CITY OF ALBUQUERQUE

Planning Department David Campbell, Director



Mayor Timothy M. Keller

June 22, 2018

David Soule, P.E. Rio Grande Engineering PO Box 93924 Albuquerque, NM, 87199

RE: North 2nd Street Storage 5124 2nd St NW Grading Plan Stamp Date: 6/12/18 Drainage Report Stamp Date: 6/8/18 Hydrology File: F15D052E

Dear Mr. Soule,

PO Box 1293 Based on the submittal received 6/13/18, the Grading Plan and Drainage Report are approved for SO-19 and Building Permit.

Prior to Certificate of Occupancy (For Information):

Albuquerque

1. Engineer's Certification, per the DPM Chapter 22.7: *Engineer's Certification Checklist For Non-Subdivision* is required. The submittal/resubmittal fee for this request is: \$150.

NM 87103

- 2. The sidewalk culverts must be inspected and approved by storm drain maintenance (Jason Rodriguez, jtrodriguez@cabq.gov or 857-8607).
- www.cabq.gov3. The Private Facility Drainage Covenant must be recorded with Bernalillo County and a copy included with the drainage certification.
 - 4. Provide photographs of the installed orifice plate, including one showing its dimensions and include with the drainage certification.

If you have any questions, please contact me at 924-3695 or dpeterson@cabq.gov.

Sincerely,

Dana Peterson, P.E. Senior Engineer, Planning Dept. Development Review Services



City of Albuquerque Treasury J-24 Deposit 6/21/2018 Office: Date: ANNEX Station ID Cashier: E39083 Batch: 9343 Trans 11 TREASURY DIVISION DAILY DEPOSIT 305 Activity ID7547210 461615 Project ID24_MS4 Dept ID: Bus_Unit: PCDMD \$696.00 Alloc Amt: Trans Amt: \$696.00 Check Tendered : \$696.00

Payment In-Lieu for Storm Water Quality **Volume Requirement**

Transmittals for:

PROJECTS Only

MD 24_MS4 7547210 \$ 696.00 TOTAL DEPOSIT \$696.00								
TOTAL DEPOSIT \$696.00								
TOTAL DEPOSIT \$696.00								
TOTAL AMOUNT TOTAL DEPOSIT								
e: <u>North 2nd St Storage, 3576SF imp</u> .								
DEPARTMENT NAME: Planning Department/Development Review Services, Hydrology								
PREPARED BY Dana Peterson PHONE 924-3695								
BUSINESS DATE 6/20/18								

The Payment-in-Lieu can be paid at the Plaza del Sol Treasury, 600 2nd St. NW. Bring two copies of this invoice to the Treasury and provide a copy of the receipt to Hydrology, Suite 201, 600 2nd St. NW, or e-mail with the Hydrology submittal to PLNDRS@cabq.gov.



City of Albuquerque

Planning Department Development & Building Services Division DRAINAGE AND TRANSPORTATION INFORMATION SHEET (REV 09/2015)

Project Title: NORTH SECOND STORAGE	Building Permit #:	
B#: EPC#:		Work Order#:
egal Description: LLOTS1-3 NORTH SECOND BUSINESS CENTER		
ity Address: 5124 SECOND STREET NW	······································	
ngincering Firm: RIO GRANDE ENGINEERING		Contact: DAVID SOULE
Address: PO BOX 93924, ALBUQUERQUE, NM 87199		
Address: PO BOX 93924, ALEOGOE AGE, March 100 Phone#: 505.321.9099 Fax#: 505.872.0999		E-mail: DAVID@RIOGRANDEENGINEERING.CO
Were: MURPHY PROPERTIES		Contact:
Address: 5124 SECOND STREET NW ALB NM87107		E-mail?
hone#: Fax#:		
rchitect: JOSEPH SIMONS		Contact:
Address:		
Phone#: Fax#:		E-mail:
		Contact:
Other Contact:		
Address:		E-mail:
Phone#:Pax#		-
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MS4/ EROSION & SEDIMENT CONTROL TYPE OF SUBMITTAL: ENGINEER/ ARCHITECT CERTIFICATION	PRELIMINA SITE PLAN SITE PLAN	ARY PLAT APPROVAL FOR SUB'D APPROVAL FOR BLDG. PERMIT APPROVAL
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REVISED DRAINAGE REPORT

For

North Second Street Storage Lots 1,2,3 North Second Business Park

Albuquerque, New Mexico

Prepared by

Rio Grande Engineering PO Box 93924 Albuquerque, New Mexico 87199

MAY 2018



David Soule P.E. No. 14522

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Proposed Conditions
Summary

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Map Site Grading and Drainage Plan

PURPOSE

The purpose of this report is to provide the Drainage Management Plan for the development of a 2.32 acre tract of land that is being consolidated and redeveloped as storage units. This plan was prepared in accordance with the City of Albuquerque design regulations, utilizing the City of Albuquerque's Development Process Manual drainage guidelines. This report will demonstrate that the grading does not adversely affect the surrounding properties, nor the upstream or downstream facilities.

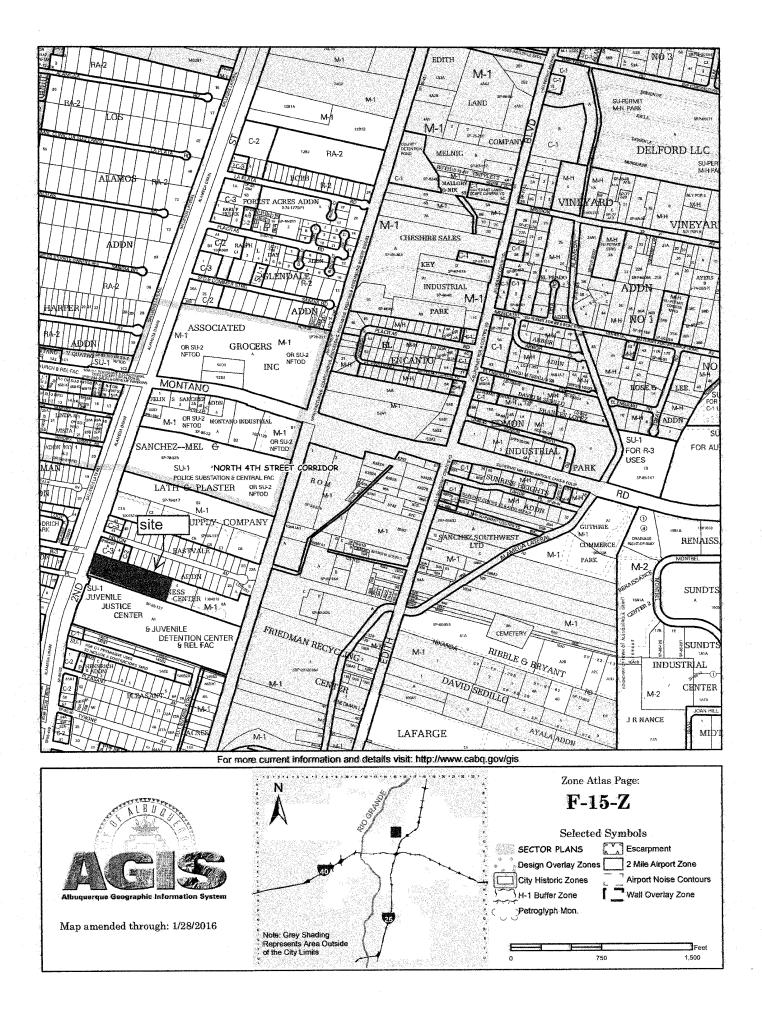
INTRODUCTION

The subject of this report, as shown on the Exhibit A, is a 2.32 -acre parcel of land located on the eastside of Second Street drive between Montano and Griegos NW. The current legal description of this site is lots 1, 2, 3 North Second Business Park. The three lots are in the process of being consolidated. As shown on FIRM map35001C0119GH, the entire site is located within Flood Zone X. The site is bound on all sides by roadways, rail road tracts and wall and is not impacted by upland flows. The site is an existing developed site, with a building on lot 3 and compacted asphalt millings and outdoor RV storage on lots 1 and 2. The site currently discharges 9.47 cfs to an inlet located at the southeast corner of this site within Second Street. The site was developed utilizing (F15-D22). The Conceptual drainage plan allowed to free discharge based upon 90% impervious. Based upon subsequent development, this appears not to be an implemented plan. The proposed improvements include the redevelopment of the existing building and the construction of several new buildings with associated paved drive isles. The site must discharge less than the existing peak flow requirements and must retain the first flush volume onsite.

EXISTING CONDITIONS

The site is currently developed. The site currently discharges developed flow of 9.47 cfs to the inlet located within Second Street at the southwest corner of this site. The flows are captured by an inlet and conveyed downstream within a city maintained storm drain. Due to rail

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road track and walls on the north and east side, as well as roadway along south side, the site is not impacted by upland flows.

PROPOSED CONDITIONS

The proposed improvements consist of interior improvements to the existing building and the construction of multiple new buildings. The area between the buildings will be paved. The buildings will drain to the interior paved access roads. The flows will be captured by a series of inline drains. The drains are connected via an 18" storm drain to a single type D inlet located at the North West corner of the storage unit areas. An 11" orifice plate is placed at the outfall of this inlet. As shown in appendix B, the orifice plate restricts the flow of 9.71 cfs to 5.73 cfs. The storage for this detention solution is provided within the access isles. The maximum predicted water surface is 4976.75. In the event of clogging the flow will exit the site via the emergency access driveway and flow directly to Second Street at an elevation of 4977.00. The throttled flow is conveyed from the onsite inlet to a first flush pond located adjacent to Second Street. This pond captures the required first flush volume of 3,369 cubic feet. The pond outfalls once full to 3-2' sidewalk culvert to be constructed directly upstream of the existing collection inlet. The site contains several smaller drainage basins, existing roadways and water blocks for the site. These basins exist therefore the resultant water quality volume for those areas not captured are 47.5 cubic feet of redeveloped and 39.1 cubic feet of new generation, creating a fee in lieu of \$696.00.

SUMMARY AND RECOMMENDATIONS

This project is a redevelopment of an existing site that discharges 9.47 cfs. The site generates a flow greater than allowed, so the flow is metered by onsite detention ponding and an orifice controlled outlet. The majority of the flow passes thru a first flush pond that retains the required volume. The portions of the site that can not be captured results in a fee in lieu to be paid. The onsite storm drain and outfalls were designed to convey the flow. The ponds will overflow in an emergency or clogging situation via the emergency access roadway to the historical outfall at Second Street. The development of this site will not negatively impact the

5

upstream nor down stream facilities. Since the work area does exceed 1 acre, erosion and sediment Control Plan shall be required prior to any construction activity.

APPENDIX A

SITE HYDROLOGY

Method	et storage
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									i i i		100-Year, 6-hr			10-day
Basin	Area	Area	Treatment A	A	Treatment B	If B	Treatment C	ent C	Treatment D	lt D	Weighted E	Volume	Flow	Volume
	(js)	(acres)	%	(acres)	%	(acres)	%	(acres)	%	(acres)	(ac-ft)	(ac-ft)	cfs	(ac-ft)
EXISTING A(FROM REPORT)													2.66	
EXISTING B	22996	0.528	%0	0	0.0%	0.000	6.0%	6.0% 0.03167	94%	0.496	2.061	0.091	2.43	0.157
EXISTING C	57287	1.315	%0	0	0.0%	0.000	0.000 88.0%	1.15731	12%	0.158	1.249	0.137	4.38	0.158
PROPOSED A	32713	0.751	%Q	0	0.0%	0.000	6.0%	0.04506	94%	0.706	2.061	0.129	3.46	0.223
PROPOSED B	90905	2.087	%0	0	0.0%	0.000	3.0%	0.06261	97%	2.024	2.090	0.364	9.71	0.633
TOTALPROPOSED	123618	2.838								2.73		0.492	13.17	0.857
COMPARISON	-			0.000		0.000		1.112		-0.548		0.356	8.794	0.699

Equations:

Weighted E = Ea*Aa + Eb*Ab + Ee*Ac + Ed*Ad / (Total Area)

Volume = Weighted D * Total Area

Flow = Qa * Aa + Qb * Ab + Qc * Ac + Qd * Ad

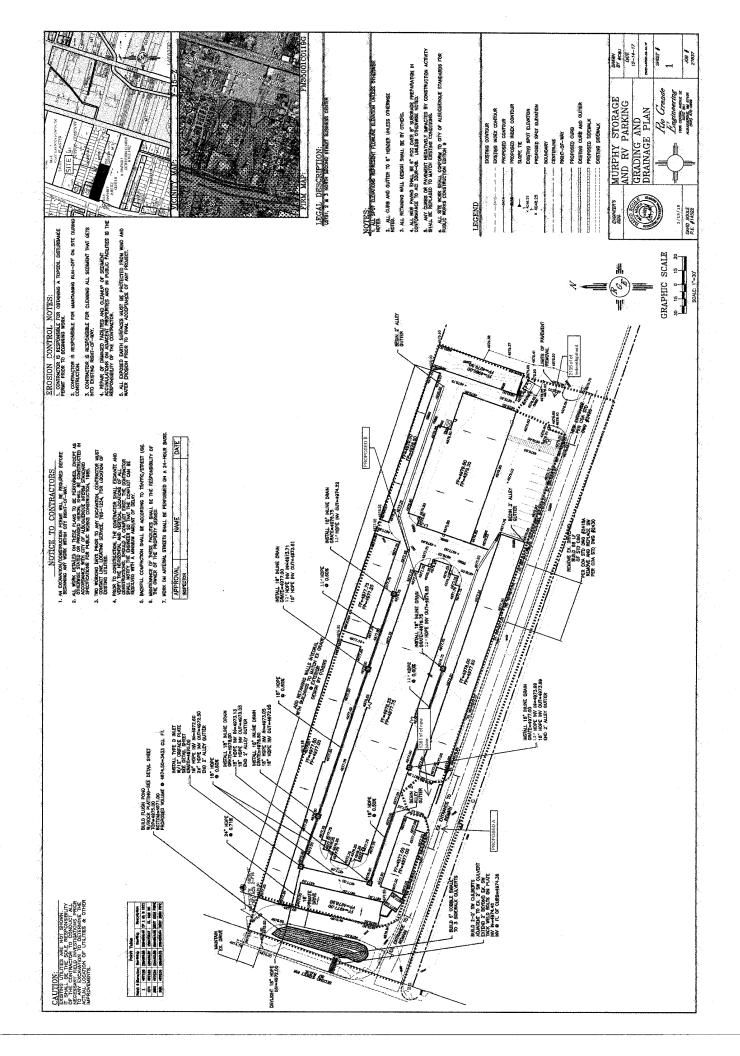
Where for 100-year, 6-hour storm (zone 2)						
Ear 0.53		Qa= 1.56				
Eb= 0.78		Qb= 2,28				
Ecr 1.13		Qc= 3.14				
Ed= 2.12		Qd= 4.7				U
	PEAK FL	PEAK FLOW	TOTAL D	SCHARGE	TOTAL DISCHARGE	
	100-YEA	R 6-HOUR	100-YEAF	2 6-HR	100-YEAR 10-DAY	
Existing	9.47	CFS	0.091	AC-FT	0.157 AC-FT	
Total discharge(PRIOR TO POND ROUTING)	13,17	GFS	0.492	AC-FT	0.857 AC-FT	
Discharge after pond routing	9,19	CFS	0.414	0.414 AC-FT	0.778 AC-FT	
water quality ponding required water rivelity nonding required		3369.629 cf				
fee in lieu volume for bypass	redev	47.55833 cf	ŝ	382		
	Men	39.12833 cf	x 8	314		

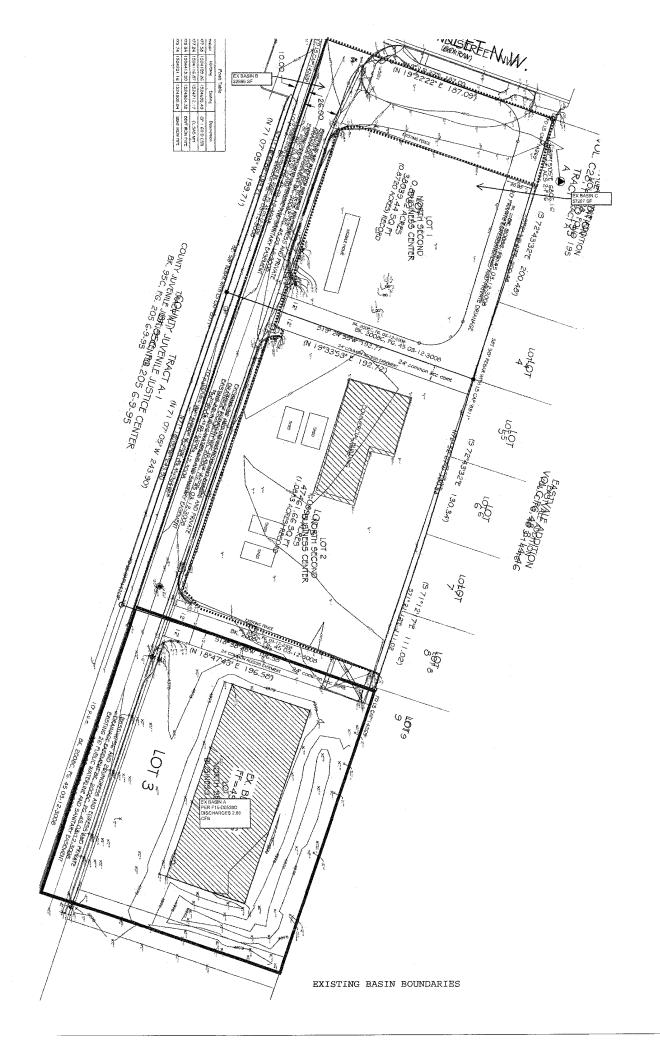
0.078810836

DRAINAGE NARRATIVE

This site is a repurposing of an existing site. The currently discharges to the private access road which conveys the flow to an single inlet located in second street at the southwest corner of the site. The proposed development will pond the increase in site discharge as compared to the existing. The flow will be collected by an onsite storm drain and discharge to second street directly upstream from the existing inlet. The flow will be collected by an onsite storm drain and discharge to second street directly upstream from the existing inlet. The flow will be solved by an onsite storm drain and discharge to second street directly upstream from the existing inlet. The flow will be solved by an existing and allowed by introducing an orifice plate to restrict the flow and the drive isles provide the required storage volume.

382 31**4** 696





OVERFLOW

Weir Equation:

$$Q = CLH^{3/2}$$

Q=13.17 cfs C = 2.95 H = 0.5 ft L = Length of weir

$$L = \frac{13.17}{2.95(0.5)^{3/2}}$$

L = 12.63 ft Use 13 feet for length of weir

APPENDIX B

HYDRAULIC MODELING AND CALCULATIONS

VOLUME CALCULATIONS

COMMONS POND

ACTUAL	DEPTH	AREA	VOLUME	VOLUME	VOLUME	Q
ELEV.	(FT)	SF	PER UNIT	CUMULATIVI	AC-FT	(CFS)
	0.00	0.0000				
73.50	0.00	340.0000	170.0000	170	0.004	0.00
76.00	2.50	360.0000	350.0000	520	0.012	5.02
76.50	3.00	400.0000	190.0000	710	0.016	5.50
76.75	3.25	3283.0000	460.3750	1170:375	0.027	5.73
77.00	3.75	7769.0000	1381.5000	2551.875	0:059	6.15
77.25	4.00	8640.0000	2051,1250	4603	0.106	6.36
	ELEV. 72.50 73.50 76.00 76.75 77.00	ELEV. (FT) 72.50 0.00 73.50 0.00 76.00 2.50 76.50 3.00 76.75 3.25 77.00 3.75	ELEV. (FI) SF 72.50 0.00 0.0000 73.50 0.00 340.0000 76.00 2.50 360.0000 76.50 3.00 400.0000 76.75 3.25 3283.0000 77.00 3.75 7769.0000	ELEV. (FT) SF PER UNIT 72.50 0.00 0.0000 170.0000 73.50 0.00 340.0000 170.0000 76.00 2.50 360.0000 350.0000 76.50 3.00 400.0000 190.0000 76.75 3.25 3283.0000 460.3750 77.00 3.75 7769.0000 1381.5000	ELEV. (FT) SF PER UNIT CUMULATIV} 72.50 0.00 0.0000 100 73.50 0.00 340.0000 170.0000 170 76.00 2.50 360.0000 350.0000 520 76.50 3.00 400.0000 190.0000 710 76.75 3.25 3283.0000 460.3750 1170.375 77.00 3.75 7769.0000 1381.5000 2551.875	ELEV. (FT) SF PER UNIT CUMULATIVI AC-FT 72.50 0.00 0.0000

POND OUT

Orifice Equation Q = CA SQRT(2gH)

C = 0.6 Diameter (in) Area (ft^2)= з**g** = H (Ft) = Q (CFS)= Flow

11 0.659952623 32.2 Depth of water above center of orifice *S AHYMO - DETENTION-NVALLEY STORAGE *S POND ROUTING

START TIME=0.0 PUNCH CODE=0

 RAINFALL
 TYPE=2 QUARTER=0.0
 ONE= 2.01 IN SIX=2.35 IN
 DAY= 2.75 IN
 DT = 0.05 HR

- COMPUTE NM HYD ID=1 HYD NO=101 DA= .003253 SQ MI PER A=0 PER B=0 PER C=03 PER D=97 TP=-.140 MASSRAIN=-1
- PRINT HYD ID=1 CODE=3

* ROUTE THE TOTAL	FLOW THROUGH THE	PROPOSED RESERV	DIR
ROUTE RESERVOIR		102 INFLOW=1	CODE=3
	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)
	0.00	0.004	73.50
	5.02	0.012	76.00
	5.50	0.016	76.50
	5.73	0.027	76.75
	6.15	0.059	77.00
6.	36 0.	106 77.2	5

FINISH

AHYMO.OUT

AHYMO PROGRAM (AHYMO-S4) RUN DATE (MON/DAY/YR) = 05/02/2018 START TIME (HR:MIN:SEC) = 16:00:01 RioGrandeSingleA41963517 INPUT FILE = tings\Owner\Desktop\2017 jobs\1732-abq north storage facility\pondrout031318.txt

*S *S	AHYMO - DETENTION-NVALLEY STORAGE POND ROUTING
START	TIME=0.0 RUNCH CODE=0
RATNEA	TYPE=2

RAINFALL	TYPE=2		
	QUARTER=0.0	ONE= 2.01 IN	
	SIX=2.35 IN	DAY= 2.75 IN	DT = 0.05 HR

2.41862.41992.42112.42232.42352.42472.42602.42722.42842.42962.43082.43202.43332.43452.43572.43692.43812.43932.44052.44172.44292.44412.44532.44652.44782.44902.45022.45142.45262.45382.45502.45612.45732.45852.45972.46092.46212.46332.46452.46572.46692.46812.46922.47042.47162.47282.47402.47522.4764	2.4858 2.4869 2.4881 2.4893 2.4905 2.4916 2.4928 2.4940 2.4951 2.4963 2.4975 2.4986 2.4998 2.5010 2.5021 2.5033 2.5044 2.5056 2.5068 2.5079 2.5091 2.5102 2.5114 2.5125 2.5137 2.5148 2.5160 2.5171 Page 1	0.2117 1.2021 2.0362 2.1722 2.2152 2.2363 2.2542 2.2697 2.2837 2.2965 2.3084 2.3195 2.3298 2.3396 2.3487 2.3576 2.3665 2.3753 2.3840 2.3927 2.4014 2.4101 2.4186 2.4272 2.4441 2.4526 2.4692 2.4692 2.4692 2.4692 2.4775 2.4858 2.4940 2.5021	0.2559 1.4666 2.0697 2.1803 2.2186 2.2391 2.2565 2.2717 2.2856 2.2983 2.3100 2.3210 2.3210 2.3500 2.3589 2.3677 2.3589 2.3677 2.3589 2.3677 2.3765 2.3853 2.3940 2.4027 2.4113 2.4199 2.4284 2.4284 2.44538 2.4538 2.4551 2.5033	0.3104 1.6752 2.1005 2.1879 2.2217 2.2417 2.2588 2.2738 2.2738 2.2738 2.2738 2.3778 2.3225 2.327 2.3422 2.3513 2.3601 2.3690 2.3778 2.3690 2.3778 2.3601 2.3690 2.3778 2.3690 2.3778 2.3601 2.3690 2.3778 2.3601 2.3690 2.3778 2.3422 2.3513 2.3601 2.3690 2.3778 2.3652 2.4296 2.4296 2.4799 2.4881 2.4963 2.5044 2.5125	0.3831 1.7800 2.1259 2.2247 2.2443 2.2611 2.2758 2.2893 2.3017 2.3133 2.3240 2.3341 2.3525 2.3614 2.3790 2.3790 2.3878 2.3790 2.3878 2.3965 2.4051 2.4137 2.4223 2.4308 2.4393 2.4478 2.4561 2.4561 2.4728 2.4728 2.4728 2.4893 2.4975 2.5056 2.5137	0.4649 1.8719 2.1418 2.2025 2.2278 2.2469 2.2633 2.2778 2.2911 2.3034 2.3148 2.3255 2.3449 2.3538 2.3627 2.3715 2.3803 2.3627 2.3715 2.3803 2.3977 2.4064 2.4150 2.4490 2.4490 2.4490 2.4490 2.4573 2.4657 2.4905 2.4986 2.5068	0.6062 1.9379 2.1530 2.2084 2.2307 2.2494 2.2654 2.2798 2.3051 2.3164 2.3269 2.3728 2.3639 2.3728 2.3639 2.3728 2.3639 2.3728 2.3815 2.3903 2.3728 2.3815 2.3903 2.3728 2.3815 2.3903 2.3728 2.3815 2.3903 2.3728 2.3815 2.3903 2.3728 2.3815 2.3639 2.3728 2.3815 2.3639 2.3728 2.3815 2.3639 2.3728 2.38452 2.4565 2.4462 2.4585 2.4585 2.4585 2.4834 2.4916 2.5079	0.8258 1.9905 2.1629 2.2118 2.2336 2.2518 2.2518 2.2518 2.2948 2.3068 2.3180 2.3284 2.3382 2.3474 2.3563 2.3652 2.3740 2.3828 2.3740 2.3828 2.3740 2.3828 2.3740 2.3828 2.3740 2.4002 2.4088 2.4174 2.4260 2.4429 2.44514 2.4597 2.4681 2.4928 2.5010 2.5091
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.2021 2.0362 2.1722 2.2152 2.2363	1.4666 2.0697 2.1803 2.2186 2.2391	1.6752 2.1005 2.1879 2.2217 2.2417	1.7800 2.1259 2.1953 2.2247 2.2443	1.8719 2.1418 2.2025 2.2278 2.2469	1.9379 2.1530 2.2084 2.2307 2.2494	1.9905 2.1629 2.2118 2.2336 2.2518
2.3576 2.3589 2.3601 2.3614 2.3627 2.3639 2.3652 2.3665 2.3677 2.3690 2.3702 2.3715 2.3728 2.3740 2.3753 2.3765 2.3778 2.3790 2.3803 2.3815 2.3828 2.3840 2.3853 2.3865 2.3878 2.3890 2.3903 2.3915 2.3927 2.3940 2.3952 2.3965 2.3977 2.3989 2.4002 2.4014 2.4027 2.4039 2.4051 2.4064 2.4076 2.4088	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.2697 2.2837 2.2965 2.3084 2.3195 2.3298 2.3396	2.2717 2.2856 2.2983 2.3100 2.3210 2.3313 2.3409	2.2738 2.2874 2.3000 2.3117 2.3225 2.3327 2.3422	2.2758 2.2893 2.3017 2.3133 2.3240 2.3341 2.3436	2.2778 2.2911 2.3034 2.3148 2.3255 2.3355 2.3449	2.2798 2.2930 2.3051 2.3164 2.3269 2.3368 2.3462	2.2817 2.2948 2.3068 2.3180 2.3284 2.3382 2.3474
	2.41862.41992.42112.42232.42352.42472.42602.42722.42842.42962.43082.43202.43332.43452.43572.43692.43812.43932.44052.44172.44292.44412.44532.44652.44782.44902.45022.45142.45262.45382.45502.45612.45732.45852.45972.46092.46212.46332.46452.46572.46692.46812.46922.47042.47162.47282.47402.47522.4764	2.3576 2.3665 2.3753 2.3840 2.3927 2.4014	2.3589 2.3677 2.3765 2.3853 2.3940 2.4027	2.3601 2.3690 2.3778 2.3865 2.3952 2.4039	2.3614 2.3702 2.3790 2.3878 2.3965 2.4051	2.3627 2.3715 2.3803 2.3890 2.3977 2.4064	2.3639 2.3728 2.3815 2.3903 2.3989 2.4076	2.3652 2.3740 2.3828 2.3915 2.4002 2.4088

			AHYMO.	JUT			
	2.5183 2.5263 2.5343 2.5263 2.5579 2.5579 2.5657 2.5735 2.5812 2.5889 2.6040 2.6116 2.6191 2.6265 2.6339 2.6486 2.6558 2.6630 2.6774 2.6844 2.6558 2.6630 2.6774 2.6844 2.6915 2.6985 2.7054 2.7192 2.7260 2.729	2.5194 2.5274 2.5354 2.5590 2.5590 2.5668 2.5590 2.5668 2.5746 2.5823 2.5976 2.6051 2.6276 2.6276 2.6276 2.6423 2.6496 2.6569 2.6441 2.6569 2.6496 2.6569 2.6496 2.6569 2.6496 2.6784 2.6784 2.6925 2.6995 2.72064 2.7202 2.7270 2.7238	AHYMO. (2.5206 2.5286 2.5365 2.5445 2.5523 2.5602 2.5679 2.5757 2.5834 2.5910 2.5986 2.6062 2.6137 2.6212 2.6286 2.6360 2.6433 2.6579 2.6651 2.6723 2.6794 2.6651 2.6794 2.6865 2.6935 2.7005 2.7074 2.7211 2.7280 2.7280	2.5217 2.5297 2.5377 2.5456 2.5535 2.5613 2.5691 2.5768 2.5921 2.5997 2.6073 2.6148 2.6223 2.6297 2.6244 2.6273 2.6297 2.6371 2.6444 2.6517 2.6589 2.66661 2.6733 2.6804 2.6875 2.6945 2.7015 2.7084 2.7221 2.7289	2.6233 2.6307 2.6381 2.6454 2.6527 2.6600 2.6672 2.6743 2.6814 2.6885 2.6955 2.7025 2.7025 2.7094 2.7163 2.7231 2.7299	2.6244 2.6318 2.6392 2.6465 2.6538 2.6610 2.6682 2.6753 2.6824 2.6895 2.6895 2.6965 2.7034 2.7104 2.7172 2.7241 2.7309	2.6105 2.6180 2.6254 2.6328 2.6402 2.6475 2.6548 2.6620 2.6692 2.6763 2.6905 2.6975 2.7044 2.7114 2.7182 2.7250 2.7318
	2.7328	2.7338	2.7347	2.7357	2.7366	2.7376	2.7386
	2.7395 2.7462	2.7405 2.7472	2.7414 2.7481	2.7424 2.7491	2.7433 2.7500	2.7443	2.7452
COMPUTE NM HYD		HYD NO A=0 PER		= .00325 _C=03 P	3 SQ MI ER D=97		

TP=-.140 MASSRAIN=-1

K = 0.076300HRCONSTANT, N = 7.106428 TP = 0.140000HR K/TP RATIO = 0.545000 SHAPE UNIT PEAK = 11.862 CFS UNIT VOLUME = 0.9975 B = 526.28 P60 = 2.01000.003155 SQ MI IA = 0.10000 INCHES INF = 0.04000 AREA =INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

K = 0.112846HR TP = 0.140000HR K/TP RATIO = 0.806046 SHAPE CONSTANT, N = 4.440407 UNIT PEAK = 0.26735 CFS UNIT VOLUME = 0.9581383.54 B = P60 = 2.0100ARĚA = 0.000098 SQ MI IA = 0.35000 INCHES INF = 0.83000 INCHES PER HOUR RUNOFF COMPUTED BY INITIAL ABSTRACTION/INFILTRATION NUMBER METHOD - DT = 0.050000

PRINT HYD ID=1 CODE=3

PARTIAL HYDROGRAPH 101.00

TIME	FLOW	TIME FLOW	TIME	FLOW
		Page 2		

			AHYMO	.OUT		
TIME	FLOW HRS	TIME	FLOW HRS	CES	HRS	CFS
HRS	CFS 0.000	HRS 0.0	CFS 4.950	0.0	9.900	0.0
14.850	0.0 0.150	19.800 0.0	0.0 5.100	0.0	10.050	0.1
15.000	0.0 0.300	19.950	0.0 5.250	0.0	10.200	0.0
15.150	0.0 0.450	20.100 0.0	0.0 5.400	0.0	10.350	0.0
15.300	0.0 0.600	20.250	0.0 5.550	0.0	10.500	0.0
15.450	0.0	20.400 0.0	0.0 5.700	0.0	10.650	0.0
15.600	0.0 0.900	20.550 0.1	0.0 5.850	0.0	10.800	0.0
15.750	0.0	20.700 0.6	0.0 6.000	0.0	10.950	0.0
15.900	0.0	20.850	0.0 6.150	0.1	11.100	0.0
16.050	0.0 1.350	21.000 3.4	0.0 6.300	0.1	11.250	0.0
16.200	0.0 1.500	21.150 9.7	0.0 6.450	0.1	11.400	0.0
16.350	0.0 1.650	21.300 6.1	0.0 6.600	0.1	11.550	0.0
16.500	0.0 1.800	21.450 3.1	0.00 6.750	0.1	11.700	0.0
16.650	0.0 1.950	21.600 1.8	0.0	0.1	11.850	0.0
16.800	1.990 0.0 2.100	^{1.0} 21.750 0.9	0.0 7.050		12.000	0.0
16.950	0.0	0.9 21.900 0.5	0.0 7.200	0.1 0.1	12.150	0.0
17.100	2.250	22.050	0.0	0.1	12.130	0.0
17.250	2.400	0.4 22.200	7.350 0.0	0.1	12.300	0.0
17.400	2.550	0.2 22.350 0.1	7.500	0.1	12.430	0.0
17.550	2.700	22.500	7.650			
17.700	2.850	0.1 22.650	7.800	0.1	12.750	0.0
17.850	3.000	0.0 22.800	7.950	0.1	12.900	0.0
18.000	3.150 0.0	0.0 22.950	$\begin{array}{r} 8.100 \\ 0.0 \end{array}$	0.1	13.050	0.0
18.150	3.300 0.0	0.0 23.100	8.250 0.0	0.1	13.200	0.0
18.300	3.450 0.0	0.0 23.250	8.400 0.0	0.0	13.350	0.0
18.450	3.600 0.0	0.0 23.400	8.550 0.0	0.0	13.500	0.0
18.600	3.750 0.0	0.0 23.550	8.700 0.0	0.1	13.650	0.0
18.750	3.900 0.0	0.0 23.700	8.850 0.0	0.1	13.800	0.0
18.900	4.050	0.0 23.850	9.000 0.0	0.0	13.950	0.0
19.050	4.200	0.0 24.000	9.150 0.0	0.1	14.100	0.0
19.200	4.350 0.0	0.0 24.150	9.300 0.0	0.0	14.250	0.0
			Pag	e 3		

Page 3

			AHYMO.	OUT		
	4.500	0.0	9.450	0.1	14.400	0.0
19.350		24.300	0.0		at a statement	
10 - 500	4.650	0.0	9.600	0.0	14.550	0.0
19.500	0.0 4.800	24.450 0.0	0.0 9.750	0.0	14.700	0.0
19.650	0.0	24.600	0.0			
	RUNOFF VOL	UME = 2.460	628 INCHES	_	0.4279 ACRI	-FFFT
0 0000		ARGE RATE =	9.70 CFS	S AT		BASIN AREA =

0.0033 SQ. MI.

* ROUTE THE TOTAL				
ROUTE RESERVOIR		102 INFLOW=1		
	OUTFLOW(CFS)	STORAGE(AC-FT)	ELEV(FT)	
	0.00	0.004	73.50	
	5.02	0.012	76.00	
		5.73	0.027	76.75
C	0.059	77.00		

6.

*

TIME (HRS)INFLOW (CFS)ELEV (FEET)VOLUME (AC-FT)OUTFLOW (CFS) 0.00 0.00 73.50 0.004 0.00 0.15 0.00 73.50 0.004 0.00 0.30 0.00 73.50 0.004 0.00 0.45 0.00 73.50 0.004 0.00 0.60 0.00 73.50 0.004 0.00 0.60 0.00 73.50 0.004 0.00 0.60 0.00 73.50 0.004 0.00 0.75 0.00 73.52 0.004 0.00 0.90 0.07 73.52 0.004 0.04 1.05 0.63 73.77 0.005 0.53 1.20 1.48 74.18 0.009 2.98 1.50 9.70 76.75 0.027 5.73 1.65 6.12 76.75 0.027 5.73 1.80 3.10 76.75 0.027 5.73 1.95 1.83 75.66 0.011 4.34 2.10 0.94 74.01 0.006 1.03 2.25 0.54 73.79 0.005 0.58 2.40 0.35 73.69 0.004 0.119 2.70 0.10 73.55 0.004 0.112 2.85 0.06 73.53 0.004 0.07 3.00 0.02 73.51 0.004 0.02 3.30 0.02 73.51 0.004 0.02	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							-				_					
3.60 0.02 73.51 0.004 0.02 3.75 0.02 73.51 0.004 0.02 Page 4	0. 0. 0. 0. 0. 1. 1. 1. 1. 1. 1. 2. 2. 2. 2. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.	15 346079050235056805015050 2350568050205015050 12050235056805015050 130500505050 130500505050 130500505050 130500505050 1305005050 13050050050 13050050050 13050050050050 13050050000000000			0.00.00.00.00.00.00.00.00.00.00.00.00.0	000007387020344570643222	9 	73. 73. 73. 73. 73. 73. 73. 73. 74. 76. 75. 73. 73. 73. 73. 73. 73. 73. 73. 73. 73	50055577197556199055322111			.00 .00 .00 .00 .00 .00 .00 .00 .00 .00	444444456977716554444444444444		0.0000000000000000000000000000000000000	00 00 00 00 00 04 53 37 98 73 73 34 03 58 11 07 04 03 02 02 02

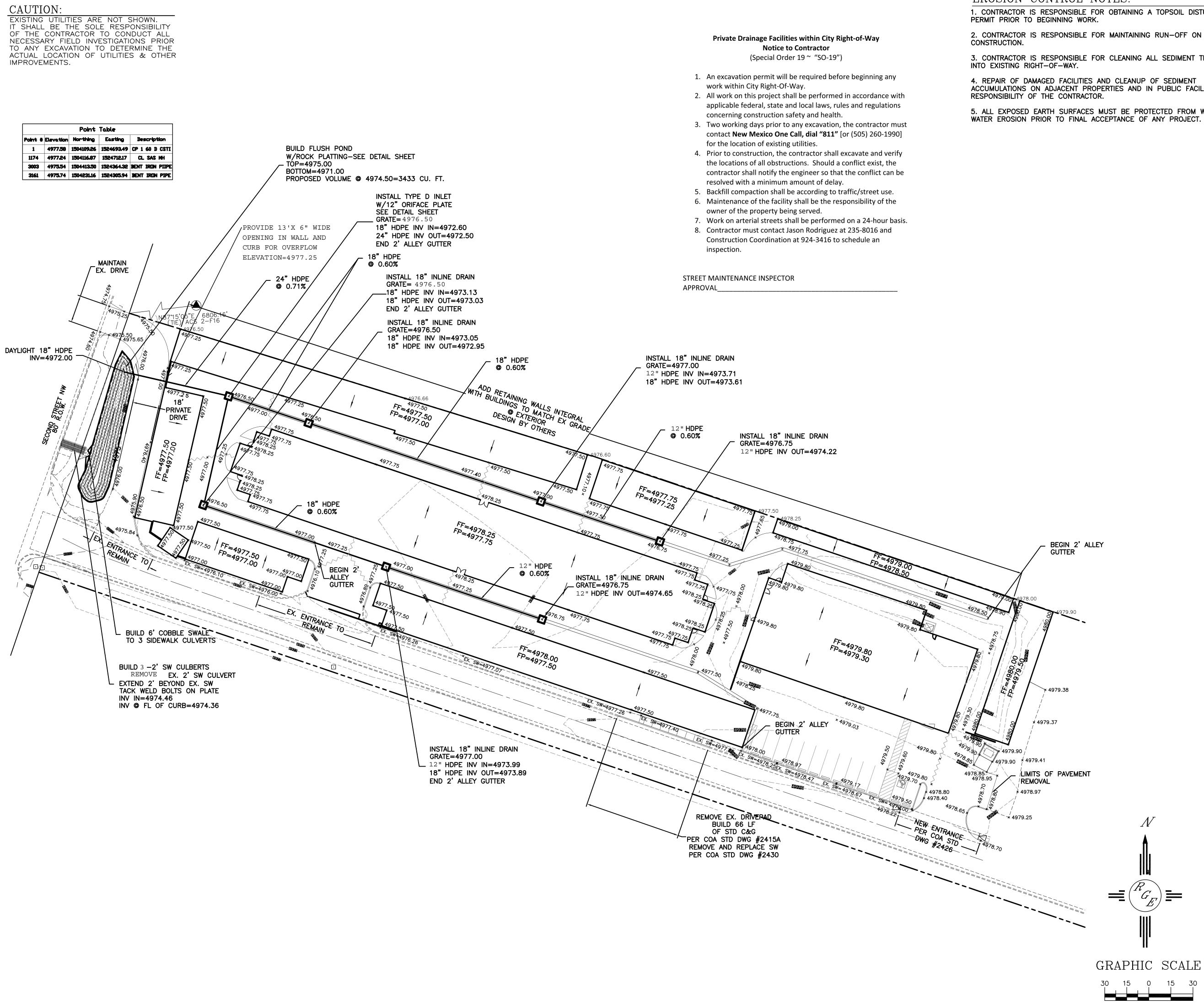
3.90 4.05 4.20 4.35 4.50 4.65 4.80 4.95 5.10 5.25 5.40 5.55 5.70 5.85 6.00 6.15 6.30 6.15 6.30 6.45 6.60 6.75 6.90 7.05 7.20 7.35 7.50 7.95 8.10 8.25	0.02 0.02 0.02 0.03 0.03 0.03 0.03 0.03 0.04 0.04 0.04 0.04 0.04 0.05	73.51 73.51 73.51 73.51 73.51 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.53 7	AHYMO.OUT 0.004	0.02 0.02 0.02 0.03 0.03 0.03 0.03 0.03 0.04 0.04 0.04 0.04 0.04 0.04 0.05	
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)	
8.40 8.55 8.70 9.00 9.15 9.30 9.45 9.60 9.75 9.90 10.05 10.20 10.35 10.50 10.65 10.80 10.65 10.80 10.95 11.10 11.25 11.40 11.55 11.70 11.85 12.00 12.15 12.60	$\begin{array}{c} 0.05\\$	73.52 7	0.004 0.004	$\begin{array}{c} 0.05\\$	

$12.75 \\ 12.90 \\ 13.05 \\ 13.20 \\ 13.35 \\ 13.50 \\ 13.65 \\ 13.80 \\ 13.95 \\ 14.10 \\ 14.25 \\ 14.40 \\ 14.25 \\ 14.40 \\ 14.55 \\ 14.70 \\ 14.85 \\ 15.00 \\ 15.15 \\ 15.30 \\ 15.45 \\ 15.60 \\ 15.75 \\ 15.90 \\ 16.05 \\ 16.20 \\ 16.35 \\ 16.50 \\ 16.65 \\ 16.6$	0.05 0.04 0.04	73.52 7	AHYMO.OUT 0.004	0.05 0.04 0.04 0.04 0.04 0.04 0.04 0.04	
TIME (HRS)	INFLOW (CFS)	ELEV (FEET)	VOLUME (AC-FT)	OUTFLOW (CFS)	
$16.80 \\ 16.95 \\ 17.10 \\ 17.25 \\ 17.40 \\ 17.55 \\ 17.70 \\ 17.85 \\ 18.00 \\ 18.15 \\ 18.30 \\ 18.45 \\ 18.60 \\ 18.75 \\ 18.90 \\ 19.05 \\ 19.20 \\ 19.05 \\ 19.20 \\ 19.35 \\ 19.50 \\ 19.65 \\ 19.80 \\ 19.95 \\ 20.10 \\ 20.25 \\ 20.40 \\ 20.55 \\ 20.40 \\ 20.55 \\ 20.70 \\ 20.85 \\ 21.00 \\ 21.15 \\ 21.30 \\ 21.45 \\ 1.00 \\ 1.00 \\$	$\begin{array}{c} 0.04\\$	73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73.52 73	0.004 0.004	0.04 0.04	

			AHYMO.OUT		
21.60	0.04	73.52	0.004	0.04	
21.75	0.04	73.52	0.004	0.04	
21.90	0.04	73.52	0.004	0.04	
22.05	0.04	73.52	0.004		
22.20	0.04	73.52	0.004	0.04	
22.35	0.04	73.52	0.004	0.04	
22.50	0.04	73.52	0.004	0.04	
22.65	0.04	73.52	0.004		
22.80	0.04	73.52		0.04	
			0.004	0.04	
22.95	0.04	73.52	0.004	0.04	
23.10	0.04	73.52	0.004	0.04	
23.25	0.04	73.52	0.004	0.04	
23.40	0.04	73.52	0.004	0.04	
23.55	0.04	73.52	0.004	0.04	
23.70	0.04		0.004	0.04	
23.85	0.04	73.52	0.004	0.04	
24.00	0.04	73.52	0.004	0.04	
24.15	0.02	73.51	0.004	0.02	
24.30	0.01	73.50	0.004	0.01	
24.45	0.00	73.50	0.004	0.00	
PEAK DISCHAR				CCURS AT HOUR	L.50
MAXIMUM WATE			= 76	. 750	
MAXIMUM STOR		0.0270		INCREMENTAL TIME	= 0.050000HRS
					3. 23 00 00 mmB

FINISH

NORMAL PROGRAM FINISH END TIME (HR:MIN:SEC) = 16:00:01



EROSION CONTROL

OL NOTES: SIBLE FOR OBTAINING A TOPSOIL DISTURBANCE WORK.		SP-79336 SU-1 A POLICE SUBSTATION & CENTRAL FAC LATH & PLASTER	
SIBLE FOR MAINTAINING RUN-OFF ON SITE DURIN		SITE M-1 SUPPDY COMPANY	87.2 85 87.2 87.2 M-1 255
SIBLE FOR CLEANING ALL SEDIMENT THAT GETS		CS STORING THASTVALE CS CS A CS A CS A A CS A A CS A A CS A A A CS A A A A A A A A A A A A A	С <u>997997</u> <u>9078576</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u> <u>1071</u>
ILITIES AND CLEANUP OF SEDIMENT NT PROPERTIES AND IN PUBLIC FACILITIES IS THE ITRACTOR.	SU-1 JUVENILE JUSTICE CENTER	ADDN DESS CENTER 1004010 / A / 32 CENTER 1004010 / A / 32 CENTER 1004010 / A / 32 CENTER 1004010 / A / 32 SP po 200	01 1011 001 001 001 001 001 001 001 001
	VICINITY SAVE FIRM MAP		AA AA AA AA AA AA AA AA AA AA AA AA AA
	TES:		
1. AI NOTE	LL SPOT ELEVATIONS I D.	REPRESENT FLOWLINE ELEVATION UNLI	ESS OTHERWISE
NOTE		R TO 6" HEADER UNLESS OTHERWISE	
2' ALLEY R 3. A	LL RETAINING WALL DE	ESIGN SHALL BE BY OTHERS.	
		BE 6" PCC OVER 8" SUBGRADE PRI 0R-08. UNLESS OTHERWISE NOTED.	EPARATION IN
5.	ANY CURBS OR PAVE	EMENT NEGATIVELY IMPACTED BY CON	ISTRUCTION ACTIVITY
90 6. /		MATCH EXISTING CONDITIONS. . CONFORM TO CITY OF ALBUQUERQUI TION EDITION 9	E STANDARDS FOR
LE	GEND		
		EXISTING CONTOUR	
		EXISTING INDEX CONTOUR	
	5414 5415	PROPOSED CONTOUR 	
	•	SLOPE TIE	
	1 × 4048.25 1•	EXISTING SPOT ELEVATION	
EMENT	× 4048.25 •	PROPOSED SPOT ELEVATION	
		BOUNDARY CENTERLINE	
\mathcal{N} —		PROPOSED CURB	

	RIGHT-OF-WAY	(
	PROPOSED CU	RB	
	EXISTING CURE	3 AND GUTTER	
	PROPOSED SID	DEWALK	
	EXISTING SIDE	NALK	
ENGINEER'S SEAL	MURPHY S	TORAGE	DRAWN BY _{WCWJ}
ON W METCOLM	GRADING A	ND	DATE 12-14-17
RECSTREESSIONING BEING	DRAINAGE		21837-LAYOUT-12-14-17
		Rio Grande	SHEET # 1
6/8/18 5/17/18		<i>Engineering</i> 1606 central avenue se	Ţ
AVID SOULE P.E. #14522		SUITE 201 ALBUQUERQUE, NM 87106 (505) 872–0999	JOB # 21837

SCALE: 1"=30'