

CITY OF ALBUQUERQUE



November 25, 2014

Ms. Asa Weber, PE
Isaacson & Arfman, PA
1287 Monroe Street NE
Albuquerque, NM 87108

**Re: Coronado Villa Retirement Community, Tract 4B
Grading and Drainage Plan Engineer's date 11-21-14
Supplemental Information to Grading and Drainage Plan
Engineer's date 11-11-14 (D18D054C)**

Dear Ms. Weber,

Based upon the information provided in your submittal received 11-24-14, the above referenced plan is approved for Building Permit. Please attach a copy of this approved plan to the construction sets prior to sign-off by Hydrology.

Prior to Certificate of Occupancy release, Engineer Certification per the DPM checklist will be required.

PO Box 1293

If you have any questions, you can contact me at 924-3994.

Albuquerque

Sincerely,

New Mexico 87103

Amy L. D. Niese, P.E.
Senior Engineer, Hydrology
Planning Department

www.cabq.gov

C: e-mail
file

NOVEMBER 11, 2014

SUPPLEMENTAL INFORMATION

for

TRACT 4-B, SANTA MONICA PLACE CORONADO VILLA RETIREMENT COMMUNITY GRADING AND DRAINAGE PLAN



Åsa Nilsson-Weber

11-11-14

Åsa Nilsson-Weber, NMPE 17631

Date



ISAACSON & ARFMAN, P.A.

Consulting Engineering Associates

Thomas O. Isaacson, PE(RET.) & LS(RET.)

Fred C. Arfman, PE

Åsa Nilsson-Weber, PE

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PROJECT INFORMATION:

PROPERTY: The site is a previously developed mobile home property located within C.O.A. Vicinity Map D-18. The site is bound to the south by Santa Monica Ave. NE, to the west by undeveloped property (proposed Tract 4-A), to the east by Louisiana Blvd. and to the north by undeveloped property (proposed Tract 3-B).

PROPOSED IMPROVEMENTS: the proposed improvements include a 65,000± SF retirement community, three garage parking buildings, associated asphalt paved access, parking and landscaping.

EXISTING LEGAL: The eastern portion of Tract 4, Santa Monica Place, Albuquerque, NM

PROPOSED LEGAL: Tract 4-B, Santa Monica Place, Albuquerque, NM

BENCHMARK: Vertical datum is based upon the Albuquerque Control Survey Benchmark "18-E18", ELEVATION = 5269.166 (NGVD88)

OFF-SITE: No off-site drainage impacts this property.

FLOOD HAZARD: The subject property lies within Zone "X" (areas determined to be outside 0.2% annual chance flood plain) in accordance with the National Flood Insurance Program Rate Map No. 35001c0137F, effective date 11-19-03.

SURVEYOR: Russ P. Hugg, Surv-Tek, Inc., (505)897-3366, Albuquerque, New Mexico.

DRAINAGE CONCEPT:

The Drainage Master Plan (DMP) by Isaacson & Arfman, P.A., dated October 9, 2014, outlined drainage requirements for each tract within Santa Monica Place (Tracts 3A, 3B, 4A & 4B). This property is tract 4B with land treatments estimated at 15%B, 35%C AND 50% D.

Per the DMP, Tract 4B shall be allowed to discharge 30.9 cfs into the storm drain system connecting to the Derickson Ave. storm drain. The onsite storm drain shall connect to 18" RCP storm drain stubs that shall be installed with the public work order for the construction of Brentwood Blvd. and San Vicente Ave.

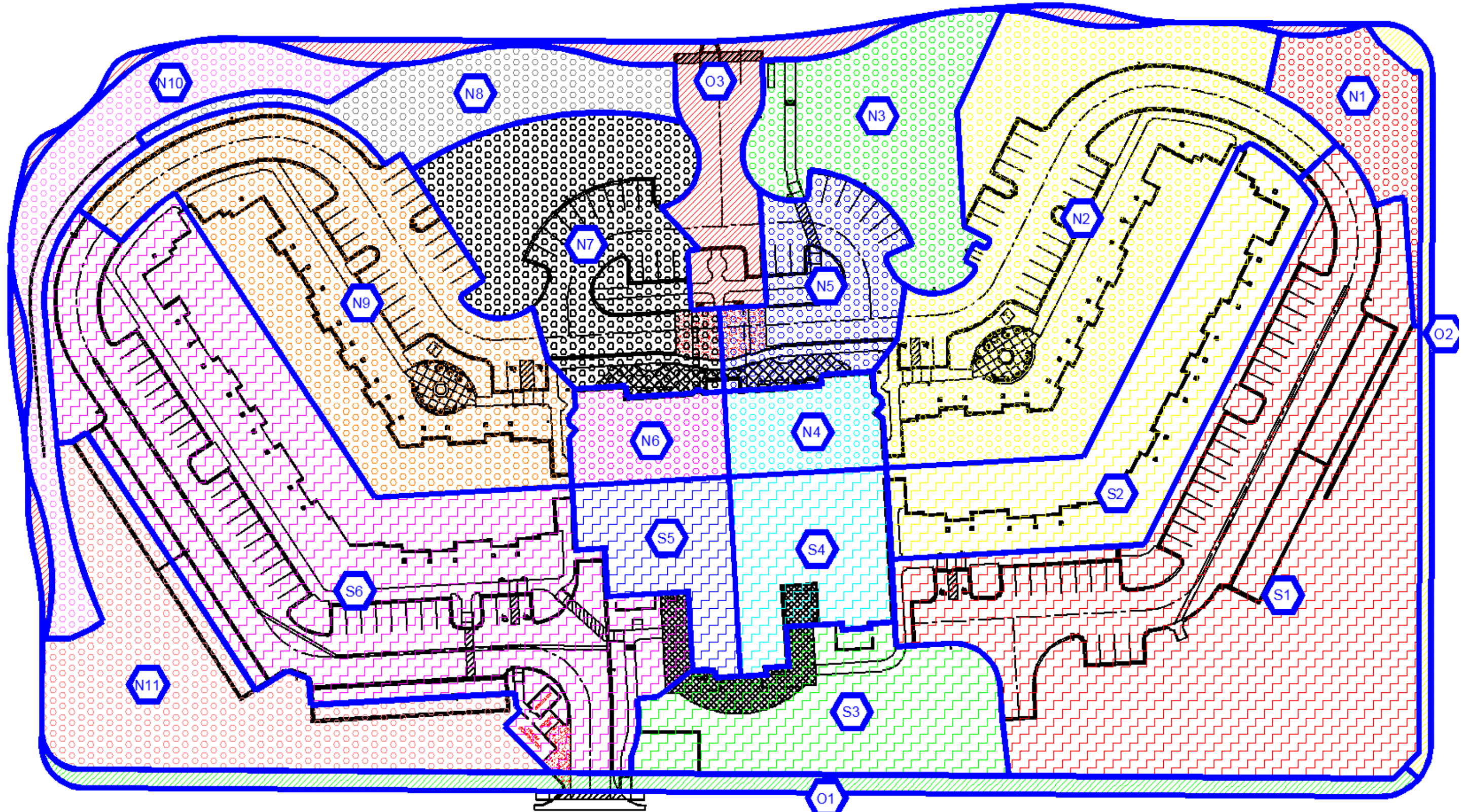
The proposed on-site private storm drain system is analyzed and sized as part as part of this submittal.

Stormwater control measures are required to provide management of 'First Flush' (defined as the 90th percentile storm event or 0.34" [0.44" less 0.1" for initial abstraction] of stormwater from impervious construction [Land Treatment 'D'] which discharges directly to a public storm drainage system).

Temporary ponds and earth swales with erosion protection as needed will be constructed off-site to pass the concentrated flow to the public storm drain system (to be constructed as part of CPN 689984).

Landscaped areas, other than those adjacent to buildings, are noted to be depressed for water harvesting. The stormwater calculations do not reflect this on-site water harvesting or 'First Flush' retention basins which may reduce the discharge rates.

DRAINAGE BASINS



DRAINAGE BASIN SUMMARY: (See the AHYMO printouts at the back of this packet)

Per the DMP, Tract 4B shall be allowed to discharge 30.9 cfs into the storm drain system connecting to the Derickson Ave. storm drain.

Based on the AHYMO calculations using the drainage basin areas and land treatment percentages shown below, the Q100-6HR will be 30.3 cfs. Therefore, the site is permitted free discharge. No retention / detention will be required other than the 'First Flush' basins.

BASIN	AREA (SF)	A (SF)	B (SF)	C (SF)	D (SF)	Q100 (AHYMO)
S1	60,993.70	0	8	50	42	4.96
S2	19,653.15	0	48	0	52	1.54
S3	15,578.25	0	25	50	25	1.16
S4	9,330.69	0	18	30	52	0.79
S5	7,169.59	0	0	0	100	0.72
S6	56,416.90	0	26	0	74	4.95
N1	6,502.48	0	20	80	0	0.44
N2	40,827.95	0	20	17	63	3.49
N3	14,046.50	0	80	16	4	0.84
N4	4,935.33	0	0	0	100	0.5
N5	10,174.78	0	12	0	88	0.97
N6	4,947.41	0	0	0	100	0.5
N7	21,048.76	0	40	13	47	1.65
N8	9,536.95	0	40	60	0	0.62
N9	33,968.47	0	28	0	72	2.95
N10	12,146.67	0	70	30	0	0.73
N11	22,445.84	0	30	70	0	1.48
O1	8,966.62	0	0	95	5	0.66
O2	3,550.91	0	0	100	0	0.26
O3	13,061.15	0	22	0	78	1.18
TOTAL DEVELOPED Q100						30.39

FIRST FLUSH REQUIREMENT:

The First Flush ponding volume required is 0.34" * Type 'D' area. The area of Land Treatment 'D' for each basin has been calculated (see chart below).

Required First Flush retention = (0.34 in /12 in per ft) * (Basin Area * % impervious) = CF volume

There are 'First Flush' retention basin areas throughout the site. Storm water from the impervious areas shall be directed to these basins via curb openings. Inlets that are placed in the basins show the top of grate located at the 'First Flush' water surface elevation.

BASIN	AREA (SF)	% IMPERV.	F.F. VOL (CF)
S1	60,993.70	42.00%	726
S2	19,653.15	52.00%	290
S3	15,578.25	25.00%	110
S4	9,330.69	52.00%	137
S5	7,169.59	100.00%	203
S6	56,416.90	74.00%	1183
N1	6,502.48	0.00%	0
N2	40,827.95	63.00%	729
N3	14,046.50	4.00%	16
N4	4,935.33	100.00%	140
N5	10,174.78	88.00%	254
N6	4,947.41	100.00%	140
N7	21,048.76	47.00%	280
N8	9,536.95	0.00%	0
N9	33,968.47	72.00%	693
N10	12,146.67	0.00%	0
N11	22,445.84	0.00%	0
O1	8,966.62	5.00%	13
O2	3,550.91	0.00%	0
O3	13,061.15	78.00%	289
TOTAL FIRST FLUSH RETENTION			5202

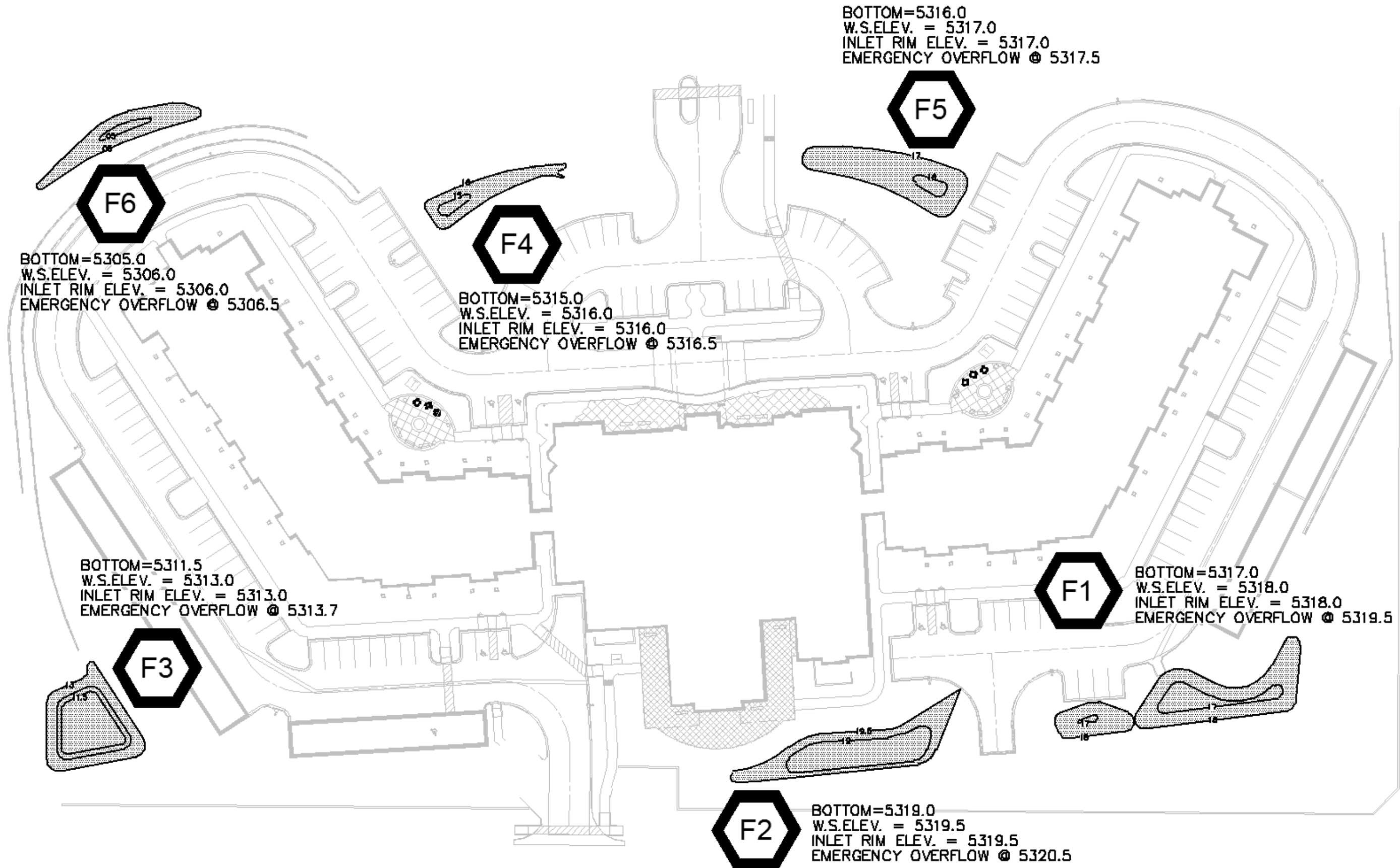
FIRST FLUSH PONDS:

The drainage from this property directs discharge to six First Flush retention ponding areas around the site. The design retention volume provided within each pond is shown below:

FIRST FLUSH POND F1				FIRST FLUSH POND F4			
Contour	Area	Volume		Contour	Area	Volume	
5318.00	3287			5316.00	1080		
5317.00	600	1944	CF	5315.00	123	602	CF
TOTAL VOL.		1944	CF	TOTAL VOL.		602	CF
FIRST FLUSH POND F2				FIRST FLUSH POND F5			
Contour	Area	Volume		Contour	Area	Volume	
5319.50	2709			5317.00	2118		
5319.00	1357	1017	CF	5316.00	154	1136	CF
TOTAL VOL.		1017	CF	TOTAL VOL.		1136	CF
FIRST FLUSH POND F3				FIRST FLUSH POND F6			
Contour	Area	Volume		Contour	Area	Volume	
5313.00	2481			5306.00	1277		
5311.50	981	2597	CF	5305.00	115	696	CF
TOTAL VOL.		2597	CF	TOTAL VOL.		696	CF

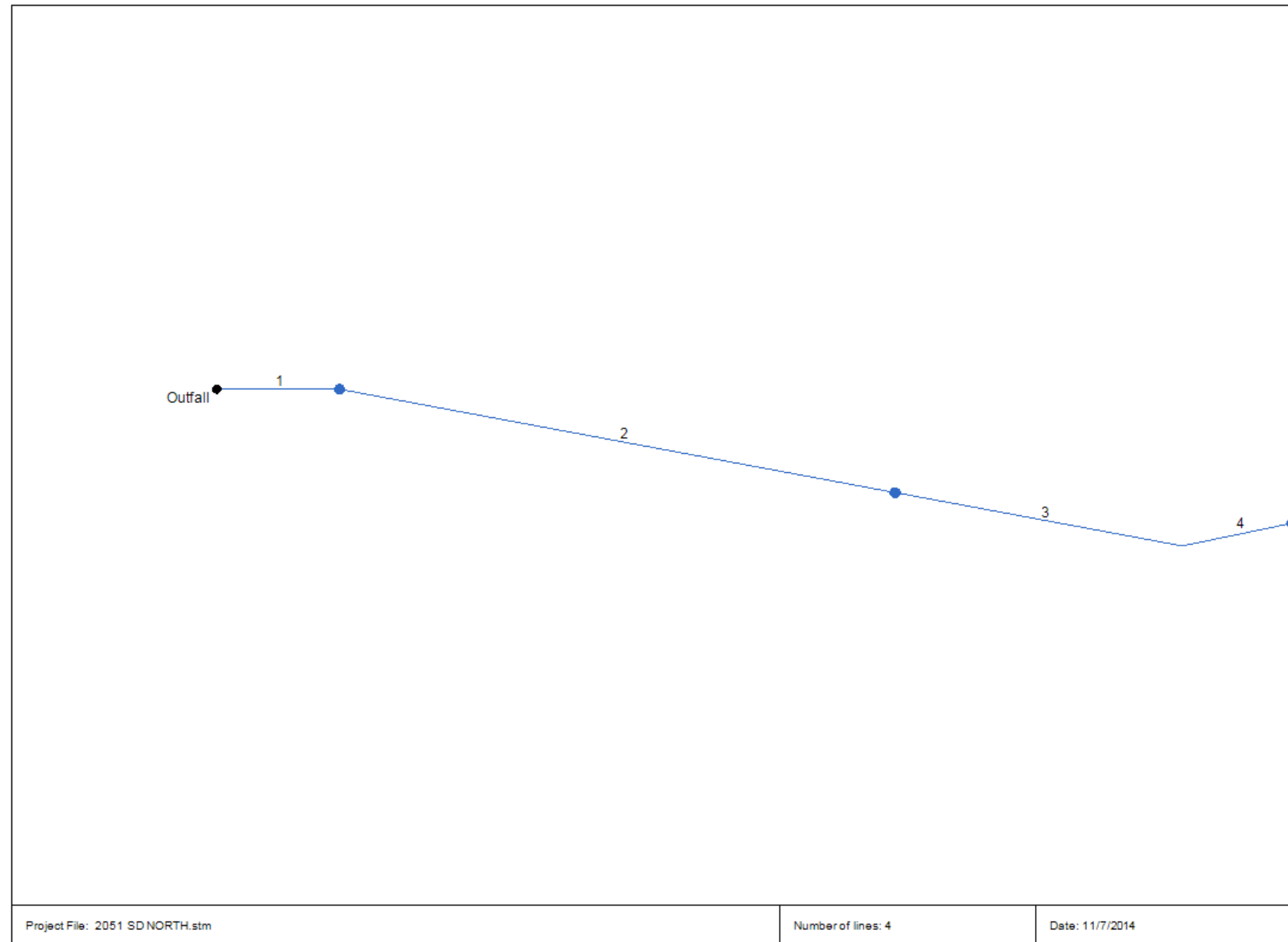
Total First Flush retention volume provided = 7,990 cf

Total First Flush retention volume required = 5,202 cf



NORTH SIDE STORM DRAIN ANALYSIS

Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



Storm Sewers v10.30

Storm Sewer Summary Report

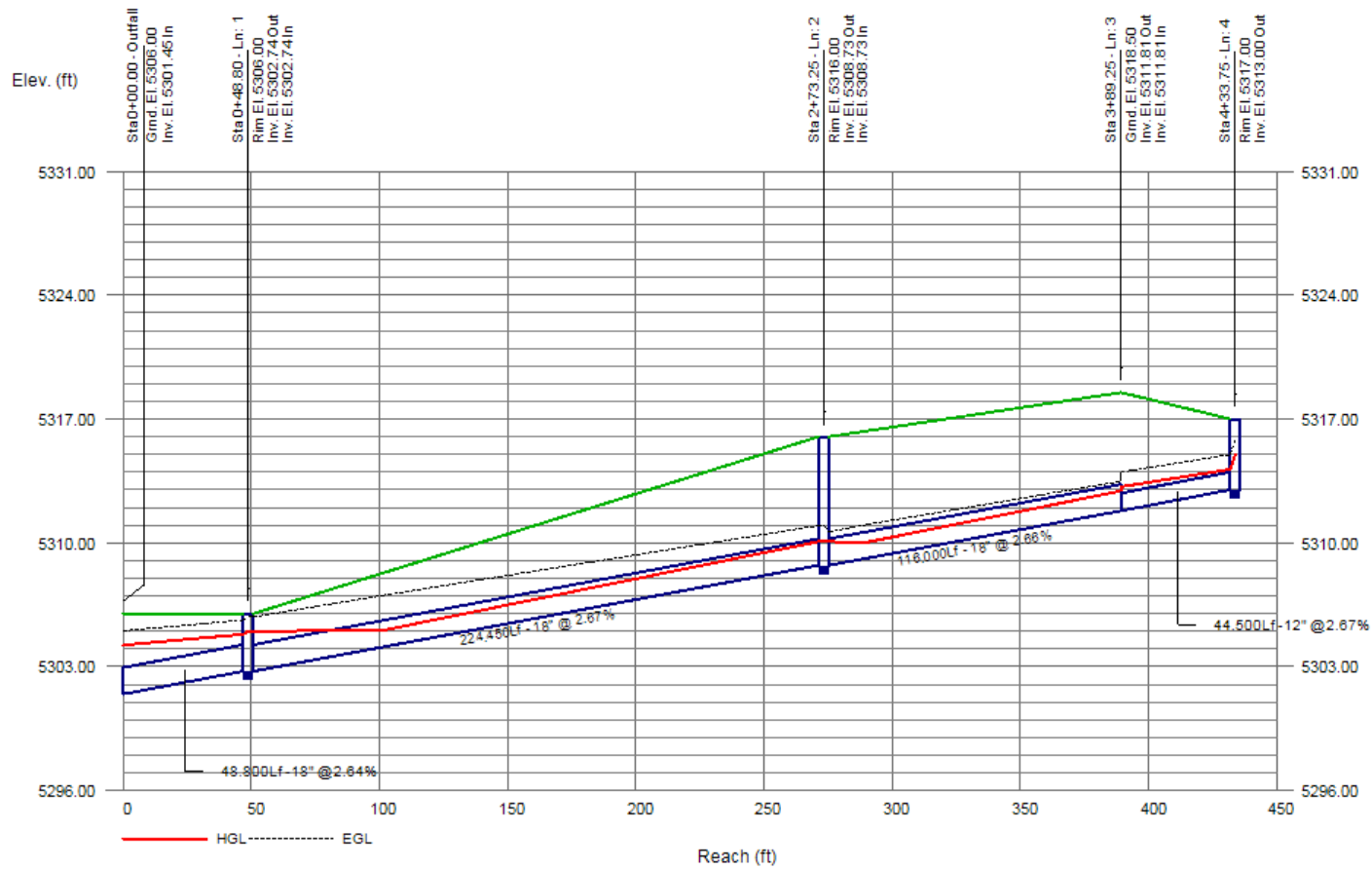
Page 1

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1		12.69	18	Cir	48.800	5301.45	5302.74	2.644	5304.22*	5304.83*	0.18	5305.00	End	Manhole
2		12.69	18	Cir	224.450	5302.74	5308.73	2.669	5305.00	5310.07	n/a	5310.07 j	1	Generic
3		8.39	18	Cir	116.000	5308.73	5311.81	2.655	5310.07	5312.93	n/a	5313.17 j	2	None
4		5.74	12	Cir	44.500	5311.81	5313.00	2.674	5313.17*	5314.16*	0.83	5314.99	3	Generic
Project File: 2051 SD NORTH.stm									Number of lines: 4			Run Date: 11/7/2014		
NOTES: Return period = 2 Yrs. ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump.														

Storm Sewers v10.30

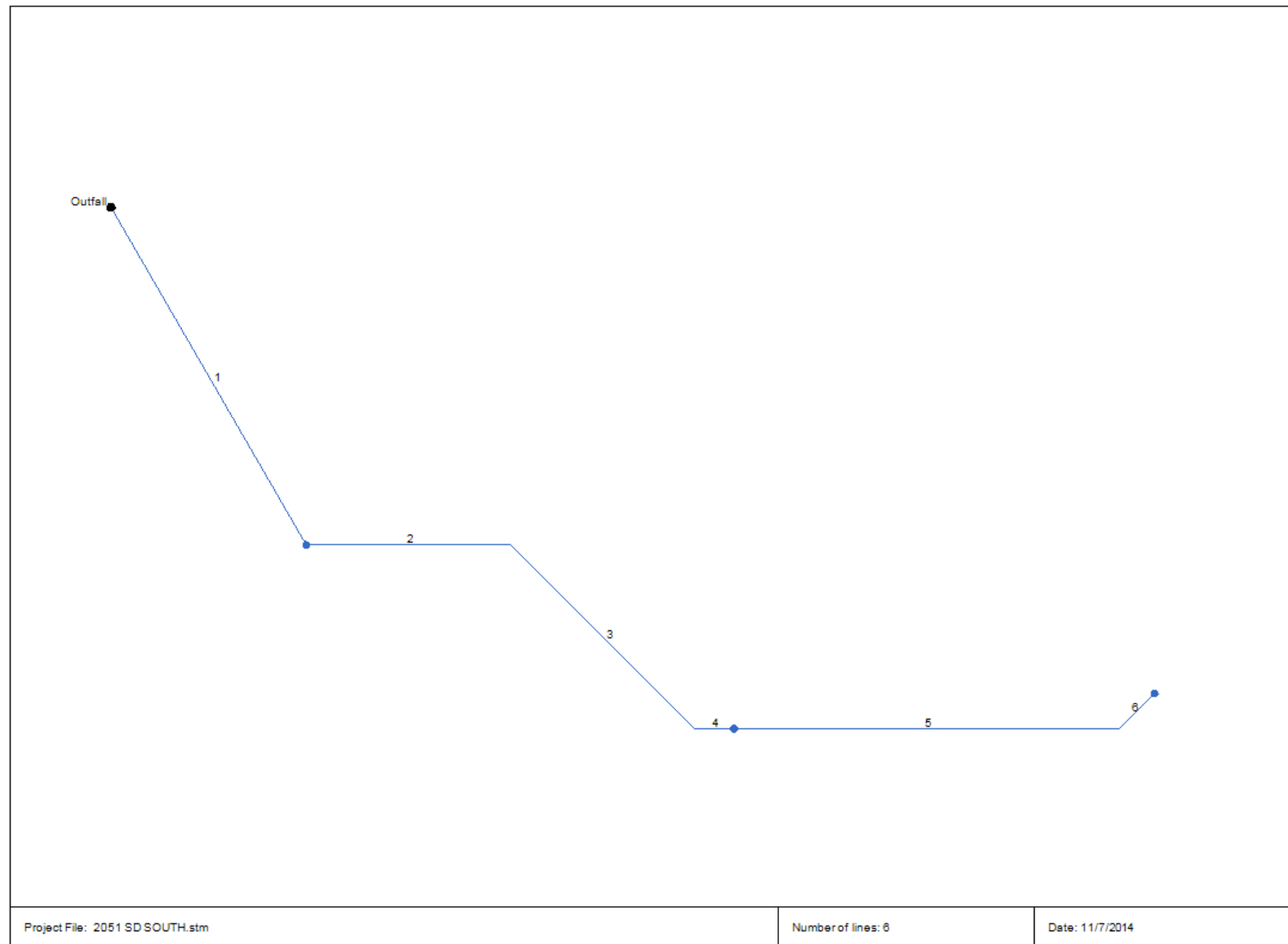
Storm Sewer Profile

Proj. file: 2051 SD NORTH.stm



SOUTH SIDE STORM DRAIN ANALYSIS

Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



Storm Sewers v10.30

Storm Sewer Summary Report

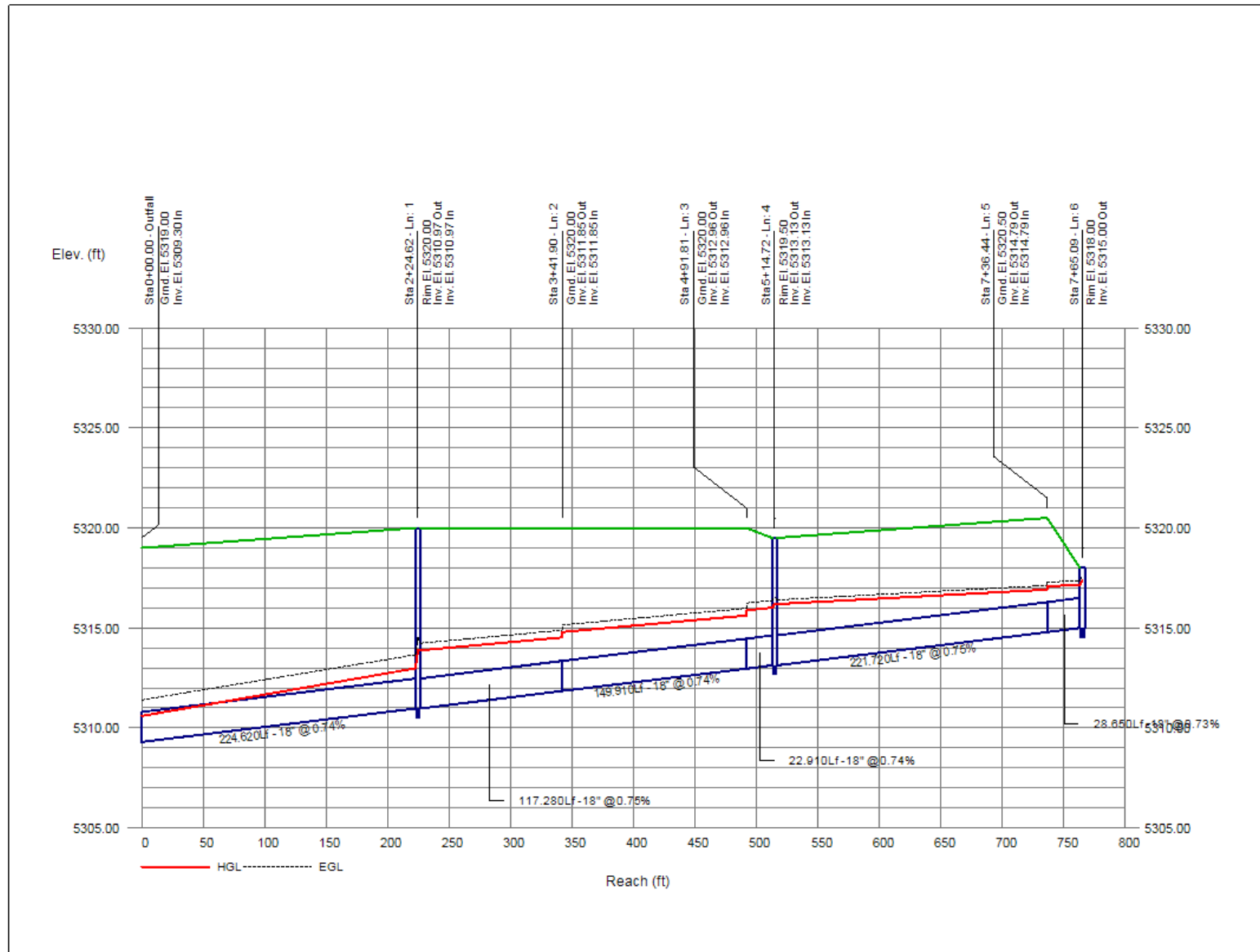
Page 1

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1		11.65	18	Cir	224.620	5309.30	5310.97	0.744	5310.60*	5312.96*	0.90	5313.88	End	Generic
2		8.45	18	Cir	117.280	5310.97	5311.85	0.750	5313.88*	5314.53*	0.27	5314.79	1	None
3		8.45	18	Cir	149.910	5311.85	5312.96	0.740	5314.79*	5315.62*	0.27	5315.89	2	None
4		8.45	18	Cir	22.910	5312.96	5313.13	0.742	5315.89*	5316.01*	0.18	5316.19	3	Generic
5		6.50	18	Cir	221.720	5313.13	5314.79	0.749	5316.19*	5316.92*	0.16	5317.07	4	None
6		6.50	18	Cir	28.650	5314.79	5315.00	0.733	5317.07*	5317.17*	0.21	5317.38	5	Generic
Project File: 2051 SD SOUTH.stm									Number of lines: 6			Run Date: 11/7/2014		
NOTES: Return period = 2 Yrs. ; *Surcharged (HGL above crown).														

Storm Sewers v10.30

Storm Sewer Profile

Proj. file: 2051 SD SOUTH.stm



Storm Sewers

WEST SIDE STORM DRAIN ANALYSIS

Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



Storm Sewers v10.30

Storm Sewer Summary Report

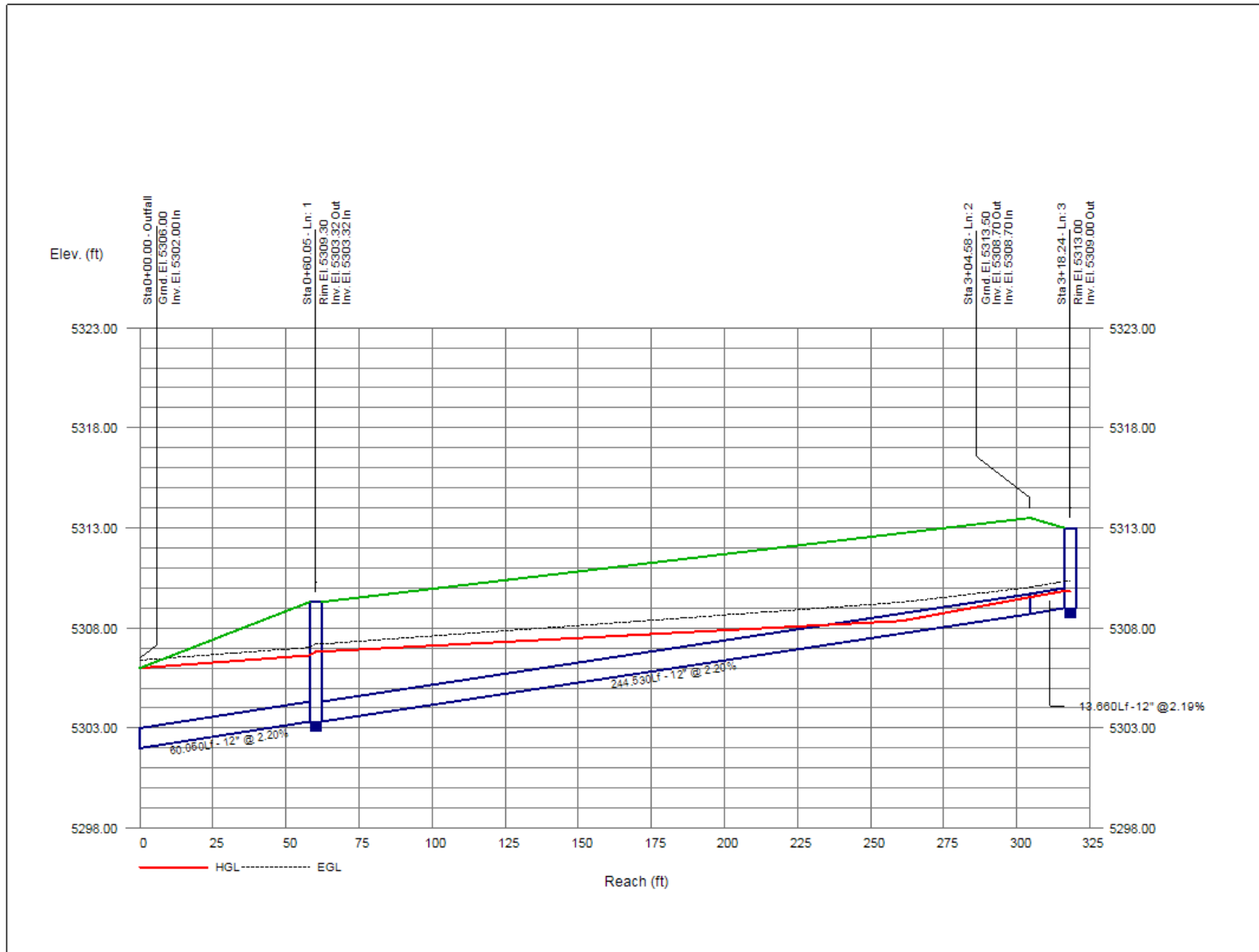
Page 1

Line No.	Line ID	Flow rate (cfs)	Line Size (in)	Line shape	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line Slope (%)	HGL Down (ft)	HGL Up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns Line No.	Junction Type
1		3.96	12	Cir	60.050	5302.00	5303.32	2.198	5306.00*	5306.63*	0.17	5306.81	End	Manhole
2		3.96	12	Cir	244.530	5303.32	5308.70	2.200	5306.81	5309.54	n/a	5309.54 j	1	None
3		3.96	12	Cir	13.660	5308.70	5309.00	2.195	5309.54	5309.84	0.49	5309.84	2	Generic
Project File: 2051 SD WEST.stm									Number of lines: 3			Run Date: 11/7/2014		
NOTES: Return period = 2 Yrs. ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump.														

Storm Sewers v10.30

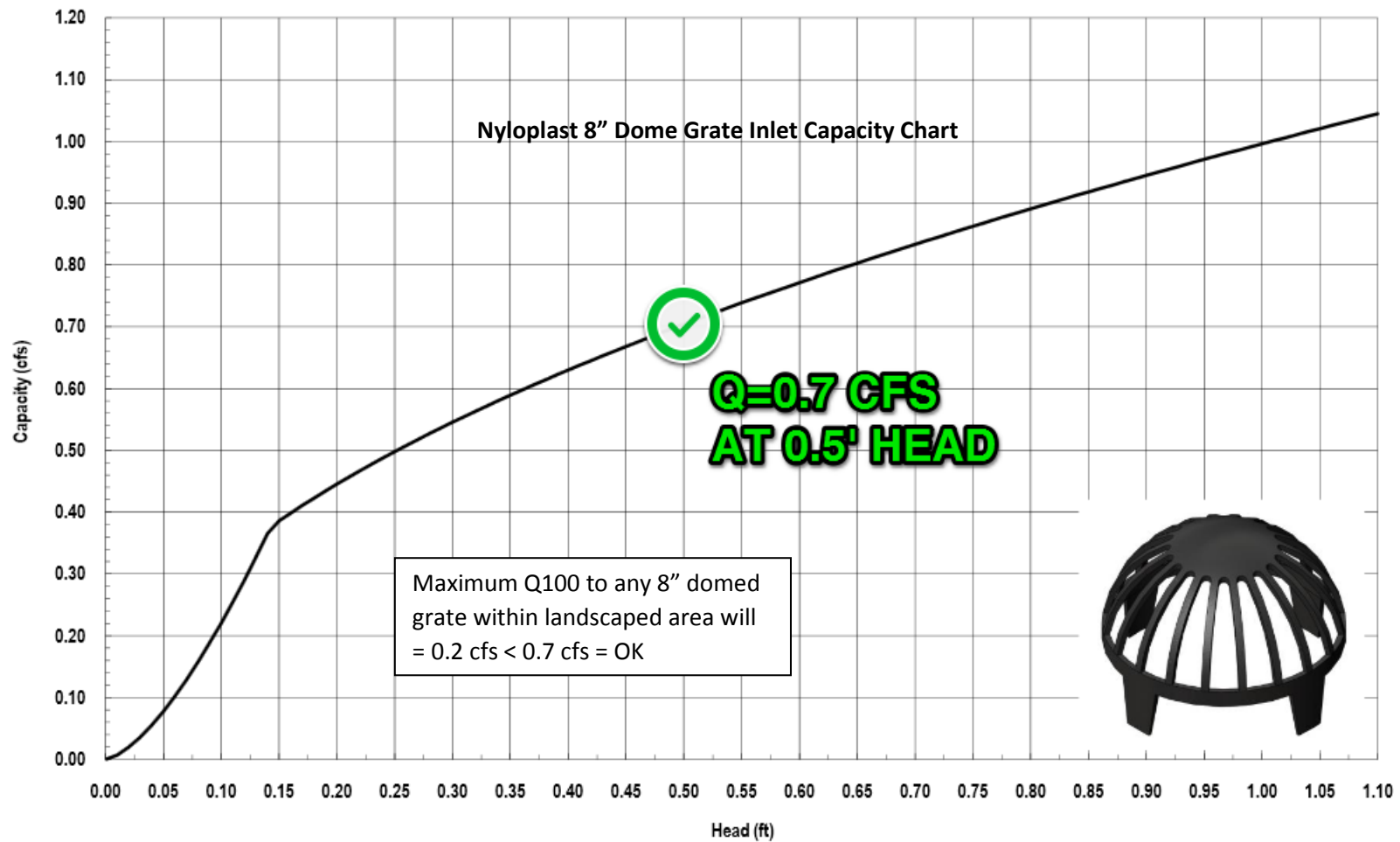
Storm Sewer Profile

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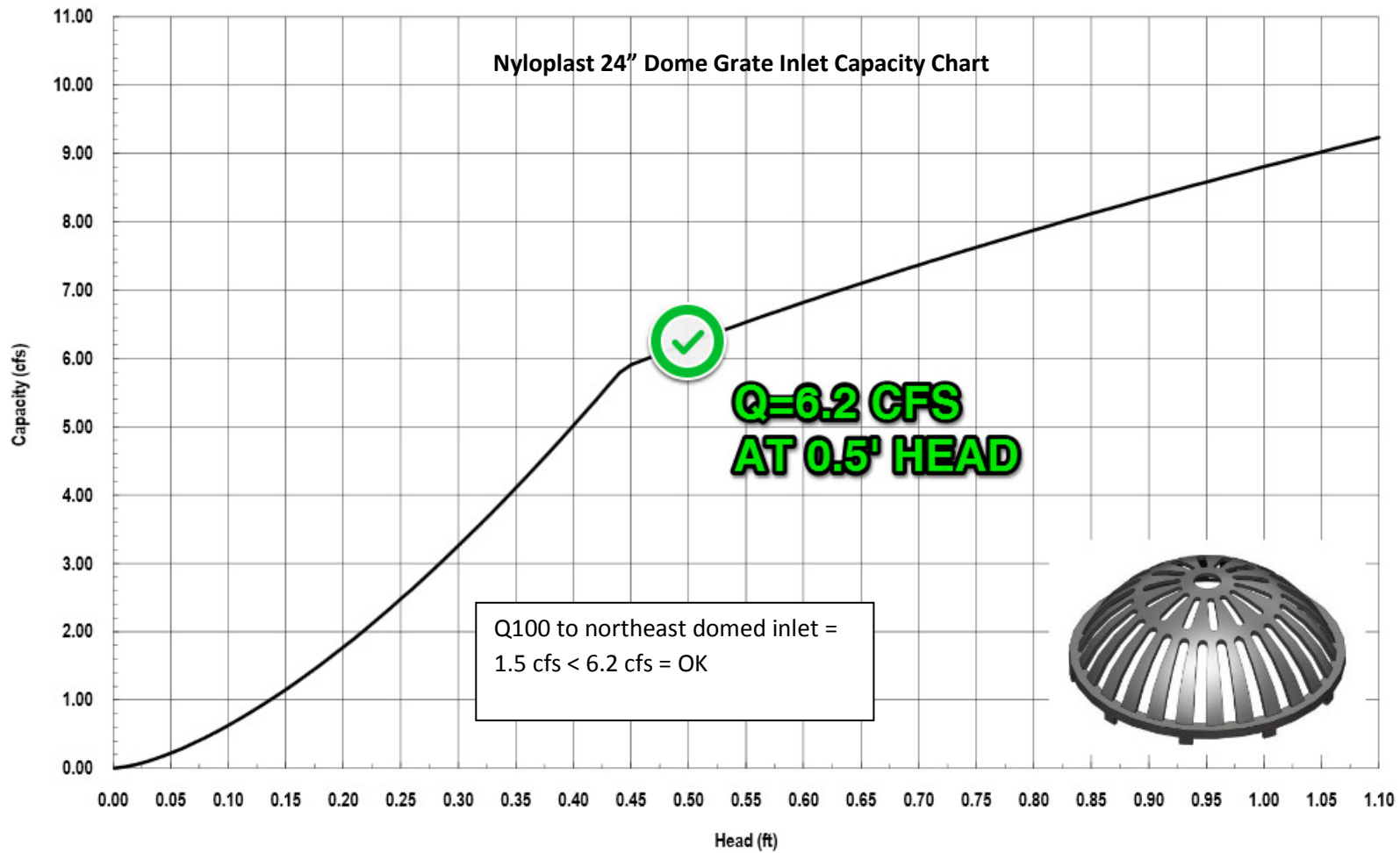


Storm Sewers

INLET GRATE CAPACITIES




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APPENDIX A

AHYMO CALCULATIONS

AHYMO PROGRAM SUMMARY TABLE (AHYMO-S4)
 INPUT FILE = M:\PROJECTS\2000-2099\2051\CALCS\2051dev.dat

- Ver. S4.01a, Rel: 01a

RUN DATE (MON/DAY/YR) =11/05/2014
 USER NO.= AHYMO_Temp_User:20122010

COMMAND	HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1 NOTATION

*S	SANTA MONICA PLACE									
*S	TRACTS 4-A									
*S	100-YEAR, 6-HOUR STORM									
*S	2051DEV.DAT									
*S										
*S	BY GENNY DONART									
*S	ISAACSON & ARFMAN, P.A.									
*S	OCTOBER, 2014									

*S										
*S	Rainfall distribution based on NOAA Atlas 14 maps									
*S	Latitude=35.1625 Longitude=-106.5741									
*S										

START									TIME=	0.00
RAINFALL TYPE= 1 NOAA 14									RAIN6=	2.410
*S	BASIN S1									
COMPUTE NM HYD	S1	-	1	0.00219	4.96	0.174	1.49143	1.533	3.539 PER IMP=	42.00
*S	BASIN S2									
COMPUTE NM HYD	S2	-	2	0.00071	1.54	0.057	1.51323	1.533	3.423 PER IMP=	52.00
*S	BASIN S3									
COMPUTE NM HYD	S3	-	3	0.00056	1.16	0.038	1.26423	1.533	3.244 PER IMP=	25.00
*S	BASIN S4									
COMPUTE NM HYD	S4	-	4	0.00034	0.79	0.028	1.58015	1.533	3.664 PER IMP=	52.00
*S	BASIN S5									
COMPUTE NM HYD	S5	-	5	0.00026	0.72	0.030	2.15347	1.500	4.370 PER IMP=	100.00
*S	BASIN S6									
COMPUTE NM HYD	S6	-	6	0.00202	4.95	0.195	1.80668	1.533	3.818 PER IMP=	74.00
*S	BASIN N1									
COMPUTE NM HYD	N1	-	11	0.00023	0.44	0.012	0.99745	1.533	2.983 PER IMP=	0.00
*S	BASIN N2									
COMPUTE NM HYD	N2	-	12	0.00147	3.49	0.133	1.69629	1.533	3.723 PER IMP=	63.00
*S	BASIN N3									
COMPUTE NM HYD	N3	-	13	0.00050	0.84	0.024	0.90239	1.533	2.611 PER IMP=	4.00
*S	BASIN N4									
COMPUTE NM HYD	N4	-	14	0.00018	0.50	0.020	2.15347	1.500	4.387 PER IMP=	100.00
*S	BASIN N5									
COMPUTE NM HYD	N5	-	15	0.00037	0.97	0.039	1.99341	1.500	4.159 PER IMP=	88.00

*S	BASIN N6											
COMPUTE	NM HYD	N6	-	16	0.00018	0.50	0.020	2.15347	1.500	4.387	PER IMP=	100.00
*S	BASIN N7											
COMPUTE	NM HYD	N7	-	17	0.00076	1.65	0.059	1.47190	1.533	3.406	PER IMP=	47.00
*S	BASIN N8											
COMPUTE	NM HYD	N8	-	18	0.00034	0.62	0.017	0.95307	1.533	2.826	PER IMP=	0.00
*S	BASIN N9											
COMPUTE	NM HYD	N9	-	19	0.00122	2.95	0.116	1.78000	1.533	3.788	PER IMP=	72.00
*S	BASIN N10											
COMPUTE	NM HYD	N10	-	20	0.00044	0.73	0.020	0.87996	1.533	2.611	PER IMP=	0.00
*S	BASIN N11											
COMPUTE	NM HYD	N11	-	21	0.00081	1.48	0.042	0.97501	1.533	2.870	PER IMP=	0.00
*S	BASIN O1											
COMPUTE	NM HYD	O1	-	31	0.00032	0.66	0.019	1.10153	1.533	3.190	PER IMP=	5.00
*S	BASIN O2											
COMPUTE	NM HYD	O2	-	32	0.00013	0.26	0.007	1.04616	1.533	3.169	PER IMP=	0.00
*S	BASIN O3											
COMPUTE	NM HYD	O3	-	33	0.00000	0.00	NaN	NaN	-0.133	NaN	PER IMP=	0.00

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*S*****
*S      SANTA MONICA PLACE
*S      TRACTS 4-A
*S      100-YEAR, 6-HOUR STORM
*S      2051DEV.DAT
*S
*S      BY GENNY DONART
*S      ISAACSON & ARFMAN, P.A.
*S      OCTOBER, 2014
*S*****
*      100-YR, 6-HR STORM
*      PRECIPITATION:
*          P15 =      0"
*          P60 =      1.79"
*          P360 =      2.41"
*          P1440 =      2.77"
*
*****
*S
*S      Rainfall distribution based on NOAA Atlas 14 maps
*S      Latitude=35.1625 Longitude=-106.5741
*S
*S*****
START          TIME=0.0 HR PUNCH CODE=0 PRINT LINE=60
RAINFALL      TYPE=1 RAIN QUARTER=0
              RAIN ONE=1.79 IN RAIN SIX=2.41 IN
              RAIN DAY=2.77 IN DT=0.03333333 HRS
        6-HOUR RAINFALL DIST. - BASED ON NOAA ATLAS 14 FOR CONVECTIVE AREAS (NM & AZ) - D1
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          0.0000  0.0027  0.0055  0.0084  0.0114  0.0144  0.0178
          0.0212  0.0248  0.0286  0.0324  0.0411  0.0498  0.0589
          0.0685  0.0781  0.0885  0.0989  0.1095  0.1204  0.1312
          0.1426  0.1539  0.1658  0.1783  0.1908  0.2048  0.2188
          0.2345  0.2517  0.2690  0.2921  0.3152  0.3430  0.3753
          0.4077  0.4563  0.5048  0.5711  0.6549  0.7388  0.9622
          1.1856  1.3593  1.4831  1.6070  1.6692  1.7314  1.7821
          1.8213  1.8605  1.8877  1.9149  1.9384  1.9583  1.9782
          1.9932  2.0083  2.0224  2.0356  2.0489  2.0607  2.0726
          2.0836  2.0936  2.1036  2.1128  2.1221  2.1312  2.1402
          2.1491  2.1532  2.1573  2.1614  2.1653  2.1693  2.1729
          2.1766  2.1803  2.1839  2.1874  2.1909  2.1944  2.1978
          2.2010  2.2043  2.2075  2.2107  2.2138  2.2170  2.2201
          2.2230  2.2260  2.2289  2.2318  2.2346  2.2374  2.2403
          2.2430  2.2457  2.2484  2.2510  2.2536  2.2562  2.2588
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          2.3395  2.3415  2.3434  2.3454  2.3473  2.3492  2.3511
          2.3530  2.3549  2.3568  2.3587  2.3605  2.3623  2.3642
          2.3660  2.3678  2.3696  2.3714  2.3732  2.3749  2.3767
          2.3784  2.3802  2.3819  2.3836  2.3854  2.3871  2.3888
          2.3904  2.3921  2.3938  2.3954  2.3971  2.3987  2.4004
          2.4020  2.4036  2.4052  2.4068  2.4084  2.4100
*S      BASIN S1
COMPUTE NM HYD      ID=1 HYD NO=S1 DA=0.002188 SQ MI
                   %A=0 %B=8 %C=50 %D=42
                   TP=-0.1333 HR
                   MASS RAINFALL=-1
      K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
      UNIT PEAK = 3.6281 CFS UNIT VOLUME = 0.9961 B = 526.28 P60 = 1.7900
      AREA = 0.000919 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
      RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

      K = 0.108749HR TP = 0.133300HR K/TP RATIO = 0.815818 SHAPE CONSTANT, N = 4.381263
      UNIT PEAK = 3.6161 CFS UNIT VOLUME = 0.9969 B = 379.84 P60 = 1.7900
      AREA = 0.001269 SQ MI IA = 0.37069 INCHES INF = 0.88793 INCHES PER HOUR
      RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333
PRINT HYD      ID=1 CODE=1
                                HYDROGRAPH FROM AREA S1

```

RUNOFF VOLUME = 1.49143 INCHES = 0.1740 ACRE-FEET
PEAK DISCHARGE RATE = 4.96 CFS AT 1.533 HOURS BASIN AREA = 0.0022 SQ. MI.

*S BASIN S2

COMPUTE NM HYD ID=2 HYD NO=S2 DA=0.000705 SQ MI
%A=0 %B=48 %C=0 %D=52
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 1.4474 CFS UNIT VOLUME = 0.9911 B = 526.28 P60 = 1.7900
AREA = 0.000367 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.132400HR TP = 0.133300HR K/TP RATIO = 0.993245 SHAPE CONSTANT, N = 3.554456
UNIT PEAK = 0.82325 CFS UNIT VOLUME = 0.9830 B = 324.29 P60 = 1.7900
AREA = 0.000338 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=2 CODE=1

HYDROGRAPH FROM AREA S2

RUNOFF VOLUME = 1.51323 INCHES = 0.0569 ACRE-FEET
PEAK DISCHARGE RATE = 1.54 CFS AT 1.533 HOURS BASIN AREA = 0.0007 SQ. MI.

*S BASIN S3

COMPUTE NM HYD ID=3 HYD NO=S3 DA= 0.000559 SQ MI
%A=0 %B=25 %C=50 %D=25
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 0.55174 CFS UNIT VOLUME = 0.9786 B = 526.28 P60 = 1.7900
AREA = 0.000140 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.114109HR TP = 0.133300HR K/TP RATIO = 0.856035 SHAPE CONSTANT, N = 4.155676
UNIT PEAK = 1.1493 CFS UNIT VOLUME = 0.9888 B = 365.42 P60 = 1.7900
AREA = 0.000419 SQ MI IA = 0.40000 INCHES INF = 0.97000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=3 CODE=1

HYDROGRAPH FROM AREA S3

RUNOFF VOLUME = 1.26423 INCHES = 0.0377 ACRE-FEET
PEAK DISCHARGE RATE = 1.16 CFS AT 1.533 HOURS BASIN AREA = 0.0006 SQ. MI.

*S BASIN S4

COMPUTE NM HYD ID=4 HYD NO=S4 DA= 0.000335 SQ MI
%A=0 %B=18 %C=30 %D=52
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 0.68775 CFS UNIT VOLUME = 0.9815 B = 526.28 P60 = 1.7900
AREA = 0.000174 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.115253HR TP = 0.133300HR K/TP RATIO = 0.864610 SHAPE CONSTANT, N = 4.110986
UNIT PEAK = 0.43729 CFS UNIT VOLUME = 0.9691 B = 362.50 P60 = 1.7900
AREA = 0.000161 SQ MI IA = 0.40625 INCHES INF = 0.98750 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=4 CODE=1

HYDROGRAPH FROM AREA S4

RUNOFF VOLUME = 1.58015 INCHES = 0.0282 ACRE-FEET
PEAK DISCHARGE RATE = 0.79 CFS AT 1.533 HOURS BASIN AREA = 0.0003 SQ. MI.

*S BASIN S5

COMPUTE NM HYD ID=5 HYD NO=S5 DA= 0.000257 SQ MI
%A=0 %B=0 %C=0 %D=100
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 1.0146 CFS UNIT VOLUME = 0.9881 B = 526.28 P60 = 1.7900
AREA = 0.000257 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=5 CODE=1

HYDROGRAPH FROM AREA S5

RUNOFF VOLUME = 2.15347 INCHES = 0.0295 ACRE-FEET
PEAK DISCHARGE RATE = 0.72 CFS AT 1.500 HOURS BASIN AREA = 0.0003 SQ. MI.

*S BASIN S6

COMPUTE NM HYD ID=6 HYD NO=S6 DA= 0.002024 SQ MI
%A=0 %B=26 %C=0 %D=74
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 5.9132 CFS UNIT VOLUME = 0.9976 B = 526.28 P60 = 1.7900
AREA = 0.001498 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.132400HR TP = 0.133300HR K/TP RATIO = 0.993245 SHAPE CONSTANT, N = 3.554456
UNIT PEAK = 1.2802 CFS UNIT VOLUME = 0.9899 B = 324.29 P60 = 1.7900
AREA = 0.000526 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

*S BASIN N1

COMPUTE NM HYD ID=11 HYD NO=N1 DA= 0.000233 SQ MI
%A=0 %B=20 %C=80 %D=0
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.110451HR TP = 0.133300HR K/TP RATIO = 0.828593 SHAPE CONSTANT, N = 4.306599
UNIT PEAK = 0.65568 CFS UNIT VOLUME = 0.9797 B = 375.12 P60 = 1.7900
AREA = 0.000233 SQ MI IA = 0.38000 INCHES INF = 0.91400 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=11 CODE=1

HYDROGRAPH FROM AREA N1

RUNOFF VOLUME = 0.99745 INCHES = 0.0124 ACRE-FEET
PEAK DISCHARGE RATE = 0.44 CFS AT 1.533 HOURS BASIN AREA = 0.0002 SQ. MI.

*S BASIN N2

COMPUTE NM HYD ID=12 HYD NO=N2 DA= 0.001465 SQ MI
%A=0 %B=20 %C=17 %D=63
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 3.6439 CFS UNIT VOLUME = 0.9961 B = 526.28 P60 = 1.7900
AREA = 0.000923 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.119794HR TP = 0.133300HR K/TP RATIO = 0.898681 SHAPE CONSTANT, N = 3.943851
UNIT PEAK = 1.4290 CFS UNIT VOLUME = 0.9911 B = 351.41 P60 = 1.7900
AREA = 0.000542 SQ MI IA = 0.43108 INCHES INF = 1.05703 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=12 CODE=1

HYDROGRAPH FROM AREA N2

RUNOFF VOLUME = 1.69629 INCHES = 0.1325 ACRE-FEET
PEAK DISCHARGE RATE = 3.49 CFS AT 1.533 HOURS BASIN AREA = 0.0015 SQ. MI.

*S BASIN N3

COMPUTE NM HYD ID=13 HYD NO=N3 DA= 0.000504 SQ MI
%A=0 %B=80 %C=16 %D=4
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 0.79593E-01CFS UNIT VOLUME = 0.8874 B = 526.28 P60 = 1.7900
AREA = 0.000020 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.127827HR TP = 0.133300HR K/TP RATIO = 0.958942 SHAPE CONSTANT, N = 3.684573
UNIT PEAK = 1.2108 CFS UNIT VOLUME = 0.9893 B = 333.57 P60 = 1.7900
AREA = 0.000484 SQ MI IA = 0.47500 INCHES INF = 1.18000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=13 CODE=1

HYDROGRAPH FROM AREA N3

RUNOFF VOLUME = 0.90239 INCHES = 0.0243 ACRE-FEET
PEAK DISCHARGE RATE = 0.84 CFS AT 1.533 HOURS BASIN AREA = 0.0005 SQ. MI.

*S BASIN N4

COMPUTE NM HYD ID=14 HYD NO=N4 DA= 0.000177 SQ MI
%A=0 %B=0 %C=0 %D=100
TP=-0.1333 HR

MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 0.69881 CFS UNIT VOLUME = 0.9840 B = 526.28 P60 = 1.7900
AREA = 0.000177 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333
PRINT HYD ID=14 CODE=1

HYDROGRAPH FROM AREA N4

RUNOFF VOLUME = 2.15347 INCHES = 0.0203 ACRE-FEET
PEAK DISCHARGE RATE = 0.50 CFS AT 1.500 HOURS BASIN AREA = 0.0002 SQ. MI.

*S BASIN N5

COMPUTE NM HYD ID=15 HYD NO=N5 DA=0.000365 SQ MI
%A=0 %B=12 %C=0 %D=88
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 1.2681 CFS UNIT VOLUME = 0.9897 B = 526.28 P60 = 1.7900
AREA = 0.000321 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.132400HR TP = 0.133300HR K/TP RATIO = 0.993245 SHAPE CONSTANT, N = 3.554456
UNIT PEAK = 0.10656 CFS UNIT VOLUME = 0.8706 B = 324.29 P60 = 1.7900
AREA = 0.000044 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=15 CODE=1

HYDROGRAPH FROM AREA N5

RUNOFF VOLUME = 1.99341 INCHES = 0.0388 ACRE-FEET
PEAK DISCHARGE RATE = 0.97 CFS AT 1.500 HOURS BASIN AREA = 0.0004 SQ. MI.

*S BASIN N6

COMPUTE NM HYD ID=16 HYD NO=N6 DA= 0.000177 SQ MI
%A=0 %B=0 %C=0 %D=100
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 0.69881 CFS UNIT VOLUME = 0.9840 B = 526.28 P60 = 1.7900
AREA = 0.000177 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=16 CODE=1

HYDROGRAPH FROM AREA N6

RUNOFF VOLUME = 2.15347 INCHES = 0.0203 ACRE-FEET
PEAK DISCHARGE RATE = 0.50 CFS AT 1.500 HOURS BASIN AREA = 0.0002 SQ. MI.

*S BASIN N7

COMPUTE NM HYD ID=17 HYD NO=N7 DA= 0.000755 SQ MI
%A=0 %B=40 %C=13 %D=47
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 1.4010 CFS UNIT VOLUME = 0.9911 B = 526.28 P60 = 1.7900
AREA = 0.000355 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.125670HR TP = 0.133300HR K/TP RATIO = 0.942762 SHAPE CONSTANT, N = 3.750104
UNIT PEAK = 1.0151 CFS UNIT VOLUME = 0.9868 B = 338.16 P60 = 1.7900
AREA = 0.000400 SQ MI IA = 0.46321 INCHES INF = 1.14698 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=17 CODE=1

HYDROGRAPH FROM AREA N7

RUNOFF VOLUME = 1.47190 INCHES = 0.0593 ACRE-FEET
PEAK DISCHARGE RATE = 1.65 CFS AT 1.533 HOURS BASIN AREA = 0.0008 SQ. MI.

*S BASIN N8

COMPUTE NM HYD ID=18 HYD NO=N8 DA= 0.000342 SQ MI
%A=0 %B=40 %C=60 %D=0
TP=-0.1333 HR
MASS RAINFALL=-1
K = 0.115938HR TP = 0.133300HR K/TP RATIO = 0.869756 SHAPE CONSTANT, N = 4.084704
UNIT PEAK = 0.92563 CFS UNIT VOLUME = 0.9857 B = 360.78 P60 = 1.7900
AREA = 0.000342 SQ MI IA = 0.41000 INCHES INF = 0.99800 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=18 CODE=1

HYDROGRAPH FROM AREA N8

RUNOFF VOLUME = 0.95307 INCHES = 0.0174 ACRE-FEET
 PEAK DISCHARGE RATE = 0.62 CFS AT 1.533 HOURS BASIN AREA = 0.0003 SQ. MI.

*S BASIN N9

COMPUTE NM HYD ID=19 HYD NO=N9 DA=0.001218 SQ MI

%A=0 %B=28 %C=0 %D=72

TP=-0.1333 HR

MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 3.4623 CFS UNIT VOLUME = 0.9961 B = 526.28 P60 = 1.7900

AREA = 0.000877 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.132400HR TP = 0.133300HR K/TP RATIO = 0.993245 SHAPE CONSTANT, N = 3.554456

UNIT PEAK = 0.82967 CFS UNIT VOLUME = 0.9844 B = 324.29 P60 = 1.7900

AREA = 0.000341 SQ MI IA = 0.50000 INCHES INF = 1.25000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=19 CODE=1

HYDROGRAPH FROM AREA N9

RUNOFF VOLUME = 1.78000 INCHES = 0.1156 ACRE-FEET
 PEAK DISCHARGE RATE = 2.95 CFS AT 1.533 HOURS BASIN AREA = 0.0012 SQ. MI.

*S BASIN N10

COMPUTE NM HYD ID=20 HYD NO=N10 DA=0.000436 SQ MI

%A=0 %B=70 %C=30 %D=0

TP=-0.1333 HR

MASS RAINFALL=-1

K = 0.124169HR TP = 0.133300HR K/TP RATIO = 0.931500 SHAPE CONSTANT, N = 3.797410

UNIT PEAK = 1.1168 CFS UNIT VOLUME = 0.9886 B = 341.43 P60 = 1.7900

AREA = 0.000436 SQ MI IA = 0.45500 INCHES INF = 1.12400 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=20 CODE=1

HYDROGRAPH FROM AREA N10

RUNOFF VOLUME = 0.87996 INCHES = 0.0205 ACRE-FEET
 PEAK DISCHARGE RATE = 0.73 CFS AT 1.533 HOURS BASIN AREA = 0.0004 SQ. MI.

*S BASIN N11

COMPUTE NM HYD ID=21 HYD NO=N11 DA=0.000805 SQ MI

%A=0 %B=30 %C=70 %D=0

TP=-0.1333 HR

MASS RAINFALL=-1

K = 0.113195HR TP = 0.133300HR K/TP RATIO = 0.849174 SHAPE CONSTANT, N = 4.192253

UNIT PEAK = 2.2211 CFS UNIT VOLUME = 0.9940 B = 367.79 P60 = 1.7900

AREA = 0.000805 SQ MI IA = 0.39500 INCHES INF = 0.95600 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=21 CODE=1

HYDROGRAPH FROM AREA N11

RUNOFF VOLUME = 0.97501 INCHES = 0.0419 ACRE-FEET
 PEAK DISCHARGE RATE = 1.48 CFS AT 1.533 HOURS BASIN AREA = 0.0008 SQ. MI.

*S BASIN O1

COMPUTE NM HYD ID=31 HYD NO=O1 DA=0.000322 SQ MI

%A=0 %B=0 %C=95 %D=5

TP=-0.1333 HR

MASS RAINFALL=-1

K = 0.072649HR TP = 0.133300HR K/TP RATIO = 0.545000 SHAPE CONSTANT, N = 7.106428

UNIT PEAK = 0.63564E-01CFS UNIT VOLUME = 0.8874 B = 526.28 P60 = 1.7900

AREA = 0.000016 SQ MI IA = 0.10000 INCHES INF = 0.04000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

K = 0.104964HR TP = 0.133300HR K/TP RATIO = 0.787430 SHAPE CONSTANT, N = 4.558258

UNIT PEAK = 0.89686 CFS UNIT VOLUME = 0.9861 B = 390.82 P60 = 1.7900

AREA = 0.000306 SQ MI IA = 0.35000 INCHES INF = 0.83000 INCHES PER HOUR

RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333

PRINT HYD ID=31 CODE=1

HYDROGRAPH FROM AREA O1

RUNOFF VOLUME = 1.10153 INCHES = 0.0189 ACRE-FEET
 PEAK DISCHARGE RATE = 0.66 CFS AT 1.533 HOURS BASIN AREA = 0.0003 SQ. MI.

*S BASIN O2

```

COMPUTE NM HYD      ID=32  HYD NO=02  DA=0.000127 SQ MI
                    %A=0  %B=0  %C=100  %D=0
                    TP=-0.1333 HR
                    MASS RAINFALL=-1
K = 0.104964HR      TP = 0.133300HR      K/TP RATIO = 0.787430      SHAPE CONSTANT, N = 4.558258
UNIT PEAK = 0.37235 CFS      UNIT VOLUME = 0.9671      B = 390.82      P60 = 1.7900
AREA = 0.000127 SQ MI      IA = 0.35000 INCHES      INF = 0.83000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.033333
PRINT HYD          ID=32 CODE=1

```

HYDROGRAPH FROM AREA 02

```

RUNOFF VOLUME = 1.04616 INCHES = 0.0071 ACRE-FEET
PEAK DISCHARGE RATE = 0.26 CFS AT 1.533 HOURS BASIN AREA = 0.0001 SQ. MI.

```

*S BASIN 03

```

COMPUTE NM HYD      ID=33  HYD NO=03  DA=0.000469 SQ MI
                    %A=0  %B=22  %C=0  %D=78
                    TP=-0.1333 HR
                    MASS RAINFALL=-1
*****WARNING***** SUM OF TREATMENT TYPES DOES NOT EQUAL 100 PERCENT OR TOTAL AREA
                    INPUT OF MASS RAINFALL WITH DT = 0.133300 HR.
K = 42.510002HR      TP = 78.000000HR      K/TP RATIO = 0.545000      SHAPE CONSTANT, N = 7.106428
UNIT PEAK = 0.00000CFS      UNIT VOLUME = NaN      B = 526.28      P60 = 1.0000
AREA = 0.000000 SQ MI      IA = 0.10000 INCHES      INF = 0.04000 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.133300

```

```

K = 64.665985HR      TP = 78.000000HR      K/TP RATIO = 0.829051      SHAPE CONSTANT, N = 4.303975
UNIT PEAK = 0.00000CFS      UNIT VOLUME = NaN      B = 374.95      P60 = 1.0000
AREA = 0.000000 SQ MI      IA = 0.35001 INCHES      INF = 0.83002 INCHES PER HOUR
RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.133300

```

```

PRINT HYD          ID=33 CODE=1

```

HYDROGRAPH FROM AREA 03

```

RUNOFF VOLUME = NaN INCHES = NaN ACRE-FEET
PEAK DISCHARGE RATE = 0.00 CFS AT -0.133 HOURS BASIN AREA = 0.0000 SQ. MI.

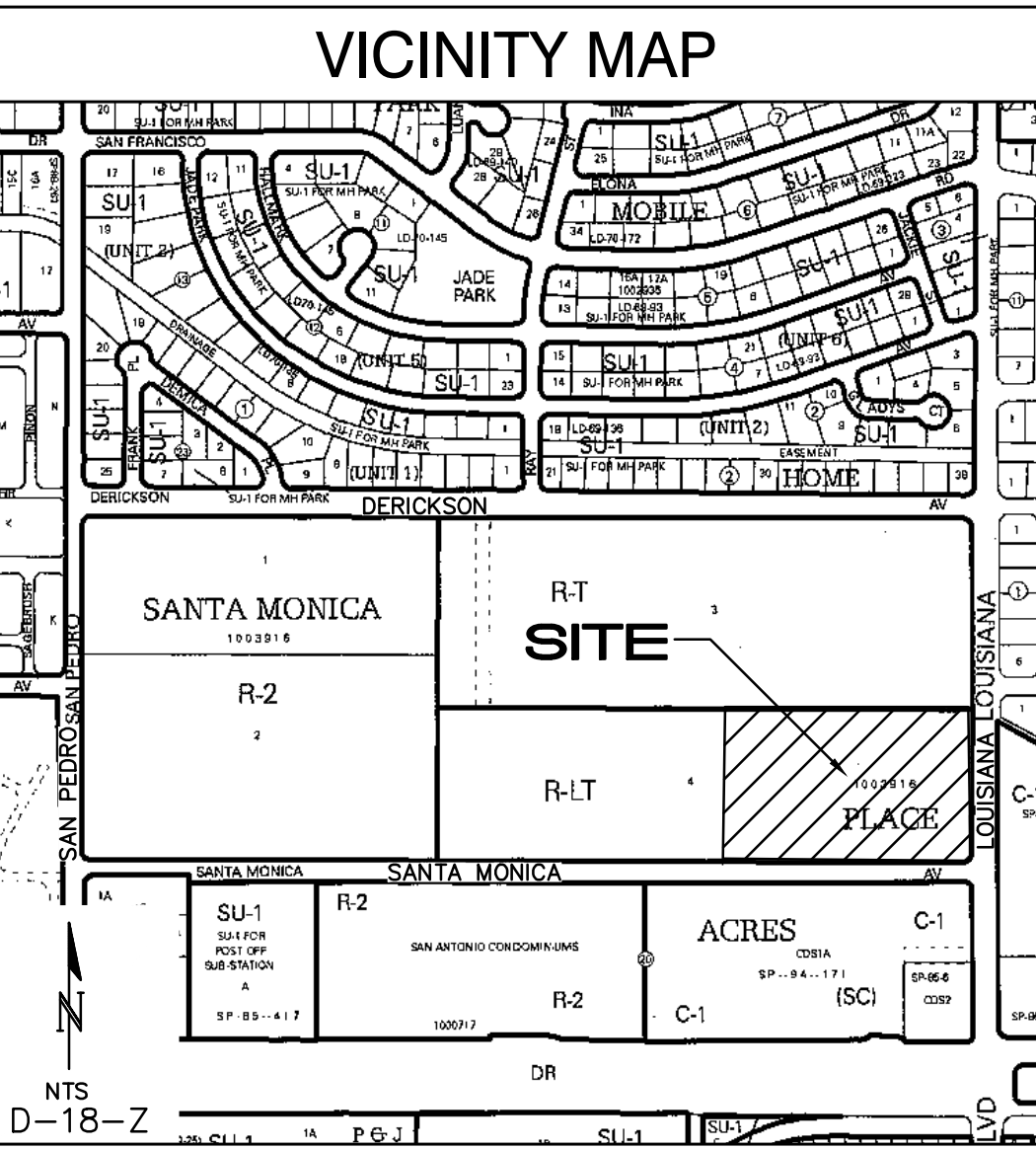
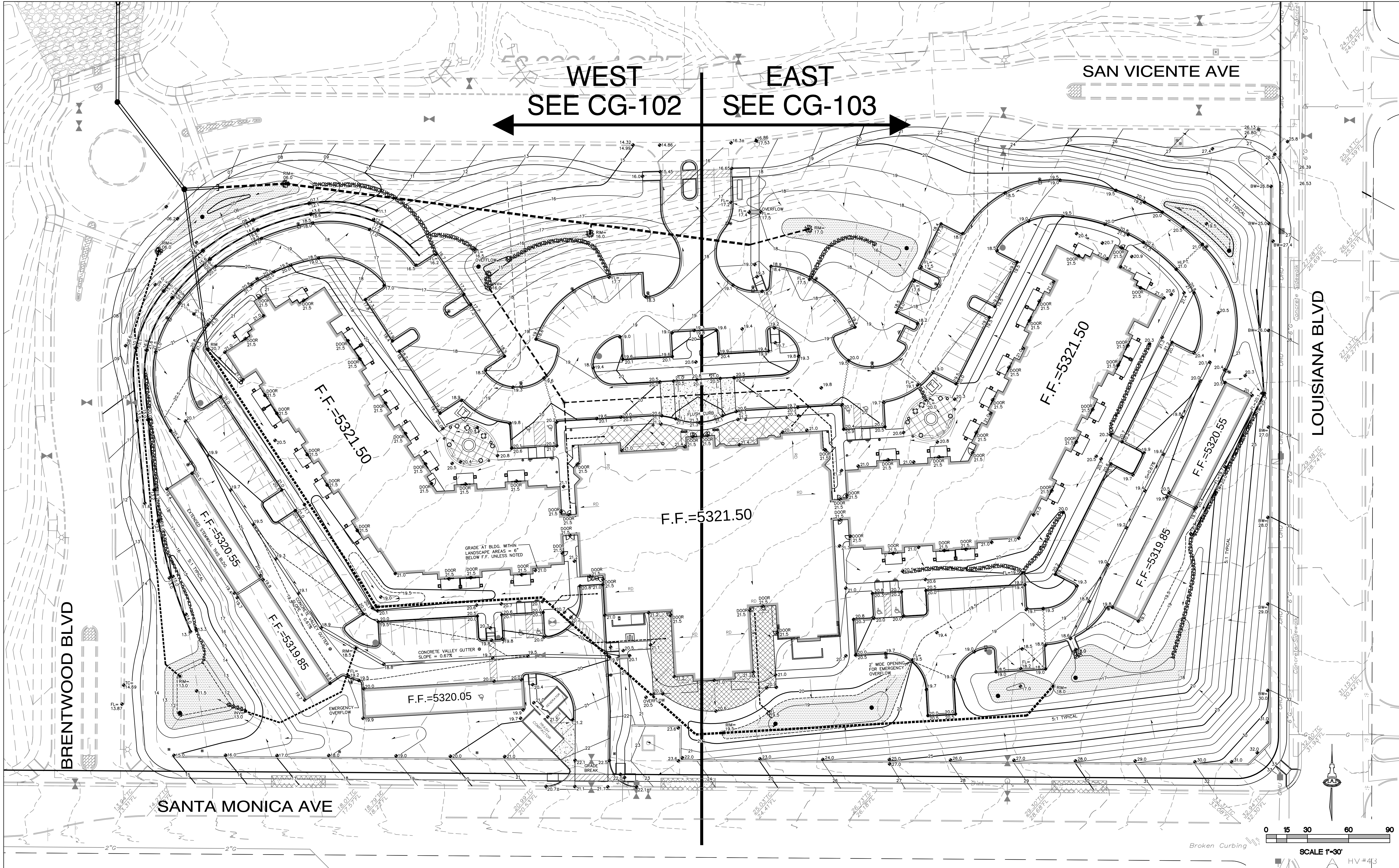
```

FINISH

```

NORMAL PROGRAM FINISH      END TIME (HR:MIN:SEC) = 14:59:18

```



PROJECT DATA

PROPERTY: THE SITE IS A PREVIOUSLY DEVELOPED MOBILE HOME PROPERTY LOCATED WITHIN C.O.A. VICINITY MAP D-18. THE SITE IS BOUND TO THE SOUTH BY SANTA MONICA AVE, NE, TO THE WEST BY APARTMENTS (TRACT 1), TO THE EAST BY LOUISIANA BLVD, AND TO THE NORTH BY UNDEVELOPED PROPERTY (TRACT 3).

PROPOSED IMPROVEMENTS: THE PROPOSED IMPROVEMENTS INCLUDE AN APPROXIMATELY 68,300 SF (FOOTPRINT) RETIREMENT COMMUNITY WITH THREE GARAGE PARKING BUILDINGS, ASSOCIATED ASPHALT PAVED DRIVES, PARKING, PEDESTRIAN WALKS AND LANDSCAPING.

EXISTING LEGAL: THE EASTERN PORTION OF TRACT 4, SANTA MONICA PLACE, ALBUQUERQUE, NM

PROPOSED LEGAL: TRACT 4-B, SANTA MONICA PLACE, ALBUQUERQUE, NM

AREA: 8.6± ACRES

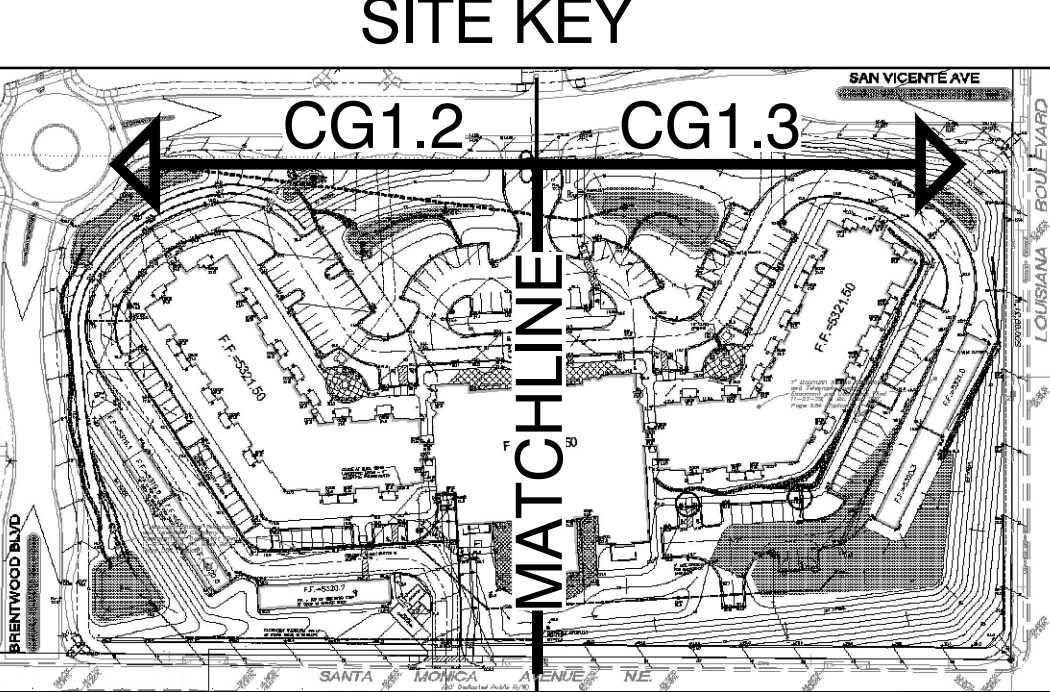
BENCHMARK: VERTICAL DATUM IS BASED UPON THE ALBUQUERQUE CONTROL SURVEY BENCHMARK "18-E18", ELEVATION = 5289.166 (NGVD88)

OFF-SITE: NO OFF-SITE DRAINAGE IMPACTS THIS PROPERTY.

FLOOD HAZARD: THE SUBJECT PROPERTY LIES WITHIN ZONE "X" (AREAS DETERMINED TO BE OUTSIDE 0.2% ANNUAL CHANCE FLOOD PLAIN) IN ACCORDANCE WITH THE NATIONAL FLOOD INSURANCE PROGRAM RATE MAP NO. 35001C0137 F, EFFECTIVE DATE 11-19-03.

SURVEYOR: RUSS P. HUGG, SURV-TEK, INC., (505)897-3366, ALBUQUERQUE, NEW MEXICO.

- GENERAL NOTES**
- A. ALL WORK DETAILED ON THESE PLANS AND PERFORMED UNDER THIS CONTRACT SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE PROJECT GEOTECHNICAL REPORT. WHERE APPLICABLE, CITY OF ALBUQUERQUE AND NMDOT STANDARDS APPLY.
- B. THE CONTRACTOR SHALL ABIDE BY ALL STATE, LOCAL, AND FEDERAL LAWS, CODES, RULES AND REGULATIONS WHICH APPLY TO THE CONSTRUCTION OF THESE IMPROVEMENTS, INCLUDING EPA AND ADA REQUIREMENTS.
- C. ALL SUBGRADE, OVEREXCAVATION, BACKFILL, AND FILL SHALL BE PLACED AND / OR COMPACTED PER THE GEOTECHNICAL REPORT.
- D. THE CONTRACTOR SHALL OBTAIN ALL REQUIRED PERMITS FOR THE PROJECT PRIOR TO COMMENCING CONSTRUCTION, OR PRIOR TO OCCUPANCY, AS APPROPRIATE. IF PERMITS ARE DELAYED OR ISSUED WITH CONDITIONS, THE CONTRACTOR SHALL NOTIFY THE OWNER AND ARCHITECT IMMEDIATELY.
- E. COORDINATE WORK WITH SITE PLAN, UTILITY PLAN, DEMOLITION PLAN, AND LANDSCAPE PLAN.
- F. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY HORIZONTAL AND VERTICAL LOCATIONS OF ALL EXISTING INFRASTRUCTURE PRIOR TO CONSTRUCTION. REPORT ALL DISCREPANCIES TO THE ARCHITECT AND VERIFY THE ARCHITECT'S INTENT BEFORE PROCEEDING.
- G. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR SITE SAFETY.
- H. THE CONTRACTOR SHALL MAINTAIN RECORD DRAWINGS ON SITE AT ALL TIMES. THE CONTRACTOR SHALL NOT SCALE DRAWINGS. ONLY WRITTEN DIMENSIONS OR KEYED NOTES SHALL BE USED.
- I. CONTRACTOR SHALL OBTAIN ALL REQUIRED INSPECTIONS OF THE WORK. CONTRACTOR SHALL REGULARLY UPDATE OWNER AND ARCHITECT REGARDING THE STATUS OF THE INSPECTIONS.
- J. CONSTRUCTION ACTIVITY SHALL BE LIMITED TO THE PROPERTY AND/OR PROJECT LIMITS. ANY DAMAGE TO ADJACENT STRUCTURES RESULTING FROM THE CONSTRUCTION PROCESS SHALL BE REPAIRED OR REPLACED AT THE CONTRACTOR'S EXPENSE. CONTRACTOR SHALL BE RESPONSIBLE FOR DOCUMENTING EXISTING CONDITIONS PRIOR TO CONSTRUCTION.
- K. CONSTRUCTION EQUIPMENT SHALL ONLY OBSTRUCT DESIGNATED TRAFFIC LANES IF APPROPRIATE BARRICADING PERMITS HAVE BEEN OBTAINED. THE CONTRACTOR SHALL NOT STORE ANY EQUIPMENT OR MATERIAL IN THE RIGHT-OF-WAY.
- L. THE CONTRACTOR SHALL PROVIDE A CONSTRUCTION TRAFFIC CONTROL AND SIGNING PLAN THAT CONFORMS TO THE LATEST EDITION OF THE "MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES" (MUTCD) AND LOCAL REQUIREMENTS. THE CONTRACTOR SHALL OBTAIN BARRICADING PERMITS FROM THE APPROPRIATE AUTHORITIES PRIOR TO ANY CONSTRUCTION WORK ON OR ADJACENT TO EXISTING STREETS.
- M. THE CONTRACTOR SHALL MAINTAIN ALL BARRICADING AND CONSTRUCTION SIGNING AT ALL TIMES. THE CONTRACTOR SHALL VERIFY THE PROPER LOCATION OF ALL BARRICADING AT THE END AND BEGINNING OF EACH DAY.
- N. PAVEMENT GRADES IN MARKED HANDICAPPED PARKING AREAS SHALL NOT EXCEED 2.0% IN ANY DIRECTION. FOR ALL ACCESSIBLE ROUTES, MAXIMUM ALLOWABLE CROSS SLOPE IS 2.0% AND MAXIMUM LONGITUDINAL SLOPE WITHOUT RAMP IS 5.0% FOLLOW ALL ADA ACCESSIBILITY GUIDELINES OR CITY CODES, WHICHEVER IS MORE STRINGENT.
- O. ALL TRASH, DEBRIS, & SURFACE VEGETATION SHALL BE CLEARED AND LEGALLY DISPOSED OF OFFSITE.
- P. PROPOSED SPOT AND CONTOUR ELEVATIONS SHOWN REPRESENT TOP OF FINISH MATERIAL (I.E. TOP OF CONCRETE, TOP OF CONCRETE BUILDING PAD, TOP OF PAVEMENT MATERIAL, TOP OF LANDSCAPING MATERIAL, ETC.). CONTRACTOR SHALL GRADE, COMPACT SUBGRADE AND DETERMINE EARTHWORK ESTIMATES BASED ON ELEVATIONS SHOWN MINUS FINISH MATERIAL THICKNESSES.
- Q. IF FIELD GRADE ADJUSTMENTS ARE REQUIRED, THE CONTRACTOR SHALL NOTIFY THE ARCHITECT/ENGINEER.
- R. MAXIMUM SLOPES SHALL BE 4:1. MINIMUM SLOPES SHALL BE 1% UNLESS OTHERWISE NOTED.
- S. EXISTING UTILITY LINES ARE SHOWN IN AN APPROXIMATE MANNER ONLY AND MAY BE INCOMPLETE OR OBSOLETE. SUCH LINES MAY OR MAY NOT EXIST WHERE SHOWN OR NOT SHOWN. CONTRACTOR SHALL CONTACT NM-811 FOR UTILITY LINE SPOTS TWO WORKING DAYS PRIOR TO CONDUCTING SITE FIELD WORK. CONTRACTOR SHALL FIELD VERIFY AND LOCATE ALL UTILITIES PRIOR TO COMMENCEMENT OF ANY CONSTRUCTION. CONTRACTOR IS FULLY RESPONSIBLE FOR ANY AND ALL DAMAGE CAUSED BY ITS FAILURE TO LOCATE, IDENTIFY AND PRESERVE ANY AND ALL EXISTING UTILITIES, PIPELINES, AND UNDERGROUND UTILITY LINES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION OF NECESSARY DRY UTILITY ADJUSTMENTS.
- T. SOIL TESTING AND INSPECTION SERVICES DURING EARTHWORK OPERATIONS ARE REQUIRED. CONTRACTOR SHALL ALLOW TESTING LABS TO INSPECT AND APPROVE COMPACTED SUBGRADES, BACKFILL, AND FILL LAYERS BEFORE FURTHER CONSTRUCTION WORK IS DONE. SHOULD COMPACTION TESTS INDICATE INADEQUATE DENSITY, CONTRACTOR SHALL PROVIDE ADDITIONAL COMPACTION AND TESTING AT THE CONTRACTOR'S SOLE EXPENSE.
- U. CONTRACTOR SHALL PROVIDE ALL OTHER CONSTRUCTION STAKING. CONTRACTOR SHALL LOCATE AND PRESERVE ALL BOUNDARY CORNERS AND REPLACE ANY LOST OR DISTURBED CORNERS AT CONTRACTOR'S SOLE EXPENSE. PROPERTY CORNERS SHALL ONLY BE RESET BY A REGISTERED LAND SURVEYOR.
- V. A CURRENT STORMWATER CONTROL PERMIT, INCLUDING AN EROSION/SEDIMENT CONTROL PLAN (E.S.C.) FOR EROSION AND SEDIMENT CONTROL IS REQUIRED FOR ALL CONSTRUCTION, DEMOLITION, CLEARING, AND GRADING OPERATIONS THAT DISTURB THE SOIL ON ONE ACRE OR MORE OF LAND. OWNER WILL COORDINATE.
- W. POST-CONSTRUCTION MAINTENANCE FOR PRIVATE STORMWATER FACILITIES WILL BE THE RESPONSIBILITY OF THE FACILITIES OWNER. PERIODIC INSPECTION AND CERTIFICATIONS OF THE FACILITIES MAY BE REQUIRED BY THE CITY ENGINEER.
- X. STORMWATER CONTROL MEASURES SHOWN ON THIS PLAN ARE REQUIRED TO PROVIDE MANAGEMENT OF "FIRST FLUSH" (CURRENTLY CALCULATED AS 0.34" OF STORMWATER MULTIPLIED BY THE IMPERMEABLE AREA).
- Y. ADJUST RIMS OF EXISTING UTILITY FEATURES AS NECESSARY TO MATCH NEW GRADES. UTILITIES IN PAVED AREAS SHALL BE HS-25 TRAFFIC RATED.
- Z. ALL NEW PAVEMENT SURFACES SHALL BE CONSTRUCTED WITH POSITIVE SLOPE AWAY FROM BUILDINGS AND POSITIVE SLOPE TOWARD EXISTING AND/OR PROPOSED DRAINAGE PATHS. PAVING AND ROADWAY GRADES SHALL BE ±0.1' FROM PLAN ELEVATIONS. BUILDING PAD ELEVATION SHALL BE ±0.05' FROM PLAN ELEVATION.
- AA. WHERE GRADES BETWEEN NEW AND EXISTING ARE SHOWN AS 'MATCH' OR '±', TRANSITIONS SHALL BE SMOOTH.
- AB. ALL EROSION PROTECTION TO BE FRACTURED FACE ROCK (F.F. ROCK) = 6" AVG. DIA. ANGULAR FACED ROCK PLACED OVER GEOTEX 501 NON-WOVEN GEOTEXTILE (O.E.).
- AC. SLOPES STEEPER THAN 4:1 BUT LESS THAN 2:1 MUST HAVE PERMANENT EROSION CONTROL (F.F. ROCK O.E.) INSTALLED, TYPICAL. NO SLOPE SHALL BE STEEPER THAN 2:1.
- AD. CONTRACTOR SHALL COMPLY WITH LOCAL REGULATIONS FOR RESEEDING OF DISTURBED AREAS.
- AE. POND DESIGN PARAMETERS (TOP OF POND, BOTTOM OF POND, SIZE OF ORIFICE, AREA OF POND, ETC.) TO BE STRICTLY ADHERED TO FOR CERTIFICATION PURPOSES. SEE DETAIL SHEET FOR ADDITIONAL INFORMATION.
- AF. ENGINEER RECOMMENDS THAT OWNER MAINTAIN EROSION PROTECTION ELEMENTS. ENGINEER RECOMMENDS THAT OWNER INSPECT SITE YEARLY AND AFTER EACH RAINFALL TO IDENTIFY NEW AREAS OF EROSION AND INSTALL ADDITIONAL EROSION PROTECTION AS NEEDED BASED ON ACTUAL OCCURRENCES.
- AG. GRADING SHALL BE PERFORMED AT THE ELEVATIONS AND IN ACCORDANCE WITH THE DETAILS SHOWN ON THIS PLAN.
- AH. MEASURES REQUIRED FOR EROSION AND SEDIMENT CONTROL SHALL BE INCIDENTAL TO THE PROJECT COST.
- AI. ALL SITE PREPARATION, GRADING OPERATIONS, FOUNDATION CONSTRUCTION, AND PAVEMENT INSTALLATION WORK SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE GEOTECHNICAL REPORT, WHICH WILL BE PROVIDED BY THE OWNER OR ARCHITECT. ALL OTHER WORK SHALL, UNLESS OTHERWISE NOTED IN THE PLANS, BE CONSTRUCTED IN ACCORDANCE WITH THE PROJECT SPECIFICATION (FIRST PRIORITY), AND/OR NMDOT STANDARD SPECIFICATIONS FOR PUBLIC WORK (SECOND PRIORITY).



ISAACSON & ARFMAN, P.A.
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Albuquerque, New Mexico 87108
Ph. 505-268-8838 www.isaacson.com

2051 CG-101.dwg Nov 20, 2014

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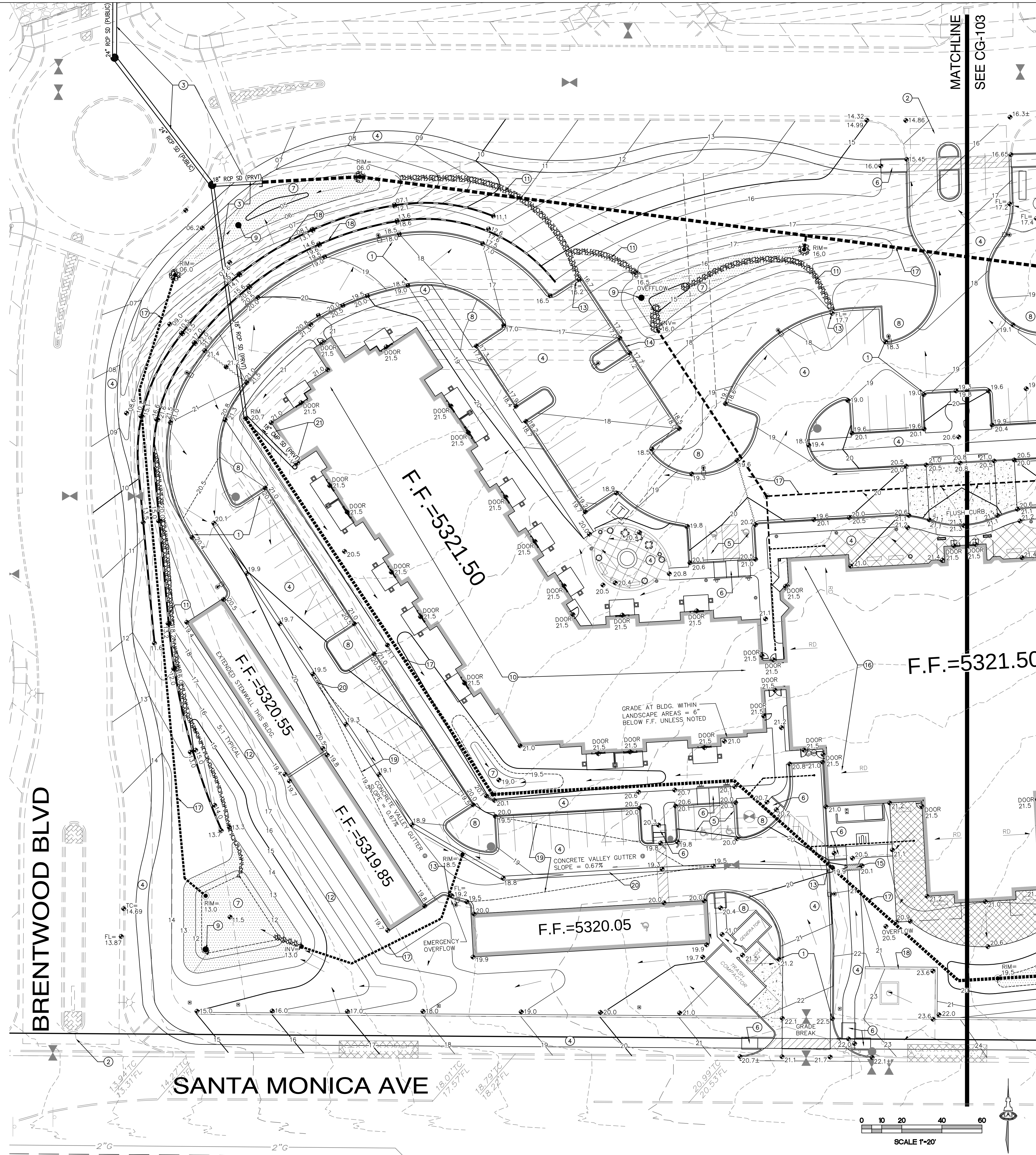
Coronado Villa Retirement Community

CAMERON GENERAL CONTRACTORS

OVERALL GRADING & DRAINAGE PLAN

Date:	No.:	Revision:	Date:	Job No.:
9/10/14				2051
Drawn By:				CG-101
Chk By:				SH OF





KEYED NOTES

THESE NOTES ARE REFERENCED ON SHEETS CG-102 AND CG-103. NOT ALL NOTES ARE USED ON EACH SHEET.

- SPOT ELEVATION LABELS WITHIN GUTTER AREA REPRESENT FLOWLINE UNLESS NOTED. ADD 0.5' TYPICAL FOR TOP OF CURB / TOP OF ADJACENT WALK ELEVATIONS.
- SEE PUBLIC WORK ORDER DRAWINGS FOR CONSTRUCTION OF NEW ACCESS DRIVES WITH CONCRETE VALLEY GUTTER AND RAMPS. SEE SHEET CP-103 FOR SIDEWALK GRADES AND TYPICAL SECTIONS FOR PERIMETER SIDEWALKS ALONG PUBLIC STREETS.
- SEE PUBLIC WORK ORDER DRAWINGS FOR CONSTRUCTION OF STORM DRAIN SYSTEM THIS AREA.
- CONSTRUCT PAVING, CURB & GUTTER, AND WALKS AT ELEVATIONS SHOWN. SEE PAVING PLAN, PAVING DETAILS AND ARCHITECTURAL SITE DETAILS FOR ADDITIONAL INFORMATION. NOTE THAT PAVEMENT SLOPES AND CROSS-SLOPES VARY THROUGHOUT TO ACHIEVE GRADES NECESSARY TO ACHIEVE PEDESTRIAN ACCESS, STREET STORMWATER CAPACITIES, PIPE COVERAGE, ETC.
- SLOPES WITHIN HANDICAP PARKING AREAS TO MEET ADA REQUIREMENTS. MAX. SLOPE = 2% IN ANY DIRECTION.
- CONSTRUCT HANDICAP ACCESS RAMP TO ADA STANDARDS. SEE SHEET CP-501 FOR DETAILS.
- CONSTRUCT RETENTION POND TO ELEVATIONS SHOWN TO CAPTURE FIRST FLUSH RUNOFF.
- DEPRESS LANDSCAPING. NOTE: DO NOT DEPRESS LANDSCAPING WITHIN 10' OF ANY STRUCTURE.
- CONSTRUCT PERCOLATION PIT. SEE DETAIL SHEET CG-501.
- BUILDING ROOF DISCHARGE SHALL BE RELEASED TO ALL SIDES.
- CONSTRUCT DRAINAGE SWALE WITH EROSION PROTECTION INTEGRATED WITH LANDSCAPING THIS AREA. SEE DETAIL SHEET CG-501.
- SLOPE AT 4:1 MAX. (5:1 TYPICAL).
- PROVIDE 2' WIDE OPENING IN CURB TO PASS FLOW.
- 1' WIDE (BOTTOM WIDTH) 'U' SHAPED CONCRETE CHANNEL THROUGH PARKING ISLAND TO PASS FLOW.
- CONSTRUCT 18" WIDE (BOTTOM WIDTH) COVERED SIDEWALK CULVERT PER DETAIL ON SHEET CG-501.
- BUILDING ROOF DISCHARGE SHALL BE PIPED TO STORM DRAIN.
- CONSTRUCT PRIVATE STORM DRAIN SYSTEM. SEE SHEET CG-501 FOR SIZES / SLOPES / INLET INFORMATION / MATERIALS.
- CONSTRUCT RETAINING WALL (MAX. 5' RETAINING) TO ACHIEVE GRADE DIFFERENCE THIS AREA. STRUCTURAL / WEEPHOLE DESIGN BY OTHERS.
- 0.5' CONTOURS ARE PROVIDED THIS AREA TO CLARIFY DRAINAGE CONCEPT.
- CONSTRUCT 2' WIDE CONCRETE ALLEY GUTTER AT ELEVATIONS SHOWN.
- REMOVE & DISPOSE 18" CMP PIPE AND STANDPIPE INSTALLED WITH PUBLIC WORK ORDER.
- CONSTRUCT PCC RUNDOWN PER DETAIL ON SHEET CG-501.

LEGEND

	79	PROPOSED CONTOUR - 1' INCREMENT
	75.5	PROPOSED CONTOUR - 0.5' INCREMENT
	78.3	PROPOSED SPOT ELEVATION
		FLOW ARROW
	FF=XXXX.XX	FINISH FLOOR ELEVATION
	78.3±	EXISTING ELEVATION (±) TO MATCH. PROVIDE SMOOTH TRANSITION.
		ROCK EROSION CONTROL
		GRADE BREAK
		PROPOSED STORM DRAIN (SEE CG5.1)
	FL=	FLOWLINE ELEVATION
	INV=	INVERT ELEVATION
		RETAINING WALL
		'FIRST FLUSH' RETENTION POND

SITE KEY

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2051 CG-101.dwg Nov 20, 2014

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Coronado Villa Retirement Community

CAMERON GENERAL CONTRACTORS

GRADING & DRAINAGE PLAN - WEST

Date:	9/10/14	No.:	Revision:	Date:	Job No.:
Drawn By:					2051
Chk By:					CG-102
FCA					SH. OF



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KEYED NOTES

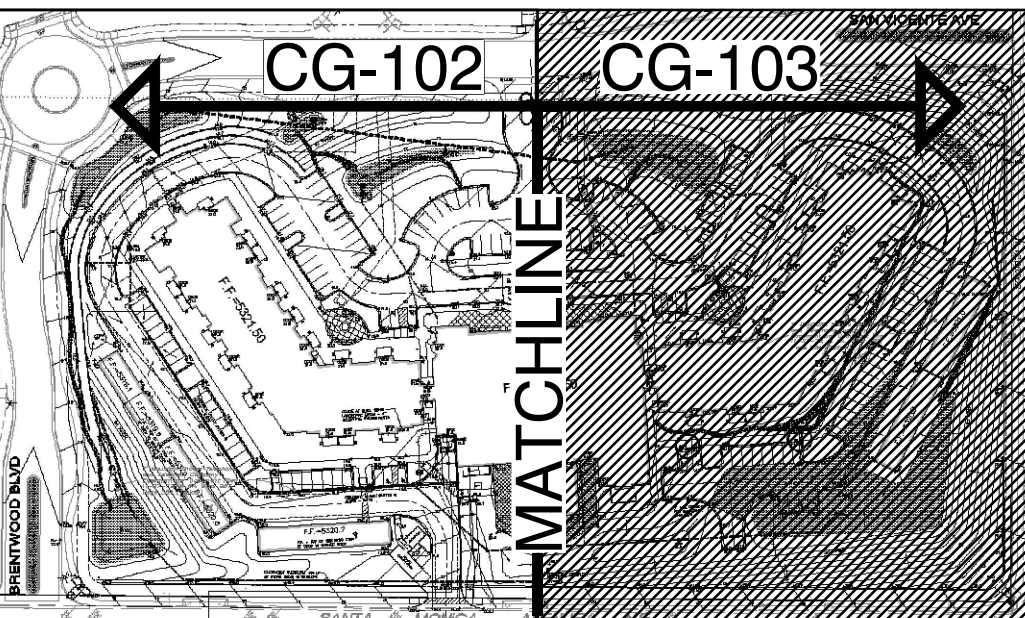
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- PROPOSED STORM DRAIN (SEE CG5.1)
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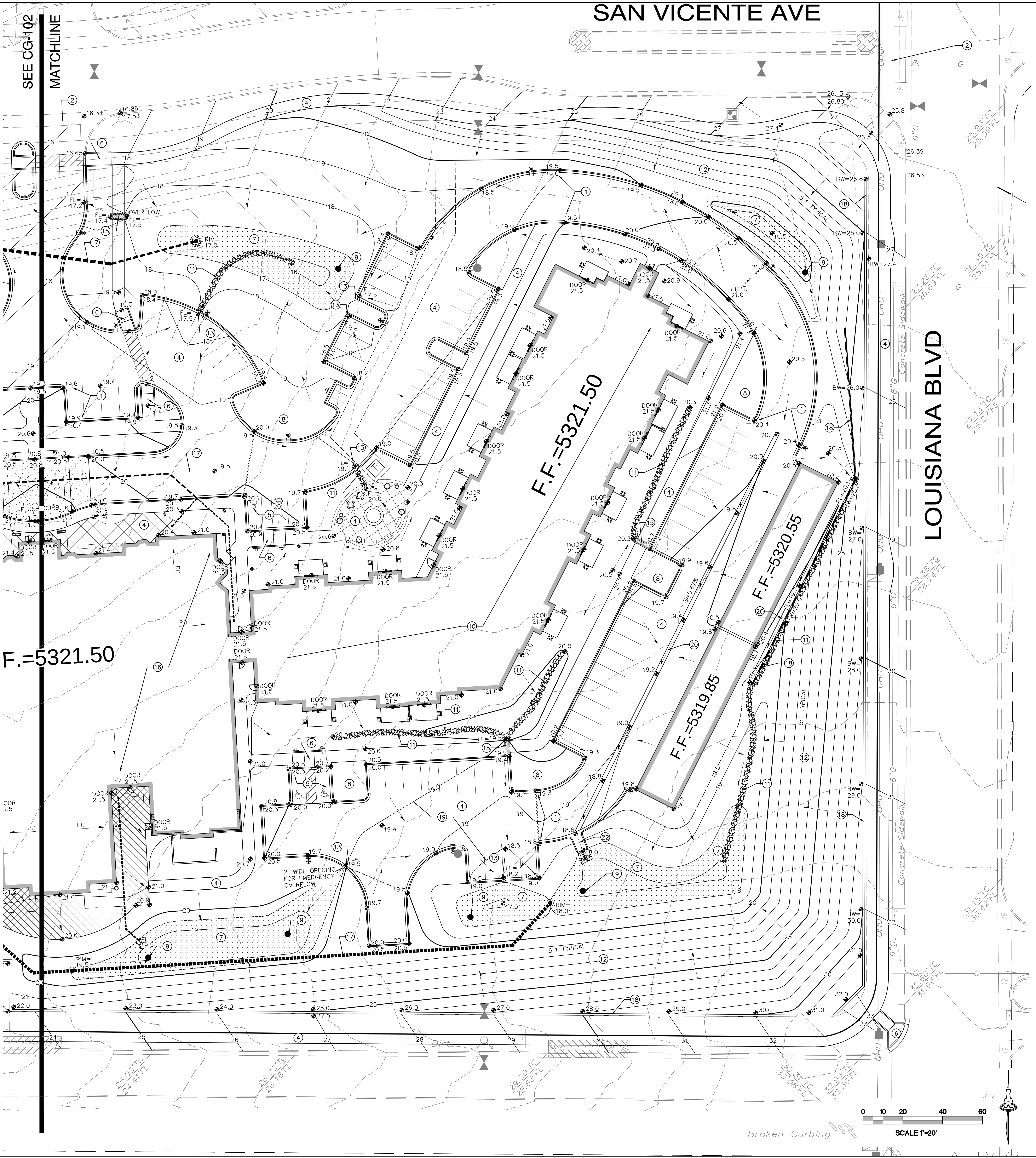
2051 CG-101.dwg Nov 20,2014

Coronado Villa Retirement Community

CAMERON GENERAL CONTRACTORS

GRADING & DRAINAGE PLAN - EAST

Date:	No.:	Revision:	Date:	Job No.:
9/10/14				2051
Drawn By:				CG-103
Ckd By:	FCA			SH. OF



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