

DRAINAGE INFORMATION SHEET

C-12/01D

PROJECT TITLE: PRIDIERIDGE, UNIT #4 ZONE ATLAS/DRAINAGE FILE # ~~812~~LEGAL DESCRIPTION: RIVERVIEW PARCEL H-21, H-22CITY ADDRESS: N/AENGINEERING FIRM: COMMUNITY SCIENCES CORP. CONTACT: MIKE YOSTADDRESS: Box 1328, CORRALES, NM, 87048 PHONE: 897-0000OWNER: BELLMAN COMMUNITY DEVELOPMENT CONTACT: BOB RYALSADDRESS: Box 3300, ALBUQUERQUE, NM, 87190 PHONE: 884-6606ARCHITECT: N/A CONTACT: _____

ADDRESS: _____ PHONE: _____

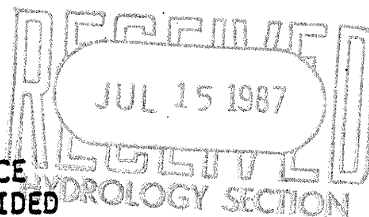
SURVEYOR: SAME AS ENGINEER CONTACT: SKIP CARLETON

ADDRESS: _____ PHONE: _____

CONTRACTOR: N/A CONTACT: _____

ADDRESS: _____ PHONE: _____

PRE-DESIGN MEETING:

☐ YES☒ NO☐ COPY OF CONFERENCE
RECAP SHEET PROVIDEDDRB NO. 87-437

EPC NO. _____

PROJECT NO. 3314

TYPE OF SUBMITTAL:

☐ DRAINAGE REPORT☐ DRAINAGE PLAN☐ CONCEPTUAL GRADING & DRAIN PLAN☒ GRADING PLAN☒ EROSION CONTROL PLAN☐ ENGINEER'S CERTIFICATION

CHECK TYPE OF APPROVAL SOUGHT:

☐ SECTOR PLAN APPROVAL☐ SKETCH PLAT APPROVAL☐ PRELIMINARY PLAT APPROVAL☐ SITE DEVELOPMENT PLAN APPROVAL☐ FINAL PLAT APPROVAL☐ BUILDING PERMIT APPROVAL☐ FOUNDATION PERMIT APPROVAL☐ CERTIFICATE OF OCCUPANCY
APPROVAL☐ ROUGH GRADING PERMIT APPROVAL☐ GRADING/PAVING PERMIT APPROVAL☒ OTHER FINAL GRADING (SPECIFY)
FOR W.O.DATE SUBMITTED: 7/15/87BY: Michael J. Yost

FILE COPY



City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

MAYOR
KEN SCHULTZ

CHIEF
ADMINISTRATIVE OFFICER

GENE ROMO

DEPUTY CAO
PUBLIC SERVICES

FRANK MARTINEZ

DEPUTY CAO
PLANNING/DEVELOPMENT

BILL MUELLER

March 23, 1988

Mike Yost, P.E.
Community Sciences Corporation
Post Office Box 1328
Corrales, New Mexico 87058

RE: REVISED PLATE 2 OF THE DRAINAGE MANAGEMENT PLAN FOR PRAIRIE
RIDGE UNIT 5, SUBMITTED 26 FEB 88 FOR PRELIMINARY PLAT APPROVAL
(C12/D1D)

Dear Mr. Yost:

I have reviewed your submittal with the added 30' drainage easement cross-section, and it is satisfactory. Would you, at your convenience, kindly change the latest revision date to "2/26/88" from "2/26/87"?

With the exception of the letter from Open Space giving the developer permission to use Tract A as an emergency overflow area, and the revision date mentioned above, I think we have all of the items we require for us to sign the final plat.

Thank you for your cooperation.

If you have any questions, please call me at 768.2650.

Cordially,

G. Stuart Reeder, P.E.
C.E./Hydrology Section

GSR/bsj

DRAINAGE MANAGEMENT PLAN

FOR

PRAIRIE RIDGE, UNITS 4 AND 5

PREPARED FOR:

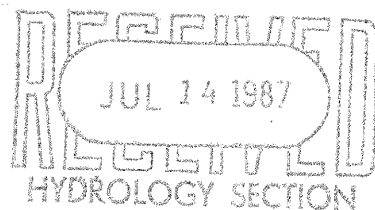
BELLAMAH COMMUNITY DEVELOPMENT

PREPARED BY:

COMMUNITY SCIENCES CORPORATION

MAY, 1987

REVISED JULY, 1987



Michael J. Yost 7/13/87
MICHAEL J. YOST, P.E.



SURVEYING
ENGINEERING
LAND PLANNING

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May, 1987

A) Purpose and Scope

Bellamah Community Development is currently planning development of their 56 acre Prairie Ridge Subdivision, Units 4 and 5, in northwest Albuquerque. The Development will consist of approximately 221 R1 lots intended for the tract housing market. The purpose of this report is to present an overall drainage management plan for the project which is based on sound engineering practice and which is acceptable to both the City of Albuquerque and the Albuquerque Metropolitan Arroyo Flood Control Authority.

Development of Prairie Ridge, Unit 4 is to commence immediately. Development of Prairie Ridge, Unit 5 will begin somewhat later. It is for this reason certain interim measures for this phasing of development are specified in this report.

This report presents a site-specific drainage plan for Prairie Ridge, Units 4 and 5. Offsite drainage basins and master plan drainage facilities are discussed in length in the "Riverview Master Drainage Plan" by Community Sciences Corporation, November, 1985, and "Drainage Management Plan for Shenandoah Unit II and III" by Community Sciences Corporation, December, 1985.

May, 1987

B) Site Location and Topography

Prairie Ridge, Units 4 and 5 is located in parcel H-21 and H-22, Riverview Subdivision. The area is bounded on the east by proposed Golf Course Road, on the north by proposed Butterfield Trail Street, on the west by existing the Homestead Hills East and the Homestead Hills North Subdivisions, on the south by future Homestead Trail Street, as shown on Plate 1. The parcel tends to slope in a southwest to northeast direction.

Soils are primarily gravelly sands and silts falling into the SCS soils hydrologic group B.

C) Design Criteria

1) Engineering Parameters

In accordance with AMAFCA and City of Albuquerque Drainage Criteria all hydrological analysis based on the 100 year frequency - 6 hour duration storm as represented in the NOAA atlas for New Mexico. The rainfall values pertinent to the study are as follows:

	<u>10 Year</u>	<u>100 Year</u>
One Hour	1.25"	1.9"
Six Hour	1.45"	2.2"

May, 1987

? WHERE FROM?
CALCULATIONS?

@ 0.133 AC LOTS
(7.5 LOTS/AC), 9% IMPERV.
2.65% , 4.25% 85 (SOL)
6.4% (2)

A fraction impervious of 0.57 was selected for the project based on proposed, typical lots, and a curve number of 70 was selected for the previous areas. Developed offsite watersheds were assigned a fraction impervious as specified in the Riverview Master Drainage Plan, and a curve number of 75 was selected for these areas. The proposed open space (Tract A) was assigned a fraction impervious of 0.02.

2) Flood Control Regulations

The drainage plan presented in this report has been designed to comply with the current City of Albuquerque Drainage Ordinance and associated technical criteria as published in the Development Process Manual. The key elements of the ordinance are as follows:

- 1) Street flow depths may not exceed a value of 0.2 feet above top of curb for any location for a 100 year event.
- 2) The product of depth and velocity must be less than or equal to 6.5 for the 10 year event.

D) Computational Procedures

The analysis approach utilized follows standard engineering practice. Key points of confluence were selected, and subsequently the associated individual and aggregate contributing basins were defined.

May, 1987

Hydrological computations were accomplished by means of our MODSCS Computer model. This model is based upon the Soil Conservation Service Triangular unit hydrograph method, but the method has been modified to be more applicable to developed watershed conditions. The model avoids the common pitfall of grappling for an appropriate developed curve number by including percent impervious as an input variable. This fraction of the watershed is then modeled at a curve number of 95. An assigned curve number is applied to the balance of the watershed, and the runoffs are combined to yield the composite hydrograph. In addition the model has the capacity to route hydrographs through reservoirs and channels, or to translate hydrographs in time for summation with other sub-basins.

Times of concentration were estimated by using a combination of approximated street flow velocities and overland flow velocities (as applicable) from the upper subcatchment reaches to the confluence point of interest. A convenient formula for overland flow velocity takes the form:

$$v = KY^{0.5}$$

where V = overland flow velocity

Y = average ground slope in percent

K = a ground cover factor

Street velocities were estimated by use of the Manning equation for uniform flow.

May, 1987

All the characteristic hydrological parameters for each subcatchment of interest and each key point of confluence are contained in Appendix A as part of the computer model output, and a summary of parameters and peak flow rates ^{is} ~~are~~ given in Table 1.

Following hydrological modeling street flow characteristics were analyzed by various methods. For uniform flow conditions the Manning equation with a roughness factor of 0.017 was used. At intersections the worst ^{of} two conditions was considered; the theoretical hydraulic jump depth for upstream flow conditions, and the theoretical pool depth to accelerate the flow to the normal, downstream conditions. The higher value was assumed to be the potential flood depth. It should be noted that this approach is valid only for incoming supercritical flow conditions at tee intersections. Subcritical flow conditions are not considered problematic at intersections unless normal flow depth is above required limits.

E) Offsite Drainage

The storm flows from the Shenandoah Units 1, 2 and 3 subdivisions, along with local flows from Taylor Ranch Drive are to be discharged into the South Branch of the Piedras Marcadas Arroyo west of the project site. These flows will be combined the storm flows from portions of Homestead Hills East and Homestead Hills North, designated as HHE2 and HHN2 respectively

May, 1987

in the Riverview Master Drainage Plan. It is proposed these flows be collected in a storm sewer system at the western boundary of the project site, conveyed through the site, and discharged back into the South Branch of the Piedras Marcadas Arroyo just east of the Golf Course Road right-of-way (see Plate 2). The MODSCS output for this hydrological routing is included in Appendix C of this report.

A portion of Homestead Hills North Drains on to proposed Butterfield Trail at the northwest corner of the project site. This drainage basin was designated HHNI in the Riverview Master Drainage Plan. These flows are combined with the flows from Riverview Basins L and M and are to be collected in catch basins at the northeast corner of the site before discharge into the South Branch of the Piedras Marcadas Arroyo.

Points C1, GCR

F) Onsite Drainage

Plate 2 illustrates the various drainage basins which are internal to the project site.

Basins A1 through A4 are to drain into a catch basin and directed into the storm sewer that is to be placed through the project site.

*No basins B1-B4
EXISTING ARE B5-B8*

~~Basin B1~~ through B8 are to drain into a catch basin and are also to be directed into the aforementioned storm sewer.

May, 1987

Basin C1 drains storm flows from the southern portion of Prairie Ridge Unit 4 and the northern portion of Prairie Ridge Unit 3.

The proposed open space (Tract A) is designated drainage basin D10. This basin also includes the backyards of the proposed lots along the east and north edge of the project site.

Table 1 summarizes the input to, and results of the hydrological analysis. Tables 2 and 3 show the hydraulic analysis of street flow characteristics at key conveyance points and intersections respectively.

G) Erosion Control

Control of excessive soil erosion into City Streets and drainage improvements during construction will be accomplished by use of temporary lot line, water-trap berms. These will be windrowed into place following mass grading operations and left in place until each home is constructed and sold. Plate 2 illustrates the dimensions of these berms, and they will be located along those boundaries of each lot which are common to City rights of way or public easement.

TABLE 1
HYDROLOGICAL FLOW PARAMETERS

AREA/ POINT DESIGNATION	AREA (SQ. MI.)	AREAS CONTRIBUTING	GROSS AREA (SQ. MI.)	FRACTION IMPERVIOUS	CN (PERVIOUS)	TC (MINUTES)	Q10 R(1)= 1.25" R(6)= 1.45"	Q100 R(1)= 1.9" R(6)= 2.2"	REMARKS
A1	0.01442	A1	0.01442	0.57	70	9	12.7	23.5	
A2	0.00700	A2	0.00700	0.57	70	7	8.2	11.4	
A3	0.00542	A3	0.00542	0.57	70	8	4.8	8.8	
A4	0.00624	A1-4	0.02746	0.57	70	9	24.3	44.7	
B5	0.00839	B5	0.00839	0.57	70	10	8.3	15.3	
B6	0.00581	B6	0.00581	0.57	70	8	5.0	9.1	
B7	0.00555	B5-7	0.02055	0.57	70	15	14.5	28.7	
B8	0.01025	B8	0.01025	0.57	70	11	8.1	15.0	
B5-8	0.03660	B5-8	0.03660	0.57	70	15	-	40.1	
D10	0.01885	D10	0.01885	0.02	70	17	-	8.8	
C1	0.01590	C1	0.01590	0.57	70	10	-	25.8	SEE DRAINAGE MANAGEMENT PLAN FOR PRAIRIE RIDGE III BY CSC MAY, 1986
SHEN 263	0.1158	SHEN 263	0.1158	0.288	75.5	14	-	131.8	SEE DRAINAGE PLAN FOR SHENANDDAH 2 & 3 BY CSC, DECEMBER, 1985.
SHEN 1	0.0269	SHEN 263	0.1427	0.38	70	10	-	185.3	
TRD	0.0072	SHEN 1, SHEN 263	0.1499	0.80	80	8.5	-	179.8	STREET FLOWS FROM TAYLOR RANCH THAT FLOW TO THE SOUTH BRANCH OF THE PIEDRAS MARCADAS.
HNN2	0.0414	SHEN 1, SHEN 263, TRD, HNN2	0.1913	0.45	75	14.2	-	234.0	SEE MASTER DRAINAGE PLAN FOR THE RIVERVIEW SECTOR DEVELOPMENT BY CSC, NOV., 1985
HHE-2	0.0102	SHEN1, SHEN 263, TRD, HNN2, HHE2	0.2015	0.45	75	12.9	-	247.3	SEE MASTER DRAINAGE PLAN FOR THE RIVERVIEW SECTOR DEVELOPMENT BY CSC, NOV., 1985
A4	-	SHEN1, SHEN 263, TRD, HNN2, HHE2, A4	0.2280	-	-	-	-	279.4	

SHEN 263 131.8

SHEN 1 88.5

HNN2 54.2

HHE-2 13.3

TABLE 1 (Continued)
HYDROLOGICAL FLOW PARAMETERS

AREA/ POINT DESIGNATION	AREA (SQ. MI.)	AREAS CONTRIBUTING	GROSS AREA (SQ. MI.)	FRACTION IMPERVIOUS	CN	TC (MINUTES)	Q10 R(1)= 1.25" R(6)= 1.45"	Q100 R(1)= 1.9" R(6)= 2.2"	REMARKS
D10	-	SHEN1, SHEN 263, TRD.HHN2, HHE2, A4, D10	0.2480	-	-	-	-	284.0	
B5-8	-	SHEN1, SHEN 263, TRD.HHN2, HHE2, A4, D10, B5-8	0.2768	-	-	-	-	324.1	
B162	0.0149	C1, B162	0.0308	0.57	70	5	-	50.1	SEE DRAINAGE MANAGEMENT PLAN FOR PRAIRIE RIDGE III BY CSC, MAY, 1988
GCR	0.0049	C1, B162, GCR	0.0357	0.77	70	10	-	57.2	STREET FLOWS FROM GOLF COURSE RD. INTO THE PIEDRAS MARCADAS
GCR	-	ALL OF THE ABOVE	0.3125	-	-	-	-	381.3	
HHN1	0.0326	HHN1	0.0326	0.45	75	10.8	-	45.8	SEE MASTER DRAINAGE PLAN FOR THE RIVERVIEW SECTOR DEVELOPMENT BY CSC, NOV., 1985
L	0.0281	L	0.0281	0.65	70	15	-	40.2	SEE MASTER DRAINAGE PLAN FOR THE RIVERVIEW SECTOR DEVELOPMENT BY CSC, NOV., 1985
L	-	HHN1, L	0.0807	-	-	-	-	85.8	
M	0.0313	M	0.0313	0.85	70	7.8	-	56.0	SEE MASTER DRAINAGE PLAN FOR THE RIVERVIEW SECTOR DEVELOPMENT BY CSC, NOV., 1985
M	-	HHN1, L, M	0.0920	-	-	-	-	128.1	
M	-	ALL OF THE ABOVE	0.4045	-	-	-	-	507.1	

Prairie Ridge. Units 4 and 5
May, 1987

TABLE 2 - STREET FLOW CHARACTERISTICS
THE RIVERSIDE SECTOR DEVELOPMENT
(ASSUMING CURB AND GUTTER AND 2% CROWN)

POINT DESIGNATION	100 YEAR PEAK FLOW	10 YEAR PEAK FLOW	ESTIMATED STREET SLOPE	ASSUMED STREET WIDTH	100 YEAR FLOW DEPTH	10 YEAR FLOW DEPTH	10 YEAR VELOCITY	10 YEAR V X D	REMARKS
A1	23.5	12.7	0.0125	32	0.45	0.38	2.84	1.08	OK
A2	11.4	6.2	0.0005	32	0.42	0.35	1.89	0.59	OK
A3	8.8	4.8	0.0250	32	0.30	0.25	2.99	0.75	OK
B5	15.3	8.3	0.0091	32	0.42	0.35	2.28	0.80	OK
B6	9.1	5.0	0.0050	32	0.39	0.33	1.81	0.53	OK
B7	26.7	14.5	0.0200	32	0.44	0.37	3.51	1.30	OK
B8	15.0	8.1	0.0050	32	0.45	0.38	1.80	0.68	OK

Prairie Ridge, Units 4 and 5
May, 1987

TABLE 3
CRITICAL STREET INTERSECTION ANALYSIS

POINT DESIGNATION	INTERSECTION	LOCATION	Q	STREET WIDTH	SLOPE	Y_1	V_1	F_{r1}	Y_c	V_c	JUMP DEPTH = $\frac{Y_1}{2} \left(\sqrt{1 + 8F_{r1}^2} - 1 \right)$	POOL DEPTH $\frac{0 + 1.25 AV^2}{2g}$	SPECIAL REQUIREMENTS
B5	1	UPSTREAM	15.3	32	0.0091	0.42	2.68	1.12	0.43	2.47	0.49	—	OK
B6		UPSTREAM	9.1	32	0.0050	0.39	1.65	0.816	0.38	2.08	N/A	—	OK
B(5+6)		DOWNSTREAM	24.4	32	0.0091	0.48	3.23	1.17	0.50	2.89	—	0.51	OK

100 y₂₀

AREA/POINT DESIGNATION = A1
AREA = .01442 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 9 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	23.5

VOL = 36591.36 CF

AREA/POINT DESIGNATION = A2
AREA = .007 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 7 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	11.4

VOL = 17762.8 CF

AREA/POINT DESIGNATION = A3
AREA = .00542 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 6 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
239	8.8

VOL = 13753.49 CF

AREA/POINT DESIGNATION = A4
AREA = .02746 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 9 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	44.7

VOL = 69680.94 CF

AREA/POINT DESIGNATION = B5
AREA = 9.389999E-03 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 10 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	15.3

VOL = 23827.53 CF

AREA/POINT DESIGNATION = B6
AREA = .00561 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 6 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	9.1

VOL = 14235.61 CF

AREA/POINT DESIGNATION = B7
AREA = .02055 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 15 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	26.7

VOL = 52146.52 CF

AREA/POINT DESIGNATION = B8
AREA = .01025 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 11 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
243	15.0

VOL = 26009.82 CF

D10

AREA/POINT DESIGNATION = D10
AREA = .01695 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 16.64 MINUTES
FRAC IMPERV= .02
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
248	6.8

VOL = 13682.4 CF

AREA/POINT DESIGNATION = A4
AREA = .02746 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 9 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	44.7

VOL = 69680.94 CF

POINT A4 ADDED TO MAIN FLOWS

TIME	Q(CFS)
190	0.1
195	0.2
200	1.1
205	2.3
210	2.8
215	6.1
220	10.4
225	12.5
230	24.1
235	39.4
240	44.7
245	32.0
250	16.0
255	10.7
260	7.4
265	3.0
270	1.5
275	1.4
280	1.2
285	1.2
290	1.2
295	1.2
300	1.2
305	1.0
310	0.9
315	0.8
320	0.9

325	1.0
330	1.0
335	0.9
340	0.8
345	0.8
350	0.7
355	0.6
360	0.6
365	0.4

AREA/POINT DESIGNATION = B7
AREA = .02055 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 15 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	26.7

VOL = 52146.52 CF

POINT B7 ADDED TO MAIN FLOWS

TIME	Q(CFS)
195	0.1
200	0.3
205	0.8
210	1.5
215	2.7
220	4.5
225	6.8
230	11.1
235	17.9
240	24.8
245	26.7
250	22.9
255	16.8
260	11.1
265	6.5
270	3.6
275	2.2
280	1.3
285	1.0
290	0.9
295	0.9
300	0.9
305	0.8
310	0.8
315	0.7
320	0.7
325	0.7

330	0.7
335	0.7
340	0.7
345	0.6
350	0.6
355	0.5
360	0.5
365	0.4
370	0.3
375	0.2

AREA/POINT DESIGNATION = B5-8
AREA = .0308 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 15 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	40.1

VOL = 78156.34 CF

POINT B5-8 ADDED TO MAIN FLOWS

TIME	Q(CFS)
195	0.2
200	0.5
205	1.3
210	2.3
215	4.0
220	6.8
225	10.2
230	16.6
235	26.8
240	37.2
245	40.1
250	34.3
255	25.2
260	16.6
265	9.7
270	5.5
275	3.3
280	1.9
285	1.4
290	1.4
295	1.3
300	1.3
305	1.3
310	1.2
315	1.1
320	1.0
325	1.0

330	1.0
335	1.0
340	1.0
345	1.0
350	0.9
355	0.8
360	0.8
365	0.6
370	0.4
375	0.2
380	0.1

AREA/POINT DESIGNATION = A1
AREA = .01442 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 9 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

10 years

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	12.7

VOL = 19500.63 CF

AREA/POINT DESIGNATION = A2
AREA = .007 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 7 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	6.2

VOL = 9466.326 CF

AREA/POINT DESIGNATION = A3
AREA = .00542 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 6 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	4.8

VOL = 7329.642 CF

AREA/POINT DESIGNATION = A4
AREA = .02746 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 9 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	24.3

VOL = 37135.03 CF

AREA/POINT DESIGNATION = B5
AREA = 9.389999E-03 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 10 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	8.3

VOL = 12698.4 CF

AREA/POINT DESIGNATION = B6
AREA = .00561 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 6 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	5.0

VOL = 7586.585 CF

AREA/POINT DESIGNATION = B7
AREA = .02055 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 15 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	14.5

VOL = 27790.42 CF

AREA/POINT DESIGNATION = B8
AREA = .01025 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 11 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
243	8.1

VOL = 13861.4 CF

AREA/POINT DESIGNATION = A4
AREA = .02746 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 9 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	24.3

VOL = 37135.03 CF

POINT A4 ADDED TO MAIN FLOWS

TIME	Q(CFS)
200	0.3
205	0.8
210	0.9
215	2.8
220	5.2
225	6.4
230	12.8
235	21.3
240	24.3
245	17.4
250	8.8
255	6.0
260	4.1
265	1.7
270	0.9
275	0.8
280	0.7
285	0.7
290	0.7
295	0.7
300	0.7
305	0.6
310	0.5
315	0.5
320	0.5
325	0.5
330	0.6

335	0.5
340	0.5
345	0.4
350	0.4
355	0.4
360	0.4
365	0.2

AREA/POINT DESIGNATION = B7
AREA = .02055 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 15 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	14.5

VOL = 27790.42 CF

POINT B7 ADDED TO MAIN FLOWS

TIME	Q(CFS)
205	0.3
210	0.5
215	1.1
220	2.1
225	3.4
230	5.7
235	9.5
240	13.4
245	14.5
250	12.5
255	9.2
260	6.1
265	3.6
270	2.0
275	1.2
280	0.7
285	0.5
290	0.5
295	0.5
300	0.5
305	0.5
310	0.4
315	0.4
320	0.4
325	0.4
330	0.4
335	0.4

340	0.4
345	0.4
350	0.3
355	0.3
360	0.3
365	0.2
370	0.2

AREA/POINT DESIGNATION = B5-8
AREA = .0308 SQ MI
1 HR RAIN = 1.25 INCHES
6 HR RAIN = 1.45 INCHES
TC= 15 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	21.7

VOL = 41651.83 CF

POINT B5-8 ADDED TO MAIN FLOWS

TIME	Q(CFS)
200	0.1
205	0.4
210	0.8
215	1.6
220	3.1
225	5.0
230	8.6
235	14.3
240	20.0
245	21.7
250	18.7
255	13.8
260	9.1
265	5.4
270	3.0
275	1.9
280	1.1
285	0.8
290	0.8
295	0.7
300	0.7
305	0.7
310	0.7
315	0.6
320	0.6
325	0.6
330	0.6

335	0.6
340	0.6
345	0.5
350	0.5
355	0.5
360	0.4
365	0.4
370	0.3
375	0.1

May, 1987

1. ANALYZE INTERSECTION NO. 1

$$V = (0.5 (9.1)(1.85) + 15.3 (2.68) \div 24.4 = 2.06 \text{ fps}$$

$$\Delta V = 3.23 - 2.06 = 1.17 \text{ fps}$$

2. ANALYZE CAPACITY OF "TRIPLE C" CATCH BASINS

Use 0.53' as max. depth (sump condition)

Ave. h for grate = 0.57' (local depression)

h for curb opening = 0.51' (to mid point of curb opening)

use 15% clogging factor for grate

$$Q_{\text{grate}} = .85 (.65)(3.2) \sqrt{2g (.57)} = 10.71 \text{ cfs}$$

$$Q_{\text{curb}} = .65 (1.5) \sqrt{2g (.51)} = 5.59 \text{ cfs}$$

$$Q_{\text{total}} = 10.71 + 5.59 = 16.30 \text{ cfs}$$

$$\text{For "Triple C" Capacity} = 3(16.3) = 48.9 \text{ cfs}$$

$$48.9 > 44.7 > 40.1, \text{ OK}$$

1. ANALYZE INTERSECTION NO. 1

$$V = (0.5)(9.1)(1.85) + 15.3(2.68) - 24.4 = 2.06 \text{ fps}$$

$$\Delta V = 3.23 - 2.06 = 1.17 \text{ fps}$$

2. ANALYZE CAPACITY OF "TRIPLE C" CATCH BASINS

Use 0.53' as max. depth (sump condition)

Ave. h for grate = 0.57' (local depression)

h for curb opening = 0.51' (to mid point of curb opening)

use 15% clogging factor for grate

$$Q_{\text{grate}} = .85 (.65)(3.2) \sqrt{2g (.57)} = 10.71 \text{ cfs}$$

$$Q_{\text{curb}} = .65 (1.5) \sqrt{2g (.51)} = 5.59 \text{ cfs}$$

$$Q_{\text{total}} = 10.71 + 5.59 = 16.30 \text{ cfs}$$

$$\text{For "Triple C" Capacity} = 3(16.3) = 48.9 \text{ cfs}$$

$$48.9 > 44.7 > 40.1, \text{ OK}$$

3. CHECK REQUIRED HEAD ON STORM SEWER INLET

$$Q = CA\sqrt{2gh}$$

$$Q = 247 \text{ cfs}$$

$$C = (1.1 + \frac{.026L}{d^{1.2}})^{-1/2}$$

$$d = 5'$$

$$L = 50' \text{ (Assume "Long" Culvert)}$$

Solve for h

$$h = 3.17'$$

RCP PIPEENTRANCE

$$Q = C a \sqrt{2gh}$$

$$Q = 247$$

$$C = \left(1.1 + \frac{0.026L}{d^{1.2}} \right)^{-1/2} \quad \text{BEVELED LIP ENTRANCE}$$

$$d = 5' \quad L = 50' \quad (\text{ASSUME LONG CULVERT})$$

$$C = \left(1.1 + \frac{0.026(50')}{(5')^{1.2}} \right)^{-1/2} = 0.88$$

$$Q^2 = C^2 a^2 \cdot 2gh$$

$$h = \frac{Q^2}{C^2 a^2 \cdot 2g}$$

$$h = \frac{(247)^2}{(0.88)^2 \left(\frac{\pi \times (5')^2}{4} \right)^2 \times 2(32.2)} = 3.17'$$

NOTE: HYDRAULIC GRADE line at Inlet = 117.01
 + 3.17

5120.18 + 100 yr
 WATER SURFACE
 ELEVATION

INVERT of PIPE = 112.00

Top of HEAD WALL = 121.00

Top of EMERGENCY Spill way = 120.50

To be placed
 in appendix B

AREA/POINT DESIGNATION = SHENANDOAH 2 & 3

AREA = .1158 SQ MI

1 HR RAIN = 1.9 INCHES

6 HR RAIN = 2.2 INCHES

TC= 14 MINUTES

FRAC IMPERV= .268

CN (PERVIOUS)= 75.5

CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
------	--------

243	131.8
-----	-------

VOL = 219508.8 CF

POINT SHENANDOAH 2 & 3 ADDED TO MAIN FLOWS

TIME	Q(CFS)
------	--------

180	0.1
185	0.1
190	0.2
195	0.3
200	1.3
205	3.2
210	4.7
215	9.0
220	16.1
225	21.4
230	47.7
235	93.7
240	131.8
245	124.1
250	86.5
255	56.4
260	35.5
265	20.8
270	10.9
275	6.0
280	4.9
285	4.6
290	4.4
295	4.4
300	4.4
305	4.1
310	3.6

315	3.3
320	3.2
325	3.4
330	3.6
335	3.6
340	3.3
345	3.1
350	2.9
355	2.6
360	2.4
365	1.9
370	1.0
375	0.4

AREA/POINT DESIGNATION = SHENANDOAH 1

AREA = .0269 SQ MI

1 HR RAIN = 1.9 INCHES

6 HR RAIN = 2.2 INCHES

TC= 10 MINUTES

FRAC IMPERV= .38

CN (PERVIOUS)= 70

CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	33.5

VOL = 52180.49 CF

POINT SHENANDOAH 1 ADDED TO MAIN FLOWS

TIME	Q(CFS)
175	0.1
180	0.1
185	0.2
190	0.3
195	0.4
200	2.0
205	4.8
210	6.5
215	13.0
220	22.9
225	29.6
230	65.1
235	122.9
240	165.3

245	148.4
250	99.2
255	65.2
260	41.6
265	23.3
270	12.2
275	7.2
280	5.9
285	5.5
290	5.4
295	5.3
300	5.4
305	5.0
310	4.4
315	4.0
320	4.0
325	4.2
330	4.5
335	4.3
340	4.0
345	3.7
350	3.5
355	3.2
360	3.0
365	2.2
370	1.1
375	0.4

AREA/POINT DESIGNATION = TAYLOR RANCH DRIVE

AREA = .0072 SQ MI

1 HR RAIN = 1.9 INCHES

6 HR RAIN = 2.2 INCHES

TC= 8.5 MINUTES

FRAC IMPERV= .8

CN (PERVIOUS)= 60

CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	14.5

VOL = 22741.93 CF

POINT TAYLOR RANCH DRIVE ADDED TO MAIN FLOWS

TIME	Q(CFS)
175	0.1
180	0.2
185	0.2
190	0.3
195	0.5
200	2.4
205	5.6
210	7.5
215	15.3
220	26.7
225	34.1
230	73.2
235	135.8
240	179.8
245	158.7
250	104.1
255	68.4
260	43.8
265	24.2
270	12.6
275	7.6
280	6.3
285	5.9
290	5.7
295	5.7
300	5.7
305	5.3
310	4.6
315	4.2
320	4.2
325	4.5
330	4.7
335	4.6
340	4.2
345	4.0
350	3.7
355	3.4
360	3.1
365	2.3
370	1.1
375	0.4

DEPTH-1(GUESS) = .5 FT.
 DEPTH-2 = 0 FT.
 SIDESLOPE-1 = 2 HORZ/VERT
 SIDESLOPE-2 = 2 HORZ/VERT
 WIDTH = 30 FT.
 N = .022
 SLOPE = .03 FT./FT.
 REACH LENGTH = 950 FT.

HYDROGRAPH AT POINT TAYLOR RANCH DRIVE TIME TRANSLATED TO POINT HHN2

COMPUTED VELOCITY = 7.739042

TIME	Q(CFS)
175	0.1
180	0.1
185	0.2
190	0.3
195	0.4
200	1.6
205	4.3
210	6.7
215	12.1
220	22.0
225	31.1
230	57.2
235	110.2
240	161.8
245	179.8
250	126.4
255	83.0
260	53.8
265	32.2
270	17.3
275	9.6
280	6.8
285	6.0
290	5.8
295	5.7
300	5.7
305	5.5
310	4.9
315	4.4
320	4.2
325	4.4
330	4.7
335	4.7
340	4.4
345	4.1
350	3.8
355	3.5
360	3.2
365	2.7
370	1.6
375	0.7
380	0.2

AREA/POINT DESIGNATION = HHN2
AREA = .0414 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 14.2 MINUTES
FRAC IMPERV= .45
CN (PERVIOUS)= 75
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
243	57.9

VOL = 98032.98 CF

POINT HHN2 ADDED TO MAIN FLOWS

TIME	Q(CFS)
170	0.1
175	0.2
180	0.2
185	0.3
190	0.4
195	0.6
200	2.4
205	6.3
210	9.6
215	17.5
220	31.5
225	43.6
230	81.0
235	152.8
240	219.6
245	234.0
250	163.6
255	106.5
260	68.2
265	40.5
270	21.7
275	12.0
280	8.8
285	7.9
290	7.5
295	7.4
300	7.4

305	7.1
310	6.3
315	5.7
320	5.5
325	5.8
330	6.1
335	6.1
340	5.7
345	5.3
350	4.9
355	4.5
360	4.2
365	3.4
370	2.0
375	0.8
380	0.2

AREA/POINT DESIGNATION = HHE2
 AREA = .0102 SQ MI
 1 HR RAIN = 1.9 INCHES
 6 HR RAIN = 2.2 INCHES
 TC= 12.9 MINUTES
 FRAC IMPERV= .45
 CN (PERVIOUS)= 75
 CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
243	14.3

VOL = 24153.05 CF

POINT HHE2 ADDED TO MAIN FLOWS

TIME	Q(CFS)
170	0.1
175	0.2
180	0.2
185	0.3
190	0.5
195	0.6
200	2.6
205	6.7
210	10.2
215	18.8
220	33.8

225	46.7
230	86.8
235	163.3
240	233.9
245	247.3
250	172.7
255	112.3
260	71.7
265	42.6
270	22.8
275	12.6
280	9.3
285	8.3
290	7.9
295	7.9
300	7.9
305	7.5
310	6.7
315	6.0
320	5.8
325	6.1
330	6.4
335	6.4
340	6.0
345	5.6
350	5.2
355	4.8
360	4.4
365	3.6
370	2.1
375	0.8
380	0.2

DIAMETER = 5

SLOPE = .015

N = .013

REACH LENGTH = 450 FT.

HYDROGRAPH AT POINT HHE2 TIME TRANSLATED TO POINT A4

COMPUTED VELOCITY = 16.89168

TIME	Q(CFS)
170	0.1
175	0.2
180	0.2
185	0.3
190	0.5
195	0.6
200	2.4
205	6.4
210	9.9
215	18.0
220	32.5
225	45.6

230	83.3
235	156.5
240	227.6
245	247.3
250	179.3
255	117.7
260	75.3
265	45.2
270	24.6
275	13.5
280	9.6
285	8.4
290	8.0
295	7.9
300	7.9
305	7.5
310	6.8
315	6.0
320	5.8
325	6.1
330	6.4
335	6.4
340	6.0
345	5.6
350	5.3
355	4.8
360	4.5
365	3.7
370	2.3
375	1.0
380	0.2

AREA/POINT DESIGNATION = A4
 AREA = .02746 SQ MI
 1 HR RAIN = 1.9 INCHES
 6 HR RAIN = 2.2 INCHES
 TC= 9 MINUTES
 FRAC IMPERV= .57
 CN (PERVIOUS)= 70
 CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	44.7

VOL = 69680.94 CF

POINT A4 ADDED TO MAIN FLOWS

TIME	Q(CFS)
170	0.2
175	0.2
180	0.3
185	0.4
190	0.6
195	0.8
200	3.6
205	8.7
210	12.7
215	24.2
220	42.9
225	58.0
230	107.4
235	195.9
240	272.3
245	279.4
250	195.3
255	128.4
260	82.7
265	48.2
270	26.1
275	14.9
280	10.8
285	9.6
290	9.1
295	9.0
300	9.0
305	8.6
310	7.6
315	6.9
320	6.7
325	7.0
330	7.4
335	7.3
340	6.9
345	6.4
350	6.0
355	5.5
360	5.1
365	4.1
370	2.3
375	1.0
380	0.2

DIAMETER = 5
SLOPE = .015
N = .013
REACH LENGTH = 1200 FT.

HYDROGRAPH AT POINT A4 TIME TRANSLATED TO POINT D10

COMPUTED VELOCITY = 17.37341

TIME	Q(CFS)
170	0.1
175	0.2
180	0.3
185	0.4
190	0.5
195	0.8
200	2.9
205	7.5
210	11.8
215	21.5
220	38.6
225	54.5
230	96.0
235	175.5
240	254.7
245	279.4
250	214.7
255	143.8
260	93.3
265	56.2
270	31.2
275	17.5
280	11.7
285	9.8
290	9.2
295	9.1
300	9.0
305	8.7
310	7.8
315	7.0
320	6.7
325	6.9
330	7.3
335	7.3
340	7.0
345	6.5
350	6.1
355	5.6
360	5.2
365	4.3
370	2.7
375	1.3
380	0.4

AREA/POINT DESIGNATION = D10
AREA = .01695 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 24.5 MINUTES
FRAC IMPERV= .02
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
252	5.6

VOL = 13682.4 CF

POINT D10 ADDED TO MAIN FLOWS

TIME	Q(CFS)
170	0.1
175	0.2
180	0.3
185	0.4
190	0.5
195	0.8
200	2.9
205	7.5
210	11.8
215	21.6
220	38.7
225	54.8
230	96.9
235	177.4
240	258.1
245	284.0
250	220.0
255	149.4
260	98.2
265	60.4
270	34.4
275	19.7
280	13.2
285	10.8
290	9.9
295	9.6
300	9.5

305	9.1
310	8.2
315	7.4
320	7.1
325	7.3
330	7.6
335	7.7
340	7.3
345	6.8
350	6.4
355	5.9
360	5.4
365	4.5
370	2.9
375	1.4
380	0.5
385	0.1

AREA/POINT DESIGNATION = B5-8
 AREA = .0308 SQ MI
 1 HR RAIN = 1.9 INCHES
 6 HR RAIN = 2.2 INCHES
 TC= 15 MINUTES
 FRAC IMPERV= .57
 CN (PERVIOUS)= 70
 CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	40.1

VOL = 78156.34 CF

POINT B5-8 ADDED TO MAIN FLOWS

TIME	Q(CFS)
165	0.1
170	0.2
175	0.2
180	0.3
185	0.4
190	0.6
195	0.9
200	3.4
205	8.8
210	14.1

215	25.6
220	45.4
225	65.0
230	113.5
235	204.2
240	295.3
245	324.1
250	254.3
255	174.6
260	114.8
265	70.2
270	39.9
275	23.0
280	15.2
285	12.3
290	11.3
295	10.9
300	10.8
305	10.3
310	9.4
315	8.5
320	8.1
325	8.3
330	8.7
335	8.7
340	8.3
345	7.8
350	7.3
355	6.7
360	6.2
365	5.2
370	3.4
375	1.7
380	0.6
385	0.2

**ANALYSIS SHIFTED TO ALTERNATE BRANCH BEGINNING AT
AREA/POINT DESIGNATION D10 **

AREA/POINT DESIGNATION = C1
AREA = .0159 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 10 MINUTES
FRAC IMPERV= .57
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	25.9

VOL = 40346.93 CF

POINT C1 ADDED TO MAIN FLOWS

TIME	Q(CFS)
195	0.1
200	0.7
205	1.4
210	1.6
215	3.6
220	6.0
225	7.2
230	14.0
235	22.8
240	25.9
245	18.5
250	9.3
255	6.2
260	4.3
265	1.8
270	0.9
275	0.8
280	0.7
285	0.7
290	0.7
295	0.7
300	0.7
305	0.6
310	0.5
315	0.5
320	0.5
325	0.6

330	0.6
335	0.5
340	0.5
345	0.5
350	0.4
355	0.4
360	0.4
365	0.2

AREA/POINT DESIGNATION = B1 & B2

AREA = .0149 SQ MI

1 HR RAIN = 1.9 INCHES

6 HR RAIN = 2.2 INCHES

TC= 5 MINUTES

FRAC IMPERV= .57

CN (PERVIOUS)= 70

CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
234	24.3

VOL = 37809.4 CF

POINT B1 & B2 ADDED TO MAIN FLOWS

TIME	Q(CFS)
185	0.1
190	0.2
195	0.2
200	1.9
205	2.8
210	3.1
215	9.2
220	12.4
225	13.6
230	35.5
235	47.0
240	50.1
245	27.2
250	15.2
255	12.1
260	5.9
265	2.6
270	1.7
275	1.5

280	1.3
285	1.3
290	1.3
295	1.3
300	1.3
305	1.1
310	0.9
315	0.9
320	1.0
325	1.1
330	1.1
335	1.0
340	0.9
345	0.9
350	0.8
355	0.7
360	0.7
365	0.3

DEPTH-1(GUESS) = .5 FT.
 DEPTH-2 = 0 FT.
 SIDESLOPE-1 = 0 HORZ/VERT
 SIDESLOPE-2 = 50 HORZ/VERT
 WIDTH = 0 FT.
 N = .017
 SLOPE = 5.000001E-03 FT./FT.
 REACH LENGTH = 1300 FT.

HYDROGRAPH AT POINT B1 & B2 TIME TRANSLATED TO POINT D10

COMPUTED VELOCITY = 3.044426

TIME	Q(CFS)
195	0.1
200	0.2
205	1.2
210	2.5
215	3.0
220	6.6
225	11.1
230	13.1
235	26.3
240	42.2
245	50.1
250	36.9
255	20.3
260	13.4
265	8.5
270	4.0
275	2.1
280	1.6
285	1.4
290	1.3
295	1.3

300	1.3
305	1.3
310	1.2
315	1.0
320	0.9
325	1.0
330	1.1
335	1.1
340	1.0
345	0.9
350	0.9
355	0.8
360	0.7
365	0.7
370	0.5
375	0.1

AREA/POINT DESIGNATION = GOLF COURSE RD

AREA = .0049 SQ MI

1 HR RAIN = 1.9 INCHES

6 HR RAIN = 2.2 INCHES

TC= 10 MINUTES

FRAC IMPERV= .77

CN (PERVIOUS)= 70

CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	10.0

VOL = 15517.08 CF

POINT GOLF COURSE RD ADDED TO MAIN FLOWS

TIME	Q(CFS)
190	0.1
195	0.2
200	0.5
205	1.8
210	3.1
215	4.5
220	9.1
225	14.0
230	18.6
235	35.1
240	52.1

245	57.2
250	40.4
255	22.5
260	15.0
265	9.2
270	4.3
275	2.4
280	1.8
285	1.6
290	1.6
295	1.5
300	1.5
305	1.5
310	1.3
315	1.2
320	1.1
325	1.2
330	1.3
335	1.3
340	1.2
345	1.1
350	1.0
355	0.9
360	0.9
365	0.8
370	0.5
375	0.1

BRANCHES AT POINT MERGE MERGED AND FLOWS ADDED

TIME	Q(CFS)
165	0.1
170	0.2
175	0.3
180	0.4
185	0.5
190	0.8
195	1.1
200	3.9
205	10.5
210	17.2
215	30.0
220	54.6
225	79.1
230	132.1
235	239.3
240	347.5
245	381.3
250	294.7
255	197.1
260	129.8
265	79.3
270	44.2
275	25.4
280	17.0
285	13.9

290	12.8
295	12.4
300	12.3
305	11.9
310	10.7
315	9.6
320	9.2
325	9.5
330	9.9
335	10.0
340	9.5
345	8.9
350	8.3
355	7.6
360	7.1
365	6.0
370	3.9
375	1.8
380	0.6
385	0.2

**ANALYSIS SHIFTED TO ALTERNATE BRANCH BEGINNING AT
AREA/POINT DESIGNATION BRANCH **

AREA/POINT DESIGNATION = HHN1
 AREA = .0326 SQ MI
 1 HR RAIN = 1.9 INCHES
 6 HR RAIN = 2.2 INCHES
 TC= 10.8 MINUTES
 FRAC IMPERV= .45
 CN (PERVIOUS)= 75
 CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
243	45.6

VOL = 77195.05 CF

POINT HHN1 ADDED TO MAIN FLOWS

TIME	Q(CFS)
190	0.1
195	0.1
200	0.6
205	1.5
210	2.2
215	4.2
220	7.4
225	9.9
230	18.7
235	33.6
240	45.6
245	42.7
250	29.2
255	18.5
260	11.3
265	6.6
270	3.4
275	1.9
280	1.5
285	1.4
290	1.4
295	1.4
300	1.4
305	1.3
310	1.1
315	1.0
320	1.0
325	1.1
330	1.1
335	1.1
340	1.0
345	1.0
350	0.9
355	0.8
360	0.8
365	0.6
370	0.3
375	0.1

DEPTH-1(GUESS) = .87 FT.
 DEPTH-2 = -.4 FT.
 SIDESLOPE-1 = 0 HORZ/VERT
 SIDESLOPE-2 = 0 HORZ/VERT
 WIDTH = 40 FT.
 N = .017
 SLOPE = .035 FT./FT.
 REACH LENGTH = 1600 FT.

HYDROGRAPH AT POINT HHN1 TIME TRANSLATED TO POINT M

COMPUTED VELOCITY = 4.990207

TIME	Q(CFS)
200	0.1
205	0.6
210	1.5
215	2.2
220	4.1
225	7.2
230	9.7
235	18.1
240	32.5
245	45.6
250	42.9
255	30.2
260	19.2
265	11.8
270	6.9
275	3.7
280	2.0
285	1.6
290	1.4
295	1.4
300	1.4
305	1.4
310	1.3
315	1.1
320	1.0
325	1.0
330	1.1
335	1.1
340	1.1
345	1.0
350	1.0
355	0.9
360	0.8
365	0.8
370	0.6
375	0.3
380	0.1

AREA/POINT DESIGNATION = L
AREA = .0281 SQ MI
1 HR RAIN = 1.9 INCHES
6 HR RAIN = 2.2 INCHES
TC= 15 MINUTES
FRAC IMPERV= .65
CN (PERVIOUS)= 70
CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	40.2

VOL = 78377.26 CF

POINT L ADDED TO MAIN FLOWS

TIME	Q(CFS)
185	0.1
190	0.2
195	0.3
200	0.7
205	1.9
210	3.8
215	6.3
220	11.1
225	17.8
230	26.7
235	45.3
240	70.0
245	85.8
250	77.2
255	55.2
260	35.6
265	21.3
270	12.2
275	6.9
280	3.9
285	3.0
290	2.8
295	2.7
300	2.6
305	2.6
310	2.4
315	2.2

320	2.0
325	2.0
330	2.1
335	2.1
340	2.1
345	2.0
350	1.8
355	1.7
360	1.6
365	1.4
370	1.0
375	0.6
380	0.2

AREA/POINT DESIGNATION = M
 AREA = .0313 SQ MI
 1 HR RAIN = 1.9 INCHES
 6 HR RAIN = 2.2 INCHES
 TC= 7.6 MINUTES
 FRAC IMPERV= .65
 CN (PERVIOUS)= 70
 CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
240	56.0

VOL = 87302.78 CF

POINT M ADDED TO MAIN FLOWS

TIME	Q(CFS)
175	0.1
180	0.2
185	0.2
190	0.3
195	0.5
200	2.1
205	4.9
210	7.4
215	14.3
220	24.7
225	33.9
230	57.2
235	94.7
240	126.1

245	125.8
250	96.9
255	68.3
260	44.6
265	25.0
270	14.0
275	8.6
280	5.4
285	4.4
290	4.2
295	4.1
300	4.0
305	3.8
310	3.5
315	3.2
320	3.1
325	3.1
330	3.3
335	3.2
340	3.1
345	2.9
350	2.7
355	2.5
360	2.3
365	1.8
370	1.1
375	0.6
380	0.2

BRANCHES AT POINT MERGE MERGED AND FLOWS ADDED

TIME	Q(CFS)
160	0.1
165	0.2
170	0.3
175	0.4
180	0.5
185	0.8
190	1.1
195	1.7
200	6.0
205	15.5
210	24.6
215	44.3
220	79.2
225	113.0
230	189.3
235	333.9
240	473.5
245	507.1
250	391.5
255	265.4
260	174.4
265	104.3
270	58.2
275	34.0

280	22.3
285	18.3
290	17.0
295	16.5
300	16.3
305	15.7
310	14.2
315	12.8
320	12.2
325	12.6
330	13.2
335	13.2
340	12.6
345	11.8
350	11.0
355	10.1
360	9.4
365	7.8
370	5.0
375	2.4
380	0.9
385	0.2

DEPTH-1(GUESS) = 3 FT.

DEPTH-2 = 0 FT.

SIDESLOPE-1 = 2 HORZ/VERT

SIDESLOPE-2 = 2 HORZ/VERT

WIDTH = 10 FT.

N = .015

SLOPE = .0267 FT./FT.

REACH LENGTH = 1500 FT.

HYDROGRAPH AT POINT MERGE TIME TRANSLATED TO POINT N

COMPUTED VELOCITY = 18.4471

TIME	Q(CFS)
165	0.2
170	0.3
175	0.4
180	0.5
185	0.7
190	1.0
195	1.5
200	4.8
205	12.9
210	22.1
215	39.0
220	69.8
225	103.8
230	168.6
235	294.7
240	435.7
245	507.1

250	422.9
255	299.6
260	199.1
265	123.3
270	70.7
275	40.5
280	25.5
285	19.4
290	17.4
295	16.6
300	16.4
305	15.9
310	14.6
315	13.2
320	12.4
325	12.5
330	13.0
335	13.2
340	12.8
345	12.0
350	11.2
355	10.4
360	9.6
365	8.2
370	5.8
375	3.1
380	1.3
385	0.4

AREA/POINT DESIGNATION = N
 AREA = .0625 SQ MI
 1 HR RAIN = 1.9 INCHES
 6 HR RAIN = 2.2 INCHES
 TC= 11.3 MINUTES
 FRAC IMPERV= .68
 CN (PERVIOUS)= 70
 CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
243	104.1

VOL = 180225.5 CF

POINT N ADDED TO MAIN FLOWS

TIME	Q(CFS)
160	0.1
165	0.2
170	0.3
175	0.5
180	0.7
185	0.9
190	1.3
195	1.9
200	6.6
205	17.3
210	28.5
215	51.1
220	91.1
225	132.1
230	216.5
235	374.1
240	539.8
245	604.1
250	488.4
255	340.0
260	223.1
265	137.2
270	78.0
275	44.5
280	28.7
285	22.4
290	20.2
295	19.5
300	19.2
305	18.6
310	17.0
315	15.3
320	14.5
325	14.7
330	15.4
335	15.6
340	14.9
345	14.0
350	13.1
355	12.1
360	11.2
365	9.5
370	6.4
375	3.3
380	1.3
385	0.4

DEPTH-1(GUESS) = 3 FT.
DEPTH-2 = 0 FT.
SIDESLOPE-1 = 2 HORZ/VERT
SIDESLOPE-2 = 2 HORZ/VERT
WIDTH = 10 FT.
N = .015
SLOPE = .0213 FT./FT.
REACH LENGTH = 750 FT.

HYDROGRAPH AT POINT N TIME TRANSLATED TO POINT DAM

COMPUTED VELOCITY = 17.98558

TIME	Q(CFS)
160	0.1
165	0.2
170	0.3
175	0.5
180	0.6
185	0.9
190	1.3
195	1.8
200	6.0
205	15.8
210	27.0
215	48.0
220	85.6
225	126.4
230	204.7
235	352.2
240	516.8
245	604.1
250	504.5
255	360.6
260	239.4
265	149.2
270	86.2
275	49.2
280	30.9
285	23.3
290	20.5
295	19.6
300	19.3
305	18.7
310	17.2
315	15.5
320	14.6
325	14.7
330	15.3
335	15.5
340	15.0
345	14.2
350	13.2

355	12.2
360	11.3
365	9.7
370	6.8
375	3.8
380	1.6
385	0.5
390	0.1

AREA/POINT DESIGNATION = H2
 AREA = .0281 SQ MI
 1 HR RAIN = 1.9 INCHES
 6 HR RAIN = 2.2 INCHES
 TC= 15.9 MINUTES
 FRAC IMPERV= .65
 CN (PERVIOUS)= 70
 CN (IMPERVIOUS)= 95

PEAK ONLY OUTPUTTED

TIME	Q(CFS)
244	40.2

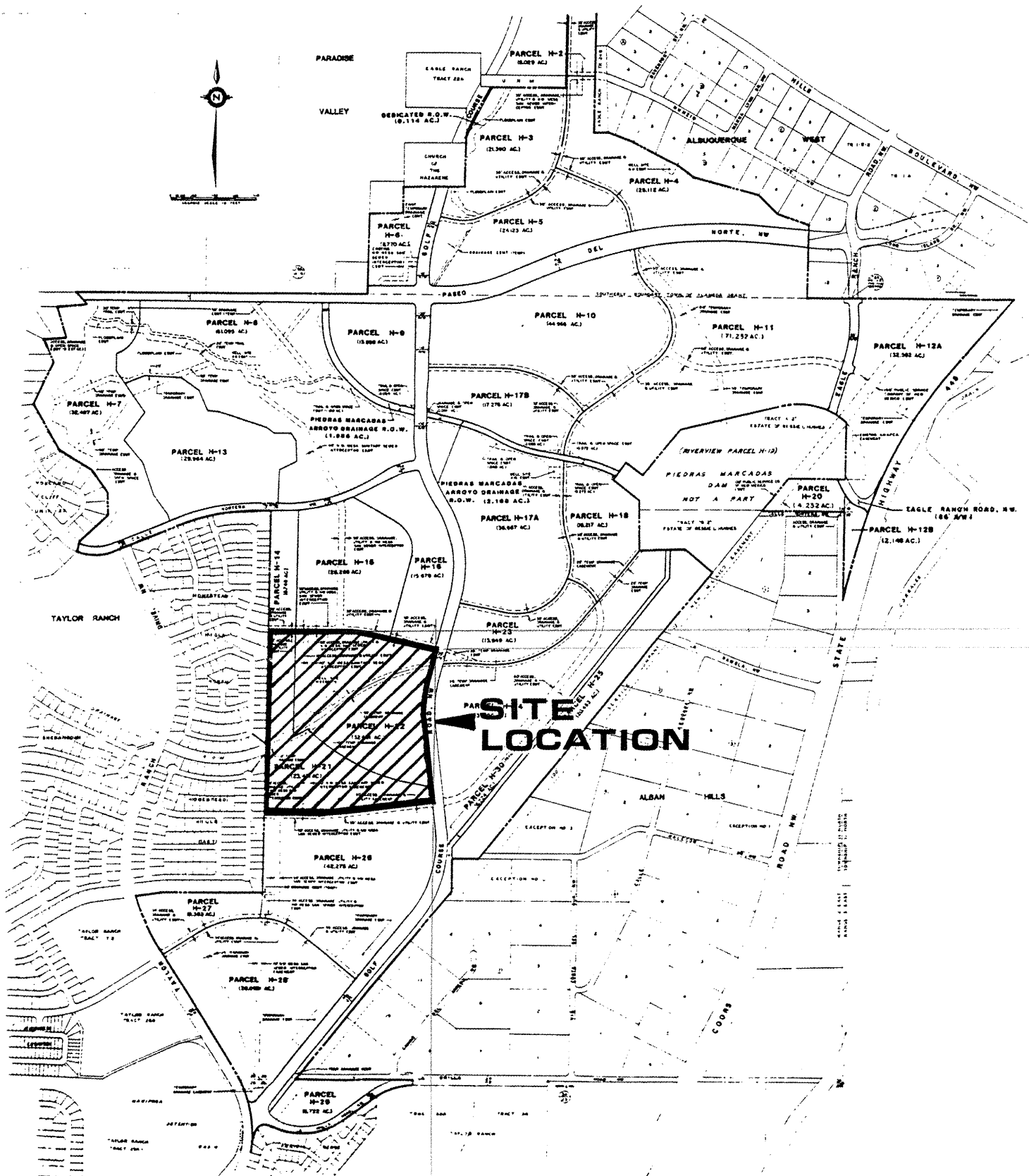
VOL = 78377.26 CF

POINT H2 ADDED TO MAIN FLOWS

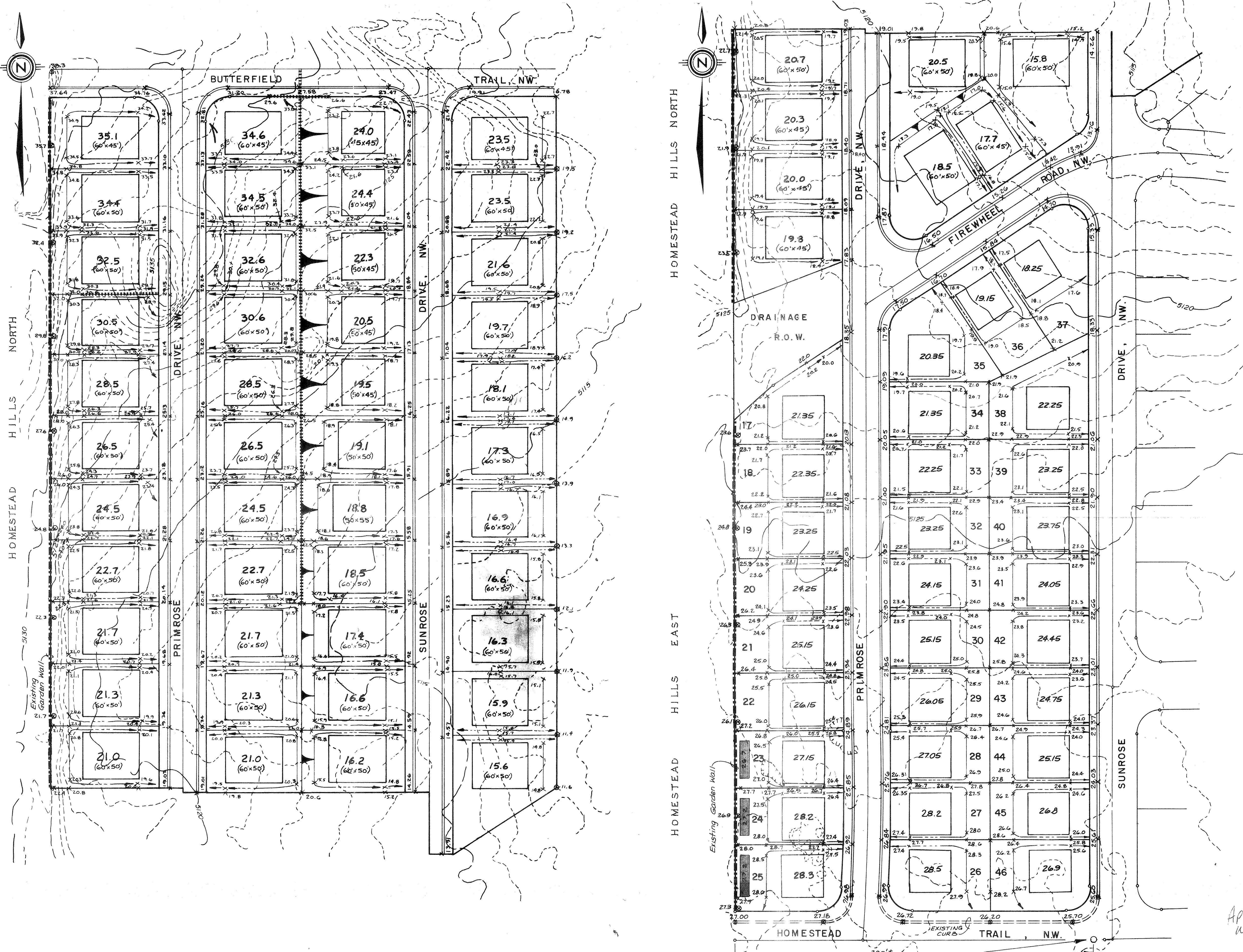
TIME	Q(CFS)
160	0.1
165	0.2
170	0.3
175	0.5
180	0.7
185	0.9
190	1.4
195	2.0
200	6.5
205	17.1
210	29.3
215	52.1
220	92.6
225	137.0
230	221.7
235	379.4
240	554.3
245	644.4
250	538.8

255	385.7
260	255.8
265	158.7
270	91.5
275	52.4
280	32.8
285	24.7
290	21.9
295	20.9
300	20.5
305	19.9
310	18.3
315	16.6
320	15.6
325	15.7
330	16.3
335	16.5
340	16.0
345	15.1
350	14.1
355	13.0
360	12.0
365	10.3
370	7.3
375	4.0
380	1.7
385	0.5
390	0.1

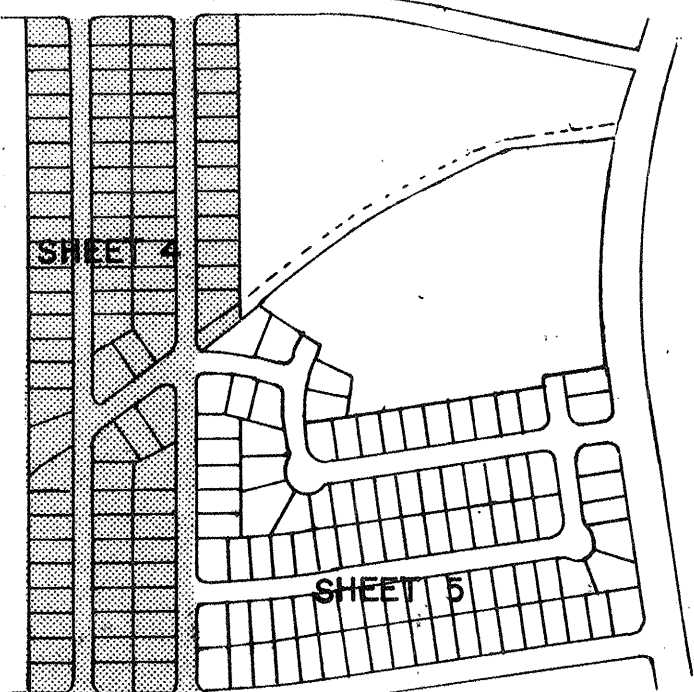
PLATE 1



VICINITY MAP



EARTHWORK QUANTITIES
CUT = 60,563 C.Y.
COMPACTED FILL = 43,694 C.Y.
CUT/FILL RATIO = 1.39



SCALE: 1" = 50'
CITY OF ALBUQUERQUE
PUBLIC WORKS DEPARTMENT
ENGINEERING GROUP
TITLE: PRAIRIE RIDGE UNIT FOUR
GRADING PLAN

APPROVALS	ENGINEER	DATE	APPROVALS	ENGINEER	DATE
D.R.C. Chair		9/18/07			
Trans. Dev.		9/18/07			
Utility Dev.		9/18/07			
Hydrology		9/18/07			
DRAWING NO.	3314	MAP NO.	D-12	SHEET	4 OF 41

AS BUILT INFORMATION	BENCH MARKS	SURVEY INFORMATION	ENGINEER'S SEAL
CONTRACTOR DATE DATE DATE DATE DATE DATE	6.1.0. BRASS CAP FOR SECTION 23, 24, 25 AND 26, LOCATED WITHIN PARCEL H-28, RIVERVIEW APPROX. 250' NORTH OF THE INTERSECTION OF GOLF COURSE ROAD, N.W. AND LA ORILLA RD., N.W. ELEV. = 5112.83.	FIELD NOTES NO. BY DATE	ENGINEER'S SEAL WHITNEY J. THOMPSON REGISTERED PROFESSIONAL ENGINEER STATE OF NEW MEXICO 6/15/07

ONSITE T.B.M. - RIM OF EXISTING
MANHOLE LOCATED APPROXIMATELY
380' EAST OF S.W. PROPERTY CORNER
(ELEV. = 5125.32) TO BE USED
FOR A GRADING BENCHMARK
ONLY.

APPROVED FOR ROUGH GRADING
(± 1 Ft.)

CITY HYDROLOGY DATE