

CITY OF ALBUQUERQUE

Planning Department
Alan Varela, Director



Mayor Timothy M. Keller

February 3, 2023

J. Graeme Means, P.E.
High Mesa Consulting Group
6010 B Midway Park Blvd NE
Albuquerque, NM 87109

**RE: Arroyo del Oso ES Public Storm Drainage Channel
Drainage Plan
Engineer's Stamp Date: 01/25/23
Hydrology File: E18D007A**

Dear Mr. Means:

Based upon the information provided in your submittal received 01/25/2023, the Drainage Plan is approved for Work Order and Grading Permit. Please place this stamp approved Grading & Drainage Plan to the Work Order set of construction drawings.

As a reminder, if the project total area of disturbance (including the staging area and any work within the adjacent Right-of-Way) is 1 acre or more, then an Erosion and Sediment Control (ESC) Plan and Owner's certified Notice of Intent (NOI) is required to be submitted to the Stormwater Quality Engineer (Doug Hughes, PE, jhughes@cabq.gov, 924-3420) 14 days prior to any earth disturbance.

If you have any questions, please contact me at 924-3995 or rbrissette@cabq.gov.

Sincerely,

Renée C. Brissette, P.E. CFM
Senior Engineer, Hydrology
Planning Department

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City of Albuquerque

Planning Department
Development & Building Services Division

DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 6/2018)

Project Title: _____ **Building Permit #:** _____ **Hydrology File #:** _____

DRB#: _____ **EPC#:** _____ **Work Order#:** _____

Legal Description: _____

City Address: _____

Applicant: _____ **Contact:** _____

Address: _____

Phone#: _____ **Fax#:** _____ **E-mail:** _____

Other Contact: _____ **Contact:** _____

Address: _____

Phone#: _____ **Fax#:** _____ **E-mail:** _____

TYPE OF DEVELOPMENT: _____ PLAT (# of lots) _____ RESIDENCE _____ DRB SITE _____ ADMIN SITE

IS THIS A RESUBMITTAL? _____ Yes _____ No

DEPARTMENT _____ TRANSPORTATION _____ HYDROLOGY/DRAINAGE

Check all that Apply:

TYPE OF SUBMITTAL:

- _____ ENGINEER/ARCHITECT CERTIFICATION
- _____ PAD CERTIFICATION
- _____ CONCEPTUAL G & D PLAN
- _____ GRADING PLAN
- _____ DRAINAGE REPORT
- _____ DRAINAGE MASTER PLAN
- _____ FLOODPLAIN DEVELOPMENT PERMIT APPLIC
- _____ ELEVATION CERTIFICATE
- _____ CLOMR/LOMR
- _____ TRAFFIC CIRCULATION LAYOUT (TCL)
- _____ TRAFFIC IMPACT STUDY (TIS)
- _____ STREET LIGHT LAYOUT
- _____ OTHER (SPECIFY) _____
- _____ PRE-DESIGN MEETING?

TYPE OF APPROVAL/ACCEPTANCE SOUGHT:

- _____ BUILDING PERMIT APPROVAL
- _____ CERTIFICATE OF OCCUPANCY
- _____ PRELIMINARY PLAT APPROVAL
- _____ SITE PLAN FOR SUB'D APPROVAL
- _____ SITE PLAN FOR BLDG. PERMIT APPROVAL
- _____ FINAL PLAT APPROVAL
- _____ SIA/ RELEASE OF FINANCIAL GUARANTEE
- _____ FOUNDATION PERMIT APPROVAL
- _____ GRADING PERMIT APPROVAL
- _____ SO-19 APPROVAL
- _____ PAVING PERMIT APPROVAL
- _____ GRADING/ PAD CERTIFICATION
- _____ WORK ORDER APPROVAL
- _____ CLOMR/LOMR
- _____ FLOODPLAIN DEVELOPMENT PERMIT
- _____ OTHER (SPECIFY) _____

DATE SUBMITTED: _____ **By:** _____

COA STAFF:

ELECTRONIC SUBMITTAL RECEIVED: _____

FEE PAID: _____

SITE HYDROLOGIC CALCULATIONS (FOR INFORMATION ONLY)

I. SITE CHARACTERISTICS

| | |
|--|------------------------|
| A. PRECIPITATION ZONE = | 3 |
| B. $P_{100, 6 \text{ HR}} = P_{300} =$ | 2.43 IN |
| C. TOTAL PROJECT AREA (A_T) = | 443,559 SF 10.18 AC |

D. LAND TREATMENTS

| EXISTING LAND TREATMENT | | | | | DEVELOPED LAND TREATMENT | | | | |
|--|--------------|------|--|--|--|--------------|-----|--|--|
| BASIN A | 431,309 SF | | | | BASIN A | 431,443 SF | | | |
| LAND TREATMENT | AREA (SF/AC) | % | | | LAND TREATMENT | AREA (SF/AC) | % | | |
| A | | | | | A | | | | |
| B | 115,437 SF | 27% | | | B | 112,835 SF | 28% | | |
| C | 137,213 SF | 32% | | | C | 82,080 SF | 19% | | |
| D | 178,659 SF | 41% | | | D | 236,728 SF | 55% | | |
| | 4.10 AC | | | | | 5.43 AC | | | |
| BASIN B | 12,250 SF | | | | BASIN B | 12,116 SF | | | |
| LAND TREATMENT | AREA (SF/AC) | % | | | LAND TREATMENT | AREA (SF/AC) | % | | |
| A | | | | | A | | | | |
| B | | | | | B | | | | |
| C | 12,250 SF | 100% | | | C | 8,806 SF | 73% | | |
| D | 0.28 AC | | | | D | 3,310 SF | 27% | | |
| | 0.28 AC | | | | | 0.08 AC | | | |
| OFFSITE BASIN (PER 1994 MDP LAND TREATMENT VALUES) | 668,645 SF | | | | OFFSITE BASIN (PER 1994 MDP LAND TREATMENT VALUES) | 668,645 SF | | | |
| LAND TREATMENT | AREA (SF/AC) | % | | | LAND TREATMENT | AREA (SF/AC) | % | | |
| A | | | | | A | | | | |
| B | 405,545 SF | 61% | | | B | 405,545 SF | 61% | | |
| C | 9.31 AC | | | | C | 9.31 AC | | | |
| D | 263,100 SF | 39% | | | D | 263,100 SF | 39% | | |
| | 6.04 AC | | | | | 6.04 AC | | | |
| | | | | | BASIN A (INTERIM)* | 9.90 AC | | | |
| | | | | | LAND TREATMENT | AREA (SF/AC) | % | | |
| | | | | | A | | | | |
| | | | | | B | 40,620 SF | 9% | | |
| | | | | | C | 85,500 SF | 20% | | |
| | | | | | D | 1.96 AC | | | |
| | | | | | | 305,323 SF | 71% | | |
| | | | | | | 7.01 AC | | | |

*INTERIM BASIN A CONDITION BASED UPON 4-6 MONTH PERIOD WHEN NEW BUILDING CONSTRUCTION IS COMPLETE AND OLD BUILDING DEMOLISHED BEGINS. FOLLOWED BY NEW FIELD INSTALLATION

II. HYDROLOGY

A. EXISTING CONDITION 100 YEAR STORM

1. BASIN A

a. VOLUME 100-YR. 6-HR

$$WTE = (E_A \cdot A_A + E_B \cdot A_B + E_C \cdot A_C + E_D \cdot A_D) / A_T$$

$$\Rightarrow (0.67 \cdot 0.00) + (0.86 \cdot 2.65) + (1.09 \cdot 3.15) + (2.58 \cdot 4.10) / 9.90 = 1.65 \text{ IN}$$

$$V_{100, 6 \text{ HR}} = (E_W / 12) \cdot A_T \Rightarrow (1.65 / 12) \cdot 9.90 = 1.3615 \text{ AC-FT} = 69,300 \text{ CF}$$

b. PEAK DISCHARGE 100-YR

$$Q_{100} = Q_A \cdot A_A + Q_B \cdot A_B + Q_C \cdot A_C + Q_D \cdot A_D$$

$$\Rightarrow (1.84 \cdot 0.00) + (2.49 \cdot 2.65) + (3.17 \cdot 3.15) + (4.49 \cdot 4.10) = 35.0 \text{ CFS}$$

2. BASIN B

a. VOLUME 100-YR. 6-HR

$$WTE = (E_A \cdot A_A + E_B \cdot A_B + E_C \cdot A_C + E_D \cdot A_D) / A_T$$

$$\Rightarrow (0.67 \cdot 0.00) + (0.86 \cdot 0.00) + (1.09 \cdot 0.28) + (2.58 \cdot 0.00) / 0.28 = 1.09 \text{ IN}$$

$$V_{100, 6 \text{ HR}} = (E_W / 12) \cdot A_T \Rightarrow (1.09 / 12) \cdot 0.28 = 0.0255 \text{ AC-FT} = 1,110 \text{ CF}$$

b. PEAK DISCHARGE 100-YR

$$Q_{100} = Q_A \cdot A_A + Q_B \cdot A_B + Q_C \cdot A_C + Q_D \cdot A_D$$

$$\Rightarrow (1.84 \cdot 0.00) + (2.49 \cdot 0.00) + (3.17 \cdot 0.28) + (4.49 \cdot 0.00) = 0.9 \text{ CFS}$$

3. OFFSITE BASIN (PER 1994 MDP LAND TREATMENT VALUES)

a. VOLUME 100-YR. 6-HR

$$WTE = (E_A \cdot A_A + E_B \cdot A_B + E_C \cdot A_C + E_D \cdot A_D) / A_T$$

$$\Rightarrow (0.67 \cdot 0.00) + (0.86 \cdot 9.31) + (1.09 \cdot 0.00) + (2.58 \cdot 6.04) / 15.35 = 1.54 \text{ IN}$$

$$V_{100, 6 \text{ HR}} = (E_W / 12) \cdot A_T \Rightarrow (1.54 / 12) \cdot 15.35 = 1.9699 \text{ AC-FT} = 85,810 \text{ CF}$$

b. PEAK DISCHARGE 100-YR

$$Q_{100} = Q_A \cdot A_A + Q_B \cdot A_B + Q_C \cdot A_C + Q_D \cdot A_D$$

$$\Rightarrow (1.84 \cdot 0.00) + (2.49 \cdot 9.31) + (3.17 \cdot 0.00) + (4.49 \cdot 6.04) = 50.3 \text{ CFS}$$

B. DEVELOPED CONDITION 100 YEAR STORM

1. BASIN A

a. VOLUME 100-YR. 6-HR

$$WTE = (E_A \cdot A_A + E_B \cdot A_B + E_C \cdot A_C + E_D \cdot A_D) / A_T$$

$$\Rightarrow (0.67 \cdot 0.00) + (0.86 \cdot 2.59) + (1.09 \cdot 1.88) + (2.58 \cdot 5.43) / 9.90 = 1.85 \text{ IN}$$

$$V_{100, 6 \text{ HR}} = (E_W / 12) \cdot A_T \Rightarrow (1.85 / 12) \cdot 9.90 = 1.5270 \text{ AC-FT} = 66,510 \text{ CF}$$

b. PEAK DISCHARGE 100-YR

$$Q_{100} = Q_A \cdot A_A + Q_B \cdot A_B + Q_C \cdot A_C + Q_D \cdot A_D$$

$$\Rightarrow (1.84 \cdot 0.00) + (2.49 \cdot 2.59) + (3.17 \cdot 1.88) + (4.49 \cdot 5.43) = 36.8 \text{ CFS}$$

2. BASIN B

a. VOLUME 100-YR. 6-HR

$$WTE = (E_A \cdot A_A + E_B \cdot A_B + E_C \cdot A_C + E_D \cdot A_D) / A_T$$

$$\Rightarrow (0.67 \cdot 0.00) + (0.86 \cdot 0.00) + (1.09 \cdot 0.20) + (2.58 \cdot 0.08) / 0.28 = 1.50 \text{ IN}$$

$$V_{100, 6 \text{ HR}} = (E_W / 12) \cdot A_T \Rightarrow (1.50 / 12) \cdot 0.28 = 0.0348 \text{ AC-FT} = 1,510 \text{ CF}$$

b. PEAK DISCHARGE 100-YR

$$Q_{100} = Q_A \cdot A_A + Q_B \cdot A_B + Q_C \cdot A_C + Q_D \cdot A_D$$

$$\Rightarrow (1.84 \cdot 0.00) + (2.49 \cdot 0.00) + (3.17 \cdot 0.20) + (4.49 \cdot 0.08) = 1.0 \text{ CFS}$$

3. OFFSITE BASIN (PER 1994 MDP LAND TREATMENT VALUES)

a. VOLUME 100-YR. 6-HR

$$WTE = (E_A \cdot A_A + E_B \cdot A_B + E_C \cdot A_C + E_D \cdot A_D) / A_T$$

$$\Rightarrow (0.67 \cdot 0.00) + (0.86 \cdot 9.31) + (1.09 \cdot 0.00) + (2.58 \cdot 6.04) / 15.35 = 1.54 \text{ IN}$$

$$V_{100, 6 \text{ HR}} = (E_W / 12) \cdot A_T \Rightarrow (1.54 / 12) \cdot 15.35 = 1.9699 \text{ AC-FT} = 85,810 \text{ CF}$$

b. PEAK DISCHARGE 100-YR

$$Q_{100} = Q_A \cdot A_A + Q_B \cdot A_B + Q_C \cdot A_C + Q_D \cdot A_D$$

$$\Rightarrow (1.84 \cdot 0.00) + (2.49 \cdot 9.31) + (3.17 \cdot 0.00) + (4.49 \cdot 6.04) = 50.3 \text{ CFS}$$

C. NEW PUBLIC STORM DRAIN CHANNEL CAPACITY (MANNING'S EQUATION FOR OPEN CHANNEL FLOW)

USING MANNING'S EQUATION FOR 10' WIDE CHANNEL, 1.5' WALL HEIGHT (0.7' WATER FLOW DEPTH @ FREEBOARD), MIN. SLOPE = 1.2%

$$Q_{\text{CHANNEL CAP}} = 1.49 \text{ ft}^3 \cdot A \cdot R^{2/3} \cdot S^{1/2} = (1.49 \cdot 0.013) \times (7 \text{ SF}) \times (0.617^{2/3}) \cdot (0.012)^{1/2} = 63.3 \text{ CFS}$$

$$Q_{\text{CHANNEL CAP}} = 63.3 \text{ CFS} > Q_{\text{OFFSITE DISCHARGE}} = 50.3 \text{ CFS; OK}$$

4. BASIN A (INTERIM)*

a. VOLUME 100-YR. 6-HR

$$WTE = (E_A \cdot A_A + E_B \cdot A_B + E_C \cdot A_C + E_D \cdot A_D) / A_T$$

$$\Rightarrow (0.67 \cdot 0.00) + (0.86 \cdot 0.93) + (1.09 \cdot 1.96) + (2.58 \cdot 7.01) / 9.90 = 2.12 \text{ IN}$$

$$V_{100, 6 \text{ HR}} = (E_W / 12) \cdot A_T \Rightarrow (2.12 / 12) \cdot 9.90 = 1.7498 \text{ AC-FT} = 76,220 \text{ CF}$$

b. PEAK DISCHARGE 100-YR

$$Q_{100} = Q_A \cdot A_A + Q_B \cdot A_B + Q_C \cdot A_C + Q_D \cdot A_D$$

$$\Rightarrow (1.84 \cdot 0.00) + (2.49 \cdot 0.93) + (3.17 \cdot 1.96) + (4.49 \cdot 7.01) = 40.0 \text{ CFS}$$

C. COMPARISON 100 YEAR STORM

1. BASIN A

a. VOLUME 100-YR. 6-HR (GROSS)

$$\Delta V_{100, 6 \text{ HR}} = 66510 - 59300 = 7,210 \text{ CF} \quad (\text{INCREASE})$$

b. PEAK DISCHARGE 100-YR

$$\Delta Q_{100} = 36.8 - 35.0 = 1.8 \text{ CFS} \quad (\text{INCREASE})$$

C. SUBSURFACE INFILTRATION SYSTEM CAPACITY

$$V_{\text{INFILTRATION CAPACITY}} = 14,593 \text{ CF}$$

$$V_{\text{DET. CAP}} > \Delta V_{100, 6 \text{ HR}} = 14,593 \text{ CF} > 7,210 \text{ CF; INCREASED RUNOFF MANAGED VIA INFILTRATION ONSITE}$$

d. STORMWATER QUALITY VOLUME =

$$1,500 + 230 + 300 = 2,030 \text{ CF}$$

e. VOLUME 100-YR. 6-HR (NET)

$$\Delta V_{100, 6 \text{ HR}} = 7,210 - 14,593 - 2,030 = -9,413 \text{ CF} \quad (\text{DECREASE})$$

2. BASIN B

a. VOLUME 100-YR. 6-HR

$$\Delta V_{100, 6 \text{ HR}} = 1510 - 1110 = 400 \text{ CF} \quad (\text{INCREASE})$$

b. PEAK DISCHARGE 100-YR

$$\Delta Q_{100} = 1.0 - 0.9 = 0.1 \text{ CFS} \quad (\text{INCREASE})$$

3. BASIN A (INTERIM)*

a. VOLUME 100-YR. 6-HR (GROSS)

$$\Delta V_{100, 6 \text{ HR}} = 76220 - 59300 = 16,920 \text{ CF} \quad (\text{INCREASE})$$

b. PEAK DISCHARGE 100-YR

$$\Delta Q_{100} = 40.0 - 35.0 = 5.0 \text{ CFS} \quad (\text{INCREASE})$$

c. SUBSURFACE INFILTRATION SYSTEM CAPACITY

$$V_{\text{INFILTRATION CAPACITY}} = 14,593 \text{ CF}$$

$$V_{\text{CAP}} < \Delta V_{100, 6 \text{ HR}} = 14,593 \text{ CF} < 16,920 \text{ CF; 86% INCREASED RUNOFF MANAGED VIA INFILTRATION ONSITE}$$

d. STORMWATER QUALITY VOLUME =

$$1,500 + 230 + 300 = 2,030 \text{ CF}$$

e. VOLUME 100-YR. 6-HR (NET)

$$\Delta V_{100, 6 \text{ HR (NET)}} = 16,920 - 14,593 - 2,030 = 297 \text{ CF} \quad (\text{INCREASE})$$

$$V_{\text{CAP}} > \Delta V_{100, 6 \text{ HR (GROSS)}} = 14,593 \text{ CF} > 2,030 \text{ CF; 99% INCREASED RUNOFF MANAGED VIA INFILTRATION & SURFACE STORM WATER QUALITY ONSITE}$$

D. STORM WATER QUALITY AND LEED CALCULATIONS

THE MEASURES ASSOCIATED WITH THIS PROJECT ARE INTENDED TO EXCEED THOSE REQUIRED FOR THE CITY OF ALBUQUERQUE STORMWATER QUALITY ORDINANCE AND ALSO THOSE FOR LEED BD+C: NEW CONSTRUCTION V4.1 SUSTAINABLE SITES RAINWATER MANAGEMENT CREDIT OPTION 1-3 CREDITS FOR MANAGING THE 90TH PERCENTILE EVENT. THE ASSOCIATED FINAL CONDITION VOLUME REQUIRED OF 8,400 CF HAS BEEN DETERMINED USING THE CITY OF ALBUQUERQUE METHODOLOGY AS FOLLOWS:

$$\text{LEED BOUNDARY AREA} = 443,559 \text{ SF (10.18 AC); IMPERVIOUS AREA} = 5.51 \text{ AC}$$

$$90^{\text{TH}} \text{ PERCENTILE RUNOFF DEPTH} = 0.42"$$

PER COA DPM ARTICLE 6-12 (STORMWATER QUALITY AND LOW IMPACT DEVELOPMENT), THE IMPERVIOUS AREA SHALL BE MULTIPLIED BY THE 0.42" STORM EVENT FROM THE 90TH PERCENTILE STORM EVENT.

$$V_{90^{\text{TH}}} = (E_W \cdot 90^{\text{TH}})^{1/2} \cdot A_T$$

$$\Rightarrow (0.42 / 12) \cdot 5.51 = 0.42 / 12 \cdot 5.51 = 0.1929 \text{ AC-FT} = 8,400 \text{ CF}$$

IN RECOGNITION THAT THERE WILL BE AN INTERIM CONDITION WHEREBY THE NEW CONSTRUCTION IS COMPLETE PRIOR TO DEMOLITION OF THE EXISTING SCHOOL, THE FOLLOWING CALCULATIONS ARE FOR THE INTERIM WORST CASE TEMPORARY CONDITION:

$$\text{LEED BOUNDARY AREA} = 443,559 \text{ SF (10.18 AC); IMPERVIOUS AREA} = 7.09 \text{ AC}$$

$$90^{\text{TH}} \text{ PERCENTILE RUNOFF DEPTH} = 0.42"$$

$$V_{90^{\text{TH}}} = (E_W \cdot 90^{\text{TH}})^{1/2} \cdot A_T$$

$$\Rightarrow (0.42 / 12) \cdot 7.09 = 0.42 / 12 \cdot 7.09 = 0.2482 \text{ AC-FT} = 10,810 \text{ CF}$$

DRAINAGE PLAN

THIS PLAN IS SUBMITTED FOR WORK ORDER APPROVAL. THIS APS SITE BUILDING PERMIT APPROVAL WILL BE THROUGH C.I.D., AND THEREFORE THIS IS NOT A REQUEST FOR COA BUILDING PERMIT APPROVAL. CALCULATIONS AND PORTIONS OF THIS DRAINAGE PLAN ARE PROVIDED FOR INFORMATION ONLY AND TO DEMONSTRATE COMPLIANCE WITH C.O.A. APPROVED MASTER PLAN REQUIREMENTS.

THE SCHOOL SITE GENERALLY SLOPES FROM NORTHEAST TO SOUTHWEST WITH APPROXIMATELY 15' FEET OF FALL, CONSISTING OF SLOPES RANGING FROM 3 TO 5%. EXISTING STORMWATER RUNOFF GENERATED BY THE SITE IS 100% SURFACE SHEET FLOW THAT ULTIMATELY DRAINS TO A 10' PAVED PUBLIC RUNDOWN IN A DEDICATED PEDESTRIAN AND DRAINAGE RIGHT-OF-WAY BETWEEN 2 RESIDENTIAL PROPERTIES NEAR THE SOUTHWEST CORNER OF THE SITE. PER THE 1999 SITE MASTER DRAINAGE PLAN FOR THE SITE PREPARED BY SCOTT MCGEE, AND SUBSEQUENT 2000 CERTIFIED RECORD DRAWINGS (E18-D7A), THE SITE HAS LIMITED, CONTROLLED DISCHARGE THROUGH THIS 10' PUBLIC DRAINAGE RUNDOWN TO ROSALIND DRIVE NE, A FULLY DEVELOPED PUBLIC STREET.

PROPOSED SITE IMPROVEMENTS WILL INCLUDE SURFACE DRAINAGE IMPROVEMENTS, PRIVATE SUBSURFACE STORM DRAIN IMPROVEMENTS AND ON-SITE STORMWATER INFILTRATION WATER QUALITY AREAS (BOTH SURFACE AND SUB-SURFACE) THAT WILL MANAGE THE DEVELOPED STORMWATER GENERATED TO MORE THAN TWICE THE CITY-REQUIRED LEVEL FOR NEW DEVELOPMENT. THE ONSITE SURFACE WATER QUALITY AREAS AND SUB-SURFACE STORMWATER INFILTRATION SYSTEM ARE SIZED TO MANAGE THE INCREASED STORMWATER GENERATION RESULTING FROM THE DEVELOPED SITE. DEVELOPED STORMWATER RUNOFF FROM THE SCHOOL SITE WILL CONTINUE TO DISCHARGE THROUGH THE SW CORNER PUBLIC DRAINAGE RUNDOWN TO ROSALIND DRIVE NE PER THE 1999 MDP APPROVED, CONTROLLED DISCHARGE RATE, MAINTAINING THE EXISTING APPROVED STORM DRAINAGE PATTERN FOR THE SITE.

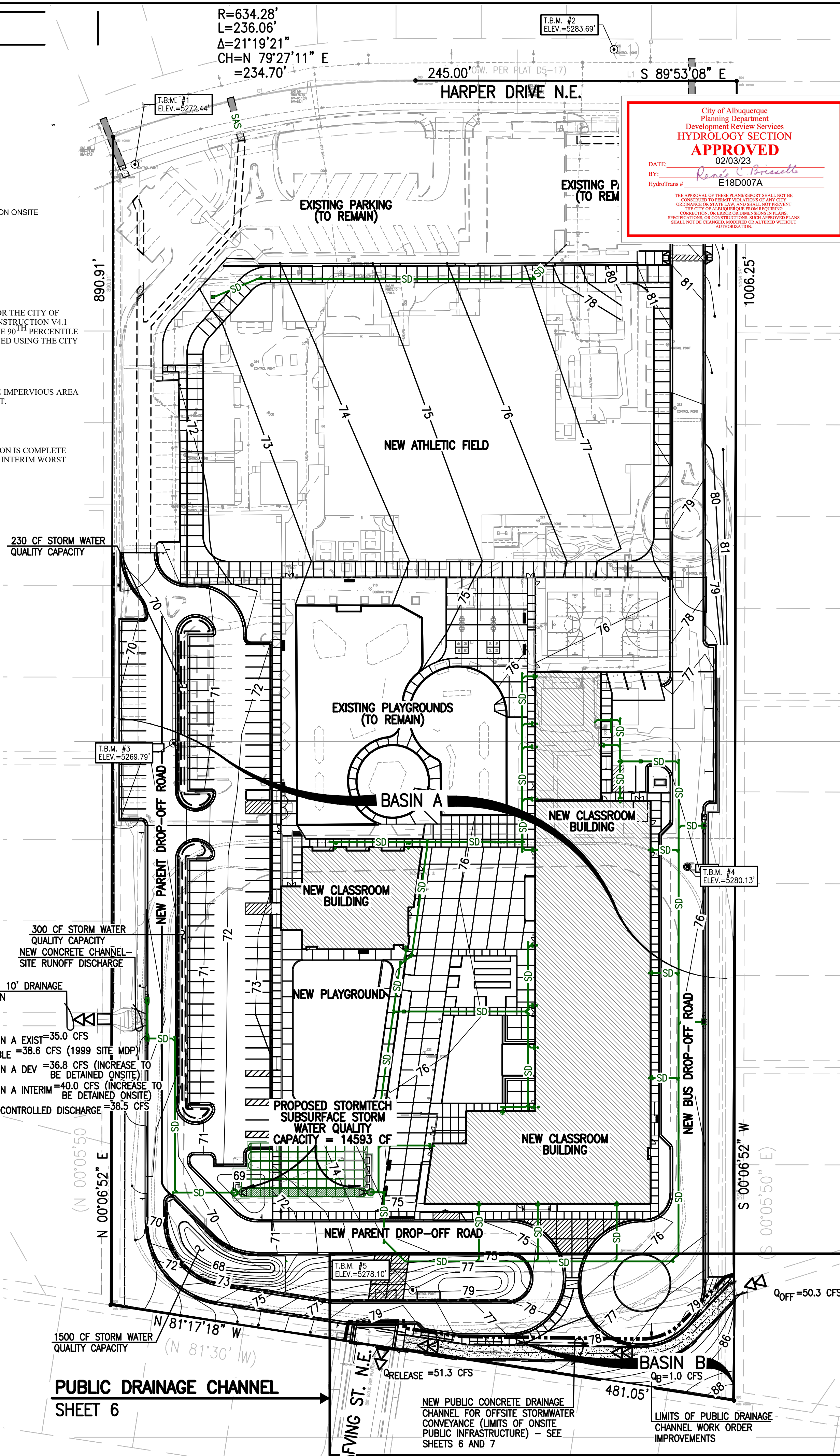
ADDITIONALLY, THERE IS AN EXISTING OFFSITE PUBLIC STORMWATER DRAINAGE RUNDOWN NEAR THE SOUTHEAST CORNER OF THE SITE THAT RELEASES A PEAK 100-YEAR DISCHARGE OF 54 CFS (1999 MDP) OF PUBLIC RUNOFF ONTO BASIN B OF THE SITE FROM THE DEVELOPED RESIDENTIAL AREA EAST OF THE SCHOOL SITE. RECORD DRAWINGS FROM 1994 & 1999, ALONG WITH THE 1999 ARROYO DEL OSO ELEMENTARY SCHOOL MASTER DRAINAGE PLAN DESIGNATE THAT THE OFFSITE RUNOFF MUST BE ACCEPTED AND CONVEYED THROUGH THE SE CORNER (BASIN B) OF THE SITE AND DISCHARGE SOUTH INTO LAVING STREET. EXISTING CONDITION SITE OBSERVATIONS IN 2022 HAVE NOTED THE OFFSITE RUNOFF IS NOT CURRENTLY DRAINING TO LAVING STREET DUE TO EROSION OF THE 1999 CONSTRUCTED EARTHWORK BERM THAT WAS DESIGNED TO CHANNEL THE OFFSITE RUNOFF TO LAVING STREET. OFFSITE RUNOFF CURRENTLY DRAINS EAST TO WEST THROUGH THE SCHOOL SITE TO RELEASE TO THE PUBLIC DRAINAGE RUNDOWN OUTLET AT THE SOUTH WEST CORNER OF THE SCHOOL SITE.

A NEW 10' PUBLIC CONCRETE STORMWATER DRAINAGE CHANNEL IS PROPOSED TO BE CONSTRUCTED AT THE SE CORNER OF THE SITE IN BASIN B; THE PROPOSED CHANNEL WILL CONVEY THE OFFSITE STORMWATER FROM THE EAST PROPERTY EDGE SOUTHWEST TO DISCHARGE INTO LAVING STREET AS DESIGNATED IN THE EXISTING MASTER DRAINAGE PLAN. THERE DOES NOT APPEAR TO BE ANY EXISTING EASEMENT OR OTHER DOCUMENT SUPPORTING THE PUBLIC STORM DRAINAGE ACROSS APS PROPERTY; A NEW 12' PUBLIC DRAINAGE ACCESS AND MAINTENANCE EASEMENT IS PROPOSED TO ADDRESS THIS ISSUE.

CALCULATIONS FOR THIS SITE WERE PREPARED BASED UPON THE 100-YEAR, 6 HOUR RAINFALL EVENT. THE PROCEDURE FOR 40 ACRE AND SMALLER BASINS, AS SET FORTH IN SECTION 22.2, HYDROLOGY OF THE CITY OF ALBUQUERQUE DEVELOPMENT PROCESS MANUAL, VOLUME 2 (UPDATED JUNE 2020) HAS BEEN USED TO QUANTIFY THE PEAK RATE OF DISCHARGE AND VOLUME OF RUNOFF FOR THE ONSITE FLOWS GENERATED AND THE OFFSITE FLOWS IMPACTING THIS SITE. IT SHOULD BE NOTED THAT THESE CALCULATIONS BASED UPON THE CURRENT METHODOLOGY DEMONSTRATE A REDUCED GENERATED PEAK VOLUME AND RATE OF DISCHARGE FOR THE OFFSITE RUNOFF IMPACTING THE SITE (50.3 CFS BY 2020 DPM VS 54 CFS BY 1999 MDP CALCULATIONS). THE PROPOSED IMPROVEMENTS ARE ALL SIZED BASED UPON THE 2020 DPM METHODOLOGY CALCULATIONS.

MANNING'S EQUATION CALCULATION FOR THE PROPOSED 10' DRAINAGE CHANNEL DEMONSTRATES THAT THE CHANNEL HAS A CAPACITY OF 63.3 CFS WHILE MAINTAINING 0.8' OF FREEBOARD. THIS CAPACITY IS MORE THAN SUFFICIENT TO CONVEY THE Q100 OFFSITE DISCHARGE OF 50.3 CFS.

THIS PROPOSED ONSITE STORM WATER QUALITY CAPACITY GREATLY EXCEEDS CITY OF ALBUQUERQUE STORM WATER QUALITY VOLUME REQUIREMENTS FOR THE SCHOOL. HYDROLOGIC CALCULATIONS FOR THE SITE INCLUDE THE COA STORM WATER QUALITY VOLUME CALCULATIONS FOR A NEW DEVELOPED SITE BASED UPON THE CITY DPM; THESE CALCULATIONS DEMONSTRATE THE SITE REQUIRES 8400 CF PER THE CITY OF ALBUQUERQUE ORDINANCE, WHICH IS SIGNIFICANTLY LESS THAN THE TOTAL SITE VOLUME (14593 CFS SUBSURFACE, 2030 CF SURFACE).

PUBLIC DRAINAGE CHANNEL
SHEET 6

BENCHMARKS

TEMPORARY BENCHMARK (T.B.M. #1)

A MAG NAIL W/WASHER, SET IN THE CONCRETE BACK OF CURB NEAR THE NORTHWEST PORTION OF THE SURVEY, AS SHOWN ON THIS SHEET.

$$\text{ELEVATION} = 5272.44 \text{ FEET (NAVD 1988)}$$

TEMPORARY BENCHMARK (T.B.M. #2)

A MAG NAIL W/WASHER, SET IN THE CONCRETE BACK OF CURB NEAR THE NORTHEAST PORTION OF THE SURVEY ON THE NORTH SIDE OF HARPER DRIVE N.E., AS SHOWN ON THIS SHEET.

$$\text{ELEVATION} = 5283.69 \text{ FEET (NAVD 1988)}$$

TEMPORARY BENCHMARK (T.B.M. #3)