

DRAINAGE REPORT

for

Bob Turner Ford

Prepared by

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Albuquerque, New Mexico 87109

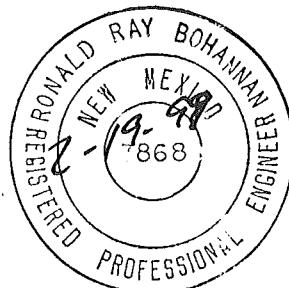
Prepared for

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February 1999



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Location

Bob Turner Ford is located at the northwest corner of Montano and Renaissance Boulevard. It is the proposed location of a car dealership and service shop. The site is identified as Tract 1C of the North Renaissance Center and contains approximately 12.22 acres. The purpose of this report is to provide the drainage analysis and management plan for the subdivision.

Existing Drainage Conditions

The site is currently undeveloped. The runoff from the site sheet flows from east to west. There is a temporary desilting pond located in the southwest corner of the site. Runoff from the site enters the desilting pond and then overflows to an existing concrete rundown located on the west side of the site. The concrete rundown drains to the existing Montano Detention Pond. There are no offsite flows entering the site from the south or the east as Montano and Renaissance Boulevards capture any flows from those directions. The natural topography of the site prevents any flows from entering the site from the west. The north side of the site will have a berm and temporary detention pond to divert any offsite flows from entering the site. When the site to the north is developed the detention pond will be removed.

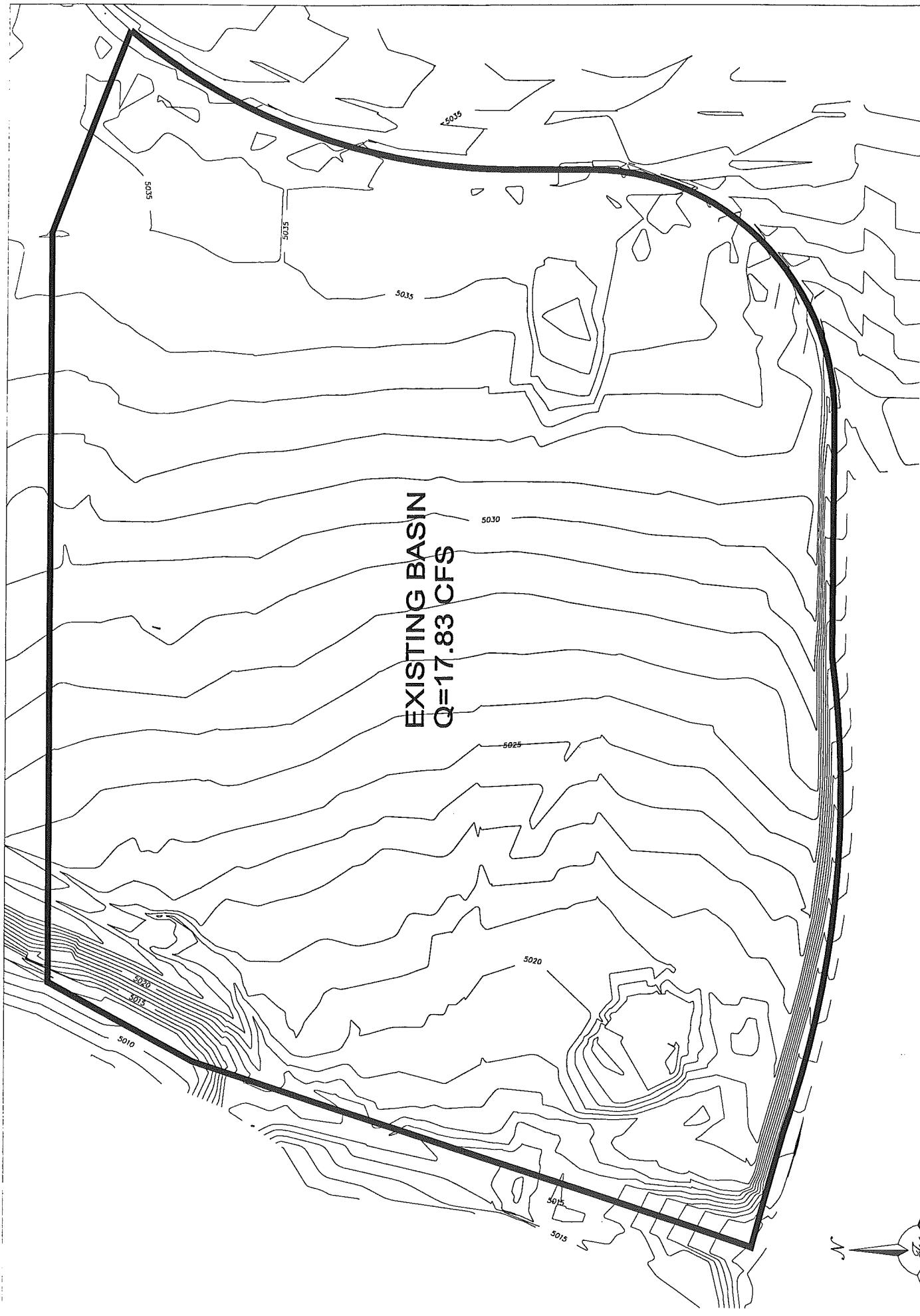
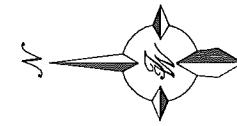
FEMA Map and Soil Conditions

The site is located on FIRM Map 35001C0138 D as shown on the attached excerpt. The map shows that the site does not lie within any 100 year flood plains.

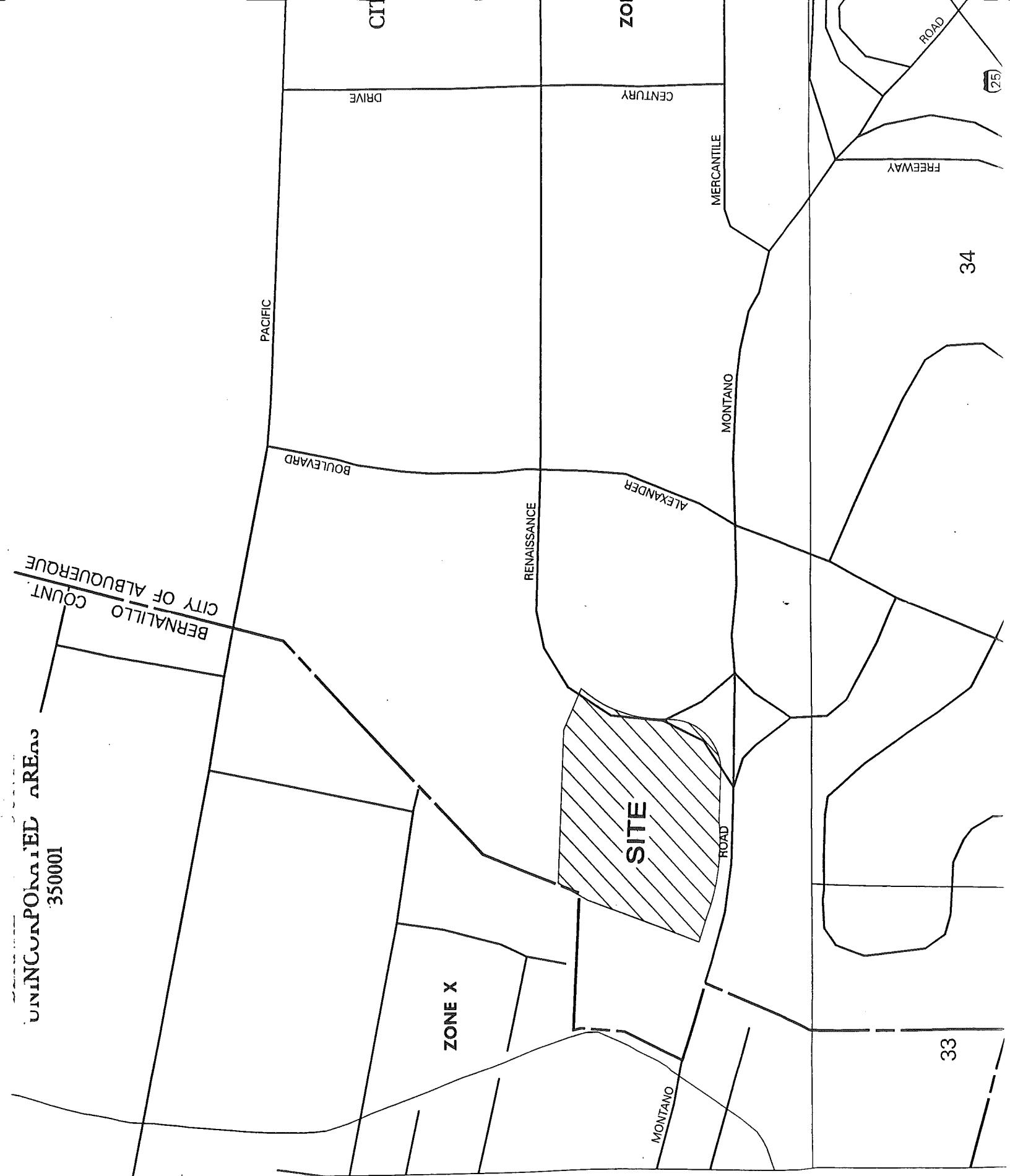
The site contains one soil type from the Soil Conservation Service Soil Survey of Bernalillo County. The soil is a Bluepoint-Kokan Association which is a loamy fine sand that has slow runoff, rapid permeability, and a moderate to severe hazard of water erosion.

UNDEVELOPED BASIN LAYOUT

EXISTING BASIN
 $Q=17.83 \text{ CFS}$



UNINCORPORATED AREA
350001



FEMA MAP 35001C0138

On-Site Drainage Management Plan

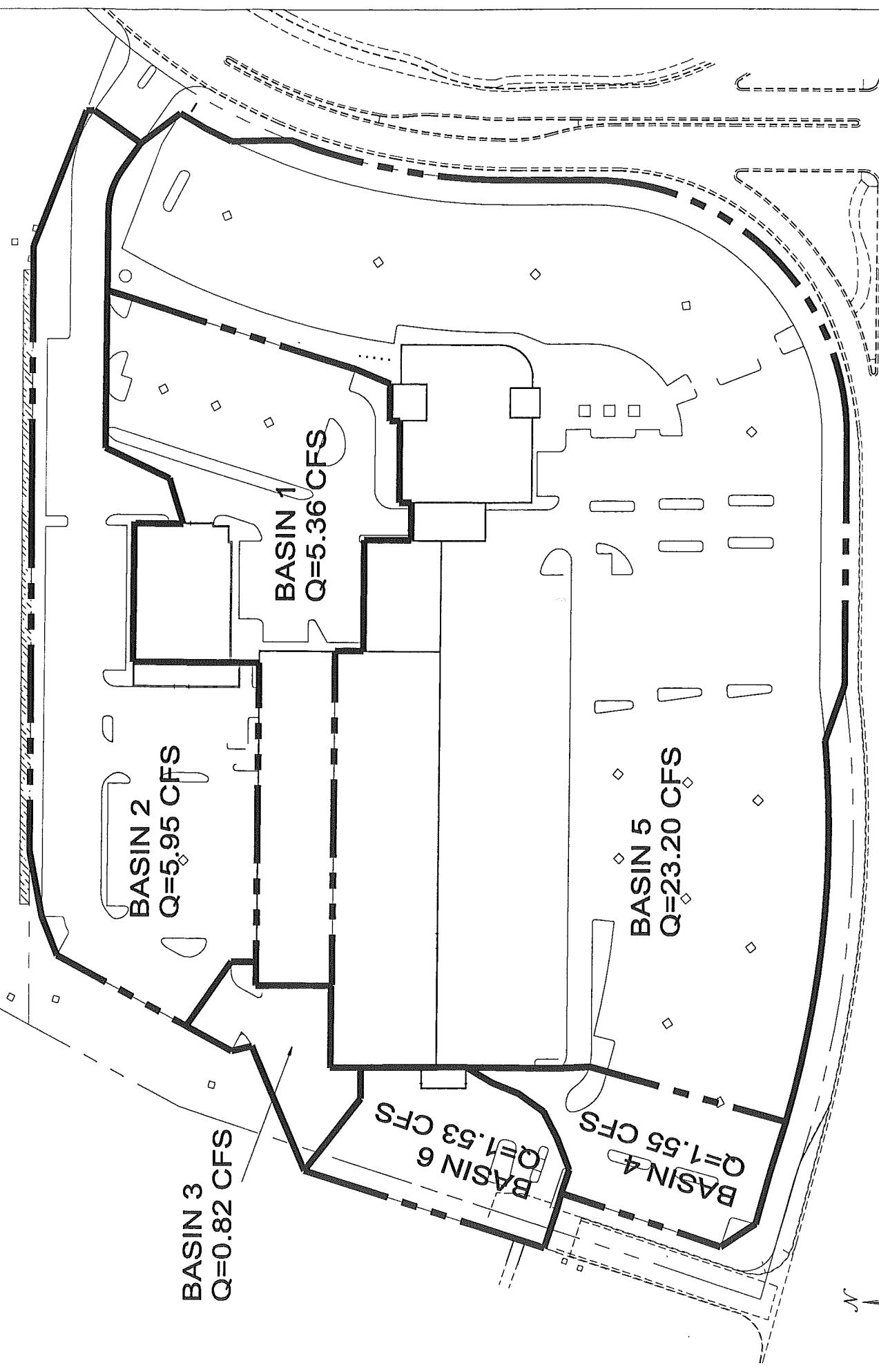
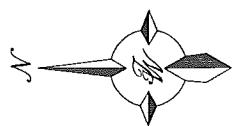
The site is located in the Renaissance Center and must follow the guidelines of the Renaissance Master Drainage Plan. The site is allowed to discharge 0.1 cfs per acre. There are approximately 11.09 acres discharging to the existing storm drain system. This is an allowable discharge of 1.11 cfs.

There are six proposed basins on the site. Five of the basins will drain to parking lot ponds and the drainage will be released at controlled discharge rates. The runoff will be conveyed via a new storm drain system to an existing 84" storm drain line. The existing 84" line will carry the runoff to the existing Montano Detention Pond. Basin 6 will continue the existing drainage pattern and drain to the Montano Detention Pond via an existing concrete rundown located on the west side of the site.

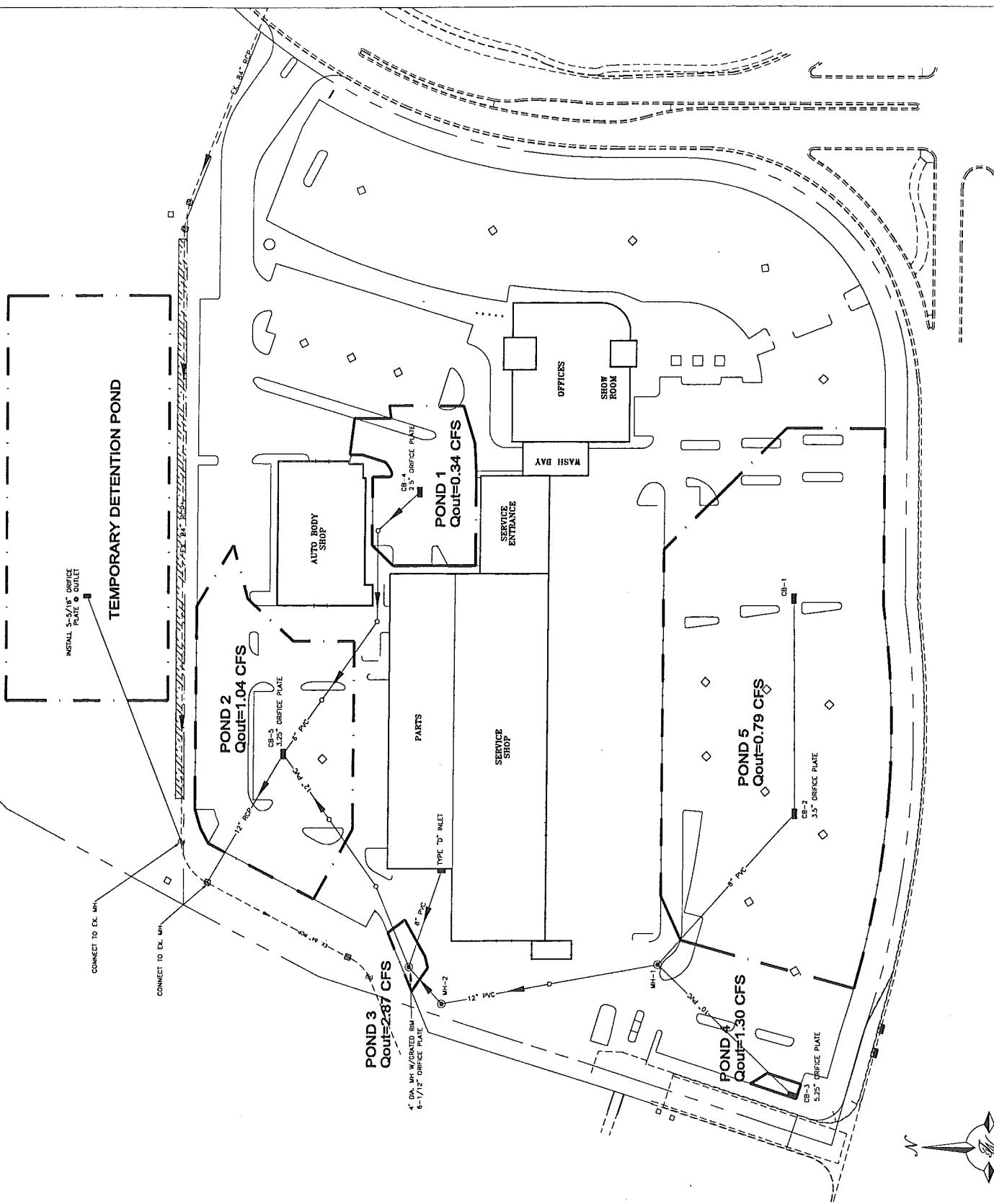
The proposed on-site storm drain system will convey the allowable discharge rate to the existing 84" storm drain. Basin 1 has a developed discharge rate of 5.36 cfs. This basin will drain to a parking lot pond (Pond 1) that will limit the runoff with a 2.5" orifice plate to 0.34 cfs. Basin 5 has a developed discharge rate of 23.20 cfs and will drain to Pond 5. This pond will control the discharge to 0.79 cfs with a 3.5" orifice plate. The developed discharge rate of 1.55 cfs for Basin 4 will drain to Pond 4. The discharge from the pond will be released at a rate of 1.3 cfs via a 5.25" orifice plate. Pond 5 and Pond 4 will both drain to Pond 3. Basin 3, with a discharge rate of 1.53 cfs, also drains to Pond 3. A 6-1/12" orifice plate will limit the flow from the pond to 2.87 cfs. Pond 3 drains to Pond 2. Basin 2 also drains to Pond 2 with a developed discharge rate of 5.95 cfs. Pond 2 limits the flow leaving the site to 1.04 cfs via a 3.25" orifice plate. The site is designed to discharge 1.04 cfs which is less than the allowable discharge of 1.11 cfs.

There is a temporary detention pond located north of the site. This pond will capture the flows entering the site from Tract 1B of the North Renaissance Center. The pond will limit the

DEVELOPED BASIN LAYOUT



PROPOSED POND LAYOUT



release to the allowable 0.1 cfs/acre. The tract contains approximately 10.03 acres. This is an allowable discharge rate of 1.00 cfs. The pond will discharge 0.93 cfs which is less than the 1.00 cfs allowed. The pond will also act as a parking area for the Bob Turner Ford site.

Summary

There are six proposed basins on the site. Five of the proposed basins drain to parking lot ponds and a proposed storm drain system that will limit the flows to the allowable discharge rate. The sixth basin consists of the entrance to the site and will drain west via an existing concrete rundown to the Montano Detention Pond.

RUNOFF CALCULATIONS

The site is @ Zone 2

LAND TREATMENT

Proposed

B = 90%

D = 10 %

Existing

B = 100%

DEPTH (INCHES) @ 100-YEAR STORM

$$P_{60} = 2.01 \text{ inches}$$

$$P_{360} = 2.35 \text{ inches}$$

$$P_{1440} = 2.75 \text{ inches}$$

DEPTH (INCHES) @ 10-YEAR STORM

$$\begin{aligned} P_{60} &= 2.01 \times 0.667 \\ &= 1.34 \text{ inches} \end{aligned}$$

$$P_{360} = 1.57$$

$$P_{1440} = 1.83$$

Drainage Basins

Undeveloped

BASIN	AREA (SF)	AREA (AC)	AREA (MI ²)
1	532174.41	12.2170	0.019089

Proposed

BASIN	AREA (SF)	AREA (AC)	AREA (MI ²)
1	69928.25	1.6053	0.002508
2	77687.12	1.7835	0.002787
3	10531.80	0.2418	0.000378
4	19955.36	0.4581	0.000716
5	303870.56	6.9759	0.010900
6	19799.54	0.4545	0.000710
Total	501772.63	11.5191	0.017999

Runoff Calculation Results

Undeveloped

BASIN	Q-100 CFS	Q-10 CFS	V-100 AC-FT	V-10 AC-FT
1	17.83	10.63	0.792	0.455

Proposed

BASIN	Q-100 CFS	Q-10 CFS	V-100 AC-FT	V-10 AC-FT
1	5.36	3.95	0.305	0.208
2	5.95	4.39	0.338	0.231
3	0.82	0.61	0.046	0.031
4	1.55	1.14	0.087	0.059
5	23.20	17.13	1.323	0.905
6	1.53	1.13	0.086	0.059
Total	38.41	28.35	2.185	1.493

VOLUME CALCULATIONS

POND 1

Ab - Bottom Of The Pond Surface Area
At - Top Of The Pond Surface Area
D - Water Depth
Dt - Total Pond Depth
C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 6.80$$

$$\text{At} = 13,851.28$$

$$\text{Dt} = 1.38$$

$$\text{C} = 10032.23$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
24.55	0	0	0.000
27.50	2.95	0.0005	0.277
27.70	3.15	0.0051	0.286
27.90	3.35	0.0189	0.296
28.10	3.55	0.0420	0.305
28.30	3.75	0.0743	0.313
28.50	3.95	0.1158	0.322
28.70	4.15	0.1665	0.330
28.88	4.33	0.2200	0.337

Orifice Equation

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$\text{Diameter (in)} \quad 2.5$$

$$\text{Area (ft}^2\text{)} = 0.034088$$

$$g = 32.2$$

$$H (\text{Ft}) = \text{Depth of water above center of orifice}$$

$$Q (\text{CFS}) = \text{Flow}$$

VOLUME CALCULATIONS

POND 2

Ab - Bottom Of The Pond Surface Area
At - Top Of The Pond Surface Area
D - Water Depth
Dt - Total Pond Depth
C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 6.80$$

$$\text{At} = 32,989.54$$

$$\text{Dt} = 1.50$$

$$\text{C} = 21988.49$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
13.85	0	0	0.000
26.50	12.65	0.0020	0.981
26.70	12.85	0.0121	0.989
26.90	13.05	0.0424	0.997
27.10	13.25	0.0929	1.005
27.30	13.45	0.1636	1.012
27.50	13.65	0.2545	1.020
27.70	13.85	0.3656	1.027
27.90	14.05	0.4969	1.035
28.00	14.15	0.5701	1.038

Orifice Equation

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$\text{Diameter (in)} \quad 3.25$$

$$\text{Area (ft}^2\text{)} = 0.05761$$

$$g = 32.2$$

H (Ft) = Depth of water above center of orifice

Q (CFS) = Flow

VOLUME CALCULATIONS

POND 3

Ab - Bottom Of The Pond Surface Area
 At - Top Of The Pond Surface Area
 D - Water Depth
 Dt - Total Pond Depth
 C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 2.82$$

$$\text{At} = 1,176.39$$

$$\text{Dt} = 0.68$$

$$\text{C} = 1725.84$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
15.3	0	0	0.0000
26.04	10.74	0.0007	3.1472
26.14	10.84	0.0009	3.1621
26.24	10.94	0.0015	3.1770
26.34	11.04	0.0025	3.1919
26.44	11.14	0.0039	3.2066
26.54	11.24	0.0057	3.2213
26.64	11.34	0.0079	3.2360
26.72	11.42	0.0099	3.2476

Orifice Equation

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$\text{Diameter (in)} \quad 6.083333$$

$$\text{Area (ft}^2\text{)} = 0.201842$$

$$g = 32.2$$

$$H (\text{Ft}) = \text{Depth of water above center of orifice}$$

$$Q (\text{CFS}) = \text{Flow}$$

VOLUME CALCULATIONS

POND 4

Ab - Bottom Of The Pond Surface Area

At - Top Of The Pond Surface Area

D - Water Depth

Dt - Total Pond Depth

C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 6.80$$

$$\text{At} = 533.67$$

$$\text{Dt} = 0.50$$

$$\text{C} = 1053.74$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
17.94	0	0	0.00
20.94	3	0.0005	1.21
21.04	3.1	0.0006	1.23
21.14	3.2	0.0010	1.25
21.24	3.3	0.0016	1.27
21.34	3.4	0.0025	1.29
21.44	3.5	0.0036	1.31

Orifice Equation

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$\text{Diameter (in)} \quad 5.25$$

$$\text{Area (ft}^2\text{)} = 0.15033$$

$$g = 32.2$$

$$H (\text{Ft}) = \text{Depth of water above center of orifice}$$

$$Q (\text{CFS}) = \text{Flow}$$

VOLUME CALCULATIONS

POND 5

Ab - Bottom Of The Pond Surface Area

At - Top Of The Pond Surface Area

D - Water Depth

Dt - Total Pond Depth

C - Change In Surface Area / Water Depth

$$\text{Volume} = \text{Ab} * \text{D} + 0.5 * \text{C} * \text{D}^2$$

$$\text{C} = (\text{At} - \text{Ab}) / \text{Dt}$$

$$\text{Ab} = 13.60$$

$$\text{At} = 91,993.08$$

$$\text{Dt} = 1.00$$

$$\text{C} = 91979.48$$

ACTUAL ELEV.	DEPTH (FT)	VOLUME (AC-FT)	Q (CFS)
18.85	0	0	0.000
24.00	5.15	0.0016	0.720
24.20	5.35	0.0439	0.734
24.40	5.55	0.1707	0.748
24.60	5.75	0.3819	0.762
24.80	5.95	0.6776	0.775
25.00	6.15	1.0577	0.788

Orifice Equation

$$Q = CA \sqrt{2gH}$$

$$C = 0.6$$

$$\text{Diameter (in)} = 3.5$$

$$\text{Area (ft}^2\text{)} = 0.066813$$

$$g = 32.2$$

H (Ft) = Depth of water above center of orifice

Q (CFS) = Flow

Pipe Capacity

Pipe	D (in)	Slope (%)	Area (ft^2)	R	Q Provided (cfs)	Q Required (cfs)	Velocity (ft/s)
CB1 to CB2	8	1	0.35	0.17	1.43	NA	0.00
CB2 to MH1	8	1	0.35	0.17	1.43	0.79	2.26
CB3 to MH1	10	0.6	0.55	0.21	2.01	1.30	2.38
MH1 to MH2	12	0.6	0.79	0.25	3.27	2.09	2.66
MH2 to CB5	12	0.6	0.79	0.25	3.27	2.87	3.65
CB4 to CB5	6	3.81	0.20	0.13	1.30	0.34	1.73
CB5 to Existing 84"	12	0.6	0.79	0.25	3.27	1.04	1.32

Manning's Equation:

$$Q = 1.49/n * A * R^{(2/3)} * S^{(1/2)}$$

A = Area

R = D/4

S = Slope

n = 0.011

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994
INPUT FILE = A:UND-POND.DAT

RUN DATE (MON / DAY / YR) =02 / 19 / 1999
USER NO. = R BOHANN.101

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994
INPUT FILE = A:9795.DAT

RUN DATE (MON/DAY/YR) =02/16/1999
USER NO.= R BOHANN.101

AHYMO SUMMARY TABLE (AHYMO194) - AMAFCA Hydrologic Model - January, 1994						RUN DATE (MON/DAY/YR) =02/16/1999					
						USER NO. = R_BOHANN.T01					
COMMAND		HYDROGRAPH IDENTIFICATION	FROM ID NO.	TO ID NO.	AREA (SQ MI)	PEAK DISCHARGE (CFS)	RUNOFF VOLUME (AC-FT)	RUNOFF (INCHES)	TIME TO PEAK (HOURS)	CFS PER ACRE	PAGE = 1
START											
RAINFALL TYPE= 2											
COMPUTE NM HYD		100.10	-	1	.00251	5.36	.305	2.27657	1.598	3.337	RAIN24= .00
COMPUTE NM HYD		100.20	-	1	.00279	5.95	.338	2.27656	1.598	3.335	PER IMP= 90.00
COMPUTE NM HYD		100.30	-	1	.00038	.82	.046	2.27686	1.598	3.399	PER IMP= 90.00
COMPUTE NM HYD		100.40	-	1	.00072	1.55	.087	2.27671	1.598	3.373	PER IMP= 90.00
COMPUTE NM HYD		100.50	-	1	.01090	23.20	1.323	2.27651	1.598	3.326	PER IMP= 90.00
COMPUTE NM HYD		100.60	-	1	.00071	1.53	.086	2.27673	1.598	3.375	PER IMP= 90.00
START											
RAINFALL TYPE= 1											
COMPUTE NM HYD		110.10	-	1	.00251	3.95	.208	1.55658	1.600	2.463	RAIN6= 1.930
COMPUTE NM HYD		110.20	-	1	.00279	4.39	.231	1.55658	1.600	2.462	PER IMP= 90.00
COMPUTE NM HYD		110.30	-	1	.00038	.61	.031	1.55658	1.600	2.507	PER IMP= 90.00
COMPUTE NM HYD		110.40	-	1	.00072	1.14	.059	1.55658	1.600	2.487	PER IMP= 90.00
COMPUTE NM HYD		110.50	-	1	.01090	17.13	.905	1.55658	1.600	2.456	PER IMP= 90.00
COMPUTE NM HYD		110.60	-	1	.00071	1.13	.059	1.55658	1.600	2.489	PER IMP= 90.00
FINISH											

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*****
* BOB TURNER FORD *
*****
* PONDING CALCULATIONS *
*****
* 100-YEAR, 24-HR STORM (UNDER PROPOSED CONDITIONS) *
*****
*
START TIME=0.0
*
*****
* BASIN 1 *
*****
RAINFALL TYPE=2 RAIN QUARTER=0.0 IN
RAIN ONE=2.01 IN RAIN SIX=2.35 IN
RAIN DAY=2.75 IN DT=0.0333 HR
COMPUTE NM HYD ID=1 HYD NO=100.1 AREA=0.002508 SQ MI
PER A=0.00 PER B=10.00 PER C=0.00 PER D=90.00
TP=-0.24 HR MASS RAINFALL=-1
PRINT HYD ID=1 CODE=1
*
ROUTE RESERVOIR ID=10 HYD NO=501.1 INFLOW ID=1 CODE=24
OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
0.00 0.0000 24.55
0.277 0.0005 27.50
0.286 0.0051 27.70
0.296 0.0189 27.90
0.305 0.0420 28.10
0.313 0.0743 28.30
0.322 0.1158 28.50
0.330 0.1665 28.70
0.337 0.2200 28.88
PRINT HYD ID=10 CODE=1
*
*****
* BASIN 4 *
*****
ROUTE RESERVOIR ID=40 HYD NO=500.4 INFLOW ID=4 CODE=24
OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
0.00 0.0000 17.94
1.21 0.0005 20.94
1.23 0.0006 21.04
1.25 0.0010 21.14
1.27 0.0016 21.24
1.29 0.0025 21.34
1.31 0.0036 21.44
PRINT HYD ID=40 CODE=1
*
*****
* BASIN 5 *
*****
ROUTE RESERVOIR ID=50 HYD NO=500.5 INFLOW ID=5 CODE=24
OUTFLOW(CFS) STORAGE(AC-FT) ELEVATION(FT)
0.000 0.0000 18.85

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