CITY OF ALBUQUE ROUE PLANNING DEPARTMENT – Development Review Services



Richard J. Berry, Mayor

September 24, 2014

Fred C. Arfman, P.E. Isaacson & Arfman, P.A. 128 Monroe St NE Albuquerque, NM 87108

RE: Morningstar at Palomas Grading and Drainage Plan with Supplemental Drainage Calculations Engineer's Stamp Date (9-5-14) File: D19D029

Dear Mr. Arfman:

Based upon the information provided in your submittal received 9-8-14, the above referenced plan cannot be approved for Building Permit until the following comments are addressed: 1. Calculations of NE Pond Outlet pipe to Paseo Del Norte use a 4" dia. pipe to restrict flow to 0.7 cfs, using a 3' head (pg.8). However, Plan Sheet CG-501 show a 8"dia. pipe, and the MH#7 detail shows a 12"dia pipe. Also, invert elevation (2425.52) and PO Box 1293 Pond WSEL elevation (2431') indicate a head of 5.3' should be used instead. Since 4" pipe is already pretty small, and head is already over, how can you meet the 0.7 max. cfs. Albuquerque 2. It appears you are grading on NMDOT ROW. I understand you had preliminary approval from the NMDOT for DRB approval. Please provide acceptance of grading and drainage of the new plan from NMDOT. Be sure that the approval letter includes the Engineer's stamp date of the approved plan. New Mexico 87103 3. Sheet CG-102, at the sidewalk behind the trash enclosure, the grade falls at more than a 2:1 slope (from 32' contour to 30.7 T.O. SW). At end of SW, the grade gets higher right before the water harvest pond. The inlet should be in a sump condition www.cabq.gov so that runoff does not bypass inlet and flow into Basin 10. 4. Along the same note, it seems that another roof drain is needed on the SW corner of the building so that all of Basin 9 (roof) does not discharge to Basin 10 and ultimately NMDOT ROW. 5. A SW culvert is needed at the private pedestrian walkway where it connects to the public sidewalk, allowing runoff to flow directly to pond. 6. On major ponds in NE, NW, and SW corners, label the WSEL, Pond Volume, and Emergency Overflow. 7. In the PROJECT DATA summary, the off-site flow is prevented by plugging up openings in adjacent wall. Show location and work to be done on the plans. 8. Provide pond calculations and hydrograph for pond in SW corner. It seems that the curb cut discharge should be based on the weir equation since it is at same elevation

as the top of pond. Discharge from these curb cuts appears to flow into sidewalk ramp on opposite side of curb return.

9. Provide street capacity calculations of Palomas for the 4.4cfs discharge.

Please attach a copy of this approved plan in the construction sets when submitting for a building permit.

Since the disturbed area on this site exceeds 1.0 acre, an Erosion and Sediment Control (ESC) Plan, prepared by a NM PE and approved by the City's Stormwater Engineer, will be required for this site, prior to Hydrology approval of a Building Permit or Work Order.

If you have any questions, you can contact me at 924-3695.

Sincerely,

Rita Harmon, P.E. Senior Engineer, Planning Dept. Development Review Services

Orig: Drainage file c.pdf: via Email: Recipient SEPTEMBER 5, 2014

SUPPLEMENTAL INFORMATION

for

MORNINGSTAR of ALBUQUERQUE

GRADING AND DRAINAGE PLAN

by





TABLE OF CONTENTS

| Project Information1 |
|--|
| Historic / Developed Calculations2 |
| Drainage Basin Map |
| Drainage Basin Calculations4-5 |
| Allowable Discharge To Paseo Del Norte R.O.W |
| Ne Detention Pond Calculations7 |
| Northeast Pond Outlet to Paseo del Norte Storm Drain |
| Northwest Pond Outlet to Paseo del Norte 'V' Ditch |
| North Side Storm Drain Analysis to NMDOT Storm Sewer |
| Allowable Discharge to Palomas Ave. NE14 |
| South Side Storm Drain Analysis to SW Pond and Palomas Ave 15-18 |
| Grate Capacity Charts |

PROJECT INFORMATION

<u>PROPERTY</u>: The site is an undeveloped 2.3 acre property (to be replatted into a single lot) located within C.O.A. Vicinity Map D-19. The site is bound to the east by developed commercial, to the west by a 0.9± acre undeveloped property (to be created as part of replat), to the north by Paseo Del Norte Blvd. R.O.W. and to the south by Palomas Blvd.

<u>PROPOSED IMPROVEMENTS</u>: the proposed improvements include an assisted living facility with associated asphalt paved access, parking and landscaping.

<u>LEGAL</u>: Portions of Lots 25, 26 and 27, 6, 7 And 8, Block 21 Tract A, Unit A, North Albuquerque Acres, Albuquerque, Nm

<u>BENCHMARK</u>: Vertical datum is based upon Albuquerque control survey monument "heaven", elevation = 5378.235 feet (NAVD 88).

<u>OFF-SITE</u>: No off-site drainage will impact this property. Existing ungrouted joints between blocks and small diameter pipes in existing adjacent property wall at NE end of property will be plugged to prevent discharge into this property.

<u>FLOOD HAZARD</u>: per Bernalillo County Firm Map #35001c0141G, the site is located within Floodzone 'x' designated as areas determined to be outside 500-year floodplain.

DRAINAGE PLAN CONCEPT: Based on the <u>NORTH AND SOUTH DOMINGO BACA ARROYOS AND PASEO</u> <u>DEL NORTE (PDN) CORRIDOR DRAINAGE MANAGEMENT PLAN</u> prepared by Resource Technology, Inc. (1991) 100% of the site historically drains to PDN. In the developed condition, the site is permitted to continue to release historic rates to PDN either as surface flow or with a new storm drain connection to the existing public storm drain inlet within the PDN R.O.W. discharge to Palomas Ave. Is unrestricted. Detention pond(s) will be constructed along the north end of the property to control discharge at approved rates.

| CALCULATIONS: 2033 - Palomas Assisted Living Facility : 09/02/2014 | | | | | | | | | |
|--|--|---------------------|--------------------------------|--|------------------|-----------------------|-----|--------------------|---|
| Based on Drainag | Based on Drainage Design Criteria for City of Albuquerque Section 22.2, DPM, Vol 2, dated Jan., 1993 | | | | | | | | |
| | | | | ON-SIT | E | | | | _ |
| AREA OF SITE: | | | | 101312 | SF | = | 2.3 | | |
| | | | | 100-year, 6-hour | | | | | |
| HISTORIC FLO | OWS: | | | DEVELOPED FLC | OWS: | | | EXCESS PRECIP: | |
| | | Treatment SF | % | | | Treatment SF | % | Precip. Zone 3 | 3 |
| A rea A | = | 50656 | 50% | Area A | = | 0 | 0% | $E_{A} = 0.66$ | |
| Area B | = | 50656 | 50% | A rea B | = | 10131 | 10% | $E_{\rm B} = 0.92$ | |
| Area C | = | 0 | 0% | A rea C | = | 13171 | 13% | $E_{c} = 1.29$ | |
| A rea D | = | 0 | 0% | Area D | = | 78010 | 77% | $E_{\rm D} = 2.36$ | |
| Total Area | = | 101312 | | , Total Area | = | 101312 | | , , | |
| | | | | | | | | | |
| On-Site Weighted | i Exces | s Precipitation (| 100-Ye | ar, 6-Hour Storm) | | | | | |
| | | Weighted E = | | $\underline{E}_{A}\underline{A}_{A} + \underline{E}_{B}\underline{A}_{B} + \underline{E}_{C}\underline{A}_{B}$ | $c + E_{D}$ | <u>A</u> _Đ | | | |
| | | | | $A_A + A_B + A_C$ | + A _D | | | | |
| Historic E | = | 0.79 | in | Developed E | = | 2.08 | in. |] | |
| | | | | | | | | - | |
| On-Site Volume | ofRun | off: V360 = | | E*A / 12 | | | | _ | |
| Historic V ₃₆₀ | = | 6670 | CF | Developed V ₃₆₀ | = | 17535 | CF |] | |
| | | | | | | | | | |
| On-Site Peak Dis | charge | Rate: $Qp = Q_{nA}$ | A _A +Q _p | $A_{B}+Q_{pC}A_{C}+Q_{pD}A_{D}$ | 43,560 | | | | |
| For Precipitation | Zone | 3 | | | | | | | |
| Q_{pA} | = | 1.87 | | Q _{pC} | = | 3.45 | | | |
| Q _{pB} | = | 2.60 | | Q _{nD} | = | 5.02 | | | |
| Historic Q _p | = | 5.2 | CFS | Developed Q _p | = | 10.6 | CFS |] | |
| - | | | | | | | | - | |

DRAINAGE BASINS



| BASIN NO. 1 | | | DESCRIPTION | | | To Palor | nas | |
|---------------------------|-------------------|----------|---------------------------|---------|-----------|-----------------|----------------|---|
| Area of basin flows = | 9260 | SF | | = | | 0.2 Ac. | | |
| The following calculation | ns are based on [| Freatme | ent areas as shown in ta | ible to | the right | LAND T | REATMENT | |
| | Sub-basin Weigl | nted Ex | cess Precipitation (see f | formul | a above) | A = | 0% | |
| | Weighted E | = | 1.73 in | L. | | B = | 25% | |
| | Sub-basin Volum | ie of Ri | moff (see formula above | e) | | C = | 25% | |
| | V360 | = | 1337 | CF | | D= | 50% | |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula ab | oove) | | | | |
| | Qp | = | 0.9 | cfs | | | | |
| BASIN NO. 2 | | | DESCRIPTION | | NE Dra | inage to Paseo | del Norte RO | W |
| Area of basin flows = | 9778 | SF | | = | | 0.2 Ac. | | |
| The following calculation | ns are based on [| Freatme | ent areas as shown in ta | ible to | the right | LAND T | REATMENT | |
| | Sub-basin Weigl | nted Ex | cess Precipitation (see f | formul | a above) | A = | 0% | |
| | Weighted E | = | 2.31 in | L. | | B = | 0% | |
| | Sub-basin Volun | ie of Ri | moff (see formula above | e) | | C = | 5% | |
| | V360 | = | 1879 | CF | | D= | 95% | |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula ab | oove) | | | | |
| | Qp | = | 1.1 | cfs | | | | |
| BASIN NO. 3 | | | DESCRIPTION | | NW Dr | ainage to Pased | o del Norte RC | W |
| Area of basin flows = | 3008 | SF | | = | | 0.1 Ac. | | |
| The following calculation | ns are based on ' | Freatme | ent areas as shown in ta | ible to | the right | LAND T | REATMENT | |
| | Sub-basin Weigl | nted Ex | cess Precipitation (see f | formul | a above) | A = | 0% | |
| | Weighted E | = | 1.48 in | | | B = | 35% | |
| | Sub-basin Volun | ie of Ri | unoff (see formula above | e) | | C = | 35% | |
| | V360 | = | 371 | CF | | D = | 30% | |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula ab | oove) | | | | |
| | Qp | = | 0.3 | cfs | | | | |
| BASIN NO. 4 | | | DESCRIPTION | | | | | |
| Area of basin flows = | 10360 | SF | | = | | 0.2 Ac. | | |
| The following calculation | ns are based on | Freatme | ent areas as shown in ta | ible to | the right | LAND T | REATMENT | |
| | Sub-basin Weigl | nted Ex | cess Precipitation (see f | formul | a above) | A = | 0% | |
| | Weighted E | = | 1.98 in | | | B = | 15% | |
| | Sub-basin Volun | e of Ru | unoff (see formula above | e) | | C = | 15% | |
| | V360 | = | 1712 | CF | | D= | 70% | |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula ab | oove) | | | | |
| | Qp | = | 1.1 | cfs | | | | |
| BASIN NO. 5 | | | DESCRIPTION | | | | | |
| Area of basin flows = | 13732 | SF | | = | | 0.3 Ac. | | |
| The following calculation | ns are based on ' | Freatme | ent areas as shown in ta | ible to | the right | LAND T | REATMENT | - |
| | Sub-basin Weigl | nted Ex | cess Precipitation (see f | formul | a above) | A = | 0% | |
| | Weighted E | = | 2.11 in | | | B = | 10% | |
| | Sub-basin Volum | ie of Ri | unoff (see formula above | e) | | C = | 10% | |
| | V360 | = | 2413 | CF | | D = | 80% | |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula ab | oove) | | | | |
| | Op | = | 1.5 | cfs | | | | |

| BASIN NO. 6 | | | DESCRIPTION | | |
|---------------------------|-------------------|----------|--------------------------------------|--------------|----------|
| Area of basin flows = | 11636 | SF | = | 0.3 Ac. | |
| The following calculation | ns are based on [| Freatme | nt areas as shown in table to the ri | right LAND T | REATMENT |
| | Sub-basin Weigl | nted Exc | cess Precipitation (see formula abo | ove) A = | 0% |
| | Weighted E | = | 2.20 in. | B = | 0% |
| | Sub-basin Volum | ue of Ru | noff (see formula above) | C = | 15% |
| | V360 | = | 2133 CF | D = | 85% |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula above) | | |
| | Qp | = | 1.3 cfs | | |
| BASIN NO. 7 | | | DESCRIPTION | | |
| Area of basin flows = | 2249 | SF | = | 0.1 Ac. | |
| The following calculation | ns are based on [| Freatme | nt areas as shown in table to the ri | right LAND T | REATMENT |
| | Sub-basin Weigl | nted Exc | cess Precipitation (see formula abo | ove) A = | 0% |
| | Weighted E | = | 1.50 in. | B= | 30% |
| | Sub-basin Volum | ue of Ru | noff (see formula above) | C = | 40% |
| | V360 | = | 281 CF | D = | 30% |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula above) | | |
| | Qp | = | 0.2 cfs | | |
| BASIN NO. 8 | | | DESCRIPTION | | |
| Area of basin flows = | 13986 | SF | = | 0.3 Ac. | |
| The following calculation | ns are based on [| Freatme | nt areas as shown in table to the ri | right LAND T | REATMENT |
| - | Sub-basin Weigh | nted Ex | cess Precipitation (see formula abo | ove) A= | 0% |
| | Weighted E | = | 2.11 in. | B= | 10% |
| | Sub-basin Volum | ie of Ru | noff (see formula above) | C = | 10% |
| | V360 | = | 2458 CF | D = | 80% |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula above) | | |
| | Qp | = | 1.5 cfs | | |
| BASIN NO. 9 | | | DESCRIPTION | | |
| Area of basin flows = | 8570 | SF | = | 0.2 Ac. | |
| The following calculation | ns are based on [| Freatme | nt areas as shown in table to the ri | right LAND T | REATMENT |
| | Sub-basin Weigl | nted Exc | cess Precipitation (see formula abo | ove) A = | 0% |
| | Weighted E | = | 2.25 in. | B = | 0% |
| | Sub-basin Volum | ue of Ru | noff (see formula above) | C = | 10% |
| | V360 | = | 1609 CF | D = | 90% |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula above) | | |
| | Qp | = | 1.0 cfs | | |
| BASIN NO. 10 | | | DESCRIPTION | | |
| Area of basin flows = | 17680 | SF | = | 0.4 Ac. | |
| The following calculation | ns are based on 7 | Freatme | nt areas as shown in table to the r | right LAND T | REATMENT |
| | Sub-basin Weigl | nted Exc | cess Precipitation (see formula abo | ove) A = | 0% |
| | Weighted E | = | 2.16 in. | B = | 10% |
| | Sub-basin Volum | ue of Ru | noff (see formula above) | C = | 5% |
| | V360 | = | 3186 CF | D = | 85% |
| | Sub-basin Peak I | Dischar | ge Rate: (see formula above) | | |
| | Qp | = | 1.9 cfs | | |

ALLOWABLE DISCHARGE tO PASEO DEL NORTE R.O.W.:

Per the approved Conceptual Grading and Drainage Plan for this property (D19/D029) submitted 05-18-14, and approved by COA Hydrology and NMDOT's Tim Trujillo, P.E., the proposed development will discharge 5.2 cfs to the Paseo del Norte R.O.W. (PDN).

The 5.2 cfs discharge to PDN will be sub-divided as follows – see drainage basin map.

- Basin 10 (1.9 cfs) will discharge via covered sidewalk culvert to the PDN 'v' ditch at the NW corner of the property using orifice control to limit the release rate to **1.5** cfs.
- **3.0** cfs (basin 5 and basin 8) will discharge to the NE on-site storm drain system. This private system will then be extended to the existing NMDOT storm drain inlet near the NE end of the property.
- 1.5 cfs (basin 6 and basin 7) basins will surface discharge to the proposed detention pond at the NE corner of the property which will pass the final allowable **0.7** cfs to the NE storm drain system.

Total discharge to PDN = 1.5 (west sidewalk culvert) + 3.0 (storm drain) + 0.7 (east pond inlet) = 5.2 cfs.

The northeast detention pond will collect the stormwater from basins 6 and 7 (total 1.5 cfs) and will release 0.7 cfs into the private storm drain extending to the PDN NMDOT storm drain system.

Per the inflow / outflow hydrograph below, the pond volume required for detention will be 1283 cf.

CALCULATIONS: 2033 - Palomas Assisted Living Facility : 09/02/2014 HYDROGRAPH FOR SMALL WATERSHED DPM SECTION 22-2 * PAGE A-13/14

Base time, t_{R} , for a small water shed hydrograph is, tB = (2.107 * E * A / Q_{P}) - (0.25 * A_{P} / A)

| tB = (2.107 *) | E * A / Qp) - | (0.25 * A _D / J | A) |
|----------------|------------------|----------------------------|--------|
| Where | E = | 2.08 | inches |
| | A = | 0.32 | acres |
| | A _D = | 0.24 | acres |
| | Q _p = | 1.47 | cfs |
| | | | |
| | t _B = | 0.76 | hours |

E is the excess precipitation in inches (from DPM TABLE A-8), Q_p is the peak flow, A_D is the area (acres) of treatment D, and A_T is the total area in acres. Using the time of concentration, t_c (hours), the time to peak in hours is:

 $t_p = (0.7 * tC) + ((1.6 - (A_p / A)) / 12) \\ Where t_c = 0.20 \text{ hours}$

 $t_p = 0.21$ hours

Continue the peak for 0.25 * A_D / A_T hours. When A_D is zero, the hydrograph will be triangular. When A_D is not zero, the hydrograph will be trapezoidal, see the graph below:



▶ 1283 CF OK

NORTHEAST POND OUTLET TO PASEO DEL NORTE STORM DRAIN:

Using the orifice equation for circular openings, a 4" diameter outlet pipe with 2.83' of head (based on an invert 3' below the inlet rim) will pass 0.7 cfs.

| Orifice Diameter | 4 | inches | 0.33 | feet | | | |
|-----------------------|-------|----------|---------------|--------------|---------------|----------|---------|
| Orifice Area | 12.57 | sq.in. | 0.09 | square feet | | | |
| | | | | | | | |
| Headwater Elevation | 3 | feet | 2.83 | Actual H to | centerline of | culvert | |
| | | | | | | | |
| С | 0.6 | | C values | Rounded | Sharp | Tube Out | Tube In |
| g | 32.2 | f/s^2 | | 0.98 | 0.61 | 0.80 | 0.51 |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| Q = C*A*((2*g*H)^0.5) | = | 0.72 cfs | for 4 in. dia | meter orific | | | |

Therefore, the storm drain inlet located within the east pond will be constructed with a 4" diameter drain pipe with a starting invert 1.5' below the pond bottom (for a total of 3' head when the pond is full).

NORTHWEST POND OUTLET TO PASEO DEL NORTE 'V' DITCH:

Using the orifice equation for rectangular openings, the proposed $18'' \times 6''$ covered sidewalk culvert will pass 1.8 cfs to the PDN 'v' ditch.

| | ORIFICE EQUATION - RECTANGULAR | | | | | | | | | |
|---------------------|--------------------------------|------|----------|--------------|--------------------|-------|-----------------------|---------|--|--|
| Rectangula | ar Area | 108 | sq.in. | 0.75 | sq.ft. | | | | | |
| | Width | 18 | in | 1.50 | ft | | | | | |
| | Height | 6 | in | 0.50 | ft | | | | | |
| Headwater Elevation | | 0.5 | feet | 0.25 | 0.25 Actual H to c | | centerline of culvert | | | |
| С | | 0.6 | | C values | Rounded | Sharp | Tube Out | Tube In | | |
| g | | 32.2 | f/s^2 | | 0.98 | 0.61 | 0.80 | 0.51 | | |
| | | | | | | | | | | |
| Q = C*A*((| 2*g*H)^0.5) | = | 1.83 cfs | for 0.75 sq. | ft. orifice | | | | | |

NORTH SIDE STORM DRAIN ANALYSIS TO NMDOT STORM SEWER



| Line No. | Defl Ang | Line Size | Line Type | Line Length | Line Slope | Junct Type | Known Q | n-val Pipe | Flow Rate | Capac Full | EGL Dn | EGL Up | Energy Loss | Crit Depth | Gnd/Rim El Dn | Gnd/Rim El Up | HGL Dn | HGL Up | Invert Dn | Invert Up | |
|-------------|--------------------------|--------------|--------------|----------------|---------------|---------------|------------|---------------|--------------|---------------|-----------|-----------|----------------|---------------|------------------|------------------|-----------|-----------|--------------|--------------|--|
| | (Deg) | (in) | | (ft) | (%) | | (cfs) | | (cfs) | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | |
| 1 | 45.338 | 12 | Cir | 60.000 | 1.30 | мн | 0.00 | 0.012 | 3.70 | 4.40 | 25.25 | 26.15 | 0.000 | 0.82 | 28.07 | 31.10 | 24.80 | 25.70 | 24.10 | 24.88 | |
| 2 | 45.103 | 12 | Cir | 16.100 | 1.30 | мн | 0.00 | 0.012 | 3.70 | 4.41 | 26.15 | 26.36 | 0.000 | 0.82 | 31.10 | 30.20 | 25.70 | 25.91 | 24.88 | 25.09 | |
| 3 | -0.121 | 12 | Cir | 22.500 | 1.29 | мн | 0.00 | 0.012 | 2.20 | 4.38 | 26.18 | 26.29 | 0.000 | 0.63 | 30.20 | 31.20 | 25.91 | 26.01 j | 25.09 | 25.38 | |
| 4 | 44.680 | 12 | Cir | 81.000 | 1.30 | мн | 0.70 | 0.012 | 2.20 | 4.39 | 26.29 | 27.34 | 0.000 | 0.63 | 31.20 | 32.20 | 26.01 | 27.06 | 25.38 | 26.43 | |
| 5 | 0.000 | 12 | Cir | 16.800 | 1.31 | мн | 0.20 | 0.012 | 1.50 | 4.41 | 27.27 | 27.38 | 0.000 | 0.52 | 32.20 | 32.20 | 27.06 | 27.17 j | 26.43 | 26.65 | |
| 6 | -90.000 | 8 | Cir | 14.300 | 1.33 | мн | 0.50 | 0.012 | 1.30 | 1.51 | 27.46 | 27.67 | 0.000 | 0.54 | 32.20 | 31.80 | 27.17 | 27.38 | 26.65 | 26.84 | |
| 7 | 0.000 | 8 | Cir | 12.200 | 1.31 | мн | 0.60 | 0.012 | 0.60 | 1.50 | 27.53 | 27.51 | 0.000 | 0.36 | 31.80 | 31.00 | 27.38 | 27.36 j | 26.84 | 27.00 | |
| 8 | 92.098 | 12 | Cir | 17.000 | 2.00 | мн | 0.00 | 0.012 | 1.50 | 5.46 | 26.12 | 26.16 | 0.000 | 0.52 | 30.20 | 31.00 | 25.91 | 25.95 j | 25.09 | 25.43 | |
| 9 | 0.000 | 12 | Cir | 41.400 | 2.00 | мн | 0.10 | 0.012 | 1.50 | 5.46 | 26.16 | 26.99 | 0.000 | 0.52 | 31.00 | 31.80 | 25.95 | 26.78 | 25.43 | 26.26 | |
| 10 | 0.000 | 12 | Cir | 43.200 | 1.99 | мн | 0.10 | 0.012 | 1.40 | 5.44 | 26.98 | 27.82 | 0.000 | 0.50 | 31.80 | 31.70 | 26.78 | 27.62 j | 26.26 | 27.12 | |
| 11 | 90.000 | 8 | Cir | 3.000 | 2.00 | мн | 0.20 | 0.012 | 0.20 | 1.85 | 27.45 | 27.18 | 0.000 | 0.21 | 31.80 | 31.70 | 27.38 | 27.11 | 26.84 | 26.90 | |
| 12 | -45.062 | 8 | Cir | 22.700 | 1.98 | мн | 0.00 | 0.012 | 1.10 | 1.84 | 27.86 | 28.31 | 0.000 | 0.50 | 31.70 | 32.20 | 27.62 | 28.07 j | 27.12 | 27.57 | |
| 13 | 0.000 | 8 | Cir | 10.000 | 2.00 | MH | 0.50 | 0.012 | 1.10 | 1.85 | 28.31 | 28.51 | 0.000 | 0.50 | 32.20 | 32.30 | 28.07 | 28.27 | 27.57 | 27.77 | |
| 14 | 44.952 | 8 | Cir | 35.500 | 2.00 | MH | 0.00 | 0.012 | 0.60 | 1.85 | 28.41 | 28.99 | 0.000 | 0.36 | 32.30 | 31.90 | 28.27 | 28.84 j | 27.77 | 28.48 | |
| 15 | -89.826 | 8 | Cir | 8.300 | 2.05 | МН | 0.60 | 0.012 | 0.60 | 1.87 | 28.99 | 29.16 | 0.000 | 0.36 | 31.90 | 31.70 | 28.84 | 29.01 | 28.48 | 28.65 | |
| 16 | -0.201 | 8 | Cir | 12.300 | 2.03 | MH | 0.20 | 0.012 | 0.20 | 1.87 | 27.69 | 27.65 | 0.000 | 0.21 | 31.70 | 31.50 | 27.62 | 27.58 | 27.12 | 27.37 | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| 2033 SI | D 1 | | | I | | | | I | | | | | | Number | of lines: 16 | | | Date: 9/5 | 6/2014 | | |
| NOTES | NOTES: ** Critical depth | | | | | | | | | | | | | | | | | | | | |

Storm Sewer Profile

Sta 0+00.00 - Outfall Gmd. El. 28.07 Inv. El. 24.10 In Sta 0+76.10 - Ln: 2 Rim EI. 30.20 Inv. EI. 25.09 Out Inv. EI. 25.09 In Sta 0+98.60 - Ln: 3 Rim EI. 31.20 Inv. EI. 25.38 Out Inv. EI. 25.38 In Sta 1+96.40 - Ln: 5 Rim EI. 32.20 Inv. EI. 26.65 Out Inv. EI. 26.65 In Sta 2+10.70 - Ln: 6 Rim EI. 31.80 Inv. EI. 26.84 In Inv. EI. 26.84 In Sta 0+60.00 - Ln: 1 Rim EI. 31.10 Inv. EI. 24.88 Out Inv. EI. 24.88 In Sta 1+79.60 - Ln: 4 Rim EI. 32.20 Inv. EI. 26.43 In Inv. EI. 26.43 In Sta 2+22.90 - Ln: 7 Rim EI. 31.00 Inv. EI. 27.00 Out Elev. (ft) 41.00 41.00 37.00 37.00 33.00 83.00 29.00 - 29.00 1 81.000Lf - 12" @ 1.30 25.00 2.200Lf - 8" @ 1.31% 25.00 60.0001 f - 12" @ 1.30% 14.300Lf - 8" @ 1.33% 16.800Lf - 12" @ 1.319 22.500Lf - 12" @ 1.29% 16.100Lf - 12" @ 1 30% 21.00 - 21.00 125 150 225 0 25 50 75 100 175 200 HGL----- EGL Reach (ft)

Storm Sewer Profile

Proj. file: 2033 SD.stm



ALLOWABLE DISCHARGE to PALOMAS AVE. NE:

Per the approved Master Drainage Plan, North and South Domingo drainage study (COA File D19/026) prepared by Tierra West, Palomas Ave has capacity to accept free discharge from this entire property based on land treatment percentages of 10% B, 20% C and 70% D = 10.4 cfs.

| Allowable discharge to Palomas Ave. | | | | | | | | |
|-------------------------------------|--------------------|----------------|--------------------------|-----------|---------|-----|--|--|
| Area of basin flows = | 101312 | SF | = | | 2.3 Ac. | | | |
| The following calculation | ons are based on T | reatment area | as as shown in table to | the right | LAND | | | |
| | Sub-basin Weigh | ted Excess Pr | recipitation (see formul | la above) | A = | 0% | | |
| | Weighted E | = | 2.00 in. | | B = | 10% | | |
| | Sub-basin Volum | e of Runoff (s | see formula above) | | C = | 20% | | |
| | V360 | = | 16902 CF | | D = | 70% | | |
| | Sub-basin Peak D | ischarge Rate | e: (see formula above) | | | | | |
| | Qp | = | 10.4 cfs | | | | | |

The total discharge to Palomas Ave. will consist of basins 1, 2, 3, 4 and 9 for a total of 4.4 cfs < 10.4 cfs. See drainage basin map.

Basin 1 will surface discharge to the water harvesting area at the southwest end of the property. Basins 2, 3, 4 and 9 will drain to the south side storm drain system and discharge to the bubble-up inlet in the water harvesting basin. Once the basin fills, excess flow will pass (free discharge) to Palomas Ave. via the proposed access drive curb cuts.



Three curb openings will each release 1.5 cfs for a total of 4.5 cfs < 4.4 cfs. OK

| ORIFICE EQUATION - RECTANGULAR | | | | | | | | | |
|--------------------------------|------|----------|---------------|--------------------|-------|-----------------------|---------|--|--|
| Rectangular Area | 90 | sq.in. | 0.63 | sq.ft. | | | | | |
| Width | 15 | in | 1.25 | ft | | | | | |
| Height | 6 | in | 0.50 | ft | | | | | |
| Headwater Elevation | 0.5 | feet | 0.25 | 0.25 Actual H to c | | centerline of culvert | | | |
| С | 0.6 | | C values | Rounded | Sharp | Tube Out | Tube In | | |
| g | 32.2 | f/s^2 | | 0.98 | 0.61 | 0.80 | 0.51 | | |
| | | | | | | | | | |
| Q = C*A*((2*g*H)^0.5) | = | 1.52 cfs | for 0.63 sq.1 | tt. orifice | | | | | |

SOUTH SIDE STORM DRAIN MAIN ANALYSIS TO SW POND OVERFLOWING TO PALOMAS AVE



Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan

| Line No. | Defl Ang | Line Size | Line Type | Line Length | Line Slope | Junct Type | Known Q | n-val Pipe | Flow Rate | Capac Full | EGL Dn | EGL Up | Energy Loss | Crit Depth | Gnd/Rim El Dn | Gnd/Rim El Up | HGL Dn | HGL Up | Invert Dn | Invert Up | |
|-------------|--------------------------|--------------|--------------|----------------|---------------|---------------|------------|---------------|--------------|---------------|-----------|-----------|----------------|---------------|------------------|------------------|-----------|-----------|--------------|--------------|--|
| | (Deg) | (in) | | (ft) | (%) | | (cfs) | | (cfs) | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft) | |
| 1 | 0.000 | 18 | Cir | 58.700 | 1.24 | MH | 0.00 | 0.012 | 3.50 | 12.69 | 5427.56 | 5427.62 | 0.056 | 0.71 | 5427.00 | 5430.50 | 5427.50 | 5427.56 | 5424.00 | 5424.73 | |
| 2 | 0.000 | 12 | Cir | 55.500 | 1.24 | MH | 1.00 | 0.012 | 3.50 | 4.30 | 5427.87 | 5428.33 | 0.457 | 0.80 | 5430.50 | 5430.40 | 5427.57 | 5428.02 | 5424.73 | 5425.42 | |
| 3 | 0.000 | 12 | Cir | 54.400 | 1.25 | None | 1.10 | 0.012 | 2.50 | 4.31 | 5428.23 | 5428.46 | 0.228 | 0.68 | 5430.40 | 5431.10 | 5428.07 | 5428.30 | 5425.42 | 5426.10 | |
| 4 | 0.000 | 8 | Cir | 74.300 | 1.24 | Grate | 1.10 | 0.012 | 1.40 | 1.46 | 5428.57 | 5429.42 | 0.851 | 0.56 | 5431.10 | 5432.40 | 5428.32 | 5429.17 | 5426.10 | 5427.02 | |
| 5 | -45.000 | 8 | Cir | 36.300 | 1.24 | Grate | 0.00 | 0.012 | 0.30 | 1.46 | 5429.47 | 5429.49 | 0.019 | 0.25 | 5432.40 | 5433.70 | 5429.46 | 5429.47 | 5427.02 | 5427.47 | |
| 6 | 0.000 | 8 | Cir | 39.300 | 1.25 | Grate | 0.10 | 0.012 | 0.30 | 1.46 | 5429.49 | 5429.51 | 0.021 | 0.25 | 5433.70 | 5431.70 | 5429.48 | 5429.50 | 5427.47 | 5427.96 | |
| 7 | 0.000 | 8 | Cir | 12.800 | 1.25 | None | 0.10 | 0.012 | 0.20 | 1.46 | 5429.51 | 5429.51 | 0.003 | 0.21 | 5431.70 | 5432.80 | 5429.51 | 5429.51 | 5427.96 | 5428.12 | |
| 8 | -45.000 | 8 | Cir | 27.900 | 1.25 | Grate | 0.10 | 0.012 | 0.10 | 1.47 | 5429.51 | 5429.52 | 0.002 | 0.14 | 5432.80 | 5431.50 | 5429.51 | 5429.51 | 5428.12 | 5428.47 | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| Project | File: 2033 | South SD |).stm | 1 | | L | | | | | | L | | Number | of lines: 8 | | I | Date: 9/5 | 5/2014 | I | |
| NOTES | NOTES: ** Critical depth | | | | | | | | | | | | | | | | | | | | |

Storm Sewer Profile

Proj. file: 2033 South SD.stm







19 | Page





20 | Page







KEYED NOTES

CG-104 AND CG-105. NOT ALL NOTES ARE USED ON EACH SHEET. SPOT ELEVATION LABELS WITHIN GUTTER AREA REPRESENT FLOWLINE UNLESS NOTED. ADD 0.5' TYPICAL FOR TOP OF CURB GRADES WITHIN R.O.W. SHOWN FOR INFORMATION ONLY. SEE PUBLIC WORK ORDER DRAWINGS FOR CONSTRUCTION WITHIN R.O.W. INCLUDING NEW ACCESS DRIVES WITH CONCRETE VALLEY GUTTER, HANDICAP RAMPS, PUBLIC SIDEWALKS, CURB OPENINGS

CONSTRUCT PAVING AT ELEVATIONS SHOWN. NOTE THAT PAVEMENT SLOPES AND CROSS-SLOPES VARY THROUGHOUT TO ACHIEVE GRADES NECESSARY FOR ADA COMPLIANCE, PIPE

SLOPES WITHIN HANDICAP PARKING AREAS TO MEET ADA REQUIREMENTS (MAX. SLOPE = 2% IN ANY DIRECTION). CONSTRUCT HANDICAP ACCESS RAMP TO ADA STANDARDS. TRANSITION LANDSCAPING TO 6" MIN. DEPRESSION TO STORE STORMWATER. FLOW IN EXCESS OF AREA CAPACITY WILL OVERFLOW AT LOW POINT. NOTE: DO NOT DEPRESS LANDSCAPING OR HOLD STORMWATER WITHIN 10' OF BUILDING.

DEPRESSION EXTEND BUILDING ROOF DISCHARGE PIPE TO ON-SITE STORM DRAIN SYSTEM. MAKE WATERTIGHT CONNECTION USING FITTINGS AS REQUIRED. SEE MECHANICAL PLAN FOR CONTINUATION. CONSTRUCT FRACTURED FACE ROCK LINED SWALE. SEE CG-501 PROVIDE OPENING IN CURB TO PASS FLOW. SEE CG-501 FOR 32. 10. CONSTRUCT 18" BOTTOM WIDTH COVERED SIDEWALK CULVERT (2

> 1. PROVIDE OPENINGS OR PIPES THROUGH WALL TO PASS FLOW. 12. CONSTRUCT PRIVATE STORM DRAIN SYSTEM. SEE DETAIL SHEET 13. CONSTRUCT BUBBLE-UP INLET. SEE CG-501 FOR DETAIL.

14. PROVIDE WATERTIGHT CONNECTION TO PUBLIC STORM SEWER. SEE 15. G.C. TO OBTAIN PERMIT(S) FROM N.M.D.O.T. FOR CONSTRUCTION

SIDEWALK, COVERED SIDEWALK CULVERTS, EROSION PROTECTION

POSITIVE DRAINAGE AWAY FROM BUILDING TO PROPOSED INLETS / WATER HARVESTING AREAS. COORDINATE WITH LANDSCAPE

RETAINING TO ACHIEVE GRADE TRANSITIONS SHOWN (SEE PLAN FOR TOP OF FINISHED GRADE EACH SIDE). SEE ARCHITECTURAL

19. INSTALL 2' WIDE X 1' DEEP TEMPORARY EROSION CONTROL. SEE

20. CONSTRUCT ON-SITE DETENTION POND TO ELEVATIONS AND EXTENTS SHOWN. SEE CG-101, GENERAL NOTE 'M'. 1. EXTENDED STEMWALL THIS AREA TO ACHIEVE GRADES SHOWN. SEE ARCHITECTURAL.

KEY ŇĒ CG-104 ₹ SE 5% CG-103 ISAACSON & ARFMAN, P.A. Consulting Engineering Associates 128 Monroe Street N.E. Albuquerque, New Mexico 87108 Ph. 505-268-8828 www.iacivil.com 2033 CG-101.dwg Sep 05,2014 This design, calculations, and concepts are owned by and remain the property of Isaacson & Arfman, P.A. and no part thereof shall be utilized by any person, firm or corporation for any purpose whatsoever except with the written permission of Isaacson & Arfman, P.A. © MorningStar of Albuquerque **GRADING & DRAINAGE PLAN-NW** Date: Job No. IA: 2033 CG-102

SH. OF

Ckd By:

FCA



3ike Path

^J426.

,

12.

- - <u>28.5</u> _









| | 32 |
|------|-----|
| — C(| DM- |
| | |
| | |
| | |
| | |

llow Stripe



