

July 28, 2000

Chris Weiss, P.E.
C.L.Weiss Engineering
P.O. Box 97
Sandia Park, NM 87047

Attn: Bryan Bobrick

RE: HOPE CHRISTIAN SCHOOL CAMPUS ADDITION (D18-D9). Revised GRADING AND DRAINAGE PLAN FOR BUILDING PERMIT APPROVAL. ENGINEER'S

STAMP DATED JULY 17, 2000.

Dear Mr. Weiss:

Based on the information provided in your July 19, 2000 submittal, the above referenced project is approved forBuilding Permit. Please furnish the Zone Atlas and FIRM Panel numbers on Sheet C-2. Also, note that only the Inspector's signature now is required on the SO#19 Permit.

Please attach a copy of this approved plan to the construction sets prior to sign-off by Hydrology.

A separate permit is required for construction within the City right-of-way. A copy of this approval letter must be on hand when applying for the excavation permit.

Prior to Certificate of Occupancy approval, an Engineer's Certification per the DPM will be required.

If I can be of further assistance, please feel free to contact me at 924-3984.

Sincerely,

John P. Murray, I

Hydrology

ca Pam Lujan
Whitney Reierson

File



May 18, 2000

Chris Weiss, PE C.L. Weiss Engineering, Inc. PO Box 97 Sandia Park, NM 87047

Hope Christian School Campus Additions Grading and Drainage Plan Re: Engineer's Stamp dated 5-3-00, (B18/D9)

Dear Mr. Weiss,

Based on your resubmittal dated 5-3-00, the above referenced plan is approved for Building Permit and SO#19 Permit.

Please attach a copy of this approved plan to the construction sets prior to sign-off by Hydrology.

A separate permit is required for construction within City R/W. A copy of this approval letter must be on hand when applying for the excavation permit.

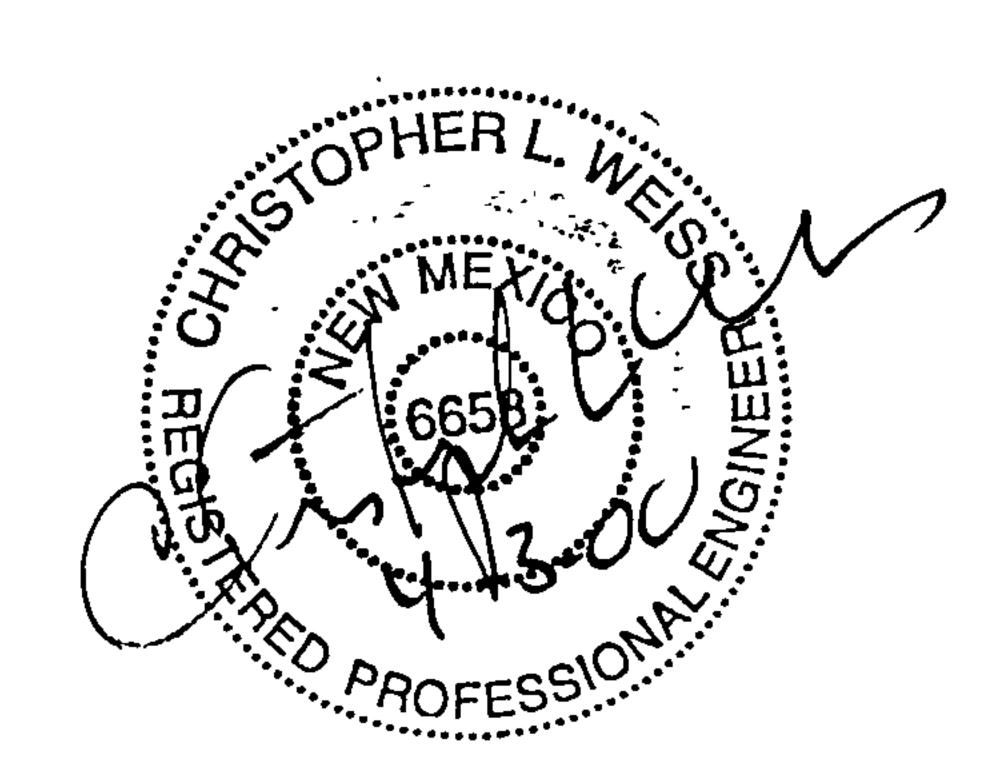
Also, prior to Certificate of Occupancy release, Engineer Certification per the DPM checklist will be required.

If you have any questions, you can contact me at 924-3986.

Bradley L. Bingham, PE

Hydrology Review Engineer





C.L. Welss Engineering, Inc. P.O. Box 97 Sandla Park, NM 87047 Tele/Fax - (505) 281-1800 E-Mall - clwnm@earthlink.net

# Background

### Palomas Campus

The Palomas Hope Christian School is a private facility located west of Louisiana Blvd., between Palomas Ave. and the Domingo Baca concrete channel. The purpose of this report is an update of the original drainage submittal to reflect proposed campus improvements, including an athletic field expansion, a music building addition, and paving an existing gravel parking area. These items reflect the overall land use patterns established by the original site plan prepared by Dekker-Perich Architects, dated 3-23-94. Additionally, this submittal provides current information regarding new classrooms and other campus changes which have been constructed in the interim period.

The site is isolated from any off-site drainage due the presence of the surrounding streets, with Louisiana Blvd. draining to an inlet connected to the Domingo Baca channel, and Palomas Ave. directing flows west past the campus.

Internal flows are handled by a central drainage swale which provides the main flow path through the campus, with secondary routes collecting flows from the south and north sides. All flows converge at the SW corner of the site and drain over a concrete rundown into the Domingo Baca channel (see photos).

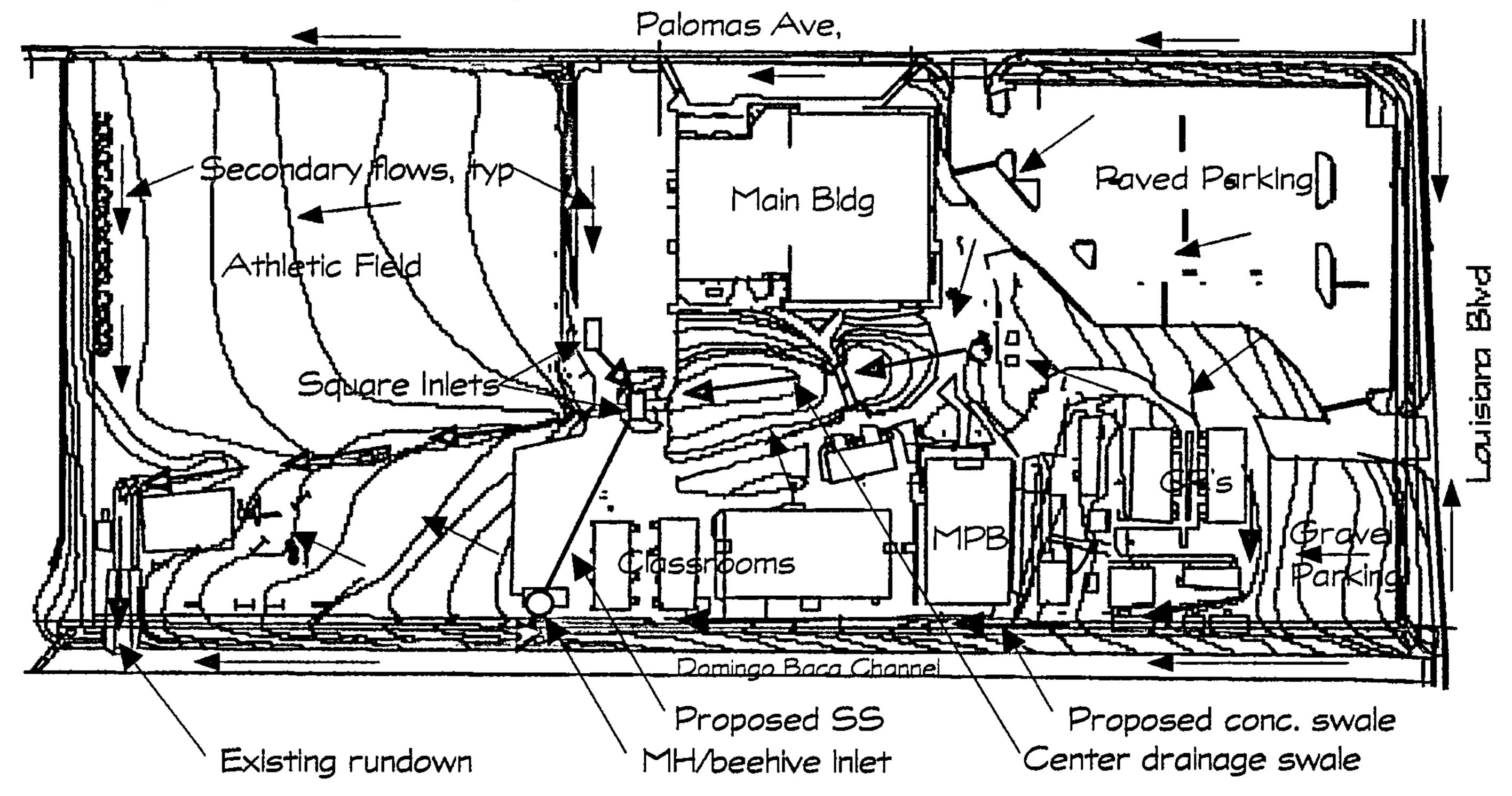
Flow patterns throughout the campus will remain unchanged, with the exception of two areas where drainage paths are in conflict with the proposed improvements. The first drainage improvement concerns flows crossing the athletic/playground area from the center drainage swale and the west parking area. Storm runoff from these sub-basins will be intercepted by a new SS system and routed directly into Domingo Baca channel. The inlets will be positioned to collect flows at the existing low points for each sub-basin, thus minimizing changes to the existing infrastructure.

The second proposed area of improvement is the south drainage route. Beginning at the east existing gravel parking lot, shown as a future paved area on the grading plan, drainage follows a western route to the east side of the Multipurpose Building, then north to the center campus swale. The proposed music building addition will create a conflict with this flow path. However, it is possible to redirect the drainage to the west along the south side of the proposed Multipurpose/Music Building. Swale improvements will consist of a concrete valley gutter to define the flow path and improve flow characteristics along the south side of the campus. The valley gutter section will extend from the east parking area, west to the new SS referenced above. Flows will be intercepted at a new drop inlet, eliminating surface drainage from this portion of the campus crossing the athletic field.

As a result of these improvements, the athletic field will be protected from upstream campus flows and flow patterns along the south side of campus will be improved.



### Existing Campus Drainage



Reconstruction of the athletic field, with a regulation sized soccer field reorientated in a N-S direction, will block the existing surface flow patterns crossing the southern portion of the field. Surface flows from the center drainage swale and west parking area will be captured by new storm inlets located as shown above (red line).

Additional drainage improvements will be constructed along the south side of the campus. A concrete swale will direct those flows to a new inlet on the SS line located near the outlet into the Domingo Baca channel (green arrows).

The existing surface rundown located at the SW corner of the campus will remain to serve as a discharge point for drainage from the athletic field.

### Drainage System Notes

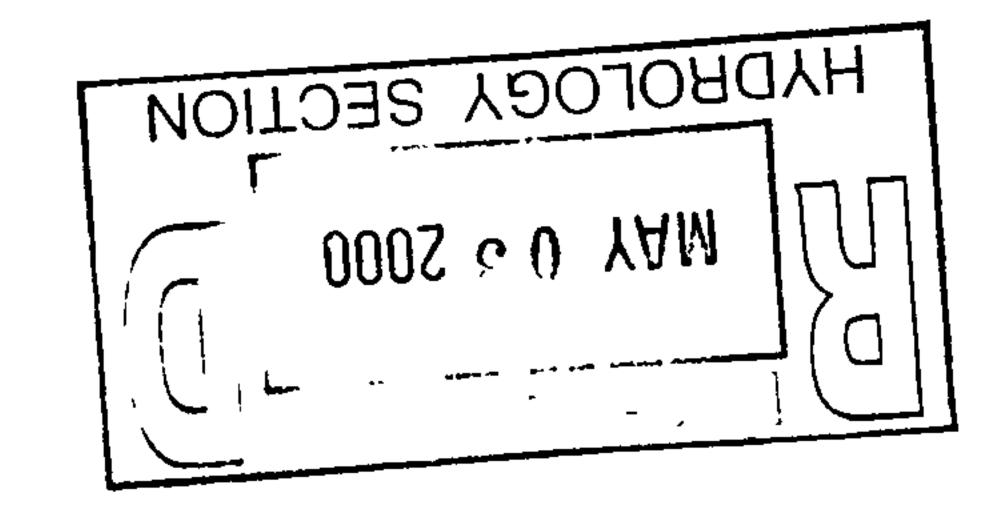
The campus drainage improvements will include a SS pipe system, using either a COA Type "D" Inlet with a Neenah steel square grate (Catg # R-3574-L), or a standard 6' dia MH with a Neenah round grate (Catg #R-2561). A triple inlet will be required for the center drainage swale, along with a single inlet to intercept runoff from the west parking area. A MH with a round beehive grate will be required at the outlet of the south drainage swale. The SS pipe will be an 12" dia PVC pipe between the first two inlets, a 24" dia PVC pipe for the second reach, with the remaining SS a 36" dia. RCP from the MH to the outlet into the Domingo Baca channel.

The south surface swale will be a 3' wide concrete valley gutter, following a route from the southeast parking area along the south side of the campus (see grading plan).

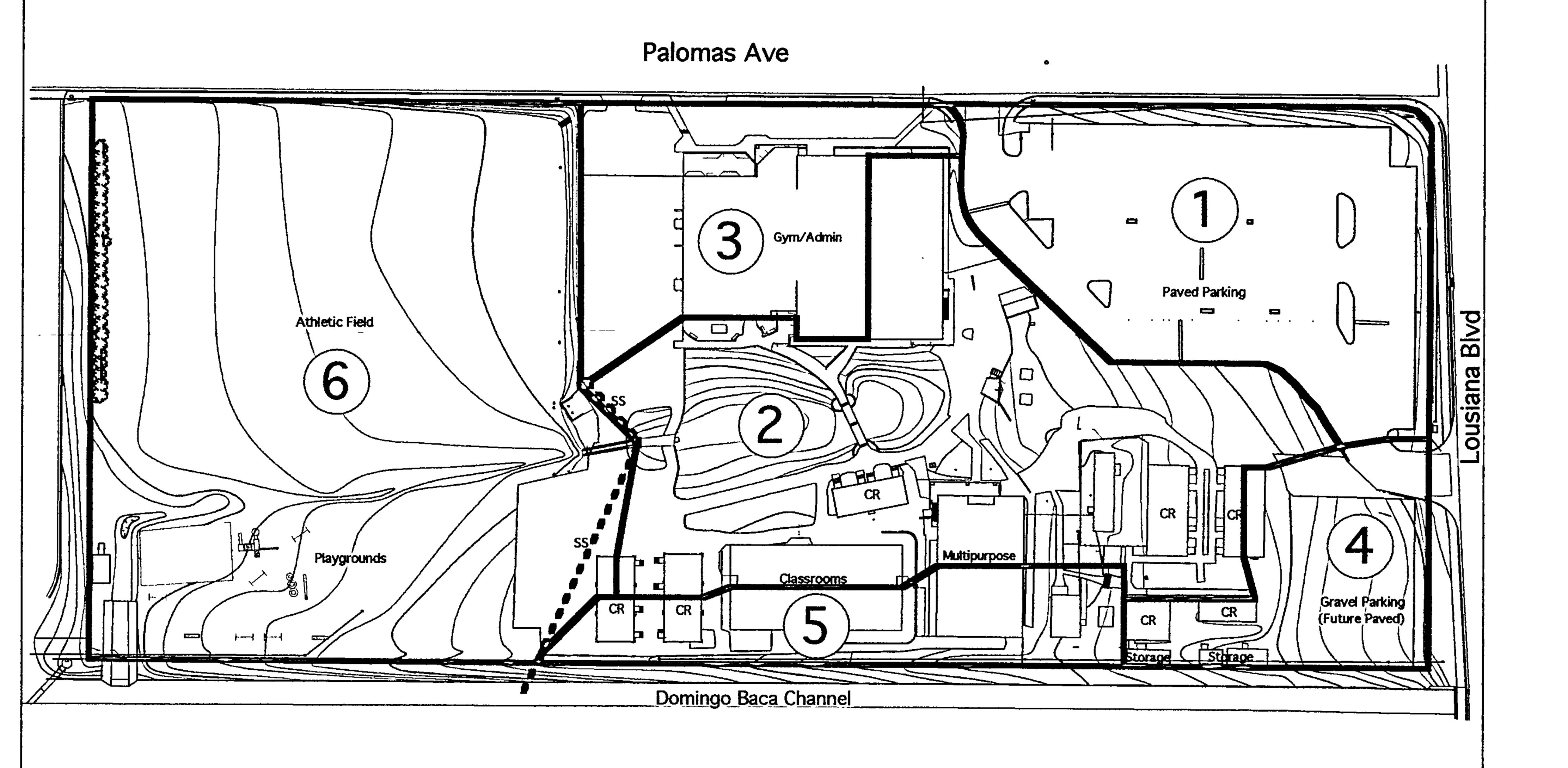


# Calculations

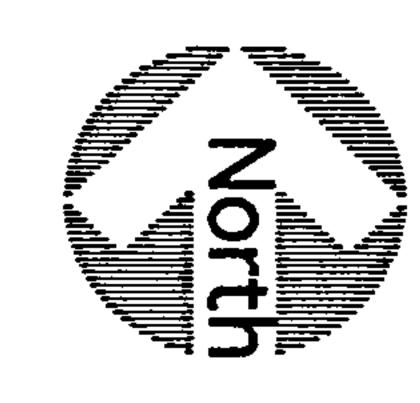
The following calculations analyze the peak flows generated for the internal sub-basins, reflecting the proposed campus improvements. Storm sewer summary data and design profiles reflect the proposed SS drainage improvements.







Drainage Sub-basins



| Calculations are based on the  |  | County Section 22.2, DPM, Vol.2, date  |   |
|--------------------------------|--|--|---|
| Calculations are based on the  |  |  |   |
| Area of sub-basin flows =      | 58017 SF                               | 1 - East Parking Area  | 16 Δο   |
|                                | based on Treatment areas as shown in   |  | 1.6 Ac.   |
| THE TOHOWING CARCUIAMONS are   |  | ——————————————————————————————————————   |   |
|                                | Sub-basin Weighted Excess Precipitat   |  | TDEATMENT   |
|                                | Weighted E =                           | 2.27 in.   | TREATMENT   |
|                                | Sub-basin Volume of Runoff (see for    |  | A = 0%  |
|                                | V360 =                                 | 10996 CF   | B == 0%   |
|                                | Sub-basin Peak Discharge Rate: (see    | formula above)   | C = 8%  |
| <del>,</del>                   | Qp =                                   | 6.5 cfs  | D = 92%   |
|                                |  | - Center Drainage Swale  |   |
| Area of sub-basin flows =      | 91592 SF                               |  | 2.1 Ac.   |
| The following calculations are | based on Treatment areas as shown in   |  |   |
|                                | Sub-basin Weighted Excess Precipitat   | <del></del>  | <del>                                      </del> |
|                                | Weighted E =                           | 2.02 in.   | TREATMENT   |
|                                | Sub-basin Volume of Runoff (see form   | mula above)  | A = 0%  |
|                                | V360 =                                 | 15422 CF   | B = 5%  |
|                                | Sub-basin Peak Discharge Rate: (see    | formula above)   | C = 25%   |
|                                | Qp =                                   | 9.5 cfs  | D = 70%   |
| !<br>}                         | SUB-BASIN 3 - Adi                      | min Bldg / West Parking Area   |   |
| Area of sub-basin flows =      | 35588 SF                               | ==   | 0.8 Ac.   |
| The following calculations are | based on Treatment areas as shown in   | table to the right   |   |
|                                | Sub-basin Weighted Excess Precipitat   | tion (see formula above)   |   |
|                                | Weighted E =                           | 2.29 in.   | TREATMENT   |
|                                | Sub-basin Volume of Runoff (see for    | والمناف والمناف والمنافع والمن | A = 0%  |
|                                | V360 =                                 | 6785 CF  | B = 5%  |
|                                | Sub-basin Peak Discharge Rate: (see    |  | C = 0%  |
|                                | On =                                   | 4.0 cfs  | D = 95%   |
|                                | CIID DACINIA                           |  |   |
| Area of sub-basin flows =      | 23402 SF                               | - Southeast Parking Area   | 0.5 Ac.   |
|                                | based on Treatment areas as shown in   | <u></u>  |   |
| The following calculations are | Sub-basin Weighted Excess Precipitat   |  |   |
|                                | Weighted E =                           | 2.04 in.   | TREATMENT   |
|                                |  |  | ······································            |
|                                | Sub-basin Volume of Runoff (see for    |  | A = 0%  |
|                                | V360 =                                 | 3976 CF  | B = 0%  |
|                                | Sub-basin Peak Discharge Rate: (see    |  | C = 30%   |
|                                | Qp ==                                  | 2.4 cfs  | D = 70%   |
| A 0 1 1 · 0                    |  | - South Drainage Swale   |   |
| Area of sub-basin flows =      | 22941 SF                               |  | 0.5 Ac.   |
| The following calculations are |  | 4  |   |
|                                | Sub-basin Weighted Excess Precipitat   |  | CD 25 A CO2 A CO3                                 |
|                                | Weighted E =                           | 2.00 in.   | TREATMENT   |
|                                | Sub-basin Volume of Runoff (see for    |  | A = 0%  |
|                                | V360 ==                                | 3827 CF  | B = 10%   |
|                                | Sub-basin Peak Discharge Rate: (see    | formula above)   | C = 20%   |
|                                | Qp =                                   | 2.4 cfs  | D = 70%   |
|                                | SUB-BAS                                | IN 6 - Athletic Field  |   |
| Area of sub-basin flows =      | 140675 SF                              |  | 3.2 Ac.   |
| The following calculations are | e based on Treatment areas as shown in |  |   |
|                                | Sub-basin Weighted Excess Precipitat   | tion (see formula above)   |   |
|                                | 337-1-1-4-1 72                         | 1 00   | TREATMENT   |
|                                | Weighted E =                           | 1.06 in.   |   |
|                                | Sub-basin Volume of Runoff (see for    |  | A = 0%  |
|                                | <u> </u>                               |  | A = 0%<br>B = 90%                                 |
|                                | Sub-basin Volume of Runoff (see for    | mula above) 12473 CF   |   |

|  | St  | IMMARY |            |                               |
|--|-----|--------|------------|-------------------------------|
| Developed Discharge Rate - Sub-Basin 1 | === | 6.5    | CFS        | Drain to Basin 2              |
| Developed Discharge Rate - Sub-Basin 2 | =   | 9.5    | <b>CFS</b> | Drain to SS Inlet             |
| Developed Discharge Rate - Sub-Basin 3 | =   | 4.0    | <b>CFS</b> | Drain to SS Inlet             |
| Developed Discharge Rate - Sub-Basin 4 | =   | 2.4    | <b>CFS</b> | Drain to valley gutter        |
| Developed Discharge Rate - Sub-Basin 5 | ==  | 2.4    | <b>CFS</b> | Drain to SS Inlet             |
| Developed Discharge Rate - Sub-Basin 6 | ==  | 2.2    | <b>CFS</b> | Drain to existing rundown     |
|  |     | 34.0   | <b>CFS</b> | Drain to Domingo Baca Channel |

### Inlet Capacity - Sub-Basins 1 & 2

| Q = C*A * (2 | 2*g*h) ^ 0.5 |      |                    |
|--------------|--------------|------|--------------------|
| Where        | Q =          | 11.1 | cfs                |
|              | C =          | 0.6  |                    |
|              | A =          | 2.30 | sq.ft.             |
|              | g =          | 32.2 | sq.ft.<br>ft/sec^2 |
|              | h =-         | 1    | ft                 |

Note: Area (A) at left, is based on the open area of a Neenah single steel square grate (Catg # 3574 -L - vane inlet). Based on calculations shown, a single inlet with a head of 1' will accept 11.1 cfs. If the inlet becomes 50% clogged, the inlet will accept 5.5 cfs. Combined flows from Sub-Basins 1 & 2 of 16 cfs will require a triple inlet. Orient vanes in direction of flow.

### Inlet Capacity - Sub-Basin 3

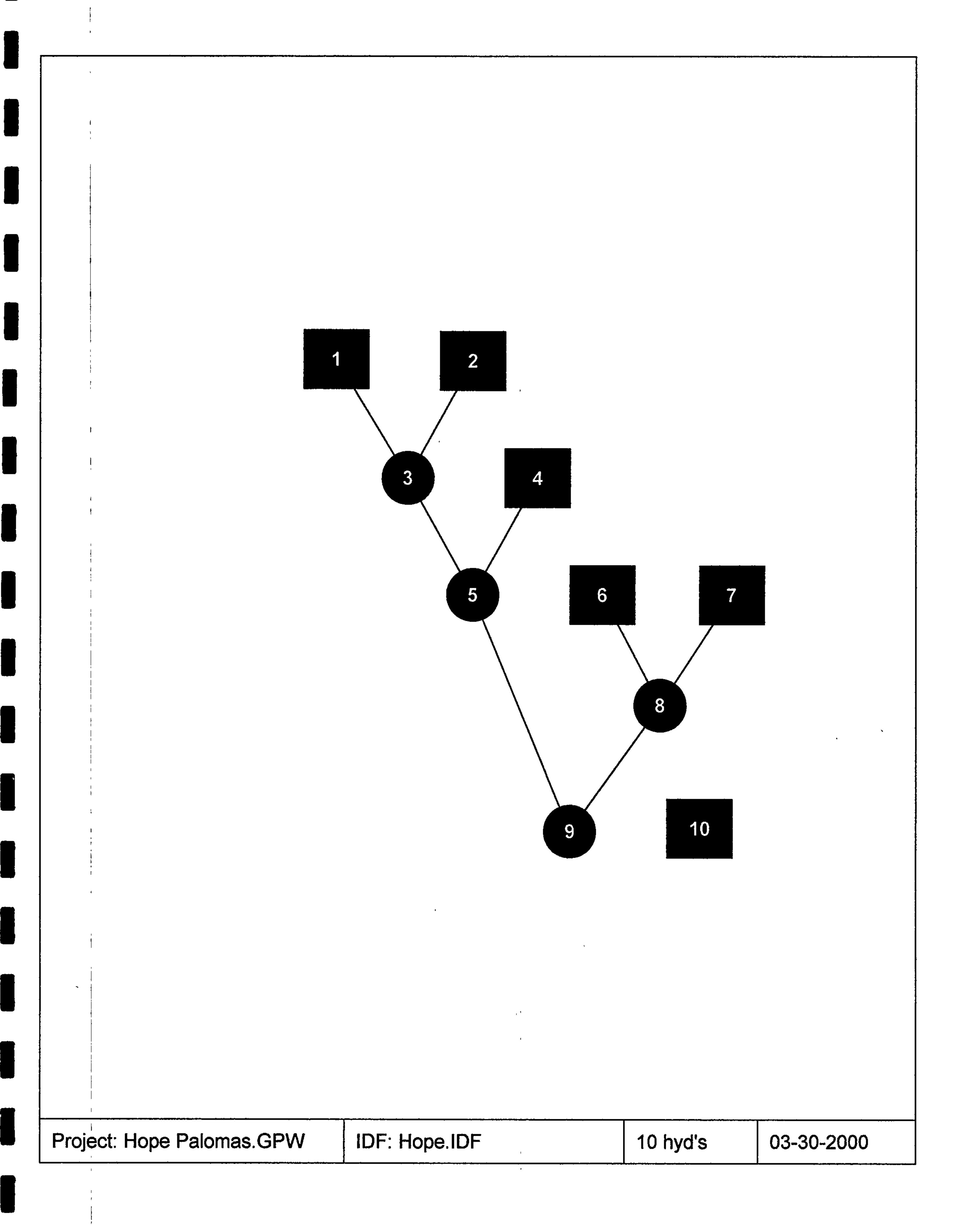
| Q = C*A * (2 | 2*g*h) ^ 0.5 |      |          |
|--------------|--------------|------|----------|
| Where        | Q ==         | 7.8  | cfs      |
|              | C =          | 0.6  |          |
|              | A =          | 2.30 | sq.ft.   |
|              | g = _        | 32.2 | ft/sec^2 |
|              | h =          | 0.5  | ft       |

Note: Area (A) at left, is based on the open area of a Neenah single steel square grate (Catg # 3574 -L - vane inlet). Based on calculations shown, a single inlet with a head of 0.5' will accept 7.8 cfs. If the inlet becomes 50% clogged, the inlet will accept 3.9 cfs. Flows from Sub-Basin 3 of 4 cfs will require a single inlet. Orient vanes in direction of flow.

### Inlet Capacity - Sub-Basins 4 & 5

| Q = C*A * (2 | 2*g*h) ^ 0.5 |      |                    |
|--------------|--------------|------|--------------------|
| Where        | Q =          | 9.6  | cfs                |
| 1            | C =          | 0.6  |                    |
|              | A =          | 2.00 | sq.ft.             |
|              | g ==         | 32.2 | sq.ft.<br>ft/sec^2 |
|              | h =          | 1    | ft                 |

Note: Area (A) at left, is based on the open area of a single Neenah steel round beehive grate (Catg # R-2561). Based on calculations shown, a single inlet with a head of 1.0' will accept 9.6 cfs. If the inlet becomes 50% clogged, the inlet will accept 4.8 cfs. Flows from Sub-Basins 4 & 5 of 4.8 cfs will require a single inlet.



# Hydrograph Plot

**English** 

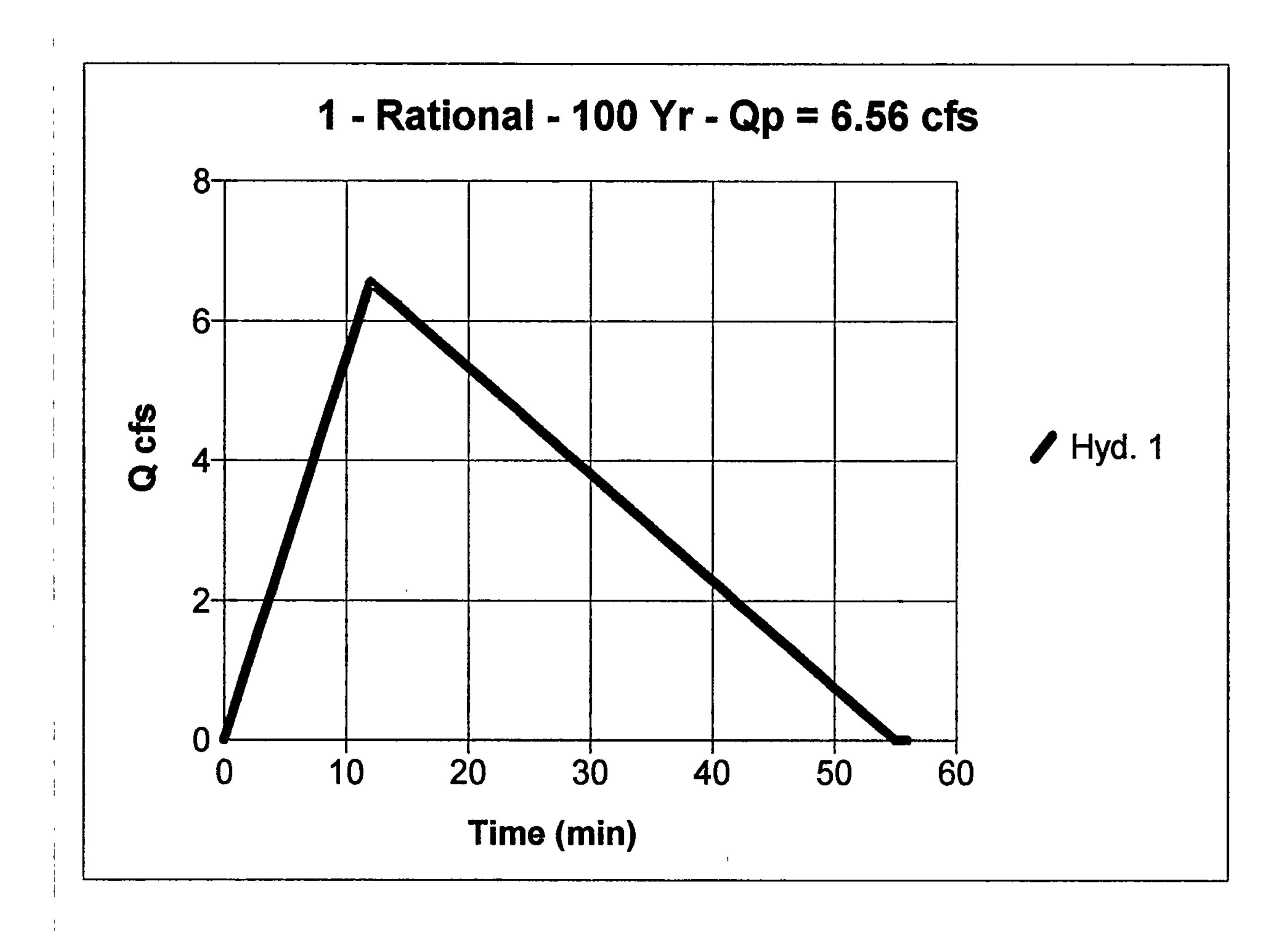
### Hyd. No. 1

Sub-basin 1

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 1.6 ac
Intensity = 6.12 in
I-D-F Curve = Hope.IDF

Peak discharge = 6.56 cfs
Time interval = 1 min
Runoff coeff. = 0.67
Time of conc. (Tc) = 12 min
Reced. limb factor = 3.657

Total Volume = 10,997 cuft



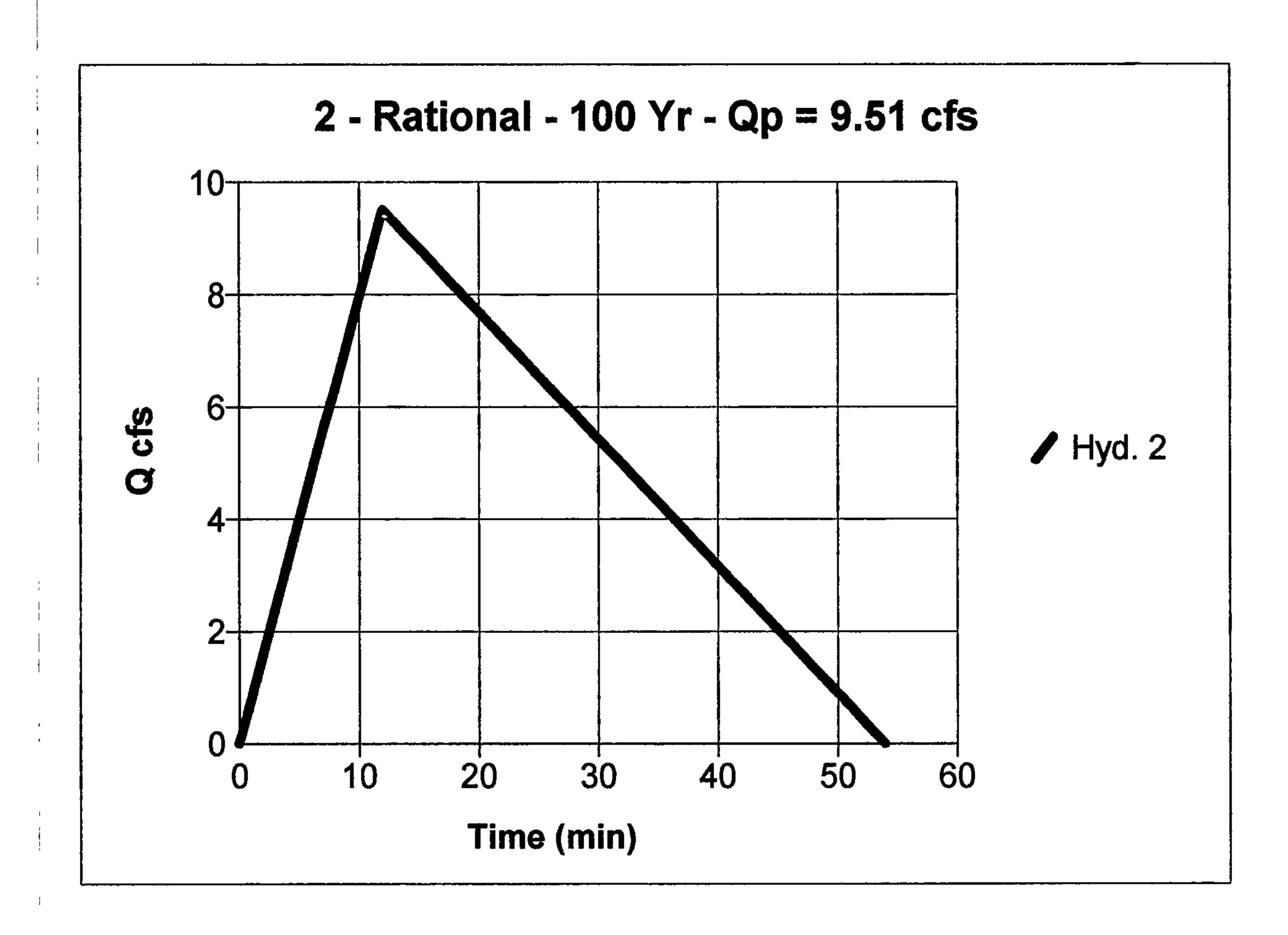
### Hyd. No. 2

Sub-basin 2

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 2.1 ac
Intensity = 6.12 in
I-D-F Curve = Hope.IDF

Peak discharge = 9.51 cfs
Time interval = 1 min
Runoff coeff. = 0.74
Time of conc. (Tc) = 12 min
Reced. limb factor = 3.505

Total Volume = 15,422 cuft



Hyd. No. 3

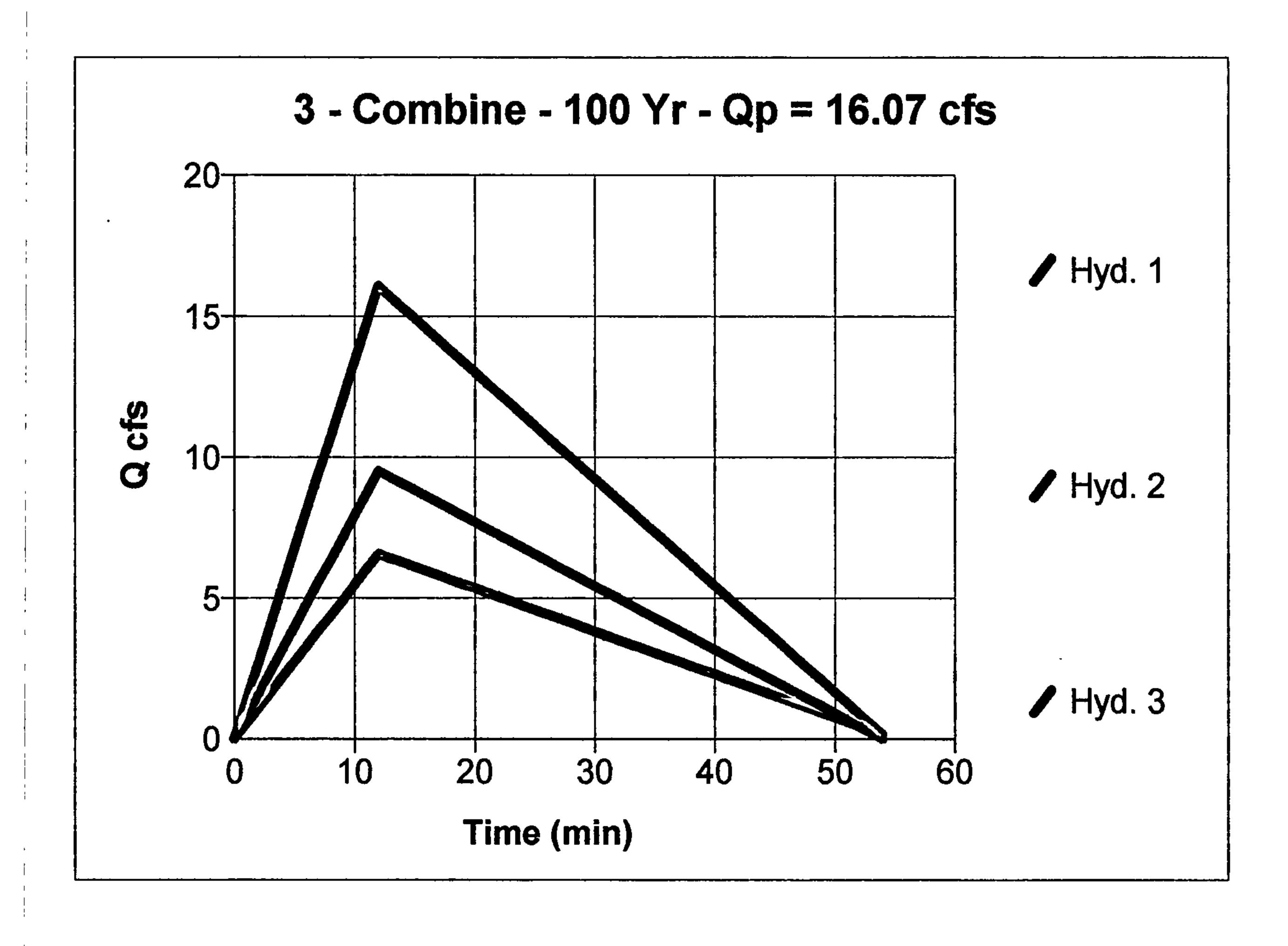
Basin 1 & 2

Hydrograph type = Combine Storm frequency = 100 yrs

1st inflow hyd. No. = 1

Peak discharge = 16.07 cfs
Time interval = 1 min
2nd inflow hyd. No. = 2

Total Volume = 26,228 cuft



# Hydrograph Plot

**English** 

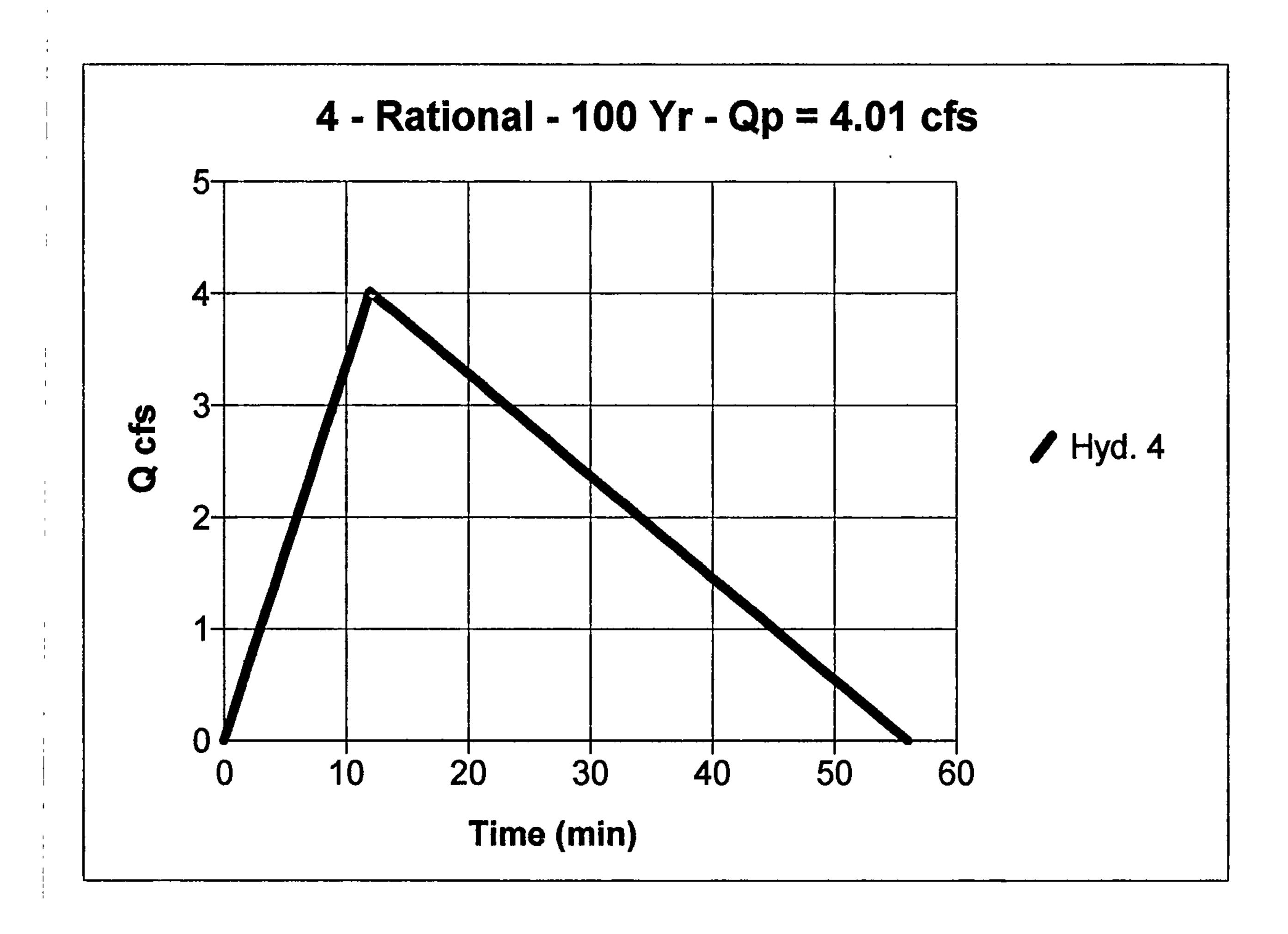
### Hyd. No. 4

Sub-basin 3

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 0.8 ac
Intensity = 6.12 in
I-D-F Curve = Hope.IDF

Peak discharge = 4.01 cfs
Time interval = 1 min
Runoff coeff. = 0.82
Time of conc. (Tc) = 12 min
Reced. limb factor = 3.696

· Total Volume = 6,786 cuft



Hyd. No. 5

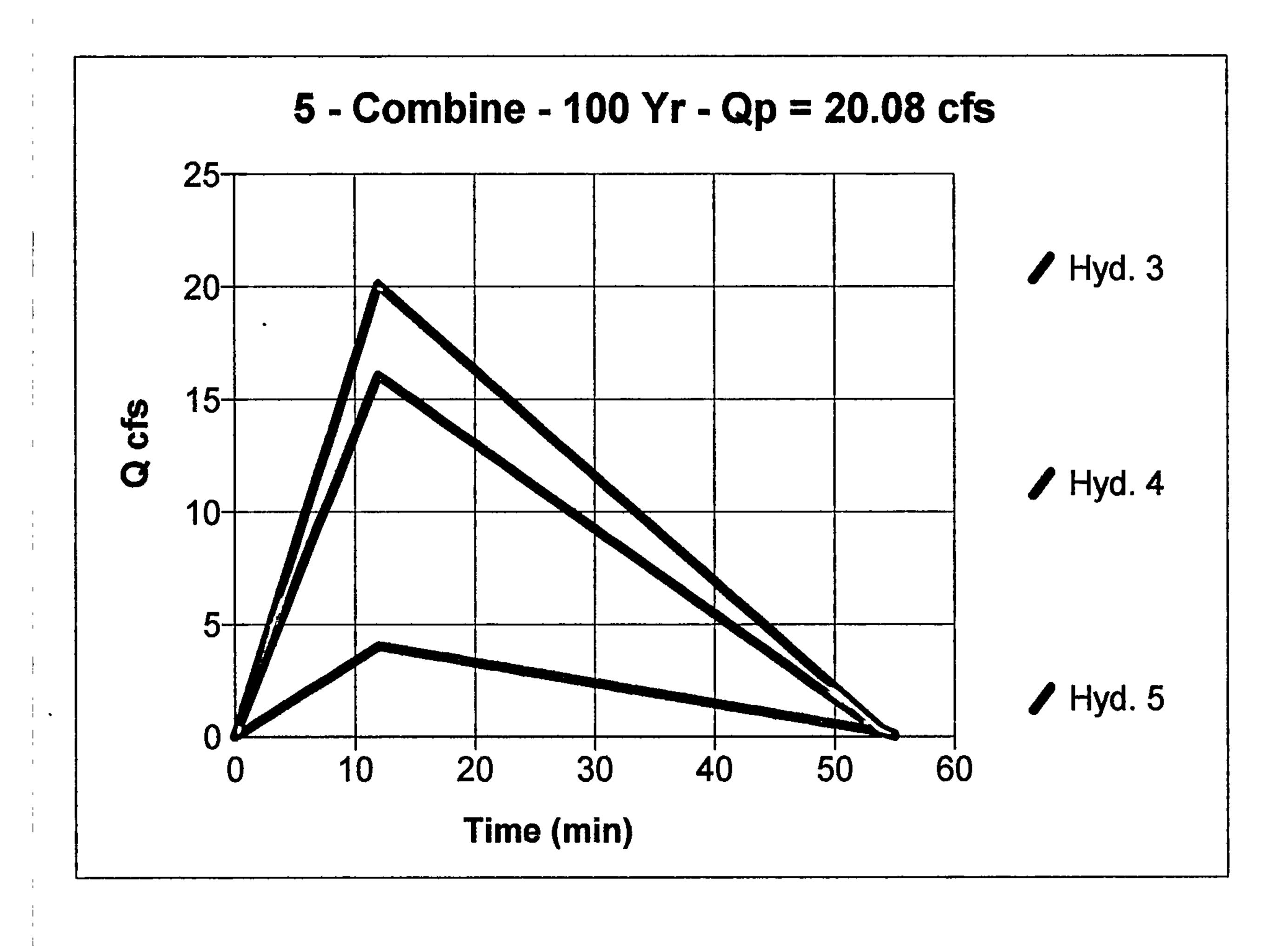
Basin 1 -3

Hydrograph type = Combine Storm frequency = 100 yrs

1st inflow hyd. No. = 3

Peak discharge = 20.08 cfs
Time interval = 1 min
2nd inflow hyd. No. = 4

Total Volume = 32,972 cuft



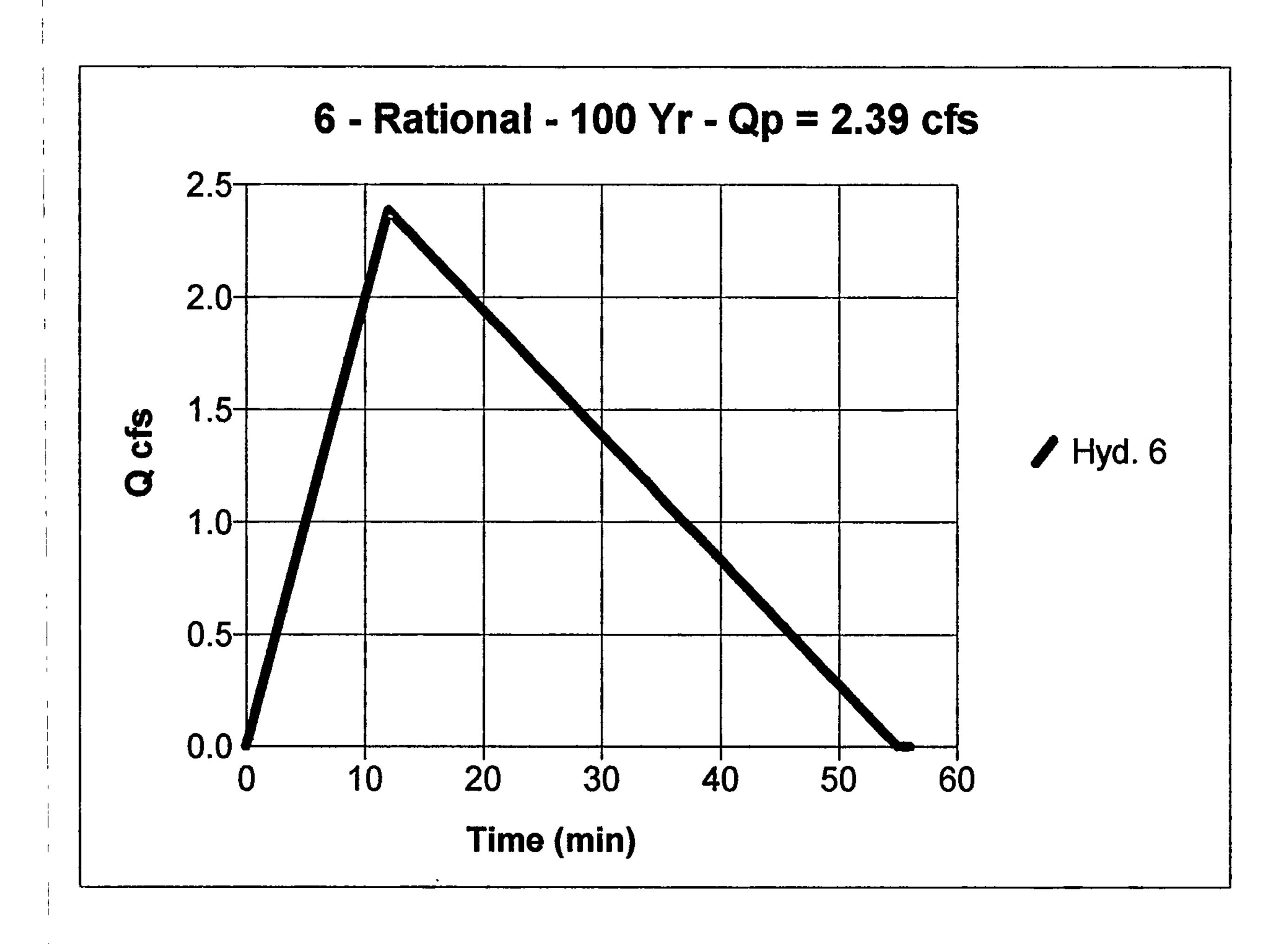
### Hyd. No. 6

Sub-basin 4

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 0.5 ac
Intensity = 6.12 in
I-D-F Curve = Hope.IDF

Peak discharge = 2.39 cfs
Time interval = 1 min
Runoff coeff. = 0.78
Time of conc. (Tc) = 12 min
Reced. limb factor = 3.6285

Total Volume = 3,976 cuft



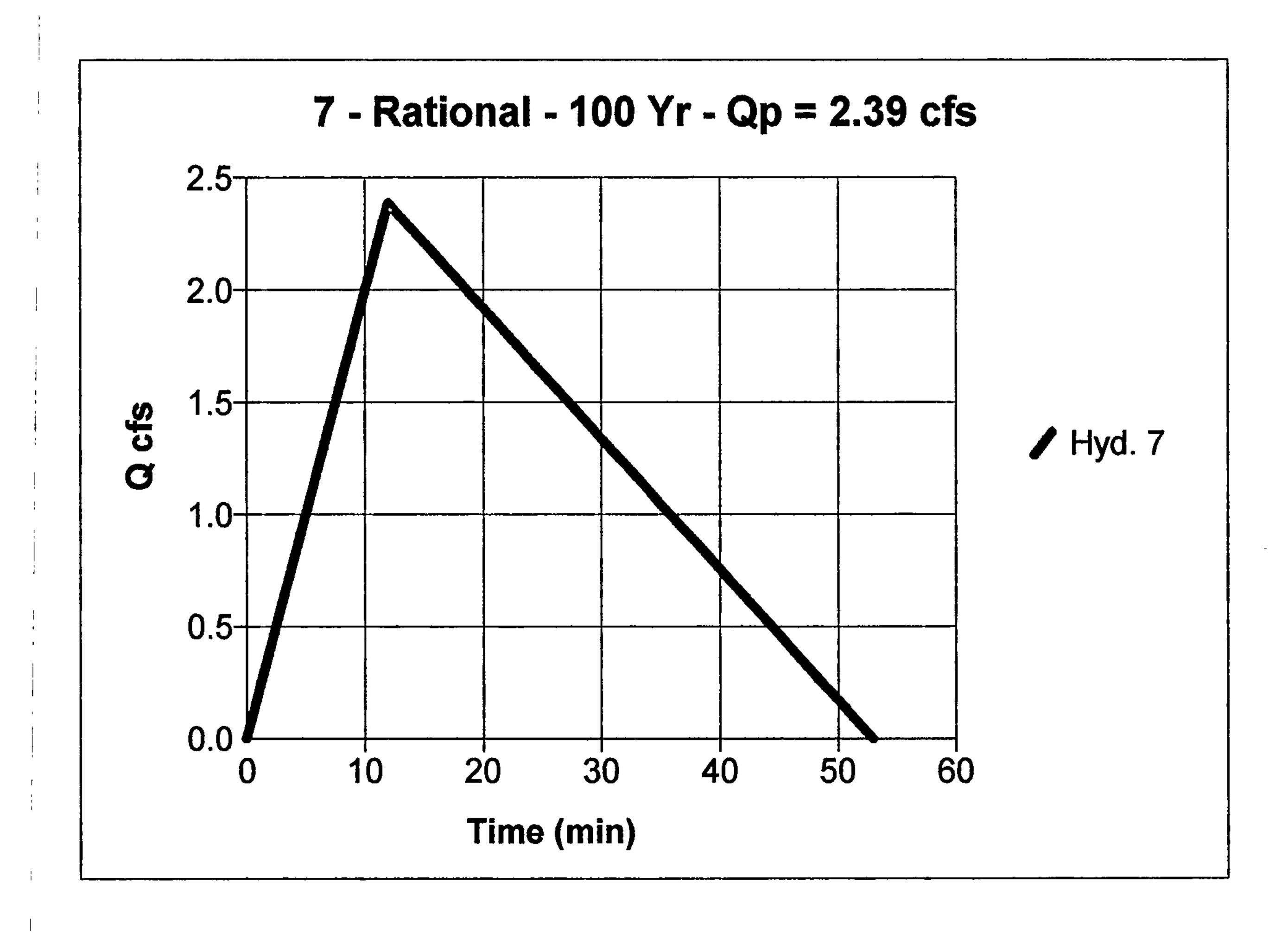
### Hyd. No. 7

Sub-basin 5

Hydrograph type = Rational
Storm frequency = 100 yrs
Drainage area = 0.5 ac
Intensity = 6.12 in
I-D-F Curve = Hope.IDF

Peak discharge = 2.39 cfs
Time interval = 1 min
Runoff coeff. = 0.78
Time of conc. (Tc) = 12 min
Reced. limb factor = 3.454

Total Volume = 3,827 cuft



Hyd. No. 8

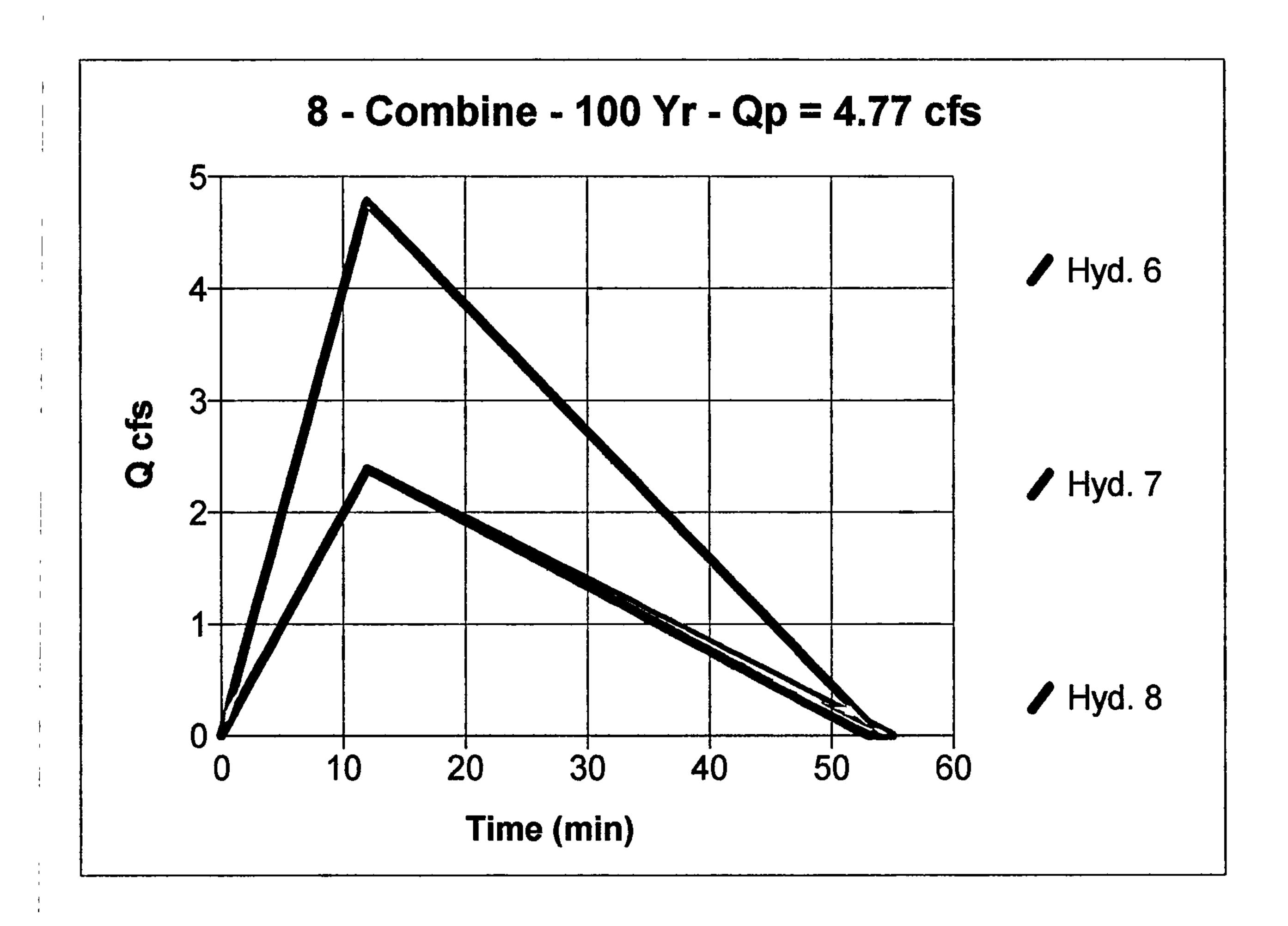
South Basins

Hydrograph type = Combine Storm frequency = 100 yrs

1st inflow hyd. No. = 6

Peak discharge = 4.77 cfs
Time interval = 1 min
2nd inflow hyd. No. = 7

Total Volume = 7,732 cuft



# Hydrograph Plot

English

Hyd. No. 9

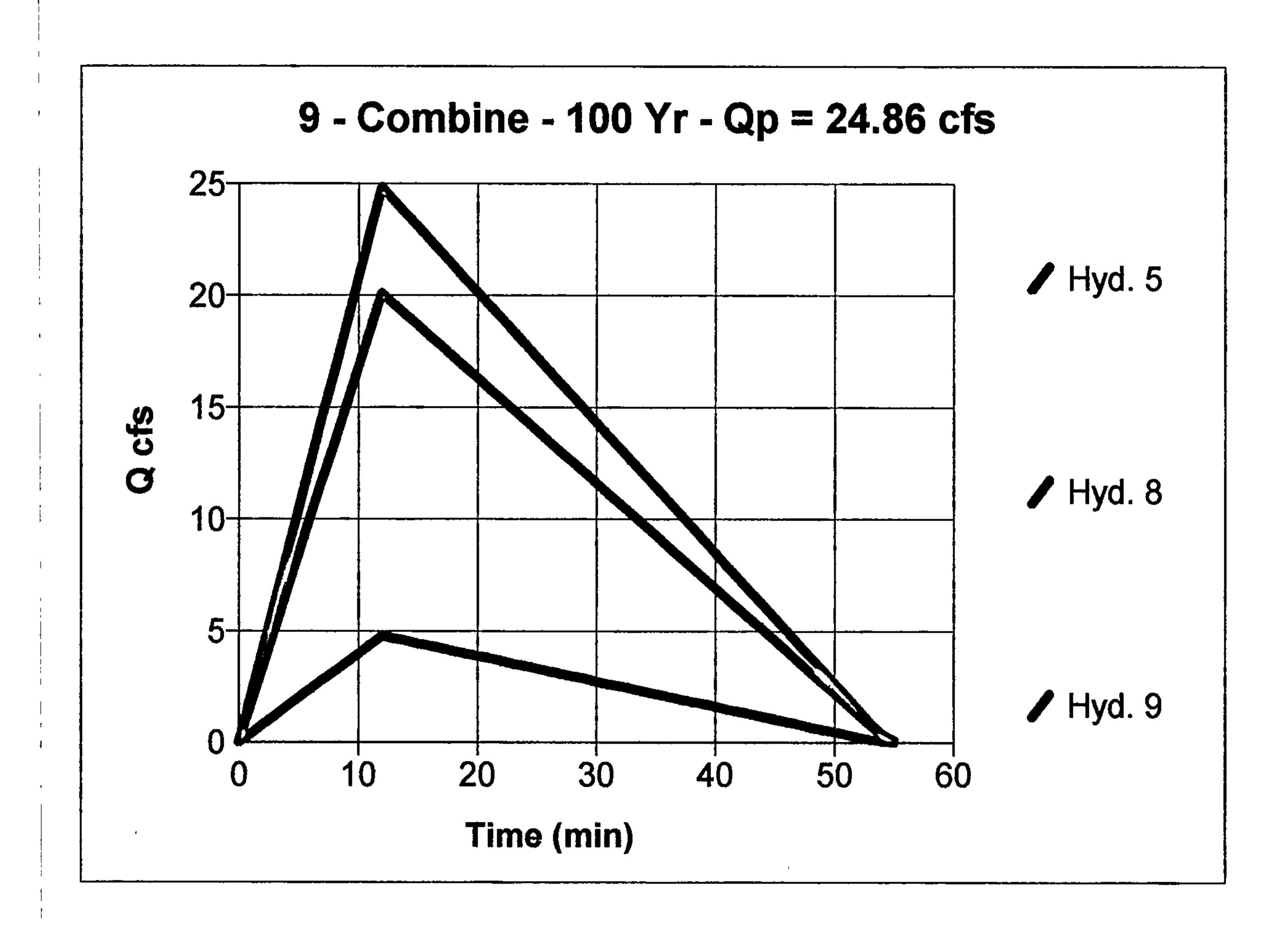
SS Outlet

Hydrograph type = Combine Storm frequency = 100 yrs

1st inflow hyd. No. = 5

Peak discharge = 24.86 cfs Time interval = 1 min 2nd inflow hyd. No. = 8

Total Volume = 40,704 cuft



# Hydrograph Plot

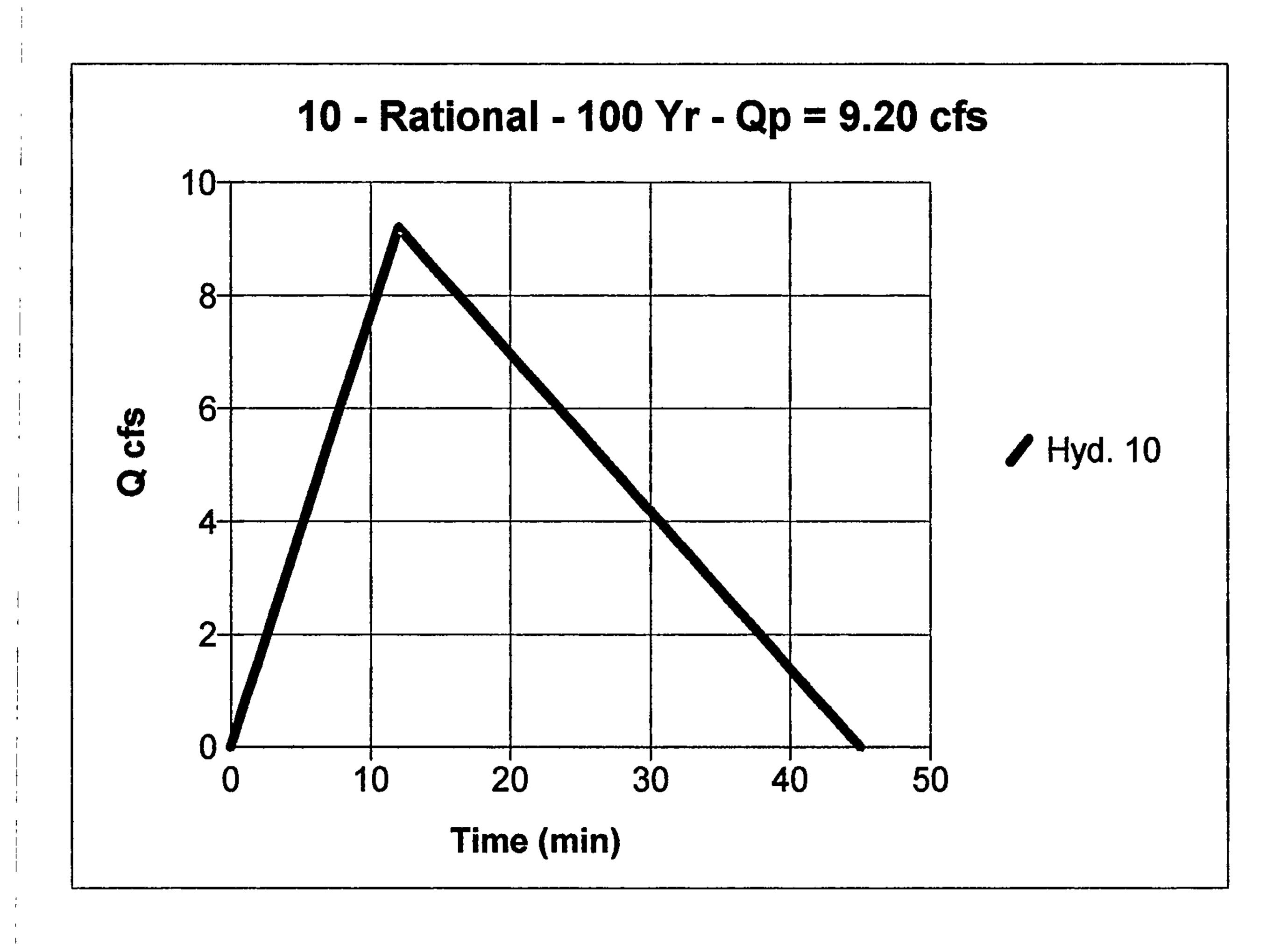
English

### Hyd. No. 10

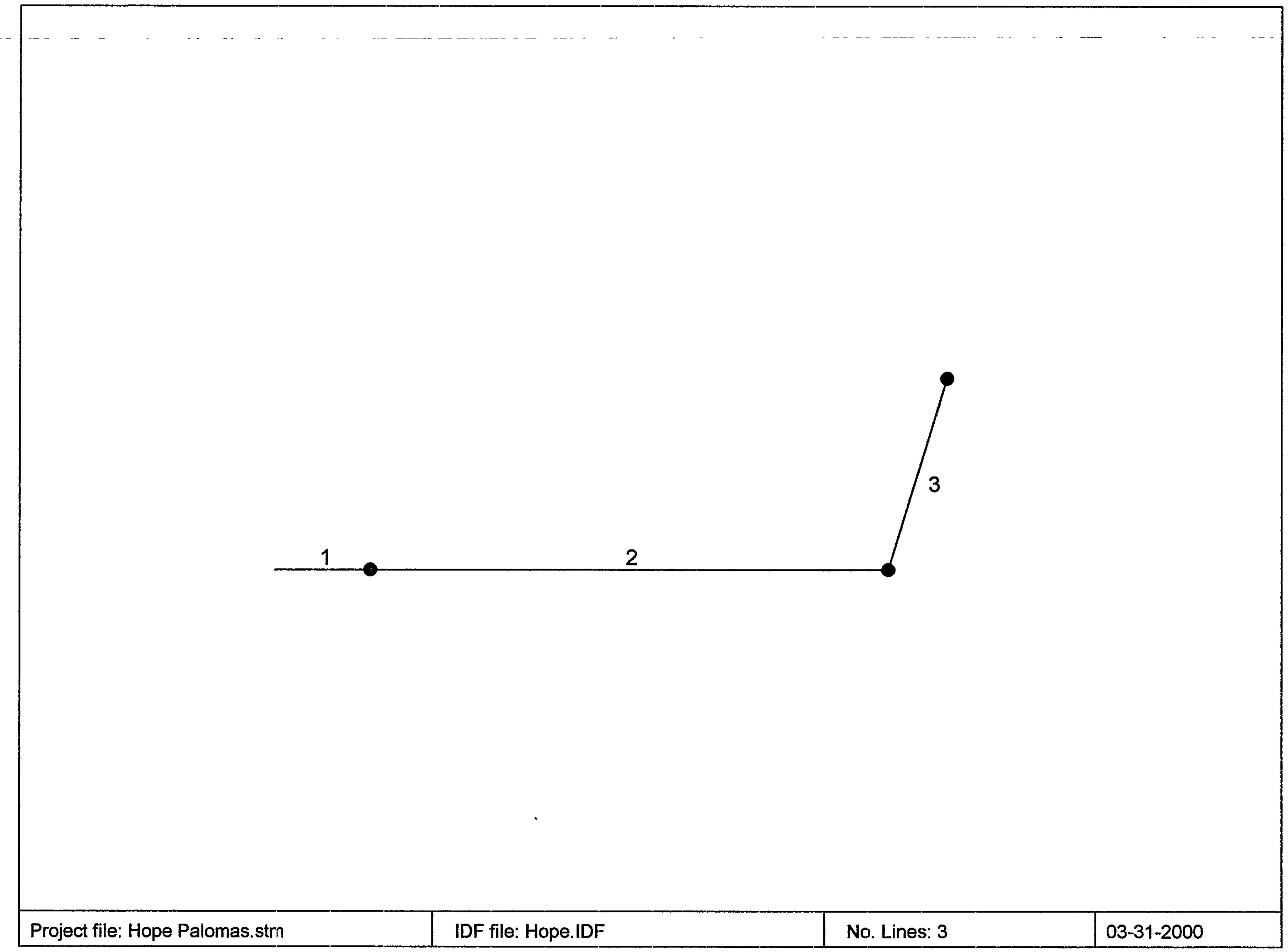
Athletic Field

Hydrograph type = Rational Storm frequency = 100 yrs Drainage area = 3.2 ac Intensity = 6.12 in I-D-F Curve = Hope.IDF Peak discharge = 9.20 cfs
Time interval = 1 min
Runoff coeff. = 0.47
Time of conc. (Tc) = 12 min
Reced. limb factor = 2.7648

Total Volume = 12,473 cuft



# Hydraflow Plan View



# Hydraflow Summary Report

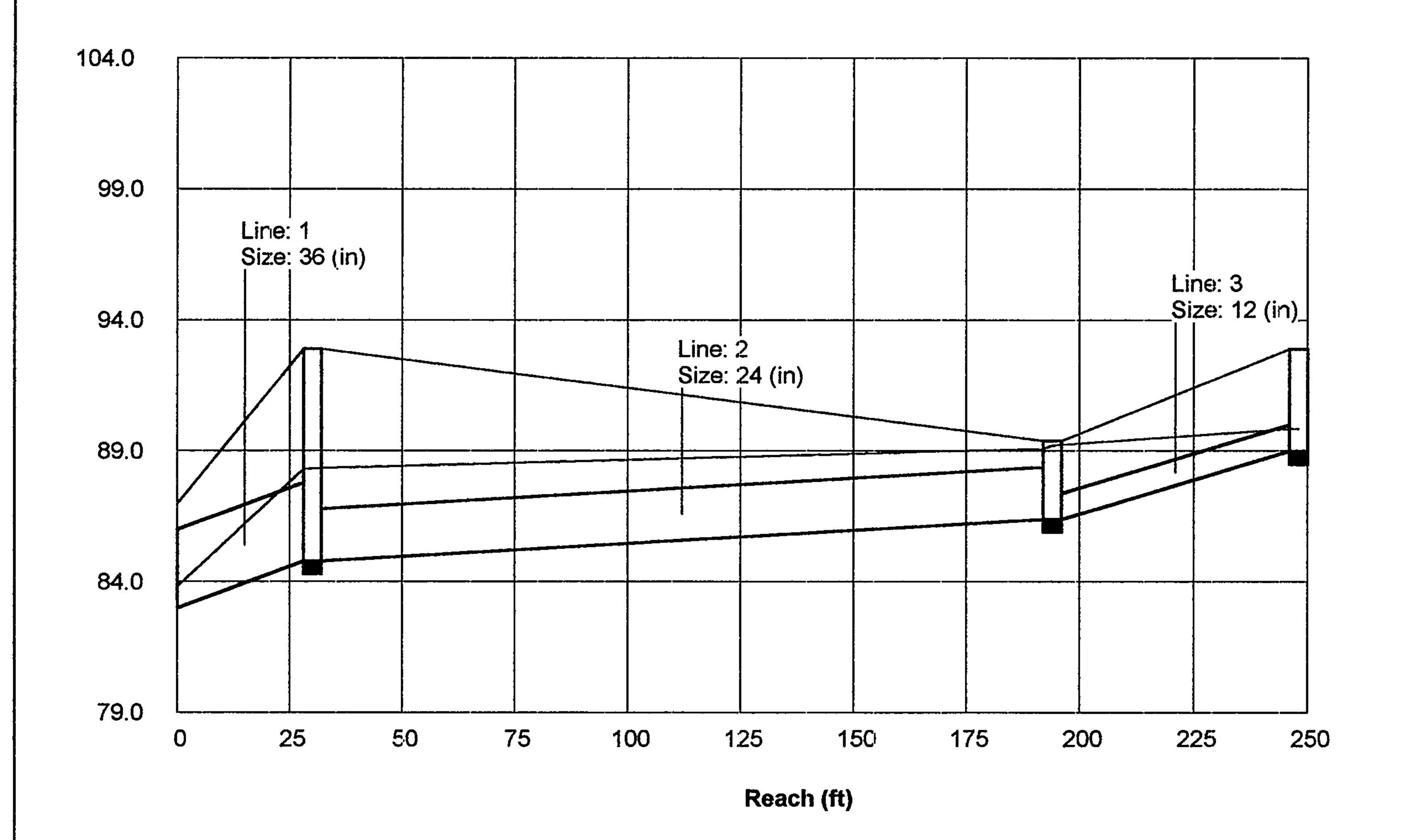
| Line<br>Vo. | Line ID             | Flow<br>rate<br>(cfs) | Line<br>size<br>(in) | Line<br>length<br>(ft) | Invert<br>EL Dn<br>(ft) | Invert<br>EL Up<br>(ft) | Line<br>slope<br>(%) | HGL<br>down<br>(ft) | HGL<br>up<br>(ft) | Minor<br>loss<br>(ft) | Dns<br>line<br>No. |
|-------------|---------------------|-----------------------|----------------------|------------------------|-------------------------|-------------------------|----------------------|---------------------|-------------------|-----------------------|--------------------|
| 1           | South Swale         | 24.80                 | 36 c                 | 30.0                   | 83.00                   | 84.80                   | 6.000                | 83.82*              | 88.33*            | 0.01                  | End                |
| 2           | Central Swale       | 20.00                 | 24 c                 | 164.0                  | 84.80                   | 86.40                   | 0.976                | 88.34*              | 89.10*            | 0.11                  | 1                  |
| <b>3</b>    | West Parking        | 4:00<br>WA<br>OK      | 12 c                 | 54.0                   | 86.40                   | 89.00                   | 4.815                | 89.21               | 89.85             | 0.02                  | 2                  |
|             |                     |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                     |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                     |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                     |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                     |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                     |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                     |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
| 1           |                     |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
| Proie       | ct File: Hope Palom | as.stm                | I-D-F File           | : Hope.ID              | F                       | Total No                | ). Lines: 3          | <u> </u>            | Run Date          | 03-31-2               | 000                |

# Hydraflow Storm Sewer Tabulation

| Sta  | tion     | Len     | Drng    | Area    | Rnoff | Are  | a x C | To    | C        |         | Total | Cap           | Vel           | Pi         | pe           | Inver    | t Elev     | HGL     | . Elev            | Grnd / I | Rim Elev   | Line ID      |
|------|----------|---------|---------|---------|-------|------|-------|-------|----------|---------|-------|---------------|---------------|------------|--------------|----------|------------|---------|-------------------|----------|------------|--------------|
| Line |          |         | Incr    | Total   | coeff | Incr | Total | Inlet | Syst     | (I)     | flow  | fuli _        | - <del></del> | Size       | Slope        | Up       | Dn         | Up      | Dn                | Up       | Dn         |              |
|      | Line     | (ft)    | (ac)    | (ac)    | (C)   |      |       | (min) | (min)    | (in/hr) | (cfs) | (cfs)         | (ft/s)        | (in)       | (%)          | (ft)     | (ft)       | (ft)    | (ft)              | (ft)     | (ft)       |              |
| 1    | End      | 30.0    | 0.00    | 0.00    | 0.00  | 0.00 | 0.00  | 0.0   | 1.2      | 0.0     | 24.80 | 163. <b>4</b> | 9.68          | 36         | 6.00         | 84.80    | 83.00      | 88.33   | 83.82             | 87.00    | 92.90      | South Swale  |
| 2    | 1        | 164.0   | 0.00    | 0.00    | 0.00  | 0.00 | 0.00  | 0.0   | 0.3      | 0.0     | 20.00 | 29.04         | 6.37          | 24         | 0.98         | 86.40    | 84.80      | 89.10   | 88.3 <del>4</del> | 92.90    | 89.40      | Central Swal |
| 3    | 2        | 54.0    | 0.00    | 0.00    | 0.00  | 0.00 | 0.00  | 0.0   | 0.0      | 0.0     | 4.00  | 10.16         | 5.36          | 12         | <b>4</b> .81 | 89.00    | 86.40      | 89.85   | 89.21             | 89.40    | 92.90      | West Parking |
|      |          |         |         |         |       |      |       |       |          |         |       |               |               |            |              |          |            |         |                   |          |            |              |
|      |          |         |         |         |       |      |       |       |          |         |       |               |               |            |              |          |            |         |                   |          |            |              |
|      |          |         |         |         |       |      |       |       |          |         |       |               |               |            |              |          |            |         |                   |          |            |              |
|      |          |         |         |         |       |      |       |       |          |         |       |               |               |            |              |          |            |         |                   |          |            |              |
|      |          |         |         |         |       |      |       |       |          |         |       |               |               |            |              |          |            |         |                   |          |            |              |
|      |          |         |         |         |       |      |       |       |          |         |       |               |               |            |              |          |            |         |                   |          |            |              |
| Pro  | ject Fil | le: Hop | e Palon | nas.stm |       |      |       | I-D-F | File: Ho | pe.IDF  |       | <u> </u>      |               | · <u> </u> |              | Total nu | ımber of i | ines: 3 | <del></del>       | Run Da   | ite: 03-31 | -2000        |

NOTES: Intensity = 0.00 / (Tc + 0.00) ^ 0.00; Return period = 100 Yrs.; Initial tailwater elevation = 83.82 (ft)





# Summary of Results

### General Notes:

- Sediment control geotextile fences should be used during the all phases of construction to control silting from all newly disturbed areas.
- SS inlets should be completely surrounded by silt fences at all times until site improvements are completed and the ground surface stabilized with pavement or other treatments. Wash-down from cement trucks should never be allowed to drain into the SS system.
- The designated square inlets use directional vane grates. The SS inlets should be positioned to provide proper orientation of the vanes to match the direction of flow to achieve maximum grate capacity.
- Pipe material designated as PVC reflects a generic product. Equivalent plastic products, such as PE pipe, can be used as long as the "n" value is 0.01.
- The SS pipe from the MH to the Domingo Baca channel connection must be reinforced concrete pipe, Class I RCP, per COA standards.

### Drainage System Requirements

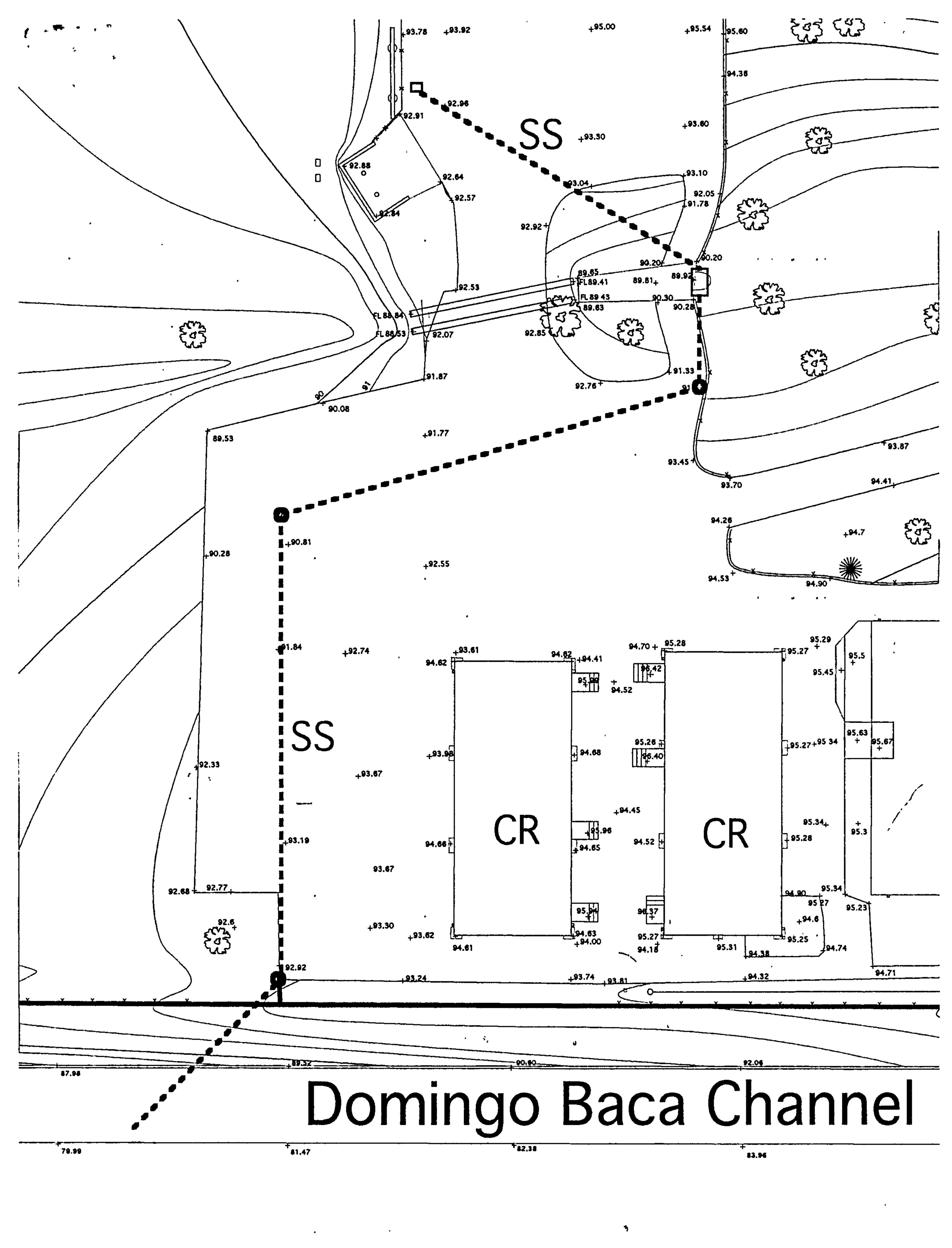
- An operating and maintenance schedule should be established for the SS pipe system and surface swales to Insure long term reliability.
- Inspections and maintenance accessed through the Inlets will insure that sediment and debris are not reducing the effective opening of the pipes.

### After Every Storm

- · Conduct Inspections of all Inlets, outlets and surface drainage swales.
- · Clear all inlet grates of any debris to insure maximum opening efficiency.
- · Remove, flush or jet out any sediment or trash buildup in pipes or swales.
- · Do not use surface swales for storage areas or obstruct the drainage path in any way.

Failure to maintain these drainage systems could result in uncontrolled flooding and damage to school facilities during a major storm event!





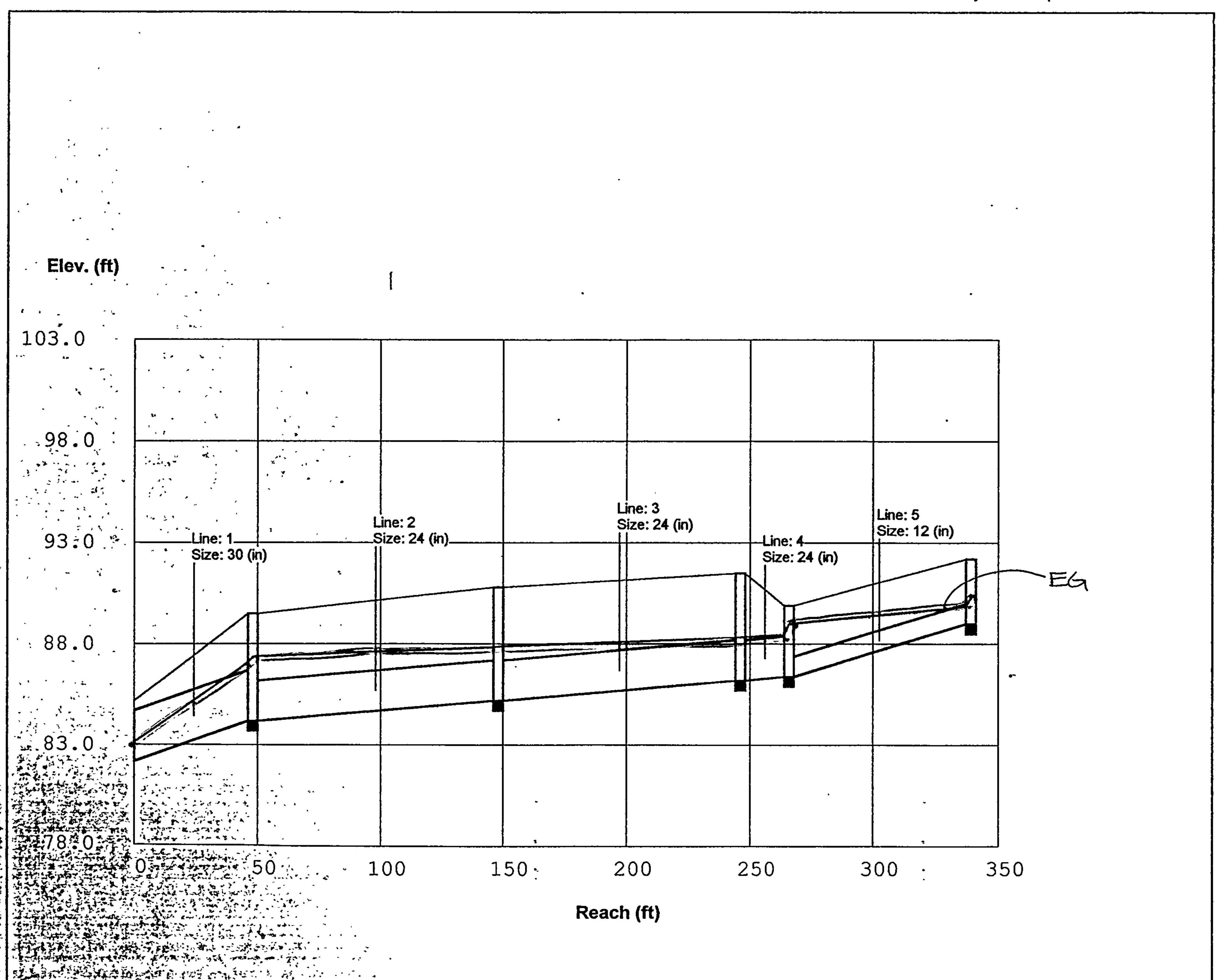
# Hydraflow Plan View

Project file: Hope Palomas Rev.stm IDF file: Hope.IDF No. Lines: 5 05-24-2000

| Line<br>No. | Line ID               | Flow<br>rate<br>(cfs) | Line<br>size<br>(in) | Line<br>length<br>(ft) | Invert<br>EL Dn<br>(ft) | Invert<br>EL Up<br>(ft) | Line<br>slope<br>(%) | HGL<br>down<br>(ft) | HGL<br>up<br>(ft) | Minor<br>loss<br>(ft) | Dns<br>line<br>No. |
|-------------|-----------------------|-----------------------|----------------------|------------------------|-------------------------|-------------------------|----------------------|---------------------|-------------------|-----------------------|--------------------|
| 1           | South Swale           | 24.80                 | 30 с                 | 48.0                   | 82.20                   | 84.20 .                 | 4.167                | 83.15*              | 87.09*            | 0.30                  | End                |
| 2           | Line 2                | 20.00                 | 24 c                 | 100.0                  | 84.20                   | 85.20                   | 1.000                | 87.39*              | 87.85*            | 0.03                  | 1                  |
| 3           | Line 3                | 20.00                 | · 24 c               | 98.0                   | 85.20                   | 86.20                   | 1.020                | 87.88*              | 88.33*            | 0.03                  | 2                  |
| 4           | Center Swale          | 20.00                 | 24 c                 | 20.0                   | 86.20                   | 86.40                   | 1.000                | 88.37*              | 88.46*            | 0.54                  | 3                  |
| 5           | West Parking          | 4.00                  | 12 c                 | 73.0                   | 86.40                   | 89.00                   | 3.562                | 88.99               | 89.85             | 0.49                  | 4                  |
|             |                       |                       |                      |                        |                         |                         |                      |                     | •                 |                       |                    |
|             |                       |                       | •                    |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                       |                       |                      |                        |                         |                         |                      |                     |                   |                       | •                  |
|             |                       |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                       |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
|             |                       |                       |                      |                        |                         |                         |                      |                     |                   | ••                    | •                  |
|             |                       |                       |                      |                        |                         |                         |                      |                     |                   |                       |                    |
| Proje       | ect File: Hope Paloma | s Rev.stm             | I-D-F Fil            | e: Hope.ID             | F                       | Total No                | . Lines: 5           |                     | Run Date:         | 05-24-2               | 000                |
| NOT         | ES: c = circular; e = | elliptical; b =       | = box; Retu          | rn period =            | 100 Yrs.; 1             | Indicates su            | rcharge co           | ndition.            |                   |                       |                    |

# Hydraflow Storm Sewer Tabulation

|  | •          |            | ·       | <del>,</del> | <del></del> | <del></del>    | <del> </del> | • !     |        |          |             | 1                                     | <del>}</del> |        | <del></del> -        |       | г     | <u>.</u> | <u> </u> |        | •        | <del></del> | <del></del>  |
|--|------------|------------|---------|--------------|-------------|----------------|--------------|---------|--------|----------|-------------|---------------------------------------|--------------|--------|----------------------|-------|-------|----------|----------|--------|----------|-------------|--------------|
| englisher to a significant                         | Sta        | ation      | Len     | Drng         | Area        | Rnoff<br>coeff |              | a x C   | T      | Ç        | Rain<br>(I) | Total                                 | Cap          | Vel    | P                    | ipe   | Inver | t Elev   | HGI      | _ Elev | Grnd / F | Rim Elev    | Line ID      |
| ا هم از از این | Line       | To<br>Line |         | Incr         | Total       | f              | Incr         | Total   | inlet  | Syst     | (*)         |                                       |              |        | Size                 | Slope | Up    | Dn       | Up       | Dn     | Up       | Dn          |              |
| ," (e ) ***  | # > ·      | Line       | (ft)    | (ac)         | (ac)        | (C)            |              | <u></u> | (min)  | (min)    | (in/hr)     | (cfs)                                 | (cfs)        | (ft/s) | (in)                 | (%)   | (ft)  | (ft)     | (ft)     | (ft)   | (ft)     | (ft)        |              |
|  | 1          | End        | 48.0    | 0.00         | 0.00        | 0.00           | 0.00         | 0.00    | 0.0    | 1.6      | 0.0         | 24.80                                 | 83.71        | 9.81   | 30                   | 4.17  | 84.20 | 82.20    | 87.09    | 83.15  | 85.20    | 89.50       | South Swale  |
| `  | 2          | 1          | 100.0   | 0.00         | 0.00        | 0.00           | 0.00         | 0.00    | 0.0    | 1.1      | 0.0         | 20.00                                 | 29.40        | 6.37   | 24                   | 1.00  | 85.20 | 84.20    | 87.85    | 87.39  | 89.50    | 90.80       | Line 2       |
|  | 3          | 2          | 98.0    | 0.00         | 0.00        | 0.00           | 0.00         | 0.00    | 0.0    | 0.5      | 0.0         | 20.00                                 | 29.70        | 6.37   | 24                   | 1.02  | 86.20 | 85.20    | 88.33    | 87.88  | 90.80    | 91.50       | Line 3       |
|  | 4          | 3          | 20.0    | 0.00         | 0.00        | 0.00           | 0.00         | 0.00    | 0,0    | 0.4      | 0.0         | 20.00                                 | 29.40        | 6.37   | 24                   | 1.00  | 86.40 | 86.20    | 88.46    | 88.37  | 91.50    | 89.90       | Center Swale |
|  | 5          | 4          |         | 0.00         | 0.00        | 0.00           | 0.00         | 0.00    | 0.0    | 0.0      | 0.0         | 4.00                                  | 8.74         | 5.36   | 12                   | 3.56  | 89.00 | 86.40    | 89.85    | 88.99  | 89.90    | 92.20       | West Parking |
| •  | · · ·      |            |         |              | _           |                |              |         | ,      |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
| · <b>-</b>   |            |            |         |              |             |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
|  |            | ٠.         | •       |              |             |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             | -            |
|  | •          | ,          |         |              |             |                |              |         |        |          |             |                                       | •            |        |                      |       |       |          |          |        |          |             |              |
|  |            |            | 2-4-2   | ·            |             |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
|  | •          |            | , , ,   |              | , .         |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
| -  |            | ٠.         |         | •            | •           | u              |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
| , ,  |            |            |         | • '•         | , ,<br>,    |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
| *,   |            |            |         |              |             |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          | ·           |              |
| •  |            |            |         |              |             |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
|  | •          |            |         |              | ·           |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
|  | ;          |            |         |              |             |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        | •-       |             |              |
| ,  | •          |            |         | ,            | -           |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
| . 2  | •          |            |         |              | ,           |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
| · .  |            |            |         |              |             |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          |        |          |             |              |
|  |            | * 4        |         |              |             |                |              |         |        |          |             |                                       |              |        |                      |       |       |          |          | -      |          |             |              |
|  |            | , ,        |         |              |             |                |              |         | ·<br>· |          |             |                                       |              |        |                      |       |       | •        |          | •      |          |             |              |
|  | <u>.</u> . |            | -       |              |             | ·              |              |         |        |          |             | · · · · · · · · · · · · · · · · · · · |              |        |                      |       |       |          | <u></u>  |        |          |             |              |
|  | Pro        | oject Fi   | le: Hop | e Palon      | nas Rev     | .stm           |              |         | I-D-F  | File: Ho | pe.IDF      |                                       |              |        | I-D-F File: Hope.IDF |       |       |          |          |        | Run Da   | te: 05-24   | -2000        |





P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

June 14, 2001

Chris Weiss, P.E.
C.L.Weiss Engineering
P.O. Box 987
Sandia Park, NM 87047

RE: HOPE CHRISTIAN SCHOOL ADDITION - PALOMAS CAMPUS, Soccor Field Revisions II (D18-D9). Revised DRAINAGE REPORT FOR BUILDING PERMIT APPROVAL. ENGINEER'S STAMP DATED MAY 24, 2001

### Dear Mr. Weiss:

Based on the information provided on your June 1, 2001 submittal, the above referenced project is approved for Building Permit.

This revision was necessitated by a bust in the stated existing elevations at the soccor field.

Please furnish another copy of the corresponding Grading and Drainage Plan.

Please attach a copy of this approved plan to the construction sets prior to sign-off by Hydrology.

Prior to Certificate of Occupancy approval, an Engineer's Certification per the DPM will be required.

If I can be of further assistance, please feel free to contact me at 924-3984.

Sincerely,

John P. Murray, P.E.

Hydrology

c: Terri Martin File



P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

May 1, 2001

Chris Weiss, P.E. C.L. Weiss Engineering P.O. Box 987 Sandia Park, NM 87047

HOPE CHRISTIAN SCHOOL CAMPUS ADDITION (D18-D9). Revised GRADING RE: AND DRAINAGE PLAN FOR BUILDING PERMIT APPROVAL. ENGINEER'S STAMP DATED APRIL 20, 2001 FOR PLAN AND APRIL 16, 2001 FOR REPORT.

Dear Mr. Weiss:

Based on the information provided on your April 25, 2001 submittal, the above referenced project is approved for Building Permit.

Please attach a copy of this approved plan to the construction sets prior to sign-off by Hydrology.

Prior to Certificate of Occupancy approval, an Engineer's Certification per the DPM will be required.

If I can be of further assistance, please feel free to contact me at 924-3984.

Sincerely,

John P. Murray, P.E.

Hydrology

**Terri Martin** 



June 29, 2000

Chris Weiss, P.E. C. L. Weiss Engineering P. O. Box 97 Sandia Park, NM 87047

RE: GRADING & DRAINAGE PLAN FOR HOPE CHRISTIAN SCHOOL ADDITION (D-18/D09) ENGINEERS STAMP DATED MAY 26, 2000 SUBMITTED FOR BUILDING PERMIT APPROVAL

Dear Mr. Weiss,

Based upon the information provided in your June 14, 2000, submittal, the project referred to above is approved for Building Permit. Please attach a copy of this approved plan to the construction sets prior to sign-off by Hydrology.

Prior to release of the Certificate of Occupancy, an Engineer Certification, per the DPM checklist, will be required.

If you have any questions, please call me at 924-3988.

Sincerely,

Stuart Reeder, P.E.

Strat Keeder, P.E.

Hydrology Division

xc: Whitney Reierson

File



July 24,1998

Chris Weiss
C.L. Weiss Engineering
P.O. Box 97
Sandia Park, New Mexico 87047

RE: DRAINAGE PLAN FOR HOPE CHRISTIAN SCHOOL ADDITION (D18-D94) ENGINEER'S STAMP DATED 6/26/98

Dear Mr. Weiss:

Based on the information provided on your June 26,1998 submittal, the above referenced site is—approved for Building Permit.

Please attach a copy of this approved plan to the construction sets prior to sign-off by Hydrology.

Also, prior to Certificate of Occupancy release, Engineer Certification per the DPM checklist will be required.

If I can be of further assistance, please feel free to contact me at 924-3986.

C: Andrew Garcia

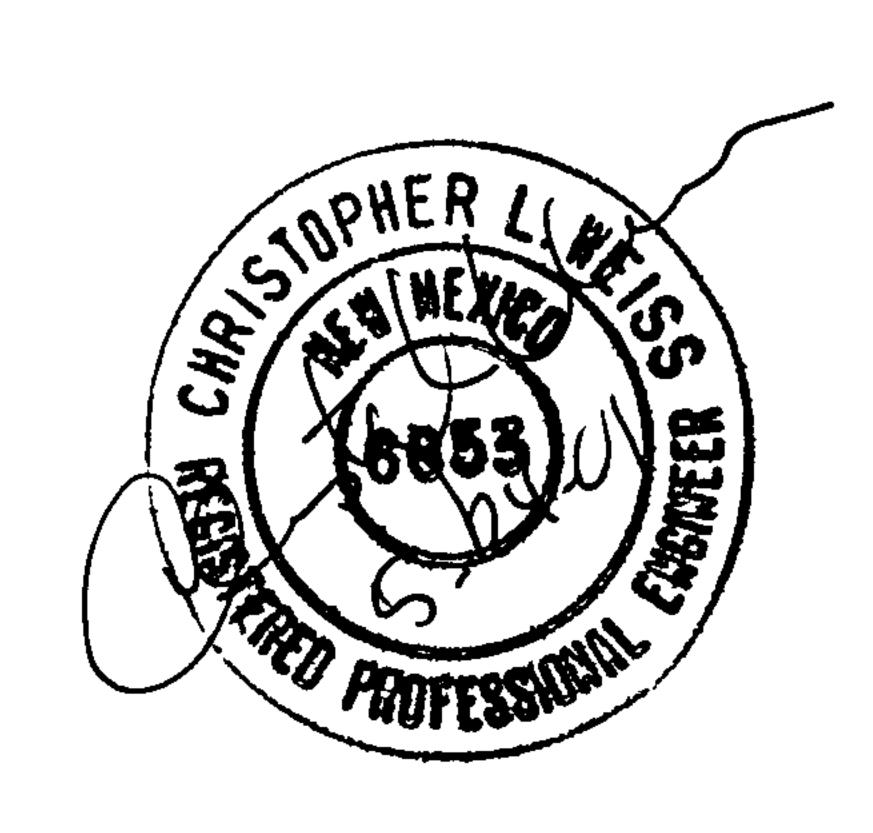
Sincerely

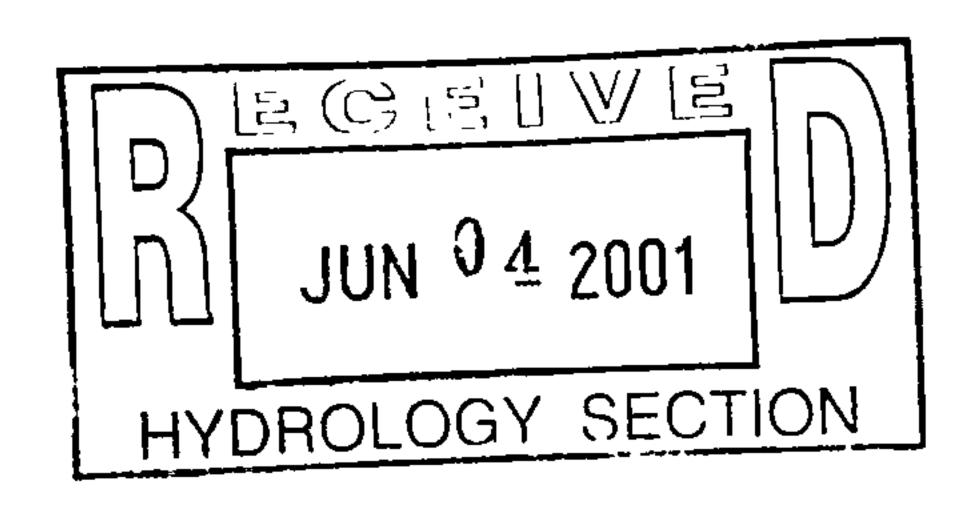
Bernie J. Montoya CE

Associate Engineer

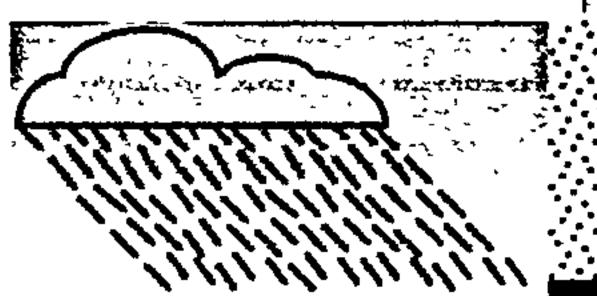








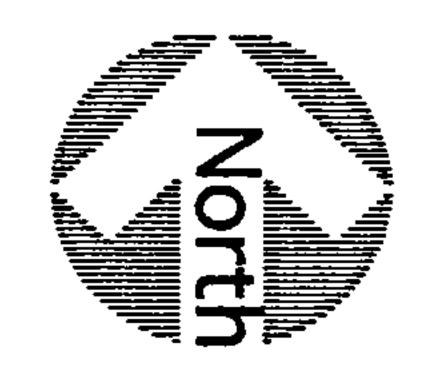
C.L. Weiss Engineering, inc P.O. Box 97 Sandia Park, NM 87047 Tele/Fax - (505) 281-1800 E-Mail - clwnm@earthlink.net

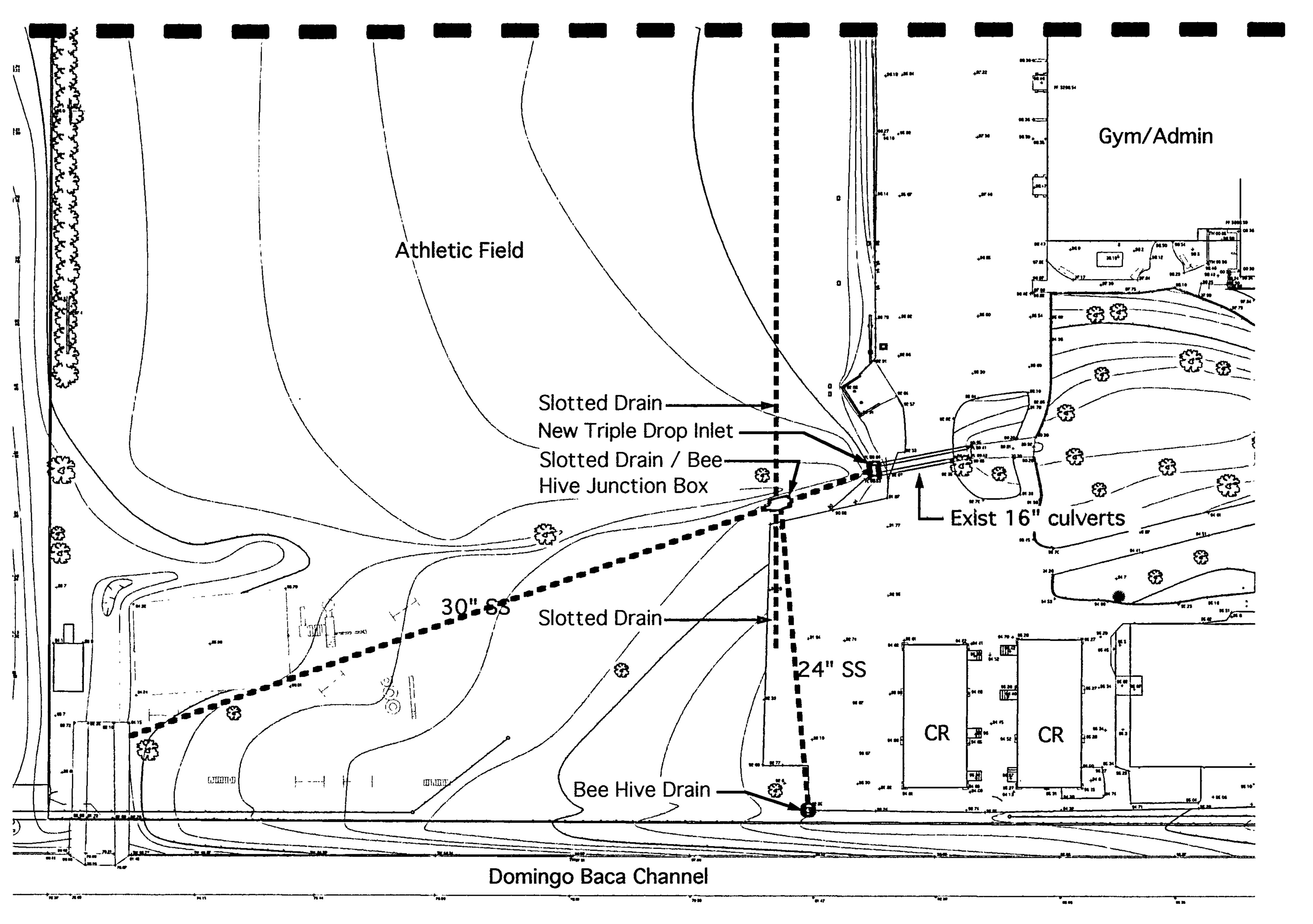


Palomas Ave \_\_\_\_\_\_ Gym/Admin Paved Parking Athletic Field Multipurpose\*\* Classrooms **Gravel Parking** (Future Paved) Domingo Baca Channel

# Drainage Sub-basins

Revised 4 -01





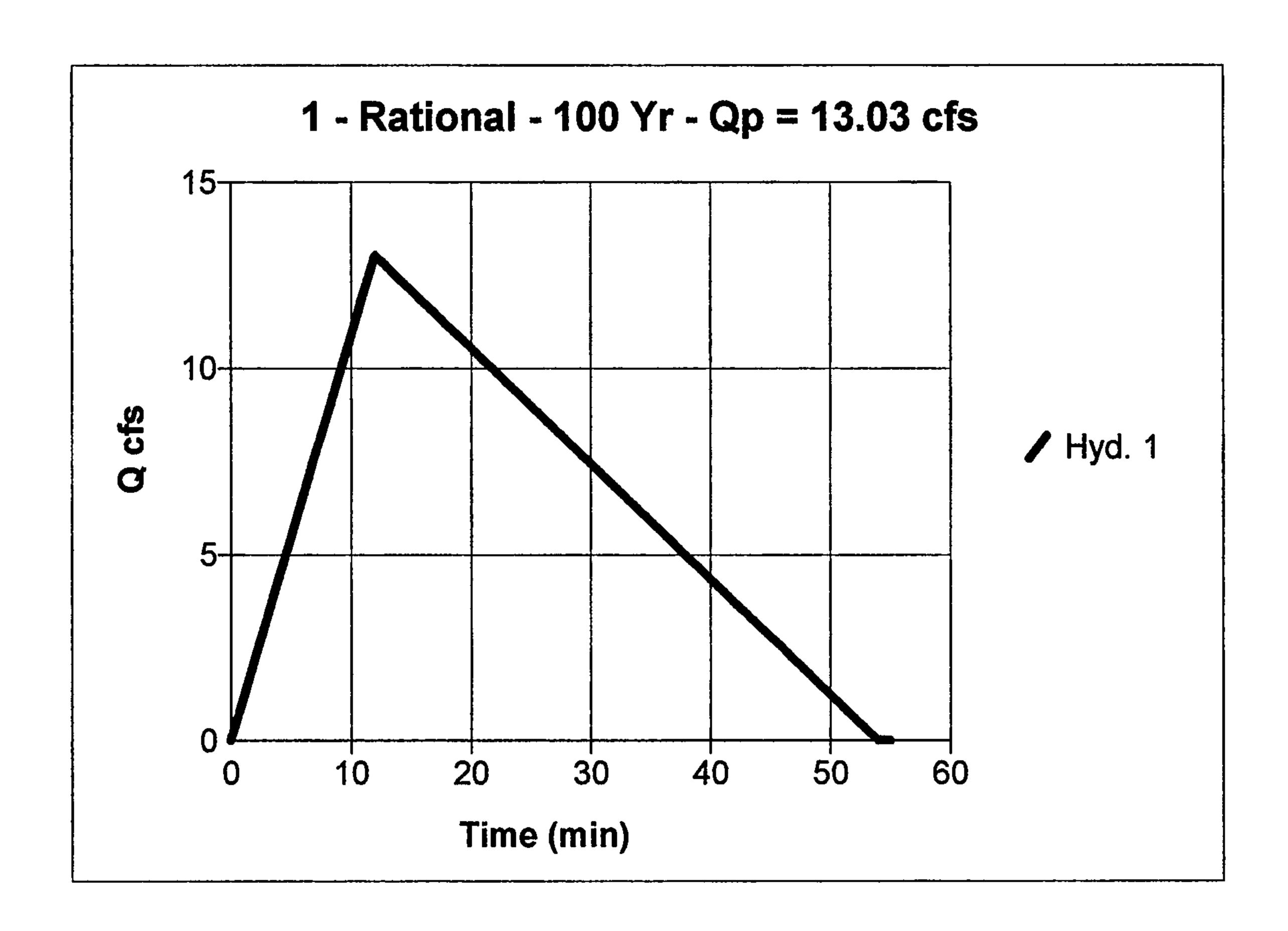
Hope Soccer/SS Plan Rev. II

### Hyd. No. 1

Sub-Basin 1

Hydrograph type = Rational Storm frequency = 100 yrs Drainage area = 3.0 ac Intensity = 6.12 in I-D-F Curve = Hope.IDF Peak discharge = 13.03 cfs
Time interval = 1 min
Runoff coeff. = 0.71
Time of conc. (Tc) = 12 min
Reced. limb factor = 3.558

Total Volume = 21,387 cuft



= 9.52 cfs

= 1 min

Hyd. No. 2

**Detention Pond** 

Hydrograph type = Reservoir Peak discharge Storm frequency = 100 yrs Time interval

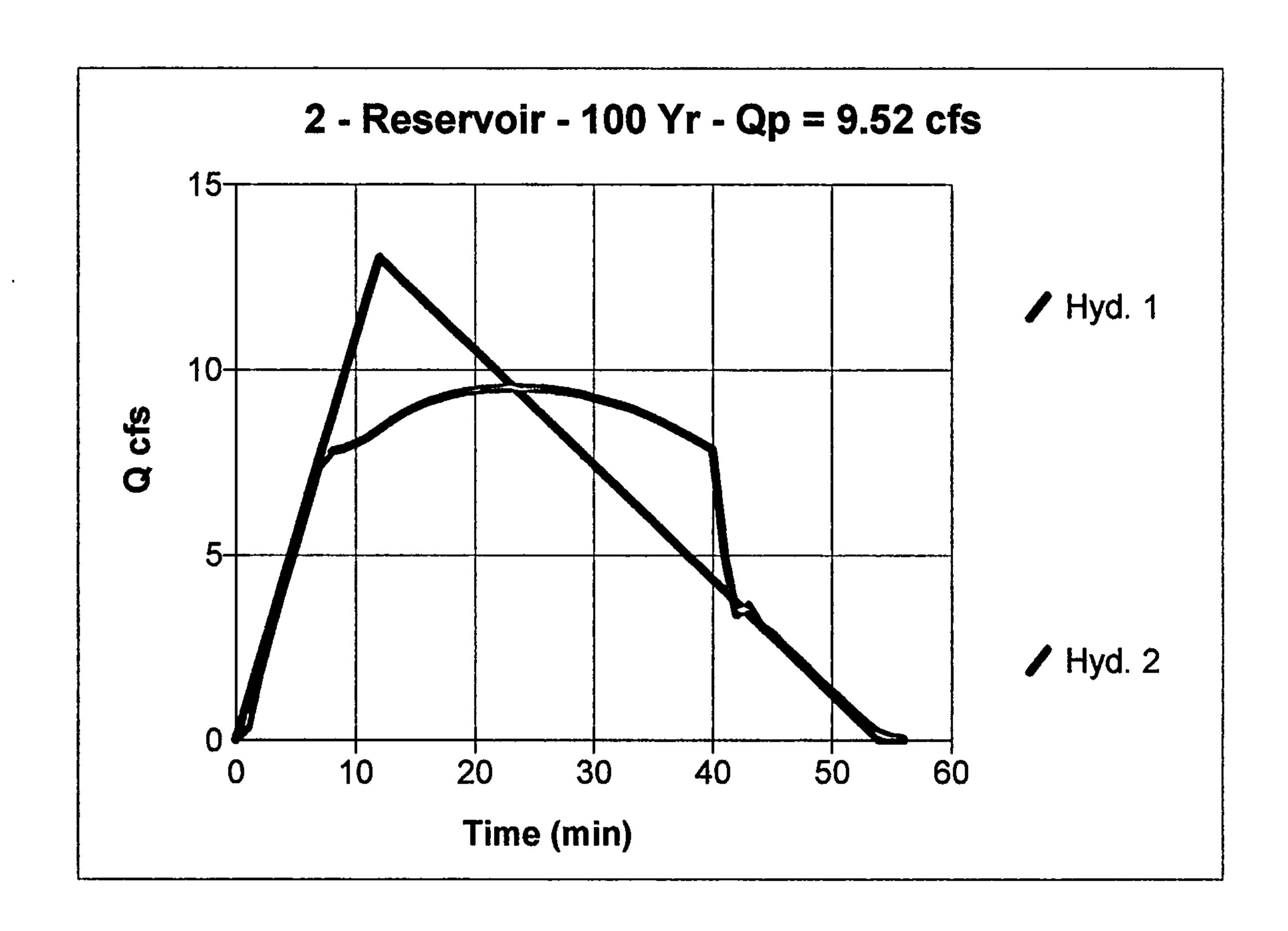
Inflow hyd. No. = 1

Reservoir name = Campus Open Spa

Max. Elevation = 90.16 ft Max. Storage = 2,259 cuft

Storage Indication method used

Total Volume = 21,114 cuft



### Reservoir No. 1 - Campus Open Space

### **Pond Data**

Pond storage is based on known contour areas

### Stage / Storage Table

| Stage<br>ft | Elevation<br>ft | Contour area<br>sqft | Incr. Storage<br>cuft | Total storage<br>cuft |
|-------------|-----------------|----------------------|-----------------------|-----------------------|
| 0.00        | 89.00           | 10                   | 0                     | 0                     |
| 1.00        | 90.00           | 246                  | 128                   | 128                   |
| 2.00        | 91.00           | 26,304               | 13,275                | 13,403                |
| 3.00        | 92.00           | 58,028               | 42,166                | 55,569                |
| 4.00        | 93.00           | 96,354               | 77,191                | 132,760               |

### Culvert / Orifice Structures

### Weir Structures

|               | [A]     | [B]  | [C]  | [D]  | [A] [B] [C]                         | [D]  |
|---------------|---------|------|------|------|-------------------------------------|------|
| Rise in       | = 16.0  | 0.0  | 0.0  | 0.0  | Crest Len ft = 0.0 0.0 0.0          | 0.0  |
| Span in       | = 16.0  | 0.0  | 0.0  | 0.0  | Crest El. ft = 0.00 0.00 0.00       | 0.00 |
| No. Barreis   | = 2     | 0    | 0    | 0    | Weir Coeff. = 0.00 0.00 0.00        | 0.00 |
| Invert El. ft | = 89.00 | 0.00 | 0.00 | 0.00 | <b>Eqn. Exp.</b> $= 0.00 0.00 0.00$ | 0.00 |
| Length ft     | = 37.0  | 0.0  | 0.0  | 0.0  | Multi-Stage = No No No              | No   |
| Slope %       | = 1.62  | 0.00 | 0.00 | 0.00 |                                     |      |
| N-Value       | = .013  | .000 | .000 | .000 |                                     |      |
| Orif. Coeff.  | = 0.60  | 0.00 | 0.00 | 0.00 |                                     |      |
| Multi-Stage   | =       | No   | No   | No   | Tailwater Elevation = 1.00 ft       |      |

### Stage / Storage / Discharge Table

Note All outflows have been analyzed under inlet and outlet control.

| Stage<br>ft | Storage<br>cuft | Elevation<br>ft | Clv A<br>cfs | Clv B<br>cfs | Clv C<br>cfs | Civ D<br>cfs | Wr A<br>cfs | Wr B<br>cfs | Wr C<br>cfs | Wr D<br>cfs | Discharge<br>cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|------------------|
| 0.00        | 0               | 89.00           | 0.00         |              |              |              |             | -           |             |             | 0.00             |
| 1.00        | 128             | 90.00           | 7.77         |              |              |              |             |             |             |             | 7.77             |
| 2.00        | 13,403          | 91.00           | 15.52        |              |              |              |             |             |             |             | 15.52            |
| 3.00        | 55,569          | 92.00           | 20.54        |              |              | <del></del>  |             |             |             |             | 20.54            |
| 4.00        | 132,760         | 93.00           | 24.55        |              |              | ***          |             |             |             |             | 24.55            |

### Hydrograph Plot

English

### Hyd. No. 2

Det Pond w/ One pipe

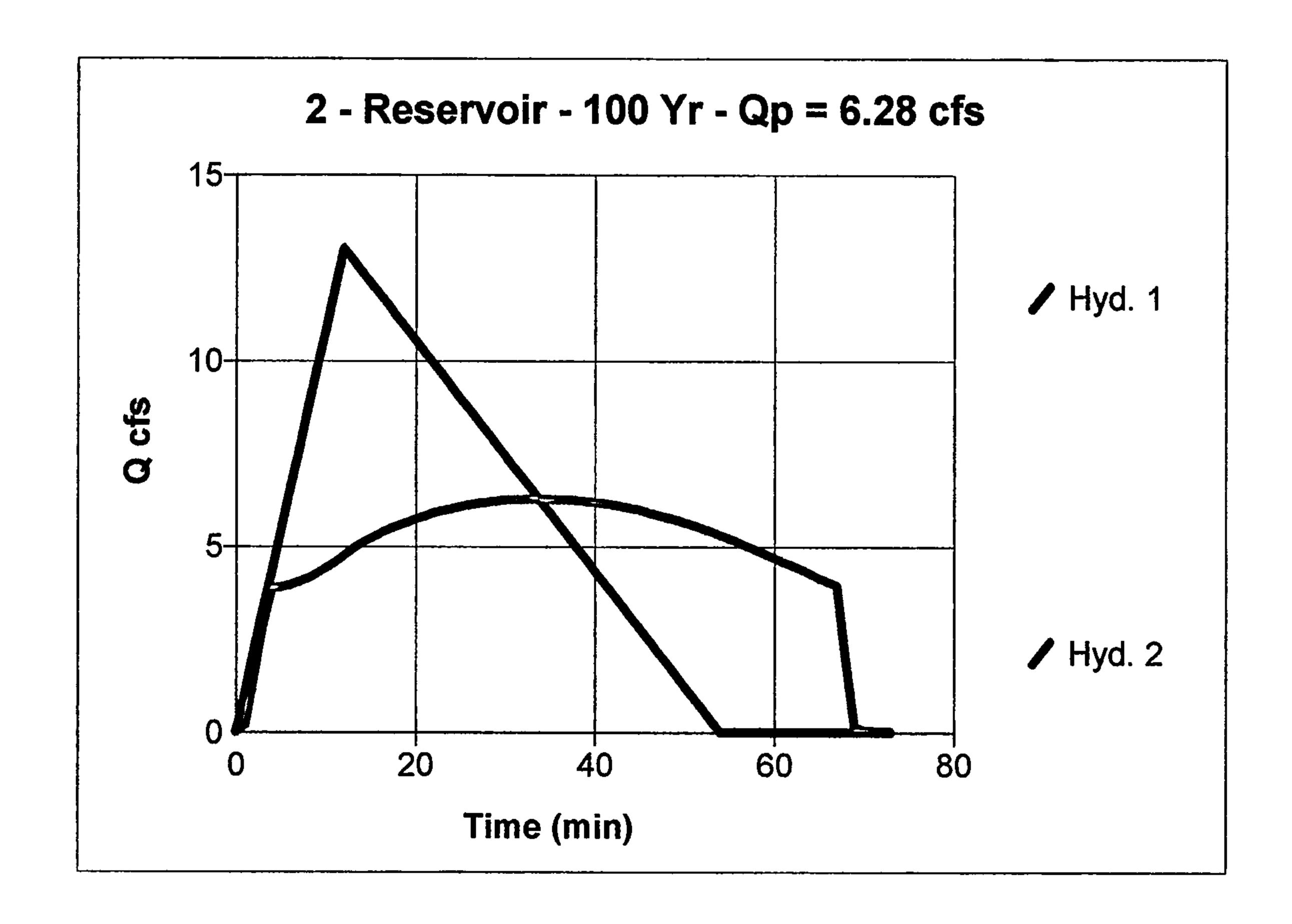
Hydrograph type = Reservoir Peak discharge = 6.28 cfs
Storm frequency = 100 yrs Time interval = 1 min

Inflow hyd. No. = 1 Reservoir name = Campus Open Spa

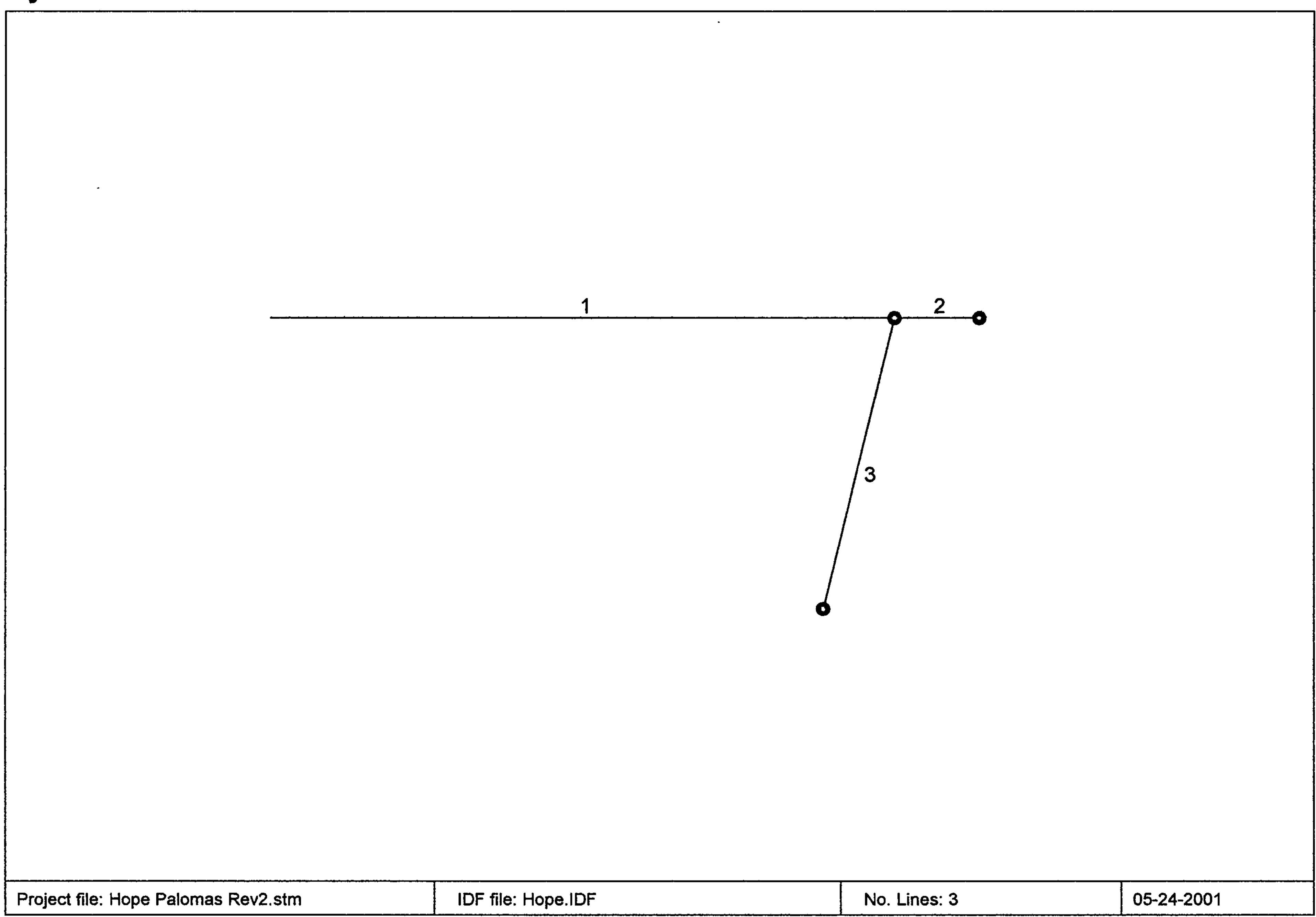
Max. Elevation = 90.54 ft Max. Storage = 7,291 cuft

Storage indication method used

Total Volume = 21,114 cuft



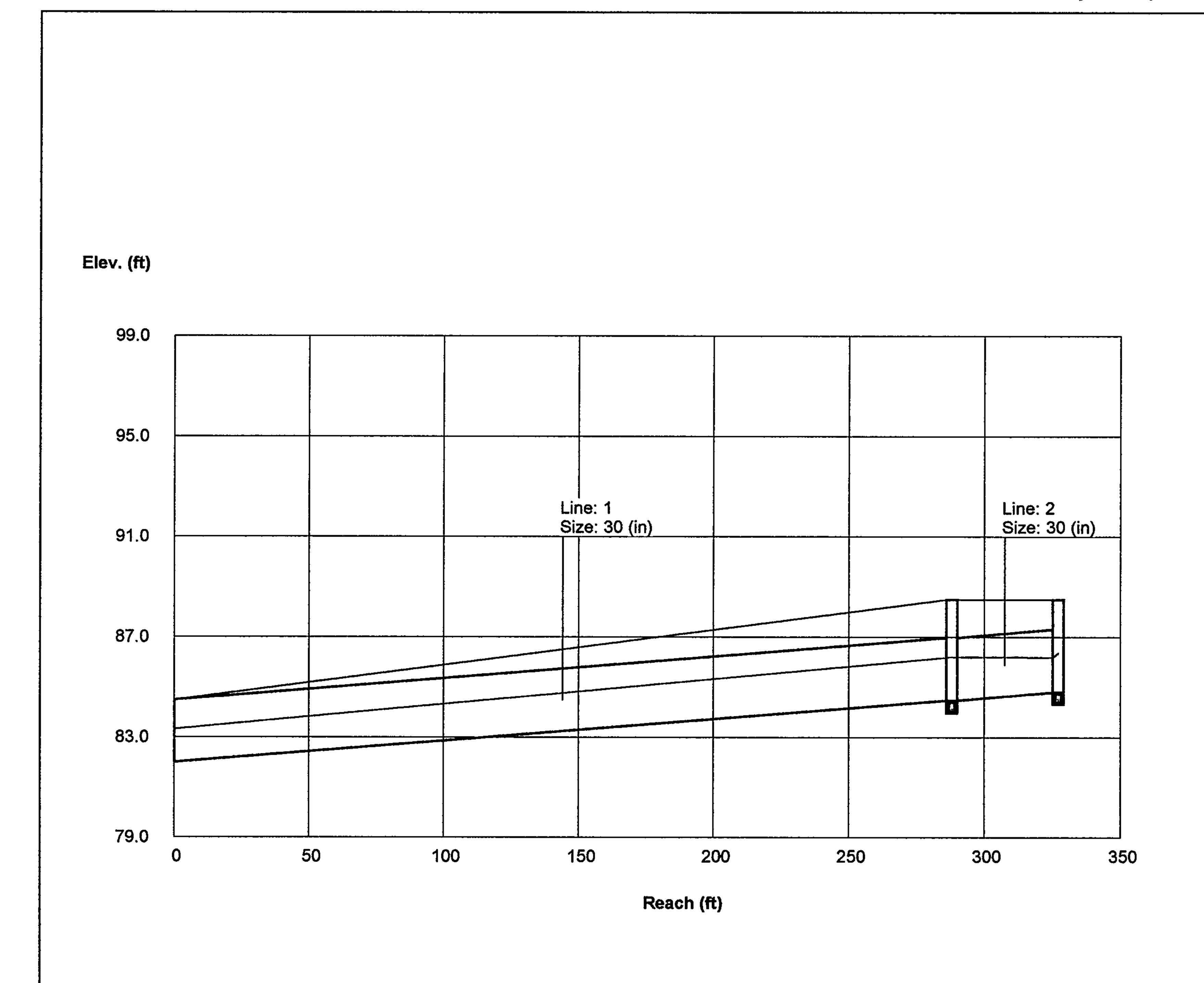
## Hydraflow Plan View

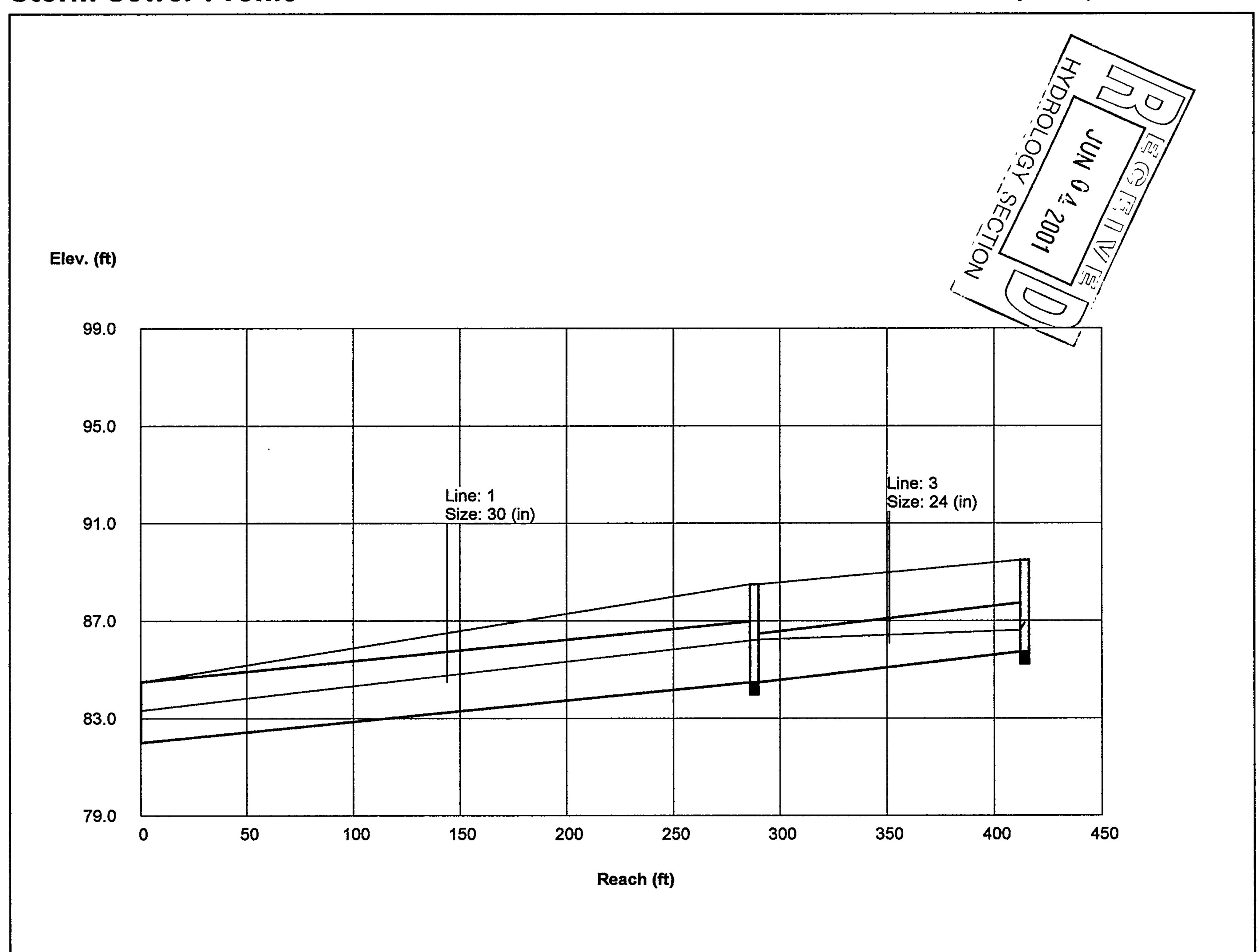


# Hydraflow Storm Sewer Tabulation

| Sta                                 | tion | Len   | Drng. | Drng Area |       | Area x C |       | Тс                   |       |            | Total    | Cap   | Vel    | Pipe       |          | invert Elev              |       | HGL Elev |       | Grnd / RIm Elev      |       | Line ID      |
|-------------------------------------|------|-------|-------|-----------|-------|----------|-------|----------------------|-------|------------|----------|-------|--------|------------|----------|--------------------------|-------|----------|-------|----------------------|-------|--------------|
| Line                                | To   |       | Incr  | Total     | coeff | Incr     | Total | Inlet                | Syst  | <b>(1)</b> | flow     | full  |        | Size       | Slope    | Up                       | Dn    | Up       | Dn    | Up                   | Dn    |              |
|                                     | Line | (ft)  | (ac)  | (ac)      | (C)   |          |       | (min)                | (min) | (ln/hr)    | (cfs)    | (cfs) | (ft/s) | (in)       | (%)      | (ft)                     | (ft)  | (ft)     | (ft)  | (ft)                 | (it)  |              |
| 4                                   | End  | 288.0 | 0.00  | 0.00      | 0.00  | 0.00     | 0.00  | ס.ס                  | 0.7   | 0.0        | 26.40    | 49.47 | 8.70   | 30         | 0.86     | 84.48                    | 82.00 | 86 20    | 83.32 | 84.50                | 88.50 | Outlet Line  |
| '<br>2                              | 1    | 39.0  | 0.00  | 0.00      |       |          | 0.00  |                      | 0.0   | 0.0        | 9.50     | 38.29 | 3.03   | 30         |          | 84.82                    | 84.48 | 86.19    | 86.22 | 88.50                | 88.50 | Triple Inlet |
| 3                                   | 1    | 126.0 |       | 0.00      |       |          | 0.00  |                      | 0.0   | ĺ          |          | 22.62 | 3.36   | 24         |          | ·                        | 84.48 | 86.61    | 86.22 | 88.50                | 89.50 | Bee Hive SS  |
| •                                   | ,    | 120.0 | 0.00  | 0.00      | 0.00  | 0.00     |       | 0.0                  |       | 0.0        | 0.10     | 22.02 |        |            | 1.00     | ]                        | 04.40 | 00.01    | JO.LL | 00.00                | 00.00 |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       | •                    |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        | <b>.</b> : |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            | <b>,</b> |       |        |            |          |                          | •     |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       | :        |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       | · .      |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
|                                     |      |       |       |           |       |          |       |                      |       |            |          |       |        |            |          |                          |       |          |       |                      |       |              |
| Project File: Hope Palomas Rev2.stm |      |       |       |           |       |          |       | I-D-F File: Hope.IDF |       |            |          |       |        |            | Total nu | Total number of lines: 3 |       |          |       | Run Date: 05-24-2001 |       |              |

NOTES: Intensity = 0.00 / (Tc + 0.00) ^ 0.00; Return period = 100 Yrs.; Initial tailwater elevation ≠ 83.32 (ft)





# <u>M</u>

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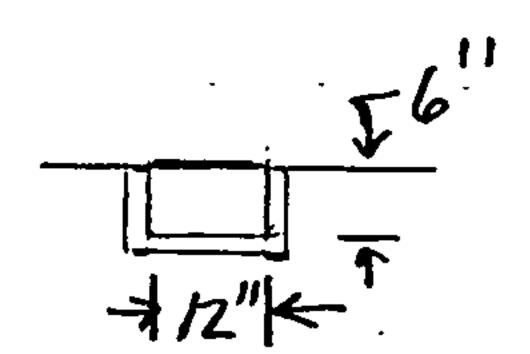
| PROJECT HOPE  | Elementing<br>541 Calvert |
|---------------|---------------------------|
| SUBJECT Basin | 54/ Calvert               |
| BY            | DATE                      |
| CHECKED       | DATE                      |
|               | SHEETOF                   |

Basin A Discharge = 0.82cfs

12" Sidewalk Culvert

0=3.3 (w)(h)<sup>3/2</sup>

$$Q = 3.3(1.0)(0.5)^{3/2}$$



5= 1,22%

WP=Z

A = 0.5

n = 0.013

