February 22, 2011

Genny Donart, P.E. Isaacson & Arfman, P.A. 128 Monroe St. NE Albuquerque, NM 87108 wanter in Cyan
to respond to approve
for SPBD

Re: Brunacini Journal Center Tracts A-2-A and A-3-A
Preliminary Grading and Drainage Plan
Engineer's Stamp dated X-X-XX (D17/D003AA7)

Dear Ms Donart,

Based upon the information provided in your submittal received 2/10/2011, the above referenced plan can not be approved for Site Development for Building Permit action by the DRB until the following comments are addressed.

- We need the plans to be stamped, signed and dated.
- We would like for the valley gutter to be extended to the treatment pond area, or more of a slope in the internal access road.
- I believe that a curb opening in the access road just east of the bend would be much more beneficial in accepting flows from the east parking lots.
- The concrete rundown to the North Diversion Channel side inlet is required to be on an Infrastructure List.

As discussed, additional information will be required on your submittal for Building Permit.

If you have any questions, you can contact me at 924-3695.

Sincerely,

Curtis A. Cherne, P.E. Senior Engineer, Planning Dept. Development and Building Services

RR

C: file Brad Bingham

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (Rev. 12/05)

PROJECT TITLE: Brunacini Journal Center	ZONE MAP/DRG. FILE <u>D-17/D003-AA7</u>
PROJECT TITLE: Brunacini Journal Center DRB#: EPC#:	WORK ORDER#:
LECAL DESCRIPTIONS TRACTS A 2 A AND A 2 A TOURNE	AL CENTED DUACE 2 IDNET 2 ALDUQUEDQUE NA
LEGAL DESCRIPTION: <u>TRACTS A-2-A AND A-3-A, JOURNA</u> CITY ADDRESS: 9721 RUTLEDGE ST. NE	AL CENTER, PHASE 2, UNIT 2, ALBUQUERQUE, NM
CITT ADDRESS. 9721 ROTLEDGE ST. NE	Garage Dance
ENGINEERING FIRM: _ ISSACSON & ARFMAN, PA	CONTACT: FRED C. ARFMAN
ADDRESS: 128 MONROE NE	
CITY, STATE: ALBUQUERQUE, NM	
OWNER:	CONTACT:
ADDRESS:	PHONE:
ADDRESS:CITY, STATE:	ZIP CODE:
ARCHITECT: CLAUDIO VIGIL ARCHITECTS	CONTACT:EDWARD AVILA
ADDRESS: 1801 RIO GRANDE BLVD. NW	PHONE: 842-1113
CITY, STATE: Albuquerque, NM	ZIP CODE:
CLIDVEVING FIRM. CLIDV TEV CONCLUTING CLIDVEV	ODE LICENSED SUBVEYOR, DUSC DUBLICO
SURVEYING FIRM: SURV-TEK CONSULTING SURVEYO	
ADDRESS: 9384 VALLEY VIEW DR. NW CITY, STATE: Albuquerque, NM	
CITT, STATE. Albuquerque, NIVI	ZIP CODE:8/114
CONTRACTOR:	CONTACT:
ADDRESS:	PHONE:
CITY, STATE:	ZIP CODE:
TYPE OF SUBMITTAL: CHE	ECK TYPE OF APPROVAL SOUGHT:
DRAINAGE REPORT	SIA/FINANCIAL GUARANTEE RELEASE
	PRELIMINARY PLAT APPROVAL
	S. DEV. PLAN FOR SUB'D APPROVAL
	S. DEV. FOR BLDG. PERMIT APPROVAL
	SECTOR PLAN APPROVAL
EROSION CONTROL PLAN	FINAL PLAT APPROVAL
ENGINEER'S CERT (HYDROLOGY)	FOUNDATION PERMIT APPROVAL
CLOMR/LOMR	BUILDING PERMIT APPROVAL
TRAFFIC CIRCULATION LAYOUT	CERTIFICATE OF OCCUPANCY (PERM)
ENGINEER/ARCHITECT CERT (TCL)	CERTIFICATE OF OCCUPANCY (TEMP)
ENGINEER/ARCHITECT CERT (DRB S.P.)	GRADING PERMIT APPROVAL
ENGINEER/ARCHITECT CERT (AA)	PAVING PERMIT APPROVAL
OTHER (SPECIFY)	WORK ORDER APPROVAL
· · · · · · · · · · · · · · · · · · ·	OTHER (SPECIFY)
WAS A PRE-DESIGN CONFERENCE ATTENDED:	The same of the sa
YES	- 0 2011
NO	FEB 1 V Zon
COPY PROVIDED	Donart
	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
SUBMITTED BY: ISAACSON & ARFMAN: Fred Arfman	DATE: March 1, 2010

Requests for approvals of Site Development Plans and/or Subdivision Plats shall be accompanied by a drainage submittal. The particular nature, location and scope to the proposed development define the degree of drainage detail. One or more of the following levels of submittal may be required based on the following:

- 1. **Conceptual Grading and Drainage Plan**: Required for approval of Site Development Plans greater than five (5) acres and Sector Plans.
- 2. **Drainage Plans**: Required for building permits, grading permits, paving permits and site plans less than five (5) acres.
- 3. **Drainage Report**: Required for subdivision containing more than ten (10) lots or constituting five (5) acres or more.

Cherne, Curtis

From:

Genny Donart [gennyd@iacivil.com]

Sent:

Monday, February 07, 2011 1:58 PM

To:

'Mazur, Lynn'

Cc:

Cherne, Curtis

Subject:

RE: Brunacini at Journal Center

Attachments: 1765 Brunacini at North Pino.pdf; 1756 CG-101-SDP.pdf

Hi Lynn,

Thanks for the letter and markups. In response to your comments on 02/04/11:

"I will need to see the site plan to determine the site drainage pattern."

I apologize, I should have included the full site plan with my earlier email. I've included it as an
attachment this time.

"On the detail sheet, it appears that only the loading dock area and the internal access road drain to the water quality pond. The intent of the water quality treatment is to take the first flush rainfall over the entire site through the pond."

 While you are correct that the treatment pond collects all its water from the loading docks and access road, what you couldn't see on that detail sheet is that the access road collects all the offsite water from the east and south. The pond is set up to treat storm water from the entire area.

"The [Essayons Boulevard] project is a few years out and has not been approved by the AMAFCA Board of Directors or the U.S. Army Corps of Engineers. Therefore, we will require a concrete rundown connection to the existing NDC rundown structure as you have shown on the plan."

 Thanks for the information about the Essayons Blvd project. My plan was to make that rundown shotcrete to help keep skateboarders off of it and to reduce costs. I mis-labeled it in the notes. Does that create any difficulties?

"We will also require it to extend to the south to capture the flow in the existing side inlet channel."

When you say we need to extend the rundown to the south, how far does that extension need to go?
 Will a dip extending 5' to 10' to the south in the side of the channel be sufficient?

"a Turnkey Agreement will be required for the work within the NDC right-of-way."

• I'll make sure the owner is informed about the turnkey agreement.

"Another issue I would like to reiterate is the new FEMA requirement to have a 15-foot clear access a the toe of slope of our drainage facilities."

• The existing topo from the surveyor shows spots at least 20' north of the North Pino right-of-way line that indicate a flat area at least 20' wide. (Please see attached.) We don't show where the slope begins, but since it's flat that far out, we should be OK for the 15' access requirement to be within the AMAFCA R/W. Please let me know if this information is sufficient.

Genny Donart, P.E.



Design Engineer

Isaacson & Arfman, P.A. Consulting Engineering Associates 128 Monroe St. N.E. Albuquerque, NM 87108

Phone: (505)268-8828 Fax: (505)268-2632

Email: gennyd@iacivil.com

From: Mazur, Lynn [mailto:lmazur@amafca.org]

Sent: Friday, February 04, 2011 1:09 PM

To: Genny Donart **Cc:** Curtis Cherne

Subject: Brunacini at Journal Center

Attached are my review letter and mark-ups.

Albuquerque Metropolitan Arroyo Flood Control Authority

Lynn M. Mazur, P.E., C.F.M. Development Review Engineer Phone: (505) 884-2215

www.amafca.org

Cherne, Curtis

From: Maz

Mazur, Lynn [lmazur@amafca.org]

Sent:

Tuesday, March 23, 2010 10:31 AM

To:

Cherne, Curtis

Subject: RE: Tract A-2-A and A-3-A Brunacini Journal Center

A water quality feature similar to the one on the Brunacini @ Journal Center plans, dated August 2004, will be required on the final plans. I gave Isaacson & Arfman a copy of it when we met earlier this year. There may be some slight modifications to the detail. AMAFCA can provide a detail of the outlet drain from the water quality sump.

Albuquerque Metropolitan Arroyo

Flood Control Authority

Lynn M. Mazur, P.E., C.F.M. Development Review Engineer

Phone: (505) 884-2215 www.amafca.org

From: Cherne, Curtis [mailto:CCherne@cabg.gov]

Sent: Monday, March 22, 2010 1:17 PM

To: Mazur, Lynn

Subject: Tract A-2-A and A-3-A Brunacini Journal Center

: Lynn,

Did Fred Arfman give you a plan for these two tracts? Ours is stamp date 3-1-10.

I figure there is about 85 cfs going to the northwest corner at the outfall Looks OK to me. We will have him include his channel to your side inlet on an IL.

I would like to hear from you before I write Fred a letter.

Curtis

FEBRUARY 10, 2011

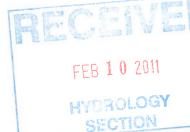
SUPPLEMENTAL INFORMATION

FOR

BRUNACINI JOURNAL CENTER OFFICE BUILDING TRACTS A2 & A3

BY





BASIN NO. A	MAFCA INLET AREA	DESCRIPTION	Entire basin that drains to inlet
Area of basin flows =	728955	SF =	16.7 Ac.
The following calculation		eas as shown in table to the right	LAND TREATMENT
	Sub-basin Weighted I	Excess Precipitation (see formula above)	A = 0%
	Weighted E	= 1.95 in.	B = 5%
		Runoff (see formula above)	C = 10%
	V ₃₆₀	= 118698 CF	D = 85%
	Sub-basin Peak Disch	arge Rate: (see formula above)	
	Q ₂	= 74.0 cfs	
BASIN NO. O	FFSITE 1	DESCRIPTION	
Area of basin flows =	324289	SF =	7.4 Ac.
The following calculation	ons are based on Treatment ar	eas as shown in table to the right	LAND TREATMENT
	Sub-basin Weighted I	Excess Precipitation (see formula above)	A = 0%
	Weighted E	= 1,95 in.	B = 5%
	Sub-basin Volume of	Runoff (see formula above)	C = 10%
	V ₃₆₀	= 52805 CF	D = 85%
	Sub-basin Peak Disch	arge Rate: (see formula above)	-nonspecime###################################
	Q _p	= 32.9 cfs	
BASIN NO. O	FFSITE 2	DESCRIPTION	
Area of basin flows =	46703	SF =	1.1 Ac.
The following calculation	ons are based on Treatment ar	eas as shown in table to the right	LAND TREATMENT
A STATE OF THE STA		excess Precipitation (see formula above)	A = 0%
	Weighted E	= 1.95 in.	B = 5%
		Runoff (see formula above)	C = 10%
	V ₃₆₀	= 7605 CF	D = 85%
		arge Rate: (see formula above)	2
	Q _P	= 4.7 cfs	
BASIN NO. O	FFSITE3	DESCRIPTION	
Area of basin flows =	122343	SF =	2.8 Ac.
		eas as shown in table to the right	LAND TREATMENT
		xcess Precipitation (see formula above)	A = 0%
	Weighted E	= 1.95 in.	B = 5%
		Runoff (see formula above)	C = 10%
	V ₃₆₀	= 19921 CF	D = 85%
	AND DESCRIPTION OF THE PERSON	arge Rate: (see formula above)	D - 8326
	Q _p	= 12.4 cfs	
BASIN NO. A	9	The state of the s	
	4/150	DESCRIPTION	South portion of site
Area of basin flows =	46417	SF =	1.1 Ac.
The following calculation		as as shown in table to the right	LAND TREATMENT
		xcess Precipitation (see formula above)	A = 0%
	Weighted E	= 1.95 in.	B = 5%
		Runoff (see formula above)	C = 10%
		= 7558 CF	D = 85%
	V ₃₆₀	D	200000000000000000000000000000000000000
	Sub-basin Peak Discha	rge Rate: (see formula above)	***************************************
		= 4.7 cfs	
ten manufacture (Charles de maior de la company)	Sub-basin Peak Dische Qp	= 4.7 cfs DESCRIPTION	North Portion of site
Area of basin flows =	Sub-basin Peak Dische Q _P 66546	= 4.7 cfs DESCRIPTION SF =	North Portion of site
Area of basin flows =	Sub-basin Peak Discher Qr Qr 66546 Ins are based on Treatment are	= 4.7 cfs DESCRIPTION SF = as as shown in table to the right	North Portion of site
Area of basin flows =	Sub-basin Peak Dische Qp 66546 are based on Treatment are Sub-basin Weighted E.	= 4.7 cfs DESCRIPTION SF = as as shown in table to the right (sees Precipitation (see formula above)	North Portion of site 1.5 Ac. LAND TREATMENT A = 0%
Area of basin flows =	Sub-basin Peak Dische Qp 66546 as are based on Treatment are Sub-basin Weighted E Weighted E	= 4.7 cfs DESCRIPTION SF = as as shown in table to the right (sees Precipitation (see formula above) = 1.95 in.	North Portion of site 1.5 Ac. LAND TREATMENT A = 0% B = 5%
Area of basin flows =	Sub-basin Peak Discher Qp Qp 66546 as are based on Treatment are Sub-basin Weighted E Sub-basin Volume of F	= 4.7 cfs DESCRIPTION SF = as as shown in table to the right (sees Precipitation (see formula above) = 1.95 in. Runoff (see formula above)	North Portion of site 1.5 Ac. LAND TREATMENT A = 0%
Area of basin flows =	Sub-basin Peak Discher Qp Qp 66546 as are based on Treatment are Sub-basin Weighted E Sub-basin Volume of F V360	= 4.7 cfs DESCRIPTION SF = as as shown in table to the right (sees Precipitation (see formula above) = 1.95 in. Runoff (see formula above) = 10836 CF	North Portion of site 1.5 Ac. LAND TREATMENT A = 0% B = 5%
Area of basin flows =	Sub-basin Peak Discher Qp Qp 66546 as are based on Treatment are Sub-basin Weighted E Sub-basin Volume of F V360	= 4.7 cfs DESCRIPTION SF = as as shown in table to the right (sees Precipitation (see formula above) = 1.95 in. Runoff (see formula above)	North Portion of site 1.5 Ac. [LAND TREATMENT] A = 0% B = 5% C = 10%

BASIN NO.	C	DESC	RIPTION		
Area of basin flows =	64541	SF		=	1.5 Ac.
The following calculat	tions are based on Treatment are	as as shown in table	to the right		LAND TREATMENT
	Sub-basin Weighted E	xcess Precipitation (see formula above	:)	A = 0%
	Weighted E	=	1.95 i	n.	B = 5%
	Sub-basin Volume of I	Runoff (see formula	above)		C = 10%
	V ₃₆₀	=	10509	CF	D = 85%
	Sub-basin Peak Discha	rge Rate: (see form	ila above)		***************************************
	Q_p	=	6.6	cfs	
BASIN NO.	D	DESC	RIPTION		
Area of basin flows =	58116	SF		=	1.3 Ac.
The following calculat	tions are based on Treatment are	as as shown in table	to the right		LAND TREATMENT
	Sub-basin Weighted E	cess Precipitation (s	ee formula above)	A = 0%
	Weighted E	==	1.95 is	1.	B = 5%
	Sub-basin Volume of I	Runoff (see formula	above)		C = 10%
	V ₃₆₀	=	9463	CF	D = 85%
	Sub-basin Peak Discha	rge Rate: (see formu	la above)		300000000000000000000000000000000000000
	Q_P	=	5.9	cfs	
BASIN NO. 1	I/4" flows	DESC	RIPTION	Backs into	calcutations of 1/4" flows. Matches volume of 1/4" x Area.
Area of basin flows =	93264	SF		=	2.1 Ac.
The following calculat	ions are based on Treatment are	as as shown in table	to the right		LAND TREATMENT
	Sub-basin Weighted Ex	cess Precipitation (s	ee formula above)	A = 0%
	Weighted E	=	1.95 is	1.	B = 55%
	Sub-basin Volume of F	unoff (see formula a	bove)		C = 10%
	V ₃₆₀	=	15187	CF	D = 85%
	Sub-basin Peak Discha	rge Rate: (see formu	la above)		0000000000 P.Tu C.T.O. C.
	Qp	=	9.5	cfs	

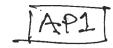
		BASIN SUMMARY	MMARY				
Basin No. Description		Discharge (Q)	AP1	AP2	AP3	AP4	Comments
MAFCA INLET ARE	Entire basin that drains to inlet	74.0					
OFFSITE 1		32.9	32.9	32.9		32.9	
OFFSITE 2		4.7		4.7		4.7	
OFFSITE 3		12.4			12.4	12.4	
Ą	South portion of site	4.7	4.7	4.7		4.7	
В	North Portion of site	8.9		8.9		8.9	
υ		9.9		9.9		9.9	
Ω		5.9			5.9	5.9	
1/4" flows lacks into	lacks into calcutations of 1/4" flows. Matches volume of 1/4" x Are;	9.5					

API AP2 AP3 OVERALL
37.6 55.7 18.3 74.0 CFS

74.0 37.6 55.7

TOTAL DISCHARGE

Channel Report



Hydraflow Express Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc.

Thursday, Feb 10 2011

Brunacini Building Drive Aisle Basin A

User-defined Invert Elev (ft) = 100.00 Slope (%) = 0.50 N-Value = 0.017

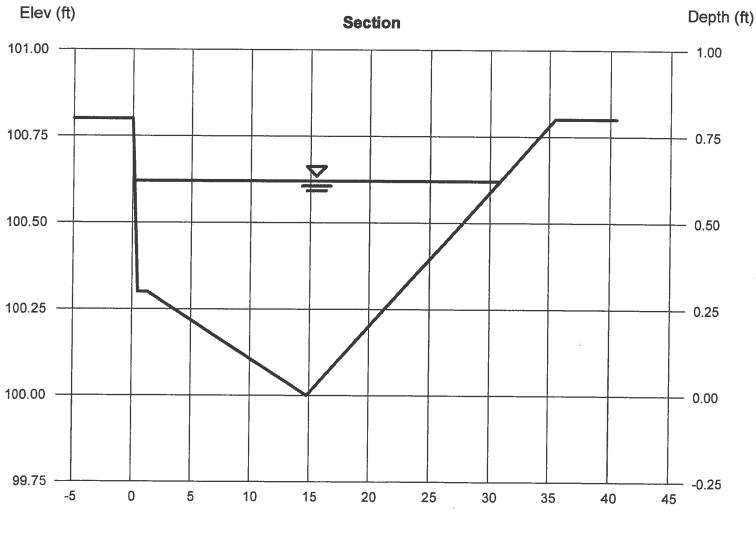
Calculations

Compute by: Known Q Known Q (cfs) = 37.60 Highlighted

Depth (ft) = 0.62 Q (cfs) = 37.60 Area (sqft) = 11.62 Velocity (ft/s) = 3.24 Wetted Perim (ft) = 30.81 Crit Depth, Yc (ft) = 0.60 Top Width (ft) = 30.66 EGL (ft) = 0.78

(Sta, El, n)-(Sta, El, n)...

(0.00, 100.80)-(0.50, 100.30, 0.013)-(1.33, 100.30, 0.013)-(14.80, 100.00, 0.017)-(35.50, 100.80, 0.017)



Sta (ft)

[AP2]

Channel Report

Hydraflow Express Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc.

Thursday, Feb 10 2011

Brunacini Building drive aisle in Basin C

 User-defined

 Invert Elev (ft)
 = 100.00

 Slope (%)
 = 0.50

 N-Value
 = 0.017

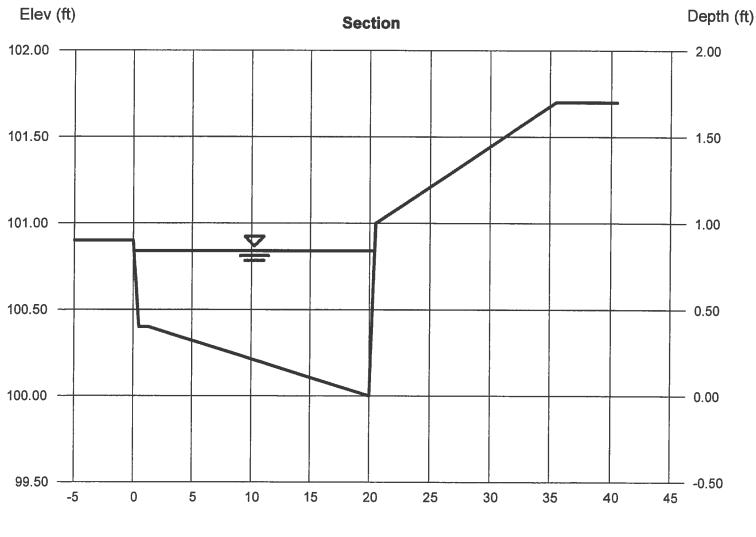
Calculations

Compute by: Known Q Known Q (cfs) = 55.70 Highlighted

Depth (ft) = 0.84 Q (cfs) = 55.70 Area (sqft) = 12.59 Velocity (ft/s) = 4.43 Wetted Perim (ft) = 21.07 Crit Depth, Yc (ft) = 0.84 Top Width (ft) = 20.36 EGL (ft) = 1.14

(Sta, El, n)-(Sta, El, n)...

(0.00, 100.90)-(0.50, 100.40, 0.013)-(1.33, 100.40, 0.017)-(20.00, 100.00, 0.017)-(20.50, 101.00, 0.013)-(35.50, 101.70, 0.017)



Sta (ft)

Channel Report



Hydraflow Express Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc.

Thursday, Feb 10 2011

1756 Brunacini Building - Shotcrete Rundown in AMAFCA R/W

Trapezoidal

Bottom Width (ft) = 18.00

Side Slopes (z:1) = 10.00, 10.00

Total Depth (ft) = 1.00 Invert Elev (ft) = 74.90

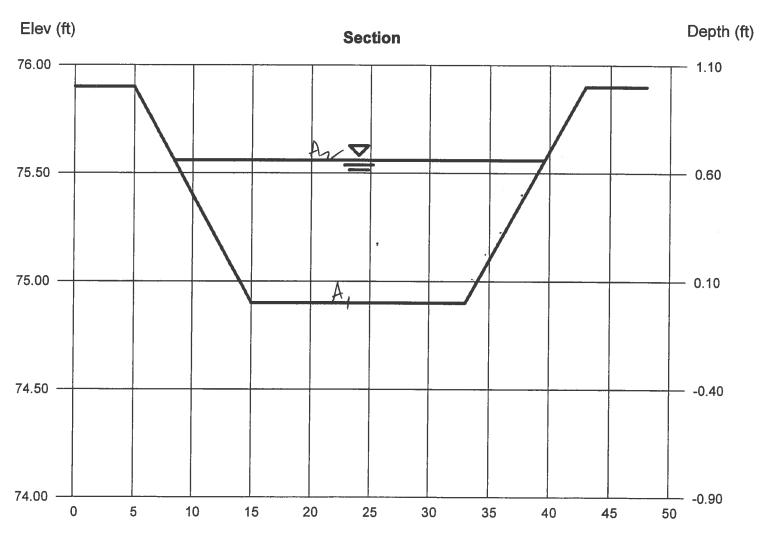
Slope (%) = 0.75 N-Value = 0.018

Calculations

Compute by: Known Q Known Q (cfs) = 74.00 Highlighted

Depth (ft) = 0.66 Q (cfs) = 74.00 Area (sqft) = 16.24 Velocity (ft/s) = 4.56 Wetted Perim (ft) = 31.27 Crit Depth, Yc (ft) = 0.71 Top Width (ft) = 31.20

EGL (ft) = 0.98



Reach (ft)

SEDIMENT CONTROL POND

0.25" OVER TOTAL AREA OF ONSITE AND OFFSITE BASINS

Maximum Pond Volume = 0.25 inches x 728954.53 SF = 15,187 CF

		TDEATE	TPEATWENT BOND WOILING		
		BRUNACI	BRUNACINI JOURNAL CENTER		
			1/24/2011		
ELEV	AREA (SF)	VOLUME (CF)	ADD'L VOL (CF) (1)	SUM VOL (CF)	SUM VOL (Ac-ft)
7.07	2542.874				
		769.6	1,726.0		
74	2587.673			2,495.6	0.057292
		2,656.1	28.3		
72	2724.47			5,180.0	0.118916
		2,783.5	28.3		
73	2842.545			7,991.8	0.183465
		2,892.6	28.3		
74	2942.615			10,912.6	0.250519
		2,984.0	28.3		
75	3025.387			13,924.9	0.319671
NOTES:					
(1)	Additional volume ba	sed on 30% voids in g	ume based on 30% voids in gravel bed, and capacity in perforated pipes.	in perforated pipes, 6'	6' dia manhole.
	24" SD and sump for	ump for pump. See calcs below.	ow.		
Gravel bed volume	l volume:				
3' deep	3' deep x 1516.4 sf area x 30	ea x 30% voids =	1,364.8		
Perforated pipes	pipes				
8" dia >	8" dia x 60 lf x 3 pipes =		62.8		
6' dia manhole	nole				
3' deep	3' deep x 6' dia =		84.8		
24" storm drain	Irain				
24" dia	24" dia x 32 lf =		100.5		
6' dia sum	6' dia sump for pump at 71.0 elev				
4' deep	4' deep x 6' dia =		113.1		
			1,726.0	total below bottom of pond	puod
6' dia sum	ξ	each addn'l foot of elev			
1' deen	1' deep x 6' dia =		28.2		

(6

Channel Report

Hydraflow Express Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc.

Thursday, Feb 10 2011

1756 Brunacini Building - Stormwater Treatment Pond Inlet Weirs (Divide Width by 3

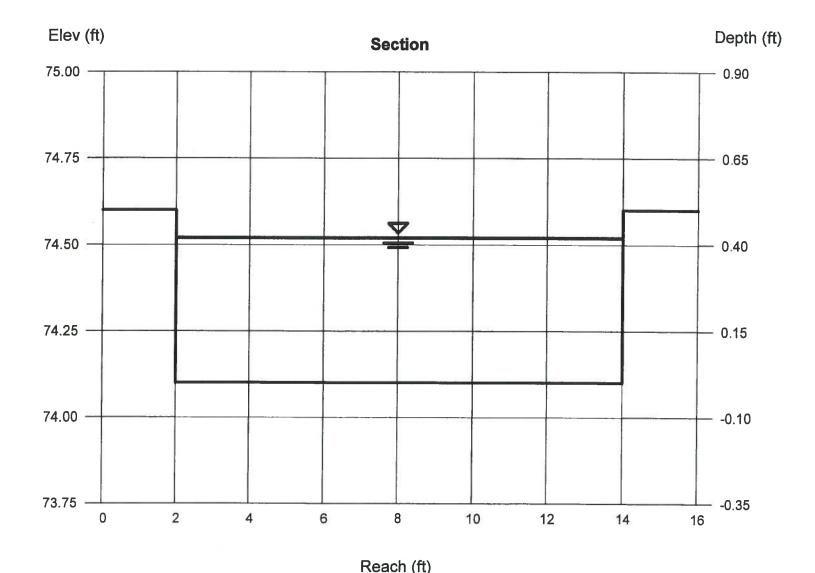
Rectangular
Bottom Width (ft) = 12.00
Total Depth (ft) = 0.50
Invert Elev (ft) = 74.40
Slope (%) = 0.10
N-Value = 0.013

Calculations
Compute by:

Known Q (cfs)

Known Q = 9.50

Highlighted
Depth (ft) = 0.42
Q (cfs) = 9.500
Area (sqft) = 5.04
Velocity (ft/s) = 1.88
Wetted Perim (ft) = 12.84
Crit Depth, Yc (ft) = 0.27
Top Width (ft) = 12.00
EGL (ft) = 0.48



PERFORATED PIPE CALCULATIONS

(Using Orifice Equation)

Brunacini Project Name:

Project #:

2.5 cfs 5074.9 ft 5071.9 ft 100-year WSEL =
Bottom of Gravel Pit ELEV =
Maximum discharge (Q_{max}) = Diameter of pipe =

Orifice Equation: Q = CA(2gH)^{1/2}

0.60 (sharp edged hole) 32.2 ft/s² **"**

ii B

		HOLE C	HOLE CALCULATIONS	SNC		
	HOLE	HOLE	# OF HOLES		OPER	Q PER TOTAL Q AT
ELEVATION AT	DIAMETER	AREA	AT THIS		HOLE	THIS LEVEL
CENTER OF HOLE	(in.)	(sq. ft.)	LEVEL	H (ft)	(cfs)	(cfs)
- 5069.73	0.5	0.001	177	5.17	0.01	2.64
5069,44	0.5	0.001	177	5.46	0.02	2.71

TOTAL Q WITHOUT CLOGGING =

2.68 TOTAL Q WITH 50% CLOGGING =

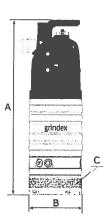
Convert to GPM for pump calcs =

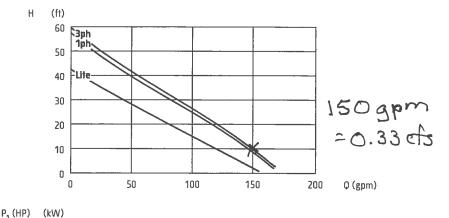
1201.73

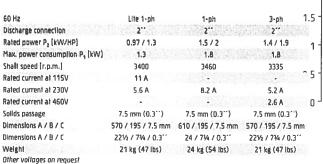
Minex

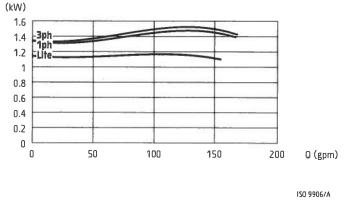
Electrical submersible drainage pump











Electrical submersible drainage pump Protection class: IP 68

Electrical motor

1-phase: Squirrel cage induction motor with start and run capacitor 3-phase: Squirrel cage induction motor

Insulation class: F (IEC 85) **Motor protection**

1-phase: Temperature guard with a thermal contact in stator opening temperature 125°C (257°F), air valve

3-phase: Phase sequence control, phase failure guard, temperature guard with thermal contacts in the stator opening temperature 125°C (257°F) (= SMART system), air valve

Cable - SubCab

1-phase: 3G1,5mm2, 20 m (66 ft) / 14AWG/3, 53 ft 3-phase: 4G1,5mm2, 20 m (66 ft) / 14AWG/4, 53 ft

Limitations

Max. submersion depth: 20 m (66 ft) Max. liquid temperature: 40 °C (104 °F)

Allowed pH range: 5 - 8

Maximum liquid density: 1100 kg/m³ (68 lbs/ft³)

Shaft seals

2 -

Cartridge seal: pre-assembled double mechnical seal running in an oil compartment

Material lower seal: tungsten carbide - tungsten carbide Material upper seal: tungsten carbide - tungsten carbide

Bearings

Ball bearings with C3 clearance

Discharge connection

2" hose, ISO-G or NPT

Materials

Casted parts: Aluminium Outer casing: Stainless steel Motor shaft: Stainless steel Impelier: Hard-Iron™ Diffusers: Nitrile rubber Screws and nuts: Stainless steel O-rings: Nitrile rubber

Accessories

Float switch (max 400 V) Zinc anodes Low suction collar Pump raft

Specifications can be changed without notice

- Version: 1997.02d

```
9.5 cfs IN
           START TIME (HR:MIN:SEC) = 14:29:23 USER NO.= AHYMO-I-9702dIsa-Arfman1
                                                                                                   0.33 cfs ow
           INPUT FILE = 17561stf.txt
*S
            BRUNACINI
*S
              FIRST FLUSH STORM
*S
             17561STF.DAT
*S
              FEB 09,2011
*5
             GENNY DONART
            ISAACSON & ARFMAN, P.A.
*$*******************
             HYDROLOGIC MODEL FOR FIRST FLUSH TREATMENT
*S
*S
              100-year, 6-hour storm
*S
*S
              PRECIPITATION:
*S
             P15 = 1.06"
             P60 =
                            1.77"
                           2.37"
*S
              P360 =
*S
              P1440 =
                           2.68"
*S
*8
              LAND TREATMENT ASSUMPTIONS:
*S
              DEVELOPED AREAS:
*5
              DETERMINE THE PERCENT OF IMPERVIOUS AREA (LAND TREATMENT TYPE "D")
              FROM SECTION 22.2 OF THE D.P.M. FOR ALBUQUEROUE, VOL. 2. TABLE 5
*5************************
START
                       RAINFALL BEGINS AT 0.0 HRS
RAINFALL
                       TYPE=1
                       RAIN QUARTER=1.06
                       RAIN ONE=1.77
                       RAIN SIX=2.37
                       RAIN DAY=2.68
                       DT=0.033333 HRS
                 COMPUTED 6-HOUR RAINFALL DISTRIBUTION BASED ON NOAA ATLAS 2 - PEAK AT 1.40 HR.
                  DT = .033333 \text{ HOURS} END TIME = 5.999940 HOURS
                     .0000 .0055 .0110
                                                 .0167 .0225
                                                                  .0284 .0345
                     .0406 .0470 .0534 .0600
.0881 .0956 .1033 .1113
                                                         .0668 .0737
.1195 .1279
                                                                              .0808
                                                                              .1366
                     .1456 .1550 .1646 .1747 .1851 .1961 .2075
                     .2194 .2319 .2452 .2501 .2553 .2609 .2729
.2998 .3412 .4006 .4818 .5884 .7243 .8935
                    1.1000 1.2911 1.3710 1.4385 1.4986 1.5532 1.6035

    1.6502
    1.6938
    1.7347
    1.7732
    1.8095
    1.8438
    1.8763

    1.9071
    1.9363
    1.9639
    1.9902
    2.0152
    2.0215
    2.0276

    2.0335
    2.0392
    2.0447
    2.0501
    2.0553
    2.0603
    2.0653

                    2.0701 2.0748 2.0794 2.0839 2.0883 2.0926 2.0969

    2.1010
    2.1051
    2.1091
    2.1131
    2.1170
    2.1208
    2.1246

    2.1283
    2.1320
    2.1356
    2.1392
    2.1427
    2.1462
    2.1497

    2.1531
    2.1564
    2.1597
    2.1630
    2.1663
    2.1695
    2.1726

                    2.1758 2.1789 2.1820 2.1850 2.1881 2.1910 2.1940

      2.1969
      2.1999
      2.2027
      2.2056
      2.2084
      2.2113
      2.2140

      2.2168
      2.2196
      2.2223
      2.2250
      2.2277
      2.2303
      2.2330

                    2.2356 2.2382 2.2408 2.2433 2.2459 2.2484 2.2509

    2.2534
    2.2559
    2.2584
    2.2608
    2.2633
    2.2657
    2.2681

    2.2705
    2.2729
    2.2752
    2.2776
    2.2799
    2.2822
    2.2845

    2.2868
    2.2891
    2.2914
    2.2937
    2.2959
    2.2981
    2.3004

                    2.3026 2.3048 2.3070 2.3091 2.3113 2.3135 2.3156
                   2.3177 2.3199 2.3220 2.3241 2.3262 2.3283 2.3303 2.3324 2.3345 2.3365 2.3385 2.3406 2.3426 2.3446
                    2.3466 2.3486 2.3506 2.3526 2.3545 2.3565 2.3584
                    2.3604 2.3623 2.3643 2.3662 2.3681 2.3700
* ENTIRE TREATMENT AREA
COMPUTE NM HYD
                   ID=1 HYD NO=101 AREA=0.02614766 SQ MI
                       PER A=0 PER B=5 PER C=10 PER D=85
                       TP=-0.1333 HR MASS RAIN=-1
     K = .072649HR TP = .133300HR K/TP RATIO = .545000
                                                                                  SHAPE CONSTANT, N = 7.106420
     UNIT PEAK = 87.748 CFS UNIT VOLUME = .9992 B = 526.28 P60 = 1.7700
AREA = .022226 SQ MI IA = .10000 INCHES INF = .04000 INCHES PER HOUR
     RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = .033333
```

.003922 SQ MI IA = .40000 INCHES INF = .97000 INCHES PER HOUR

AHYMO PROGRAM (AHYMO 97) -

RUN DATE (MON/DAY/YR) = 02/09/2011

PRINT HYD

ID=1 CODE=1

PARTIAL HYDROGRAPH 101.00

RUNOFF VOLUME = 1.92881 INCHES 2.6898 ACRE-FEET PEAK DISCHARGE RATE = 65.66 CFS AT 1.500 HOURS BASIN AREA = .0261 SQ. MI.

DIVIDE HYD

ID=1 Q=9.5 CFS ID ONE=2 HYD ONE=102

ID TWO=3 HYD TWO=103

PRINT HYD

ID=2 CODE=1

PARTIAL HYDROGRAPH 102.00

RUNOFF VOLUME = 1.92880 INCHES = 1.2578 ACRE-FEET

PEAK DISCHARGE RATE = 9.50 CFS AT 1.300 HOURS BASIN AREA = .0122 SQ. MI.

PRINT HYD ID=3 CODE=1

PARTIAL HYDROGRAPH 103.00

RUNOFF VOLUME = 1.92880 INCHES = 1.4320 ACRE-FEET

PEAK DISCHARGE RATE = 56.16 CFS AT 1.500 HOURS BASIN AREA = .0139 SQ. MI.

* TREATMENT POND WITH SUMP PUMP

ROUTE RESERVOIR ID=10 HYD NO=110 INFLOW ID=2 CODE=5 0 0 70.7 0.326 0.057292 71.0 0.328 0.118916 72.0 0.330 0.183465 73.0 0.332 0.250519 74.0 9.5 337 0.319671 75.0 OUTFLOW(CFS) STORAGE(AF) ELEV(FT)

1400s 2 + 2

* * * * * * * * * *

TIME	INFLOW	ELEV	VOLUME	OUTFLOW						
(HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)	Т	IME	INFLOW	ELEV	VOLUME	OUTFLOW
						HRS)	(CFS)	(FEET)	(AC-FT)	(CFS)
.00	.00	70.70	.000	.00		,	,	,,	(1.0 11)	(015)
.17	.00	70.70	.000	.00		5.83	.79	74.05	.254	.78
.33	.00	70.70	.000	.00		6.00	.81	74.05	.254	.80
.50	.00	70.70	.000	.00		6.17	.32	74.03	.253	.60
.67	1.47	70.73	.006	.03		6.33	.09	73.98	.249	.33
.83	2.94	70.89	.036	.21		6.50	.04	73.93	.246	.33
1.00	3.88	71.35	.079	.33		6.67	.02	73.86	.241	.33
1.17	2.89	72.10	.125	.33		6.83	.01	73.80	.237	.33
1.33	9.50	73.43	.212	.33		7.00	.00	73.73	.232	.33
1.50	9.50	74.72	.300	6.92	- hre	7.17	.00	73.66	.228	.33
1.67	9.50	74.96	.317	9.09		7.33	.00	73.60	.223	.33
1.83	9.50	74.99	.319	9.44	•	7.50	.00	73.53	.219	.33
2.00	9.50	75.00	.320	9.49	into storm	7.67	.00	73.46	.214	.33
2.17	7.09	74.94	.316	8.97	a lic	7.83	.00	73.39	.210	.33
2.33	3.56	74.52	.287	5.14		8.00	.00	73.32	.205	.33
2.50	2.38	74.30	.272	3.13	C 11	8.17	.00	73.26	.201	.33
2.67	1.73	74.20	.264	2.12	full	8.33	.00	73.19	.196	.33
2.83	1.36	74.14	.260	1.58	•	0.50	.00	73.12	.192	.33
3.00	1.13	74.10	.258	1.26		8.67	.00	73.05	.187	.33
3.17	.98	74.08	.256	1.07		8.83	-00	72.98	.182	.33
3.33	.89	74.07	.255	.94		9.00	.00	72.91	.178	.33
3.50	.83	74.06	.255	.86		9.17	.00	72.84	.173	.33
3.67	.79	74.05	.254	.81		9.33	.00	72.77	.169	.33
3.83	.77	74.05	.254	.78		9.50	.00	72.70	.164	.33
4.00	.75	74.05	.254	.76		9.67	.00	72.63	.160	.33
4.17	.74	74.05	.254	.75	:	9.83	.00	72.56	.155	.33
4.33	.74	74.04	.254	.74	1	0.00	.00	72.49	.151	.33
4.50	.73	74.04	.254	.73	1	0.17	.00	72.42	.146	.33
4.67	.73	74.04	.254	.73	1.	0.33	.00	72.35	.142	. 33
4.83	.74	74.04	.254	.73	10	0.50	.00	72.28	.137	.33
5.00	.74	74.04	.254	.74	10	0.67	.00	72.21	.133	.33
5.17	.75	74.04	.254	.74		0.83	.00	72.14	.128	.33
5.33	.76	74.05	.254	.75		1.00	-00	72.07	.124	.33
5.50	76	74.05	.254	.76		1.17	.00	72.00	.119	.33
5.67	.78	74.05	.254	.77	1:	1.33	.00	71.93	.114	.33

TIME (HRS)	INFLOW (CFS)	ELEV [FEET)	VOLUME	OUTFLOW (CFS)		TIME (HRS)	INFLOW (CFS)	ELEV	VOLUME	OUTFLOW
()	(615)	(LDD1)	(AC-EI)	(023)		(nka)	(CES)	(FEET)	(AC-FT)	(CFS)
11.50	.00	71.85	.110	.33		15.67	.00	70.81	.020	.11
11.67	.00	71.78	.105	.33		15.83	.00	70.80	.019	.11
11.83	.00	71.71	.101	.33		16.00	.00	70.79	.017	.10
12.00	.00	71.63	.096	.33		16.17	.00	70.78	.016	.09
12.17	.00	71.56	.092	.33		16.33	.00	70.78	.015	.08
12.33	.00	71.49	.087	.33		16.50	.00	70.77	.014	.08
12.50	.00	71.42	.083	.33		16.67	.00	70.77	.013	.07
12.67	.00	71.34	.078	.33		16.83	.00	70.76	.012	.07
12.83	.00	71.27	.074	.33		17.00	.00	70.76	.011	.06
13.00	.00	71.20	.069	.33		17.17	.00	70.75	.010	.06
13.17	.00	71.12	.065	.33		17.33	.00	70.75	.009	.05
13.33	.00	71.05	.060	.33		17.50	.00	70.74	.009	.05
13.50	.00	70.99	.056	.32		17.67	.00	70.74	.008	.04
13.67	.00	70.97	.052	.29		17.83	.00	70.74	.007	.04
13.83	.00	70.95	.048	.27		18.00	.00	70.74	.007	.04
14.00	.00	70.93	.044	.25		18.17	.00	70.73	.006	.04
14.17	.00	70.91	.041	.23		18.33	.00	70.73	.006	.03
14.33	.00	70.90	.038	.22		18.50	.00	70.73	.005	.03
14.50	.00	70.88	.035	.20		18.67	.00	70.73	.005	.03
14.67	.00	70.87	.032	.18		18.83	.00	70.72	.005	.03
14.83	.00	70.86	.030	.17		19.00	.00	70.72	.004	.02
15.00	.00	70.84	.028	.16		19.17	.00	70.72	.004	.02
15.17	.00	70.83	.026	.15		19.33	.00	70.72	.004	.02
15.33	.00	70.82	.024	.13		19.50	.00	70.72	.003	.02
15.50	.00	70.81	.022	.12		19.67	.00	70.72	.003	.02
						19.83	.00	70.71	.003	.02
PEAK DISC	HARGE =	9.4	197 CFS -	PEAK OCCUR	S AT HOUR	2.10				
MAXIMUM W	ATER SURF			75.000						
MAXIMUM S			3196 AC-F		REMENTAL TI	ME= 0	33333HRS			
		•	orro no r	11101	WILLIAM III	.0	JJJJJIKS			

PRINT HYD

ID=10 CODE=1

PARTIAL HYDROGRAPH 110.00

RUNOFF VOLUME = 1.92473 INCHES = 1.2552 ACRE-FEET PEAK DISCHARGE RATE = 9.50 CFS AT 2.100 HOURS BASIN AREA = .0122 SQ. MI.

FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 14:29:23