

CITY OF ALBUQUERQUE



January 14, 2017

Richard J. Berry, Mayor

Maryam Giahi, P.E.
Wilson & Company
4900 Lang Ave. NE
Albuquerque, NM, 87109

**RE: La Cuentista Subdivision – Tract B-2
Grading and Drainage Plan
Engineer's Stamp Date 1-3-17 (File: D10D002B)**

Dear Ms. Giahi:

Based upon the information provided in your submittal received 6-20-2016, the above referenced Grading and Drainage Plan and Report is approved for Preliminary Plat.

A submittal for Grading Permit will be needed prior to any Grading on the Site. An ESC Plan and Permit will be needed prior to Hydrology's approval for Grading.

If you have any questions, you can contact the City Engineer, at 924-3999.

Sincerely,

Abiel Carrillo, P.E.
Principal Engineer, Planning Dept.
Development Review Services

PO Box 1293

Albuquerque

New Mexico 87103

www.cabq.gov

Orig: Drainage file



City of Albuquerque

Planning Department

Development & Building Services Division DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 02/2013)

Project Title: La Cuentista Subdivision Tract B-2 Building Permit #: _____ City Drainage #: D100002B
DRB#: 1000922 EPC#: _____ Work Order#: _____
Legal Description: _____
City Address: Rosa Parks Rd NW, Albuquerque, NM
Engineering Firm: Wilson & Company, Inc. Contact: Maryam Giahi
Address: 4900 Lang Ave NE Albuquerque, NM 87109
Phone#: 505-948-5133 Fax#: _____ E-mail: mdgiahi@wilsonco.com
Owner: Legacy Sustainable Development Contact: Frances Pavich
Address: 21 Vista Calle Cir., Lamy, NM 87540
Phone#: 505-980-9124 Fax#: _____ E-mail: Email: legacy@cybermesa.com
Architect: _____ Contact: _____
Address: _____
Phone#: _____ Fax#: _____ E-mail: _____
Surveyor: _____ Contact: _____
Address: _____
Phone#: _____ Fax#: _____ E-mail: _____
Contractor: _____ Contact: _____
Address: _____
Phone#: _____ Fax#: _____ E-mail: _____

TYPE OF SUBMITTAL:

- ☒ DRAINAGE REPORT
☐ DRAINAGE PLAN 1st SUBMITTAL
☐ DRAINAGE PLAN RESUBMITTAL
☐ CONCEPTUAL G & D PLAN
☐ GRADING PLAN
☐ EROSION & SEDIMENT CONTROL PLAN (ESC)
☐ ENGINEER'S CERT (HYDROLOGY)
☐ CLOMR/LOMR
☐ TRAFFIC CIRCULATION LAYOUT (TCL)
☐ ENGINEER'S CERT (TCL)
☐ ENGINEER'S CERT (DRB SITE PLAN)
☐ ENGINEER'S CERT (ESC)
☐ SO-19
☐ OTHER (SPECIFY)

CHECK TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

- ☐ SIA/FINANCIAL GUARANTEE RELEASE
☒ PRELIMINARY PLAT APPROVAL
☐ S. DEV. PLAN FOR SUB'D APPROVAL
☐ S. DEV. FOR BLDG. PERMIT APPROVAL
☐ SECTOR PLAN APPROVAL
☐ FINAL PLAT APPROVAL
☐ CERTIFICATE OF OCCUPANCY (PERM)
☐ CERTIFICATE OF OCCUPANCY (TCL TEMP)
☐ FOUNDATION PERMIT APPROVAL
☐ BUILDING PERMIT APPROVAL
☐ GRADING PERMIT APPROVAL
☐ PAVING PERMIT APPROVAL
☐ WORK ORDER APPROVAL
☐ GRADING CERTIFICATION
☐ SO-19 APPROVAL
☐ ESC PERMIT APPROVAL
☐ ESC CERT. ACCEPTANCE
☐ OTHER (SPECIFY)



RECEIVED
1-9-17

WAS A PRE-DESIGN CONFERENCE ATTENDED: ☒ Yes ☐ No ☐ Copy Provided
DATE SUBMITTED: 01-03-17 By: Maryam Giahi

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location, and scope to the proposed development defines the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

1. **Conceptual Grading and Drainage Plan:** Required for approval of Site Development Plans greater than five (5) acres and Sector Plans
2. **Drainage Plans:** Required for building permits, grading permits, paving permits and site plans less than five (5) acres
3. **Drainage Report:** Required for subdivision containing more than ten (10) lots or constituting five (5) acres or more
4. **Erosion and Sediment Control Plan:** Required for any new development and redevelopment site with 1-acre or more of land disturbing area, including project less than 1-acre than are part of a larger common plan of development

January 3, 2017

Mr. Abiel Carrillo, P.E.
Principal Engineer - Hydrology
Planning Department
600 2nd Street, NW
Albuquerque, NM 87102

RE: La Cuentista Subdivision, Tract B-2; D10D002B

Dear Mr. Carrillo,

Wilson & Company has reviewed the comments provided in an email dated Dec. 29, 2016 on the La Cuentista Subdivision Tract B-2 Project. **Below are the responses to the comments:**

1. A maintenance agreement and covenants will be required to be a part of the SIA. For now, the Infrastructure List just needs to include the requirement in the Notes section. **Note added**
2. The 18" Diameter pipe on Page 3 on Line 9 of the infrastructure List should be 24" (the short segment from the inlet to the manhole) around the bend. **Pipe sizes upstream of manhole was upsized to 30" due to addition of inlets. Mainline does not include 18" pipe**
3. Show the intended crown to no crown transitions on the Grading Plan 9th this can be deferred to Grading Permit). **Crown transitions added to grading plan**
4. The corner of Smoketree and Redroot is proposed to drain by setting the outer corner high. Will this fit with the future extension to the west? It should not be planned for the interim condition only, or the Developer would be responsible for reconstructing the corner to produce a standard, smooth transition to the west. **Yes, in the future a transition will be required as Tract B-1 develops, a high point in Smoketree west of Redroot will be added to direct runoff**
5. Show the proposed manhole information (at least proposed depths/inverts) on the Grading Plan. **Manhole depths were added to the plan**
6. The inlets just north of Cornsilk are Double Type "C". Since they are the most upstream inlets, they need to be Type "A", or a combination of a single Type "A" + Type "C". The downstream inlets can be Type "C", per the DPM. **Inlets revised to Type A and C**
7. Provide invert information for the existing inlets along Rosa Parks Rd, and the invert of the inlet pipes within Pond 1 on the Grading Plan. **Added to the plan**
8. Clarify on the Grading Plan how the Open Space area between blocks 1 and 4 will drain. Will it utilize the existing stub? **Graded to drain to a pillbox manhole to connect to the existing cap in Rosa Parks road. The area produces less than 1 cfs.**

9. Provide elevation information for the interim Pill Box off of Redroot St. on the Grading Plan.
Added to the plan
10. On Page 3 of the Report there is a minor discrepancy between the text and the table for the Pond MSWEL for the Ultimate Condition (when the pond is operating as a detention pond). **Note deleted**
11. Show on the Grading Plan where the existing temporary storm drain cap is located. **Note added to the plan**
12. What is the Max Surface Elevation of the Pond in the Interim Condition (under retention conditions). **Note added to**
13. The Grading Plan describes the interim conditions as described in Section 5.3 (Page 4) of the Report, where Pond 1 is a 10-day Retention Pond. A such, it is confusing to include elements of the Ultimate Conditions such as the Outflow Discharge rate of Pond 1, and the detention volume instead of the retention volume needed (which means that the pond needs to be larger?). When the interim condition is transformed into the Ultimate Condition, a new, separate Grading Plan should be completed. Alternatively, the Grading Plan should be developed for the Interim Plan AND a Final Plan since you are trying to get approval for both scenarios depending on the Construction schedule of offsite improvements. **Table added to clarify the Developed and Interim Conditions pond data. La Cuentista Subdivision Unit II is to be constructed early this year. The ultimate conditions pond footprint will be used in the Interim Condition if no outfall from Pond 1 is available.**
14. Clarify the Ultimate, Developed and Interim Conditions in the exhibits. **Plate title corrected for Plate 1 to read Tracts B-1 and B-2, Plate 2 show Tract B-2 in the Developed Condition. Interim Condition is only if no outfall is available which is noted on the Grading and Drainage Plan**
 - a. In the Ultimate Condition, Basin 201 is built out. So show the conceptual layout that is known so far on Plate 1. **Conceptual layout is added**
 - b. Are these statements correct (just to make sure I understand the sections of the report):
 - i. In the "Developed Condition", Tract B-2 is developed and the Outfall through La Cuentista Phase II is available. The Pond then needs to be a detention pond with the smaller footprint. **Yes. Note added to report**
 - ii. In the "Interim Condition", Tract B-2 is developed and the Outfall through La Cuentista Phase II is NOT available. The Pond then needs to be a retention Pond with the footprint shown on Plate 1. **Yes. Note added to report**
 - iii. In the "Ultimate Condition", Tract B in its entirety is developed and the Outfall through La Cuentista II is available. The Pond then needs to be a detention Pond with the footprint shown on Plate 1. **Yes. Note added to report**
15. Also, just to clarify, these comments are specific to Preliminary Plat, although some of these comments would apply to the review for Grading Permit, no grading is allowed on this site until approval for Grading is secured.

16. As previously agreed, the wall heights are higher than the Sector Plan guidelines because it does appear that it is necessary to improve tie ins. The interior walls were designed higher, and the outer walls are held closer to the Sector Plan guidelines. As noted in the Sector Plan, these are variances that can be approved by Hydrology (no need to respond to this comment).

Please feel free to contact me at 505-948-5133 or via email, should you have any further questions or comments on these responses, The La Cuentista Subdivision Tract B-2 project. Thank you for your time.

WILSON & COMPANY



Maryam Giahi, P.E.

Project Engineer

maryam.giahi@wilsonco.com

Current DRC
Project Number:

FIGURE 12
INFRASTRUCTURE LIST

Date Submitted: 1/3/2017

Date Site Plan Approved:

Date Preliminary Plat Approved:

Date Preliminary Plat Expires:

DRB Project No.:

DRB Application No.:

1000922
16-70322

"EXHIBIT A"
TO SUBDIVISION IMPROVEMENTS AGREEMENT
DEVELOPMENT REVIEW BOARD (D.R.B.) REQUIRED INFRASTRUCTURE LIST

LA CUENTISTA SUBDIVISION TRACT B-2

PROPOSED NAME OF PLAT

PRELIMINARY PLAT OF LA CUENTISTA SUBDIVISION TRACT B-2

EXISTING LEGAL DESCRIPTION PRIOR TO PLATTING ACTION

Following is a summary of PUBLIC/PRIVATE Infrastructure required to be constructed or financially guaranteed for the above development. This Listing is not necessarily a complete listing. During the SIA process and/or in the review of the construction drawings, if the DRC Chair determines that appurtenant items and/or unforeseen items have not been included in the infrastructure listing, the DRC Chair may include those items in the listing and related financial guarantee. Likewise, if the DRC Chair determines that appurtenant or non-essential items can be deleted from the listing, those items may be deleted as well as the related portions of the financial guarantees. All such revisions require approval by the DRC Chair, the User Department and agent/owner. If such approvals are obtained, these revisions to the listing will be incorporated administratively. In addition, any unforeseen items which arise during construction which are necessary to complete the project and which normally are the Subdivider's responsibility will be required as a condition of project acceptance and close out by the City.

Financially Guaranteed DRC #	Constructed Under DRC #	Size	Type of Improvement	Location	From	To	Construction Certification		
							Private		City Construct Engineer
							Inspector	P.E.	
			PAVING						
		One -half 34' F-F W/ 7' Retail Collector	Retail Collector Paving W/ C & G, 6' Sidewalk North Side	Rosa Parks Road	West Property Line	East Property Line	/	/	/
		48' F-F W/ 4' Median	Res. Paving W/ C& G, 6' Sidewalk Both Sides	Redroot Street	Rosa Parks Road	Privet Street	/	/	/
		30' F-F	Res. Paving W/ C & G, * 6' Sidewalk East Side, ** 6' Sidewalk West Side	Redroot Street	Privet Street	Smoketree Avenue	/	/	/
		30' F-F	Res. Paving W/ C & G, 6' Sidewalk North Side, * 6' Sidewalk South Side	Privet Street	Redroot Street	220' East of Redroot Street	/	/	/
		30' F-F	Res. Paving W/ C & G, * 6' Sidewalk Both Side	Privet Street	220' East of Redroot Street	96' South of Smoketree Avenue	/	/	/
		30' F-F	Res. Paving W/ C & G, ** 6' Sidewalk East Side, * 6' Sidewalk West Side	Privet Street	96' South of Smoketree Avenue	Smoketree Avenue	/	/	/

Financially Guaranteed DRC #	Constructed Under DRC #	Size	Type of Improvement	Location	From	To	Construction Certification		
							Private	P.E.	City Construct Engineer
		30" F-F	Res. Paving W/ C & G, 6' Sidewalk South Side, **6' Sidewalk North Side	Smokefree Avenue	Redroot Street	Privet Street	/	/	/
		30" F-F	Res. Paving W/ C & G, 6' Sidewalk Both Sides	Cornsilik Avenue	Redroot Street	Privet Street	/	/	/
			Street Lighting Per DPM	Rosa Parks Road			/	/	/
			WATER						
		8" Dia.	Waterline W/ Appertences	Redroot Street	Rosa Parks Road	Smokefree Avenue	/	/	/
		8" Dia.	Waterline W/ Appertences	Privet Street	Redroot Street	Smokefree Avenue	/	/	/
		8" Dia.	Waterline W/ Appertences	Smokefree Avenue	Redroot Street	Privet Street	/	/	/
		8" Dia.	Waterline W/ Appertences	Permanent 52' Roadway and Utility Easement	Privet Street	Existing 51' Public Roadway and Utility Easement North	/	/	/
		8" Dia.	Waterline W/ Appertences	Azucena Place	Rosa Parks Road	Permanent 52' Roadway and Utility Easement	/	/	/
		8" Dia.	SANITARY SEWER						
		8" Dia.	Sanitary Sewer Gravidy lines W/ Appertences	Redroot Street	Rosa Parks Road	Smokefree Avenue	/	/	/
		8" Dia.	Sanitary Sewer Gravidy linesn W/ Appertences	Privet Street	Redroot Street	Smokefree Avenue	/	/	/
		8" Dia.	Sanitary Sewer Gravidy linesn W/ Appertences	Smokefree Avenue	Redroot Street	Privet Street	/	/	/

Financially Guaranteed DRC #	Constructed Under DRC #	Size	Type of Improvement	Location	From	To	Construction Certification		
							Private Inspector	P.E.	City Construct Engineer
			STORM SEWER						
		48" Dia	Storm Drain Pipe	Redroot Street	Detention Pond	Privet Street	/	/	/
		N/A	Pond Inlet Structure	Redroot Street	North of Rosa Parks Road	Detention Pond	/	/	/
		18" Dia.	Storm Drain pipe W/Inlet	Redroot Street	Redroot Street	Lot 1, Block 1	/	/	/
		36" Dia	Storm Drain Pipe	Redroot Street	Privet Street	Corn silk Avenue	/	/	/
		24" Dia.	Storm Drain Pipe	Redroot Street	Corn silk Avenue	Lot 1, Block 3	/	/	/
		18" Dia.	Storm Drain pipe W/Inlets	Redroot Street	Lot 1, Block 3	Lot 2, Block 3	/	/	/
		36" Dia.	Storm Drain Pipe W/Stub out	Corn silk Avenue	Redroot Street	West of Redroot Street	/	/	/
		36" Dia.	Storm Drain Pipe	Privet Street	Redroot Street	Lot 6, Block 1	/	/	/
		30" Dia.	Storm Drain pipe W/Inlets	Privet Street	Lot 6, Block 1	Lot 1, Block 4	/	/	/
		24" Dia.	Storm Drain Pipe	Privet Street	Lot 1, Block 4	Lot 8, Block 4	/	/	/
		18" Dia.	Storm Drain pipe W/Inlets	Privet Street	Lot 6, Block 1	Lot 6, Block 1	/	/	/
		18" Dia.	Storm Drain pipe W/Inlets	Privet Street	Lot 9, Block 4	Lot 10, Block 4	/	/	/
		18" Dia.	Pond Outlet Structure	Detention Pond	Detention Pond	Existing Inlet on Rosa Parks Road	/	/	/
		0.29 ac-ft	First Flush Volume	Pond 1	N/A	N/A	/	/	/
NOTES									
1 - * 6" sidewalk deferred per current DRB Project # 1000922 (Tract B-2 home construction)									
2 - ** 6" sidewalk deferred per current DRB Project # 1000922 (Future Tract B-1 home construction)									
3 - Storm drain maintenance agreement and covenant for Pond 1									

Financially Guaranteed DRC #	Constructed Under DRC #	Size	Type of Improvement	Location	From	To	Construction Certification		
							Private	P.E.	City Construct Engineer

AGENT/OWNER		DEVELOPMENT REVIEW BOARD MEMBER APPROVALS	
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Maryam Ghihi (Agent) NAME(print) Wilson & Co., 4900 Lang Ave. NE 87109	DRB CHAIR -- date PARKS & GENERAL SERVICES -- date
---	---

FIRM SIGNATURE 01-03-17	TRANSPORTATION DEVELOPMENT -- date ABCWUA -- date AMAFCA -- date
-------------------------------	--

MAXIMUM TIME ALLOWED TO CONSTRUCT
 THE IMPROVEMENTS WITHOUT A DRB
 EXTENSION: _____ CITY ENGINEER -- date _____ - date _____

DESIGN REVIEW COMMITTEE REVISIONS				
REVISION	DATE	DRB CHAIR	USER DEPARTMENT	AGENT/OWNER

Drainage Report

for

**LA CUENTISTA SUBDIVISION,
TRACTS B-1 AND B-2**

December 2016

Prepared for:

Legacy Sustainable Development, Inc.

Prepared by:

**Wilson & Company, Inc.
4900 Lang Avenue NE
Albuquerque, New Mexico 87109
(505) 348-4000
(505) 348-4072**

WCI File No: 16-600-006-00

Drainage Report

for

LA CUENTISTA SUBDIVISION, TRACTS B-1 AND B-2

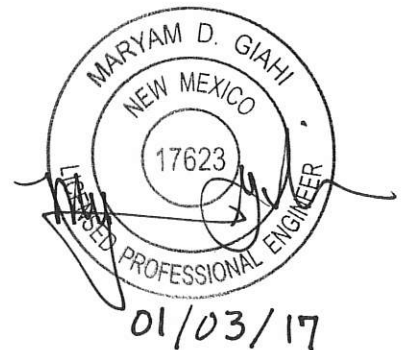
December 2016

Prepared for:

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4900 Lang Avenue NE
Albuquerque, New Mexico 87109
(505) 348-4000
(505) 348-4072**



WCI File No: 16-600-006-00

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- 6. First Flush Retention Calculations**
- 7. Hydraulics**
- 8. Conclusion**

Appendix A

Related Documents

- VCSDP Zoning Map
- NOAA Atlas Point Precipitation Frequency Estimates
- FEMA FIRM

Appendix B

Hydrology Calculations

- AHYMO Models Summary and Input Files
 - o Ultimate Conditions
 - o Developed Conditions

Appendix C

Hydraulic Calculations

- FlowMaster Calculations
 - o Street Capacity
 - o Inlet Capacity
- CulvertMaster Calculations
- Hydraflow Calculations
- Pillbox Manhole Calculations

Appendix D

Referenced Documents

- Selected pages from a Drainage Report for La Cuentista Subdivision – Unit II a Supplement to the Drainage Report for La Cuentista Subdivision
- Selected pages from Drainage Report Addendum for La Cuentista Subdivision – Unit II

- Selected sheets from La Cuentista Subdivision – Unit II Paving Plan & Profile sheets – Rosa Parks Road and Redroot Street

Appendix E

Plates/Plan

- Plate 1 – Ultimate Conditions Drainage Map
- Plate 2 – Developed Conditions Drainage Map
- Grading & Drainage Plan

1. Introduction

La Cuentista Subdivision Tract B now divided into Tracts B-1 and B-2 has an area of 60.18 acres is the fourth of five bulk land tracts which collectively comprise La Cuentista Subdivision. The site is bounded by Paseo Del Norte Boulevard to the north, Calle Plata to the east, Rosa Parks Road to the south and Urraca Street to the west. See Figure 1, Location Map.



Figure 1, Location Map

The site is located within boundaries of the Volcano Cliffs Sector Development Plan (VCSDP) and designated as Urban Residential (VCUR). See VCSDP Zoning Map in Appendix A.

2. Background

La Cuentista Subdivision Drainage Report dated November 2003 prepared by Wilson & Company, Inc. (WCI) was prepared for the overall site development of Tracts A through E. In January 2007, WCI prepared a Supplement to this Drainage Report due to changes to site designs of Tract A (Unit I) and Tract C (Unit II) and plans for Tract B. With these modifications, the west basin of Tract B drains into a proposed detention pond (Pond 1). The outflow from this pond and the east basin of Tract B drain into a second proposed detention pond (Pond 2) in the southeast corner of Tract B and north of Rosa Parks Road. The outfall from Pond 2 connects into an existing 24 inch storm drain stub out in Rosa Parks Road which connects to curb inlets in the road. This system is capped at the intersection of Rosa Parks Road and Redroot Street. Wilson & Company prepared a Drainage Report Addendum for La Cuentista Subdivision Unit II dated Dec. 2014 which analyzed existing conditions peak flows and runoff volume for the area. See Appendix D, Plate 1- Existing Conditions Map from La

Cuentista Subdivision Unit II Drainage Report Addendum. Plate 1 shows two offsite basins OS1 and OS8 drain a total of 52 cfs through the site into Rosa Parks Road. See Appendix D for selected pages of both reports.

A storm drain system to be constructed with La Cuentista Unit II offsite infrastructure improvements will connect to the capped storm drain in Rosa Parks Road conveying runoff from the pond in Tracts B-1 and B-2 and Unit II into Pond 4 in Unit I. The maximum allowable discharge from Tracts B-1 and B-2 is 15 cfs.

3. Methodology

The hydrologic model from the Supplement to the Drainage Report was utilized to compute peak flows and runoff volume from the site. Based on the 2007 model, the AHYMO 97 program was used for hydrologic calculations in development of the previous reports. See AHYMO Summary and input files in Appendices B & C. Rainfall data was updated per NOAA Atlas 14 website. See Appendix A, NOAA Atlas Point Precipitation Frequency Estimates. Land treatment percentages for Tracts B-1 and B-2 were updated per latest land use of 8 dwelling units per acre (du/ac). The Hydraflow Storm Sewers 2007 hydraulic model is used to analyze the storm system. Bentley CulvertMaster V3.3 is used to analyze culvert capacities. Bentley FlowMaster V8.i is utilized to compute street and inlet capacities. See Appendix C for calculations.

4. Existing Conditions

Tracts B-1 and B-2 of La Cuentista lies within the Flood Zone X – an area outside of the 500-year flood plain limits per FEMA Flood Insurance Rate Map (FIRM) number 35001C0112G, Panel 112 of 825 dated September 26, 2008. See Appendix A for FIRM. The site is vegetated with native grasses and shrubs. It slopes generally from west to southeast. Offsite flows have been minimized by construction of Paseo Del Norte Boulevard. Per La Cuentista Subdivision Unit II Drainage Report Addendum, two basins north and south of Unser Boulevard drain through the site. Tract B is divided into two basins east and west which both drain south into Rosa Parks Road then Pond 4 in Unit I and ultimately discharge through the Petroglyph National Monument. See Appendix D, Plate 1- Existing Conditions Map from La Cuentista Subdivision Unit II Drainage Report Addendum.

5. Proposed Conditions

Current Improvements are intended for Tract B-2 with an area of 11.2 ac. The rest of the site will remain undeveloped. The AHYMO model from the 2007 drainage report was updated to include the new rainfall data and land treatments. Two AHYMO models were developed to analyze the Ultimate and Developed Conditions for Tract B-2. Three conditions were developed which are described below:

- a. Ultimate Condition – This condition refers to when Tracts B-1 and B-2 are fully developed and the outfall through La Cuentista Unit II is available. A detention pond with footprint shown on Plate 1 is required.
- b. Developed Condition – This condition refers to when only Tract B-2 is developed and the outfall through La Cuentista Unit II is available. A detention pond with smaller footprint as shown on Plate 2 is required.

- c. Interim Condition – This condition refers to when only Tract B-2 is developed and the outfall through La Cuentista Unit II is not available. A retention pond with footprint shown on Plate 1 is required.

5.1 Ultimate Conditions

In the Ultimate Conditions, no offsite runoff will enter the site. Land treatments in the AHYMO model were modified for density of 8 du/ac for the entire site. The east basin was divided into smaller subbasins to correctly model the development. One pond was modeled to detain runoff from Tracts B-1 and B-2. Maximum allowable discharge from the site is about 15 cfs. See Tables 1 & 2, Ultimate Conditions AHYMO Results and Pond Data. Refer to Appendices B & C, 2007 & Ultimate Conditions AHYMO Summary and Input files.

Table 1 - Ultimate Conditions AHYMO Results, 100-Yr, 24-Hr				
Basin ID	Area		Peak Flow	Runoff Volume
	ac	sq mi	cfs	ac-ft
201	36.97	0.0578	129	5.7
202.1	8.43	0.0132	27	1.1
202.2	1.69	0.0026	6	0.3
202.3	11.01	0.0172	38	1.7

Ultimate Conditions Pond Data						
Peak Flow (cfs)		Pond Elevation (ft)		Volume (ac-ft)		Max WSEL
In	Out	Top*	Bottom**	Req'd	Prv'd	ft
201	15.5	5344.0	5336.5	5.97	9.48	5341.61
* Includes 1' freeboard						
** Elevation 5337.0 to 5336.5 is provided for the first flush volume						

In the Ultimate Conditions outflow from Pond 1 will be connected to the existing inlets in Rosa Parks Road. Maximum allowable discharge from the pond is 15.5 cfs. The storm system ultimately discharges into Pond 4 in Unit I. See Appendix E, Plate 1-Ultimate Conditions Drainage Map.

5.2 Developed Conditions

The Current Improvements are proposed for development of Tract B-2. The AHYMO model land treatments for the basin were adjusted. Per La Cuentista Subdivision Unit II Drainage Report Addendum, offsite basins draining into the site were included in the model. The offsite basin area covering Tract B-2 was adjusted in the model. See Appendix E, Plate 2 - Developed Conditions Drainage Map. See Developed Conditions Table 3, AHYMO Results, Table 4, Pond data and Appendix B, Developed Conditions AHYMO Summary and Input files.

Table 3 - Developed Condition AHYMO Results, 100-Yr, 24-Hr

Basin ID	Area		Peak Flow	Runoff Volume
	ac	sq mi	cfs	ac-ft
OS1	14.74	0.0230	17	0.52
OS8.1	59.51	0.0930	46	2.47
202.1	21.69	0.0339	27	0.77
202.2	3.29	0.0051	4	0.12
202.3	11.01	0.0172	38	1.70

Developed Conditions Pond Data

Peak Flow (cfs)		Pond Elevation (ft)		Volume (ac-ft)		Max WSEL (ft)
In	Out	Top*	Bottom**	Req'd	Prv'd	
103.4	15.6	5344.0	5336.0	3.42	5.28	5341.66
* Includes 1' freeboard						
** Elevation 5337.0 to 5336.0 is provided for the first flush volume						

A sediment capture area was designed to capture sediments from the undeveloped area of west basin sheet flowing into Rosa Parks Road. See Table 5 – Sediment Capture Area Data

Table 5 - Sediment Capture Area Data

Basin ID	Area		Peak Flow	Runoff Volume
	ac	sq mi	cfs	ac-ft
202.1	21.34	0.0333	1	0.07

5.3 Interim Conditions

In the Ultimate and Developed Conditions Pond 1 was designed as a detention pond. The pond outlet connects to the existing storm stub out from the inlets in Rosa Parks with 24 inch pipe which terminates at the intersection of Rosa Parks and Redroot Street. Redroot Street storm drain outfall is planned to be constructed with La Cuentista Unit II Subdivision this year. If this system is not constructed before Tract B-2 development, Pond 1 will serve as a retention pond. Calculations to retain the 10 day runoff volume per City of Albuquerque (COA) Development Process Manual (DPM) Chapter 22, Section 2, Hydrology was made which is summarized in Table 6.

Table 6 - Retention Pond Calculations							
Basin	Condition	Area (ac)	Land Treatment (%)				Volume (ac-ft)
							10 day
OS1	Existing	14.74	90	0	10	0	0.61
OS8.1	Existing	59.51	86	0	10	4	3.05
202.1	Existing	21.69	90	0	10	0	0.89
202.2	Existing	3.29	90	0	10	0	0.14
202.3	Developed	11.01	0	4	31	65	2.49
Total							6.29
*Sheet flows south into Rosa Parks Road							

Maximum water surface elevation in the interim conditions will be 5341.83 ft. When Redroot Street storm drain system construction is completed, the pond will be filled in and converted into a detention pond per Developed Conditions calculations.

6. First Flush Retention Calculations

Pond 1 will accommodate 'first flush' retention volume in compliance with the COA requirements for new developments per the "Significant Drainage Ordinance Changes" effective May 12, 2014. First Flush is defined as the 90th percentile storm event or 0.34 inch (0.44 inch less 0.1 inch for initial abstraction). See Table 7 – First Flush Volume Calculation.

Table 7 - First Flush Volume Calculation		
Rainfall Depth (in)	Impervious Area (ac)	V _{FF} (ac-ft)
0.34	10.36	0.29

The pond bottom elevation will be lowered one foot below the pond outlet invert elevation to provide a retention volume of 0.50 ac-ft.

7. Hydraulics

Tract B-2 includes an area of 11.2 ac. Improvements include 72 units. Inlets in developed areas of the site will capture street flows and convey runoff into Pond 1. Street and inlet capacity calculations were made utilizing Bentley FlowMaster. See Table 8, Inlet Calculation.

Table 8 - Inlet Calculations							
Analysis Point	Peak Flow (cfs)						
	Accumulated	Inlet		Captured		Bypass	Bypass to
		Sgl A	Dbl C	One side	Total		
AP2	8.0		3.1	3.1	6.2	1.8	AP5
AP3	14.0	-	4.7	4.7	9.5	4.5	AP4
AP4	16.8	8.4	-	8.4	16.8	0.0	-
AP5	7.5	3.8	-	3.8	7.5	0.0	-

A pillbox manhole at analysis point 1 was designed to capture offsite runoff of 46 CFS until Tract B-1 is developed and upstream drainage structures are constructed. See Appendix C, pillbox manhole calculations. Hydraflow Storm Sewers Extension for AutoCAD was used to analyze the proposed storm system. See Appendix C, FlowMaster & Hydraflow Calculations and Grading & Drainage Plan in Appendix E. Inlets were designed with the maximum hydraulic grade line below top of curb elevation and a minimum of leaving one dry driving lane.

Runoff from offsite basins west of Tract B-2 will be collected in a pillbox manhole and conveyed by the onsite storm drain system. This pillbox manhole will be converted into a regular manhole when areas west of Tract B-2 are developed. See Appendix C, FlowMaster Calculations. Pond 1 outlet will tie to the existing inlet in Rosa Parks Road. See CulvertMaster Calculations in Appendix C. The underground storm system will be conveyed through Redroot Street into Pond 4 in Unit I.

8. Conclusion

Per analysis presented in this report, Ponds 1 was designed to detain developed flows from the onsite east and west basins in the ultimate Conditions. Drainage improvements recommended for Tract B-2 are capable of collecting and conveying accumulated runoff to Pond 1. This Pond contains retention volume to store the first flush in compliance with the COA requirements for new developments.

Pond 1 outlet will tie into the existing underground storm system in Rosa Parks Road which outfalls into La Cuentista Subdivision Unit I Pond 4.

Appendix A

Related Documents

- VCSDP Zoning Map
- NOAA Atlas Point Precipitation Frequency Estimates
- FEMA FIRM

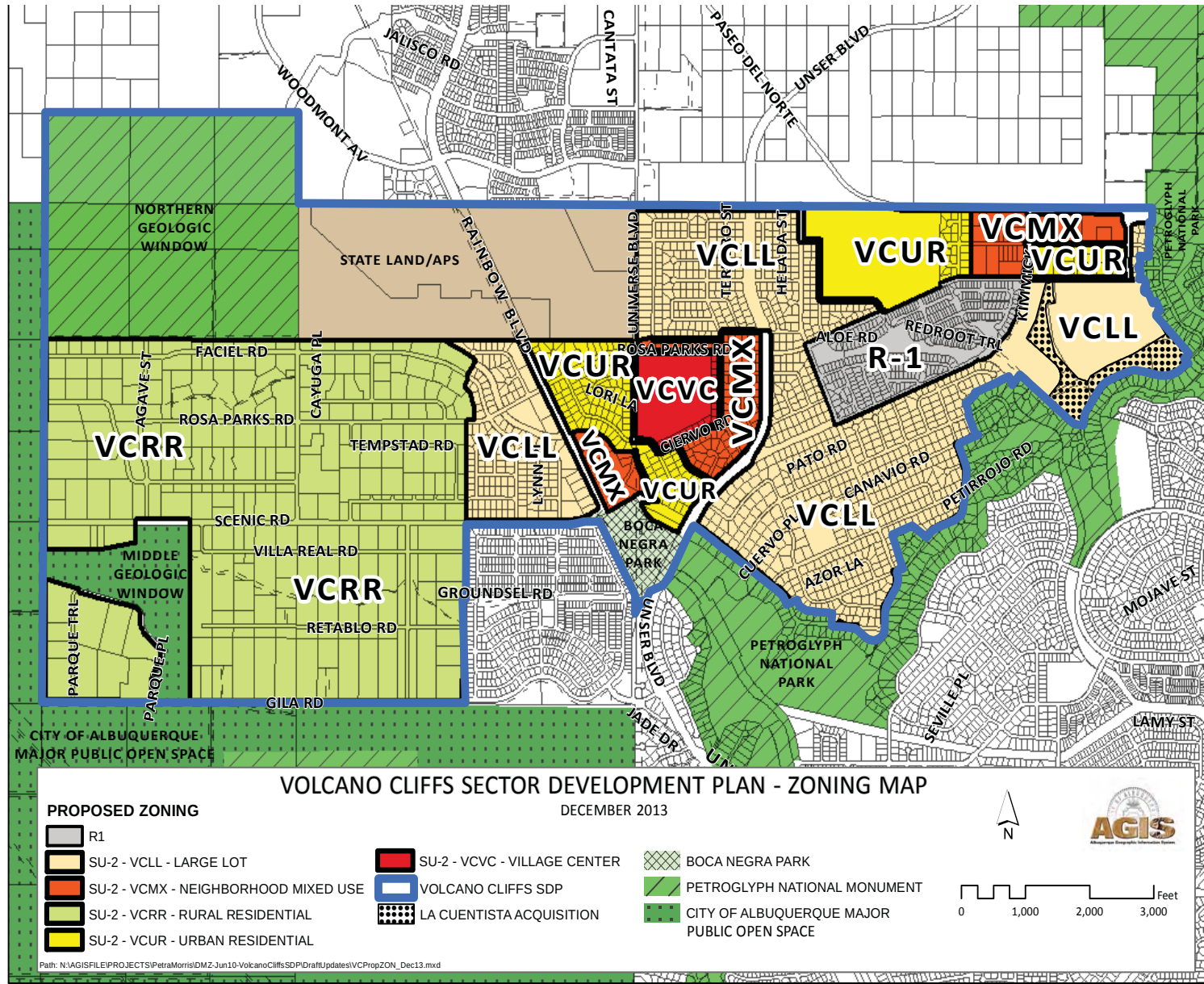


Exhibit 7: Zoning Established by the Volcano Cliffs Sector Development Plan



NOAA Atlas 14, Volume 1, Version 5
Location name: Albuquerque, New Mexico, US*
Latitude: 35.1773°, Longitude: -106.7134°
Elevation: 5352 ft*
 * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aeriels](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.159 (0.136–0.186)	0.206 (0.176–0.242)	0.278 (0.236–0.326)	0.335 (0.285–0.391)	0.412 (0.348–0.481)	0.473 (0.398–0.550)	0.537 (0.449–0.624)	0.606 (0.502–0.704)	0.699 (0.574–0.814)	0.774 (0.630–0.900)
10-min	0.242 (0.208–0.284)	0.314 (0.268–0.367)	0.423 (0.359–0.496)	0.510 (0.433–0.595)	0.627 (0.529–0.732)	0.719 (0.605–0.837)	0.818 (0.683–0.950)	0.922 (0.764–1.07)	1.06 (0.873–1.24)	1.18 (0.958–1.37)
15-min	0.300 (0.257–0.351)	0.389 (0.332–0.455)	0.524 (0.445–0.615)	0.632 (0.537–0.738)	0.778 (0.656–0.907)	0.892 (0.751–1.04)	1.01 (0.847–1.18)	1.14 (0.948–1.33)	1.32 (1.08–1.54)	1.46 (1.19–1.70)
30-min	0.404 (0.347–0.473)	0.524 (0.447–0.613)	0.706 (0.599–0.828)	0.852 (0.724–0.993)	1.05 (0.884–1.22)	1.20 (1.01–1.40)	1.37 (1.14–1.59)	1.54 (1.28–1.79)	1.78 (1.46–2.07)	1.97 (1.60–2.29)
60-min	0.500 (0.429–0.585)	0.648 (0.553–0.759)	0.874 (0.741–1.03)	1.05 (0.895–1.23)	1.30 (1.09–1.51)	1.49 (1.25–1.73)	1.69 (1.41–1.96)	1.91 (1.58–2.21)	2.20 (1.81–2.56)	2.43 (1.98–2.83)
2-hr	0.588 (0.506–0.685)	0.752 (0.645–0.877)	0.998 (0.853–1.16)	1.20 (1.02–1.38)	1.47 (1.25–1.70)	1.70 (1.43–1.95)	1.94 (1.62–2.22)	2.19 (1.81–2.51)	2.54 (2.09–2.91)	2.83 (2.30–3.25)
3-hr	0.629 (0.551–0.732)	0.801 (0.699–0.932)	1.05 (0.920–1.22)	1.26 (1.09–1.45)	1.54 (1.32–1.77)	1.76 (1.51–2.03)	2.00 (1.71–2.30)	2.26 (1.91–2.60)	2.62 (2.19–3.01)	2.92 (2.40–3.36)
6-hr	0.727 (0.638–0.834)	0.920 (0.812–1.06)	1.19 (1.05–1.37)	1.41 (1.23–1.61)	1.70 (1.48–1.94)	1.93 (1.68–2.20)	2.17 (1.87–2.47)	2.42 (2.08–2.75)	2.78 (2.35–3.16)	3.07 (2.58–3.50)
12-hr	0.812 (0.718–0.919)	1.03 (0.907–1.16)	1.31 (1.15–1.48)	1.53 (1.35–1.73)	1.82 (1.60–2.05)	2.06 (1.79–2.31)	2.30 (1.99–2.58)	2.55 (2.19–2.86)	2.88 (2.46–3.25)	3.16 (2.67–3.57)
24-hr	0.927 (0.818–1.06)	1.17 (1.03–1.32)	1.46 (1.29–1.66)	1.70 (1.50–1.92)	2.02 (1.77–2.28)	2.26 (1.98–2.56)	2.52 (2.20–2.85)	2.78 (2.42–3.13)	3.14 (2.70–3.53)	3.41 (2.92–3.84)
2-day	0.974 (0.868–1.09)	1.22 (1.09–1.37)	1.53 (1.37–1.72)	1.78 (1.58–1.99)	2.11 (1.87–2.35)	2.36 (2.09–2.64)	2.62 (2.31–2.93)	2.89 (2.53–3.23)	3.25 (2.83–3.64)	3.53 (3.06–3.96)
3-day	1.13 (1.02–1.25)	1.41 (1.28–1.56)	1.75 (1.58–1.93)	2.01 (1.82–2.22)	2.37 (2.13–2.61)	2.64 (2.37–2.92)	2.92 (2.61–3.22)	3.20 (2.85–3.53)	3.57 (3.17–3.95)	3.86 (3.41–4.27)
4-day	1.29 (1.18–1.41)	1.60 (1.46–1.75)	1.96 (1.79–2.15)	2.25 (2.05–2.45)	2.63 (2.40–2.87)	2.93 (2.66–3.19)	3.22 (2.92–3.51)	3.51 (3.17–3.83)	3.90 (3.51–4.26)	4.19 (3.76–4.59)
7-day	1.47 (1.35–1.61)	1.83 (1.68–1.99)	2.23 (2.04–2.42)	2.54 (2.33–2.76)	2.94 (2.69–3.19)	3.25 (2.97–3.52)	3.55 (3.24–3.85)	3.84 (3.50–4.17)	4.21 (3.83–4.58)	4.49 (4.07–4.89)
10-day	1.63 (1.50–1.78)	2.03 (1.86–2.20)	2.48 (2.28–2.69)	2.84 (2.61–3.07)	3.31 (3.03–3.58)	3.66 (3.35–3.96)	4.01 (3.66–4.34)	4.36 (3.97–4.72)	4.81 (4.36–5.21)	5.15 (4.65–5.58)
20-day	2.05 (1.88–2.23)	2.54 (2.33–2.77)	3.09 (2.84–3.36)	3.50 (3.21–3.80)	4.02 (3.68–4.36)	4.39 (4.02–4.77)	4.76 (4.35–5.16)	5.10 (4.66–5.53)	5.53 (5.04–6.00)	5.84 (5.31–6.34)
30-day	2.45 (2.25–2.65)	3.03 (2.79–3.28)	3.65 (3.36–3.95)	4.11 (3.77–4.43)	4.67 (4.29–5.04)	5.08 (4.65–5.47)	5.46 (5.00–5.88)	5.82 (5.32–6.27)	6.25 (5.70–6.73)	6.55 (5.97–7.05)
45-day	2.99 (2.76–3.24)	3.70 (3.42–4.00)	4.41 (4.07–4.76)	4.92 (4.53–5.30)	5.53 (5.10–5.95)	5.94 (5.48–6.40)	6.32 (5.83–6.80)	6.65 (6.13–7.15)	7.02 (6.48–7.55)	7.25 (6.70–7.79)
60-day	3.44 (3.17–3.72)	4.25 (3.92–4.60)	5.06 (4.68–5.47)	5.64 (5.22–6.09)	6.34 (5.86–6.84)	6.82 (6.30–7.35)	7.25 (6.71–7.82)	7.64 (7.06–8.24)	8.07 (7.47–8.71)	8.34 (7.73–9.00)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).
 Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.
 Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)

PF graphical

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the summary of Stillwater Elevations table in the Flood Insurance Study Report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures in this jurisdiction.

The **projection** used in the preparation of this map was New Mexico State Plane, Central Zone. The **horizontal datum** was NAD 83, GRS80 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services
NOAA, NGS12
National Geodetic Survey, SSMC-3, #9202
1315 East-West Highway
Silver Spring, Maryland 20910-3282
(301) 713-3242

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit their website at <http://www.ngs.noaa.gov>.

Base map information shown on this FIRM was provided in digital format by Bernalillo County produced at a scale of 1:12,000 from photography dated 1999 or later.

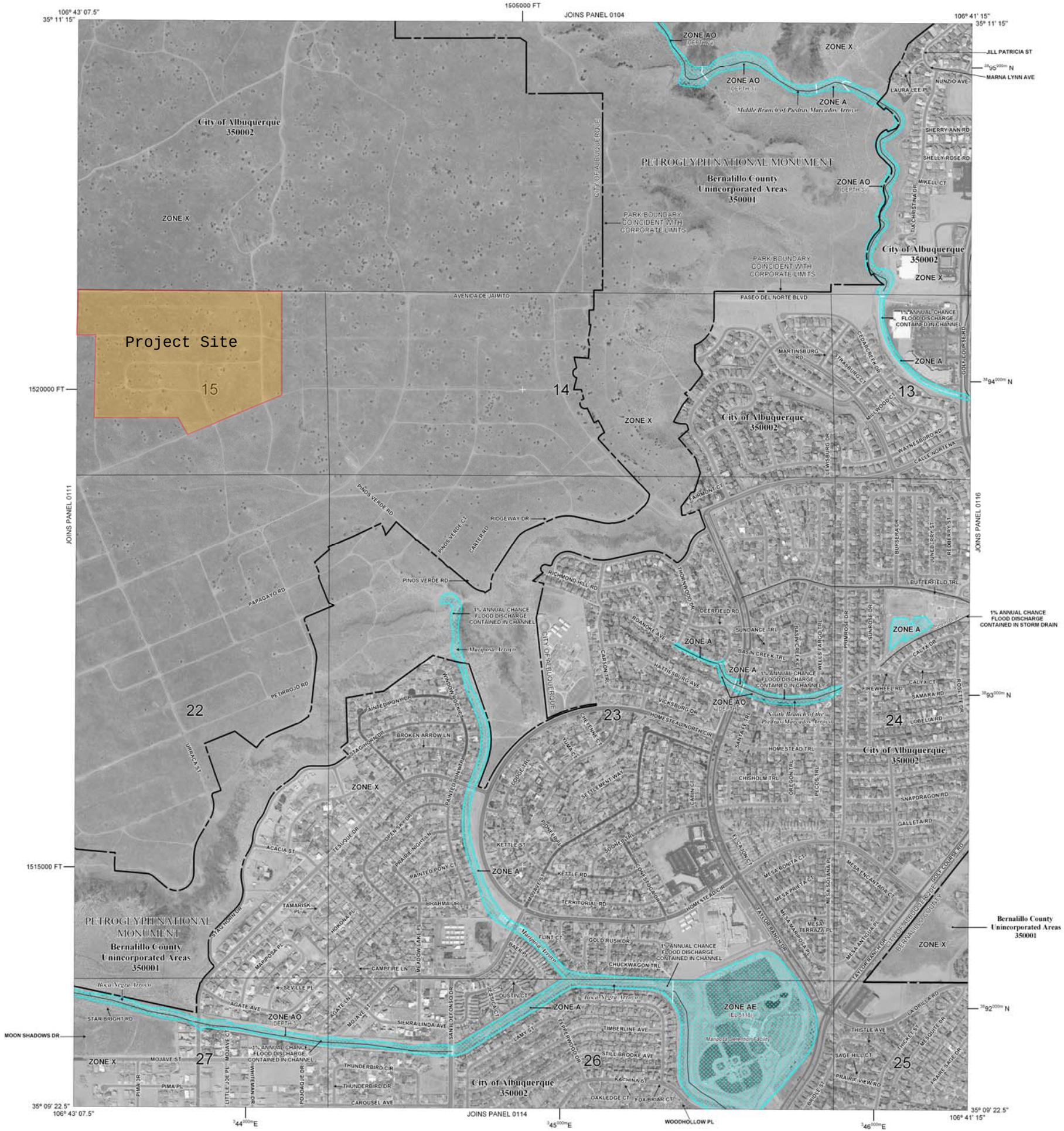
Based on updated topographic information, this map reflects more detailed and up-to-date **stream channel configurations and floodplain delineations** than those shown on the previous FIRM for this jurisdiction. As a result, the Flood Profiles and Floodway Data tables for the Flood Insurance Study report may reflect stream channel distances that differ from what is shown on the map. Also, the road to floodplain relationships for unrevised streams may differ from what is shown on previous maps.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the **FEMA Map Service Center** at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and their website at <http://www.msc.fema.gov>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/rlp>.



LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

- ZONE A** No Base Flood Elevations determined.
- ZONE AE** Base Flood Elevations determined.
- ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.
- ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- ZONE AR** Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- ZONE A99** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.
- ZONE VE** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE K Areas determined to be outside the 0.2% annual chance floodplain.

ZONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- 1% annual chance floodplain boundary
- 0.2% annual chance floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.
- Base Flood Elevation line and value: elevation in feet
- Base Flood Elevation value where uniform within zone; elevation in feet

*Referenced to the North American Vertical Datum of 1988

Cross section line

Transect line

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83), Western Hemisphere

1000-meter Universal Transverse Mercator grid values, zone 13

5000-foot grid ticks: New Mexico State Plane coordinate system, Central zone (FIPSZONE 3502), Transverse Mercator

Bench mark (see explanation in Notes to Users section of this FIRM panel)

MAP REPOSITORIES

Refer to Map Repositories list on Map Index.

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP PANEL

SEPTEMBER 20, 1996

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

April 2, 2002 - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to add roads and road names, to reflect updated topographic information, and to incorporate previously issued Letters of Map Revision.

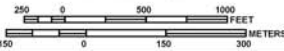
November 18, 2003 - to update corporate limits and to incorporate previously issued Letters of Map Revision.

September 26, 2005 - to update corporate limits, to change Special Flood Hazard Areas, to add roads and road names, to incorporate previously issued Letters of Map Revision, to reflect updated topographic information, to change Base Flood Elevations, to add Base Flood Elevations.

For community map revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500'



NFIP

NATIONAL FLOOD INSURANCE PROGRAM

PANEL 0112G

FIRM
FLOOD INSURANCE RATE MAP
BERNALILLO COUNTY,
NEW MEXICO
AND INCORPORATED AREAS

PANEL 112 OF 825

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS	COMMUNITY	NUMBER	PANEL	SUFFIX
	ALBUQUERQUE, CITY OF	350002	0112	G
	BERNALILLO COUNTY	350001	0112	G
	UNINCORPORATED AREAS	350001	0112	G

Notice to User: The **Map Number** shown below should be used when placing map orders. The **Community Number** shown above should be used on insurance applications for the subject community.



MAP NUMBER
35001C0112G

MAP REVISED
SEPTEMBER 26, 2008

Federal Emergency Management Agency

Appendix B

Hydrology Calculations

- AHYMO Models Summary and Input Files
 - o Ultimate Conditions
 - o Developed Conditions

Ultimate Conditions AHYMO Summary & Input Files

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1 NOTATION
S	1- COMPUTING RAINFALL	*****ORIGINAL RAINFALL *****								
	START RAINFALL TYPE= 2	TIME= .00 RAIN24= 2.520								
S	3- COMPUTE HYD FOR BASIN 301, (assume platted to 5 DU/ACRE, %D=50)									
	COMPUTE NM HYD 301.00 - 1 .06800				129.35	5.332	1.47033	1.500	2.972	PER IMP= 50.00
S	4- Route HYDROGRAPH 301 through POND 5 (0.30/0.52ac surface/bottom, 2.20AF									
S	Historical flow Basin 301 (100% A)= 74.42CFS use 75+/- thru 34" orifice plat									
	ROUTE RESERVOIR POND.301.1 1 2 .06800				60.70	5.332	1.47033	1.700	1.395	AC-FT= 1.415
S	5- Route POND 5 outflow (BASIN 301) through BASIN 302 via 36"X 1800'RCP									
S	(24'/1800'= 0.15 slp) Add to basin 302 at pond 6, (#8)									
	ROUTE MCUNGE 301.20 2 3 .06800				60.62	5.333	1.47036	1.700	1.393	CCODE = .2
S	7- COMPUTE HYD FOR BASIN 302 (assume replat to 4 DU/Ac, D=42%, use 45%)									
S	Historical flow (100% A)= 57.95CFS									
	COMPUTE NM HYD 302.00 - 1 .05800				107.92	4.330	1.39962	1.500	2.907	PER IMP= 45.00
S	8- ADD HYDROGRAPHS 301.2 (ROUTED THROUGH 302) AND 302 - INFLOW TO POND 6									
	ADD HYD 302.10 1& 3 2 .12600				151.66	9.662	1.43779	1.500	1.881	
S	9- ROUTE HYDROGRAPH 302.1 through POND 6 (0.2/0.4AC surf/bottom, 1.5AF st									
S	Historical flow- 100% A (Basin 301= 74.42)+(Basin 302= 57.95)= 132.37CF									
S	discharge through 48" RCP w/ 45" orifice plate									
	ROUTE RESERVOIR POND.302.2 2 1 .12600				110.72	9.662	1.43779	1.700	1.373	AC-FT= 1.087
S	10- Route outflow from POND 6 (BASIN 301 & 302) through									
S	48"x 2300'RCP (50/2300= 2.2% slp) through Basin 214 TO POND 8									
	ROUTE MCUNGE 302.30 1 2 .12600				110.64	9.662	1.43787	1.700	1.372	CCODE = .2
S	77- COMPUTE HYD FOR BASIN 214									
	COMPUTE NM HYD 214.00 - 1 .08600				159.90	6.420	1.39962	1.500	2.905	PER IMP= 45.00
S	78- ADD HYDROGRAPHS 302.3 AND 214									
	ADD HYD 214.10 2& 1 3 .21200				237.22	16.082	1.42235	1.500	1.748	
S	79- Route HYDROGRAPH 214.1 through POND 8 (1.7/2.2AC surf/btm, 11.3AF stor									
	ROUTE RESERVOIR POND.214.2 3 2 .21200				101.14	16.082	1.42235	2.100	.745	AC-FT= 5.585
S	12- COMPUTE HYD FOR BASIN 303 (assume replat to 4 DU/Ac, D=42%, use 45%)									
S	BASIN 303 Historical flow (100% A)= 75.29CFS									
	COMPUTE NM HYD 303.00 - 1 .06700				124.65	5.001	1.39962	1.500	2.907	PER IMP= 45.00
S	13- ROUTE HYDROGRAPH 303 THROUGH POND 9 (0.3/0.52AC surface/bottom, 2.11AF									
S	303 Hist. flow= 75.29CFS, discharge through 36" RCP w/ 34" orifice pla									
	ROUTE RESERVOIR POND.303.1 1 2 .06700				59.27	5.001	1.39962	1.700	1.382	AC-FT= 1.337
S	14- Route outflow from POND 9 (BASIN 303.1) through 36"x 1300'RCP									
	ROUTE MCUNGE 303.20 2 3 .06700				59.23	5.000	1.39935	1.750	1.381	CCODE = .1
S	83- ADD HYDROGRAPHS 303.2 AND 215									
	ADD HYD 215.10 1& 3 2 .13400				163.18	10.002	1.39948	1.500	1.903	
S	85- Route HYDROGRAPH 215.1 through POND 10 (1.0/0.7AC surf/btm, 4.65AF sto									
	ROUTE RESERVOIR POND.215.2 2 1 .13400				14.38	10.001	1.39934	2.500	.168	AC-FT= 6.991
S	16- Compute HYD for BASIN 304 (ex.platting 2.33+/- DU/Acre => 35%D, use 40									
S	BASIN 304 @ 100% A: Historical flow area= 0.05 sq mi, flow= 41.24cfs									
	COMPUTE NM HYD 304.00 - 1 .10800				196.23	7.657	1.32939	1.500	2.839	PER IMP= 40.00
S	17- Route HYDROGRAPH 304 through POND 7 (H=4.0', 0.40/0.25AC surf/bottom,									
S	cap.). 304 historical: 100% A;area= 0.05 sq mi; flow= 41.24cfs;									
S	discharge through 28" orifice plate into 30' RCP									
	ROUTE RESERVOIR POND.304.1 1 2 .10800				41.88	7.657	1.32938	1.900	.606	AC-FT= 3.712
S	24- COMPUTE HYD FOR BASIN P-203 (2.5 DU/acre, use D=45)									

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 2 NOTATION
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AHYMO.SUM

COMPUTE NM HYD	203.00	-	2	.00200	3.73	.149	1.39962	1.500	2.918 PER IMP=	45.00
COMPUTE NM HYD	204.00	-	1	.00800	14.90	.597	1.39962	1.500	2.910 PER IMP=	45.00
S 84- ADD HYDROGRAPHS 203 AND 204										
ADD HYD	204.20	1& 2	5	.01000	18.63	.746	1.39956	1.500	2.911	
S 33- Route HYDROGRAPH 204.2 through BASIN 208 IN 24'X570 LF PIPE										
ROUTE MCUNGE	204.30	5	10	.01000	18.58	.747	1.39981	1.500	2.903 CCODE =	.2
S 35- COMPUTE HYD FOR BASIN P-205 (assume 4 DU/Acre=> 42%D, use 45%D)										
COMPUTE NM HYD	205.00	-	1	.01400	26.03	1.045	1.39962	1.500	2.905 PER IMP=	45.00
S 36- ROUTE HYDROGRAPH 205 THROUGH PIPE TO CONFLUENCE W/ BASIN 208										
ROUTE MCUNGE	205.10	1	2	.01400	25.73	1.045	1.39991	1.500	2.872 CCODE =	.2
COMPUTE NM HYD	208.00	-	1	.01300	19.30	.661	.95381	1.500	2.320 PER IMP=	20.00
S 47- ADD HYDROGRAPHS 205.1 and 208										
ADD HYD	208.10	1& 2	3	.02700	45.04	1.707	1.18508	1.500	2.606	
S 48- ADD HYDROGRAPHS 204.3 AND 208.1										
ADD HYD	208.20	3&10	1	.03700	63.62	2.453	1.24309	1.500	2.686	
*S*51- ROUTE ADDED FLOWS AT HYDROGRAPH 208.2 through PIPE TO POND 4										
ROUTE MCUNGE	208.30	1	5	.03700	62.41	2.453	1.24329	1.500	2.635 CCODE =	.2
S 38- COMPUTE HYD FOR BASIN P-206 (assume 4 DU/Acre=> 42%D, use 45%D)										
COMPUTE NM HYD	206.00	-	1	.00700	13.02	.523	1.39962	1.500	2.906 PER IMP=	45.00
S 59- COMPUTE TP FOR BASIN P-210 (let tp=0.133= Min.)										
S 60- COMPUTE HYD FOR BASIN P-210 (3.0 DU/acre=> 35%D, use 40%D)										
COMPUTE NM HYD	210.00	-	2	.00400	7.29	.284	1.32939	1.500	2.847 PER IMP=	40.00
S - ADD HYDROGRAPHS 206 AND 210										
ADD HYD	210.10	1& 2	3	.01100	20.31	.806	1.37403	1.500	2.885	
S 63- COMPUTE HYD FOR BASIN P-211 (3.7 DU/acre=> 40%D, use 45%D)										
COMPUTE NM HYD	211.00	-	1	.01000	18.62	.746	1.39962	1.500	2.909 PER IMP=	45.00
S 64- ADD HYDROGRAPHS 210.1 AND 211										
ADD HYD	211.10	1& 3	2	.02100	38.93	1.553	1.38620	1.500	2.896	
S 42- COMPUTE HYD FOR BASIN P-207 (actual 3.7DU/acre, assume 4 DU/Acre=>)										
COMPUTE NM HYD	207.00	-	1	.00400	7.45	.299	1.39962	1.500	2.909 PER IMP=	45.00
S - ADD HYDROGRAPHS 211.1 AND 207										
ADD HYD	207.10	1& 2	3	.02500	46.38	1.851	1.38834	1.500	2.898	
S 53- Compute HYD for BASIN 209 (3.86du/acre=> 41%D, use 45%D)										
COMPUTE NM HYD	209.00	-	1	.00600	11.18	.448	1.39962	1.500	2.911 PER IMP=	45.00
S - ADD HYDROGRAPHS 207.1 AND 209										
ADD HYD	209.10	1& 3	2	.03100	57.55	2.299	1.39051	1.500	2.901	
S 66- COMPUTE TP FOR BASIN P-212 (Let TP=0.133= Min.)										
S 67- Computing HYD for BASIN P-212 (2.5 DU/acre=> 30%D, use 35%D)										
COMPUTE NM HYD	212.00	-	1	.00500	8.90	.336	1.25947	1.500	2.782 PER IMP=	35.00
S 68- ADD HYDROGRAPHS 209.1 AND 212										
ADD HYD	212.10	2& 1	3	.03600	66.45	2.635	1.37230	1.500	2.884	
S 69 ROUTE HYDROGRAPH 212.1 down Kimmick in 48"x 175' RCP to POND 4										
ROUTE MCUNGE	212.20	3	2	.03600	66.45	2.635	1.37230	1.500	2.884 CCODE =	.0
S 70- Add HYDROGRAPHS 212.2 TO 208.3 (At POND 4)										
ADD HYD	212.30	2& 5	6	.07300	128.86	5.088	1.30690	1.500	2.758	
*S										
*S										
*S										
S 20- COMPUTE HYD FOR BASIN P-201 (8 DU/Acre)										
COMPUTE NM HYD	201.00	-	1	.05780	129.32	5.723	1.85664	1.500	3.496 PER IMP=	71.00
COMPUTE NM HYD	202.10	-	2	.01320	27.29	1.096	1.55682	1.500	3.230 PER IMP=	49.00
S ADD BASINSS 201 TO 202.1										

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 3 NOTATION
ADD HYD	202.12	1& 2	12	.07100	156.61	6.819	1.80089	1.500	3.446	
COMPUTE NM HYD	202.20	-	2	.00260	5.83	.257	1.85664	1.500	3.504 PER IMP=	71.00

				AHYMO.SUM							
COMPUTE NM HYD	202.30	-	3	.01720	38.49	1.703	1.85664	1.500	3.497	PER IMP=	71.00
S	ADD BASINSS	202.1	TO 202.2								
ADD HYD	202.32	3& 2	13	.01980	44.32	1.961	1.85661	1.500	3.498		
S	ADD BASINSS	201,	202.1, 202.2 TO 202.3								
ADD HYD	202.14	12&13	13	.09080	200.93	8.780	1.81304	1.500	3.458		
S	29- Route HYDROGRAPH	202.14	Through POND 1								
S	discharge 15 cfs through 18" PIPE into Rosa Parks System										
ROUTE RESERVOIR	POND.203.1	13	3	.09080	15.47	7.248	1.49664	2.200	.266	AC-FT=	5.970
S	56B- COMPUTE HYD FOR BASIN 213 (3.86du/acre=> 41%D, use 45%D)										
COMPUTE NM HYD	213.00	-	1	.06300	117.22	4.703	1.39962	1.500	2.907	PER IMP=	45.00
S	56C- Add HYDROGRAPH	202.2	(outflow from POND 2) and 213								
ADD HYD	213.10	1& 3	2	.15380	122.05	11.950	1.45690	1.500	1.240		
S	56D- Add HYDROGRAPHS	212.3	and 213.1 (INFLOW TO POND 4)								
ADD HYD	213.20	2& 6	1	.22680	250.91	17.039	1.40862	1.500	1.729		
S	57- Route BASIN	213.1	through POND 4								
ROUTE RESERVOIR	POND.213.3	1	2	.22680	84.31	17.038	1.40853	1.800	.581	AC-FT=	3.593
FINISH											

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P100_24 ULTIMATE.dat
*** LA CUMENTISTA SUBDIVISION ***
*** FULLY DEVELOPED CONDITIONS RUNOFF MODEL - REVISED JANUARY 2007 ***
*** DESIGN STORM IS THE 100 YEAR - 24 HOUR STORM ***
*** COA DPM TYPE 2, 24 HOUR STORM WITH A PEAK INTENSITY AT 1.4 HOURS ***
*** AHYMO MODEL FROM DRANAGE REPORT FOR LA CUMENTISTA SUBDIVISION - UNIT II ***
*** DATED JANUARY 2007 PREPARED BY WCI, A SUPPLEMENT TO THE DRAINAGE REPORT ***
*** FOR LA CUMENTISTA SUBDIVISION PREPARED BY WCI DATED NOV. 2003 ***
*** ORIGINAL MODEL INCLUDED 4 DU/AC LOTS ***
*** ULTIMATE CONDITIONS MODEL UPDATED DECEMBER 2016 FOR TRACT B ***
*** THIS MODEL USES 8 DU/AC FOR TRACT B ***
*** RAINFALL DATA UPDATED PER NOAA ATLAS 14 WEBSITE ***
*****
* * * * *
*S* 1- COMPUTING RAINFALL ***** ORIGINAL RAINFALL *****
*RAINFALL TYPE = 2
*
RAIN QUARTER = 0.00 INCHES
*
RAIN ONE = 1.87
RAIN SIX = 2.20
RAIN DAY = 2.66
DT = 0.05 HOURS
*****
START TIME = 0
*****
RAINFALL TYPE = 2
RAIN QUARTER = 0.00 INCHES
RAIN ONE = 1.69
RAIN SIX = 2.17
RAIN DAY = 2.52
DT = 0.05 HOURS
* * * * *
*S* 3- COMPUTE HYD FOR BASIN 301, (assume platted to 5 DU/ACRE, %D=50)
COMPUTE NM HYD ID=1 HYDNO=301 DA=0.068 SQ MI
PERCENT A=10 B=15 C=25 D=50
TP=0.133 HOURS MASSRAIN=-1
PRINT HYD ID=1 CODE=5
*****
*S* 4- Route HYDROGRAPH 301 through POND 5 (0.30/0.52ac surface/bottom, 2.20AF stor req'd)
*S* Historical flow Basin 301 (100% A)= 74.42CFS use 75+/- thru 34" orifice plate
ROUTE RESERVOIR ID=2 HYD=POND.301.1 INFLOWID=1 CODE=5
OUTFLOW(CFS) STORAGE(AC-FT) ELEV(FT)
0 0 0
21.82 0.154 0.5
30.86 0.316 1
37.80 0.486 1.5
43.65 0.665 2
48.80 0.853 2.5
53.46 1.049 3
57.74 1.255 3.5
61.73 1.470 4
65.47 1.694 4.5
69.02 1.928 5
72.38 2.172 5.5
75.60 2.427 6
PRINT HYD ID=2 CODE=1
*****
*S* 5- Route POND 5 outflow (BASIN 301) through BASIN 302 via 36"X 1800' RCP
*S* (24'/1800'= 0.15 slp) Add to basin 302 at pond 6, (#8)
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=-1 SLP=0.015
DIAM=3.0 N=0.013
ROUTE MCUNGE ID=3 HYD NO= 301.2 INFLOW ID=2
DT=0.0 L=1400 FT NS=0 SLOPE=0.015
PRINT HYD ID=3 CODE=5

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P100_24 ULTIMATE.dat

S 7- COMPUTE HYD FOR BASIN 302 (assume replat to 4 DU/Ac, D=42%, use 45%)
 S Historical flow (100% A)= 57.95CFS
 COMPUTE NM HYD ID=1 HYDNO=302 DA=0.058 SQ MI
 PERCENT A=10 B=15 C=30 D=45
 TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=1 CODE=5

S 8- ADD HYDROGRAPHS 301.2 (ROUTED THROUGH 302) AND 302 - INFLOW TO POND 6

ADD HYD ID=2 HYD=302.1 ID=1 ID=3
 PRINT HYD ID=2 CODE=1

S 9- ROUTE HYDROGRAPH 302.1 through POND 6 (0.2/0.4AC surf/bottom, 1.5AF stor cap)
 S Historical flow- 100% A (Basin 301= 74.42)+(Basin 302= 57.95)= 132.37CFS
 S discharge through 48" RCP w/ 45" orifice plate

ROUTE RESERVOIR	ID=1 HYD=POND.302.2 INFLOWID=2 CODE=5	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)
		0	0	0
		38.23	0.103	0.5
		54.07	0.213	1.0
		66.22	0.330	1.5
		76.46	0.454	2.0
		85.49	0.585	2.5
		93.65	0.723	3.0
		101.15	0.869	3.5
		108.13	1.023	4.0
		114.69	1.186	4.5
		120.90	1.356	5.0
		126.80	1.535	5.5
		132.43	1.723	6.0
		132.43	1.919	6.5
		132.43	2.125	7.0

PRINT HYD ID=1 CODE=1

S 10- Route outflow from POND 6 (BASIN 301 & 302) through
 S 48"x 2300'RCP (50/2300= 2.2% slp) through Basin 214 TO POND 8

COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=-1 SLP=0.022
 DIAM=4.0 N=0.013

ROUTE MCUNGE ID=2 HYD NO= 302.3 INFLOW ID=1
 DT=0.0 L=2300 FT NS=0 SLOPE=0.022

PRINT HYD ID=2 CODE=5

S 77- COMPUTE HYD FOR BASIN 214
 COMPUTE NM HYD ID=1 HYDNO=214 DA=0.086 SQ MI
 PERCENT A=10 B=15 C=30 D=45
 TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=1 CODE=5

S 78- ADD HYDROGRAPHS 302.3 AND 214

ADD HYD ID=3 HYD=214.1 ID=2 ID=1
 PRINT HYD ID=3 CODE=1
 PUNCH HYD ID=3

S 79- Route HYDROGRAPH 214.1 through POND 8 (1.7/2.2AC surf/btm, 11.3AF stor.cap.)
 ROUTE RESERVOIR ID=2 HYD=POND.214.2 INFLOWID=3 CODE=5

ROUTE RESERVOIR	ID=2 HYD=POND.214.2 INFLOWID=3 CODE=5	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)
		0	0	0
		40.82	0.859	0.5
		57.73	1.738	1
		70.71	2.635	1.5
		81.64	3.552	2
		91.28	4.489	2.5
		99.99	5.445	3
		108.00	6.421	3.5
		115.46	7.417	4
		122.47	8.434	4.5
		129.09	9.472	5
		135.39	10.530	5.5

P100_24 ULTIMATE.dat
141.41 11.609 6
141.41 12.710 6.5
141.41 13.831 7

PRINT HYD ID=2 CODE=1

*** FLOW TO MARIPOSA CHANNEL ***

S 12- COMPUTE HYD FOR BASIN 303 (assume replat to 4 DU/Ac, D=42%, use 45%)
S BASIN 303 Historical flow (100% A)= 75.29CFS
COMPUTE NM HYD ID=1 HYDNO=303 DA=0.067 SQ MI
PERCENT A=10 B=15 C=30 D=45
TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=1 CODE=5

S 13- ROUTE HYDROGRAPH 303 THROUGH POND 9 (0.3/0.52AC surface/bottom, 2.11AF stor. cap.)
S 303 Hist. flow= 75.29CFS, discharge through 36" RCP w/ 34" orifice plate
ROUTE RESERVOIR ID=2 HYD=POND.303.1 INFLOWID=1 CODE=5

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)
0	0	0
21.82	0.154	0.5
30.86	0.316	1
37.80	0.486	1.5
43.65	0.665	2
48.80	0.853	2.5
53.46	1.049	3
57.74	1.255	3.5
61.73	1.470	4
65.47	1.694	4.5
69.02	1.928	5
72.38	2.172	5.5
75.60	2.427	6
75.60	2.691	6.5
75.60	2.966	7

PRINT HYD ID=2 CODE=1

S 14- Route outflow from POND 9 (BASIN 303.1) through 36"x 1300'RCP
*** (50/1300=3.9% slp) through BASIN 215 to POND 10

COMPUTE RATING CURVE CID=1 VS NO=1 NO SEG=-1 SLP=0.03
DIAM=3.0 N=0.013

ROUTE MCUNGE ID=3 HYD NO= 303.2 INFLOW ID=2
DT=0.0 L=1300 FT NS=0 SLOPE=0.039

PRINT HYD ID=3 CODE=5

S 83- ADD HYDROGRAPHS 303.2 AND 215

ADD HYD ID=2 HYD=215.1 ID=1 ID=3
PRINT HYD ID=2 CODE=1

S 85- Route HYDROGRAPH 215.1 through POND 10 (1.0/0.7AC surf/btm, 4.65AF stor.cap.)
ROUTE RESERVOIR ID=1 HYD=POND.215.2 INFLOWID=2 CODE=5

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)
0	0	0
4.39	0.5	0.5
6.21	1.3	1
8.78	2.6	2
10.75	3.9	3
12.42	5.2	4
13.88	6.5	5
15.21	7.8	6
15.21	9.1	7

PRINT HYD ID=1 CODE=1

*** FLOW TO PIEDRAS MARCADAS ***

S 16- Compute HYD for BASIN 304 (ex.platting 2.33+/- DU/Acre => 35%D, use 40%)
S BASIN 304 @ 100% A: Historical flow area= 0.05 sq mi, flow= 41.24cfs

```

                                P100_24 ULTIMATE.dat
COMPUTE NM HYD          ID=1      HYDNO=304  DA=0.108  SQ MI
                                PERCENT A=10 B=15 C=35 D=40
                                TP=0.133 HOURS   MASSRAIN=-1

PRINT HYD                ID=1      CODE=5
*****
*S* 17- Route HYDROGRAPH 304 through POND 7 (H=4.0', 0.40/0.25AC surf/bottom, 1.14AF stor.
*S* cap.). 304 historical: 100% A;area= 0.05 sq mi; flow= 41.24cfs;
*S* discharge through 28" orifice plate into 30' RCP
ROUTE RESERVOIR          ID=2 HYD=POND.304.1 INFLOWID=1 CODE=5
                                OUTFLOW(CFS)   STORAGE(AC-FT)   ELEV(FT)

                                0              0              0
                                14.80           0.381           0.5
                                20.93           0.775           1
                                25.64           1.182           1.5
                                29.60           1.602           2
                                33.10           2.035           2.5
                                36.26           2.482           3
                                39.16           2.942           3.5
                                41.86           3.416           4
                                41.90           3.904           4.5
                                42.00           4.407           5

PRINT HYD                ID=2      CODE=1
***** FLOW TO MARIPOSA BASIN *****
*****

*S* 24- COMPUTE HYD FOR BASIN P-203 (2.5 DU/acre, use D=45)
COMPUTE NM HYD          ID=2      HYDNO=203  DA=0.002  SQ MI
                                PERCENT A=10 B=15 C=30 D=45
                                TP=0.133 HOURS   MASSRAIN=-1

PRINT HYD                ID=2      CODE=5
*****

*S* 32- COMPUTE HYD FOR BASIN P-204 (actual 3.3DU/acre, assume 4 DU/Acre=>
42%D, use 45%D)
COMPUTE NM HYD          ID=1      HYDNO=204  DA=0.008  SQ MI
                                PERCENT A=10 B=15 C=30 D=45
                                TP=0.133 HOURS   MASSRAIN=-1

PRINT HYD                ID=1      CODE=5
*****
*S* 84- ADD HYDROGRAPHS 203 AND 204

ADD HYD                ID=5      HYD=204.2      ID=1      ID=2
PRINT HYD                ID=5      CODE=1

*****

*S* 33- Route HYDROGRAPH 204.2 through BASIN 208 IN 24'X570 LF PIPE
***
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=-1 SLP=0.04
                        DIAM=2.0 N=0.013

ROUTE MCUNGE            ID=10  HYD NO= 204.3  INFLOW ID=5
                        DT=0.0 L=570 FT NS=0 SLOPE=0.04
PRINT HYD                ID=10  CODE=5
*****

*****

*S* 35- COMPUTE HYD FOR BASIN P-205 (assume 4 DU/Acre=> 42%D, use 45%D)
COMPUTE NM HYD          ID=1      HYDNO=205  DA=0.014  SQ MI
                                PERCENT A=10 B=15 C=30 D=45
                                TP=0.0 HOURS   MASSRAIN=-1

PRINT HYD                ID=1      CODE=5
*****
*S* 36- ROUTE HYDROGRAPH 205 THROUGH PIPE TO CONFLUENCE W/ BASIN 208
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=-1 SLP=0.02
                        DIAM=4.0 N=0.013

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                                P100_24 ULTIMATE.dat
ROUTE MCUNGE                ID=2  HYD NO= 205.1  INFLOW ID=1
                             DT=0.0 L=800 FT NS=0 SLOPE=0.02
PRINT HYD                   ID=2    CODE=5
* * * * *
* * * * *

*** 46- COMPUTE HYD FOR BASIN P-208 (actual 0.4DU/acre=> 10%D, use 20%D)
COMPUTE NM HYD              ID=1      HYDNO=208  DA=0.013 SQ MI
                             PERCENT A=10 B=50 C=20 D=20
                             TP=0.133 HOURS   MASSRAIN=-1

PRINT HYD                   ID=1      CODE=5
* * * * *
*S* 47- ADD HYDROGRAPHS 205.1 and 208

ADD HYD                     ID=3      HYD=208.1    ID=1    ID=2
PRINT HYD                   ID=3      CODE=1
* * * * *
*S* 48- ADD HYDROGRAPHS 204.3 AND 208.1

ADD HYD                     ID=1      HYD=208.2    ID=3    ID=10
PRINT HYD                   ID=1      CODE=1
* * * * *

*S*51- ROUTE ADDED FLOWS AT HYDROGRAPH 208.2 through PIPE TO POND 4
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=-1 SLP=0.025
                        DIAM=4.0 N=0.013

ROUTE MCUNGE                ID=5  HYD NO= 208.3  INFLOW ID=1
                             DT=0.0 L=814 FT NS=0 SLOPE=0.025
PRINT HYD                   ID=5    CODE=5
* * * * *
* * * * *

*S* 38- COMPUTE HYD FOR BASIN P-206 (assume 4 DU/Acre=> 42%D, use 45%D)
COMPUTE NM HYD              ID=1      HYDNO=206  DA=0.007 SQ MI
                             PERCENT A=10 B=15 C=30 D=45
                             TP=0.0 HOURS   MASSRAIN=-1

PRINT HYD                   ID=1      CODE=5
* * * * *
*S* 59- COMPUTE TP FOR BASIN P-210 (let tp=0.133= Min.)
* * * * *

*S* 60- COMPUTE HYD FOR BASIN P-210 (3.0 DU/acre=> 35%D, use 40%D)
COMPUTE NM HYD              ID=2      HYDNO=210  DA=0.004 SQ MI
                             PERCENT A=10 B=15 C=35 D=40
                             TP=0.133 HOURS   MASSRAIN=-1

PRINT HYD                   ID=2      CODE=5
* * * * *
*S* - ADD HYDROGRAPHS 206 AND 210

ADD HYD                     ID=3      HYD=210.1    ID=1    ID=2
PRINT HYD                   ID=3      CODE=1
* * * * *
* * * * *

*S* 63- COMPUTE HYD FOR BASIN P-211 (3.7 DU/acre=> 40%D, use 45%D)
COMPUTE NM HYD              ID=1      HYDNO=211  DA=0.010 SQ MI
                             PERCENT A=10 B=15 C=30 D=45
                             TP=0.133 HOURS   MASSRAIN=-1

PRINT HYD                   ID=1      CODE=5
* * * * *
*S* 64- ADD HYDROGRAPHS 210.1 AND 211

ADD HYD                     ID=2      HYD=211.1    ID=1    ID=3
PRINT HYD                   ID=2      CODE=1
* * * * *
* * * * *

```

P100_24 ULTIMATE.dat

```

*S* 42- COMPUTE HYD FOR BASIN P-207 (actual 3.7DU/acre, assume 4 DU/Acre=>
* 42%D, use 45%D)
COMPUTE NM HYD ID=1 HYDNO=207 DA=0.004 SQ MI
PERCENT A=10 B=15 C=30 D=45
TP=0.0 HOURS MASSRAIN=-1

PRINT HYD ID=1 CODE=5
*****
*S* - ADD HYDROGRAPHS 211.1 AND 207

ADD HYD ID=3 HYD=207.1 ID=1 ID=2
PRINT HYD ID=3 CODE=1
*****
*****

*S* 53- Compute HYD for BASIN 209 (3.86du/acre=> 41%D, use 45%D)
COMPUTE NM HYD ID=1 HYDNO=209 DA=0.006 SQ MI
PERCENT A=10 B=15 C=30 D=45
TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=1 CODE=5
*****
*S* - ADD HYDROGRAPHS 207.1 AND 209

ADD HYD ID=2 HYD=209.1 ID=1 ID=3
PRINT HYD ID=2 CODE=1
*****
*****

*S* 66- COMPUTE TP FOR BASIN P-212 (Let TP=0.133= Min.)
*****
*****

*S* 67- Computing HYD for BASIN P-212 (2.5 DU/acre=> 30%D, use 35%D)
COMPUTE NM HYD ID=1 HYDNO=212 DA=0.005 SQ MI
PERCENT A=10 B=15 C=40 D=35
TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=1 CODE=5
*****
*S* 68- ADD HYDROGRAPHS 209.1 AND 212

ADD HYD ID=3 HYD=212.1 ID=2 ID=1
PRINT HYD ID=3 CODE=1
*****
*****

*S* 69 ROUTE HYDROGRAPH 212.1 down Kimmick in 48"x 175' RCP to POND 4
COMPUTE RATING CURVE CID=1 VS NO=1 NO SEGS=-1 SLP=0.001
DIAM=4.0 N=0.013

ROUTE MCUNGE ID=2 HYD NO= 212.2 INFLOW ID=3
DT=0.0 L=175 FT NS=0 SLOPE=0.001
PRINT HYD ID=2 CODE=5
*****
*S* 70- Add HYDROGRAPHS 212.2 TO 208.3 (At POND 4)

ADD HYD ID=6 HYD=212.3 ID=2 ID=5
PRINT HYD ID=6 CODE=1
*****
*****
**S MODEL UPDATED FOR TRACT B USING 8 DU/AC *****
*S
*S
*S
*****

*S* 20- COMPUTE HYD FOR BASIN P-201 (8 DU/Acre)
COMPUTE NM HYD ID=1 HYDNO=201 DA=0.0578 SQ MI
PERCENT A=0 B=4 C=25 D=71
TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=1 CODE=5
*****
*****

*** COMPUTE HYD FOR BASIN P-202.1 (8 DU/Acre, INCLUDES POND AND OPEN SPACE)
COMPUTE NM HYD ID=2 HYDNO=202.1 DA=0.0132 SQ MI
PERCENT A=0 B=3 C=48 D=49

```

P100_24 ULTIMATE.dat
TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=2 CODE=5

S ADD BASINSS 201 TO 202.1

ADD HYD ID=12 HYD=202.12 ID=1 ID=2
PRINT HYD ID=12 CODE=1

*** COMPUTE HYD FOR BASIN P-202.2 (8 DU/Acre)
COMPUTE NM HYD ID=2 HYDNO=202.2 DA=0.0026 SQ MI
PERCENT A=0 B=4 C=25 D=71
TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=2 CODE=5

*** COMPUTE HYD FOR BASIN P-202.3 (8 DU/Acre)
COMPUTE NM HYD ID=3 HYDNO=202.3 DA=0.0172 SQ MI
PERCENT A=0 B=4 C=25 D=71
TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=3 CODE=5

S ADD BASINSS 202.1 TO 202.2

ADD HYD ID=13 HYD=202.32 ID=3 ID=2
PRINT HYD ID=13 CODE=1

S ADD BASINSS 201, 202.1, 202.2 TO 202.3

ADD HYD ID=13 HYD=202.14 ID=12 ID=13
PRINT HYD ID=13 CODE=1

S 29- Route HYDROGRAPH 202.14 Through POND 1
S discharge 15 cfs through 18" PIPE into Rosa Parks System
ROUTE RESERVOIR ID=3 HYD=POND.203.1 INFLOWID=13 CODE=5

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)
0.0	0.0	5336
0.01	0.499	5337
0.1	1.548	5338
6.23	2.669	5339
10.8	3.868	5340
13.9	5.147	5341
16.5	6.508	5342
18.7	7.951	5343
20.6	9.478	5344

PRINT HYD ID=3 CODE=5

S 56B- COMPUTE HYD FOR BASIN 213 (3.86du/acre=> 41%D, use 45%D)
COMPUTE NM HYD ID=1 HYDNO=213 DA=0.063 SQ MI
PERCENT A=10 B=15 C=30 D=45
TP=0.133 HOURS MASSRAIN=-1

PRINT HYD ID=1 CODE=5

S 56C- Add HYDROGRAPH 202.2 (outflow from POND 2) and 213

ADD HYD ID=2 HYD=213.1 ID=1 ID=3
PRINT HYD ID=2 CODE=1

S 56D- Add HYDROGRAPHS 212.3 and 213.1 (INFLOW TO POND 4)
ADD HYD ID=1 HYD=213.2 ID=2 ID=6

PRINT HYD ID=1 CODE=1

```

                                P100_24 ULTIMATE.dat
*S* 57- Route BASIN 213.1 through POND 4
ROUTE RESERVOIR                ID=2 HYD=POND.213.3 INFLOWID=1 CODE=5
                                OUTFLOW(CFS)    STORAGE(AC-FT)    ELEV(FT)
                                0.0              0.0              5298
                                71.8              0.82             5299
                                76.5              1.73             5300
                                81.0              2.72             5301
                                85.1              3.80             5302
                                89.1              4.97             5303
                                93.0              6.23             5304
                                96.7              7.58             5305
                                100.2             9.03             5306

```

```

PRINT HYD                      ID=2    CODE=1
* * * * *
* * * * *
FINISH

```


Developed Conditions AHYMO Summary & Input Files

AHYMO PROGRAM SUMMARY TABLE (AHYMO_97) -
INPUT FILE = C:\LC\P100_2~2.DAT

AHYMO.SUM

- VERSION: 1997.02c

RUN DATE (MON/DAY/YR) =12/02/2016
USER NO.= AHYMO-C-9803c01UNMLIB-AH

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1 NOTATION
START										TIME= .00
RAINFALL TYPE= 2										RAIN24= 2.520
COMPUTE NM HYD	202.10	-	1	.03390	27.24	.765	.42296	1.500	1.256	PER IMP= .00
COMPUTE NM HYD	202.20	-	2	.00510	4.10	.115	.42296	1.500	1.257	PER IMP= .00
COMPUTE NM HYD	202.30	-	3	.01720	38.49	1.703	1.85664	1.500	3.497	PER IMP= 71.00
S	ADD HYDROGRAPHS	202.3	and 202.2							
ADD HYD	202.21	3& 2	12	.02230	42.59	1.818	1.52875	1.500	2.985	
*S	ADD OFFSITE BASINS OS1 & OS8 FROM ADDENDUM FOR LA CUENTISTA SUBD UNIT II									
*S	SUBTRACT DEVELOPED BASIN 202.3 FROM OS8 IN ORIGINAL REPORT (12.59 AC)									
*S										
COMPUTE NM HYD	1.00	-	4	.02300	17.16	.519	.42296	1.500	1.166	PER IMP= .00
*S***	ROUTE BASINS OS1 THRU BASIN OS8									
ROUTE MCUNGE	OS8	4	5	.02300	15.95	.505	.41152	2.450	1.084	CCODE = .1
COMPUTE NM HYD	108.00	-	8	.09300	45.95	2.472	.49835	1.650	.772	PER IMP= 4.00
*S*ADD	BASIN OS1 AND OS8									
ADD HYD	OS8.1	5& 8	58	.11600	45.95	2.977	.48113	1.650	.619	
*S	ADD ALL THE BASINS DRAINING INTO POND 1									
S	ADD BASINS OS1, OS8.1, 202.2 AND 202.3									
ADD HYD	202.40	12&58	2	.13830	77.77	4.795	.65005	1.550	.879	
S	ADD ALL BASINS INTO THE POND									
ADD HYD	202.50	2& 1	3	.17220	103.41	5.559	.60534	1.550	.938	
S	Route HYDROGRAPH 202.14 Through POND 1									
S	discharge 15 cfs through 18" PIPE into Rosa Parks System									
ROUTE RESERVOIR	POND.202.6	3	31	.17220	15.61	4.558	.49629	2.600	.142	AC-FT= 3.418
FINISH										

P100_24 TRACT B Int.dat

```

*** LA CUMENTISTA SUBDIVISION ***
*** FULLY DEVELOPED CONDITIONS RUNOFF MODEL - REVISED JANUARY 2007 ***
*** DESIGN STORM IS THE 100 YEAR - 24 HOUR STORM ***
*** COA DPM TYPE 2, 24 HOUR STORM WITH A PEAK INTENSITY AT 1.4 HOURS ***
*** AHYMO MODEL FROM DRANAGE REPORT FOR LA CUMENTISTA SUBDIVISION - UNIT II ***
*** DATED JANUARY 2007 PREPARED BY WCI, A SUPPLEMENT TO THE DRAIANGE REPORT ***
*** FOR LA CUMENTISTA SUBDIVISION PREPARED BY WCI DATED NOV. 2003 ***
*** ORIGINAL MODEL INCLUDED 4 DU/AC LOTS ***
*** DEVELOPED CONDITIONS MODEL UPDATED NOVEMBER 2016 FOR TRACT B INTERIM CONDITIONS *
*** THIS MODEL USES 8 DU/AC (BASIN 202.3)*****
*** OFFSITE BASINS OS1 & OS8.1 (AREA ADJUSTED) AND BASIN 202.2 IN EXISTING
*** CONDITIONS-ADDENDUM FOR LC UNIT II, DEC 2014
*** RAINFALL DATA UPDATED PER NOAA ATLAS 14 WEBSITE ***
***
*****

```

```

*****
START TIME = 0
*****
RAINFALL TYPE = 2

```

RAIN QUARTER = 0.00 INCHES

RAIN ONE = 1.69

RAIN SIX = 2.17

RAIN DAY = 2.52

DT = 0.05 HOURS

```

*****
*** COMPUTE HYD FOR BASIN P-202.1 (EXISTING CONDITIONS)
COMPUTE NM HYD ID=1 HYDNO=202.1 DA=0.0339 SQ MI
PERCENT A=90 B=0 C=10 D=0
TP=0.133 HOURS MASSRAIN=-1

```

PRINT HYD ID=1 CODE=5

```

*** COMPUTE HYD FOR BASIN P-202.2 (EXISTING CONDITIONS)
COMPUTE NM HYD ID=2 HYDNO=202.2 DA=0.0051 SQ MI
PERCENT A=90 B=0 C=10 D=0
TP=0.133 HOURS MASSRAIN=-1

```

PRINT HYD ID=2 CODE=5

```

*** COMPUTE HYD FOR BASIN P-202.3 (8 DU/Acre)
COMPUTE NM HYD ID=3 HYDNO=202.3 DA=0.0172 SQ MI
PERCENT A=0 B=4 C=25 D=71
TP=0.133 HOURS MASSRAIN=-1

```

PRINT HYD ID=3 CODE=5

S ADD HYDROGRAPHS 202.3 and 202.2

ADD HYD ID=12 HYD=202.21 ID=3 ID=2
PRINT HYD ID=12 CODE=1

*S ADD OFFSITE BASINS OS1 & OS8 FROM ADDENDUM FOR LA CUMENTISTA SUBD UNIT II

*S SUBTRACT DEVELOPED BASIN 202.3 FROM OS8 IN ORIGINAL REPORT (12.59 AC)

*S

***** COMPUTING TP FOR BASIN EX-OS1 *****

```

COMPUTE LT TP
LCODE=1 NK=2 ISLOPE=0
LENGTH=400 FT SLOPE=0.0125 K=0.7
LENGTH=630 FT SLOPE=0.0146 K=2

```

P100_24 TRACT B Int.dat

*** COMPUTING HYD FOR BASIN EX-OS1

COMPUTE NM HYD ID=4 HYDNO=OS1 DA=0.0230 SQ MI
PERCENT A=90 B=0 C=10 D=0
TP=0.0 HOURS MASSRAIN=-1

PRINT HYD ID=4 CODE=5

*S*** ROUTE BASINS OS1 THRU BASIN OS8

COMPUTE RATING CURVE CID=1 VS NO=1 SEGS=1 MIN ELEV=5368 MAX ELEV=5372
CH SLP=0.013 FP SLP=0.013 N=0.03 DIST=350
DIST ELEV DIST ELEV
0 5372 80 5368
284 5368 350 5372

ROUTE MCUNGE ID=5 HYD NO= OS8 INFLOW ID=4
DT=0.0 L=3462 FT NS=0 SLOPE=0.013
PRINT HYD ID=5 CODE=5

*** COMPUTING TP FOR BASIN EX-OS8.1

COMPUTE LT TP LCODE=1 NK=3 ISLOPE=0
LENGTH=400 FT SLOPE=0.017 K=0.7
LENGTH=1600 FT SLOPE=0.017 K=2
LENGTH=1462 FT SLOPE=0.017 K=3
KN=0.033 CENTROID DISTANCE=1730

*** COMPUTING HYD FOR BASIN EX-OS8.1

COMPUTE NM HYD ID=8 HYDNO=108 DA=0.093 SQ MI
PERCENT A=86 B=0 C=10 D=4
TP=0.0 HOURS MASSRAIN=-1

PRINT HYD ID=8 CODE=5

*S*ADD BASIN OS1 AND OS8

ADD HYD ID=58 HYD=OS8.1 ID=5 ID=8

PRINT HYD ID=58 CODE=1

*S ADD ALL THE BASINS DRAINING INTO POND 1

S ADD BASINS OS1, OS8.1, 202.2 AND 202.3

ADD HYD ID=2 HYD=202.4 ID=12 ID=58
PRINT HYD ID=2 CODE=1

S ADD ALL BASINS INTO THE POND

ADD HYD ID=3 HYD=202.5 ID=2 ID=1
PRINT HYD ID=3 CODE=1

S Route HYDROGRAPH 202.14 Through POND 1
S discharge 15 cfs through 18" PIPE into Rosa Parks System
ROUTE RESERVOIR ID=31 HYD=POND.202.6 INFLOWID=3 CODE=5

OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)
0.0	0.0	5336
0.01	0.501	5337
0.1	1.044	5338
6.23	1.630	5339
10.8	2.261	5340
13.9	2.940	5341
16.5	3.668	5342
18.7	4.446	5343
20.6	5.277	5344

PRINT HYD

ID=31 CODE=1

* * * * *
* * * * *
FINISH

Appendix C

Hydraulic Calculations

- FlowMaster Calculations
 - Street Capacity
 - Inlet Capacity
- CulvertMaster Calculations
- Hydraflow Calculations
- Pillbox Manhole Calculations

Worksheet for Redroot St-Capacity

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Channel Slope 0.00510 ft/ft
Discharge 14.00 ft³/s
Section Definitions

Station (ft)	Elevation (ft)
0+00	0.79
0+06	0.67
0+11	0.67
0+11	0.00
0+26	0.30
0+41	0.00
0+41	0.67
0+46	0.67
0+52	0.79

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.79)	(0+06, 0.67)	0.013
(0+06, 0.67)	(0+11, 0.67)	0.030
(0+11, 0.67)	(0+41, 0.67)	0.016
(0+41, 0.67)	(0+46, 0.67)	0.030
(0+46, 0.67)	(0+52, 0.79)	0.013

Options

Current Roughness Weighted Method Pavlovskii's Method
Open Channel Weighting Method Pavlovskii's Method
Closed Channel Weighting Method Pavlovskii's Method

Worksheet for Redroot St-Capacity

Results

Normal Depth		0.36	ft
Elevation Range	0.00 to 0.79 ft		
Flow Area		6.17	ft ²
Wetted Perimeter		30.72	ft
Hydraulic Radius		0.20	ft
Top Width		30.00	ft
Normal Depth		0.36	ft
Critical Depth		0.34	ft
Critical Slope		0.00670	ft/ft
Velocity		2.27	ft/s
Velocity Head		0.08	ft
Specific Energy		0.44	ft
Froude Number		0.88	
Flow Type	Subcritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.36	ft
Critical Depth	0.34	ft
Channel Slope	0.00510	ft/ft
Critical Slope	0.00670	ft/ft

Worksheet for Privet St-Capacity

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Channel Slope 0.00670 ft/ft
Discharge 26.30 ft³/s
Section Definitions

Station (ft)	Elevation (ft)
0+00	0.79
0+06	0.67
0+11	0.67
0+11	0.00
0+26	0.30
0+41	0.00
0+41	0.67
0+46	0.67
0+52	0.79

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.79)	(0+06, 0.67)	0.013
(0+06, 0.67)	(0+11, 0.67)	0.030
(0+11, 0.67)	(0+41, 0.67)	0.016
(0+41, 0.67)	(0+46, 0.67)	0.030
(0+46, 0.67)	(0+52, 0.79)	0.013

Options

Current Roughness Weighted Method Pavlovskii's Method
Open Channel Weighting Method Pavlovskii's Method
Closed Channel Weighting Method Pavlovskii's Method

Worksheet for Privet St-Capacity

Results

Normal Depth		0.43	ft
Elevation Range	0.00 to 0.79 ft		
Flow Area		8.30	ft ²
Wetted Perimeter		30.86	ft
Hydraulic Radius		0.27	ft
Top Width		30.00	ft
Normal Depth		0.43	ft
Critical Depth		0.44	ft
Critical Slope		0.00587	ft/ft
Velocity		3.17	ft/s
Velocity Head		0.16	ft
Specific Energy		0.58	ft
Froude Number		1.06	
Flow Type	Supercritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.43	ft
Critical Depth	0.44	ft
Channel Slope	0.00670	ft/ft
Critical Slope	0.00587	ft/ft

Worksheet for AP2 - Single Grate A - at grade

Project Description

Solve For Efficiency

Input Data

Discharge	4.00	ft ³ /s
Slope	0.01050	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.016	
Local Depression	2.75	in
Local Depression Width	2.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	7.00	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	87.85	%
Intercepted Flow	3.51	ft ³ /s
Bypass Flow	0.49	ft ³ /s
Spread	11.11	ft
Depth	0.32	ft
Flow Area	1.36	ft ²
Gutter Depression	0.10	ft
Total Depression	0.33	ft
Velocity	2.94	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.06	
Grate Flow Ratio	0.52	
Equivalent Cross Slope	0.08580	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.37	
Total Interception Length	14.28	ft

Worksheet for AP2 - Single Grate C - at grade

Project Description

Solve For Efficiency

Input Data

Discharge	0.49	ft ³ /s
Slope	0.01050	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.016	
Local Depression	2.75	in
Local Depression Width	3.20	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.20	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	100.00	%
Intercepted Flow	0.49	ft ³ /s
Bypass Flow	0.00	ft ³ /s
Spread	3.26	ft
Depth	0.17	ft
Flow Area	0.23	ft ²
Gutter Depression	0.10	ft
Total Depression	0.33	ft
Velocity	2.12	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.10	
Grate Flow Ratio	0.94	
Equivalent Cross Slope	0.12233	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.32	
Total Interception Length	4.78	ft

Worksheet for AP3 - Single Grate A - at grade

Project Description

Solve For Efficiency

Input Data

Discharge	7.00	ft ³ /s
Slope	0.00670	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.016	
Local Depression	2.75	in
Local Depression Width	2.95	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	7.00	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	75.03	%
Intercepted Flow	5.25	ft ³ /s
Bypass Flow	1.75	ft ³ /s
Spread	15.47	ft
Depth	0.41	ft
Flow Area	2.52	ft ²
Gutter Depression	0.10	ft
Total Depression	0.33	ft
Velocity	2.78	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.06	
Grate Flow Ratio	0.38	
Equivalent Cross Slope	0.06933	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.30	
Total Interception Length	17.94	ft

Worksheet for AP3 - Single Grate C - at grade

Project Description

Solve For Efficiency

Input Data

Discharge	1.83	ft ³ /s
Slope	0.01050	ft/ft
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.016	
Local Depression	2.75	in
Local Depression Width	3.20	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	3.20	ft

Options

Calculation Option	Use Both
Grate Flow Option	Exclude None

Results

Efficiency	83.56	%
Intercepted Flow	1.53	ft ³ /s
Bypass Flow	0.30	ft ³ /s
Spread	7.71	ft
Depth	0.25	ft
Flow Area	0.72	ft ²
Gutter Depression	0.10	ft
Total Depression	0.33	ft
Velocity	2.54	ft/s
Splash Over Velocity	7.39	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.07	
Grate Flow Ratio	0.68	
Equivalent Cross Slope	0.09870	ft/ft
Active Grate Length	1.67	ft
Length Factor	0.16	
Total Interception Length	9.46	ft

Worksheet for AP4 - Single Grate A - sump

Project Description

Solve For Spread

Input Data

Discharge	6.40	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Local Depression	2.75	in
Local Depression Width	17.00	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	6.98	ft
Opening Height	0.67	ft
Curb Throat Type	Horizontal	
Throat Incline Angle	90.00	degrees

Options

Calculation Option Use Both

Results

Spread	6.88	ft
Depth	0.28	ft
Gutter Depression	0.10	ft
Total Depression	0.33	ft
Open Grate Area	3.12	ft ²
Active Grate Weir Length	5.41	ft

Worksheet for AP5 - Single Grate A - sump

Project Description

Solve For Spread

Input Data

Discharge	2.85	ft ³ /s
Gutter Width	2.50	ft
Gutter Cross Slope	0.06	ft/ft
Road Cross Slope	0.02	ft/ft
Local Depression	2.75	in
Local Depression Width	17.00	ft
Grate Width	2.08	ft
Grate Length	3.33	ft
Grate Type	P-50 mm (P-1-7/8")	
Clogging	50.00	%
Curb Opening Length	6.98	ft
Opening Height	0.67	ft
Curb Throat Type	Horizontal	
Throat Incline Angle	90.00	degrees

Options

Calculation Option Use Both

Results

Spread	4.99	ft
Depth	0.14	ft
Gutter Depression	0.10	ft
Total Depression	0.33	ft
Open Grate Area	3.12	ft ²
Active Grate Weir Length	5.41	ft

Culvert Calculator Report

Pond Outlet

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	5,344.00 ft	Headwater Depth/Height	4.67
Computed Headwater Elev.	5,344.00 ft	Discharge	20.65 cfs
Inlet Control HW Elev.	5,343.43 ft	Tailwater Elevation	5,338.50 ft
Outlet Control HW Elev.	5,344.00 ft	Control Type	Outlet Control

Grades			
Upstream Invert	5,337.00 ft	Downstream Invert	5,336.45 ft
Length	60.00 ft	Constructed Slope	0.009167 ft/ft

Hydraulic Profile			
Profile	Pressure Profile	Depth, Downstream	2.05 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	1.47 ft
Velocity Downstream	11.68 ft/s	Critical Slope	0.034673 ft/ft

Section			
Section Shape	Circular	Mannings Coefficient	0.013
Section Material	Concrete	Span	1.50 ft
Section Size	18 inch	Rise	1.50 ft
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	5,344.00 ft	Upstream Velocity Head	2.12 ft
Ke	0.50	Entrance Loss	1.06 ft

Inlet Control Properties			
Inlet Control HW Elev.	5,343.43 ft	Flow Control	Submerged
Inlet Type	Square edge w/headwall	Area Full	1.8 ft²
K	0.00980	HDS 5 Chart	1
M	2.00000	HDS 5 Scale	1
C	0.03980	Equation Form	1
Y	0.67000		

[illegible]

Date: 1/3/2017

Line No.	Line ID	Line Size (in)	Line Length (ft)	Line Slope (%)	Flow Rate (cfs)	Invert Dn (ft)	Invert Up (ft)	Gnd/Rim EI Dn (ft)	Gnd/Rim EI Up (ft)	HGL Dn (ft)	HGL Up (ft)	Cover Dn (ft)	Cover Up (ft)	J-Loss Coeff	Vel Ave (ft/s)	Capac Full (cfs)	
1		48	53.00	0.70	86.14	5337.00	5337.37	5343.00	5343.39	5339.51	5340.18	2.00	2.02	0.15	9.76	120.04	
2		48	34.00	0.32	83.24	5337.37	5337.48	5343.39	5343.65	5340.38	5340.56	2.02	2.17	0.90	8.12	81.66	
3		48	147.40	0.31	80.34	5337.47	5337.92	5343.65	5346.43	5341.62	5342.08	2.18	4.51	0.90	6.39	79.34	
4		36	285.50	0.70	54.00	5337.92	5339.92	5346.43	5350.40	5342.65	5344.52	5.51	7.48	0.80	7.64	55.82	
5		24	27.20	0.70	8.00	5340.92	5341.11	5350.40	5350.35	5345.25	5345.29	7.48	7.24	0.93	2.55	18.90	
6		18	24.50	2.12	4.00	5344.60	5345.12	5350.35	5350.62	5345.38	5345.89 j	4.25	4.00	0.50	4.37	15.30	
7		18	8.30	2.05	4.00	5344.60	5344.77	5350.35	5350.62	5345.38	5345.54 j	4.25	4.35	0.50	4.37	15.03	
8		36	241.00	0.50	26.34	5337.92	5339.12	5346.43	5343.64	5342.65	5343.03	5.51	1.52	0.80	3.73	47.07	
9		30	19.00	0.89	19.94	5339.12	5339.29	5343.64	5343.64	5343.20	5343.25	2.02	1.85	0.69	4.06	38.78	
10		30	76.00	0.91	13.54	5339.29	5339.98	5343.64	5343.95	5343.42	5343.51	1.85	1.47	0.72	2.76	39.08	
11		24	241.00	1.01	13.54	5339.98	5342.42	5343.95	5346.90	5343.59	5344.40	1.97	2.48	0.90	4.31	22.76	
12		18	27.70	1.01	6.77	5342.42	5342.70	5346.90	5346.86	5344.67	5344.78	2.98	2.66	0.50	3.83	10.56	
13		18	14.50	0.97	6.77	5342.42	5342.56	5346.90	5346.86	5344.67	5344.73	2.98	2.80	0.50	3.83	10.32	
14		18	11.50	2.00	2.90	5338.84	5339.07	5343.65	5343.39	5341.62	5341.63	3.31	2.82	0.50	1.64	14.85	
15		36	48.00	0.71	46.00	5339.92	5340.26	5350.40	5350.23	5345.25	5345.48	7.48	6.97	0.15	6.51	56.12	
16		36	10.00	0.70	46.00	5340.26	5340.33	5350.23	5350.50	5345.58	5345.63	6.97	7.17	0.80	6.51	55.92	
17		18	29.70	0.54	6.40	5340.11	5340.27	5343.64	5343.64	5343.20	5343.31	2.03	1.87	0.50	3.62	7.71	
18		18	6.00	2.00	3.51	5345.12	5345.24	5350.62	5350.62	5345.89	5345.96 j	4.00	3.88	0.00	4.05	14.86	
19		18	6.00	2.00	3.51	5344.77	5344.89	5350.62	5350.62	5345.54	5345.60 j	4.35	4.23	0.00	4.05	14.86	
20		18	6.00	1.99	5.17	5342.70	5342.82	5346.86	5346.86	5344.89	5344.91	2.66	2.54	0.00	2.93	14.83	
21		18	6.00	2.00	5.17	5342.56	5342.68	5346.86	5346.86	5344.84	5344.85	2.80	2.68	0.00	2.93	14.86	

TRACT B-2

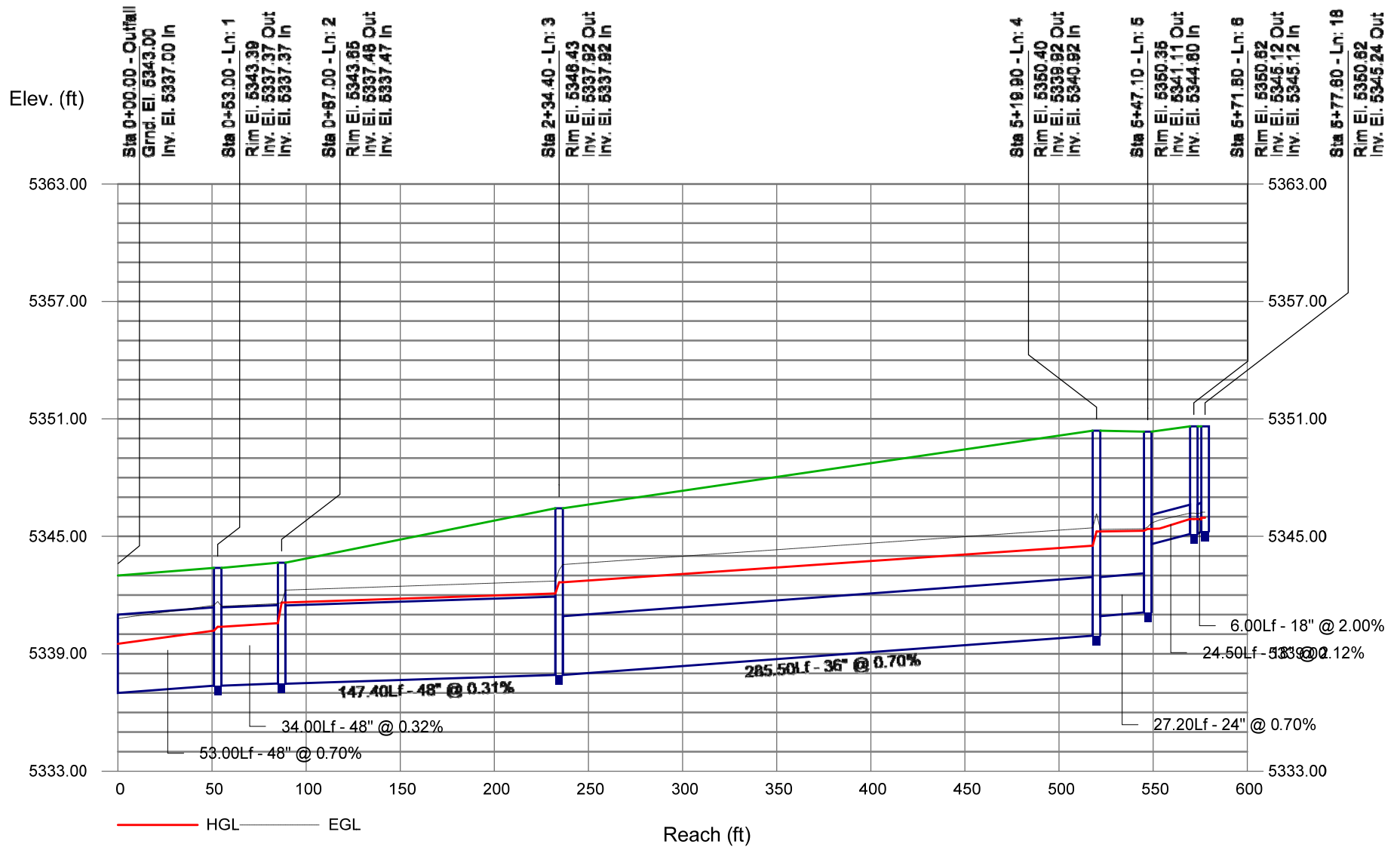
Number of lines: 21

Date: 1/3/2017

NOTES: i Inlet control; ** Critical depth

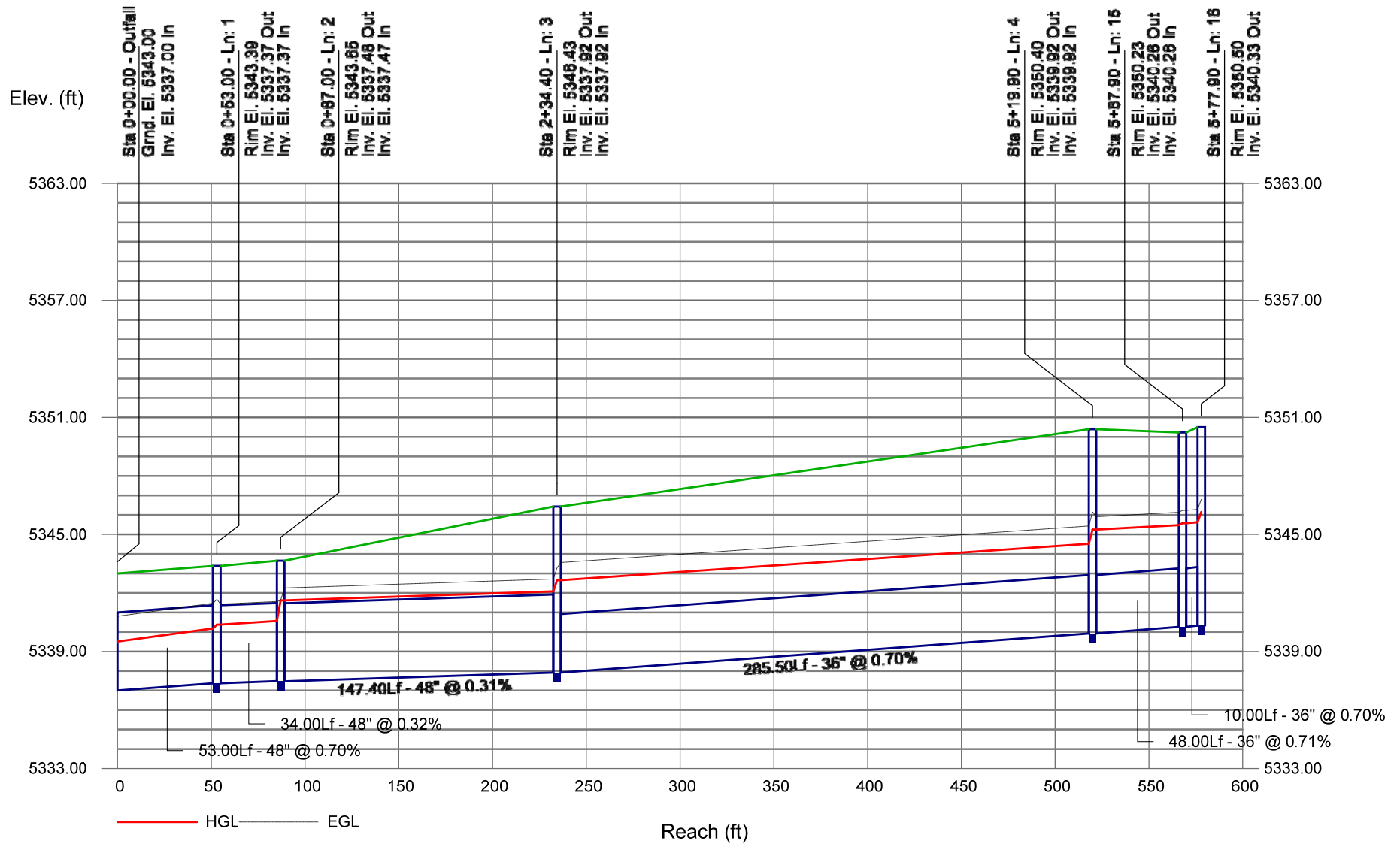
Storm Sewer Profile

Proj. file: Tract B-2.stm

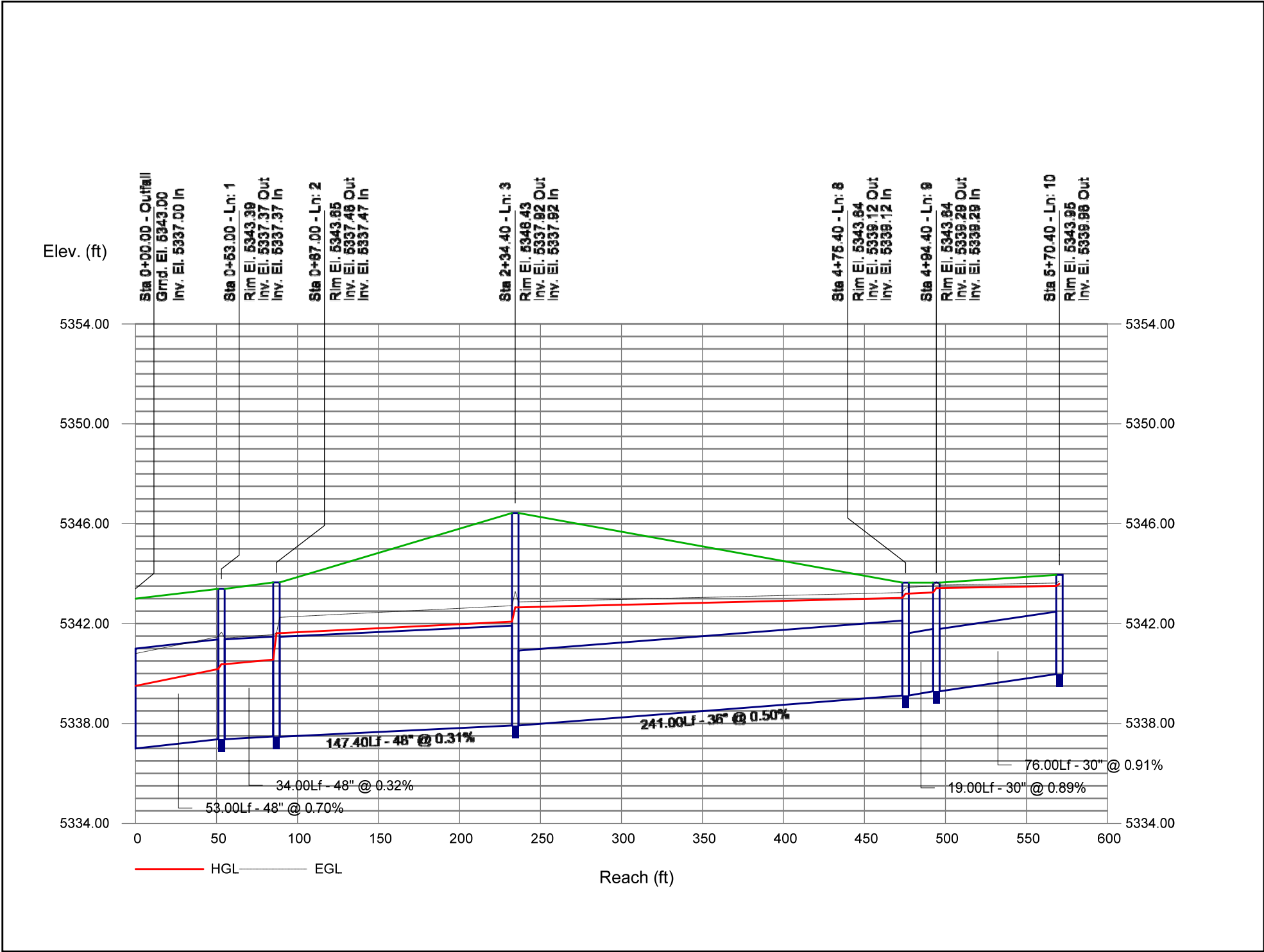


Storm Sewer Profile

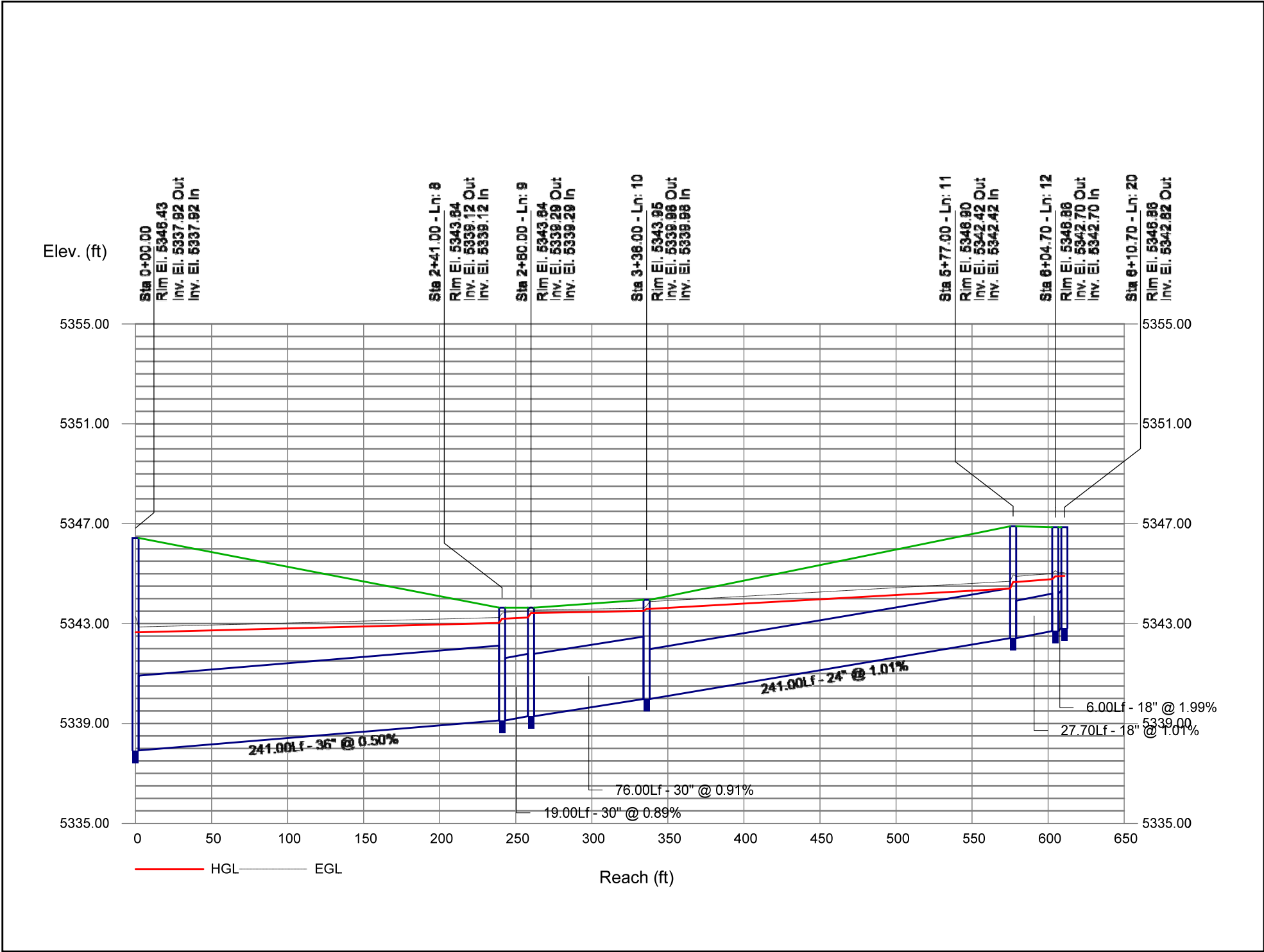
Proj. file: Tract B-2.stm



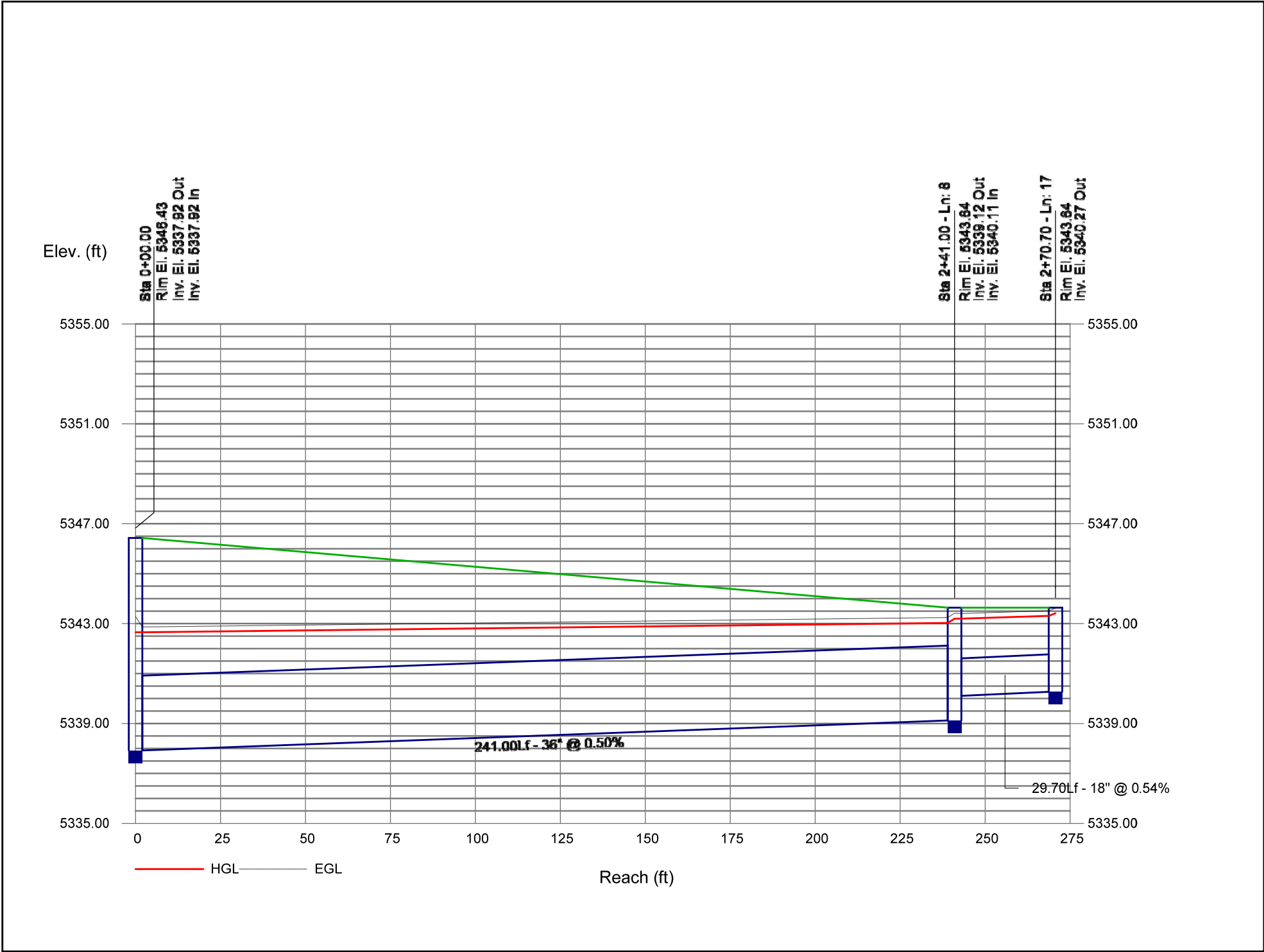
Storm Sewer Profile



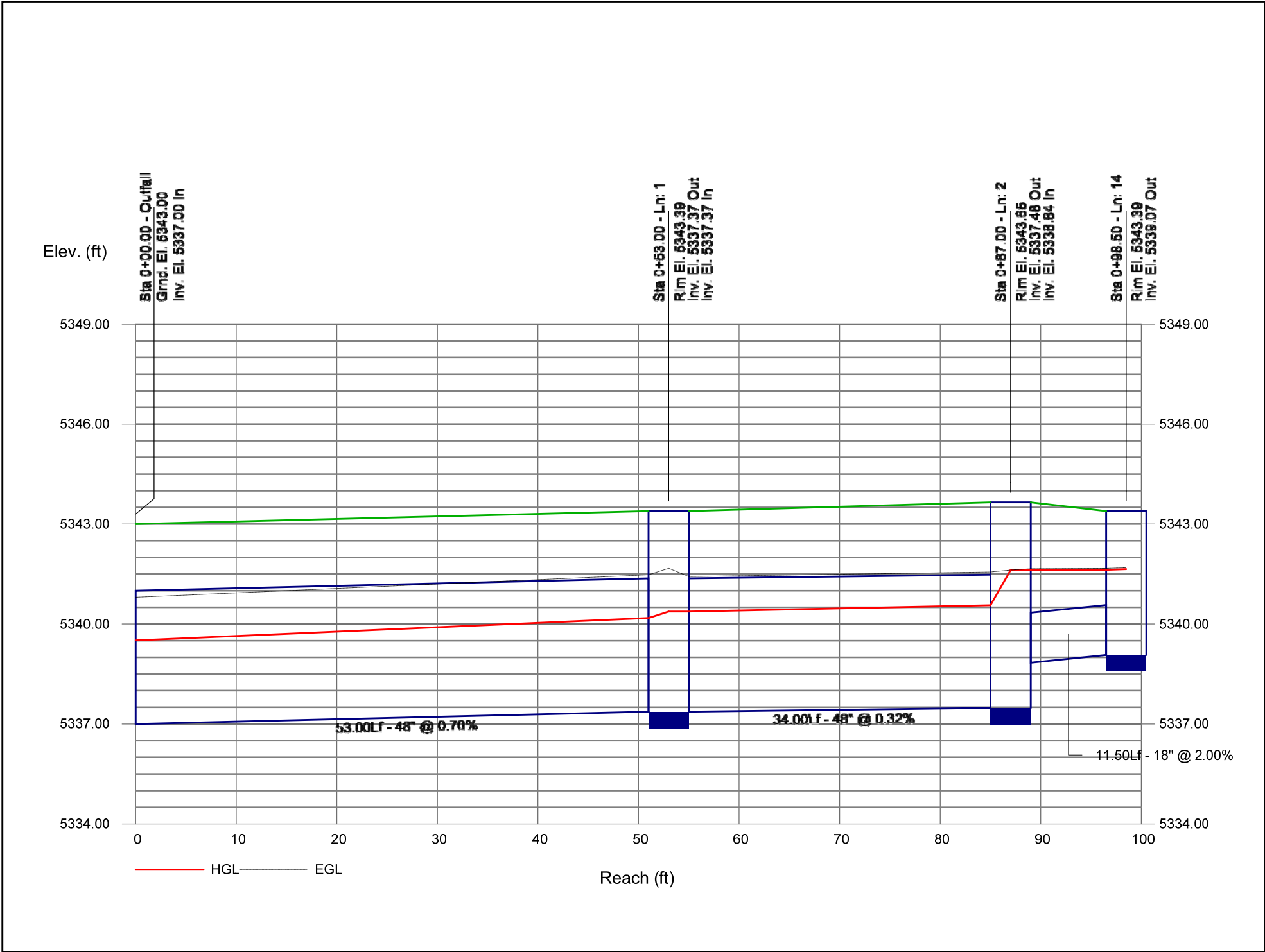
Storm Sewer Profile



Storm Sewer Profile



Storm Sewer Profile



LA CUENTISTA TRACT B-2

PILL BOX MANHOLE INLET - DISCHARGE CALCULATIONS

36" STORM DRAIN

INVERT OF OUTLET PIPE
ORIFICE SIZE (in)
TAILWATER EL:

5340.93
36
5342.94 Based on HGL calcs for 46 cfs

ORIFICE FLOW			
ELEVATION	A (sf)	h (ft)	Q (cfs)
5343.00	7.07	0.06	8.61
5343.25	7.07	0.31	19.58
5343.50	7.07	0.56	26.32
5343.75	7.07	0.81	31.65
5344.00	7.07	1.06	36.21
5344.25	7.07	1.31	40.25
5344.50	7.07	1.56	43.93
5344.66	7.07	1.72	46.12
5345.00	7.07	2.06	50.48
5346.00	7.07	3.06	61.52
5347.00	7.07	4.06	70.86
5348.00	7.07	5.06	79.11
5349.00	7.07	6.06	86.58
5350.00	7.07	7.06	93.45
5350.23	7.07	7.29	94.96

Orifice Equation, $Q=0.62 \cdot A \cdot (2g\Delta h)^{1/2}$, submerged orifice

A = area of orifice, Δh = differential head, Q = discharge rate

PILL BOX MANHOLE INLET

INVERT OF PERFORATION(S) 5348.4
HEIGHT OF PERFORATION(S) (in) 14
LENGTH OF PERFORATION(S) (ft) 3.38

4 - 16" L X 14" H X 8" W BLOCK

# PERFORATIONS		1	2	3	4
ELEVATION	A (sf)	h (ft)	Q (cfs)	Q (cfs)	Q (cfs)
5348.50	3.94	-	-	-	-
5348.75	3.94	-	-	-	-
5349.00	3.94	0.02	2.53	5.07	7.60
5349.25	3.94	0.27	10.13	20.26	30.40
5349.33	3.94	0.35	11.55	23.10	34.66
5349.50	3.94	0.52	14.10	28.21	42.31
5350.00	3.94	1.02	19.78	39.57	59.35
5350.23	3.94	1.25	21.91	43.81	65.72

~GROUND ELEVATION AT TOP OF BOX

Appendix D

Referenced Documents

- Selected pages from a Drainage Report for La Cuentista Subdivision – Unit II a Supplement to the Drainage Report for La Cuentista Subdivision
- Selected pages from Drainage Report Addendum for La Cuentista Subdivision – Unit II
- Selected sheets from La Cuentista Subdivision – Unit II Paving Plan & Profile sheets – Rosa Parks Road and Redroot Street

Drainage Report

for

LA CUENTISTA SUBDIVISION – Unit II

**A Supplement to the
Drainage Report for La Cuentista Subdivision
Dated November 2003**

Prepared by:

**Wilson & Company, Inc.
4900 Lang Ave NE
Albuquerque, New Mexico 87109
(505) 348-4191**

**January 2007
WCI File No: 0660004701**

**WILSON
& COMPANY**

CITY OF ALBUQUERQUE



January 25, 2007

Dan Aguirre, PE
Wilson & Company
4900 Lang Ave
Albuquerque, NM 87109

Re: La Cuentista Subdivision Unit 2 Drainage Report
Engineer Stamp 1-23-07 (D10/D2)

Dear Mr. Aguirre,

Based upon information provided in your submittal dated 1-24-07, the above referenced report is approved for Preliminary Plat action by the DRB. Once that board has approved the plan, please provide a mylar copy for my signature in order to obtain a Grading Permit.

This project requires a National Pollutant Discharge Elimination System (NPDES) permit. Refer to the attachment that is provided with this letter for details. If you have any questions please feel free to call the Municipal Development Department, Hydrology section at 768-3654 (Charles Caruso).

Prior to Release of SIA and Financial Guarantees, an Engineer's Certification of this grading plan will be required.

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE
Principal Engineer, Planning Dept.
Development and Building Services

C: Chuck Caruso, CoA
file

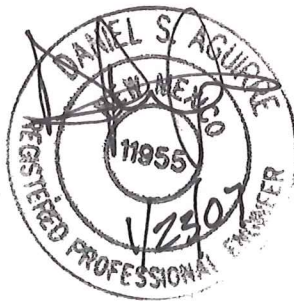
Drainage Report

for

LA CUENTISTA SUBDIVISION – Unit II

**A Supplement to the
Drainage Report for La Cuentista Subdivision
Dated November 2003**

Prepared by:



**Daniel S. Aguirre, PE
NM #11955**

**Wilson & Company, Inc.
4900 Lang Ave NE
Albuquerque, New Mexico 87109
(505) 348-4191**

**January 2007
WCI File No: 0660004701**

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Proposed Improvements/Modifications.....	1
Updated Data Tables	2
Conclusion	2
Appendix A – Hydrologic Model- Fully Developed Conditions – Revised January 2007	
Appendix B – Unit II Storm Drain Analysis, 213 Sub-Basin Boundary Map	
Plate 1 – Grading & Drainage Plan: Unit II	
Plate 2 – Fully Developed Conditions Basin Boundary Map	

Summary

La Cuentista Subdivision - Unit II, a residential development, is Tract C and the second of five bulk land tracts which collectively comprise La Cuentista Subdivision. The 35.47 acres of Unit II (Tract C) is approximately 15% of the total La Cuentista Subdivision. The approved "Drainage Report for La Cuentista Subdivision" dated November 2003 by Wilson & Company, Inc., provides site and existing conditions information.

Drainage

Proposed Conditions/Modification:

Unit II (Tract C) approximately replicates Basin 213 from the approved Drainage Report. This basin is designated to discharge into Pond 4 along with Unit I (Tract A) discharge. Pond 4, located north of Kimmick Dr., along with the outfall structure to the Petroglyph National Monument allowed per agreement with COA Open Space Division, are currently under construction.

Site design of Unit I (Tract A), Unit II (Tract C) and plans for Tract B require modifications to the approved Drainage Report. Basins 201 and 202 make up Tract B, an as yet undesignated unit of La Cuentista. The approved Drainage Report routed Basin 201 flows through Pond 1 and then through Unit I (Tract A) basins into Pond 4. Basin 202 was routed through Basin 213 to Pond 4. Flows from Basin 201 are herein proposed to route through Basin 202 and a newly designated Pond 2. A maximum flow of 15 cfs from Pond 2 will then be directed into Basin 213 via appropriately sized storm drain pipe, with Basin 213 discharging to Pond 4, as previously designed.

Flows from Basin 301 and 302, previously designed to route through storm drain in Kimmick Drive and into Pond 8 will be routed through Basin 214 to Pond 8.

A review and the updating of hydraulic data led to changes to Tables 3 & 4 from the approved Drainage Report. These are presented below. Additionally, a revised **Proposed Conditions: Drainage Basin Map** (Plate 2) is provided herein.

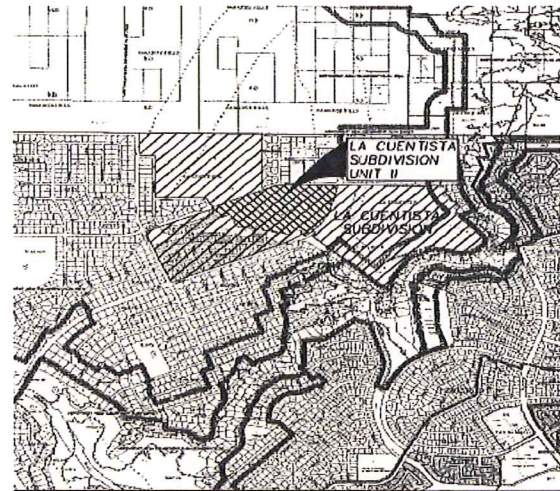


Table 3: Summary of Fully Developed Flows		
Basin	Area (acres)	100_{year}-24_{hour} Peak Flow (Q₁₀₀) cfs
201	22.1	71.8
202	35.0	112.9
203	1.2	4.1
204	5.0	16.4
205	8.8	28.7
206	4.6	14.4
207	2.4	8.2
208	8.5	21.2
209	3.6	12.3
210	2.6	8.0
211	6.2	20.5
212	3.3	9.8
213	40.2	129.3
214	55.1	176.6
215	34.5	110.8
301	43.7	142.6
302	37.3	119.0
303	43.0	137.5
304	69.0	217.1

Table 4: Summary of Discharge Points – Fully Developed		
Pond #		100_{year} 6_{hour} Peak Flow (Q₁₀₀) cfs
4		87
8		106
7		42 (40 Allowable)
Total discharge to Petroglyph NM		235 cfs
10	Calle Norteña/ Piedras Marcadas	15

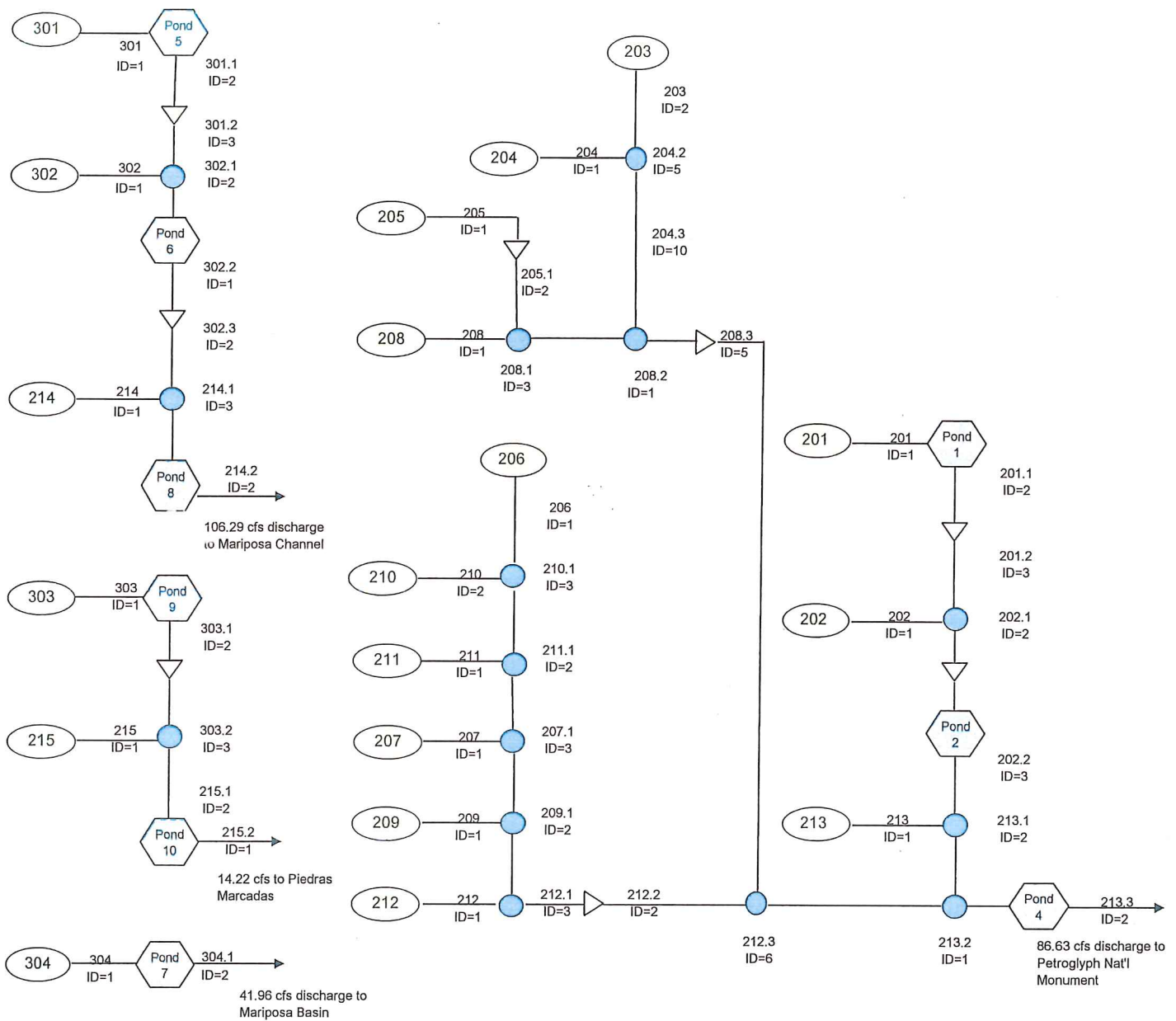
Unit II Proposed Improvement.

The AHYMO discharge from Basin 213 is 130 cfs (See Appendix A). For design purposes for inlets and onsite storm drain, the sub-basin flows, totaling approximately the 130 cfs, are proportionately distributed based on basin areas. See Appendix B for Unit II hydrology and Sub-Basin Boundary Map.

Conclusion

The development of Unit II has been analyzed in this report. The project's design will adhere to the requirements of the approved Drainage Report dated November 2003 and all developed flows in Unit II will be conveyed to Pond 4, discharge through the required water quality standpipe and outfall structure being constructed as part of Unit I, with ultimate discharge to the Petroglyph National Monument. The system is designed to convey existing offsite flows through the site. Off site drainage basins will be required to detain developed flows as future development occurs.

La Cuentista; Hydrologic Model Diagram: Fully Developed Conditions - Revised January 2007



KEY

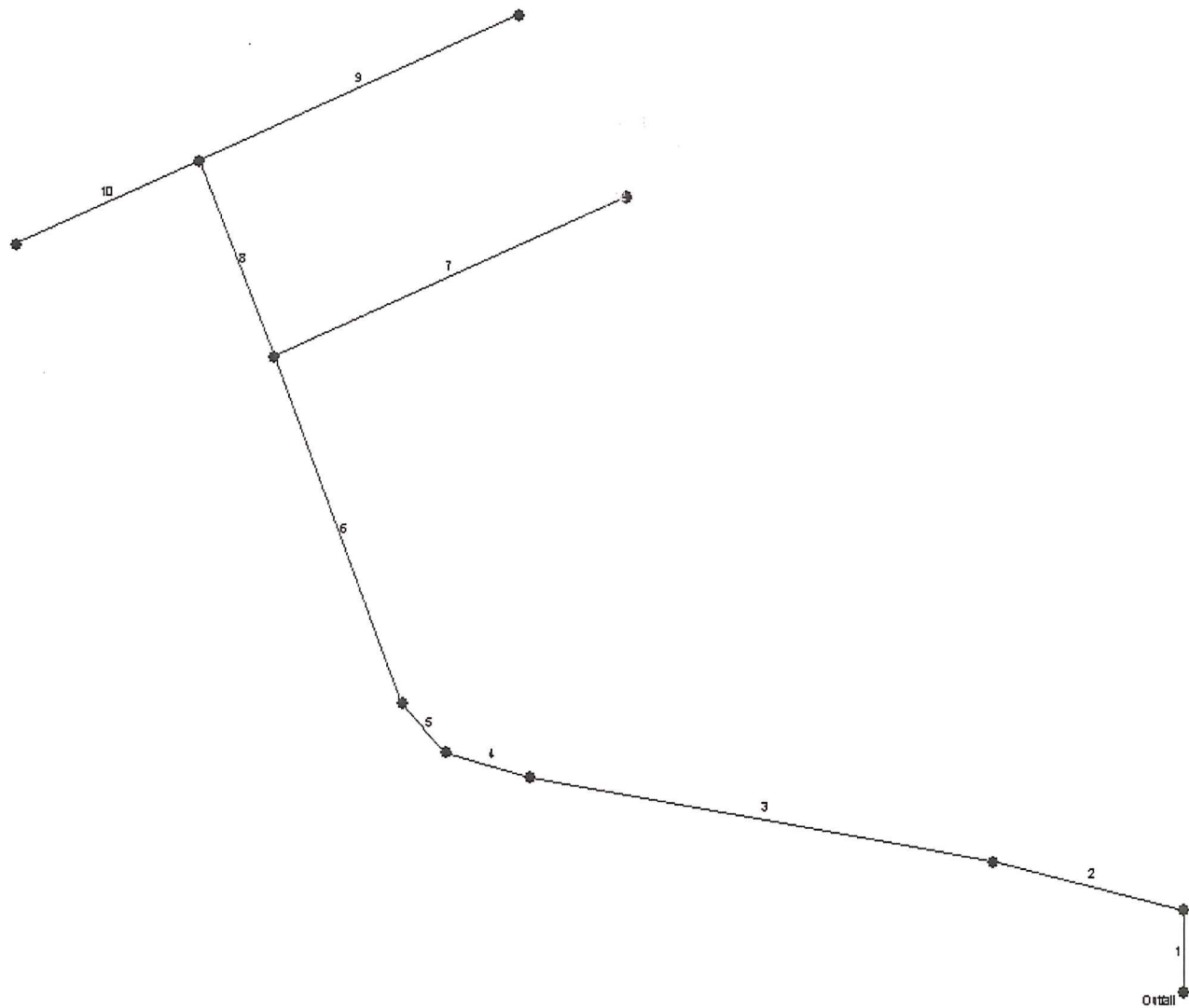


COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1 NOTATION
START										TIME= .00
S 1- COMPUTING RAINFALL						***				
RAINFALL TYPE= 2										RAIN24= 2.660
S 2- COMPUTE TP FOR OFFSITE BASIN 301 (SET tp= MIN 0.133 HRS						***				
S 3- COMPUTE HYD FOR BASIN 301, (assume platted to 5 DU/ACRE, %D=50)										
COMPUTE NM HYD	301.00	-	1	.06800	142.62	5.767	1.59006	1.500	3.277 PER IMP=	50.00
S 4- Route HYDROGRAPH 301 through POND 5 (0.30/0.52ac surface/bottom, 2.20AF										
S Historical flow Basin 301 (100% A)= 74.42CFS use 75+/- thru 34" orifice plat										
ROUTE RESERVOIR	POND.301.1	1	2	.06800	64.26	5.767	1.59006	1.700	1.477 AC-FT=	1.622
S 5- Route POND 5 outflow (BASIN 301) through BASIN 302 via 36"X 1800'RCP										
S (24'/1800'= 0.15 slp) Add to basin 302 at pond 6, (#8)										
ROUTE MCUNGE	301.20	2	3	.06800	64.25	5.767	1.59027	1.750	1.476 CCODE =	.2
S 6- COMPUTE TP FOR BASIN 302 (LET tp= 0.133 MIN)						***				
S 7- COMPUTE HYD FOR BASIN 302 (assume replat to 4 DU/Ac, D=42%, use 45%)										
S Historical flow (100% A)= 57.95CFS										
COMPUTE NM HYD	302.00	-	1	.05800	119.01	4.693	1.51708	1.500	3.206 PER IMP=	45.00
S 8- ADD HYDROGRAPHS 301.2 (ROUTED THROUGH 302) AND 302 - INFLOW TO POND 6										
ADD HYD	302.10	1 & 3	2	.12600	164.30	10.460	1.55657	1.500	2.037	
S 9- ROUTE HYDROGRAPH 302.1 through POND 6 (0.2/0.4AC surf/bottom, 1.5AF st										
S Historical flow- 100% A (Basin 301= 74.42)+(Basin 302= 57.95)= 132.37CF										
S discharge through 48" RCP w/ 45" orifice plate										
ROUTE RESERVOIR	POND.302.2	2	1	.12600	117.19	10.460	1.55658	1.700	1.453 AC-FT=	1.254
S 10- Route outflow from POND 6 (BASIN 301 & 302) through										
S 48"x 2300'RCP (50/2300= 2.2% slp) through Basin 214 TO POND 8										
ROUTE MCUNGE	302.30	1	2	.12600	117.10	10.462	1.55684	1.750	1.452 CCODE =	.2
S 76- COMPUTE TP FOR BASIN 214 (Let tp= 0.133= Min.)						***				
S 77- COMPUTE HYD FOR BASIN 214										
COMPUTE NM HYD	214.00	-	1	.08600	176.58	6.958	1.51708	1.500	3.208 PER IMP=	45.00
S 78- ADD HYDROGRAPHS 302.3 AND 214										
ADD HYD	214.10	2 & 1	3	.21200	256.75	17.420	1.54071	1.500	1.892	
S 79- Route HYDROGRAPH 214.1 through POND 8 (1.7/2.2AC surf/btm, 11.3AF stor										
ROUTE RESERVOIR	POND.214.2	3	2	.21200	106.29	17.420	1.54071	2.150	.783 AC-FT=	6.213
S 11- COMPUTE TP FOR BASIN P-303 (let TP= 0.133 hrs= min)						***				
S 12- COMPUTE HYD FOR BASIN 303 (assume replat to 4 DU/Ac, D=42%, use 45%)										
S BASIN 303 Historical flow (100% A)= 75.29CFS										
COMPUTE NM HYD	303.00	-	1	.06700	137.50	5.421	1.51708	1.500	3.207 PER IMP=	45.00
S 13- ROUTE HYDROGRAPH 303 THROUGH POND 9 (0.3/0.52AC surface/bottom, 2.11AF										
S 303 Hist. flow= 75.29CFS, discharge through 36" RCP w/ 34" orifice pla										
ROUTE RESERVOIR	POND.303.1	1	2	.06700	62.82	5.421	1.51708	1.700	1.465 AC-FT=	1.536
S 14- Route outflow from POND 9 (BASIN 303.1) through 36"x 1300'RCP										
ROUTE MCUNGE	303.20	2	3	.06700	62.82	5.422	1.51721	1.700	1.465 CCODE =	.2
S 81- COMPUTE TP FOR BASIN P-215 (Let tp= 0.133 Min.)						***				
S 82- COMPUTE HYD FOR BASIN P-215										
COMPUTE NM HYD	215.00	-	1	.05400	110.81	4.369	1.51708	1.500	3.206 PER IMP=	45.00
S 83- ADD HYDROGRAPHS 303.2 AND 215										
ADD HYD	215.10	1 & 3	2	.12100	156.91	9.791	1.51715	1.500	2.026	
S 85- Route HYDROGRAPH 215.1 through POND 10 (1.0/0.7AC surf/btm, 4.65AF sto										
ROUTE RESERVOIR	POND.215.2	2	1	.12100	14.22	9.789	1.51696	2.500	.184 AC-FT=	6.835
S 15- COMPUTE TP FOR OFFSITE BASIN 304 Let TP= 0.133 hrs= min.)						***				
S 16- Compute HYD for BASIN 304 (ex.platting 2.33+/- DU/Acre => 35%D, use 40										

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 2 NOTATION
S	BASIN 304 @ 100% A: Historical flow			area= 0.05 sq mi,	flow= 41.24cfs					
COMPUTE NM HYD	304.00	-	1	.10800	217.09	8.321	1.44459	1.500	3.141	PER IMP= 40.00
S	17- Route HYDROGRAPH 304 through POND 7 (H=4.0', 0.40/0.25AC surf/bottom, cap.). 304 historical: 100% A;area= 0.05 sq mi; flow= 41.24cfs;									
S	discharge through 28" orifice plate into 30' RCP									
ROUTE RESERVOIR	POND.304.1	1	2	.10800	41.96	8.321	1.44459	1.950	.607	AC-FT= 4.223
S	23- COMPUTE TP FOR BASIN P-203 (let TP= 0.133= Min.)					***				
S	24- COMPUTE HYD FOR BASIN P-203 (2.5 DU/acre, use D=45)									
COMPUTE NM HYD	203.00	-	2	.00200	4.12	.162	1.51708	1.500	3.218	PER IMP= 45.00
S	31- COMPUTE TP FOR BASIN P-204 (Let tp= 0.133= Min.)					***				
COMPUTE NM HYD	204.00	-	1	.00800	16.43	.647	1.51708	1.500	3.209	PER IMP= 45.00
S	84- ADD HYDROGRAPHS 203 AND 204									
ADD HYD	204.20	1& 2	5	.01000	20.55	.809	1.51703	1.500	3.211	
S	33- Route HYDROGRAPH 204.2 through BASIN 208 IN 24'X570 LF PIPE									
ROUTE MCUNGE	204.30	5	10	.01000	20.45	.809	1.51741	1.500	3.196	CCODE = .2
S	34- COMPUTE TP FOR BASIN P-205 (Let tp= 0.133= Min.)					***				
S	35- COMPUTE HYD FOR BASIN P-205 (assume 4 DU/Acre=> 42%D, use 45%D)									
COMPUTE NM HYD	205.00	-	1	.01400	28.70	1.133	1.51708	1.500	3.203	PER IMP= 45.00
S	36- ROUTE HYDROGRAPH 205 THROUGH PIPE TO CONFLUENCE W/ BASIN 208									
ROUTE MCUNGE	205.10	1	2	.01400	28.31	1.133	1.51746	1.500	3.160	CCODE = .2
S	45- COMPUTE TP FOR BASIN P-208 (Let tp= 0.133= Min.)					***				
COMPUTE NM HYD	208.00	-	1	.01300	21.22	.725	1.04601	1.500	2.550	PER IMP= 20.00
S	47- ADD HYDROGRAPHS 205.1 and 208									
ADD HYD	208.10	1& 2	3	.02700	49.53	1.858	1.29043	1.500	2.866	
S	48- ADD HYDROGRAPHS 204.3 AND 208.1									
ADD HYD	208.20	3&10	1	.03700	69.98	2.667	1.35176	1.500	2.955	
*S*51-	ROUTE ADDED FLOWS AT HYDROGRAPH 208.2 through PIPE TO POND 4									
ROUTE MCUNGE	208.30	1	5	.03700	68.50	2.668	1.35209	1.500	2.893	CCODE = .2
S	37- COMPUTE TP FOR BASIN P-206 (Let tp= 0.133= Min.)					***				
S	38- COMPUTE HYD FOR BASIN P-206 (assume 4 DU/Acre=> 42%D, use 45%D)									
COMPUTE NM HYD	206.00	-	1	.00700	14.36	.566	1.51708	1.500	3.205	PER IMP= 45.00
S	59- COMPUTE TP FOR BASIN P-210 (let tp=0.133= Min.)					***				
S	60- COMPUTE HYD FOR BASIN P-210 (3.0 DU/acre=> 35%D, use 40%D)									
COMPUTE NM HYD	210.00	-	2	.00400	8.04	.308	1.44459	1.500	3.141	PER IMP= 40.00
S	- ADD HYDROGRAPHS 206 AND 210									
ADD HYD	210.10	1& 2	3	.01100	22.40	.875	1.49067	1.500	3.182	
S	62- Compute TP for BASIN P-211 (let tp=0.133= Min.)					***				
S	63- COMPUTE HYD FOR BASIN P-211 (3.7 DU/acre=> 40%D, use 45%D)									
COMPUTE NM HYD	211.00	-	1	.01000	20.53	.809	1.51708	1.500	3.208	PER IMP= 45.00
S	64- ADD HYDROGRAPHS 210.1 AND 211									
ADD HYD	211.10	1& 3	2	.02100	42.93	1.684	1.50323	1.500	3.194	
S	41- COMPUTE TP FOR BASIN P-207 (Let tp= 0.133= Min.)					***				
S	42- COMPUTE HYD FOR BASIN P-207 (actual 3.7DU/acre, assume 4 DU/Acre=>									
COMPUTE NM HYD	207.00	-	1	.00400	8.21	.324	1.51708	1.500	3.208	PER IMP= 45.00
S	- ADD HYDROGRAPHS 211.1 AND 207									
ADD HYD	207.10	1& 2	3	.02500	51.14	2.007	1.50544	1.500	3.196	
S	52- Compute TP for BASIN P-209 (Let tp=0.133= Min.)					***				
S	53- Compute HYD for BASIN 209 (3.86du/acre=> 41%D, use 45%D)									
COMPUTE NM HYD	209.00	-	1	.00600	12.33	.485	1.51708	1.500	3.210	PER IMP= 45.00
S	- ADD HYDROGRAPHS 207.1 AND 209									
ADD HYD	209.10	1& 3	2	.03100	63.47	2.493	1.50768	1.500	3.199	
S	66- COMPUTE TP FOR BASIN P-212 (Let TP=0.133= Min.)					***				

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 3	NOTATION
S	67- Computing HYD for BASIN P-212 (2.5 DU/acre=> 30%D, use 35%D)										
COMPUTE NM HYD	212.00	-	1	.00500	9.81	.366	1.37175	1.500	3.066	PER IMP=	35.00
S	68- ADD HYDROGRAPHS 209.1 AND 212										
ADD HYD	212.10	2& 1	3	.03600	73.28	2.858	1.48879	1.500	3.181		
S	69 ROUTE HYDROGRAPH 212.1 down Kimmick in 48"x 175' RCP to POND 4										
ROUTE MCUNGE	212.20	3	2	.03600	73.28	2.858	1.48879	1.500	3.181	CCODE =	.0
S	70- Add HYDROGRAPHS 212.2 TO 208.3 (At POND 4)										
ADD HYD	212.30	2& 5	6	.07300	141.78	5.527	1.41950	1.500	3.035		
S	19- COMPUTE TP FOR BASIN 201 (let TP= 0.133= Min.)										
S	20- COMPUTE HYD FOR BASIN P-201 (assume 4 DU/Acre=> 42%D, use 45%D)										
COMPUTE NM HYD	201.00	-	1	.03500	71.82	2.832	1.51708	1.500	3.206	PER IMP=	45.00
S	21- Route HYDROGRAPH 201 through POND 1 (0.5/0.25AC surf/btm, 1.65AF stor.										
S	discharge 15.21cfs through 15" orifice plate route to POND 2										
ROUTE RESERVOIR	POND.201.1	1	2	.03500	13.29	2.832	1.51707	2.000	.593	AC-FT=	1.474
S	22- Route outflow from POND 1 (BASIN 201) in 24"PIPE through BASIN 202 TO										
S	NEW POND #2 IN BASIN 202										
ROUTE MCUNGE	201.20	2	3	.03500	13.28	2.830	1.51601	2.050	.593	CCODE =	.2
S	27- COMPUTE TP FOR BASIN P-202 (set tp= 0.133= Min.)										
COMPUTE NM HYD	202.00	-	1	.05500	112.86	4.450	1.51708	1.500	3.206	PER IMP=	45.00
S	28A- Add HYDROGRAPHS 201.2 and 202										
ADD HYD	202.10	1& 3	2	.09000	120.52	7.280	1.51665	1.500	2.092		
S	29- Route HYDROGRAPH 202.1 Through POND 2 (0.77/0.5AC surf/btm, 3.50AF st										
S	discharge 15.21cfs through 15" orifice plate into Rosa Parks System										
ROUTE RESERVOIR	POND.202.2	2	3	.09000	14.73	7.280	1.51665	2.550	.256	AC-FT=	3.513
S	56A- Compute TP for BASIN 213 (Let tp=0.133= Min.)										
S	56B- COMPUTE HYD FOR BASIN 213 (3.86du/acre=> 41%D, use 45%D)										
COMPUTE NM HYD	213.00	-	1	.06300	129.28	5.097	1.51708	1.500	3.206	PER IMP=	45.00
S	56C- Add HYDROGRAPH 202.2 (outflow from POND 2) and 213										
ADD HYD	213.10	1& 3	2	.15300	138.12	12.377	1.51682	1.500	1.410		
S	56D- Add HYDROGRAPHS 212.3 and 213.1 (INFLOW TO POND 4)										
ADD HYD	213.20	2& 6	1	.22600	279.89	17.904	1.48538	1.500	1.935		
S	57- Route BASIN 213.1 through POND 4										
ROUTE RESERVOIR	POND.213.3	1	2	.22600	86.63	17.904	1.48538	1.850	.599	AC-FT=	4.249
FINISH											

Hydraflow Plan View



LA CUENTISTA UNIT II - SD	No. Lines: 10	01-17-2007
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Hydraulic Grade Line Computations

Line	Size (in)	Q (cfs)	Downstream								Len (ft)	Upstream								Check		JL coeff (K)	Minor loss (ft)
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy loss (ft)		
1	54	142.0	5298.00	5301.42	3.42	12.96	10.95	1.87	5303.28	0.609	72.6	5301.39	5304.81	3.42**	12.96	10.95	1.87	5306.67	0.609	0.609	n/a	0.98	1.83
2	48	63.00	5301.39	5306.28	4.00	12.56	5.01	0.39	5306.67	0.192	189	5301.59	5306.65	4.00	12.57	5.01	0.39	5307.04	0.192	0.192	0.363	0.15	0.06
3	42	63.00	5301.59	5306.71	3.50	9.62	6.55	0.67	5307.37	0.392	450	5306.42	5308.85	2.43**	7.13	8.83	1.21	5310.06	0.571	0.482	n/a	0.15	0.18
4	36	63.00	5306.42	5308.85	2.43	6.14	10.27	1.64	5310.49	0.911	84.0	5307.77	5310.30	2.53**	6.36	9.91	1.53	5311.83	0.850	0.881	n/a	0.57	n/a
5	36	63.00	5308.27	5310.59	2.32	5.87	10.74	1.79	5312.38	1.002	60.0	5309.57	5312.10	2.53**	6.36	9.91	1.53	5313.63	0.850	0.926	n/a	0.43	n/a
6	30	39.00	5309.57	5312.64	2.50	4.91	7.95	0.98	5313.63	0.905	330	5323.56	5325.65	2.09**	4.38	8.91	1.23	5326.88	0.876	0.890	n/a	1.00	1.23
7	24	10.00	5323.56	5326.72	2.00	3.14	3.18	0.16	5326.88	0.196	365	5324.17	5327.44	2.00	3.14	3.18	0.16	5327.59	0.195	0.196	0.713	1.00	0.16
8	30	18.00	5323.56	5326.67	2.50	4.91	3.67	0.21	5326.88	0.193	188	5332.53	5333.95	1.42**	2.87	6.27	0.61	5334.56	0.509	0.351	n/a	1.00	0.61
9	24	16.00	5332.53	5334.53	2.00*	3.14	5.09	0.40	5334.93	0.501	332	5333.00	5336.19	2.00	3.14	5.09	0.40	5336.60	0.500	0.501	1.663	1.00	0.40
10	24	2.00	5332.53	5334.55	2.00	3.14	0.64	0.01	5334.56	0.008	190	5332.07	5334.57	2.00	3.14	0.64	0.01	5334.57	0.008	0.008	0.015	1.00	0.01

LA CUENTISTA UNIT II - SD

Number of lines: 10

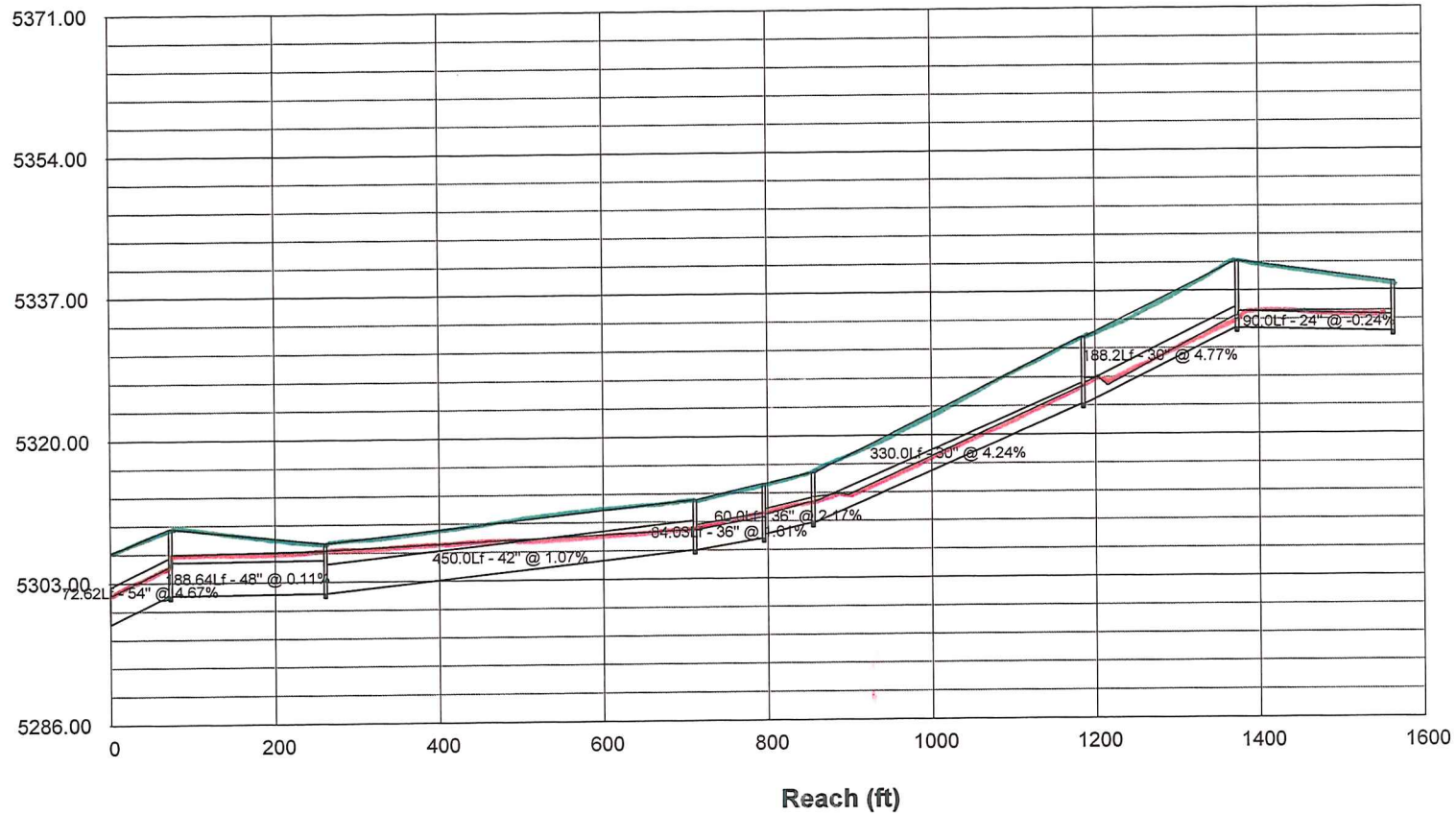
Run Date: 01-17-2007

Notes: * Normal depth assumed.; ** Critical depth.; j-Line contains hyd. jump.

Storm Sewer Profile

Proj. file: ONSITE LA CUENTISTA II-SD_W_UNIT II.stm

Elev. (ft)



Storm Sewer Summary Report

Page 1

Line No.	Line ID	Flow rate (cfs)	Line size (in)	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line slope (%)	HGL down (ft)	HGL up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns line No.
1		142.0	54 c	72.6	5298.00	5301.39	4.668	5301.42	5304.81	1.83	5304.81	End
2		63.00	48 c	188.6	5301.39	5301.59	0.106	5306.28*	5306.65*	0.06	5306.71	1
3		63.00	42 c	450.0	5301.59	5306.42	1.073	5306.71	5308.85	0.18	5308.85	2
4		63.00	36 c	84.0	5306.42	5307.77	1.607	5308.85	5310.30	n/a	5310.30	3
5		63.00	36 c	60.0	5308.27	5309.57	2.166	5310.59	5312.10	n/a	5312.10	4
6		39.00	30 c	330.0	5309.57	5323.56	4.239	5312.64	5325.65	n/a	5325.65	5
7		10.00	24 c	364.6	5323.56	5324.17	0.167	5326.72*	5327.44*	0.16	5327.59	6
8		18.00	30 c	188.2	5323.56	5332.53	4.766	5326.67	5333.95	n/a	5333.95	6
9		16.00	24 c	332.2	5332.53	5333.00	0.142	5334.53*	5336.19*	0.40	5336.60	8
10		2.00	24 c	190.0	5332.53	5332.07	-0.242	5334.55*	5334.57*	0.01	5334.57	8
LA CUENTISTA UNIT II - SD							Number of lines: 10			Run Date: 01-17-2007		
NOTES: c = cir; e = ellip; b = box; Return period = 100 Yrs. ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump.												

**Drainage Report
ADDENDUM
for
LA CUENTISTA
SUBDIVISION, UNIT II**

DECEMBER 2014

**Addendum to
Drainage report for
La Cuentista
Subdivision Unit II
January 2007**

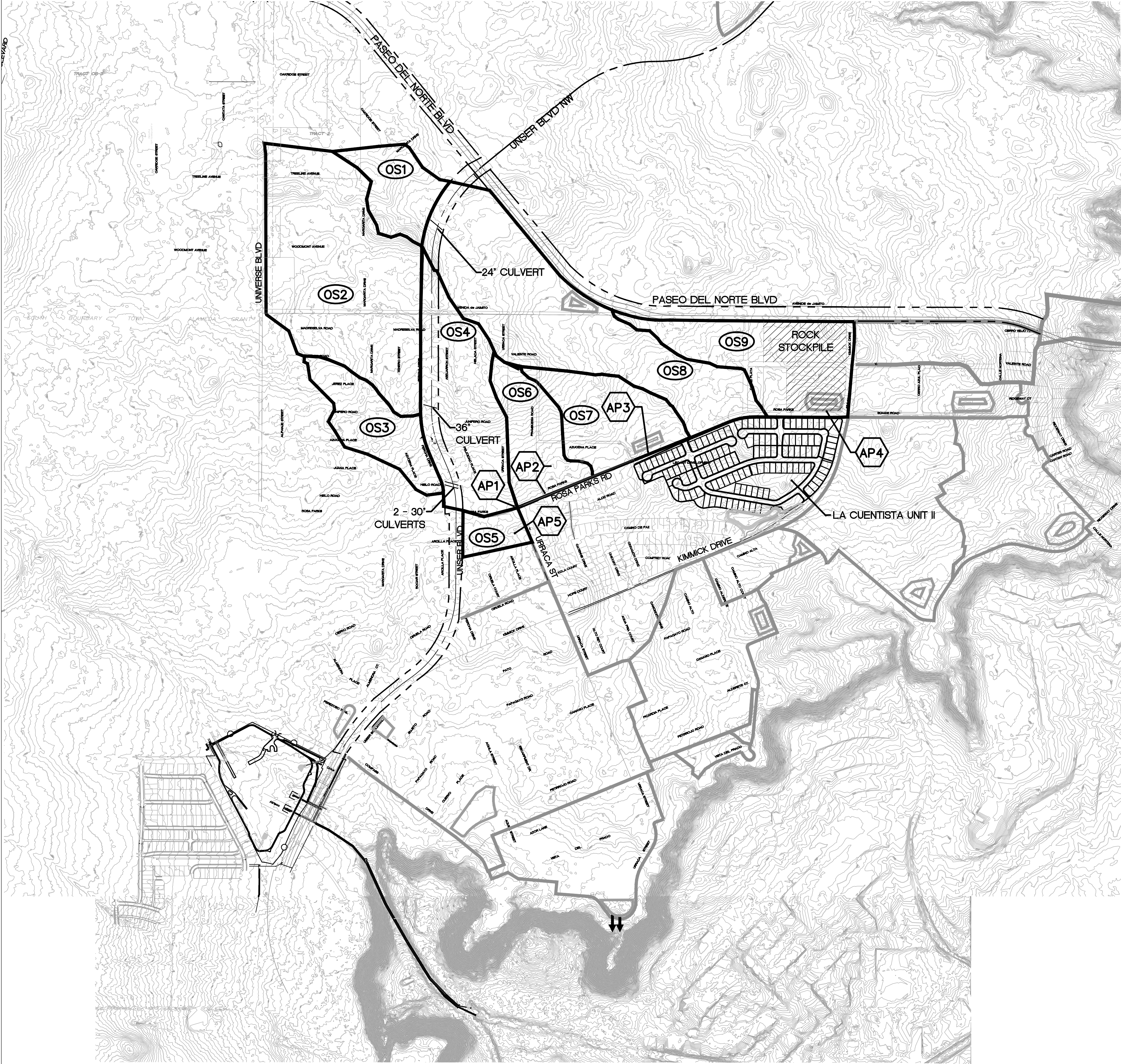
**A Supplement to the
Drainage Report for
La Cuentista Subdivision
Date: November 2003**

Prepared by:

**Wilson & Company, Inc.
4900 Lang Avenue NE
Albuquerque, New Mexico 87109
(505) 348-4000
(505) 348-4072**

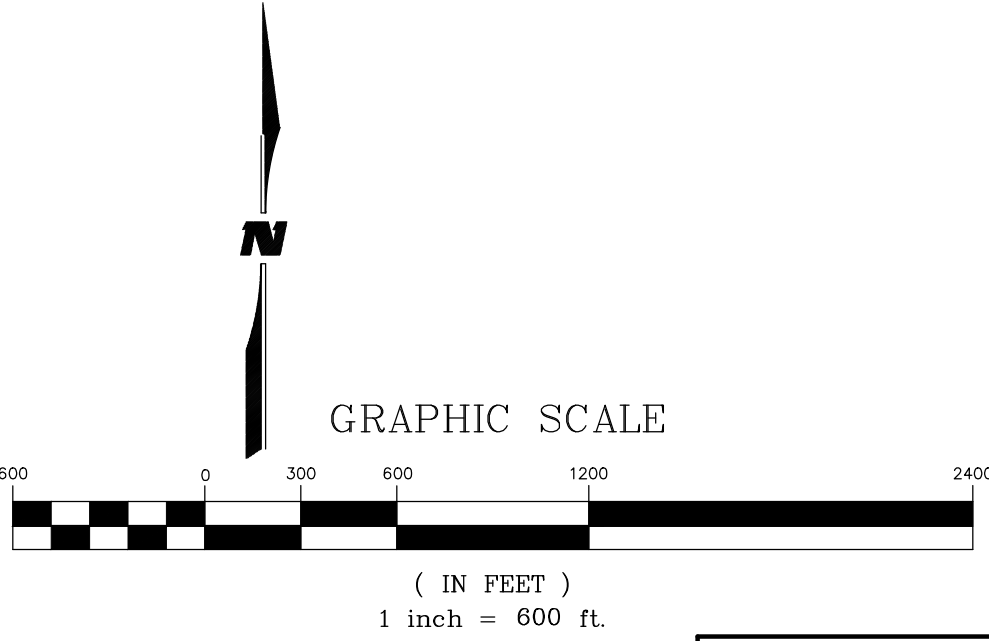
December 2014

Wilson & Company File No: 14-600-089-00



ANALYSIS POINT	FLOW (CFS)
AP1	100
AP2	24
AP3	30
AP4	99
AP5	7

	AREA (Acres)	LT A (%)	LT B (%)	LT C (%)	LT D (%)	Q (cfs)	V (fps)
OS1	14.74 ±	90	0	10	0	18	0.52
OS2	73.15 ±	90	0	10	0	59	2.59
OS3	19.00 ±	90	0	10	0	20	0.67
OS4	38.80 ±	80	0	10	10	55	1.87
OS5	5.91 ±	90	0	10	0	7.0	0.21
OS6	18.80 ±	90	0	10	0	24	0.67
OS7	24.56 ±	90	0	10	0	30	0.87
OS8	71.77 ±	86	0	10	4	52	2.91
OS9	33.91 ±	45	0	55	0	54	1.75



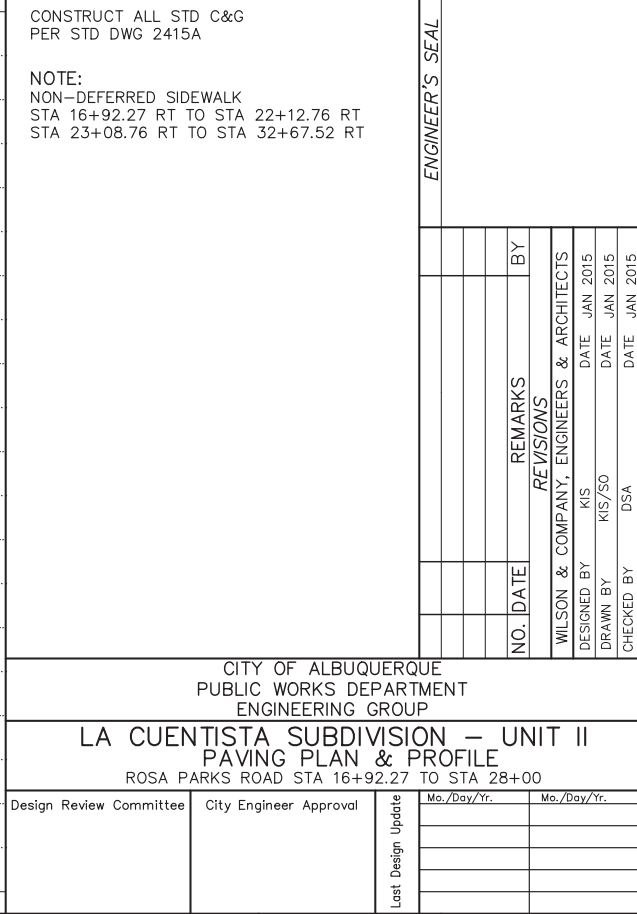
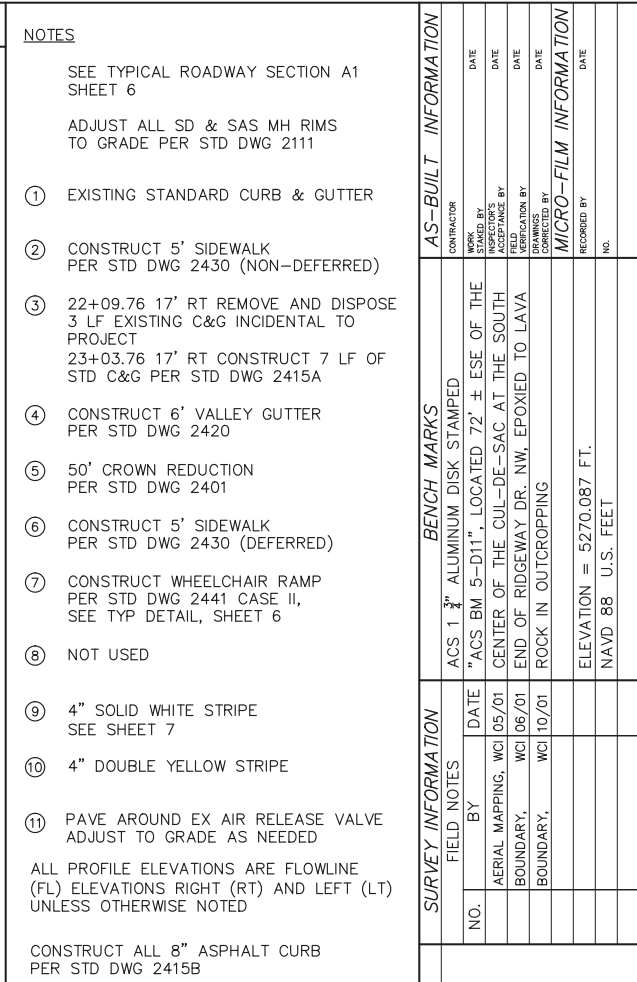
WILSON & COMPANY 4900 LANG AVE NE ALBUQUERQUE, NEW MEXICO 87109 PH (505) 348-4000 FAX (505) 348-4072 www.wilsonco.com	CITY OF ALBUQUERQUE PUBLIC WORKS DEPARTMENT ENGINEERING GROUP		
	LA CUENTISTA UNIT II DRAINAGE REPORT ADDENDUM		
	EXISTING CONDITIONS MAP		
	CPN 709786	DRAWN: KIS DESIGN: DSA	PLATE 1

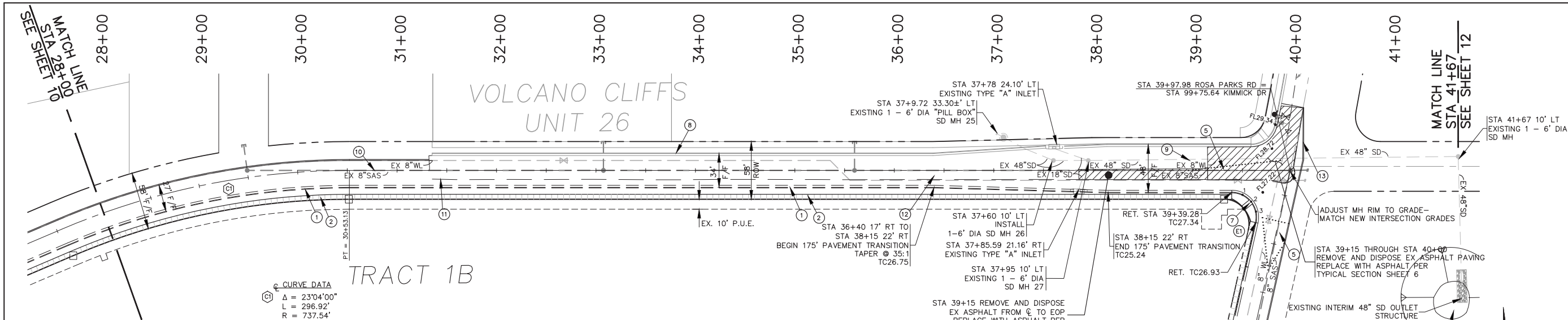
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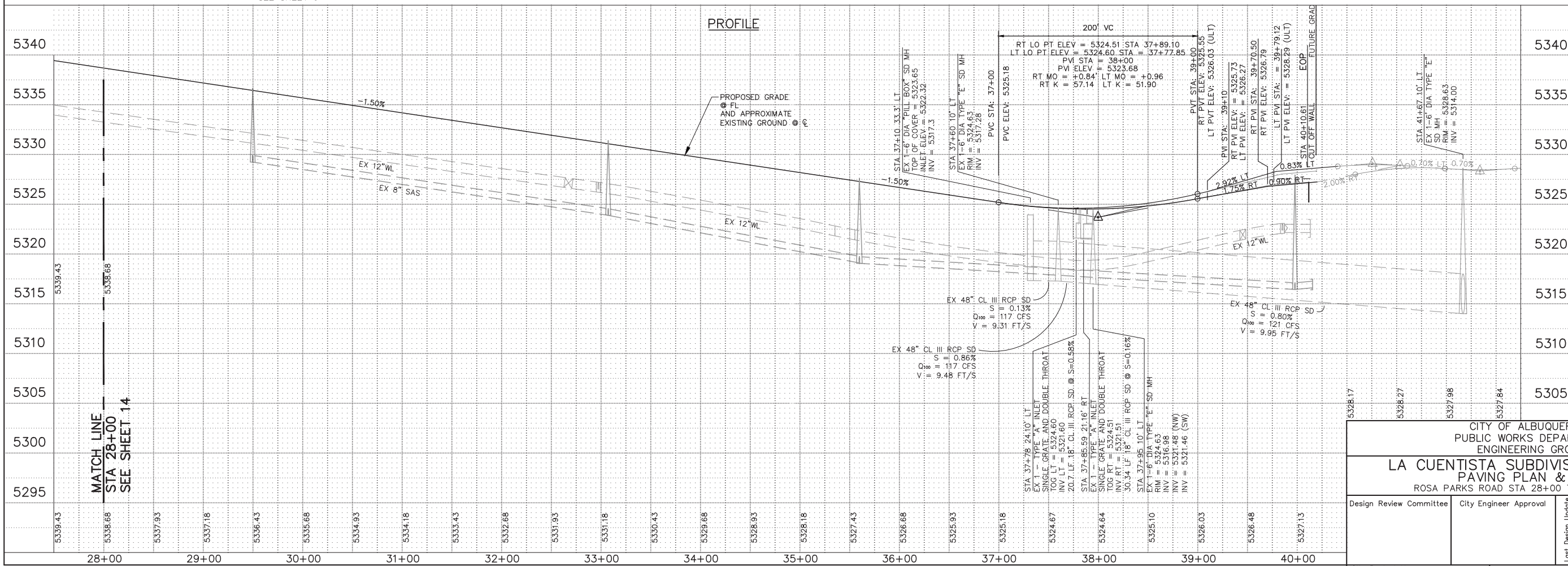
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COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1 NOTATION
START										TIME= .00
RAINFALL TYPE= 1										RAIN6= 2.170
COMPUTE NM HYD	2.00	-	2	.11430	59.22	2.594	.42560	1.600	.810	PER IMP= .00
COMPUTE NM HYD	3.00	-	3	.02970	20.39	.674	.42560	1.533	1.073	PER IMP= .00
*S ADD BASINS OS2 AND OS3										
ADD HYD	OS3.1	3& 2	32	.14400	77.99	3.269	.42560	1.600	.846	
*S*** ROUTE BASINS OS2 AND OS3 THRU BASIN OS4										
ROUTE MCUNGE	33.10	32	33	.14400	76.86	3.252	.42344	1.767	.834	CCODE = .1
COMPUTE NM HYD	4.00	-	4	.06060	55.34	1.869	.57839	1.533	1.427	PER IMP= 10.00
*S*** ADD BASIN OS4 - ANALYSIS POINT 1										
ADD HYD	OS4.1	4&33	3	.20460	100.11	5.121	.46933	1.733	.764	
*S*** - ANALYSIS POINT 2										
COMPUTE NM HYD	6.00	-	6	.02938	23.78	.667	.42560	1.533	1.265	PER IMP= .00
*S*** - ANALYSIS POINT 3										
COMPUTE NM HYD	7.00	-	7	.03838	30.45	.871	.42560	1.533	1.240	PER IMP= .00
COMPUTE NM HYD	1.00	-	1	.02300	17.71	.522	.42560	1.533	1.203	PER IMP= .00
*S*** ROUTE BASINS OS1 THRU BASIN OS8										
ROUTE MCUNGE	OS8	1	5	.02300	16.00	.502	.40952	2.633	1.087	CCODE = .1
COMPUTE NM HYD	108.00	-	8	.11220	51.85	2.912	.48671	1.667	.722	PER IMP= 4.00
*S*ADD BASIN OS1 AND OS8										
ADD HYD	OS8.1	5& 8	1	.13520	51.85	3.415	.47358	1.667	.599	
*S										
COMPUTE NM HYD	9.00	-	2	.05300	53.70	1.750	.61924	1.533	1.583	PER IMP= .00
*S*ADD BASIN OS1, OS8 AND OS9 -ANALYSIS POINT 4										
ADD HYD	OS9.1	1& 2	3	.18820	98.66	5.165	.51460	1.600	.819	
*S*** - ANALYSIS POINT 5										
COMPUTE NM HYD	5.00	-	5	.00920	7.45	.209	.42560	1.533	1.266	PER IMP= .00
FINISH										





- NOTES**
- SEE TYPICAL ROADWAY SECTION A1-A3 SHEET 6
- ADJUST ALL SD & SAS MH RIMS TO GRADE PER STD DWG 2111
- 1 EXISTING STANDARD CURB & GUTTER
- 2 CONSTRUCT 5' SIDEWALK PER STD DWG 2430 (NON-DEFERRED)
- 3 CONSTRUCT WHEELCHAIR RAMP PER DTL SHEET 6
- 4 CONSTRUCT 12" VALLEY GUTTER PER STD DWG 2420
- 5 50' CROWN REDUCTION PER STD DWG 2401
- 6 CONSTRUCT 5' SIDEWALK PER STD DWG 2430 (DEFERRED)
- 7 CONSTRUCT WHEELCHAIR RAMP PER STD DWG 2441 CASE II, SEE DTL SHEET 6
- 8 EX C&G, SW, PAVING - SAD 228
- 9 4" SOLID WHITE STRIPE SEE SHEET 6
- 10 4" DOUBLE YELLOW STRIPE SEE SHEET 6
- 11 STA 31+35 BEGIN SECTION A2, SAWCUT 1' FROM EX EOP REMOVE AND DISPOSE EX PAVING NEW PAVING TO MATCH EX PAVING ELEVATION
- 12 STA 36+40 BEGIN SECTION A3 SAWCUT 1' FROM EX EOP REMOVE AND DISPOSE EX PAVING NEW PAVING TO MATCH EX PAVING ELEVATION
- 13 TRANSITION EOP TO MATCH KIMMICK DR EOP NORTH OF ROSA PARKS RD
- ALL PROFILE ELEVATIONS ARE FLOWLINE (FL) ELEVATIONS RIGHT (RT) AND LEFT (LT) UNLESS OTHERWISE NOTED
- ROSA PARKS RD PLAN**
- TRAFFIC DATA**
- | TC | FL |
|---------|-------|
| 1 27.24 | 27.57 |
| 2 - | 26.96 |
| 3 27.03 | 26.36 |
- $\Delta = 102'38''00''$
 $L = 44.78'$
 $R = 25.00'$
- NOTE:**
NON-DEFERRED SIDEWALK
STA 33+63.52 RT TO STA 39+45.52 RT
- SCALE:**
HORIZ: 1" = 50'
VERT: 1" = 5'



SECTION - UNIT II PROFILE TO STA 39+97.98									
ROUTE INSTRUMENT DUP									
REVISIONS									
WILSON & COMPANY, ENGINEERS & ARCHITECTS									
DESIGNED BY KIS DATE DEC 2004									
DRAWN BY VKL DATE DEC 2004									
CHECKED BY DSA DATE DEC 2004									
Mo./Day/Yr.									
Mo./Day/Yr.									
Mo./Day/Yr.									
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CITY OF ALBUQUERQUE
PUBLIC WORKS DEPARTMENT
ENGINEERING GROUP

LA CUENTISTA SUBDIVISION - UNIT II
PAVING PLAN & PROFILE
ROSA PARKS ROAD STA 28+00 TO STA 39+97.98

Design Review Committee	City Engineer Approval	Mo./Day/Yr.	Mo./Day/Yr.

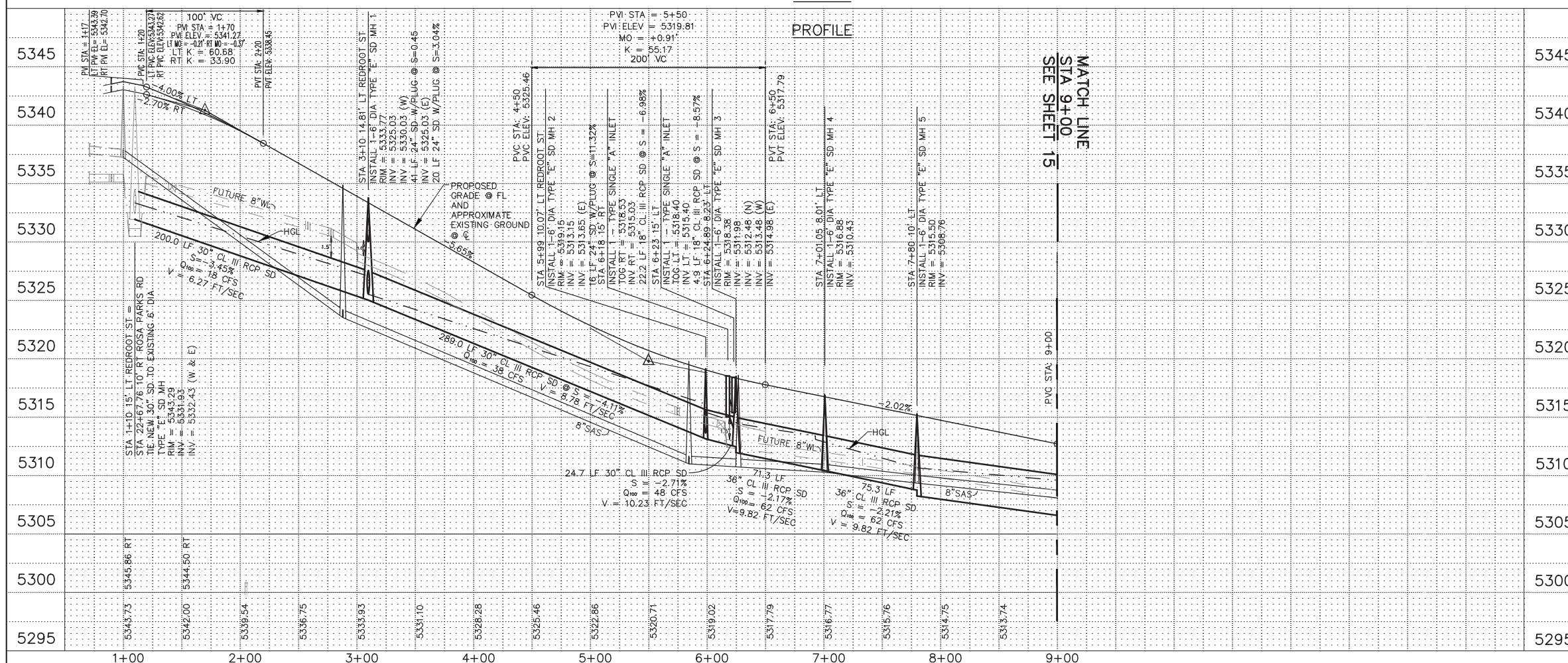
City Project No. 709786

Zone Map No. C-10, C-11

Drawing 11

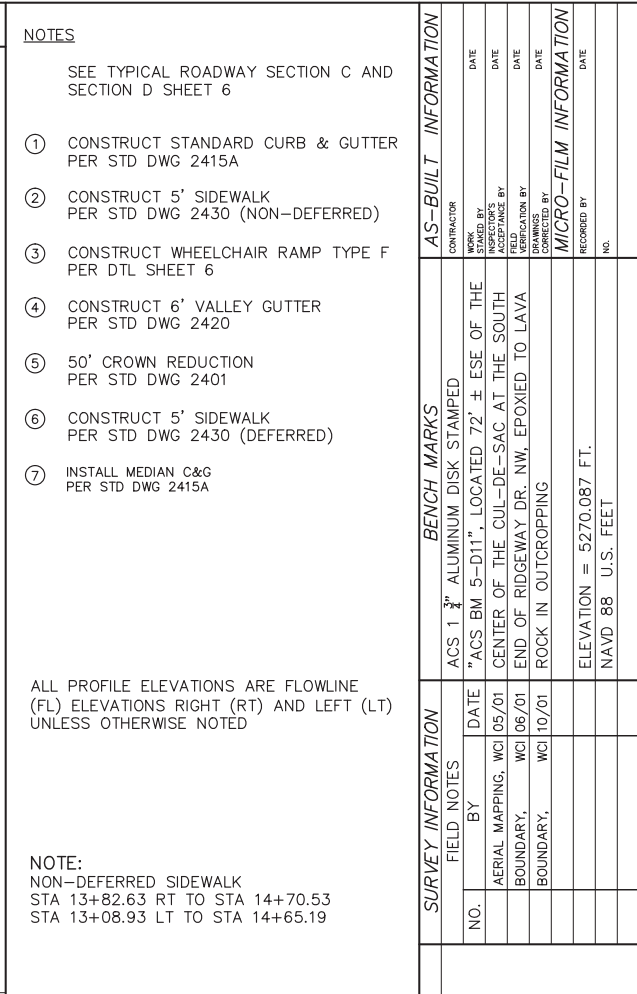
Sheet 17





ALL PROFILE ELEVATIONS ARE FLOWLINE
(FL) ELEVATIONS RIGHT (RT) AND LEFT (LT)
UNLESS OTHERWISE NOTED

CITY OF ALBUQUERQUE									
PUBLIC WORKS DEPARTMENT									
ENGINEERING GROUP									
LA CUENTISTA SUBDIVISION – UNIT II									
PAVING PLAN & PROFILE									
REDROOT STREET STA 1+00 TO STA 9+00									
Design Review Committee		City Engineer Approval		Last Design Update	Mo./Day/Yr.		Mo./Day/Yr.		
City Project No.		Zone Map No.		Drawing		Sheet			
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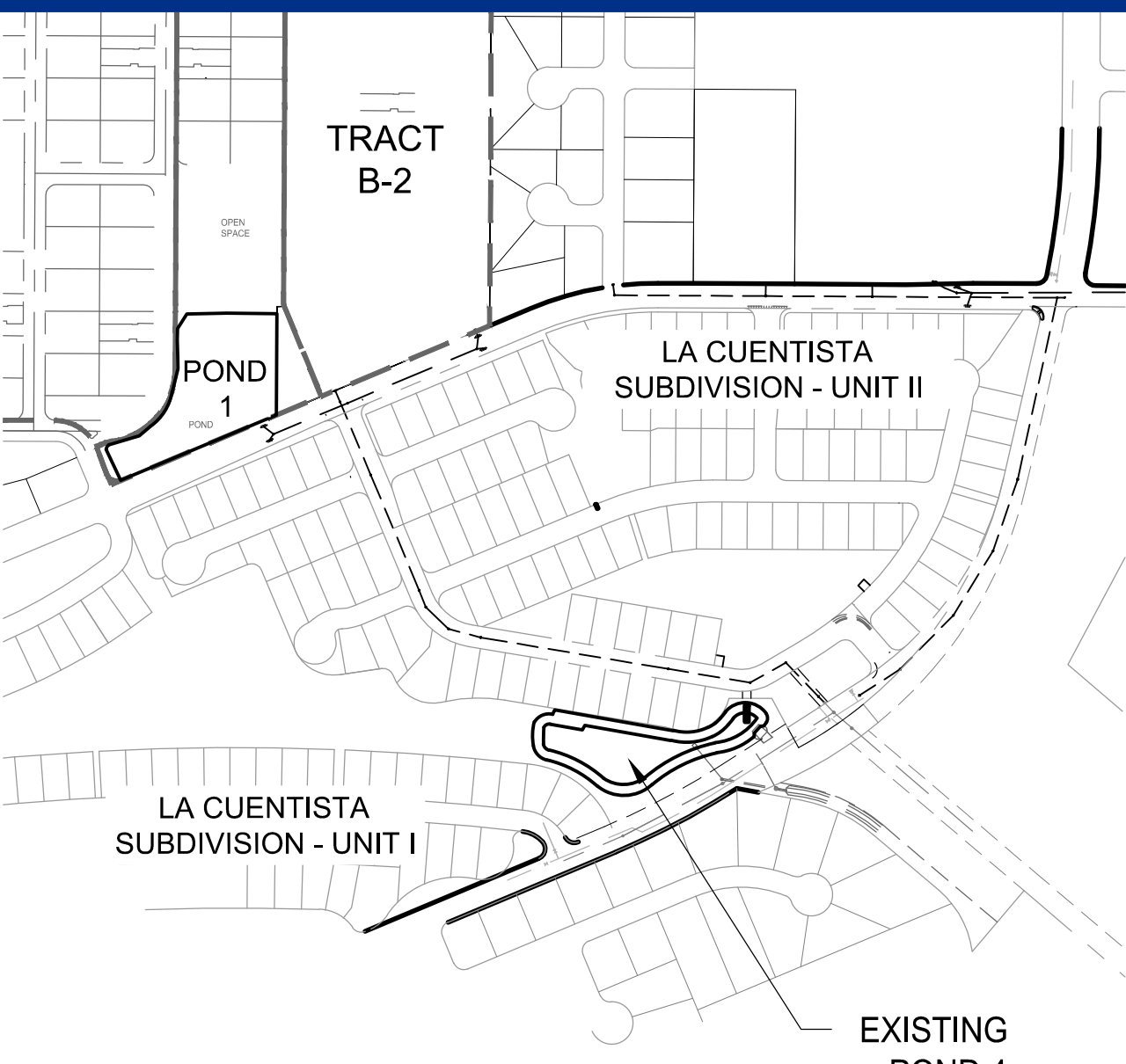
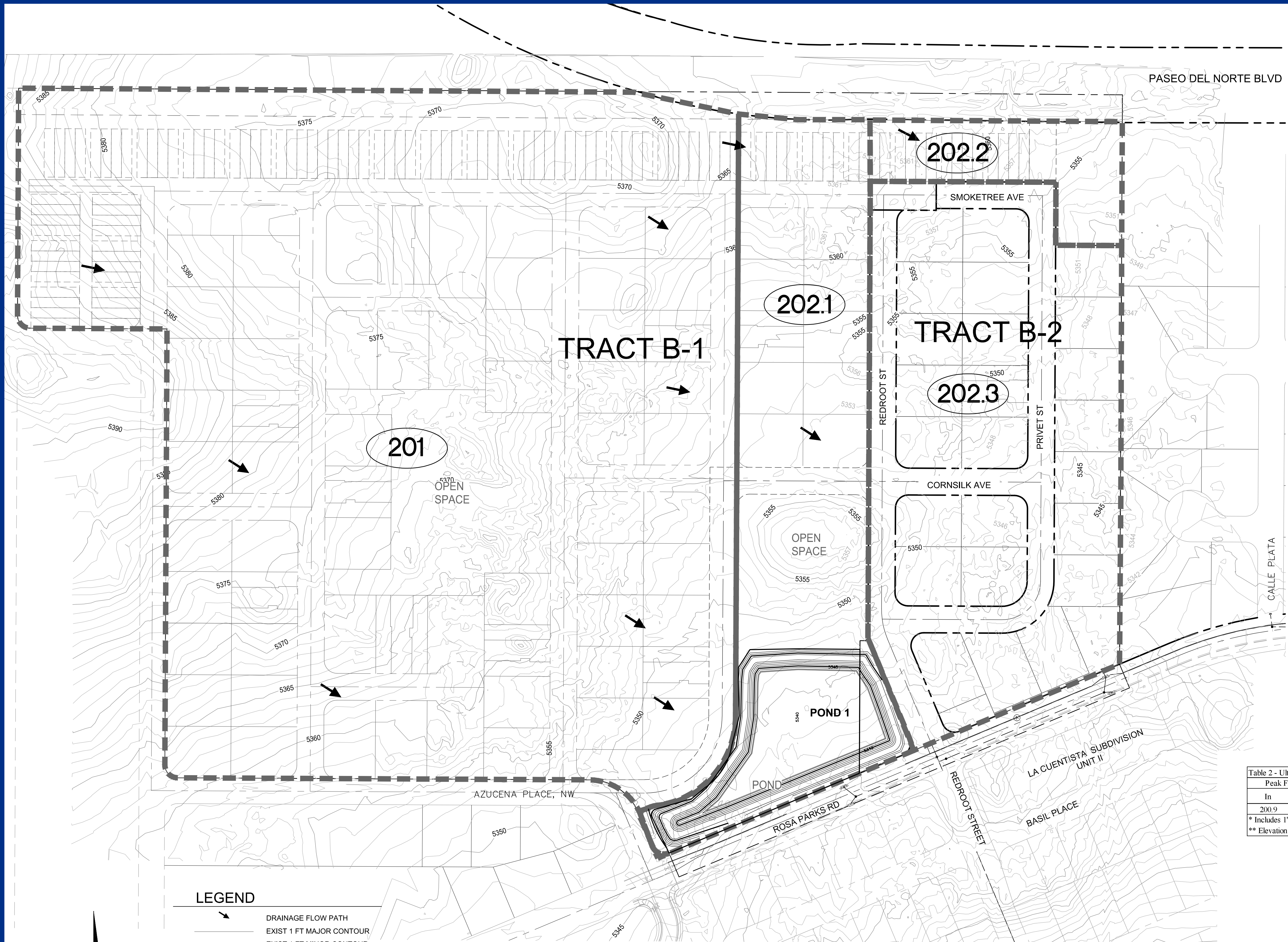


Appendix E

Plates/Plan

- Plate 1 – Ultimate Conditions Drainage Basin Map
- Plate 2 – Developed Conditions Drainage Basin Map
- Grading & Drainage Plan

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OVERALL DRAINAGE MAP

Table 1 - Ultimate Conditions AHYMO Results, 100-Yr, 24-Hr				
Basin ID	Area		Peak Flow	Volume
	ac	sq mi	cfs	ac-ft
201.00	36.97	0.06	129	5.7
202.10	8.43	0.01	27	1.1
202.20	1.69	0.00	6	0.3
202.30	11.01	0.02	38	1.7

Table 2 - Ultimate Conditions Pond Data						
Peak Flow (cfs)		Pond Elevation (ft)		Volume (ac-ft)		ft
In	Out	Top*	Bottom**	Req'd	Prv'd	Max WSEL
200.9	15.5	5344	5336.5	5.97	9.48	5341.61

* Includes 1' freeboard
** Elevation 5337.0 to 5336.5 is provided for the first flush volume

LEGEND

- DRAINAGE FLOW PATH
- EXIST 1 FT MAJOR CONTOUR
- EXIST 1 FT MINOR CONTOUR
- BASIN BOUNDARY LINE

201

BASIN ID

NOTE:
TRACT B-1 LAYOUT IS CONCEPTUAL AND SHOWN
FOR INFORMATION ONLY.

PLATE 1 - ULTIMATE CONDITIONS DRAINAGE MAP
LA CUENTISTA SUBDIVISION, TRACTS B-1 AND B-2

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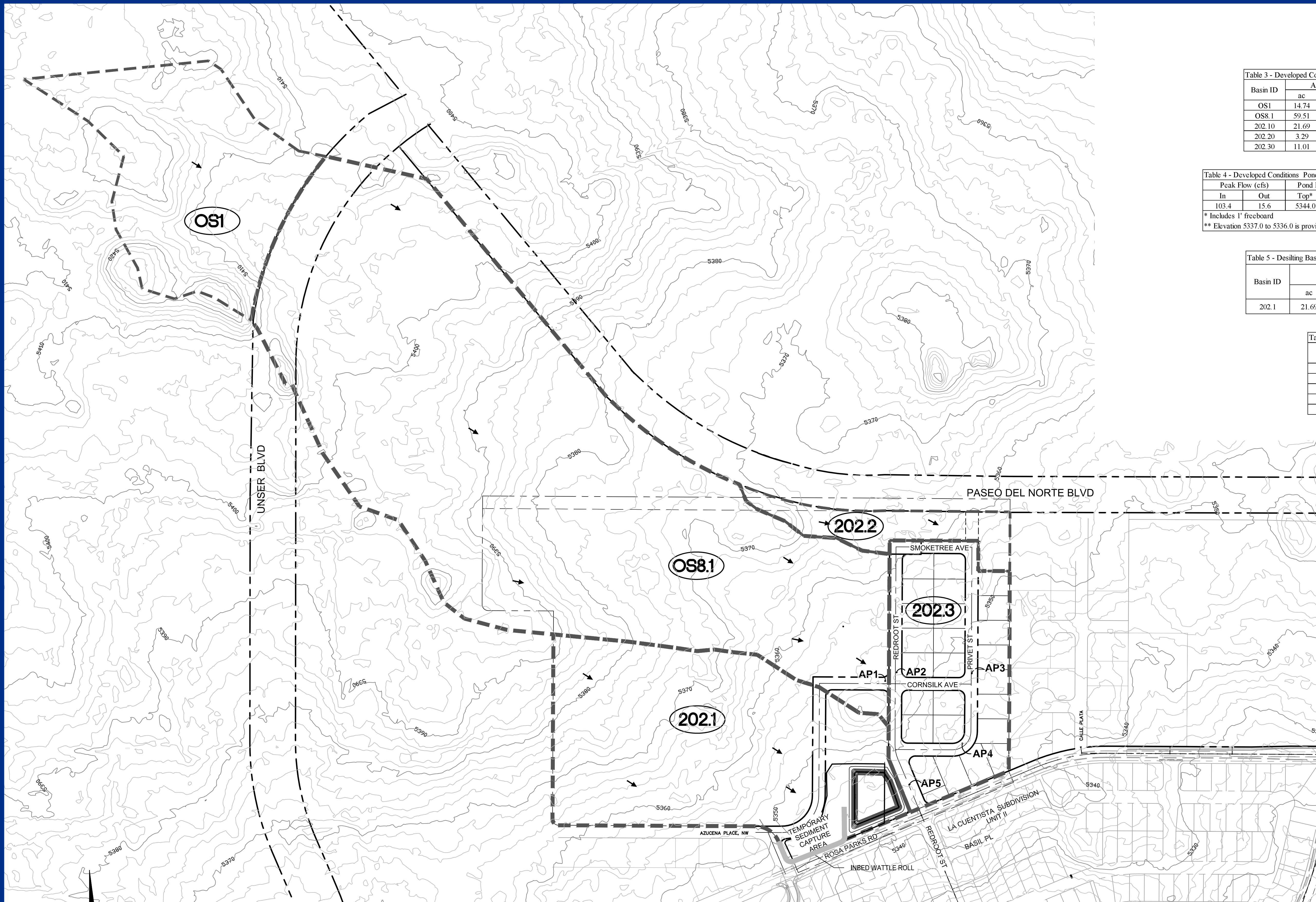
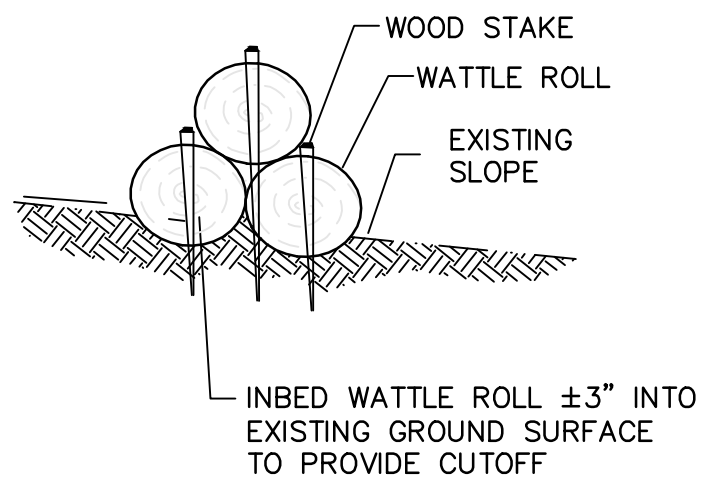


Table 3 - Developed Condition AHYMO Results, 100-Yr, 24-Hr					
Basin ID	Area		Peak Flow	Volume	
	ac	sq mi	cfs	ac-ft	
OS1	14.74	0.02	17	0.5	
OS8.1	59.51	0.09	46	2.5	
202.10	21.69	0.03	27	0.8	
202.20	3.29	0.01	4	0.1	
202.30	11.01	0.02	38	1.7	

Table 4 - Developed Conditions Pond Data						
Peak Flow (cfs)		Pond Elevation (ft)		Volume (ac-ft)		Max WSEL
In	Out	Top*	Bottom**	Req'd	Prv'd	(ft)
103.4	15.6	5344.0	5336.00	3.4	5.28	5341.66
* Includes 1' freeboard						
** Elevation 5337.0 to 5336.0 is provided for the first flush volume						

Table 5 - Desilting Basin Data				
Basin ID	Area		Peak Flow	Runoff Volume
	ac	sq mi	cfs	ac-ft
202.1	21.69	0.034	1	0.07

Table 6 - Analysis Point	
AP	Peak Flow (cfs)
AP1	46
AP2	8
AP3	14
AP4	12
AP5	85



WATTLE ROLL DETAIL
SCALE: 1" = 2'

LEGEND	
	DRAINAGE FLOW PATH
	EXIST 1 FT MAJOR CONTOUR
	EXIST 1 FT MINOR CONTOUR
	BASIN BOUNDARY LINE
	BASIN ID
	ANALYSIS POINT

PLATE 2 - DEVELOPED CONDITIONS DRAINAGE MAP
LA CUENTISTA SUBDIVISION, TRACT B-2

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