.24' \text{ (SEE SPREAD SHEET ATTACHED)}$$

EXISTING DOUBLE 'C' INLET CAPACITY = 4.7 cfs (PER DPM PL) (22.3 D-6)

$$S = 3.5\%$$

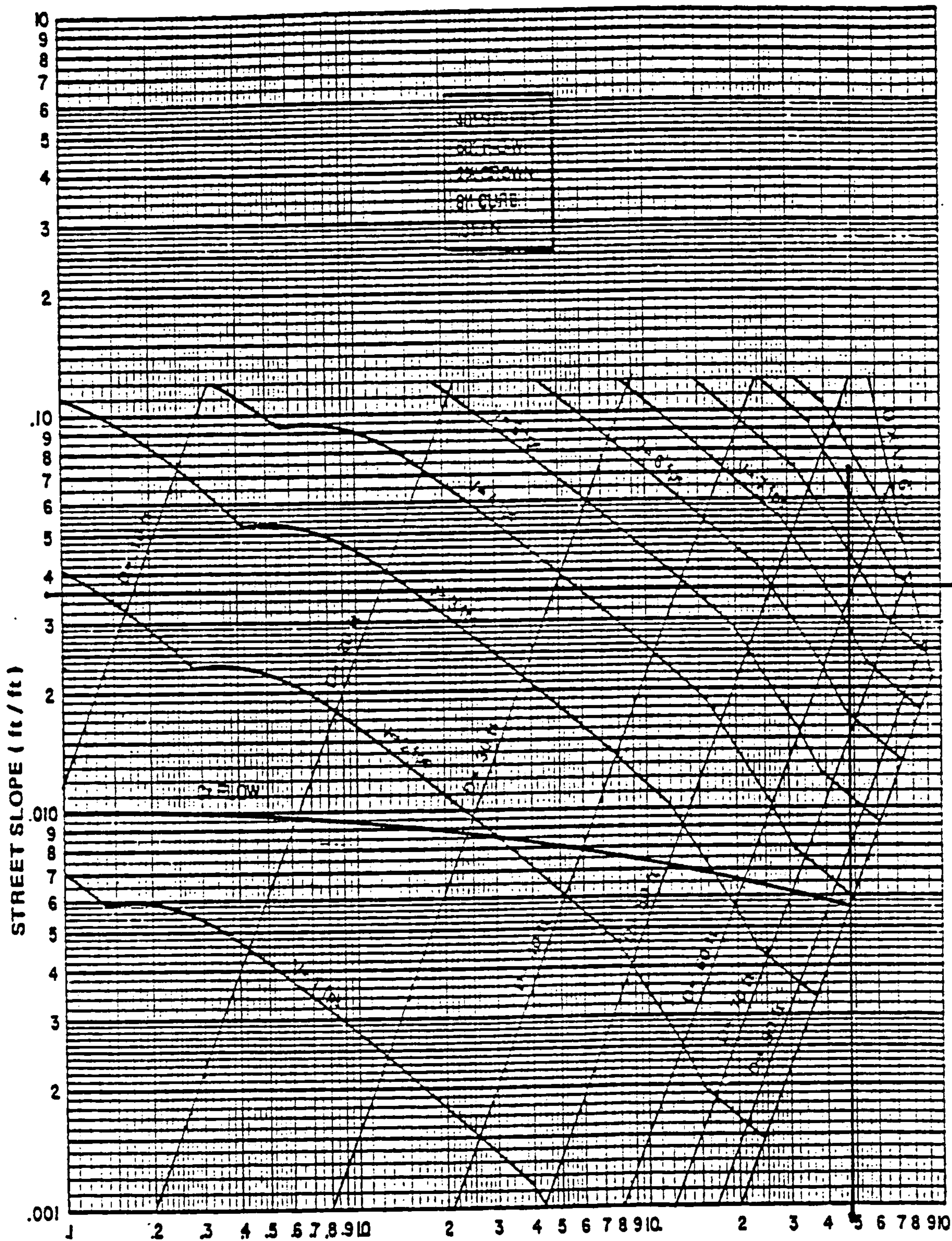
CORONA AVE. CAPACITY & DEPTH AT Q100
Worksheet for Irregular Channel

Project Description	
Project File	a:\fire sta.fm2
Worksheet	CORONA AVE. CAPACITY
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data				
Channel Slope	0.025547 ft/ft			
Elevation range: 99.13 ft to 100.00 ft.				
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness
0.00	100.00	0.00	30.00	0.017
10.00	99.80			
10.10	99.13			
30.00	99.53			
Discharge	4.92	cfs		

Results	
Wtd. Mannings Coefficient	0.017
Water Surface Elevation	99.37 ft
Flow Area	1.46 ft ²
Wetted Perimeter	12.27 ft
Top Width	12.06 ft
Height	0.24 ft
Critical Depth	99.43 ft
Critical Slope	0.008113 ft/ft
Velocity	3.38 ft/s
Velocity Head	0.18 ft
Specific Energy	99.55 ft
Froude Number	1.71
Flow is supercritical.	

STREET CAPACITY

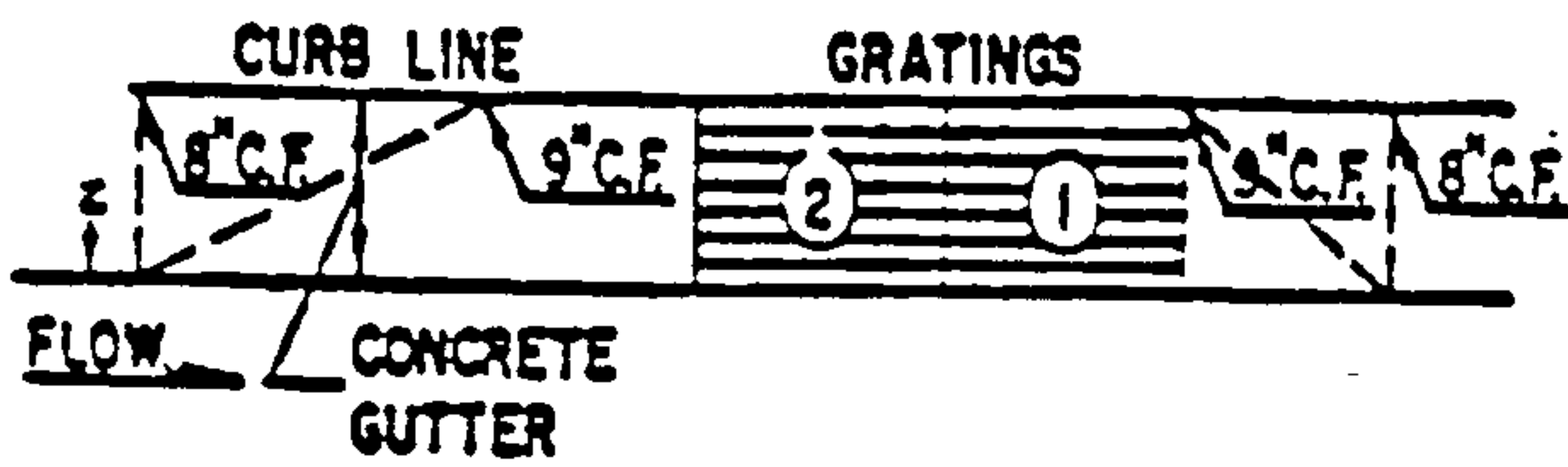


3.690

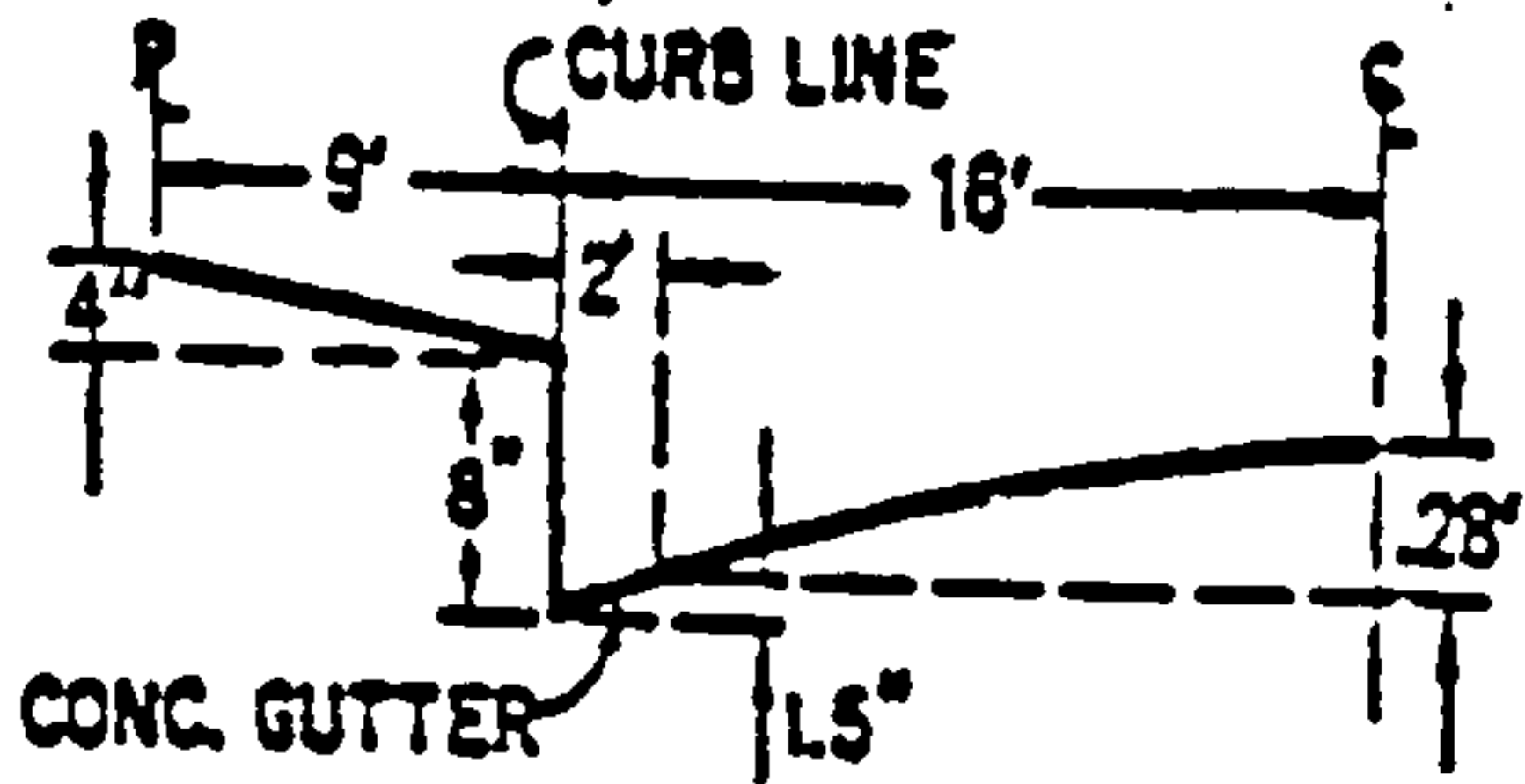
ONE HALF STREET FLOWS (cfs)

$Q_{100} = 4.9 \text{ cfs}$
 $d = 0.54' < 0.87 \text{ of}$

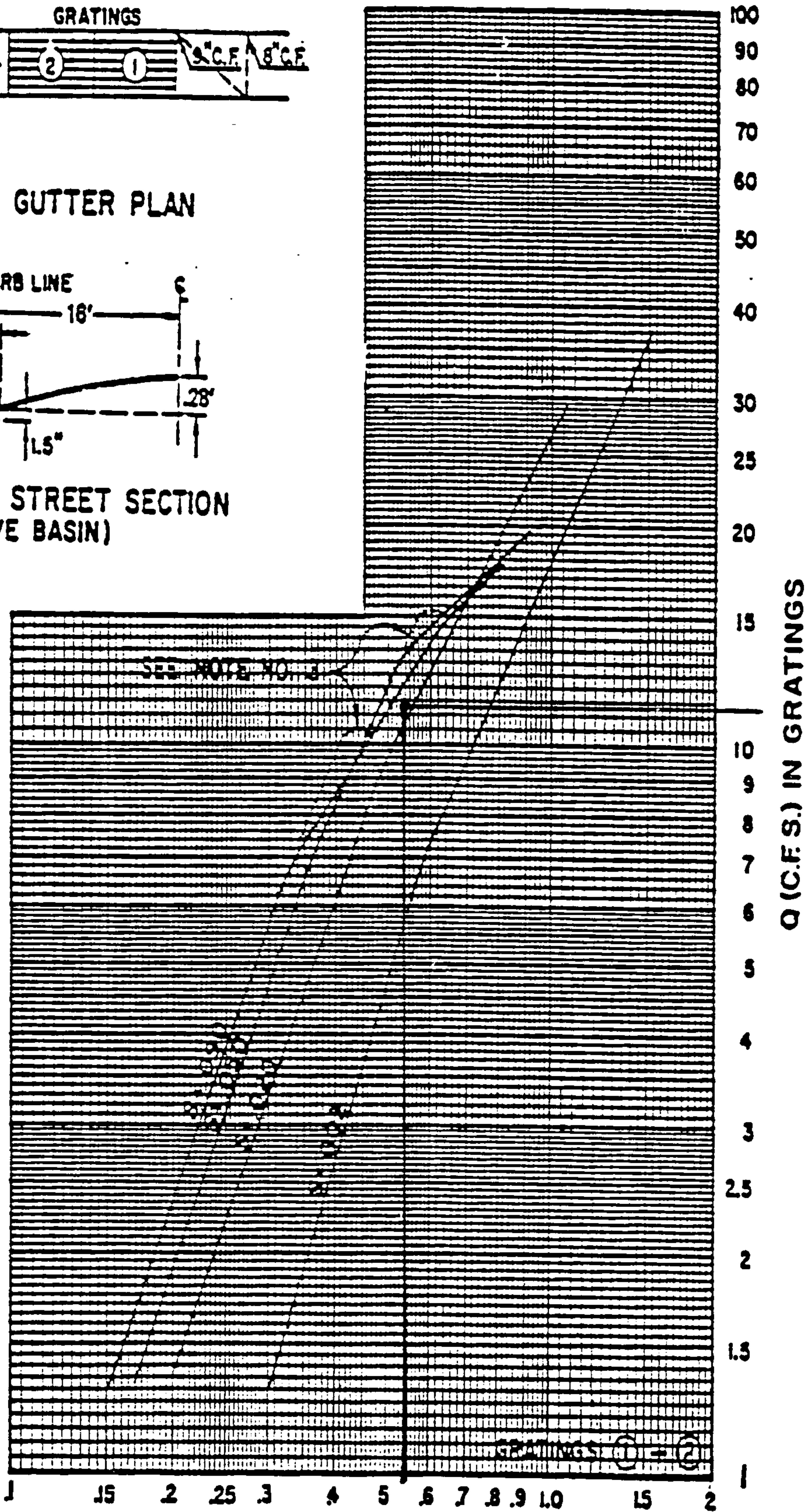
GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)



D = DEPTH OF FLOW (FT.) ABOVE NORMAL GUTTER GRADE

PLATE 22.3 D-6

$S = 3.6\%$

$d = 0.94'$

$Q_i = 11 \text{ cfs}$ $Q_{100} = 4.9 \text{ cfs}$ OK

CORONA AVENUE

EXISTING CAPACITY - WITHOUT FS-20

$$S = 3.6\%$$

$$D = 1473'$$

WYOMING TO EXISTING INLET - SOUTH SIDE
OF CORONA @ MURRELET DRIVE (FALCON
RIDGE SUBDIVISION)

$$W(\text{NORTH}) - \text{STREET} - 20' \quad D = \frac{20}{30} = .87$$

$$\text{SIDEWALK} - 6' \quad C = .13$$

$$\text{DIRT} - 4'$$

$$W(\text{SOUTH}) - \text{STREET} - 4' \quad D = 1.0$$

SIDEWALK - NONE

DIRT - NONE - LAND SLOPES SOUTH AWAY FROM
STREET

$$Q_{100}(\text{NORTH}) = 5.02 * 1.019 * .87 + 3.45 * 1.019 * .13 = 4.9$$

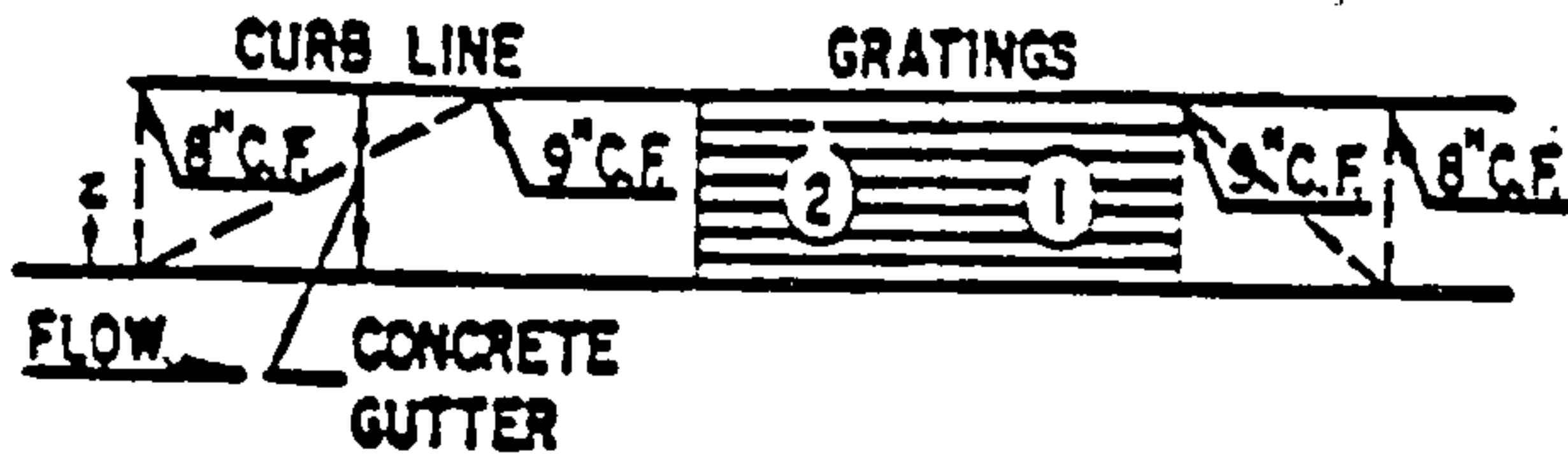
$$A = 1473 * 30 = 44,190 (1.01920)$$

$$Q_{100}(\text{SOUTH}) = 5.02 * 0.135 * 1 = 0.68 \text{ cfs}$$

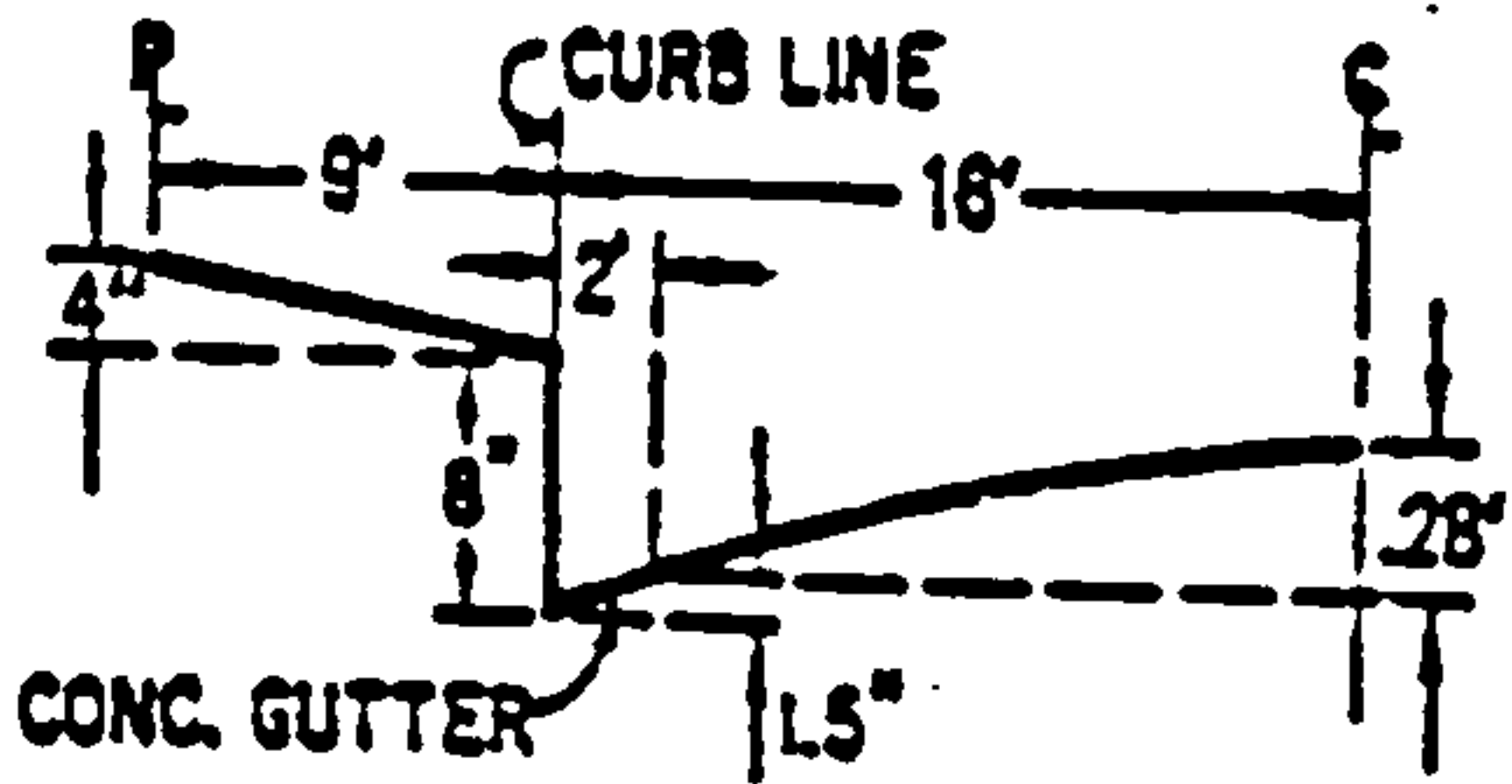
$$A = 1473 * 4 = 5892 (0.13520)$$

NOTE: $Q_{100}(\text{SOUTH}) = Q_{100}(\text{NORTH}) = 4.9 \text{ cfs}$ for
FULLY CONSTRUCTED SECTION.

GRATING CAPACITIES FOR TYPE DOUBLE "C," AND "D"



GRATING & GUTTER PLAN



TYPICAL HALF STREET SECTION (ABOVE BASIN)

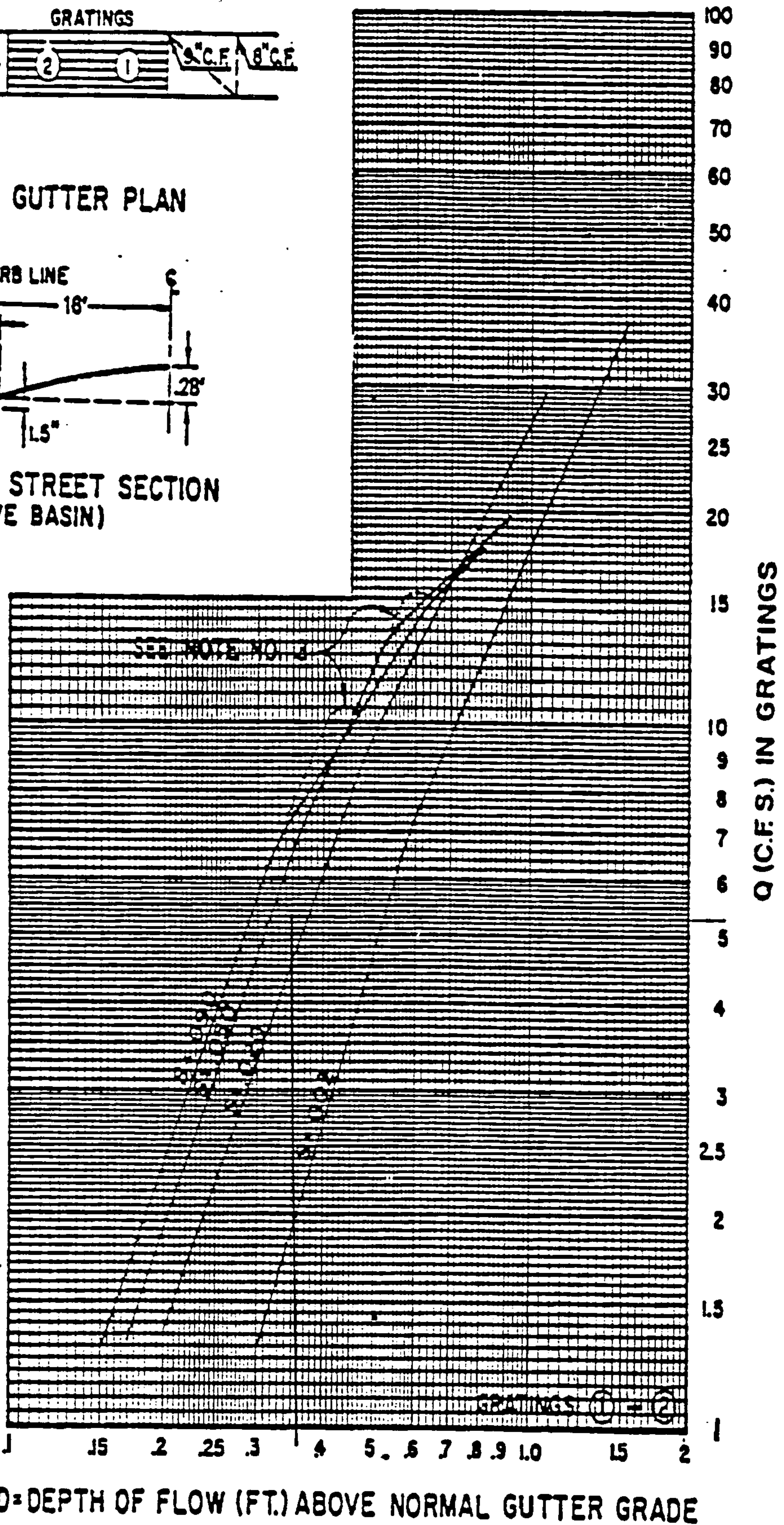
$D = 99.45 - 99.13$
 $\approx 0.28'$

$S = 3.6\%$

$Q_i = 5.3 \text{ cfs}$

$Q_{BY} = 8.26 - 5.3$
 $= 2.96 \text{ cfs}$

No Good



CORONA TEMP SECTION W/4' TEMP PVMT
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	CORONA - EXISTING SECTION W/4' TEMP PVMT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data	
Channel Slope	0.036000 ft/ft
Elevation range: 99.13 ft to 100.12 ft.	
Station (ft)	Elevation (ft)
66.00	100.12
66.01	99.45
70.00	99.53
90.00	99.13
90.01	99.80
100.00	100.00
Discharge	8.57 cfs

FLOW IN SOUTH CURB = 0.3 cfs
 FLOW IN NORTH CURB =
 $8.57 - 0.35 = 8.26 \text{ cfs}$

Results	
Wtd. Mannings Coefficient	0.017
Water Surface Elevation	99.41 ft
Flow Area	1.95 ft ²
Wetted Perimeter	14.23 ft
Top Width	13.95 ft
Height	0.28 ft
Critical Depth	99.51 ft
Critical Slope	0.007834 ft/ft
Velocity	4.40 ft/s
Velocity Head	0.30 ft
Specific Energy	99.71 ft
Froude Number	2.08
Flow is supercritical.	

CORONA FULL SECTION W/BASIN B
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	CORONA AVE FULL SECTION
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data	
Channel Slope	0.036000 ft/ft
Elevation range: 99.13 ft to 100.00 ft.	
Station (ft)	Elevation (ft)
40.00	100.00
50.00	99.80
50.01	99.13
70.00	99.53
90.00	99.13
90.01	99.80
100.00	100.00
Discharge	12.79 cfs

$$Q_{100} = 4.9 + 4.9 + 2.99 \text{ (BASIN B)}$$

$$= 12.79 \text{ cfs}$$

$$\text{MAX DEPTH} = 99.38 - 99.13 = 0.25'$$

$$< .87 \text{ OK}$$

Results	
Wtd. Mannings Coefficient	0.017
Water Surface Elevation	99.38 ft
Flow Area	3.13 ft ²
Wetted Perimeter	25.50 ft
Top Width	25.00 ft
Height	0.25 ft
Critical Depth	99.46 ft
Critical Slope	0.007863 ft/ft
Velocity	4.09 ft/s
Velocity Head	0.26 ft
Specific Energy	99.64 ft
Froude Number	2.04
Flow is supercritical.	
Flow is divided.	

← CROWN DEPTH FLOW NOT EVENLY SPLIT.

EXIST CORONA SOUTH - TEMP SECTION
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	CORONA SOUTH - EXIST
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data				
Channel Slope	0.036000 ft/ft			
Water Surface Elevation	99.41 ft			
Elevation range: 99.33 ft to 100.00 ft.				
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness
4.00	100.00	4.00	8.01	0.017
4.01	99.33			
8.01	99.41			

Results	
Wtd. Mannings Coefficient	0.017
Discharge	0.31 cfs
Flow Area	0.16 ft ²
Wetted Perimeter	4.08 ft
Top Width	4.00 ft
Height	0.08 ft
Critical Depth	99.43 ft
Critical Slope	0.011376 ft/ft
Velocity	1.91 ft/s
Velocity Head	0.06 ft
Specific Energy	99.47 ft
Froude Number	1.69
Flow is supercritical.	

$Q_{100} = 0.68 \text{ cfs}$
 $.68 - .31 = 0.37$ spills to north
 w/o FS-20
 (BASIN B)
 $Q_{100} = 0.68 + 2.99 = 3.67 \text{ cfs}$
 with FS-20 BASIN B
 $3.67 - .31 = 3.36 \text{ cfs}$ spills
 to NORTH.

100-YR FLOW DEPTH - CORONA NORTH
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	HALF CORONA AVE SECTION
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data				
Channel Slope	0.035000 ft/ft			
Elevation range: 99.13 ft to 100.00 ft.				
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness
70.00	100.00	70.00	100.00	0.017
80.00	99.80			
80.01	99.13			
100.00	99.53			
Discharge	4.90	cfs		

Results	
Wtd. Mannings Coefficient	0.017
Water Surface Elevation	99.36 ft
Flow Area	1.29 ft ²
Wetted Perimeter	11.60 ft
Top Width	11.37 ft
Height	0.23 ft
Critical Depth	99.43 ft
Critical Slope	0.008147 ft/ft
Velocity	3.79 ft/s
Velocity Head	0.22 ft
Specific Energy	99.58 ft
Froude Number	1.98
Flow is supercritical.	

*SINCE CROWN ELEV 99.53
THERE IS NO SPILL TO SOUTH*

EXIST CORONA SOUTH - TEMP SECTION
Worksheet for Irregular Channel

Project Description	
Project File	c:\haestad\fmw\fs20-cor.fm2
Worksheet	CORONA SOUTH - EXIST
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Input Data				
Channel Slope	0.036000 ft/ft			
Elevation range: 99.33 ft to 100.00 ft.				
Station (ft)	Elevation (ft)	Start Station	End Station	Roughness
4.00	100.00	4.00	8.01	0.017
4.01	99.33			
8.01	99.41			
Discharge	0.68	cfs		

Results	
Wtd. Mannings Coefficient	0.017
Water Surface Elevation	99.43 ft
Flow Area	0.26 ft ²
Wetted Perimeter	4.13 ft
Top Width	4.00 ft
Height	0.10 ft
Critical Depth	99.47 ft
Critical Slope	0.009772 ft/ft
Velocity	2.62 ft/s
Velocity Head	0.11 ft
Specific Energy	99.54 ft
Froude Number	1.81
Flow is supercritical.	
Water elevation exceeds lowest end station by 0.02 ft.	

*SPILL TO NORTH
CROWN @ 99.41*



Federal Emergency Management Agency

Washington, D.C. 20472

L. Blair

MAYOR'S OFFICE
98 MAY -4 AM 8:52

CERTIFIED MAIL
RETURN RECEIPT REQUESTED

IN REPLY REFER TO:
Case No.: 98-06-990P

The Honorable Martin J. Chavez
Mayor, City of Albuquerque
P.O. Box 1293
Albuquerque, New Mexico 87103-1293

Community: City of Albuquerque,
New Mexico
Community No.: 350002
Panel Affected: 35001C0141 D
Effective Date of **APR 24 1998**
This Revision:

102-D-A

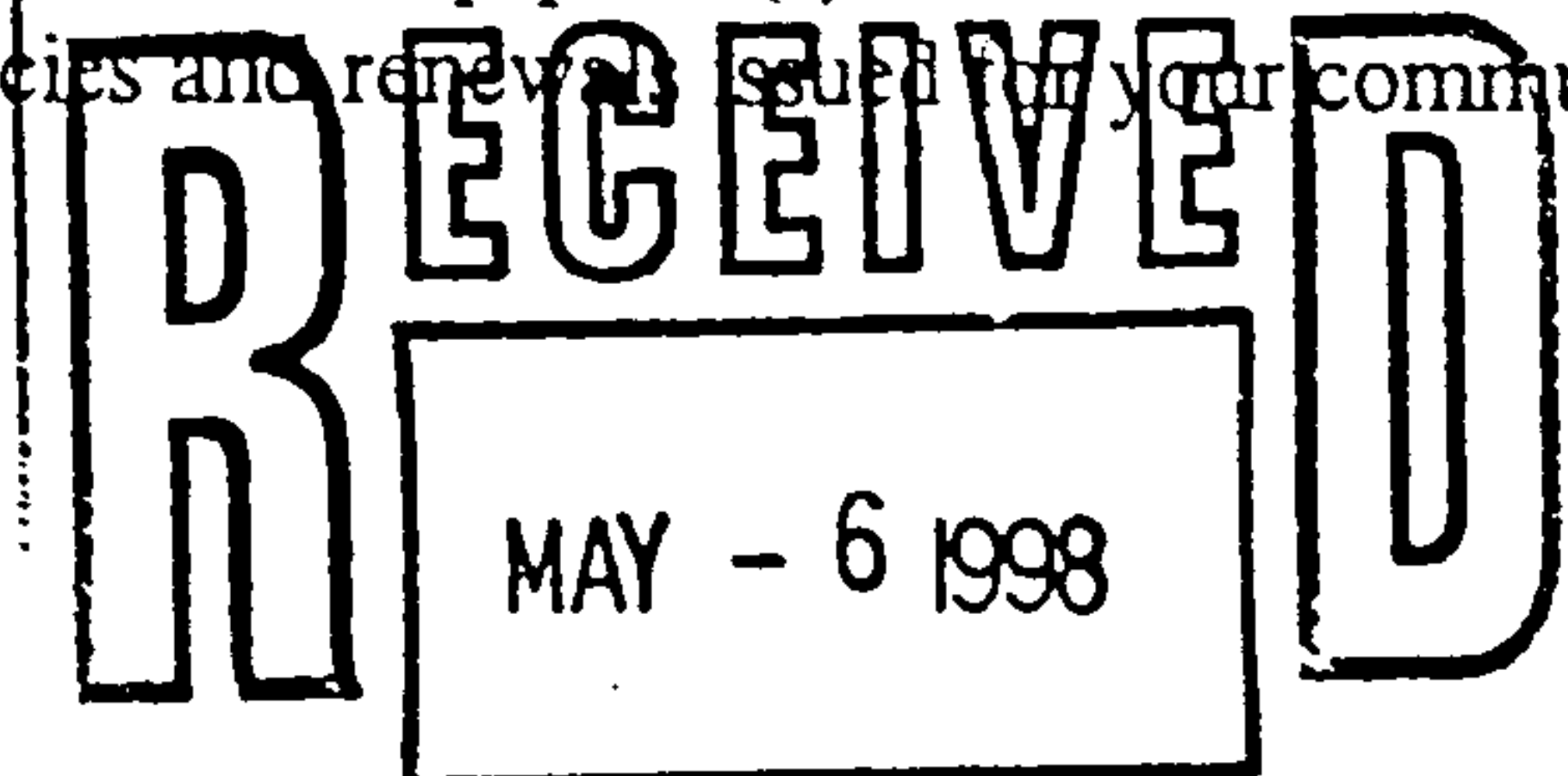
Dear Mayor Chavez:

This responds to a request that the Federal Emergency Management Agency (FEMA) revise the effective Flood Insurance Rate Map (FIRM) for Bernalillo County, New Mexico and Incorporated Areas (the effective FIRM for your community), in accordance with Part 65 of the National Flood Insurance Program (NFIP) regulations. In a letter dated March 11, 1998, Ms. Susan M. Calongne, P.E., City/County Floodplain Administrator, City of Albuquerque/Bernalillo County, requested that FEMA revise the FIRM to show the effects of channelization along the North Arroyo de Domingo Baca from just downstream of Wyoming Boulevard to just downstream of Barstow Street. The channel is soil cement-lined, with a 24-foot bottom width and 1:1 side slopes. Although the effective FIRM shows portions of the channel within the unincorporated areas of Bernalillo County, these areas were annexed by the City of Albuquerque on June 7, 1996. This request follows up on a Conditional Letter of Map Revision issued on March 6, 1997.

All data required to complete our review of this request were submitted with letters from Ms. Calongne.

We have completed our review of the submitted data and the flood data shown on the effective FIRM. We have revised the FIRM to modify the elevations and floodplain boundary delineations of the flood having a 1-percent chance of being equaled or exceeded in any given year (base flood) along North Arroyo de Domingo Baca from just downstream of Wyoming Boulevard to just downstream of Barstow Street. As a result of the modifications, the base flood is contained in the channel and the width of the Special Flood Hazard Area (SFHA), the area that would be inundated by the base flood, decreased. The modifications are shown on the enclosed annotated copy of FIRM Panel(s) 35001C0141 D. This Letter of Map Revision (LOMR) hereby revises the above-referenced panel(s) of the effective FIRM dated September 20, 1996.

The modifications are effective as of the date shown above. The map panel(s) as listed above and as modified by this letter will be used for all flood insurance policies and renewals issued for your community.



PUBLIC WORKS DEPT.
ADMINISTRATION

The following table is a partial listing of existing and modified BFEs:

Location	Existing BFE (feet)*	Modified BFE (feet)*
Approximately 1,000 feet upstream of Wyoming Boulevard	1	None
Approximately 1,000 feet downstream of Barstow Street	1	None

*Depth in feet above ground rounded to the nearest whole foot

Public notification of the modified BFEs will be given in the *Albuquerque Journal* on or about May 21 and May 28, 1998. A copy of this notification is enclosed. In addition, a notice of changes will be published in the *Federal Register*. Within 90 days of the second publication in the *Albuquerque Journal*, a citizen may request that FEMA reconsider the determination made by this LOMR. Any request for reconsideration must be based on scientific or technical data. All interested parties are on notice that, until the 90-day period elapses, the determination to modify the BFEs presented in this LOMR may itself be modified.

Because this LOMR will not be printed and distributed to primary users, such as local insurance agents and mortgage lenders, your community will serve as a repository for these new data. We encourage you to disseminate the information reflected by this LOMR throughout the community, so that interested persons, such as property owners, local insurance agents, and mortgage lenders, may benefit from the information. We also encourage you to prepare a related article for publication in your community's local newspaper. This article should describe the assistance that officials of your community will give to interested persons by providing these data and interpreting the NFIP maps.

We will not physically revise and republish the FIRM and Flood Insurance Study (FIS) report for your community to reflect the modifications made by this LOMR at this time. When changes to the previously cited FIRM panel(s) and FIS report warrant physical revision and republication in the future, we will incorporate the modifications made by this LOMR at that time.

This LOMR is based on minimum floodplain management criteria established under the NFIP. Your community is responsible for approving all floodplain development, and for ensuring all necessary permits required by Federal or State law have been received. State, county, and community officials, based on knowledge of local conditions and in the interest of safety, may set higher standards for construction in the SFHA. If the State, county, or community has adopted more restrictive or comprehensive floodplain management criteria, these criteria take precedence over the minimum NFIP criteria.

The basis of this LOMR is, in whole or in part, a channel-modification project. NFIP regulations, as cited in Paragraph 60.3(b)(7), require that communities ensure that the flood-carrying capacity within the altered or relocated portion of any watercourse is maintained. This provision is incorporated into your community's existing floodplain management regulations. Consequently, the ultimate responsibility for maintenance of the modified channel rests with your community.

This determination has been made pursuant to Section 206 of the Flood Disaster Protection Act of 1973 (Public Law 93-234) and is in accordance with the National Flood Insurance Act of 1968, as amended (Title XIII of the Housing and Urban Development Act of 1968, Public Law 90-448), 42 U.S.C. 4001-4128, and 44 CFR Part 65. Pursuant to Section 1361 of the National Flood Insurance Act of 1968, as amended, communities participating in the NFIP are required to adopt and enforce floodplain management regulations that meet or exceed NFIP criteria. These criteria are the minimum requirements and do not supersede any State or local requirements of a more stringent nature. This includes adoption of the effective FIRM to which the regulations apply and the modifications described in this LOMR.

If you have any questions regarding floodplain management regulations for your community or the NFIP in general, please contact the Consultation Coordination Officer (CCO) for your community. Information on the CCO for your community may be obtained by contacting the Director, Mitigation Division of FEMA in Denton, Texas, at (940) 898-5127. If you have any technical questions regarding this LOMR, please contact Mr. Alan Johnson of our staff in Washington, DC, either by telephone at (202) 646-3403 or by facsimile at (202) 646-4596.

Sincerely,



Matthew B. Miller, P.E., Chief
Hazards Study Branch
Mitigation Directorate

Enclosure(s)

cc: Ms. Susan M. Calongne, P.E.
City/County Floodplain Administrator
City of Albuquerque/Bernalillo County

Mr. John Kelly, P.E.
Acting Executive Engineer
Albuquerque Metropolitan Arroyo
Flood Control Authority

Mr. Jeffrey G. Mortensen, P.E.
President
Jeff Mortensen & Associates, Inc.