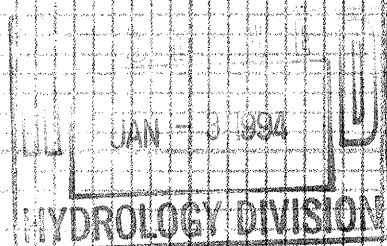




D. MARK GOODWIN & ASSOCIATES, P.A.
CONSULTING ENGINEERS & SURVEYORS

PROJECT _____
SUBJECT _____
BY _____ DATE _____
CHECKED _____ DATE _____
SHEET _____ OF _____

*Design Analysis for Channelization
of the North Branch - South Domingo
Baca Arroyo*



Revised December 1993



D. Mark Goodwin & Associates, P.A.
Consulting Engineers and Surveyors

PROJECT N. Br. S. Domingo Baca
SUBJECT Arroyo Channelization
BY JMM DATE 11/10/93
CHECKED _____ DATE _____

SHEET 2 OF _____

SCOUR ANALYSIS - MAIN CHANNEL

(pt. B-sht. 3)
Elev. @ Base of
Subsurface
Channel
Penetration

(pt. A - Sht. 3)

Sec.
No.
(supercrit.)
Channel
Bottom

Hyd. Depth

F_r

q_s

VCH

$\frac{1}{2} h_a$

Total
Scour

2	83.65	1.58	1.19	6.71	9.58	1.25	7.96	75.69
3	81.84	1.30	1.90	6.41	12.61	2.17	8.58	73.26
4	78.90	1.29	1.88	6.33	12.68	2.20	8.53	70.37
5	75.81	1.08	2.24	5.66	13.21	2.38	8.02	67.79
6	73.04	1.13	1.70	5.40	9.71	1.29	6.69	66.35
7	70.20	0.99	1.68	4.69	10.79	1.59	6.28	63.92
8	67.48	0.82	1.88	4.06	11.12	1.69	5.75	61.73
9	64.30	1.18	1.55	5.45	9.85	1.32	6.78	57.52
10	61.25	1.27	1.70	6.04	10.93	1.63	7.67	53.58
11	58.21	1.50	1.68	7.13	11.76	1.89	9.02	49.19
4*	53.71	2.42	0.74	8.76	6.63	0.60	9.36	44.35
3*	48.97	4.09	0.12	8.12	1.87	0.48	8.17	40.79

$$y_s = h_L (4)(F_r)^{0.33}$$
$$\frac{1}{2} h_a = 0.07 \frac{2\pi V^2}{g}$$

Local Scour Anti-Dune Scour

* Subcritical Flow Sections



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PROJECT N. Br. S. Domingo Baca
SUBJECT Arroyo Channelization
BY JMM DATE 11/10/93
CHECKED _____ DATE _____
SHEET 3 OF _____

MINIMUM CHANNEL EMBANKMENT ELEVATIONS

MAIN CHANNEL

HEC-2 Sec. No	EGL (HEC-2) (ft.)	Depth (ft.)	Vel (fps)	FB (ft.)	b (ft.)	z	r (ft.)	SE (ft.)	Minimum Embankment Elevation
1 *	58.17	12.47	6.28	1.65					58.82
2 *	58.22	11.38	1.75	1.47					59.69
3 *	58.23	9.23	1.87	1.47					59.70
4 *	58.48	4.88	6.63	1.60					60.08
11	63.07	2.52	11.76	1.68	12	2.2	358	0.36	65.11
10	65.47	2.23	10.93	1.65	12	2.2	358	0.29	67.41
9	67.76	2.11	9.85	1.62	12	2.2	358	0.23	69.61
8	70.27	1.51	11.12	1.63	12	2.2	358	0.26	72.16
7	73.10	1.59	10.79	1.62					74.72
6	75.17	2.06	9.71	1.62					76.79
5	78.97	1.58	13.21	1.67					80.64
4	82.53	1.63	12.68	1.66					84.19
3	85.32	2.20	12.61	1.69	12	1.9	287	0.45	87.45
2	86.87	2.39	9.58	1.62	12	7.0	382	0.32	88.81

Freeboard

$$FB = 0.7(2 + 0.025v^{1/3})$$

Super-elevation

$$SE = \frac{1.3v^2(b + 2zd)}{gr}$$

* Subcritical flow

z = cotangent of embankment slope

b = channel bottom width

r = radius of channel curve @ toe



MAIN CHANNEL

Easement Curves were designed into the channel on each side of the two inside curves, as shown on sheet 1. The minimum length of the easement curve at the temporary diversion is:

$$L_E = 0.32(b + 2zd) \frac{V}{\sqrt{d}} \quad - \text{at Sec. 10 of the supercritical HEC 2 analysis}$$

$$b = 12 \text{ ft} \quad z = 2.2$$

$$V = 10.93 \text{ fps} \quad d = 2.23$$

$$L_E = 53 \text{ ft}$$

For the curve just downstream of Tramway Lane, the minimum L_E is

@ sec. 3 of the supercritical analysis:

$$b = 12 \text{ ft} \quad z = 1.9 \quad d = 2.20 \text{ ft} \quad V = 12.61 \text{ fps}$$

$$L_E = 55 \text{ ft}$$



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PROJECT N. Br. S. Domingo Baca
SUBJECT Arroyo Channelization
BY JMM DATE 11/10/93
CHECKED _____ DATE _____
SHEET 5 OF _____

Freeboard and Super-elevation - Temporary Diversion

$$\text{Freeboard} = 0.7(2.0 + 0.025 V d^{.33})$$

$$\text{Super-elevation} = 1.3 V^2 [(b + 2 z d) / g r]$$

At Section No. 8 of HEC2 - Diversion Structure Run:

$$V = 7.66 \text{ fps} \quad d = 1.88 \text{ ft} \quad z = 3.5 \quad b = 13 \text{ ft} \quad r = 210 \text{ ft}$$

$$\text{FB} = 0.7(2.0 + 0.025(7.66)(1.88)^{.33})$$

$$\rightarrow \text{FB} = 1.43 \text{ ft}$$

$$\text{SE} = 1.3(7.66)^2 [(13 + 2(3.5)(1.88)) / (32.2)(210)]$$

$$\text{SE} = 0.23 \text{ ft}$$

$$\text{Energy Grade @ Sec. 8} = 6070.78$$

Design Elevation for Rip-Rap Placement @ Sec 8

$$\text{EG} + \text{FB} + \text{SE} = 70.78 + 1.43 + 0.23 = 6072.44$$



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PROJECT N.Br. S. Domingo Baca
SUBJECT Arroyo Channelization
BY JMM DATE 11/10/93
CHECKED _____ DATE _____
SHEET 6 OF _____

At Section No. 7 of HEC 2 - Diversion Structure Run:

$$V = 9.37 \text{ fps} \quad d = 1.47 \quad z = 2.74 \quad b = 13 \text{ ft} \quad r = 210 \text{ ft}$$

$$FB = 0.7(2.0 + 0.025(9.37)(1.47)^{0.33})$$

$$FB = 1.59 \text{ ft}$$

$$SE = 1.3(9.37)^2 \left[13 + 2(2.74)(1.47) / (32.2)(210) \right]$$

$$SE = 0.36 \text{ ft}$$

$$\text{Energy Grade @ Sec No. 7} = 6072.82$$

Design Elevation for Rip Rap Placement @ Sec 7

$$EG + FB + SE = 72.82 + 1.59 + 0.36 = 6074.77$$



Temporary Diversion Structure - Rip Rap Sizing

For the temporary diversion, we will evaluate side slope shear at Sec. No. 9 of the HEC-2 run (highest velocity along the diversion) and we will evaluate boundary shear at Sec No. 8 (in the middle of the curve).

At Sec No. 9, $V = 5.71$ fps $d = 2.08$ ft
(overbank)

check VL Rip Rap $D_{50} = 0.5$ ft

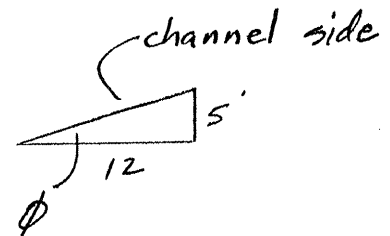
$$\tau = a (\gamma_s - \gamma) D_{50} = .04 (155 - 62.4) (0.5)$$

$$\tau = 1.85 \text{ psf}$$

$$\tau'_{(\text{allowable})} = \tau \left(1 - \frac{\sin^2 \phi}{\sin^2 \theta} \right)^{0.5}$$

$$\tau' = 1.85 \left(1 - \frac{\left(\frac{5}{13} \right)^2}{(0.64)^2} \right)^{0.5}$$

$$\tau' = 1.48 \text{ psf (allowable)}$$



$\theta = 40^\circ =$ angle of repose
for RipRap



Temporary Diversion

Actual Shear Stress on channel side slope

$$\tau_o' = \frac{8 (d)^2}{\left[32.6 \log \frac{12.2 (V)}{D_{50}} \right]^2} = \frac{62.4 (5.71)^2}{\left[32.6 \log \frac{12.2 (2.08)}{(0.5)} \right]^2}$$

$$\tau_o' = 0.67 \text{ psf}$$

→ Since $0.67 < 1.48$ side slope shear is acceptable for VL size

Boundary Shear Stress along Inside of Channel Curve

$$\tau_{\text{allowable}}' = 1.48 \text{ psf}$$

$$\text{@ Sec 8: } V = 4.73 \text{ fps } d = 1.88 \text{ ft (overbank)}$$

$$\frac{\text{Radius}}{\text{Top Width}} = \frac{202.1}{181} = 1.12$$

From Corps of Engineers
E 1110-2-1601, plate 34, (1970):

VL riprap

$$\frac{R}{W} = 1.12 \rightarrow \tau_b / \tau_o' = 2.90$$

$$\tau_o' = \frac{62.4 (4.73)^2}{\left[32.6 \log \frac{12.2 (1.88)}{0.5} \right]^2} = 0.48 \text{ psf}$$

$$\text{Boundary Shear} \rightarrow \tau_b = 2.90 (0.48) = 1.39 \text{ psf}$$

→ Boundary Shear OK since $1.39 < 1.48$ VL-OK



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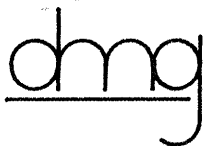
PROJECT N. Br. S. Domingo Baca
SUBJECT Arroyo Channelization
BY JMM DATE 11/10/93
CHECKED _____ DATE _____
SHEET 9 OF _____

SCOUR ANALYSIS

TEMPORARY DIVERSION STRUCTURE

Sec No. (Supercritical)	(pt. C - sht. 3)		(pt. D sht. 3)							
	Elev. @ Exposed Channel Bottom	Hyd Depth	F _r	y _s	V _{CH}	1/2 hr Scour	Total Scour	Elev. @ Base of Subsurface Channel Penetration		
7 (sta 14+77)	70.00	0.93	1.71	4.44	9.37	1.20	5.64	64.36		
8 (sta 14+14)	67.64	1.20	1.23	5.14	7.66	0.80	5.94	61.70		
9 (sta 13+39)	64.84	1.05	1.67	4.97	11.95	1.95	6.92	57.92		
Bet. 9 & 10 * (sta 12+92)	62.75	1.01	1.67	4.78	11.95	1.95	6.73	56.02		

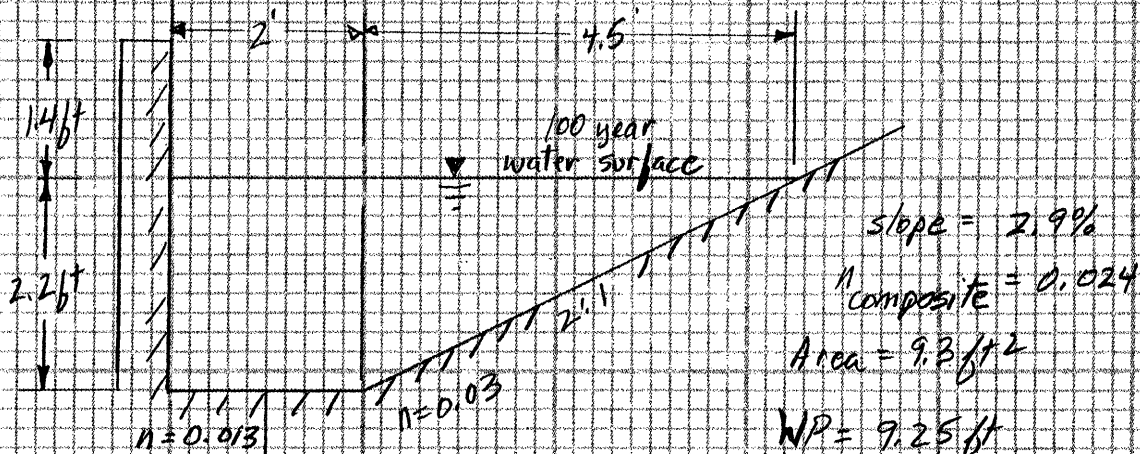
* avg. hydraulic values utilized



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PROJECT N. Br. S. Domingo Baca Arroyo
SUBJECT Tributary channel
BY JMM DATE 12/30/93
CHECKED _____ DATE _____
SHEET 10 OF _____

TRIBUTARY CHANNEL AT SECTION A (SEE SHT. 3 OF PLANS)



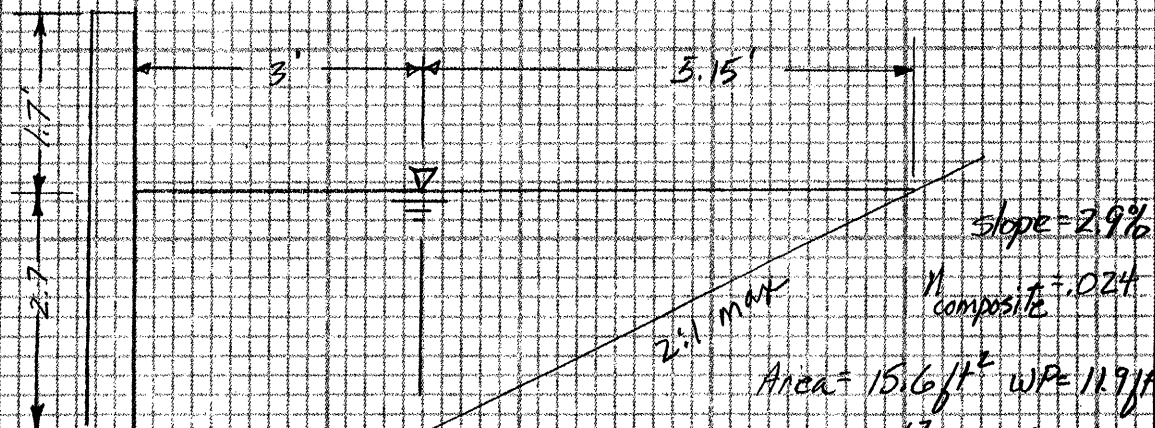
$$FB = 1 + 0.025(10.6)(2.2)^{.33}$$

$$FB = 1.34 \text{ ft}$$

$$Q = \frac{1.49}{0.024} (9.3) \left(\frac{9.3}{9.25} \right)^{.67} (.029)^{.5}$$

$$Q = 98.7 \text{ cfs} \quad V = 10.6 \text{ fps}$$

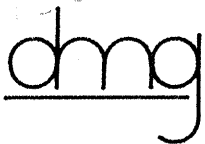
TRIBUTARY CHANNEL AT SECTION B



$$FB = 0.7 \left[2 + 0.025(12.67)(2.7)^{.33} \right] = 1.7 \text{ ft}$$

$$Q = \frac{1.49}{0.024} (15.6) \left(\frac{15.6}{11.9} \right)^{.67} (.024)^{.5}$$

$$Q = 197.7 \text{ cfs} \quad V = 12.7 \text{ fps}$$



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PROJECT N. Br. S. Domingo Baca
SUBJECT Tributary Channel
BY JMM DATE 12/30/93
CHECKED _____ DATE _____
SHEET 11 OF _____

TRIBUTARY CHANNEL AT SECTION C (SHT. 3 OF PLANS)

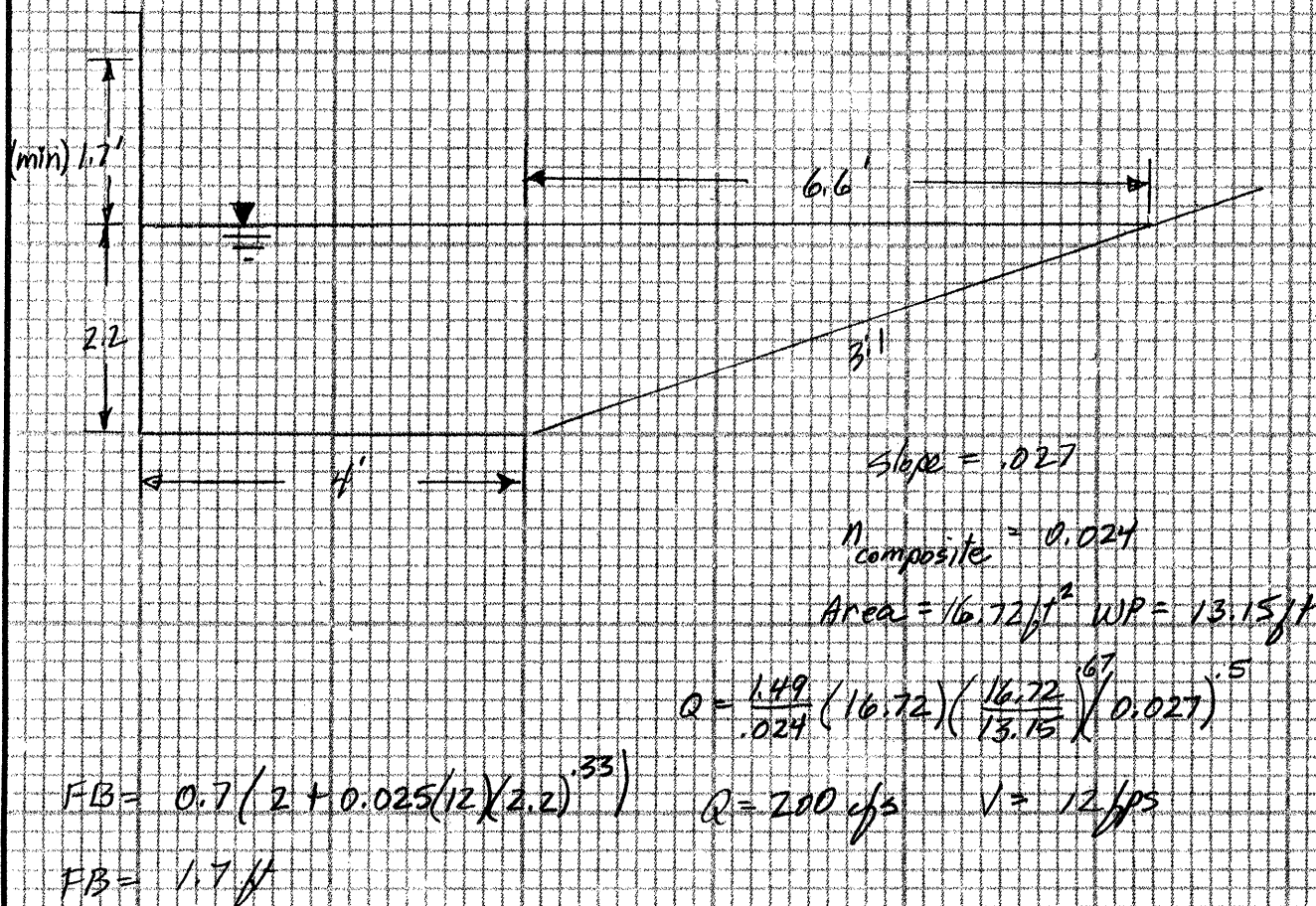


TABLE "A"			
STATION		ELEVATION "A"	ELEVATION "B"
10+52.83	6.5' RT.	6048.97	6040.79
11+25.10	6.5' RT.	6053.71	6044.35
11+96.02	6.5' RT.	6058.21	6049.19
12+64.99	6.5' RT.	6061.25	6053.58
13+36.32	6.5' RT.	6064.30	6057.52
14+07.39	6.5' RT.	6067.48	6061.73
14+76.71	6.5' RT.	6070.20	6063.92
15+48.77	6.5' RT.	6073.04	6066.35
16+14.83	6.5' RT.	6075.81	6067.79
16+89.98	6.5' RT.	6078.90	6070.37
17+61.32	6.5' RT.	6081.84	6073.26
18+31.50	6.5' RT.	6083.65	6075.69

TABLE "B"			
STATION		ELEVATION "C"	ELEVATION "D"
12+91.85	20.53' LT.	6062.75	6056.02
13+38.62	41.13' LT.	6064.84	6057.92
14+14.89	19.08' LT.	6067.64	6061.70
14+77.62	2.20' RT.	6070.00	6064.36

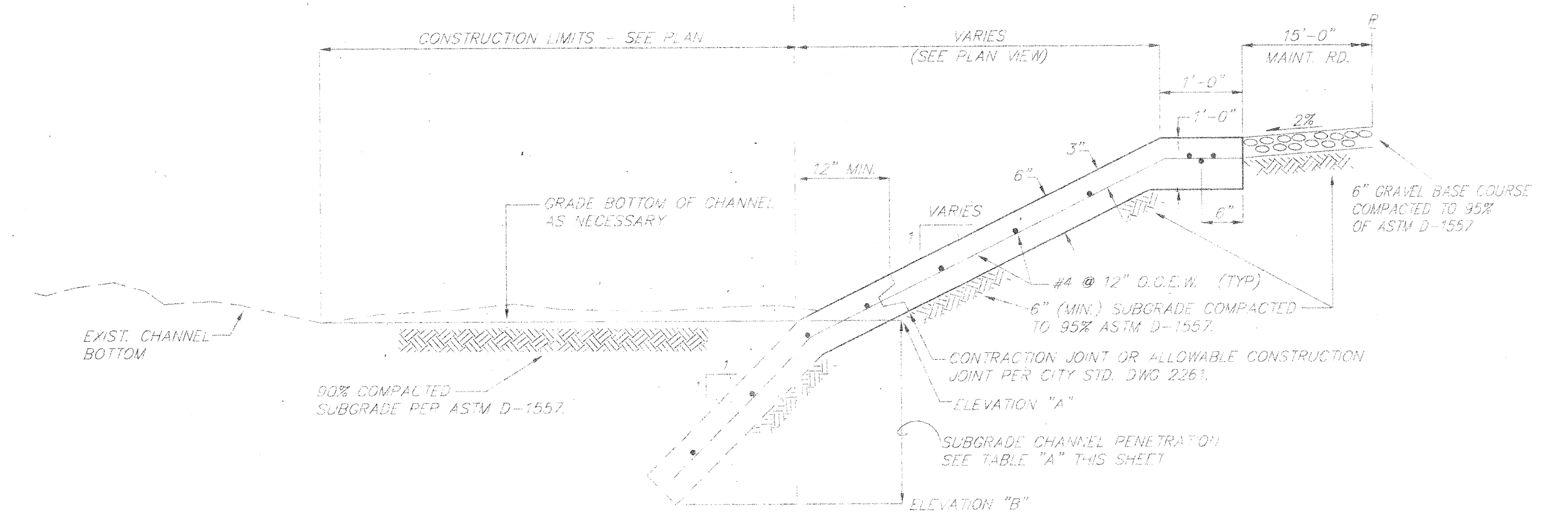
* FROM STA. 12+91.85, 20.53' LT. TAPER BELOW GRADE PENETRATION OF RIP RAP TO NO PENETRATION AT STA. 14+18.42, 27.70' RT.

TYPE II GRANULAR BEDDING GRADATION

U.S. STD. SIEVES SIZE	PERCENT PASSING BY WEIGHT SQUARE MESH SIEVES
3"	90-100
3/4"	20-90
#4	0-20
#200	0-3

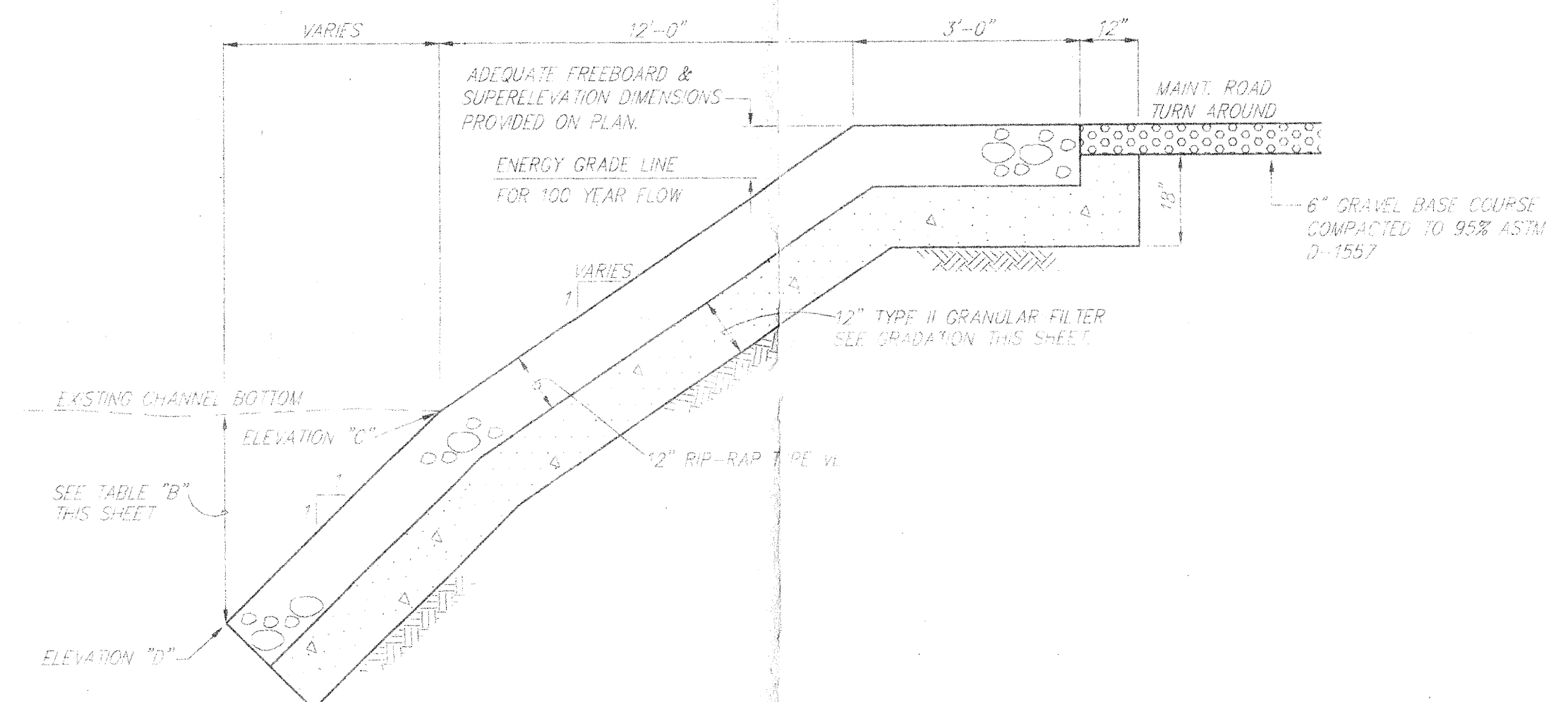
CLASSIFICATION AND GRADATION OF RIPRAP

RIPRAP DESIGNATION	% SMALLER THAN GIVEN SIZE BY WEIGHT	INTERMEDIATE ROCK DIMENSION (INCHES)	MEAN PARTICLE SIZE - D ₅₀ (INCHES)
TYPE VI	70-100	12	6
	50-70	9	
	35-50	6	
	2-10	2	



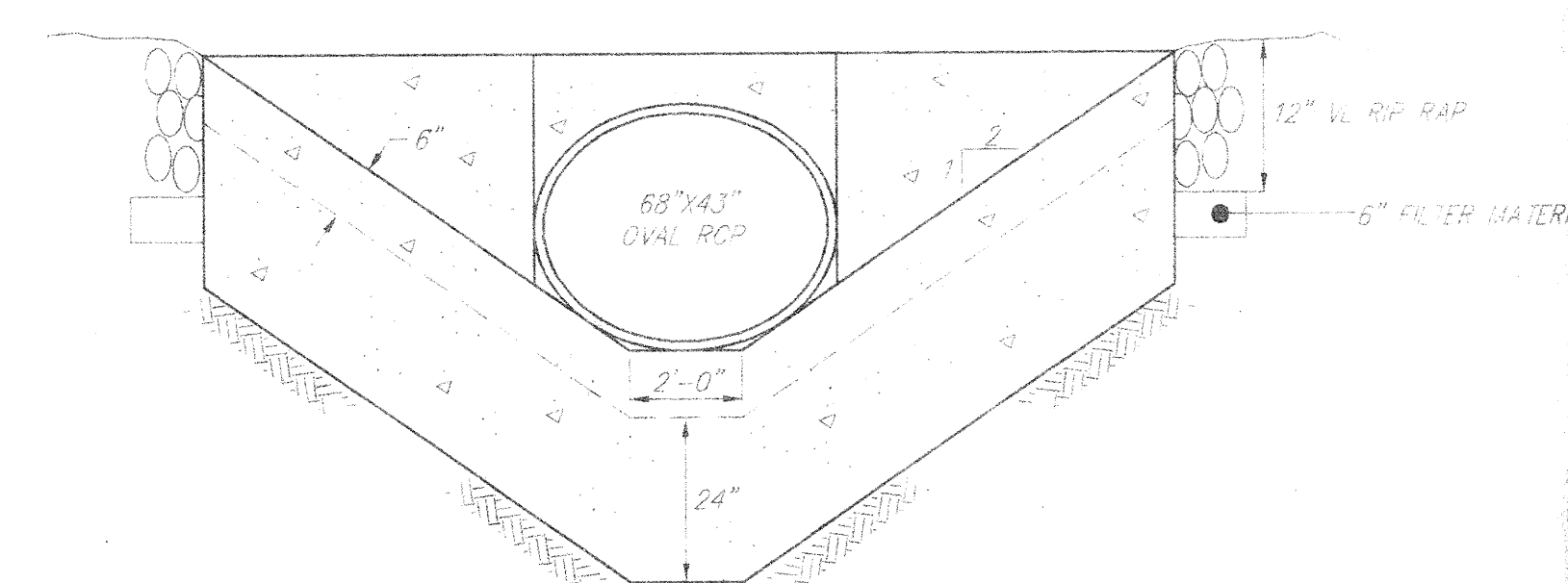
TYPICAL CHANNEL SECTION

SCALE: NONE



TEMPORARY DIVERSION STRUCTURE (THIS PHASE)

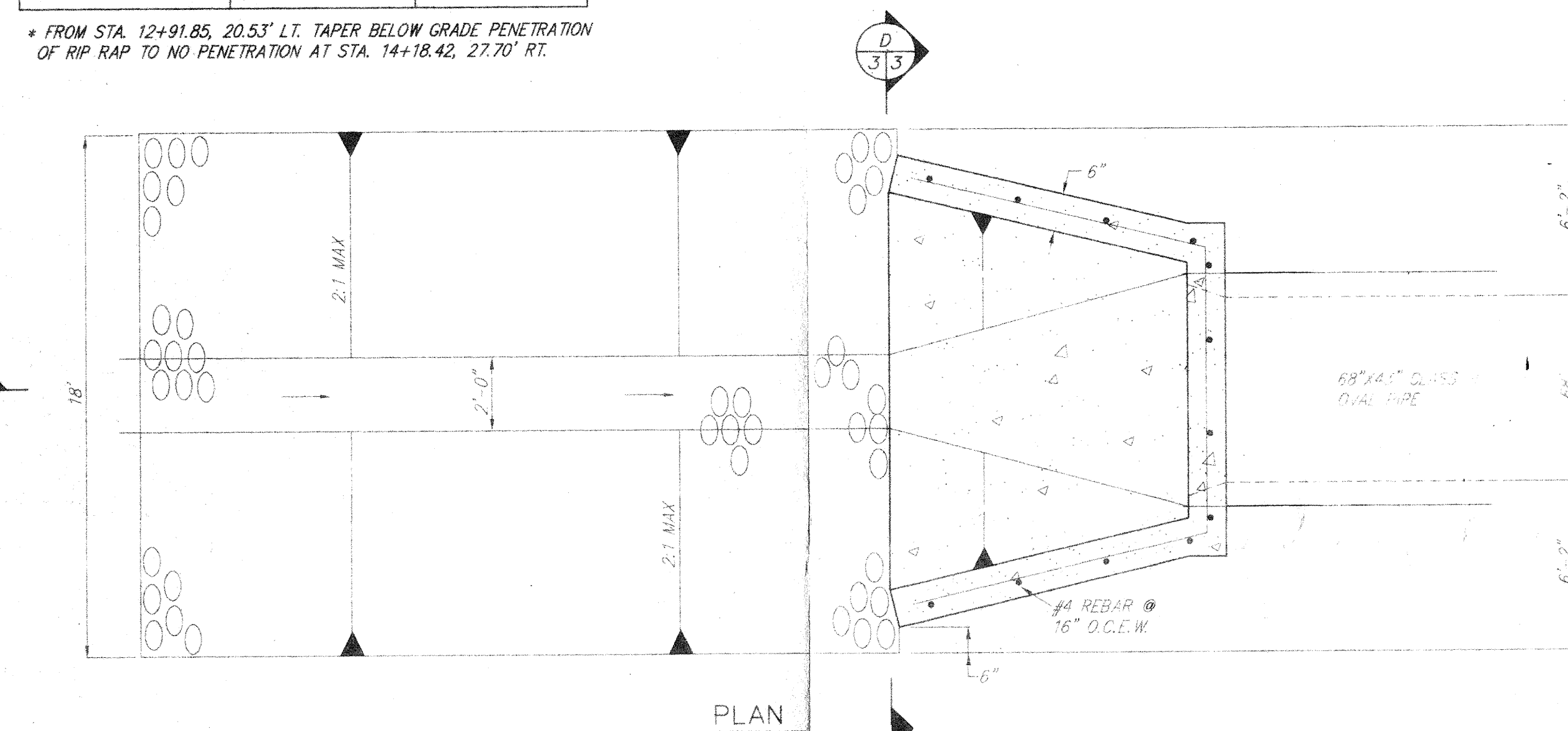
SCALE: NONE



SECTION

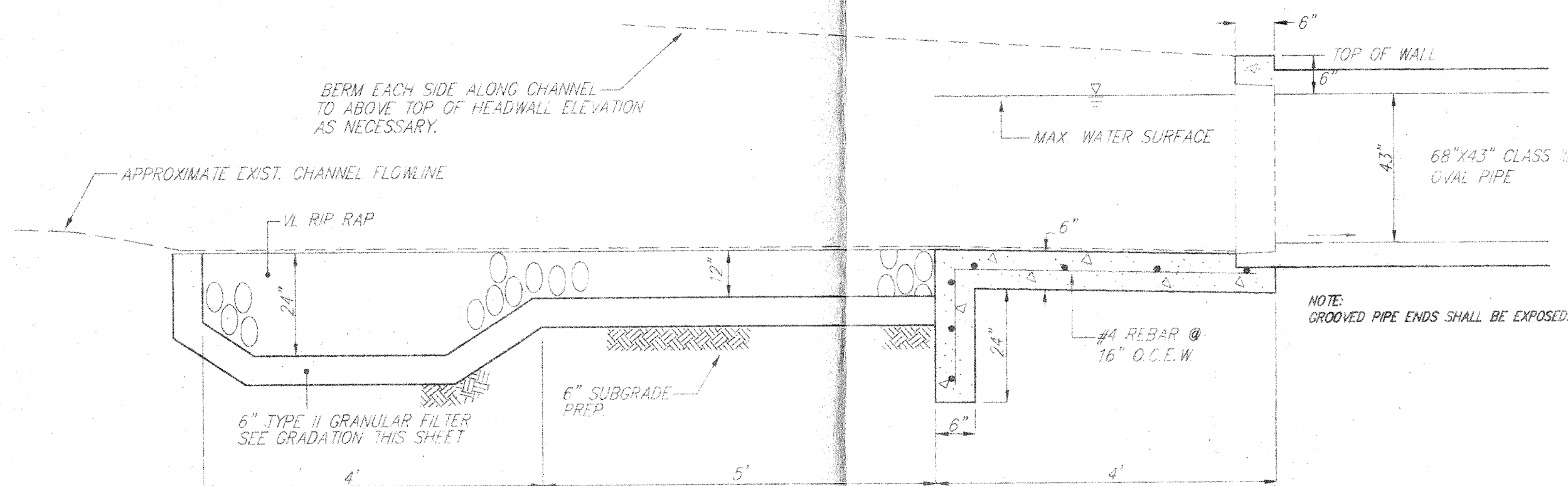
TRIBUTARY CHANNEL HEADWALL

SCALE: NONE



TRIBUTARY CHANNEL HEADWALL

SCALE: NONE



PROFILE

TRIBUTARY CHANNEL HEADWALL

SCALE: NONE

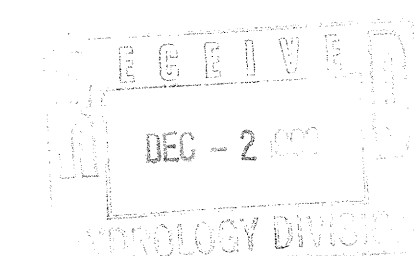
NOTES

1. CHANNEL EMBANKMENT MATERIAL PLACED BENEATH CHANNEL LINING AND FINAL SUBGRADE SHALL BE COMPACTED TO A MIN. OF 90% OF ASTM D-1557.

NORTH BRANCH - SOUTH DOMINGO BACA ARROYO
ARROYO CHANNELIZATION DETAILS

dmg D. MARK GOODWIN & ASSOCIATES, P.A.
CONSULTING ENGINEERS & SURVEYORS
P.O. BOX 90606
ALBUQUERQUE, NEW MEXICO 87199
(505) 828-2200

Designed: JMM	Drawn: STAFF	Checked: DMG	Sheet 3 of 3
Scale: NONE	Date: 11/93	Job: 93093	



MOR/CHANLDTL

CURVE DATA - DESCRIBES TOE OF CONCRETE CHANNEL

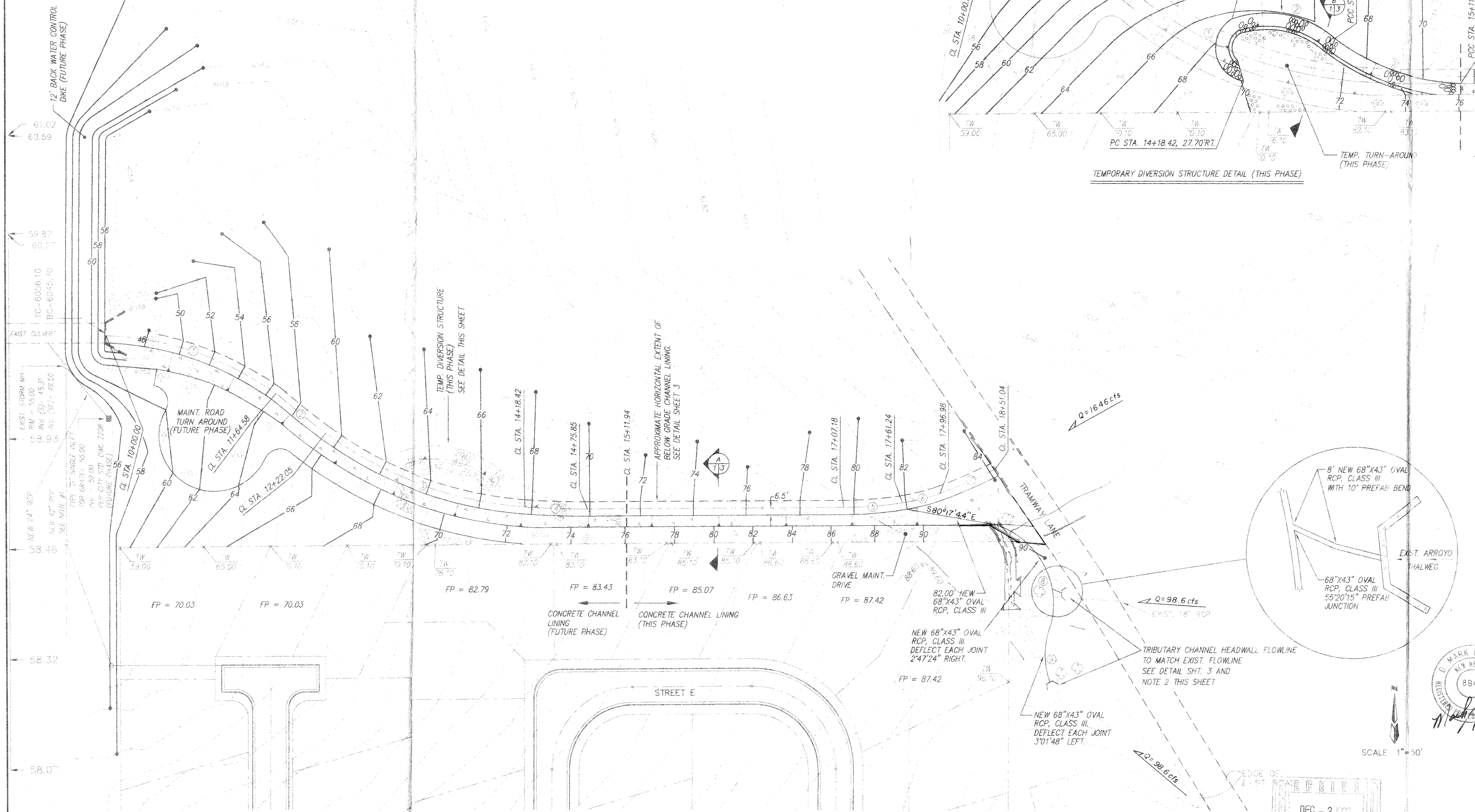
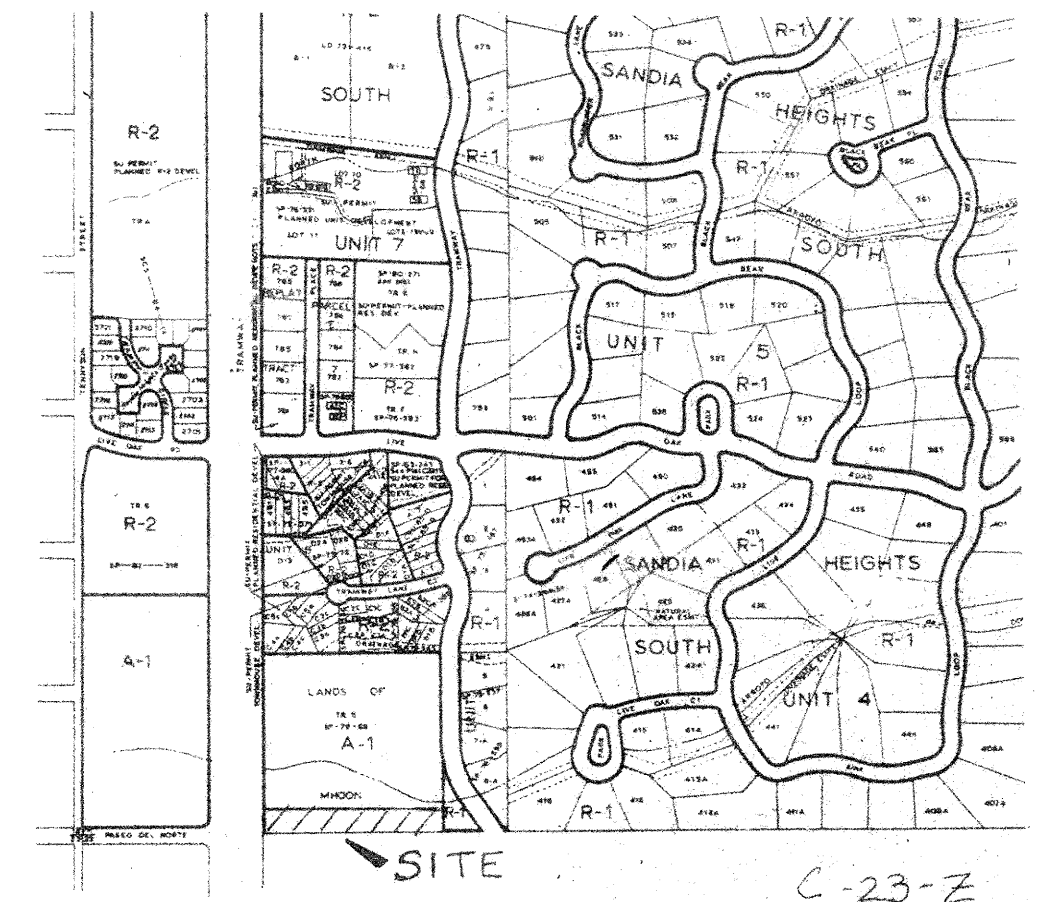
① Δ = 34°05'26"	② Δ = 04°38'29"	③ Δ = 31°57'51"
R = 270.11'	R = 716.00'	R = 358.50'
L = 160.71'	L = 58.00'	L = 200.00'
T = 82.81'	T = 29.02'	T = 102.68'
④ Δ = 04°38'17"	⑤ Δ = 08°14'58"	⑥ Δ = 11°04'13"
R = 715.96'	R = 382.00'	R = 191.50'
L = 57.96'	L = 55.00'	L = 37.00'
T = 28.99'	T = 27.55'	T = 18.56'
⑦ Δ = 08°14'58"	⑧ Δ = 87°42'47"	⑨ Δ = 39°36'09"
R = 382.00'	R = 75.00'	R = 75.00'
L = 55.00'	L = 114.82'	L = 51.84'
T = 27.55'	T = 72.06'	T = 27.00'

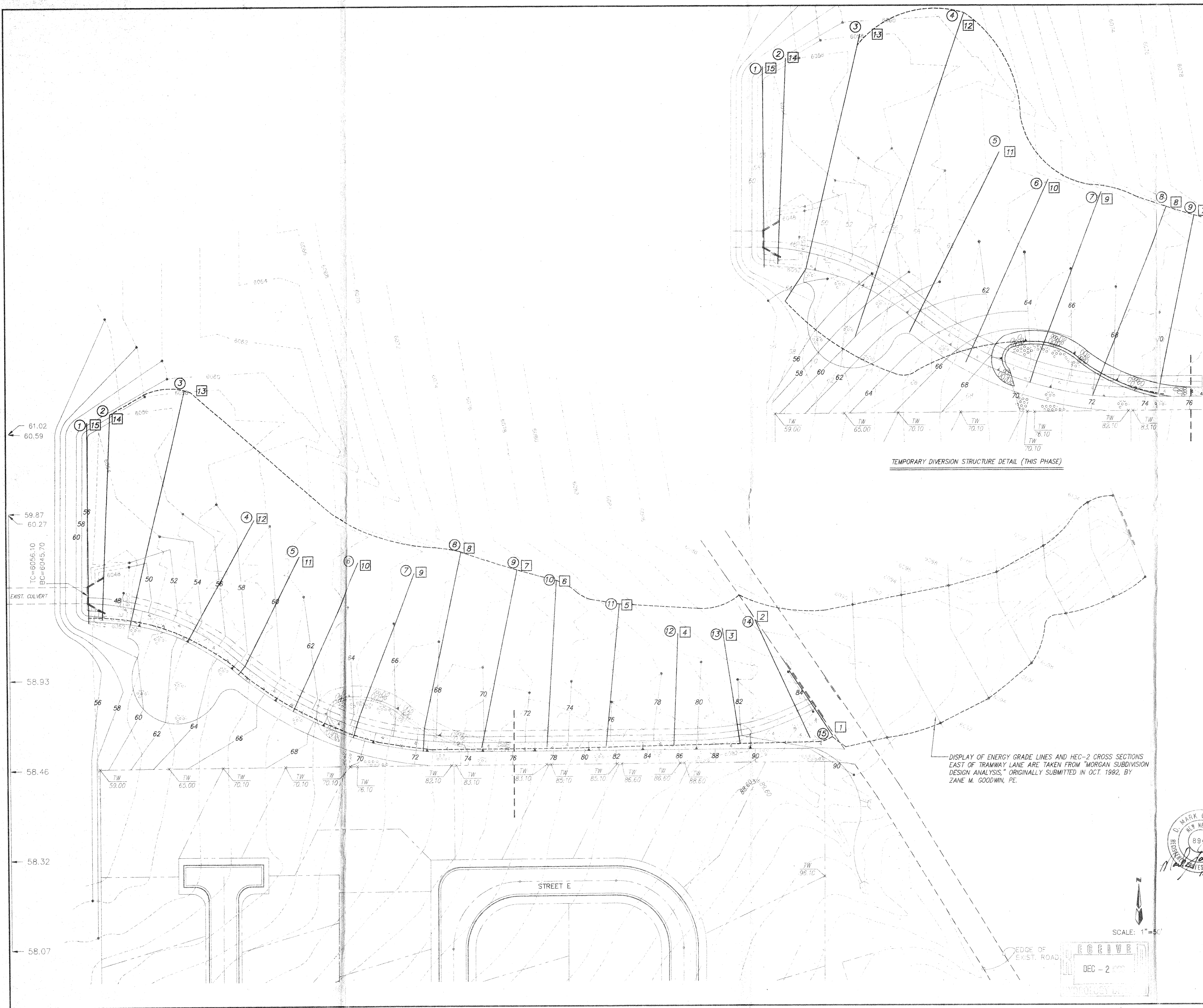
CURVE DATA - DESCRIBES TOE OF RIP RAP CHANNEL DIVERSION

① Δ = 139°41'43"	② Δ = 61°30'25"	③ Δ = 35°07'30"
R = 30.50'	R = 91.32'	R = 202.17'
L = 74.36'	L = 98.03'	L = 123.94'
T = 83.11'	T = 54.34'	T = 63.99'

NOTE:

1. REFER TO SHEET 13 OF MORGAN SUBDIVISION PLANS FOR DETAILS OF NEW DRAINAGE IMPROVEMENTS, DATED 2/93.
2. CONTRACTOR SHALL MAKE EFFORT TO MINIMIZE CONSTRUCTION DAMAGE TO EXISTING TREES IN THE VICINITY OF THE SUBSURFACE STORM DRAIN. CONTACT THE ENGINEER IF ANY CONFLICTS ARISE.

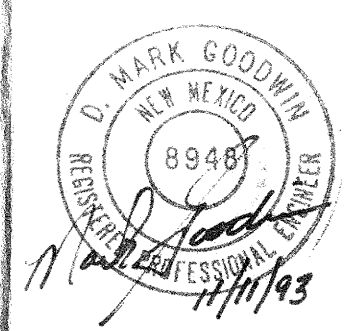




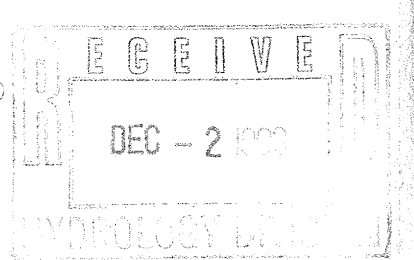
TEMPORARY DIVERSION STRUCTURE DETAIL (THIS PHASE)

DISPLAY OF ENERGY GRADE LINES AND HEC-2 CROSS SECTIONS EAST OF TRAMWAY LANE ARE TAKEN FROM "MORGAN SUBDIVISION DESIGN ANALYSIS," ORIGINALLY SUBMITTED IN OCT. 1992, BY ZANE M. GOODWIN, P.E.

- LEGEND:
- 70 — PROPOSED CONTOUR
 - --- ENERGY GRADE LINE
 - --- EXISTING CONTOUR
 - x 86.60 EXISTING SPOT ELEVATION
 - ④ SUBCRITICAL HEC-2 ANALYSIS
 - ⑫ SUPERCRITICAL HEC-2 ANALYSIS



SCALE: 1"=50'

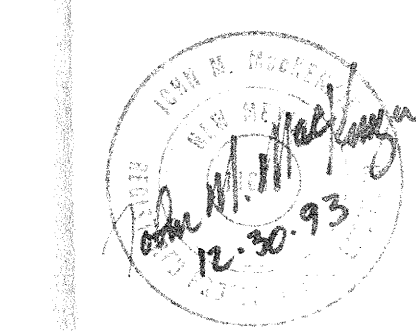


NORTH BRANCH — SOUTH DOMINGO BACA ARROYO

ARROYO CHANNELIZATION HYDRAULICS

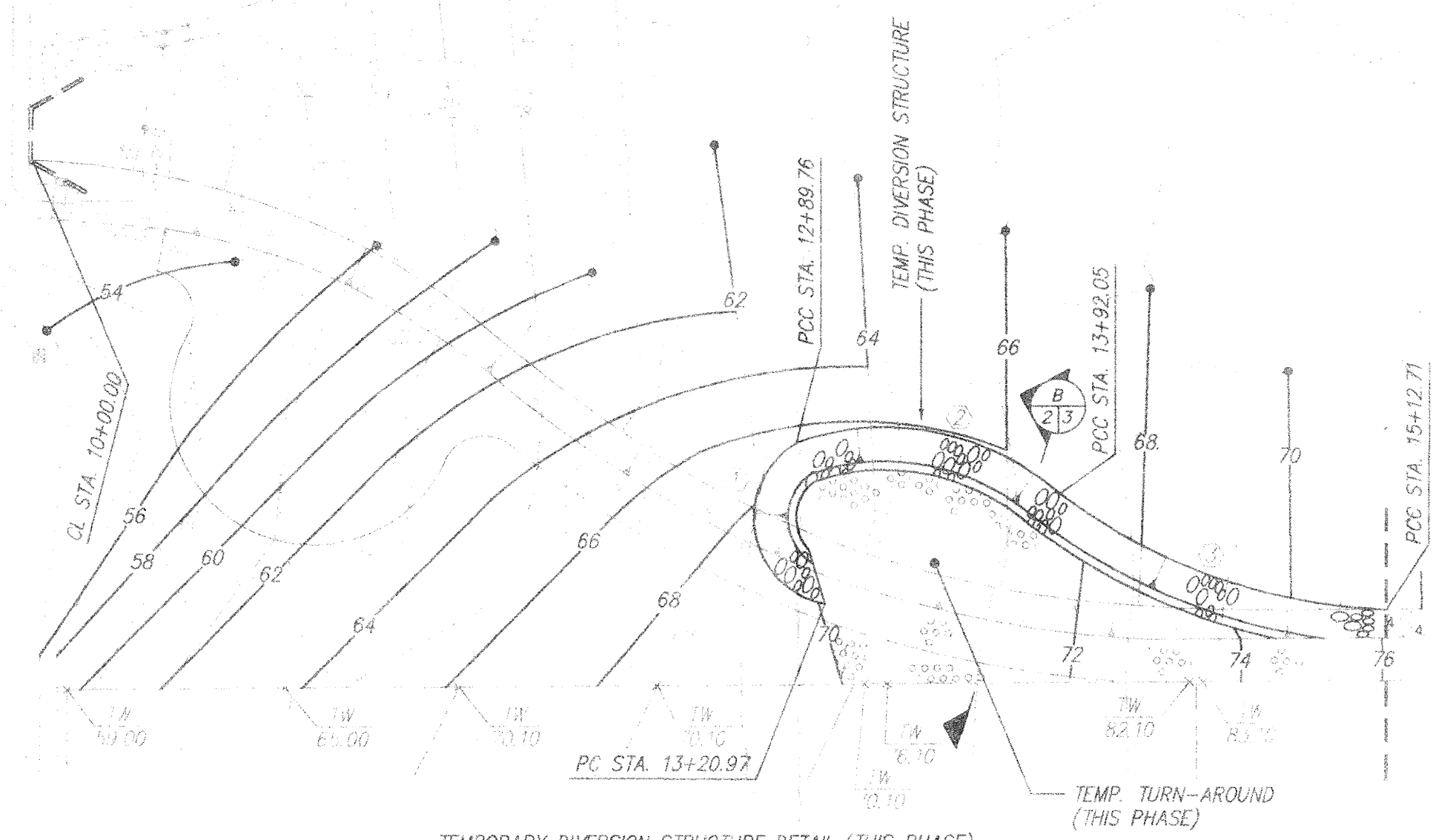
dmg D. MARK GOODWIN & ASSOCIATES, P.A.
CONSULTING ENGINEERS & SURVEYORS
P.O. BOX 90606
ALBUQUERQUE, NEW MEXICO 87199
(505) 828-2200

Designed: JMM	Drawn: STAFF	Checked: DMG	Sheet 2 of 3
Scale: 1"=50'	Date: 11/93	Job: 93093	

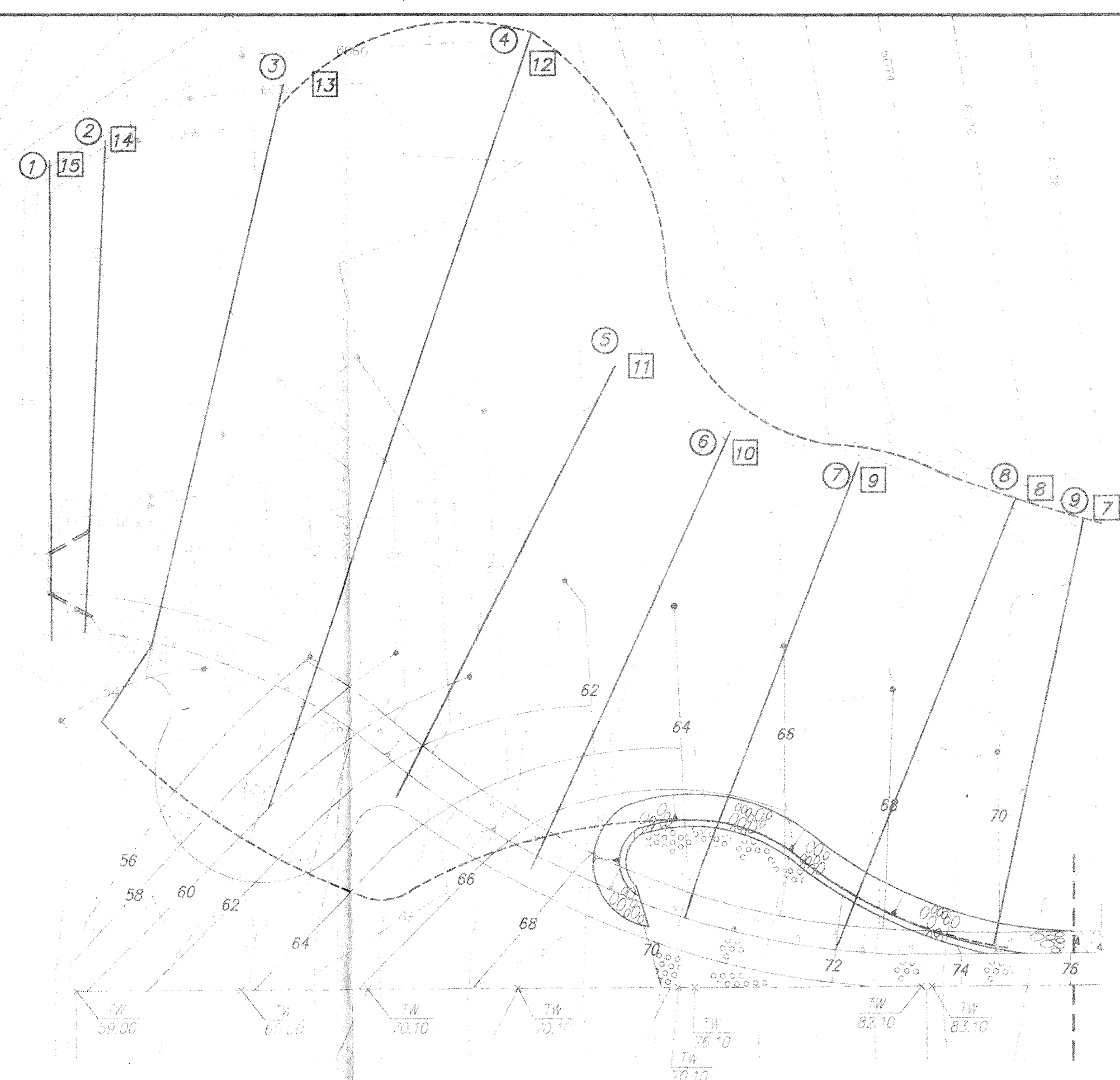


CURVE DATA - DESCRIBES TOE OF RIP RAP CHANNEL DIVERSION

① $\Delta = 139^{\circ}41'43''$ $R = 30.50'$ $L = 74.36'$ $T = 83.11'$
 ② $\Delta = 61^{\circ}30'25''$ $R = 91.32'$ $L = 98.03'$ $T = 54.34'$
 ③ $\Delta = 35^{\circ}07'30''$ $R = 202.17'$ $L = 123.94'$ $T = 63.99'$



TEMPORARY DIVERSION STRUCTURE DETAIL (THIS PHASE)



TEMPORARY DIVERSION STRUCTURE DETAIL (THIS PHASE)

APPROXIMATE LIMITS OF 100-YEAR FLOODPLAIN FROM FEMA PANEL NO. 350002 0011 C.

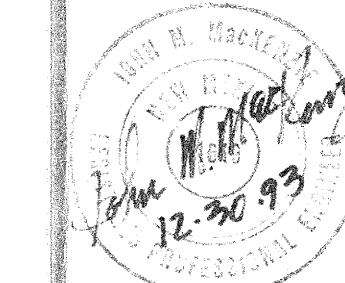
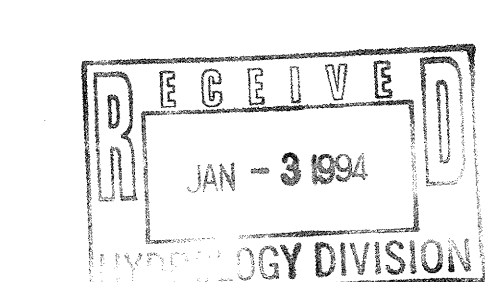
DRAINAGE EASEMENT TO BE GRANTED TO AMAFCA BY SUBSEQUENT DOCUMENT.

TEMPORARY DIVERSION STRUCTURE SEE DETAIL THIS SHEET.

DRAINAGE EASEMENT TO BE GRANTED TO AMAFCA BY SUBSEQUENT DOCUMENT.

DISPLAY OF ENERGY GRADE LINES AND HEC-2 CROSS SECTIONS EAST OF TRAMWAY LANE ARE TAKEN FROM "MORGAN SUBDIVISION DESIGN ANALYSIS," ORIGINALLY SUBMITTED IN OCT 1992, BY ZANE M. GOODWIN, PE.

- LEGEND:
- 70 PROPOSED CONTOUR
 - ENERGY GRADE LINE
 - EXISTING CONTOUR
 - EXISTING SPOT ELEVATION
 - ④ SUBCRITICAL HEC-2 ANALYSIS
 - ⑫ SUPERCRITICAL HEC-2 ANALYSIS

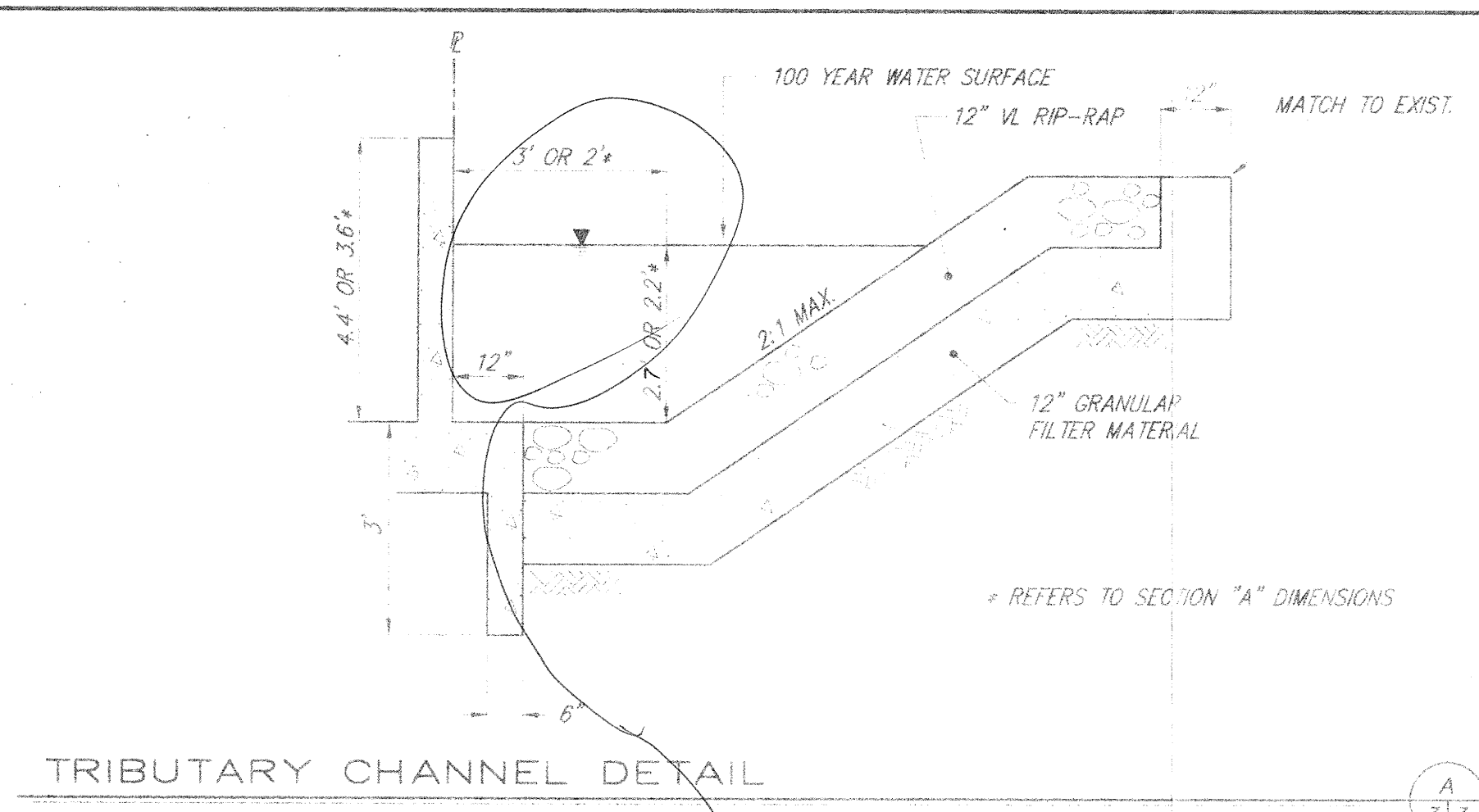


SCALE: 1"=50'

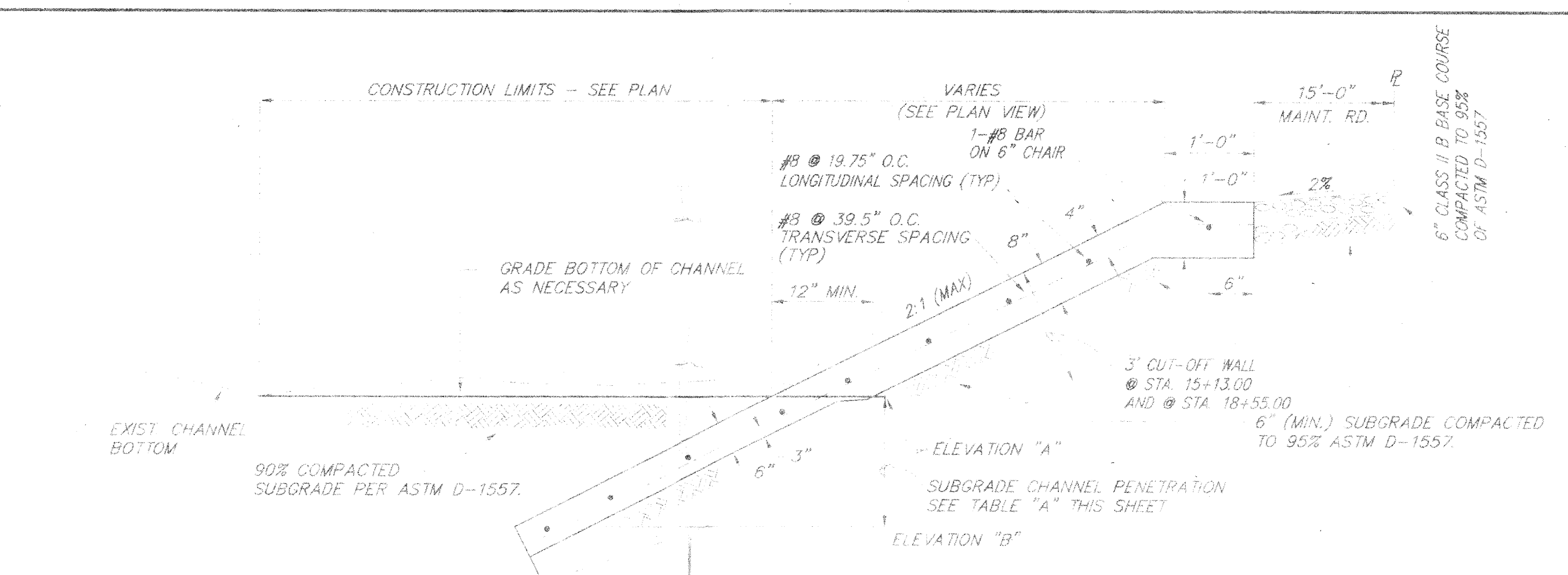
NORTH BRANCH - SOUTH DOMINGO BACA ARROYO
 ARROYO CHANNELIZATION HYDRAULICS

dmg D. MARK GOODWIN & ASSOCIATES, P.A.
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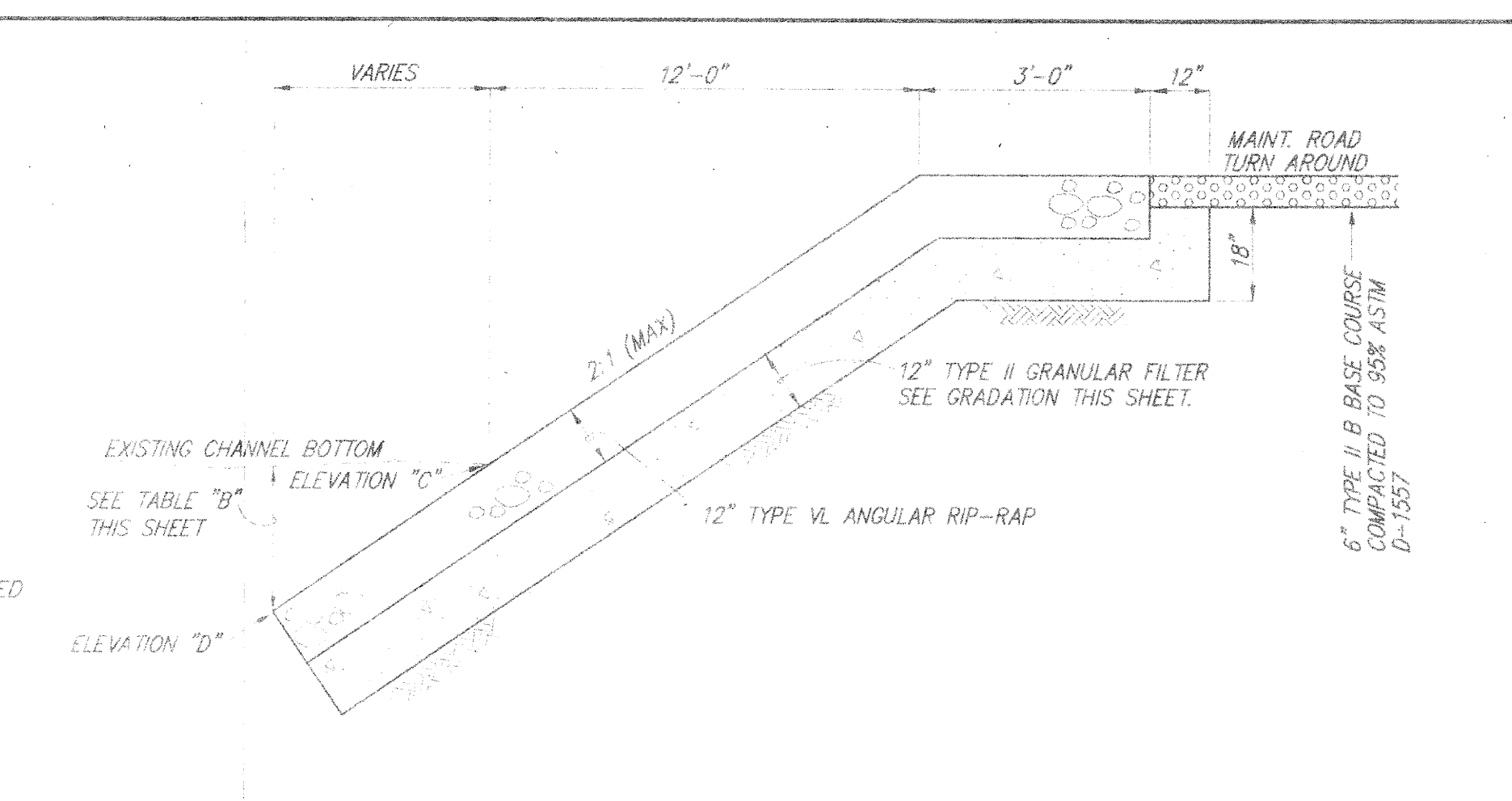
Designed: JMM	Drawn: STAFF	Checked: DMG	Sheet 2 of 3
Scale: 1"=50'	Date: 12/93	Job: 93033	



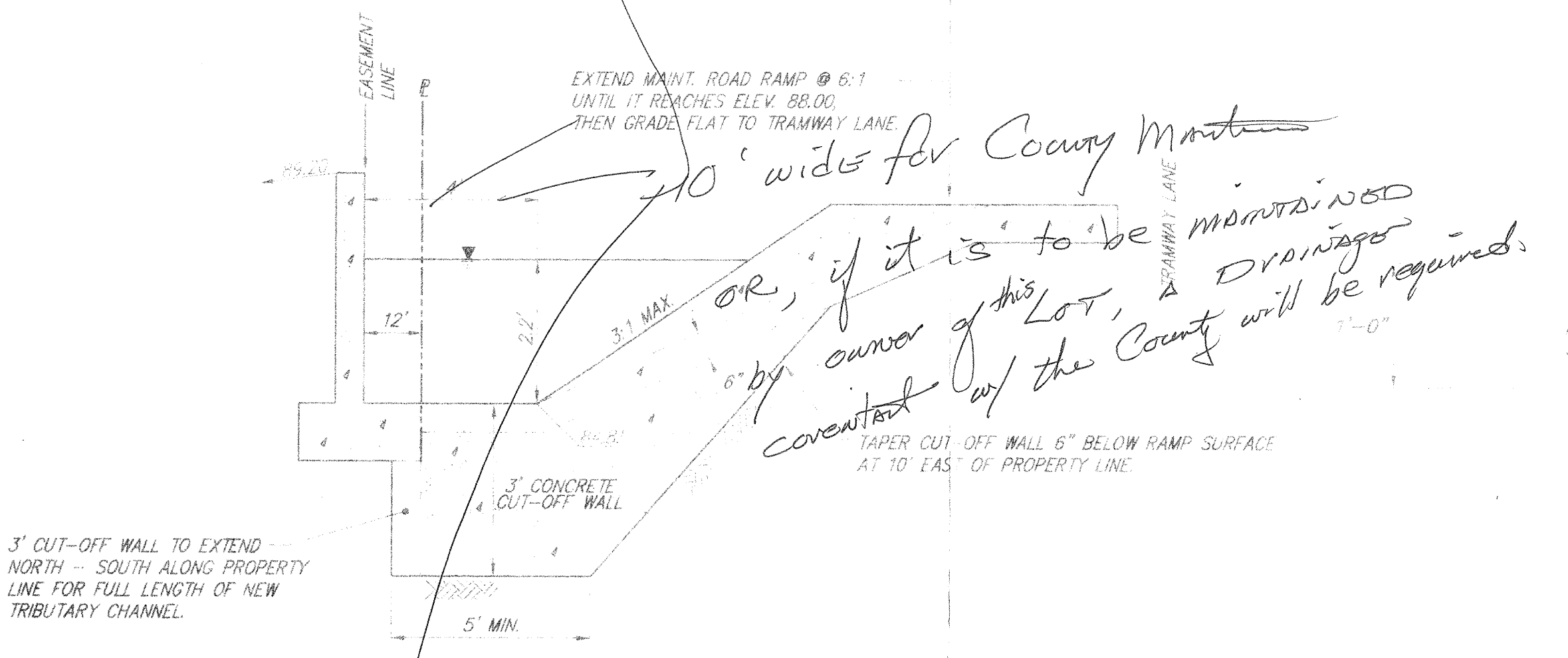
TRIBUTARY CHANNEL DETAIL



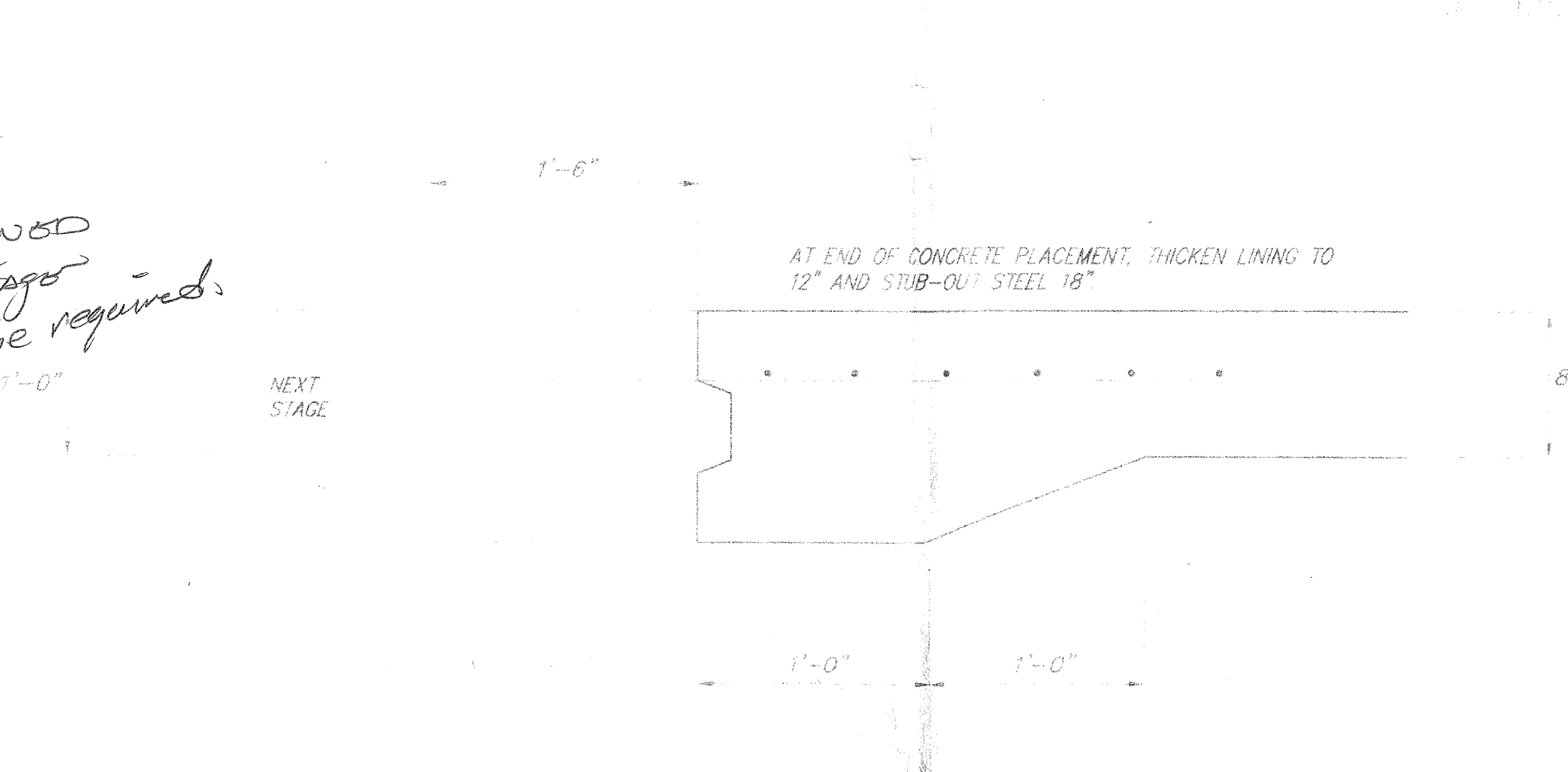
TYPICAL CHANNEL SECTION



TEMPORARY DIVERSION STRUCTURE (THIS PHASE)



TRIBUTARY CHANNEL DETAIL



TYPICAL TRANSVERSE CONSTRUCTION JOINT

TYPE II GRANULAR BEDDING GRADATION

U.S. STD. SIEVES SIZE	PERCENT PASSING BY WEIGHT SQUARE MESH SIEVES
3"	90-100
3/4"	20-30
#4	0-20
#200	0-3

CLASSIFICATION AND GRADATION OF RIPRAP

RIPRAP DESIGNATION	% SMALLER THAN GIVEN SIZE BY WEIGHT	INTERMEDIATE ROCK DIMENSION (INCHES)	MEAN PARTICLE SIZE - D ₅₀ (INCHES)
TYPE VI	70-100 50-70 35-50 2-10	12 9 6 2	6

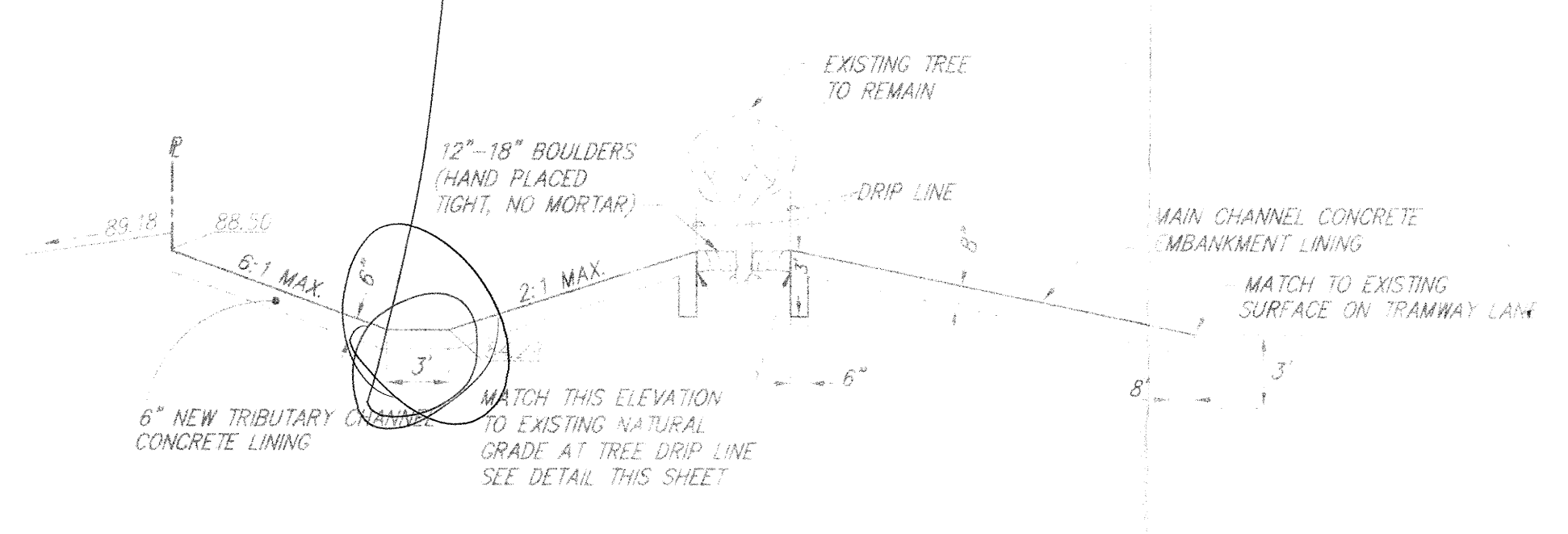
TABLE "A"

STATION	ELEVATION "A"	ELEVATION "B"
10+52.83	6048.97	6040.79
11+25.10	6053.71	6044.35
11+96.02	6058.21	6049.19
12+64.99	6061.25	6053.58
13+35.32	6064.30	6057.52
14+07.39	6067.48	6061.73
14+76.71	6070.20	6063.92
15+48.77	6073.04	6066.35
16+14.83	6075.81	6067.79
16+89.98	6078.90	6070.37
17+61.32	6081.84	6073.26
18+31.50	6083.65	6075.69

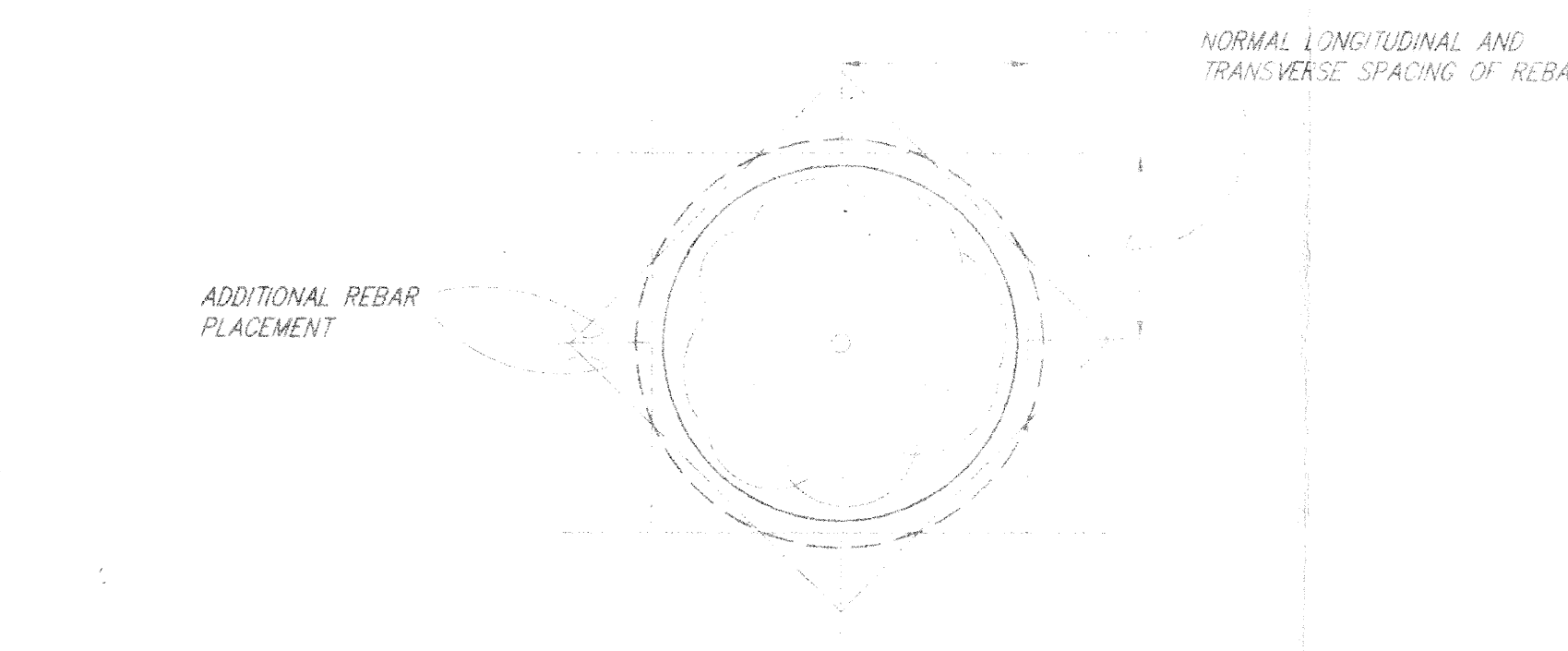
TABLE "B"

STATION	ELEVATION "C"	ELEVATION "D"
12+91.85, 20.53' LT. *	6062.75	6056.02
13+38.62, 41.13' LT.	6064.84	6057.92
14+14.89, 19.08' LT.	6067.64	6061.70
14+77.62, 2.20' RT.	6070.00	6064.36

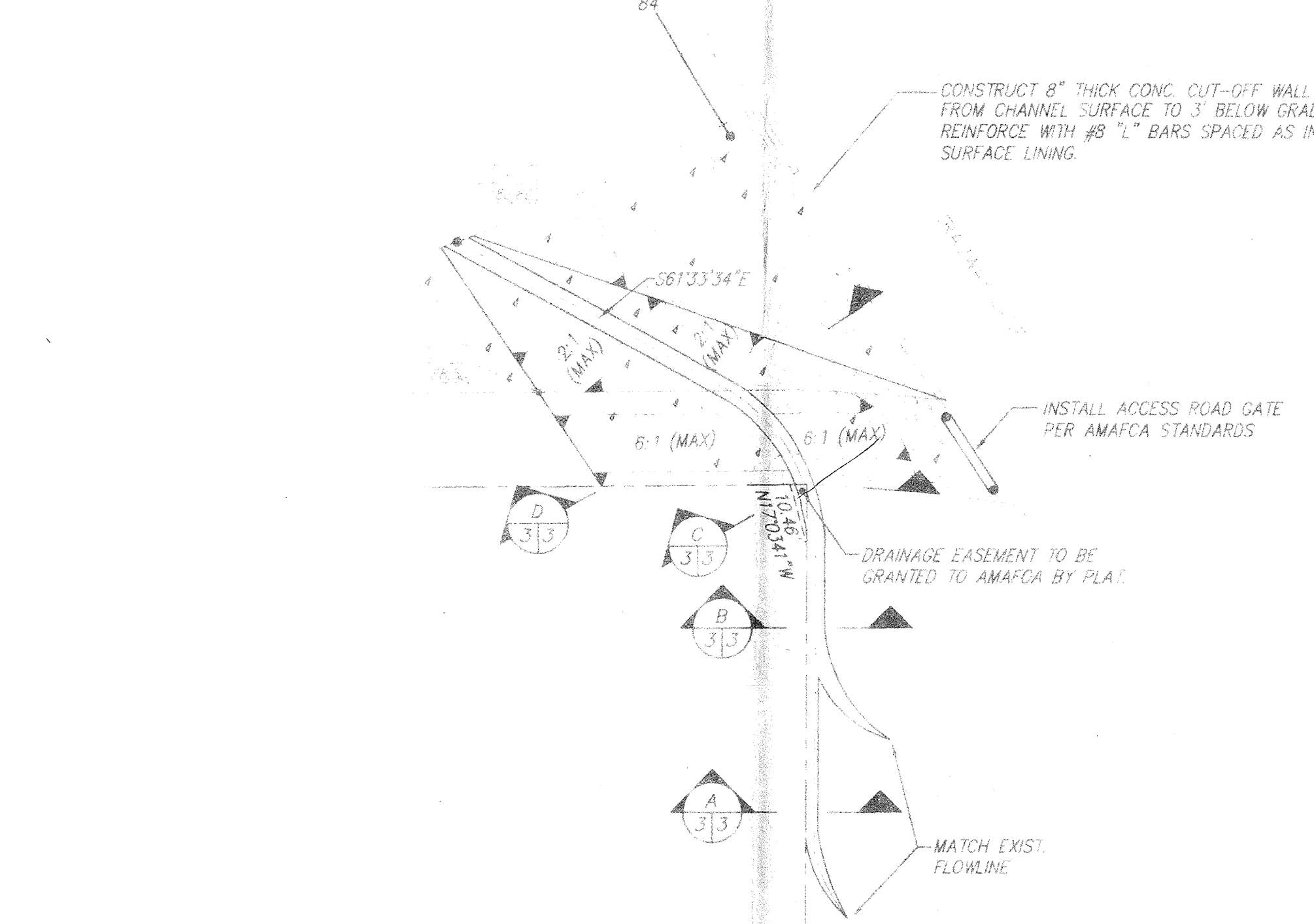
* FROM STA. 12+91.85, 20.53' LT. TAPER BELOW GRADE PENETRATION OF RIP RAP TO NO PENETRATION AT STA. 14+18.42, 27.70' RT.



TRIBUTARY CHANNEL - BETWEEN MAINTENANCE ROAD AND MAIN CHANNEL



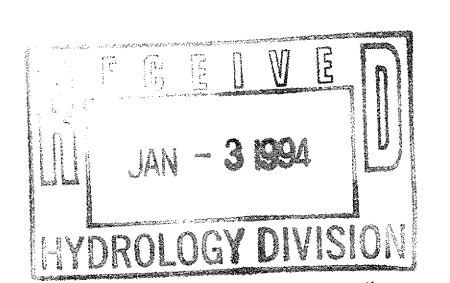
EXISTING TREE REINFORCEMENT PLAN DETAIL



TRIBUTARY CHANNEL PLAN DETAIL

CHANNEL CONCRETE NOTES:

1. TYPE IIA OR I-ILIA (NO CALCIUM)
2. MINIMUM OF 5.5 SACKS CEMENT / C.Y.
3. MAXIMUM W/C RATIO OF 0.53
4. SIZES OF COARSE AGGREGATE SHALL RANGE FROM #4 TO 1" IN DIA.
5. 20% FLYASH MEETING THE REQUIREMENTS OF ASTM C618.
6. RANGE OF AIR ENTRAINMENT SHALL BE 4-7%
7. MAXIMUM SLUMP SHALL BE 3"
8. MINIMUM COMPRESSIVE STRENGTH SHALL BE 3000 PSI @ 28 DAYS
9. ALL EXPOSED SURFACES SHALL HAVE A LIGHT BROOM FINISH
10. ALL EXPOSED CONCRETE SHALL BE TINTED DAVIS SAN DIEGO BUFF (OR EQUIVALENT) @ 1#/SACK
11. ALL STEEL REINFORCEMENT SHALL BE GRADE 60, ASTM 615.



John W. W. W. W. W.
12-30-93

NORTH BRANCH - SOUTH DOMINGO BACA ARROYO
ARROYO CHANNELIZATION DETAILS

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Scale: NONE	Date: 12/93	Job: 93093	