# ALBUQUERQUE NEW MEXICO

### City of Albuquerque

April 4, 2000

J. Graeme Means, PE Jeff Mortensen & Associates, Inc 6010-B Midway Park Blvd. NE Albuquerque, NM 87109

Re: Rinconada Mesa Subdivision

**Conceptual Grading and Drainage Plan Engineer's Stamp dated 3-14-00 (F10/D10)** 

Dear Mr. Means,

Based upon the information provided in your submittal dated 3-15-00, the above referenced conceptual grading and drainage plan is acceptable and is approved for Site Development Plan for Subdivision and Site Development Plan for Building Permit.

Please be advised that a more comprehensive grading and drainage submittal to Hydrology will be necessary prior to DRB approval of the Preliminary Plat. Please include a copy of the Infrastructure List with that submittal.

If you have any questions, you can contact me at 924-3986.

Sincerely,

Bradley L. Bingham, PE

Hydrology Review Engineer

C: file



## City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

August 25, 2000

J. Graeme Means, P. E. Jeff Mortensen & Associates, Inc. 6010-B Midway Park Blvd. NE Albuquerque, New Mexico 87109

RE: Grading and Drainage Plan for Rinconada Mesa Subdivision (F10/D10) Submitted for Preliminary and Final Plat Approval, Rough Grading and Work Order Approval, Engineer's Stamp Dated 8/2/00.

Dear Mr. Means:

Based on the information provided, the above referenced Grading and Drainage Plan for Rinconada Mesa Subdivision dated August 2, 2000 is approved for Preliminary Plat action.

The above referenced plan is also approved for Rough Grading. As you are aware, a topsoil disturbance permit must be obtained before any grading may occur on this site.

Prior to Final Plat sign-off, the Subdivision Improvements Agreement (SIA) must be in place. The Grading and Drainage Certification is required prior to the release of the SIA, or financial guarantees, for this subdivision.

If you have any questions, or if I may be of further assistance to you, please call me at 924-3982.

Sincerely,

Susan M. Calongne, P.E.

City/County Floodplain Administrator

Arlan Collatz, Collatz, Inc. c: DRB 1000352

File



#### City of Albuquerque

August 29, 2000

J. Graeme Means, P. E. Jeff Mortensen & Associates, Inc. 6010-B Midway Park Blvd. NE Albuquerque, New Mexico 87109

RE: Grading and Drainage Plan for Rinconada Mesa Subdivision (F10/D10) Submitted for Preliminary and Final Plat Approval, Rough Grading and Work Order Approval, Engineer's Stamp Dated 8/2/00, Revised on 8/29/00.

Dear Mr. Means:

Based on the information provided, the above referenced Grading and Drainage Plan for Rinconada Mesa Subdivision dated August 2, 2000 is approved for Preliminary Plat action.

The above referenced plan is also approved for Rough Grading. As you are aware, a topsoil disturbance permit must be obtained before any grading may occur on this site.

Prior to Final Plat sign-off, the Subdivision Improvements Agreement (SIA) must be in place. The Grading and Drainage Certification is required prior to the release of the SIA, or financial guarantees, for this subdivision.

If you have any questions, or if I may be of further assistance to you, please call me at 924-3982.

Sincerely,

Susan M. Calongne, P.E.

City/County Floodplain Administrator

c: DRB 1000352

File



## City of Albuquerque

P.O. BOX 1293 ALBUQUERQUE, NEW MEXICO 87103

April 15, 2002

J. Graeme Means, P.E.Jeff Mortensen & Assoc..6010-B Midway Park Blvd NEAlbuquerque, New Mexico 87109

RE: RINCONADA MESA SUBDIVISION

(F-10/D10)

**Engineers Certification For Release of Financial Guaranty** 

Engineers Stamp dated 8/2/2000 Rev. 8/29/2000

**Engineers Certification dated 4/9/2002** 

Dear Mr. Means:

Based upon the information provided in your Engineers Certification dated 4/9/2002, the above referenced plan is adequate to satisfy the Grading and Drainage Certification for Release of Financial Guaranty for the above referenced project.

If you have any questions, please call me at 924-3981.

Sincerely,

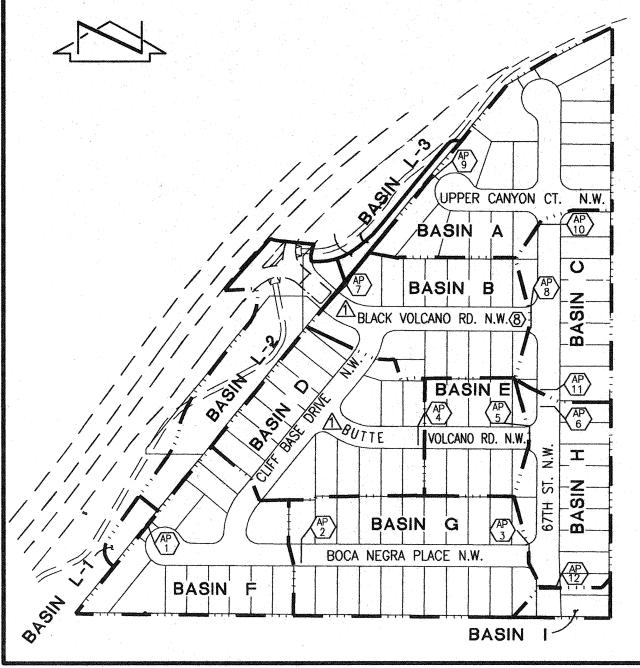
Teresa A. Martin

Hydrology Plan Checker Public Works Department

5UB

C: Arlene Portillo, PWD – #663981

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I. SITE CHARACTERISTICS
                                                                                              VI. STREET CAPACITY CALCULATIONS
                                                                                              (USING HAESTAD FLOWMASTER 6.0, MANNINGS EQUATION: n = 0.017)
 A. PRECIPITATION ZONE = 1
                                                                                              A. AP-2: Q_{100} = 9.0 CFS; s = 0.0050;
B. P_{6,100} = P_{360} = 2.20 IN.
                                                                                                  SECTION C-C: 28' F-F W/MOUNTABLE CURB AND GUTTER (ROLL TYPE);
                                                                                                  DEPTH = 0.33 FT (CURB HEIGHT)
C. TOTAL AREA (A_T) = 743,360 \text{ SF} (17.07 \text{ AC})
                                                                                                  F = 0.80 (SUBCRITICAL: NO HYDRAULIC JUMP POTENTIAL)
                                                                                                  OKAY TO USE MOUNTABLE CURB AND GUTTER (ROLL TYPE) UPSTREAM FROM AP-2;
 D. EXISTING LAND TREATMENT
                                                                                                  USE STANDARD CURB AND GUTTER DOWNSTREAM FROM AP-2
   TREATMENT AREA (SF/AC) %
   A 743,360/17.07 100
                                                                                               B. AP-4: Q_{100} = 9.2 CFS; s = 0.0060;
 E. DEVELOPED LAND TREATMENT
                                                                                                  SECTION C-C: 28' F-F W/MOUNTABLE CURB AND GUTTER (ROLL TYPE);
                                                                                                 DEPTH = 0.33 FT (CURB HEIGHT)
   TREATMENT AREA (SF/AC) %
                                                                                                 F = 0.88 (SUBCRITICAL: NO HYDRAULIC JUMP POTENTIAL)
               149,755/3.44 20
                                                                                                  OKAY TO USE MOUNTABLE CURB AND GUTTER (ROLL TYPE) UPSTREAM FROM AP-4;
               149,755/3.44 20
                                                                                                  USE STANDARD CURB AND GUTTER DOWNSTREAM FROM AP-4
              443,850/10.10 60
                                                                                               C. AP-8: Q_{100} = 11.1 CFS; s = 0.0100;
II. EXISTING CONDITION
                                                                                                  SECTION A-A: 32' F-F W/MOUNTABLE CURB AND GUTTER (ROLL TYPE);
 A. VOLUME
                                                                                                  DEPTH = 0.32 FT (LESS THAN CURB HEIGHT)
   E^{\mathbf{M}} = (E^{\mathbf{A}} \mathbf{A}^{\mathbf{A}} + E^{\mathbf{B}} \mathbf{A}^{\mathbf{B}} + E^{\mathbf{C}} \mathbf{A}^{\mathbf{C}} + E^{\mathbf{D}} \mathbf{A}^{\mathbf{D}}) / \mathbf{A}^{\mathbf{L}}
                                                                                                 F = 1.11 (SUPERCRITICAL: SPECIFIC ENERGY = 0.41 FT < R.O.W. HEIGHT)
                                                                                                  OKAY TO USE MOUNTABLE CURB AND GUTTER (ROLL TYPE) UPSTREAM FROM AP-8;
   E_{W} = 0.44 \text{ IN}.
                                                                                                 USE STANDARD CURB AND GUTTER DOWNSTREAM FROM AP-8
  V_{100} = (E_W/12)A_T
                                                                                               D. AP-6: Q_{100} = 37.8 CFS; s = 0.0050;
  V_{100} = (0.44/12)(743,360) = 27,260 \text{ CF}
                                                                                                 SECTION B-B: 28' F-F W/STANDARD CURB AND GUTTER;
DEPTH = 0.62 FT (LESS THAN CURB HEIGHT);
 B. PEAK DISCHARGE
                                                                                                 F = 0.92 (SUBCRITICAL: NO HYDRAULIC JUMP POTENTIAL)
  Q_{P} = Q_{PA}A_{A} + Q_{PB}A_{B} + Q_{PC}A_{C} + Q_{PD}A_{D}
                                                                                               E. AP-11: Q_{100} = 27.3 CFS; s = 0.0050;
  Q_p = Q_{100} = (1.29)(17.07) = 22.0 CFS
                                                                                                  SECTION B-B: 28' F-F W/STANDARD CURB AND GUTTER;
III. DEVELOPED CONDITION
                                                                                                  DEPTH = 0.55 FT (LESS THAN CURB HEIGHT);
 A. VOLUME
                                                                                                 F = 0.89 (SUBCRITICAL: NO HYDRAULIC JUMP POTENTIAL)
   E_{\mathbf{W}} = (E_{\mathbf{A}}A_{\mathbf{A}} + E_{\mathbf{B}}A_{\mathbf{B}} + E_{\mathbf{C}}A_{\mathbf{C}} + E_{\mathbf{D}}A_{\mathbf{D}})/A_{\mathbf{T}}
                                                                                              VII. SUMP CONDITION
  E_W = [(0.67)(3.44) + (0.99)(3.44) + (1.97)(10.19)]/(17.07) = 1.51 \text{ IN}.
                                                                                               A. INLET CALCULATIONS
                                                                                                  METHODOLOGY FROM U.S.D.O.T. FEDERAL HIGHWAY ADMINISTRATION URBAN DRAINAGE
  V_{100} = (E_W/12)A_T
                                                                                                  MANUAL (HEC-22)
  V_{100} = (1.51/12)(743,360) = 93,540 \text{ CF}
                                                                                                 Q_{100} = 65.1 \text{ CFS}
 B. PEAK DISCHARGE
                                                                                                  MAXIMUM DEPTH = CURB HEIGHT = 0.90 FT (MEASURED FROM TC TO GRATE)
  Q_{P} = Q_{PA}A_{A} + Q_{PB}A_{B} + Q_{PC}A_{C} + Q_{PD}A_{D}
                                                                                                  6 INLETS TOTAL (4 SINGLE A, 2 DOUBLE C)
                                                                                                  ASSUME GRATES 100 % CLOGGED (WORST CASE)
  Q_{p} = Q_{100} = (2.03)(3.44)+(2.87)(3.44)+(4.37)(10.19) = 61.4 CFS
                                                                                                  ALL FLOWS WILL ENTER CURB OPENINGS
                                                                                                 Q_1 = 0.67 hL(2gd_0)^{0.5} (EQ. 4-35)
 C. SITE BASIN CALCULATIONS
                                                                                                  h = CURB OPENING HEIGHT = 0.5 FT
                                                                                                 L = LENGTH OF OPENING = 7 FT (PER INLET)
  A_{TOTAL} = 17.1 AC
                                                                                                  g = 32.2 FT/S^2
                                                                                                  d = EFFECTIVE DEPTH AT CENTER OF OPENING = 0.65 FT
   BASIN AREA
                                                                                                 Q_{\rm c} = 15.2 CFS PER INLET
          2.9 AC
                                                                                                 15.2 CFS/INLET x 6 INLETS = 91.2 \text{ CFS} > Q_{100}
           1.5 AC
                                                                                               B. EMERGENCY OVERFLOW CALCULATIONS
           2.5 AC
          1.2 AC
                                                                                                   BECAUSE INLETS ARE LOCATED AT A SUMP CONDITION, AN EMERGENCY OVERFLOW IS
          2.4 AC
                                                                                                  PROVIDED WITHIN 67TH STREET. OVERFLOW SPILLWAY CALCULATIONS WERE PERFORMED
          2.6 AC
                                                                                                  USING HAESTAD FLOWMASTER 6.0 ASSUMING A BROAD CRESTED WEIR AS FOLLOWS:
           1.7 AC
          0.2 AC 01 0.7
                                                                                                  MAX HEADWATER ELEVATION = 5115.35 (MAX W.S.L.)
                                                                                                   CREST ELEVATION = 5114.50 (FL @ OVERFLOW)
  TOTAL | 17.1 AC | 100 | 61.4
                                                                                                   TAILWATER = 5114.82 (FL + 1.00' @ SOUTH BOUNDARY)
                                                                                                  CREST LENGTH: 30' (STREET WIDTH @ OVERFLOW)
 D. ANALYSIS POINT SUMMARY
                                                                                                  DISCHARGE = 71.3 \text{ CFS} (> Q_{100})
 ANALYSIS CONTRIBUTING CONTRIBUTING
   POINT BASINS
                                                                                              VIII. OFFSITE DOWNSTREAM STORM DRAIN CALCULATIONS (MANNING'S EQUATION)
                                                                                               A. 42" RCP @ S = 0.0037
                                             9.0 CFS
                                                                                                n = 0.013
  AP-3 L-1, F,G
                              5.2 AC
                                            18.2 CFS
                                                                                                Q_{100} = 65.1 \text{ CFS}
                                             9.2 CFS
                                            13.5 CFS
                                                                                               Q_{CAP} = 65.8 \text{ CFS} > Q_{100}
                                            37.8 CFS
                             10.6 AC
                                             3.7 CFS
                                                                                               B. 54" RCP @ S = 0.0035
                             3.6 AC
                                            11.1 CFS
                                            0.3 CFS
10.7 CFS
  AP-9 | L-3
                              0.1 AC
  AP-10 \mid L-3, A
                                                                                               Q_{100} = 65.1 + 55.7 = 120.8 \text{ CFS}
                             3.0 AC
  AP-11 | L-2,L-3,A,B,C | 8.1 AC | 27.3 CFS
                                                                                                Q_{CAP} = 125.1 \text{ CFS} > Q_{100}
  TOTAL FLOW TO STORM DRAIN = AP 6 + AP 11 = 37.8 + 27.3 = 65.1 CFS
IV. OFFSITE FLOWS
 A. FUTURE DEVELOPMENT ON TRACT A-1
 A = 14.76 AC
   ASSUME MULTIFAMILY ATTACHED (70 % D, 15 % C, 15 % B)
  Q_{100} = (2.03)(2.20) + (2.87)(2.20) + (4.37)(10.27) = 55.7 \text{ CFS}
 B. BASIN L-1
  A_{T} = 8,000 \text{ SF/0.18 AC}; A_{B} = 7,000 \text{ SF/0.16 AC};
  A_{D} = 1,000 \text{ SF}/0.02 \text{ AC}
  Q_{100} = (2.03)(0.16) + (4.37)(0.02) = 0.4 \text{ CFS}
 C. BASIN L-2
  A_T = 63,500 \text{ SF}/1.46 \text{ AC}; A_R = 49,500 \text{ SF}/1.14 \text{ AC};
  A_D = 14,000 \text{ SF}/0.32 \text{ AC}
  Q_{100} = (2.03)(1.14) + (4.37)(0.32) = 3.7 \text{ CFS}
 D. BASIN L-3
  A_T = 6,100 \text{ SF}/0.14 \text{ AC}; A_R = 5,300 \text{ SF}/0.12 \text{ AC};
  A_{D} = 800 \text{ SF}/0.02 \text{ AC}
  Q_{100} = (2.03)(0.12)+(4.37)(0.02) = 0.3 CFS
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BASIN MAP WITH ANALYSIS POINTS

SCALE :  $1" = 200' \pm$ 

#### SITE BASIN CALCULATIONS

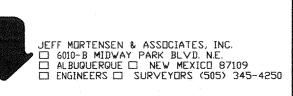
BASIN	AREA	%	Q <sub>100</sub>
A B C D E F G H	2.9 AC 2.1 AC 1.5 AC 2.5 AC 1.2 AC 2.4 AC 2.6 AC 1.7 AC 0.2 AC	17 12 09 15 07 14 15 10	10.4 7.4 5.5 9.2 4.3 8.6 9.2 6.1 0.7
OTAL	17.1 AC	100	61.4

#### ANALYSIS POINT SUMMARY

ANALYSIS	CONTRIBUTING	CONTRIBUTING	Q <sub>100</sub>
POINT	BASINS	AREA	
AP-1 AP-2 AP-3 AP-4 AP-5 AP-6 AP-7 AP-8	L-1 L-1, F L-1, F,G D D, E L-1, D,E,F,G,H L-2 L-2, B	0.2 AC 2.6 AC 5.2 AC 2.5 AC 3.7 AC 10.6 AC 1.5 AC 3.6 AC	0.4 CFS 9.0 CFS 18.2 CFS 9.2 CFS 13.5 CFS 37.8 CFS 3.7 CFS
AP-9	L-3	0.1 AC	0.3 CFS
AP-10	L-3, A	3.0 AC	10.7 CFS
AP-11	L-2,L-3,A,B,C	8.1 AC	27.3 CFS

TOTAL FLOW TO STORM DRAIN = AP 6 + AP 11 = 37.8 + 27.3 = 65.1 CFS

08-02-2000



CALCULATIONS AND BASIN MAP RINCONADA MESA

REVISIONS NO. DATE BY 2000.016.2 DESIGNED BY G.M. 1 08/00 G.M. REVISE STREET NAMES 08-2000 DRAWN BY J.Y.R. APPROVED BY J.G.M.

 $\Delta V_{100} = 93,540 - 27,250 = 66,290 \text{ CF (INCREASE)}$ 

 $\Delta Q_{100} = 61.4 - 22.0 = 39.4 \text{ CFS (INCREASE)}$ 

V. COMPARISON

